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2	Performance of physically and chemically
3	activated biochars in copper removal from
4	contaminated mine effluents
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25 Abstract

26 The increasing global demand for metals and minerals justifies the intensive study of treatment 27 options for contaminated mine effluents. The present study evaluated the conversion of wood 28 residues into physically and chemically activated biochars, and their subsequent use in the 29 treatment of Cu in synthetic and actual contaminated mine drainage. First, wood residues were 30 converted into biochar by fast pyrolysis. Then, physical (using steam or CO₂) or chemical (using KOH) activation was carried out in a homemade pilot-scale furnace. After activation, highly 31 32 microporous (KOH materials) and micro/mesoporous activated biochars (CO₂ and steam 33 materials) were obtained. Batch adsorption testing was first conducted with synthetic effluents. Results showed that CO₂-activated biochar was the most Cu effective adsorbent (99% removal) 34 at low concentrations (5–20 mg L^{-1}). The mechanisms of Cu²⁺ adsorption involved physical and 35 chemisorption for biochars and CO2-activated biochar, while chemisorption for KOH-activated 36 37 biochars was probably due to the high proportion of functional groups connected to their surface. In multi-metal acid mine drainage, metal adsorption capacities deteriorated for most of 38 39 the materials, probably due to effects of ion competition. However, KOH-activated biochar decreased Cu²⁺ concentrations to below the authorized monthly mean allowed by Canadian law 40 (0.3 mg L⁻¹), and decreased Co, Pb, and Mn concentrations up to 95%. These findings indicate 41 42 that high porosity and oxygenated functional groups connected to the surface of activated 43 biochars are important properties for the enhancement of interactions between carbon materials 44 and metals from mine effluents, as well as for their performance improvement in mine drainage 45 treatment.

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48 Keywords: Activated biochar, adsorption, copper removal, water treatment, actual mine49 effluents

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1. Introduction

51 Current mining activities, which exploit low-grade ore, generate large amounts of waste. The subsequent contamination is associated with air pollution by gases (CO₂, SO₂, NO_x, etc.) 52 53 and particulate matter emissions, solid waste that deteriorates the soil, and contaminated 54 effluents that may reach drinking water systems and pose a risk to humans and wildlife (Dudka 55 and Adriano 1997). The main issue is the exposure of geochemically reactive minerals to air 56 and water, which leads to contaminated mine drainage, either acidic (AMD) or contaminated 57 neutral (CND), as well as to surface and underground water pollution (Nordstrom et al. 2015). 58 Cu mining and smelting are one of the major sources of mine waste. Although Cu is an essential element required for living organisms, its divalent form (Cu²⁺) is potentially toxic and 59 carcinogenic when ingested by aquatic organisms and humans. An excess of Cu leads to 60 61 vomiting, headache, nausea, liver/kidney failure, and respiratory problems (Akar et al. 2009), 62 and can be harmful to soil biota, plants (Lamb et al. 2012), and aquatic ecosystems (Lee et al. 63 2010).

64 Several regulators monitor the levels of Cu in wastewater treatment plants, drinking water, 65 and industrial effluents to certify that the maximum contaminant level should be below a value 66 at which there is no known or expected risk to health. In drinking water, Health Canada fixed the threshold at less than 1 mg L⁻¹ (Health Canada 1992), whereas the maximum authorized 67 monthly mean concentration of Cu should be below 0.3 mg L⁻¹ according to metal mining 68 69 effluent regulations (Environment and Climate Change Canada 1999). Several options are 70 available for the treatment of Cu in water: chemical precipitation, ion exchange, membrane 71 filtration, coagulation/flocculation, electrolytic recovery, reverse osmosis, and adsorption. Each 72 technology has its advantages and limits for an efficient Cu removal from wastewater, but high 73 costs are a common drawback. However, adsorption is an attractive technique due to the 74 availability of cost-effective, sustainable, and eco-friendly bioadsorbents (Sekhula et al. 2012).

Literature reveals that activated carbons are the most appropriate bioadsorbents between algal,
bacterial, agriculture and forest, and fungal and yeast biomass for Cu uptake in water media
(Bilal et al. 2013).

78 Several inexpensive waste precursors have been used for the production of activated 79 carbons, including wood residues, fruit shells, stones, husks, and hulls (Tan et al. 2017). 80 Recently, biochar, a by-product carbon-rich material produced from the thermochemical 81 conversion processes of biomass (e.g., torrefaction, slow to fast pyrolysis, and gasification) has 82 also been tested (Lehmann and Joseph 2015). Although biochar has high carbon content and a 83 high proportion of oxygenated functional groups, it is often characterized by low surface area 84 with a small amount of micropores (Liu et al. 2015). Activation is a widely used technique in 85 which a selective gasification of carbon atoms by physical agents (CO₂ or steam) or chemicals 86 (KOH or H₃PO₄) is performed at increasing temperature (e.g., 900 °C) for the development of 87 materials' porosity (Marsh and Rodríguez-Reinoso 2006). The feedstock, pyro-gasification, and activation operating conditions have significant influence on the resultant activated biochar, 88 89 while highly porous materials with properties similar to activated carbons (e.g., surface areas up to 2500 m² g⁻¹) can be produced. However, an optimization study of the operating conditions 90 91 for the preparation of activated biochars to improve the material porosity is required (Braghiroli 92 et al. 2018a).

The effective sorption of metals by activated biochars made by using different operating conditions and feedstock have been reported in the literature. According to a very recent review (Braghiroli et al. 2018b), the surface functional groups (e.g., carboxylic, phenolic, amino groups), specific surface area, and pore volume (narrow and wide micropores), as well as the optimum pH, are the most important factors in potentially providing more bonding sites for heavy metals interactions with activated biochars. The overall metal removal mechanisms include physical adsorption, electrostatic attraction between positive charges (metals) and

100 negative charges (surface of activated biochar), ion exchange, surface complexation, and metal 101 precipitation (Chowdhury et al. 2012; Adebisi et al. 2017a, 2017b). Hence, the removal of up to 18 mg g⁻¹ of Cu (C₀ from 50 to 100 mg L⁻¹) was reported using KOH-activated fruit peel of 102 mangostene biochar (Hamid et al. 2014). Then, up to 96% of Cu ($C_0 = 63.5 \text{ mg L}^{-1}$) elimination 103 104 using steam-activated soybean straw biochars was published by Lima et al. (2010). The 105 improved efficiency compared to biochars (96 vs. 85%) was associated with increased surface area (up to 793 m² g⁻¹), which eventually facilitated the access of functional groups connected 106 to the surface of activated biochars. High adsorption capacity of Cu (203 mg g⁻¹; C₀ from 0.1 to 107 600 mg L⁻¹) was also attributed to the presence of both carboxylic and phenolic groups on steam-108 109 activated date pit biochars, improving cation exchange and complexation of adsorbent surface-110 metal interactions, as well as greater surface area (1467 m² g⁻¹) for physical sorption (Bouchelta 111 et al. 2012). In another study, steam-activated manure biochar showed high Cu sorption capacity $(104 \text{ mg g}^{-1}; C_0 = 1270 \text{ mg L}^{-1})$ due to the presence of inorganics (e.g., P, S, Ca, Na) that played 112 113 an important role in the development of specific surface functionalities and of multiple interactions between activated biochar' surface and Cu²⁺ ions. It was also reported that metals 114 115 sorption were favored at low pH level (fixed at 4.8), whereas at pH higher than 6, Cu 116 precipitation occurred (Lima et al. 2014).

117 Based on the authors' best knowledge, this study is the first to examine the use of wood 118 residues (white birch and black spruce) for the production of activated biochars in pilot-scale 119 technologies for the treatment of Cu in synthetic and actual mine effluents. Most previous studies evaluated the performance of activated biochars in the removal of very high 120 121 concentrations of Cu from synthetic solutions, but very few studies focused on the use of 122 activated biochar for the removal of multi-metal contaminants from actual mine effluents. 123 According to the circular economy principle (recover and recycle, instead of "take, make, and 124 discard"), the use of wood residues in mine effluent treatment appears to be a winning formula

for both the mining and forestry industries, such as in Abitibi-Témiscamingue, the region of
Québec, Canada, where the present study was conducted.

127 In this context, the objective of the present study is to evaluate the removal efficiency of 128 physically and chemically activated biochars made from wood residues for the treatment of Cu 129 in synthetic effluent and actual AMD.

130

131 **2. Materials and methods**

132 2.1 Material sampling and synthesis of biochar and activated biochar

133 White birch (WB) and black spruce (BS) residues were sampled from sawmills located in 134 the Abitibi-Témiscamingue region, Québec, Canada. More details on wood residues 135 preparation, CarbonFX fast pyrolysis technology, and pilot-scale activation furnace are 136 available elsewhere (Braghiroli et al. 2018a). In summary, biochars were produced at 454 °C in 137 an oxygen-free environment using the CarbonFX fast pyrolysis technology developed by Airex 138 Energy Inc. (Bécancour, QC, Canada). The resulting biochars made from WB and BS residues 139 were activated in a homemade pilot oven. Three types of activating agents were used for the 140 production of activated biochars: KOH, CO₂, and steam. In chemical activation, 100 g of each 141 biochar were mixed with 200 g of distilled water and 100 g of KOH, and left in the fume hood 142 for 2 h. Then, the mixture was left in an oven at 120 °C overnight. The impregnated biochar was then placed in the feed hopper; and when the furnace reached 900 °C in a N₂ atmosphere, 143 144 the material was transported into the furnace by a screw conveyor (driven by an electronic 145 engine) to the recovery hopper. The same procedure was carried out in physical activation, in which the flowing gas of CO₂ (3 L min⁻¹) or steam (0.3 L min⁻¹) was introduced when the 146 147 temperature reached 900 °C. The raw biochars were labelled BWB and BBS, while activated biochars depending on the type of activation agent, were labelled as e.g., CO2BWB, KOHBWB,or H2OBBS.

150 2.2 Physical and chemical characterization of biochar and activated biochar

151 Biochars and activated biochars were characterized for their physicochemical parameters: 152 pH, elemental composition (C, H, N, S, O), morphology, surface chemistry, specific surface 153 area, and pore volume. The pH of activated biochars was determined according to a standard 154 test method (ASTM D3838 - 05(2017)) using a SevenMulti, Mettler Toledo (Greifensee, 155 Switzerland) equipped with Inlab Routine Pro electrode. Elemental composition of all materials 156 was determined in a CHNS elemental analyzer, Perkin Elmer 2400 CHNS/O Analyzer 157 (Waltham, MA, USA), by combustion of the samples in a stream of pure O₂. The morphology of biochars and activated biochars was investigated with a JEOL JSM-5500 (JEOL USA, Inc., 158 159 Peabody, MA, USA) Scanning Electron Microscope (SEM), after metallization. X-ray 160 photoelectron spectroscopy (XPS) spectra were recorded with a Kratos AXIS ULTRA system 161 (Wharfside, MA, UK) equipped with a channel electron multiplier detector. The XPS core level 162 spectra were analyzed with Casa software.

163 Micromeritics ASAP 2460 automatic apparatus (Norcross, GA, USA) was used for 164 obtaining N₂ adsorption/desorption isotherms of porous materials at -196 °C. The data were then treated for measuring surface area, S_{BET} (m² g⁻¹), calculated by the Brunauer-Emmett-Teller 165 (BET) model (Brunauer et al. 1938); micropore volume, $V_{\mu, N2}$ (cm³ g⁻¹), determined by the 166 167 Dubinin-Radushkevich (DR) equation (Dubinin 1989); total pore volume, V_t (cm³ g⁻¹), calculated from the amount of nitrogen adsorbed at the relative pressure of 0.97 (Gregg and 168 Sing 1991); and mesopore volume, V_m (cm³ g⁻¹), calculated by the difference $V_t - V_{\mu, N2}$. 169 Ultramicroporosity was obtained by CO₂ adsorption at 0 °C (V_{μ , CO₂} (cm³ g⁻¹)) and the pore size 170 171 distribution (PSD) was determined by application of density functional theory (DFT) using N₂ 172 adsorption isotherms (Tarazona 1995).

173 2.3 Adsorption kinetics experiments

174 Kinetic experiments were conducted in 100 mL beakers containing 0.05 g of adsorbent material and 50 mL of synthetic effluent with Cu^{2+} concentration of 100 mg L⁻¹. The 175 supernatants were sampled after predefined intervals at 2, 4, 6, 8, 10, 12, 18, 24, and 48 h. The 176 177 beakers were placed on a multi-position stirring plate, at 500 rpm, and at room temperature (20 178 ± 2 °C). The pH, potential redox (Eh), and dissolved oxygen (DO) of the supernatant were 179 measured in the beginning and on each sample collected. DO and Eh were measured using LDO 180 Hatch and ORP Hach (London, ON, Canada) meters, respectively, with a double junction Ag/AgCl reference electrode. The supernatants were filtered, and the residual metal trace was 181 182 determined by using microwave plasma atomic emission spectroscopy (MP-AES 4200, Agilent 183 Technologies, Mississauga, ON, Canada). This procedure was carried out for all 8 materials, 184 including 2 biochars (BWB and BBS) and 6 activated biochars (CO2BWB, KOHBWB, 185 H2OBWB, CO2BSB, KOHBSB, and H2OBSB).

186 Sorption capacity $q_t (mg g^{-1})$ was calculated with the application of Eq. 1:

187
$$q_t = [C_0 - C_t] \cdot \frac{V}{m} \tag{1}$$

188 where C_0 , C_t , V, and m represent, respectively, the concentrations of Cu in solution (mg L⁻¹) at 189 the initial and at t moment, the total volume of solution (L), and the amount of the material used 190 (g).

The equations of pseudo-first (Eq. 2) and pseudo-second (Eq. 3) order model (Lagergren
1898), and Elovich (Eq. 4) were employed to describe Cu adsorption kinetics.

193
$$\log(q_e - q_t) = \log(q_e) - k_1 \cdot \frac{t}{2.303}$$
(2)

194
$$\frac{1}{(q_e - q_t)} = \frac{1}{q_e} + k_2 t$$
(3)

195
$$q_t = \frac{1}{b} \cdot \ln(ab) + \frac{1}{b} \cdot \ln(t)$$
(4)

where q_e and q_t refer to the amount of Cu adsorbed (mg g⁻¹) at equilibrium and at any time, *t* (h), respectively, and k_1 is the equilibrium rate constant of pseudo-second order adsorption (h⁻¹), and k_2 is the kinetic constant of pseudo-first order adsorption (g (mg h)⁻¹), *a* is the initial adsorption rate (mg (g h)⁻¹), and the parameter 1/b is related to the number of sites available for adsorption.

201 2.4 Adsorption equilibrium experiments

The tests of isotherm adsorption were conducted at different initial Cu concentrations (5, 10, 20, 50, 100, 200, 500, and 1000 mg L⁻¹) under the same conditions as the kinetic experiments. Equilibrium was carried out for 48 h adsorption testing. Sorption capacity q_e (mg g^{-1}) was calculated with Eq. 5, where C_0 , C_e , V, and m represent, respectively, the concentrations of Cu (mg L⁻¹) at the initial and equilibrium solutions, the total volume of solution (L), and the amount of the material used (g). The adsorption (%) was calculated with Eq. 6:

208
$$q_e = [C_0 - C_e] \cdot \frac{V}{m}$$
(5)

209
$$Adsorption(\%) = [C_0 - C_e] \cdot \frac{100}{C_0}$$
 (6)

The equations of Langmuir (Langmuir 1918) and Freundlich (Freundlich 1906) represented
by Eq. 7 and 8, respectively, were employed to describe Cu sorption:

212
$$\frac{C_e}{q_e} = \frac{1}{b \cdot q_{max}} + \frac{C_e}{q_{max}}$$
(7)

213
$$\log q_e = \log k_f + n \cdot \log C_e \tag{8}$$

where C_e and q_e have the same meaning for both equations, q_{max} is the maximum uptake per unit mass of adsorbent (mg g⁻¹), and *b* is the Langmuir constant related to the adsorption energy (L mg⁻¹) while k_f and *n* are Freundlich coefficients.

The constant *b* allows the determination of the R_L equilibrium parameter (Eq. 9) that indicates the shape of the isotherm (at $R_L = 0$, the adsorption is irreversible; $0 < R_L < 1$, the adsorption is favorable; at $R_L = 1$, the adsorption is linear; and at $R_L > 1$, the adsorption is 220 unfavorable):

$$R_L = \frac{1}{1 + b \cdot C_0} \tag{9}$$

222 2.5 Adsorption of Cu in actual mine effluent

223 The actual effluent, containing Cu and other metals, was collected from an operating gold mine located in Abitibi-Témiscamingue, QC, Canada, and preserved at 4 °C, prior to testing. 224 The same testing conditions for the kinetics and isotherms studies of Cu in synthetic effluents 225 226 were also applied for this effluent. The supernatants were filtered, and the residual metals were 227 measured by MP-AES equipment while the pH, Eh, and DO were measured using the same multimeter. Anions $(NO_2^-, NO_3^-, SO_4^{2-}, PO_4^{3-})$ were determined using the ion chromatography 228 229 Dionex ICS-5000 with a capillary column Ionpac AS18 (ThermoFisher Scientific, Waltham, 230 USA).

231 2.6 Geochemical modelling

The thermodynamic geochemical equilibrium model Visual MINTEQ (VMINTEQ) version 3.1 (Visual MINTEQ 2018) was applied to calculate saturation indices (SI) of potential mineral phases present in the AMD. The data on the effluent (e.g., pH, contaminant concentrations) was used to calculate equilibrium distribution of chemical species according to geochemical processes (e.g., precipitation, complexation, ion exchange). If SI < 0, minerals are undersaturated or in a dissolved form; if SI = 0, minerals are at equilibrium; and finally if SI > 0, minerals are oversaturated and might precipitate.

239 2.7 Activated biochar regeneration

240 Chemical regeneration tests were performed with an activated biochar for six cycle 241 adsorption-desorption tests. Adsorption tests were conducted under the same conditions as the 242 isotherm experiments. After sorption, 0.1 g of dried adsorbent was mixed and shaken with 20 243 mL eluents of 0.1 M HNO₃, 0.5 M H₂SO₄, and 1 M HCl, according to Kołodyńska et al. (2017).

244 The desorption was determined using Eq. 10:

245
$$\%D = \frac{C_{des}}{C_0} \times 100\%$$
 (10)

where C_0 and C_{des} (mg L⁻¹) are the initial Cu concentration and the concentration of Cu ions in solution after desorption, respectively.

248

249 **3. Results and discussion**

250 3.1 Physicochemical characterization of the activated biochars

251 SEM images of activated biochars (Fig. 1) show a typical morphology of wood-derived 252 carbons where the original wood structure is maintained. Fast pyrolysis followed by activation 253 leads to the formation of various sizes of pits, holes, and cave-type openings on the carbon 254 structure for all three types of activating agents. The development of narrow and wide pores 255 was noticed, but no clear structural differences were identified across materials physically or 256 chemically activated. The physicochemical properties of biochar and activated biochars are 257 presented in Table 1. Notably, the carbon content of materials made by fast pyrolysis and 258 activation substantially increased, whereas oxygen and hydrogen contents decreased. During 259 the thermal treatment of lignocellulosic and biochar-derived materials, various carbon 260 compounds (e.g., H₂O, CO₂, CO, NH₃, HCN, C_xH_yO_z) are released. With further increase in 261 temperature, compounds with less carbon (e.g., CO₂, CO, NO_x) are continuously released, 262 leading to increased material's carbon content and pore development (Liu et al. 2015).

Biochar activation involves mostly a reaction between the carbon (in biochar molecular structure) and injected CO_2 or steam as seen in Eq. 11 (Boudouard reaction) (Calo and Perkins 1987) and Eq. 12, respectively. In fact, the physical agents will promote the removal of carbon atoms (burn off) from the structure of biochar at high temperatures, causing the development of 267 pores. In chemical activation, the main reaction mechanism (Eq. 13), as proposed by Radovic 268 and Rodriguez-Reinoso (1997), involves the following steps: KOH dehydration to form K₂O; 269 K₂O reduction to metallic potassium (K); K oxidation to form K₂O; and K₂O hydration to form 270 KOH. Chemical activation is considered efficient because different potassium compounds and 271 gases (physical agents) are formed as well as K that penetrates into the biochar structure to 272 expand its framework and porosity. Therefore, before and after activation, materials showed an 273 acid and basic character, respectively. At any type of activation, pH ranged from 8.2 to 10.3 274 (Table 1).

$$C + CO_2 \leftrightarrow 2 CO \tag{11}$$

 $C + H_2 O \leftrightarrow CO + H_2$ (12)

$$277 \qquad 6KOH + 2C \rightarrow 2K + 3H_2 \uparrow + 2K_2CO_3 \qquad (13)$$

278 The oxygen functional groups present on the surface of biochars and activated biochars were 279 investigated by XPS. After deconvolution of C1s peaks, the relative proportions of the 280 functional groups were estimated (Supplementary Material, Table 1S). The two most 281 predominant peaks measured for most of all materials were related to aliphatic/aromatic carbon 282 (C–C, C–H, and C=C), at BE lower than 285 eV (62–76%), and the C–O bond, at BE in a range 283 285.7–287.1 (18–8%). The other peaks (at 286.1–288, and 288–289.4 eV) were then attached 284 to the oxygen-containing moieties, i.e., C=O or O-C-O, and O-C=O, respectively (Lazzarini et al. 2016). KOH-activated biochars had the highest proportion of total oxygenated groups: 285 22.4 and 25.4% for KOHBBS and KOHBWB, respectively, followed by CO2BWB (19.5%), 286 287 H2OBWB (17.9%), CO2BBS (17.5%), and H2OBBS (13.4%). In addition, KOHBBS had a more evenly divided proportion of oxygenated groups-8.1% (C-O bond), 7.9% (C=O or 288 289 O-C-O), and 6.4% (O-C=O) relative to CO2BWB, 12.8, 4.5, and 2.2%, respectively—which 290

291 Analysis of the textural properties of biochars shows that they are highly ultramicroporous, as evidenced by the CO₂ adsorption analysis with low surface areas: 177 and 208 m² g⁻¹ for 292 293 BWB and BBS, respectively. After activation, birch-activated biochars presented highly 294 developed surface areas in presence of KOH, CO₂, and steam, 1700, 881, and 590 and m² g⁻¹, 295 respectively. However, these materials had a porous structure highly different from each other. 296 According to the IUPAC classification (Sing 1985), N₂ adsorption/desorption isotherms at -196 297 °C for KOH-activated biochars are of Type I, characteristic of microporous solids with a narrow elbow at $P/P_0 = 0.05$ and a horizontal plateau (Fig. 1S a). For the other materials, the N₂ 298 299 isotherms are a combination of Type I and Type IV, with an important nitrogen uptake at relative 300 pressures $P/P_0 < 0.01$. This indicates the existence of a well-developed narrow microporosity, 301 and a slight slope up to $P/P_0 = 0.9$. The development of wider microporosity and mesoporosity 302 with the presence of a narrow hysteresis loop is hence confirmed. PSDs obtained by DFT (Fig. 303 1S b) are in good agreement with results obtained from N₂ isotherms. No pics higher than 2 nm 304 were observed for highly microporous KOH-activated biochars (i.e., 0% mesoporosity), 305 whereas the other materials presented two pics: one in micropore range (< 2 nm), and the other 306 in mesopores (10–50 nm).

307 3.2 Adsorption kinetics

The kinetics of adsorption describe the rate of Cu²⁺ ions uptake on biochar-derived 308 materials. The adsorption capacity of Cu^{2+} increased with time for all materials (Fig. 2). The 309 310 adsorption equilibrium was reached for most of materials at 24 h testing. Thereafter, it reached a plateau, which indicates that no additional Cu^{2+} was removed from the synthetic effluent at 311 100 mg L⁻¹. The Cu²⁺ adsorption capacity for CO2BWB increased 5 times (~49 mg L⁻¹) 312 compared to biochars ($\sim 10 \text{ mg L}^{-1}$). The adsorption capacities of biochar-derived materials for 313 Cu^{2+} varied according to the following sequence: CO2BWB < KOHBBS < H2OBWB < 314 315 KOHBWB ~ CO2BBS < H2OBBS < BBS ~ BWB.

The experimental data for the adsorption of Cu²⁺ onto biochar-derived materials were 316 317 interpreted with the kinetic models (pseudo-first and pseudo-second order, and Elovich's 318 equation) to evaluate the controlling mechanism of adsorption process. The derived kinetic 319 parameters of these models (Table 2) show that experimental data obtained from biochars and activated biochars do not follow the pseudo-second kinetic model as evidenced by R^2 320 321 coefficients between 0.02 and 0.72. Biochars and CO₂-activated biochars best fit the pseudofirst ($R^2 = 0.79-0.99$) and Elovich models ($R^2 = 0.82-0.97$), whereas steam and KOH-activated 322 biochars best defined the adsorption process of the Elovich kinetic model as evidenced by R^2 323 324 coefficients: 0.67-0.95. These results are in agreement with several other metal adsorption 325 systems that have been described by the Elovich equation (Wu et al. 2009).

Pseudo-first model is based on the assumption that physisorption limits the rate of 326 adsorption of Cu²⁺ onto the adsorbent (Lagergren 1898), whereas the Elovich model gives a 327 good correlation on highly heterogeneous surfaces and chemisorptive interaction onto 328 329 materials' surface (Aharoni and Tompkins 1970). These results suggest that physical and chemical interactions may simultaneously contribute and control Cu²⁺ uptake onto biochars and 330 CO₂-activated biochars surfaces, whereas chemisorption is the main adsorption interaction 331 between Cu²⁺ metal ions and activated biochars made with steam and KOH. Physisorption 332 333 involves Van der Waals or electrostatic forces as confirmed by the effect of optimum pH (4.5), while chemisorption involves covalent forces (Xie et al. 2017), which can be formed with active 334 335 oxygenated functional groups as observed by XPS analysis in the prepared materials structure 336 (Chowdhury et al. 2015).

337 3.3 Adsorption isotherms

Biochars and activated biochars were tested for their ability to adsorb Cu in synthetic effluent. Comparative adsorption isotherms of Cu show that activated biochars (e.g., CO2BWB) exhibited almost fivefold higher Cu sorption relative to biochars (Fig. 3 a). The efficiency of Cu removal in synthetic effluents ($C_0 = 5-20 \text{ mg L}^{-1}$) was up to 50%, for biochars, whereas it varied from 95 to 99%, for activated biochars (Fig. 3 b). In addition, Cu removal for all materials deteriorated with increases in initial concentrations. For example, CO2BWB decreased more than four times (from 99 to 24%), when initial concentrations increased (from 5 to 200 mg L⁻¹, respectively).

346 Langmuir and Freundlich, two widely used isotherm models, were applied to describe the 347 sorption of Cu by biochars and activated biochars (Table 3). The Langmuir model describes the 348 monolayered adsorbents on the homogeneous surface (Langmuir 1918), whereas the Freundlich 349 model indicates that the adsorption would take place on a heterogeneous surface (Freundlich 1906). According to the correlation coefficients (R^2) listed in Table 3, the experimental data fit 350 Freundlich ($R^2 = 0.77-0.94$) better than Langmuir ($R^2 = 0.15-0.92$), although the separation 351 factor (R_L) lower than 1 suggests that Cu^{2+} adsorption on biochar-derived materials is a 352 353 favorable process. This result is consistent with the kinetic studies, in which data matched the Elovich model, i.e., based on chemisorption process. 354

With an increase of Cu concentration to up to 1000 mg L⁻¹, KOHBBS showed the greatest 355 adsorption capacity: q_{exp} and q_{max} obtained from experiments and predicted based on Langmuir 356 model, respectively, were 137 and 132 mg g⁻¹. Ion exchange and complexation are the most 357 358 important mechanisms associated with Cu uptake by adsorbents (Baccar et al. 2009; Bouchelta 359 et al. 2012; Bilal et al. 2013). Hamid et al. (2014) reported that Cu was mainly adsorbed by chemical interactions with active functional groups present on the surface of the KOH-activated 360 361 fruit peel of mangostene biochar. Indeed, KOHBBS presented a great and evenly divided 362 proportion of oxygenated groups (phenolic, carboxylic, aldehyde or ether), which improve the 363 cation exchange capacity and complexation properties of these adsorbents in addition to the 364 greater specific surface area and microporosity.

A comparison of adsorption capacity of Cu²⁺ on different activated biochars in the available 365 366 literature (Table 4) shows that higher adsorption capacities of activated biochar (even better 367 than commercial activated carbon) are attributed to several factors, as mentioned before, such as physicochemical properties (high specific surface area, pore size, type of functional groups 368 connected to the materials surface), high affinity between carbon material and Cu^{2+} , optimum 369 370 pH, increasing carbon (g): contaminant (mL) ratio, and high initial Cu concentration used. The 371 comparable adsorption capacity of materials made in this study with other adsorbents reveals 372 that physical and chemical activated biochar made from wood residues is suitable for the removal of Cu²⁺ since it has a relatively high adsorption capacity. 373

374 3.4 Cu removal in actual AMD

The initial concentration of Cu^{2+} in actual AMD (1.75 mg L⁻¹) collected from an operating 375 376 mine site largely exceeded the maximum authorized monthly mean concentration of Cu (0.3 mg L⁻¹) allowed by the Canadian law (Environment and Climate Change Canada 1999). For most 377 of biochar-derived materials, the removal of Cu²⁺ was not significant, and varied from 17 to 378 379 56% (Fig. 4). The only material for which Cu removal topped 99% was KOHBBS. The sorption 380 of the activated biochar seems to be unaffected by the nature of the precursor (WB or BS). 381 Rather, it is associated with increased surface area (highly porous materials) and improved 382 access of functional groups connected to the surface of activated biochars that may have 383 improved the interactions between Cu and the surface of the material. KOHBBS also exhibited 384 the highest adsorption capacity in synthetic effluents at very high Cu concentrations.

Comparing the composition of AMD before and after adsorption onto KOHBBS (Table 5), it was noticed that pH, Eh, and DO of the effluent did not vary significantly, but metal adsorption capacities were reduced (Fig. 4) relative to single-metal synthetic effluent, probably due to multi-metal competition from an actual effluent onto KOHBBS (Mohan and Chander 2001, 2006). In addition to Cu removal, other metals were also removed in presence of KOHBBS, including Co, Fe, Mn, Na, Pb, and Zn (Table 5). Among these metals, Co and Pb had the highest removal efficiency of 95 and 43%, respectively, although a significant increase of K is probably coming from the KOH activation during the production of activated biochar. Therefore, a decrease of metals concentration was observed in presence of activated biochar, even though a pre- and/or post-treatment is required to reduce the level of metal concentrations (e.g., Mn, Zn, Fe) to meet Canadian regulations (see q_{exp} in Table 3).

396 Metals can form soluble and precipitate complexes, but to precipitate them from water, the pH must range from 6 to 9, although Fe^{3+} can precipitate at pH higher than 3.5 (Ríos et al. 2008). 397 398 According to VMINTEQ geochemical modelling, oversaturation and possible precipitation for 399 MnHPO₄ was performed in initial AMD, whereas all metals in AMD after sorption onto 400 KOHBBS were undersaturation. Ríos et al. (2008) employed a significant zeolite: effluent ratio 401 (5 g:100 mL) for the treatment of AMD, which increased the pH of the system, and, 402 consequently, metal concentrations decreased probably due to precipitation on the surface of 403 zeolite. According to Table 1, all materials, including KOHBBS, exhibited an acid character, so 404 precipitation of certain solid phases on the surface of the ion exchanger might not be promoted. 405 However, precipitation also depends on metal concentration, temperature, the existence of 406 metals and anions, and time to thermodynamic equilibrium (Cuppett 2006). In the study, at such 407 low adsorbent: effluent ratio (0.1 g:100 mL), the pH was maintained at very low value (2.6); 408 thus, the presence of a precipitate was not obvious.

409 3.5 Regeneration of activated biochar

The feasibility of the adsorption technology on an industrial scale depends on the reusability of spent activated biochar. In addition, chemical regeneration is largely used for desorbing inorganic contaminants, especially metals. Desorption experiments were carried out in order to estimate the metal releasing capacity of an activated biochar loaded with Cu^{2+} . Three types of acid eluents were applied for Cu desorption: HNO₃, H₂SO₄, and HCl at different 415 concentrations 0.1, 0.5, and 1 M. By comparing the three eluents, HNO₃ was found to be the 416 most efficient, even if used at the lowest concentration, followed by HCl and, finally, H₂SO₄. 417 Under strong acid condition, the surface of the sorbent is in a protonated form, which allows 418 desorption of positively charged ions. In the first adsorption-desorption cycle, desorption 419 efficiency was found to be 99.6, 99.2, and 98.6%, respectively (Fig 5. a). After the six 420 regeneration cycles (Fig. 5 b), the efficiency of Cu desorption was reduced to 76.2, 51.4, and 421 36.2% using HNO₃, H₂SO₄, and HCl, respectively. These results suggest that activated biochar 422 made from wood residues has high regenerability, more stable Cu desorption efficiency with 423 HNO₃ compared to the other two acid eluents, and suitability for a minimum of at least six 424 successive adsorption-desorption cycles.

425

426 **4. Conclusion**

427 Activated biochars were produced from wood residues using physical (steam and CO₂) 428 and chemical (KOH) processes. The experimental data revealed that Cu removal depends on 429 the physicochemical characteristics (e.g., high surface area and porosity, and oxygenated 430 functional groups connected to materials surface) of the sorbent material as well as the effluent type (single or multi-metal) and initial metal concentrations ($C_0 < 2 \text{ mg } L^{-1}$ or $C_0 \ge 5 \text{ mg } L^{-1}$). 431 432 CO₂-activated biochar showed better efficiency for Cu in synthetic effluent at up to 200 mg L⁻ 433 ¹, whereas KOH-activated biochar was the most efficient material for Cu from high concentration synthetic effluent (1000 mg L⁻¹) and from multi-metal actual effluent. Elovich 434 435 kinetic and Freundlich isotherm models were found to fit the experimental data, indicating that 436 chemical interactions of oxygenated functional groups with Cu on the heterogeneous surface 437 might be occurring. The desorption of Cu ions was successfully carried out through chemical 438 regeneration with HNO₃, which was the most efficient approach, even after six adsorption-439 desorption cycles, relative to H₂SO₄ and HCl. Therefore, wood residues seem to be an attractive 440 precursor for the production of activated biochar for remediating Cu present in actual mine 441 effluent. However, a pre- and/or post-AMD treatment would be required to reduce high levels 442 of other metals such as Fe, Al, and Mn according to the fixed Canadian thresholds for mine 443 effluent.

444

445 Acknowledgments

446 This research was funded by the Québec's Ministry of Economy, Science and Innovation 447 (Ministère de l'Économie, de la Science et de l'Innovation du Québec), the Natural Sciences 448 and Engineering Research Council of Canada (NSERC), the Canada Research Chairs Program, 449 the College of Abitibi-Témiscamingue, and the Technology Centre for Industrial Waste (Centre 450 Technologique des Résidus Industriels) through its partners on this project, Airex Energy and 451 Iamgold Corporation. The first author, Dr. Flavia Lega Braghiroli, also sincerely acknowledges 452 NSERC financial support via a Banting Postdoctoral Fellowship (2017–2019). The authors also 453 thank Anne-Marie Marleau Claveau, Félicia Porqueres, Maéva Giasson, Gilles Villeneuve, 454 Mamadou Dia, Nicolas Bergeron and Hélie Jacob Turmel for their assistance with experiments, 455 analysis and testing in the laboratory.

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631	Table captions
632	Table 1. Textural and physicochemical properties of biochars and activated biochars
633	Table 2. Kinetic parameters obtained from the adsorption of Cu onto biochars and activated
634	biochars
635	Table 3. Parameters of Cu adsorption isotherms onto biochars and activated biochars
636	Table 4. Comparative sorption capacity of activated biochars and commercial activated carbon
637	for Cu ²⁺ in water
638	Table 5. Composition (mg L ⁻¹ , except for pH and Eh) of initial and final (after adsorption with
639	KOHBBS) AMD
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656 Figure captions

657	Fig. 1. SEM images of activated biochars prepared from WB and BS wood residues in presence
658	of CO ₂ (a and b); steam (c and d); and KOH (e and f)
659	Fig. 2. Adsorbed amounts of Cu^{2+} at initial concentration of 100 mg $L^{-1}(q_t)$ as function of time
660	for both biochars: () RWB, () BS; and activated biochars: (\triangle CO2BWB, (\blacktriangle)
661	CO2BBS, (O) H2OBWB, (•) H2OBBS, (□) KOHBWB, and (■) KOHBBS
662	Fig. 3. a) Adsorbed isotherms of Cu^{2+} , and b) Cu^{2+} adsorption (%) as function of different initial
663	concentrations of Cu^{2+} ($C_0 = 5$, 10, 20, 50, 100, and 200 mg L ⁻¹) for both biochars: ()
664	BWB, () &BS and activated biochars: () CO2BWBA() CO2BBS, () H2OBWBO(
665) H2OBBS, (\bullet) KOHBWE and () KOHBBS
666	Fig. 4. Adsorbed Cu ²⁺ from real effluent (mg L ⁻¹) as function of the contact time for both
667	biochars: (◊) BWB, (♦) BBS; and activated biochars: (△) CO2BWB, (▲) CO2BBS, (○)
668	H2OBWB, (•) H2OBBS, (□) KOHBWB, and (■) KOHBBS
669	Fig. 5. Desorption efficiency of Cu^{2+} ions after a) chemical regeneration using three different
670	eluents: HNO3 0.1 M, H2SO4 0.5 M, and HCl 1 M, and b) after six cycles adsorption-
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	BWB	BBS	CO2BWB	CO2BBS	H2OBWB	H2OBBS	KOHBWB	KOHBBS
Textural properties								
$S_{BET} (m^2 g^{-1})$	177*	208*	881**	735**	590**	412**	1700**	1662**
$V_t (cm^3 g^{-1})$			0.53	0.39	0.34	0.18	0.75	0.72
$V_{\mu,N2}(cm^3g^{1})$			0.33	0.28	0.23	0.17	0.75	0.72
$V_{\mu,CO2}(cm^3~g^{1})$	0.11	0.14	0.28	0.20	0.22	0.20	0.36	0.45
$V_{m} (cm^{3} g^{-1})$			0.20	0.11	0.11	0.01	0.00	0.00
Physicochemical properties								
pH	5.0	6.7	10.2	10.3	9.9	9.3	8.2	9.3
C (%)	75.4	75.4	89.9	88.9	89.1	83.8	77.5	80.1
H (%)	3.5	3.8	0.9	0.6	0.6	0.8	1.7	1.0
N (%)	0.9	0.9	0.4	1.2	0.2	0.8	2.0	2.7
S (%)	0.5	0.5	0.0	0.1	0.0	0.0	0.1	0.0
O° (%)	19.7	19.4	8.8	9.2	10.1	14.6	18.7	16.2

Table 1. Textural and physicochemical properties of biochars and activated biochars

 S_{BET} obtained from *CO₂ and **N₂ adsorption analysis; °O content was obtained by difference (O% = 100 – CHNS%)

		Pseudo-first order			Pseu	do-second or	der	Elovich's equation			
		$q_{exp.} \ (\mathrm{mg \ g^{-1}})$	$q_e \pmod{(\mathrm{mg \ g}^{-1})}$	k_l (h ⁻¹)	R^2	$q_e \pmod{(\mathrm{mg \ g^{-1}})}$	<i>k</i> ₂ (mg (g h) ⁻¹)	R^2	<i>a</i> (mg (g h) ⁻¹)	1/b (mg g ⁻¹)	R^2
	BWB	10.04	9.09	0.04	0.79	4.78	0.0041	0.65	2.79	2.43	0.82
	BBS	9.98	10.81	0.05	0.99	14.14	0.0093	0.72	2.22	2.06	0.97
	CO2BWB	48.91	33.99	0.081	0.92	35.71	0.0049	0.51	$2.17.10^{1}$	11.51	0.92
	CO2BBS	25.25	23.96	0.072	0.83	11.4	0.0018	0.33	$1.13.10^4$	2.04	0.96
	H2OBWB	24.90	8.86	0.058	0.61	10.16	0.0029	0.27	$2.07.10^{1}$	4.55	0.95
	H2OBBS	19.18	7.95	0.061	0.56	3.80	0.024	0.12	7.83	4.90	0.67
	KOBBW	25.15	9.08	0.069	0.66	7.40	0.0132	0.06	$1.08.10^{3}$	2.70	0.73
	KOHBBS	36.71	7.61	0.053	0.70	9.51	0.0023	0.02	9.79.10 ²	4.07	0.95
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Table 2. Kinetic parameters obtained from the adsorption of Cu onto biochars and activated

biochars

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		<i>k</i> _f	п	R^2	$q_{exp} (\text{mg g}^{-1})$	q_{max} (mg g ⁻¹)	<i>b</i> (L mg ⁻¹)	R_L	R^2
-	BWB	1.16	0.52	0.82	85	120	0.001	0.45-0.99	0.15
	BBS	1.45	0.60	0.88	77	105	0.001	0.45-0.99	0.21
	CO2BWB	17.66	0.26	0.90	127	127	0.016	0.06-0.93	0.92
	CO2BBS	5.82	0.34	0.89	98	102	0.005	0.16-0.98	0.73
	H2OBWB	11.11	0.26	0.80	122	132	0.005	0.15-0.97	0.77
	H2OBBS	5.45	0.30	0.77	101	100	0.003	0.22-0.98	0.51
	KOBBWB	10.80	0.26	0.86	105	109	0.006	0.14-0.97	0.73
	KOHBBS	17.51	0.23	0.94	137	132	0.009	0.10-0.96	0.81
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Table 3. Parameters of Cu adsorption isotherms onto biochars and activated biochars

Table 4. Comparative sorption capacity of activated biochars and commercial activated carbon

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Activated biochar precursor	gAC:mL	pН	Activation/ S _{BET} (m ² g ⁻¹)	qmax (mg g ⁻¹)	Kinetic/ Isotherm model	C₀ (mg L ⁻¹)	References
Soybean straw	1:100	4.8	Steam (up to 793)	96% removal	-	64	(Lima et al. 2010)
Date pits	0.1:100	-	Steam (1467)	203	Langmuir	600	(Bouchelta et al. 2012)
Waste peels of mangosteen fruits	0.4:100	5.5	CO ₂ /KOH (367)	19	Pseudo-second order; Langmuir and Freundlich	50-100	(Hamid et al. 2014)
Broiler litter Broiler cake	1:100	4.8	Steam (up to 425)	104 49	_	2690	(Lima et al. 2014)
Miscanthus plant	0.2:100	6	Steam (322)	14	Two-compartment model; Langmuir	0.2-150	(Shim et al. 2015)
Colocasia esculenta roots	0.06:100	5	Steam (102)	2.3	Pseudo-second order; Langmuir	30	(Banerjee et al. 2016)
Hickory chips	_	5	NaOH (873)	54	-	2-250	(Ding et al. 2016)
Pine sawdust	0.025:100	4.5	H ₃ PO ₄ (900)	2	Freundlich	1-10	(Peng et al. 2017)
White birch	0.1:100	4.5	CO ₂ (880)	127	Elovich, Freundlich	5-1000	Present study
Black spruce	0.1:100	4.5	KOH (1662)	137	Elovich, Freundlich	5-1000	Present study
NORIT C GRAN	1:100	4.8	H ₃ PO ₄ (624)	56	-	1270	(Wilson et al. 2006)

Table 5. Composition (mg L⁻¹, except for pH and Eh) of initial and final (after adsorption with

753 KOHBBS) AMD

Parameter	Initial AMD	Final AMD	Removal (%)
pН	2.70	2.60	-
Eh (mV)	584	548	-
Dissolved oxygen	10.0	7.90	-
Al	141	145	0
Ca	466	468	0
Cd	< 0.05	< 0.05	0
Со	9.38	0.502	95
Cr	0.067	0.093	0
Cu	1.753	0.0055	99
Fe	468	405	13
K	4.41	24.9	0
Mg	131	138	0
Mn	10.9	9.72	11
Na	57	52.5	8
Ni	0.367	0.605	0
Pb	0.143	0.0813	43
Zn	4.92	4.62	6
NO ₂ -	16	16.3	0
NO ₃ -	750	726	3
SO4 ²⁻	2390	2411	-
PO ₄ ³⁻	16.1	12.1	25