



Environmental implications of biohydrogen based energy production from steam reforming of alcoholic waste

Antonio Cortés, Gumersindo Feijoo, Antonio Chica, Javier Francisco Da Costa-Serra, María Teresa Moreira

Accepted Mansucript

How to cite:

Cortés, A., Feijoo, G., Chica, A., Da Costa-Serra, J., & Moreira, M. (2019). Environmental implications of biohydrogen based energy production from steam reforming of alcoholic waste. Industrial Crops And Products, 138, 111465. doi: 10.1016/j.indcrop.2019.111465

Copyright information:

© 2019 Elsevier Ltd. This manuscript version is made available under the CC-BY-NC-ND 4.0 license (http://creativecommons.org/licenses/by-nc-nd/4.0/)

1	Environmental implications of biohydrogen based energy production from steam reforming
2	of alcoholic waste
3	Antonio Cortés ^a , Gumersindo Feijoo ^a , Antonio Chica ^b , Javier Francisco Da Costa-Serra ^b and
4	María Teresa Moreira ^{a*}
5	^a Department of Chemical Engineering, School of Engineering, Universidade de Santiago de
6	Compostela, Rúa Lope Gómez de Marzoa, s/n, 15782 Santiago de Compostela (Spain)
7	^b Institute of Chemical Technology, Universitat Politècnica de València-Consejo Superior de
8	Investigaciones Científicas, Avd. de los Naranjos s/n, 46022 València (Spain)
9	* Corresponding author
10	E-mail: maite.moreira@usc.es
11	
1 7	
12	Abstract
13	Nowadays, there is an increasing demand for energy in the world. With an energy system still
14	based on fossil fuels, a paradigm shifts towards clean energy production based on available
15	renewable resources is necessary. Hydrogen is a high-quality energy carrier that can be used
16	with great efficiency and is expected to acquire a great importance in the next generation of
17	fuels. This study aims to analyze the potential environmental impacts associated with the
18	steam reforming of alcoholic waste from distilleries to produce clean electricity by using the
19	Life Cycle Assessment methodology. The main findings from this study reported that the global
20	environmental profile is better than other alternatives more common as sanitary landfill or
21	incineration. In terms of some impact categories as Abiotic and Ozone Depletion, Acidification
22	and Eutrophication, steam reforming of alcoholic waste performed better profiles than other
23	processes that produce hydrogen from diverse feedstocks.

24 Keywords: Alcoholic waste; Environmental profile; LCA; SOFC; Biohydrogen

25 Abbreviations

LCA	Life Cycle Assessment
SS	Subsystem
CC	Climate change
OD	Ozone depletion
ТА	Terrestrial acidification
FE	Freshwater eutrophication
ME	Marine eutrophication
HT	Human toxicity
POF	Photochemical oxidant formation
PMF	Particulate matter formation
TET	Terrestrial ecotoxicity
FET	Freshwater ecotoxicity
MET	Marine ecotoxicity
FD	Fossil depletion
WW	Wastewater
WGS	Water Gas Shift
PSA	Pressure Swing Adsorption
ISO	International Organization for Standardization

26

27 1. Introduction

28 Currently, global energy production is based on the use of fossil fuels such as coal, oil and 29 natural gas (Rossetti et al., 2015a) and accounts for approximately 65% of global GHG 30 emissions (Uusitalo et al., 2017). Dependence on the use of fossil fuels as an energy resource 31 has caused environmental problems of global impact, such as air pollution in terms of emission 32 of pollutants and particles, as well as the depletion of natural resources, among others (Hajjaji 33 et al., 2016; Reyes-Valle et al., 2015), which leads to adverse consequences for society in terms 34 of human health and damage to the ecosystem (Valente et al., 2019). So much so that the 35 2030 Agenda and the 17 Sustainable Development Goals (SDGs) set by the United Nations

includes ensuring access to affordable, reliable and sustainable energy for all. This objective
aims at guaranteeing universal access to energy service, substantially increasing the share of
renewable energy in the global energy mix and doubling the rate of improvement in energy
efficiency. This is why the paradigm shift towards clean energy production must be based on
available renewable resources (Da Costa-Serra and Chica, 2018).

41 In recent years, numerous alternatives to the use of traditional fossil fuels have been 42 proposed, such as the production of biofuels, bioalcohols, hydrogen or any type of renewable 43 energy (Balat, 2011). In particular, biomass is one of the renewable energy sources that has 44 experienced strong growth in recent years, due to its global availability and diversity (Spiridon 45 et al., 2016; Tian et al., 2018). Biofuels derived from biomass offer a number of advantages 46 over their oil-based counterparts according to Demirbas (2008): they can be considered carbon 47 neutral after-combustion by fixing carbon during biomass growth, close to a carbon-neutral 48 balance, so that they contribute to achieving sustainability goals. For this reason, numerous 49 initiatives have been developed in the development of conversion technologies based on 50 resources derived from biomass (Unrean et al., 2018).

Focusing on the different types of fuels, hydrogen is a high quality energy carrier that can be used with high efficiency (Frolov et al., 2013) and is expected to acquire great importance in next generation fuels (Alipour-Moghadam et al., 2014). This fact, together with declining fossil fuel reserves, steadily rising prices and increasing pollution make hydrogen a very attractive product for meeting global energy demand (Khaodee et al., 2011).

However, the environmental profile of hydrogen-based energy systems is as "clean" or "dirty"
depending on the scheme of conversion (Rabenstein and Hacker, 2008). The traditional
schemes producing H₂ from natural gas are a major source of CO₂, with emissions of
approximately 10-12 kg of CO₂ per kg of H₂ (Spath and Mann, 2001). Traditional plants produce
hydrogen by catalytic steam reforming of natural gas, which is a mature technology and is the

pathway by which most hydrogen is produced today. Because of this, reducing CO₂ emissions
associated with hydrogen production would result in a considerable reduction of pollution
(Salkuyeh et al., 2018).

In this sense, fuel cells technology and the use of hydrogen are proposed as one of the most promising environmental solutions in relation to the reduction of global emissions (Díaz Alvarado and Gracia, 2010). Fuel cells are devices that electrochemically convert chemical energy from fuels into electricity (Morales et al., 2010). Among the different types of fuel cells, the Solid Oxide Fuel Cell (SOFC) is the most efficient, due to its high operating temperatures and the fact that it is not poisoned with CO (Hernández and Kafarov, 2009). When this type of battery is used, an efficiency around 50% can be obtained (Strazza et al., 2015); in addition, an

efficiency of 70% can be achieved if cogeneration system is used (Strazza et al., 2010).

72 Hydrogen production from renewable sources such as poplar (Susmozas et al., 2016) or willow 73 wood (González-García et al., 2012), sugar cane (Halleux et al., 2008), sweet potato (Costa et 74 al., 2018), sorghum (Aguilar-Sánchez et al., 2018) or sugar beet (Luo et al., 2009) have been 75 investigated as the first actions to achieve a significant reduction of environmental impacts 76 (Salkuyeh et al., 2018). Hydrogen can be obtained from different feedstocks through steam 77 reforming (Braga et al., 2016; López et al., 2019; Zheng et al., 2019), autothermal reforming 78 (Khila et al., 2017; Spallina et al., 2018; Xue et al., 2017) and aqueous phase reforming 79 (Coronado et al., 2018; Esteve-Adell et al., 2017; García et al., 2018), among them, steam 80 reforming is the most common, as almost 90% of H₂ is produced by natural gas reforming. It 81 also has the highest conversion efficiency, around 70% (Haryanto et al., 2005). 82 Steam reforming of natural gas is the most popular method for producing commercial 83 hydrogen that currently covers about 50% of global hydrogen demand (Anzelmo et al., 2018) 84 and is sometimes referred to as steam methane reforming (SMR). Steam reforming is an 85 endothermic process based on the reaction of gas with steam at high temperature and

86 moderate pressure. In this way, the chemical reaction taking place leads to hydrogen and

87 carbon dioxide (Reaction 1):

88
$$CH_3CH_2OH + H_2O \rightarrow 2CO_2 + 6H_2$$
 $\Delta H_r = 174 \text{ kJ mol}^{-1}$ (1)

However, depending on the reaction mixture and operating conditions in the reactor, another
route can be followed, producing undesirable products (Ni et al., 2007), such as carbon
monoxide (Reaction 2), methane (Reaction 3) or ethylene (Reaction 4):

92
$$CH_3CH_2OH + H_2O \rightarrow 2CO + 4H_2$$
 $\Delta H_r = 256 \text{ kJ mol}^{-1}$ (2)

93
$$CH_3CH_2OH \rightarrow CO + CH_4 + H_2$$
 $\Delta H_r = 50 \text{ kJ mol}^{-1}$ (3)

94
$$CH_3CH_2OH \rightarrow C_2H_4 + H_2O$$
 $\Delta H_r = 46 \text{ kJ mol}^{-1}$ (4)

Once the process is complete, the output stream must undergo purification treatment to avoid
the presence of by-products such as methane and carbon monoxide. The removal of CO is an
important step because it normally poisons the catalyst in fuel cells, that is why CO is removed
first by the Water Gas Shift (WGS) reaction (Reaction 5). WGS is an exothermic and reversible
reaction usually used in industry to produce high purity hydrogen (Alamolhoda et al., 2019).
Normally, 90% of the CO outflowing from the steam reforming reactor can be converted to
CO₂ (Rossetti et al., 2015b).

102
$$CO + H_2O \rightarrow H_2 + CO_2$$
 $\Delta H_r = -41 \text{ kJ mol}^{-1}$ (5)

Following this stage, the Pressure Swing Adsorption (PSA) process separates hydrogen from the rest of the components of the gas stream with 85% efficiency, obtaining H₂ with 99% purity (Susmozas et al., 2013), and whose energy content is usually higher than that of the natural gas used for reforming.

The implementation of other alternatives of hydrogen production can be considered from
alternative raw materials, such as alcohols (Rossetti et al., 2015a). In addition to steam
reforming of ethanol, studies have been published on steam reforming of different types of

110 alcohol with the aim of producing hydrogen. Some of these alcohols are butanol (Kumar et al., 111 2018), propanol (Wang et al., 2015), methanol (Tian et al., 2017) or glycerol (Menezes et al., 112 2018) but, even so, the use of ethanol for this purpose offers the best opportunity to produce 113 hydrogen from renewable sources (Ramírez and Homs, 2008), especially if this ethanol is 114 derived as residue from other processes. Specifically, the alcoholic wastes from the wine 115 industry results an attractive raw material due to 65% of world wine production is managed by 116 European winegrowers mostly small and medium-sized wineries according to the Comité 117 Européen des Enterprises Vins (CEEV, 2016). Wine production generates large amounts of solid 118 and liquid wastes, with a serious impact on the environment when they are not adequately 119 treated. The liquid wastes are processed in distilleries to obtain purified alcohols, but in these 120 processes, alcoholic purges without commercial value containing impurities separated from 121 the good quality alcohols are generated. Thus, the process here analysed aims to raise 122 awareness of the potential of these by-products and their valorization activities as a 123 sustainable way to produce hydrogen.

The main objective of the study is to analyze the potential environmental impacts associated with the steam reforming of alcoholic waste from distilleries. Quantifying the consumption of material and energy resources during the life cycle makes it possible to estimate potential changes and emissions to the environment. The main product of the process is hydrogen (H₂), along with a certain amount of carbon monoxide (CO), carbon dioxide (CO₂), methane (CH₄) and ethylene (C₂H₄), which accounts for a proportion lower than 30%. This output stream is used to produce energy in a 3 kW SOFC.

- 131 2. Materials and methods
- 132 2.1. Definition of goal and scope

The Life Cycle Analysis methodology has been considered as a fundamental tool in the analysisof the environmental profile associated with the steam reforming of alcoholic waste from

- distilleries in order to identify key environmental performance indicators. In distilleries, alcohol
- 136 can be extracted from some wines that cannot been marketed. During this distillation process,
- 137 an ethanol-rich fraction is obtained, but also a residual fraction that remains in the distiller's
- tail, which is the residue used in this study.
- 139 Figure 1 presents the block diagram of the process, identifying the system boundaries, the
- 140 different subsystems considered and the main inputs and outputs of the system.
- 141 No infrastructure process was considered in the evaluation, since the environmental impacts
- 142 per process unit, from installation, construction, decommissioning, infrastructure, machinery,
- 143 etc., have been considered negligible during the lifetime of this type of facilities. This has been
- a common practice in other life cycle assessment studies of biorefineries (Jeswani et al., 2015;
- 145 Karlsson et al., 2014). However, this study has taken into account the manufacture of the
- 146 catalyst and the SOFC phase, due to the fact that their useful life is clearly shorter than that of
- 147 large installations.



- 149 **Figure 1.** System boundaries of the reforming system for the valorization of the alcoholic
- 150 waste. Caption: T: Transport; R1: Reforming reactor; T1: Heat exchanger.

The foreground system includes the process units that are the direct object of this study. For
the purposes of the study, three subsystems (SS) have been considered, which are detailed
below:

Subsystem 1: Catalyst formulation. This subsystem considers all the materials necessary for the manufacture of the catalyst used in the reforming reactor (Menor et al., 2017). The catalyst is composed of a sepiolite base with Nickel (15% weight) and Lanthanum (1% weight). Its considered useful life is 20 months, regenerating every 4 months. The transport of the catalyst to the plant is also considered, taking as distance 100 km.

Subsystem 2: Steam reforming. This process includes all the inputs needed to perform the steam reforming process. These inputs are mainly electricity, water and alcohol residues from distilleries. The transport of alcoholic waste to the plant is not included, as this type of facility is designed to be included in the distillery. The waste produced in this subsystem is the catalyst spent at the end of its useful life and is considered 100 km as the average transport to the landfill.

165 Subsystem 3: SOFC. This subsystem includes the net production of electricity in the SOFC using 166 the SS2 gas stream as feed. At the exit of this subsystem, CO_2 and H_2O emissions are derived 167 from the reactions taking place with CO and CH₄, C₂H₄ and H₂ inside the SOFC. The electricity 168 produced is fed into the grid. The SOFC works at a high temperature of around 600°C and 169 produces a large amount of heat, as represented is Figures 1 and 2, this heat is redirected to 170 the system and used to heat the stream entering the reforming reactor. This subsystem 171 includes the SOFC manufacturing stage. Gas stream purifying processes are not included 172 because SOFC are not poisoned by the presence of CO (Hernández and Kafarov, 2009). This 173 type of device directly provides electricity from the chemical reaction taking place. The 174 electrodes of this type of battery are catalytic, so they are relatively stable and are not 175 consumed (Fragiacomo et al., 2018).

The Background System includes the production of raw materials, fuel, chemicals and water
used in the process, as well as the consumption of fuel used in the transportation of materials.
As the basis for the calculation or Functional Unit (FU), the treatment of 1 tonne of alcoholic
waste in the facility was chosen, which will be taken as a reference for all the inputs and
products of the system as well as the emissions, energy consumption and transport associated
with this process (ISO, 2006a, 2006b).

182 The description of the steam reforming process is presented in detail in Figure 2. The waste 183 from the distillery enters the plant with approximately 92% v/v ethanol, to which water is 184 added to reach 80% v/v water and 20% v/ ethanol. The steam-to-carbon molar ratio (S/C ratio) 185 used in most cases is 3:1 (Jeon et al., 2018), but in this case a steam-to-carbon ratio of 6:1 was 186 considered. This steam-to-carbon ratio increases the production of CO_2 and H_2 and reduces the 187 formation of the undesirable products mentioned in Equations 2-4, but increases the heat 188 necessary to vaporize the water/ethanol mixture. However, since this heat is supplied by the 189 residual heat produced in the SOFC, the use of additional fuel is not necessary. The stream 190 passes through a heat exchanger where it is heated up to 600°C, the temperature required for 191 the inlet stream of the reforming reactor. The output of the reactor is a gas stream comprised 192 by H₂, CO₂, CO, CH₄, H₂O and a minor proportion of C₂H₄. This stream is fed to the SOCF, where 193 heat and electricity are produced. The high temperature stream is recycled in the system to 194 heat the water and ethanol feed, reducing energy consumption. The electricity produced is fed 195 into the grid.



Figure 2. Detailed scheme of Subsystem 2, showing the composition of the different streamsand their temperature.

199 2.2. Data acquisition and life cycle inventory

200 Life cycle inventory involves the collection of qualitative and/or quantitative input/output data 201 for the system. In the case of Subsystem 1, catalyst manufacturing data were obtained from a 202 previous study about the formulation of a sepiolite-based catalyst with the addition of Ni 203 (Menor et al., 2017), although the amount of catalyst used is a primary data. In relation to the 204 Steam Reforming Subsystem, all the information on the consumption of the process comes 205 from primary data, except electricity consumption, which was obtained from a study about the 206 life-cycle assessment of biomass gasification as an alternative to steam methane reforming for 207 hydrogen production (Susmozas et al., 2013); where an electric consumption of 1.35 kWh per 208 kg H₂ produced was considered. Finally, the inventory of Subsystem 3 has been obtained from

- 209 various scientific publications. (Strazza et al., 2015, 2010) conducted several studies to assess
- 210 the environmental profile of two SOFC systems: one with 230 kW and other one with 20 kW
- system. (Lee et al., 2015) obtained the environmental impact of a 100 kW SOFC power
- 212 generation system. The different life cycle inventories published in the above-mentioned
- 213 manuscripts were adapted to the characteristics of the battery used in the study. Background
- system processes have been taken from Ecoinvent[®] database. Tables 1-3 present the life cycle
- 215 inventory of the different subsystem considered in this study.
- 216 **Table 1.** Life cycle inventory for Subsystem 1. Catalyst formulation per FU

Inputs from Tecl	nnosphere	Outputs to Technosphere		
Materials	kg	Products	kg	
MiliQ water	2.63	Catalyst to SS2	8.15·10 ⁻²	
Ni(NO ₃) ₂ ·6H ₂ O	6.05·10 ⁻²	Wastes	I.	
$La(NO_3)_3 \cdot 6H_2O$	2.54·10 ⁻³	Wastewater	2.63	
Sepiolite	6.84·10 ⁻²			
Energy	kWh			
Electricity	0.72			
Transport	kg∙km			
Catalyst to plant	8.15			

218 Table 2. Inventory for subsystem S2. Steam Reforming per FU

Inputs from Technosphere						
Materials	kg	Energy	MWh			
Water	4470	Electricity	2.49.10-1			
Alcoholic waste	1000	Transport	kg∙km			
Catalyst from SS1	8.15·10 ⁻²	Catalyst waste to landfill	8.15			
Outputs to Technosphere						
Products	kg	Waste	kg			
Gas stream to SS3	5509	Catalyst waste to landfill	8.15·10 ⁻²			

²¹⁹

220

Inputs from Technosphere						
Materials	kg	Materials	kg			
LaMnO₃	10.05	Polyethyleneglycol	0.03			
LaCrO₃	0.15	Dibutylpthalat	0.03			
Zirconium chloride	1.96	Water, deionised	2.32			
Yttrium chloride	0.29	Nitric acid	13.45			
Zirconium oxide	0.18	Chlorine	1.61			
Nickel oxide	0.18	Petroleum coke	0.26			
Nickel	2.36·10 ⁻⁴	Urea, as N	6.61			
Ethanol	0.44	Gas stream from SS2	5509			
Polyvinilbutyral	0.07	Transport	kg∙km			
Energy	MJ	Freight rail	31.92			
Heating, natural gas	50.76	Lorry > 16t	5.67			
Spray drying, natural gas	560.71	Transoceanic freight	202.09			
Outputs to Technosp	here	Outputs to Nat	ture			
Products	MWh	Emissions	kg			
Electricity	1.81·10 ⁻¹	CO ₂ , biogenic	1800			
		CO ₂	33.10			
		H ₂ O	5810			

Table 3. Life cycle inventory for Subsystem SS3. SOFC per FU

224 2.3. Life Cycle Impact Analysis: Methodology

225	Simapro 8.5.2 (PRé Consultants, 2017) has been the software used for the implementation of
226	the Life Cycle Inventory. To analyze the inputs and outputs of the Life Cycle Inventory, the
227	Classification and Characterization guidelines defined by ISO 14040 and ISO 14044 (ISO, 2006a,
228	2006b) were followed. The environmental results have been presented in terms of the
229	following impact categories of the ReCiPe methodology: Climate Change (CC), Ozone Layer
230	Depletion (OD), Terrestrial Acidification (TA), Freshwater Eutrophication (FE), Marine
231	Eutrophication (ME), Human Toxicity (HT), Photochemical Oxidant Formation (POF), Particulate
232	Matter Formation (PMF), Terrestrial Ecotoxicity (TET), Freshwater Ecotoxicity (FET), Marine
233	Ecotoxicity (MET) and Fossil Fuel Depletion (FD).

235 3. Results and Discussion

- 236
- 3.1. Environmental characterization
- 237 The environmental characterization of the alcoholic waste steam reforming resulted in the
- 238 impacts reported in Table 4. All impacts in Table 4 are attributed to the Functional Unit (1
- tonne feedstock).

Impact category	Units	SS1	SS2	SS3	Total
СС	kg CO ₂ eq	33.08	109.91	207.79	350.78
OD	kg CFC-11 eq	5.98·10 ⁻⁶	1.40·10 ⁻⁵	4.52·10 ⁻⁵	6.52·10 ⁻⁵
ТА	kg SO ₂ eq	0.22	0.67	1.32	2.21
FE	kg P eq	1.41·10 ⁻²	3.09·10 ⁻²	7.56·10 ⁻²	1.21·10 ⁻¹
ME	kg N eq	6.08·10 ⁻²	2.16·10 ⁻²	4.23·10 ⁻²	1.25·10 ⁻¹
НТ	kg 1,4-DB eq	17.11	24.57	122.23	163.91
POF	kg NMVOC	0.10	0.35	0.62	1.07
PMF	kg PM10 eq	0.10	0.24	0.66	1.00
TET	kg 1,4-DB eq	1.04·10 ⁻²	3.15·10 ⁻³	8.05·10 ⁻²	9.41·10 ⁻²
FET	kg 1,4-DB eq	0.76	1.59	4.67	7.01
MET	kg 1,4-DB eq	0.61	1.42	3.68	5.71
FD	kg oil eq	11.65	30.11	89.78	131.55

240 Table 4. Characterized results of the system per FU

242	The SOFC is the main contributor to the Climate Change (CC) category, since this subsystem
243	comprises several processes necessary for the manufacture of the main components. In SS3,
244	direct emissions into the atmosphere are quantified, directly from the alcoholic stream,
245	residue produced from grape fermentation. Therefore, CO_2 emissions from SS3 should not be
246	considered as fossil carbon, but as biogenic CO_2 . This decision agrees with a study on the
247	production of hydrogen and electricity by reforming supercritical water from bioglycerol
248	feedstock (Galera and Gutiérrez-Ortiz, 2015). If CO_2 was not considered biogenic, direct CO_2
249	emissions would represent almost 60% of environmental impact in the climate change
250	category. Therefore, the final impact on this category would be 2146 kg CO_2 eq per tonne of
251	alcoholic waste processed at the facility.

252 The Ozone Layer Depletion category has fairly low values in all subsystems. Freshwater and 253 Marine Eutrophication (FE and ME) show similar behavior, as they are influenced by the same 254 type of substances. The impact value in these categories is relatively similar in all subsystems, 255 which makes the final impact value low. Human Toxicity (HT) and Fossil Depletion (FD) have 256 relatively high levels compared to the rest of the impact categories. The reason is the 257 formulation of catalysts and the manufacture of SOFC, since heavy metals and hazardous 258 substances are required that cause a high impact in the HT category. As for the FD category, its 259 value is related to the high consumption of fossil fuels associated with the formulation of 260 catalysts and the manufacture of SOFC. 261 The specific contribution of each subsystem to the impacts calculated for the system is shown 262 in Figure 3. The manufacture and operation of the SOFC (SS3) was found to dominate almost 263 all impact categories, with percentages ranging from 57.7% in Photochemical Oxidant 264 Formation (POF) to 85.6% in Terrestrial Ecotoxicity (TET). Additionally, the steam reforming 265 subsystem (SS2) showed a significant contribution to Climate Change (31,3%), Terrestrial 266 Acidification (30,4%) and Photochemical Oxidant Formation (32,9%). The remaining subsystem 267 (SS1) accounted for a contribution percentage around 10%, except for ME, where the 268 contribution was higher than 45%.



Figure 3. Relative contribution (%) of the different subsystems to the total environmentalimpact

In order to highlight the processes with the highest environmental impact on the life cycle
performance of the system, the individual contributions to the impact are broken down in
Figure 4. These results show that SOFC manufacturing is the major contribution in almost all
impact categories, except for ME. Therefore, the manufacture of SOFC is the main hotspot of
the system and must have the highest priority in the improvement actions from the
environmental point of view.

278 The second largest contributor to the total environmental impact is electricity consumption,

with contributions percentage ranging from 15% in HT to 32.9% in POF. If electricity

280 production is taken into account, its contribution to environmental impact decreases

significantly to 4.2% and 9.1% in HT and POF, respectively. The formulation of catalysts

282 presented a uniform distribution of environmental impacts in all categories, with contributions

always below 10.6%. The consumption of natural gas to heat the process is only responsible

for a maximum of 9.4% in CC and 8.5% in FD, but in the rest of the impact categories, their

contributions never exceed 6%. The rest of the substances (transport, water consumption and
waste treatment) contributed practically insignificantly to the environmental impact.

Wastewater treatment is the main contributor to the ME impact, due to the high amount of nitrogen-based compounds such as nitrites and nitrates that are discharged in the treated effluent. This may explain, as seen in Figure 3, why the main contributor to the ME impact category is SS1, due to the wastewater generated during the formulation of the catalyst.



291

292 Figure 4. Relative contribution (%) of the components of alcoholic waste steam reforming to

the overall impact

294 The environmental profile of alcoholic waste steam reforming is mainly due to two factors. On

```
the one hand, the use of a raw material that is considered waste from another process and
```

- 296 therefore has no associated environmental impact. On the other hand, the production of
- 297 electricity makes it possible to obtain environmental credits that promote a better
- 298 environmental profile.
- 299

300 *3.2. Sensitivity analysis*

301 In order to compare the environmental characterization results of some alternative waste 302 treatments to steam reforming, a sensitivity analysis was performed. The methods selected for 303 this analysis were landfill and incineration. Note that the inventory data for incineration and 304 landfill were taken from the Ecoinvent[®] database. Figure 5 depicts the environmental 305 performance of the alternative treatments for the alcoholic waste considered. As noted, the 306 steam reforming scenario potentially implied a more acceptable environmental profile than 307 the other scenarios, except for Ozone Layer Depletion, Terrestrial Acidification, Freshwater 308 Eutrophication and Terrestrial Ecotoxicity. In particular, steam reforming makes it possible to 309 reduce GHG emissions by 33% compared to incineration and by 30% compared to landfill. 310 Steam reforming is the largest contributor to OD impact for the emission of harmful gases to 311 the stratospheric ozone layer during some operations such as electricity generation or 312 chemical production. Regarding Terrestrial Acidification and Freshwater Eutrophication, steam 313 reforming presents the worst environmental performance. The consumption of Ni-based 314 compounds in the manufacture of SOFC and some processes derived from the extraction of 315 lanthanum for SOFC are the responsible processes of the poor performance in TA and FE 316 respectively. With respect to TET, steam reforming has worse results, but if the three 317 ecotoxicity categories (TTE, MET and FET) are considered, the environmental impact of steam 318 reforming is lower, improving 95.8% with respect to incineration and 97.8% with respect to the 319 sanitary landfill.





Figure 5. Comparative environmental profile of the alternative treatments for alcoholic wasteconsidering 1 tonne as functional unit

323 *3.3. Comparative analysis*

324 In addition to the basic scheme, a comparison was made with some processes published in the 325 scientific literature. The FU was changed to 1 kg of hydrogen produced in the plant with 99.9 326 vol% purity by steam reforming (Figure 6), in agreement with other reforming studies using 327 other raw materials for hydrogen production (Hajjaji et al., 2016, 2013; Khila et al., 2016; 328 Susmozas et al., 2016, 2015, 2013), thus allowing the comparison of the environmental profile 329 of different processes. Therefore, the new facility configuration does not consider the 330 operation of the SOFC, consequently the output stream of the system is led to a purification 331 system: First, the WGS process removes carbon monoxide and produces a small amount of 332 additional hydrogen. Additionally, in a COPROX reactor the remaining CO can be further 333 reduced to CO₂ in the presence of oxygen. Finally, the PSA process separates H₂ from the rest 334 of the gases in the stream, obtaining H2 with 99% purity. Therefore, two additional subsystems 335 were introduced to purify the output hydrogen stream (SS3) and provide cooling water (SS4)



Figure 6. New flowchart considered to compare the steam reforming of alcoholic waste withother published studies.

339 The following processes have been considered: SMR-H₂: Steam reforming of methane obtained 340 from natural gas (Susmozas et al., 2013). PG-H₂: Poplar biomass gasification. The system 341 includes the cultivation of poplar and its transport to the plant. Once in the plant are included 342 all the operations necessary to obtain hydrogen and the production of electricity from the 343 steam produced in the system (Susmozas et al., 2013). PG&C-H₂: Gasification of poplar 344 biomass, as mentioned above, but includes carbon fixation during the cultivation stage 345 (Susmozas et al., 2016). GSR-H₂: Glycerol reforming, obtained as a co-product of biodiesel 346 production by transesterification of rapeseed oil. Carbon sequestration during oil production is 347 considered (Susmozas et al., 2015). BSR-H₂: Biofuel reforming, including also carbon fixation 348 produced during the growth of biomass used for biofuel (Susmozas et al., 2015). SBR-H₂: Steam 349 reforming of bioethanol, including bioethanol production (Hajjaji et al., 2016). BAR-H₂: 350 Autothermal reforming of bioethanol (Khila et al., 2016). 351 In order to carry out the comparative analysis, life cycle inventories were modified. In relation 352 to the type and quantity of reaction catalyst, the WGS data were obtained from (Compagnoni 353 et al., 2017). All the necessary data to measure the inputs and outputs in SS3. WGS and PSA

- and SS4. Cooling water supply were obtained from (Susmozas et al., 2015, 2013). Inventory
- data of WGS, PSA and Cooling water supply can be found in Table 5.
- **Table 5.** New life cycle inventory to compare the steam reforming of alcoholic wastes with
- 357 other published processes

Inputs from Tec	hnosphere	Outputs to Technosphere		
Materials	kg	Products	kg	
Alcoholic waste	5.42	H ₂	1.00	
Water	24.21	Emissions	kg	
SR catalyst	4.41·10 ⁻⁴	CO ₂	8.16	
WGS catalyst	1.11·10 ⁻³	CH ₄	0.45	
Energy	kWh	C_2H_4	9.41·10 ⁻³	
Electricity	1.36	CO	1.97	
Transport	t∙km	Wastes	kg	
Road	0.48	SR catalyst to landfill	1.11·10 ⁻³	
		WGS catalyst to landfill	4.41·10 ⁻⁴	
		Wastewater from WGS	4.61	

359	The results of the comparison between steam reforming of alcoholic residues and other
360	related processes are presented in terms of the impact categories of the CML methodology
361	Global warming potential (GWP – kg CO_2 eq), Depletion of abiotic resources (ADP – kg Sb eq),
362	Ozone layer depletion (ODP – kg CFC-11 eq), Photochemical oxidation (POFP – kg C_2H_4 eq),
363	Acidification potential (AP – kg SO ₂ eq) and Eutrophication potential (EP – kg PO_4^{3-}). The
364	magnitudes of the environmental impacts of hydrogen production systems are displayed in
365	Table 6, in order to simplify the comparative study, the results are scaled to 100 and
366	represented in Figure 7. For example, alcoholic waste steam reforming shows the best results
367	in terms of ADP, ODP, AP and EP, but performs worse in GWP and has the worst result in POFC.
368	
369	

Present study 9.55 4.25·10 ⁻³ 5.29·10 ⁻⁸ 3.17·10 ⁻³ 4.20·10 ⁻³ 8.11·10 ⁻⁴ Present study SMR-H2 10.60 8.90·10 ⁻² 1.20·10 ⁻⁶ 5.18·10 ⁻⁴ 8.40·10 ⁻³ 1.64·10 ⁻³ (Susmozas et al., 2013) PG-H2 0.41 8.57·10 ⁻² 1.62·10 ⁻⁷ 4.40·10 ⁻⁴ 1.19·10 ⁻² 2.85·10 ⁻³ (Susmozas et al., 2013)	Processes	GWP	ADP	ODP	POFP	AP	EP	Reference
SMR-H2 10.60 8.90·10 ⁻² 1.20·10 ⁻⁶ 5.18·10 ⁻⁴ 8.40·10 ⁻³ 1.64·10 ⁻³ (Susmozas et al., 2013) PG-H2 0.41 8.57·10 ⁻² 1.62·10 ⁻⁷ 4.40·10 ⁻⁴ 1.19·10 ⁻² 2.85·10 ⁻³ (Susmozas et al., 2013)	Present study	9.55	4.25·10 ⁻³	5.29·10 ⁻⁸	3.17·10 ⁻³	4.20·10 ⁻³	8.11.10-4	Present study
PG-H ₂ 0.41 8.57·10 ⁻² 1.62·10 ⁻⁷ 4.40·10 ⁻⁴ 1.19·10 ⁻² 2.85·10 ⁻³ (Susmozas et al., 2013)	SMR-H ₂	10.60	8.90·10 ⁻²	1.20.10-6	5.18·10 ⁻⁴	8.40·10 ⁻³	1.64·10 ⁻³	(Susmozas et al., 2013)
	PG-H₂	0.41	8.57·10 ⁻²	1.62·10 ⁻⁷	4.40·10 ⁻⁴	1.19·10 ⁻²	2.85·10 ⁻³	(Susmozas et al., 2013)
PG&C-H₂ -14.60 2.85·10 ⁻⁷ 8.31·10 ⁻⁴ 2.07·10 ⁻² 4.60·10 ⁻³ (Susmozas et al., 2016)	PG&C-H ₂	-14.60		2.85·10 ⁻⁷	8.31·10 ⁻⁴	2.07·10 ⁻²	4.60·10 ⁻³	(Susmozas et al., 2016)
GSR-H ₂ 12.70 5.69·10 ⁻² 8.90·10 ⁻⁷ 5.16·10 ⁻⁴ 6.51·10 ⁻² 5.26·10 ⁻² (Susmozas et al., 2015)	GSR-H₂	12.70	5.69·10 ⁻²	8.90·10 ⁻⁷	5.16·10 ⁻⁴	6.51·10 ⁻²	5.26·10 ⁻²	(Susmozas et al., 2015)
BSR-H ₂ 3.79 4.13·10 ⁻² 5.54·10 ⁻⁷ 6.00·10 ⁻⁴ 1.56·10 ⁻² 3.20·10 ⁻³ (Susmozas et al., 2015)	BSR-H₂	3.79	4.13·10 ⁻²	5.54·10 ⁻⁷	6.00·10 ⁻⁴	1.56.10-2	3.20·10 ⁻³	(Susmozas et al., 2015)
SBR-H ₂ 6.81 2.13·10 ⁻² 3.96·10 ⁻⁷ 1.55·10 ⁻³ 3.53·10 ⁻² 2.54·10 ⁻² (Hajjaji et al., 2016)	SBR-H ₂	6.81	2.13.10-2	3.96·10 ⁻⁷	1.55·10 ⁻³	3.53·10 ⁻²	2.54·10 ⁻²	(Hajjaji et al., 2016)
BAR-H ₂ 7.27 4.87·10 ⁻² 3.13·10 ⁻⁶ 1.65·10 ⁻³ 2.76·10 ⁻² 2.81·10 ⁻² (Khila et al., 2016)	BAR-H ₂	7.27	4.87·10 ⁻²	3.13·10 ⁻⁶	1.65·10 ⁻³	2.76·10 ⁻²	2.81.10-2	(Khila et al., 2016)

371 **Table 5.** Summarized results of comparative life cycle assessment



373

Figure 7. Comparison (in %) of different reforming processes to obtain hydrogen. Caption: Dark
Blue: Present studio; Light Blue: SMR-H₂; Pink: PG-H₂; Brown: PG&C-H₂; Green: GSR-H₂; Purple:
BSR-H₂; Red: SBR-H₂; Yellow: BAR-H₂.

The comparison between the present study and other published processes is possible because the environmental performance of the different studies is published in some LCA studies with a methodological framework consistent with this study. Steam reforming of alcoholic residues has the highest value in POF, due to direct emissions of CH₄, which occur in relatively high quantities during steam reforming. However, this process performs well in terms of ODP with a value around 2% of BAR-H₂, which is the process with the worst environmental performance in this category. 384 Four impact categories are detailed in this section: Depletion of abiotic resources (ADP), 385 Acidification potential (AP), Eutrophication potential (EP) and Global warming potential (GWP). 386 These are the most common and well-established categories for assessing bioenergy systems 387 in LCA studies (Cherubini and Strømman, 2011; Muench and Guenther, 2013; Peters et al., 388 2015). The total GHG emissions of the system are estimated at approximately 9.55 kg CO₂ eq 389 per kg of H₂ produced. As can be seen in Figure 8.a, this value is relatively higher than that of 390 other technologies but is considerably lower than that of a conventional H₂ production system 391 (SMR-H₂). Approximately 90% of these emissions are attributed to direct methane emissions 392 from the reforming reactor, as CH₄ is 21 times more likely to affect GWP over a 100-year 393 period, according to IPCC. The lowest value in this category corresponds to PG&G-H₂, since this 394 process considers CO₂ capture during biomass cultivation. This explains the importance of 395 system boundaries in an LCA study, since PG&G-H₂ covers from biomass cultivation to 396 hydrogen production with CO₂ capture. However, in the present study the limit of the system 397 ranges from alcoholic residues entering the plant to the production of electricity, so carbon 398 sequestration during biomass cultivation is not considered. 399 Some metals, minerals and fossil fuels are used in all H₂ production systems. Figure 8b shows

400 that fossil methane to hydrogen system (SMR- H_2) has the greatest impact on ADP, as expected, 401 due to the large consumption of fossil fuels in the reforming process. H₂ produced from 402 bioethanol consumes considerable non-renewable resources throughout the life cycle when 403 ethanol production phases are considered (Hajjaji et al., 2013). However, in this study, steam 404 reforming of alcoholic waste (mainly ethanol) is the best process in terms of ADP because this 405 ethanol is a waste derived from another process that has no associated impact. With respect 406 to Acidification Potential and Eutrophication Potential (Figure 8c and 8d), steam reforming of 407 alcoholic waste presents the best results. The processes with the highest impact in these 408 impact categories are those that take into account the cultivation phase (SBR-H₂, BAR-H₂ and

409 GSR-H₂), mainly due to the use of fertilizers containing nitrate, ammonia and phosphate in the





412

413 Figure 8. Comparison of the environmental impacts in GWP, ADP, AP and EP categories

- 414 4. Conclusions
- 415 From a life cycle perspective, the results suggest that this type of energy systems that produce
- 416 hydrogen from alcoholic waste through steam reforming has good environmental
- 417 performance. Overall, steam reforming of this type of alcoholic waste for energy production
- 418 could play a significant role in future energy systems.
- 419 The SOFC is the main contributor to environmental impact in most impact categories.
- 420 Analysing the different processes, the manufacture of SOFC is the process with the greatest
- 421 environmental impact in all impact categories except in ME, where wastewater treatment is
- 422 the main contributor. The sensitivity analysis shows the promising performance of this waste
- 423 treatment, since the treatment of 1 tonne of alcoholic waste produces 351 kg of CO₂ eq, this
- 424 result is 33% and 30% better than incineration and sanitary landfill respectively.
- 425 It is clear that Life Cycle Assessment is a useful tool to determine the environmental
- 426 performance of steam reforming of alcoholic waste to produce electricity. However, these

- 427 results have been obtained by evaluating the data taken on a laboratory scale, and more
- 428 studies on a larger scale will be needed in the future to determine a more accurate estimate of
- 429 the actual environmental profile of the process.
- 430 Comparative analysis has allowed us to compare this process with others related to the
- 431 production of hydrogen from different raw materials. Although steam reforming has some
- 432 poor results in GWP and POF due to methane emissions, its environmental performance is
- 433 generally better than other processes published in the scientific literature.
- 434

435 Acknowledgements

- 436 This research was supported by the European Projects STAR-ProBio (Grant Agreement Number
- 437 727740) and life-ECOELECTRICITY. The authors (Mr. Antonio Cortés, Prof. Gumersindo Feijoo
- 438 and Prof. Maria Teresa Moreira) belong to the Galician Competitive Research Group GRC
- 439 ED413C 2017/2019 and to the CRETUS Strategic Partnership (ED431E 2018/01), co-funded by
- 440 FEDER (EU). Prof. María Teresa Moreira and Prof. Antonio Chica acknowledge to Red de
- 441 Excelencia en biorrefinerías sostenibles (CTQ2016-81848-REDT)

442 References

- 443 Aguilar-Sánchez, P., Navarro-Pineda, F.S., Sacramento-Rivero, J.C., Barahona-Pérez, L.F., 2018.
- 444 Life-cycle assessment of bioethanol production from sweet sorghum stalks cultivated in
- the state of Yucatan, Mexico. Clean Technol. Environ. Policy 20, 1685–1696.
- 446 https://doi.org/10.1007/s10098-017-1480-4
- 447 Alamolhoda, S., Vitale, G., Hassan, A., Nassar, N.N., Almao, P.P., 2019. Synergetic effects of
- 448 cerium and nickel in Ce-Ni-MFI catalysts on low-temperature water-gas shift reaction.
- 449 Fuel 237, 361–372. https://doi.org/10.1016/j.fuel.2018.09.096
- 450 Alipour-Moghadam, R., Yusup, S., Azlina, W., Nehzati, S., Tavasoli, A., 2014. Investigation on

- 451 syngas production via biomass conversion through the integration of pyrolysis and air-
- 452 steam gasification processes. Energy Convers. Manag. 87, 670–675.
- 453 https://doi.org/10.1016/j.enconman.2014.07.065
- 454 Anzelmo, B., Wilcox, J., Liguori, S., 2018. Hydrogen production via natural gas steam reforming
- 455 in a Pd-Au membrane reactor. Investigation of reaction temperature and GHSV effects
- 456 and long-term stability. J. Memb. Sci. 568, 113–120.
- 457 https://doi.org/10.1016/j.memsci.2018.09.054
- 458 Balat, M., 2011. Production of bioethanol from lignocellulosic materials via the biochemical
- 459 pathway: A review. Energy Convers. Manag. 52, 858–875.
- 460 https://doi.org/10.1016/j.enconman.2010.08.013
- 461 Braga, A.H., Sodré, E.R., Batista, J., Santos, O., Paula, C.M. De, Maria, J., Bueno, C., 2016. Steam
- 462 reforming of acetone over Ni- and Co-based catalysts : Effect of the composition of
- 463 reactants and catalysts on reaction pathways. Appl. Catal. B, Environ. 195, 16–28.
- 464 https://doi.org/10.1016/j.apcatb.2016.04.047
- 465 Cherubini, F., Strømman, A.H., 2011. Life cycle assessment of bioenergy systems: State of the
- 466 art and future challenges. Bioresour. Technol. 102, 437–451.
- 467 https://doi.org/10.1016/j.biortech.2010.08.010
- 468 Comité Européen des Enterprises Vins, 2016. European Wine: a solid pillar of the European
 469 Union economy. Brussels.
- 470 Compagnoni, M., Mostafavi, E., Tripodi, A., Mahinpey, N., Rossetti, I., 2017. Techno-economic
- 471 Analysis of a Bioethanol to Hydrogen Centralized Plant. Energy and Fuels 31, 12988–
- 472 12996. https://doi.org/10.1021/acs.energyfuels.7b02434
- 473 Coronado, I., Pitínová, M., Karinen, R., Reinikainen, M., Puurunen, R.L., Lehtonen, J., 2018.
- 474 Aqueous-phase reforming of Fischer-Tropsch alcohols over nickel-based catalysts to
- 475 produce hydrogen: Product distribution and reaction pathways. Appl. Catal. A Gen. 567,

- 476 112–121. https://doi.org/10.1016/j.apcata.2018.09.013
- 477 Costa, D., Jesus, J., Virgínio e Silva, J., Silveira, M., 2018. Life Cycle Assessment of Bioethanol
- 478 Production from Sweet Potato (Ipomoea batatas L.) in an Experimental Plant. Bioenergy
- 479 Res. 11, 715–725. https://doi.org/10.1007/s12155-018-9932-1
- 480 Da Costa-Serra, J.F., Chica, A., 2018. Catalysts based on Co-Birnessite and Co-Todorokite for
- 481 the efficient production of hydrogen by ethanol steam reforming. Int. J. Hydrogen Energy
- 482 43, 16859–16865. https://doi.org/10.1016/j.ijhydene.2017.12.114
- 483 Demirbas, A., 2008. Biofuels sources, biofuel policy, biofuel economy and global biofuel
- 484 projections. Energy Convers. Manag. 49, 2106–2116.
- 485 https://doi.org/10.1016/j.enconman.2008.02.020
- 486 Díaz Alvarado, F., Gracia, F., 2010. Steam reforming of ethanol for hydrogen production:
- 487 Thermodynamic analysis including different carbon deposits representation. Int. J.
- 488 Hydrogen Energy 165, 649–657. https://doi.org/10.1016/j.cej.2010.09.051
- 489 Esteve-Adell, I., Crapart, B., Primo, A., Serp, P., Garcia, H., 2017. Aqueous phase reforming of
- 490 glycerol using doped graphenes as metal-free catalysts. Green Chem. 19, 3061–3068.
- 491 https://doi.org/10.1039/c7gc01058c
- 492 Fragiacomo, P., de Lorenzo, G., Corigliano, O., 2018. Performance Analysis of a Solid Oxide Fuel
- 493 Cell-Gasifier Integrated System in Co-Trigenerative Arrangement. J. Energy Resour.
- 494 Technol. 140, 092001 (1-9). https://doi.org/10.1115/1.4039872
- 495 Frolov, S.M., Medvedev, S.N., Basevich, V.Y., Frolov, F.S., 2013. Self-ignition of hydrocarbon-
- 496 hydrogen-air mixtures. Int. J. Hydrogen Energy 38, 4177–4184.
- 497 https://doi.org/10.1016/j.ijhydene.2013.01.075
- 498 Galera, S., Gutiérrez-Ortiz, F.J., 2015. Life cycle assessment of hydrogen and power production
- 499 by supercritical water reforming of glycerol. Energy Convers. Manag. 96, 637–645.

500 https://doi.org/10.1016/j.enconman.2015.03.031

- 501 García, L., Valiente, A., Oliva, M., Ruiz, J., Arauzo, J., 2018. Influence of operating variables on
- 502 the aqueous-phase reforming of glycerol over a Ni/Al coprecipitated catalyst. Int. J.
- 503 Hydrogen Energy 43, 20392–20407. https://doi.org/10.1016/j.ijhydene.2018.09.119
- 504 González-García, S., Iribarren, D., Susmozas, A., Dufour, J., Murphy, R.J., 2012. Life cycle
- assessment of two alternative bioenergy systems involving Salix spp. biomass: Bioethanol
- 506 production and power generation. Appl. Energy 95, 111–122.
- 507 https://doi.org/10.1016/j.apenergy.2012.02.022
- 508 Hajjaji, N., Khila, Z., Baccar, I., Pons, M.N., 2016. A thermo-environmental study of hydrogen
- 509 production from the steam reforming of bioethanol. J. Energy Storage 7, 204–219.
- 510 https://doi.org/10.1016/j.est.2016.06.010
- 511 Hajjaji, N., Pons, M.N., Renaudin, V., Houas, A., 2013. Comparative life cycle assessment of
- 512 eight alternatives for hydrogen production from renewable and fossil feedstock. J. Clean.

513 Prod. 44, 177–189. https://doi.org/10.1016/j.jclepro.2012.11.043

- 514 Halleux, H., Lassaux, S., Renzoni, R., Germain, A., 2008. Comparative Life Cycle Assessment of
- 515 Two Biofuels. Ethanol from Sugar Beet and Rapeseed Methyl Ester. Int. J. Life Cycle
- 516 Assess. 13, 184–190. https://doi.org/10.1065/lca2008.03.382
- 517 Haryanto, A., Fernando, S., Murali, N., Adhikari, S., 2005. Current status of hydrogen
- 518 production techniques by steam reforming of ethanol: A review. Energy & Fuels 19,
- 519 2098–2106. https://doi.org/10.1021/ef0500538
- 520 Hernández, L., Kafarov, V., 2009. Use of bioethanol for sustainable electrical energy
- 521 production. Int. J. Hydrogen Energy 34, 7041–7050.
- 522 https://doi.org/10.1016/j.ijhydene.2008.07.089
- 523 ISO, 2006a. ISO 14040 Environmental Management Life Cycle Assessment Principles and

- 524 Framework. International Organization for Standardization.
- 525 ISO, 2006b. ISO 14044 Environmental Management Life Cycle Assessment Requirements
- 526 and Guidelines. International Organization for Standardization.
- 527 Jeon, J., Nam, S., Ko, C.H., 2018. Rapid evaluation of coke resistance in catalysts for methane
- reforming using low steam-to-carbon ratio. Catal. Today 309, 140–146.
- 529 https://doi.org/10.1016/j.cattod.2017.08.051
- 530 Jeswani, H.K., Falano, T., Azapagic, A., 2015. Life cycle environmental sustainability of
- 531 lignocellulosic ethanol produced in integrated thermo-chemical biorefineries. Biofuels,

532 Bioprod. Biorefining 9, 661–676. https://doi.org/10.1002/bbb

- 533 Karlsson, H., Börjesson, P., Hansson, P.A., Ahlgren, S., 2014. Ethanol production in biorefineries
- 534 using lignocellulosic feedstock GHG performance, energy balance and implications of

535 life cycle calculation methodology. J. Clean. Prod. 83, 420–427.

- 536 https://doi.org/10.1016/j.jclepro.2014.07.029
- 537 Khaodee, W., Wongsakulphasatch, S., Kiatkittipong, W., Arpornwichanop, A., Laosiripojana, N.,
- 538 Assabumrungrat, S., 2011. Selection of appropriate primary fuel for hydrogen production
- 539 for different fuel cell types: Comparison between decomposition and steam reforming.
- 540 Int. J. Hydrogen Energy 36, 7696–7706. https://doi.org/10.1016/j.ijhydene.2011.03.123
- 541 Khila, Z., Baccar, I., Jemel, I., Hajjaji, N., 2017. Thermo-environmental life cycle assessment of
- 542 hydrogen production by autothermal reforming of bioethanol. Energy Sustain. Dev. 37,
- 543 66–78. https://doi.org/10.1016/j.esd.2016.12.003
- 544 Khila, Z., Baccar, I., Jemel, I., Houas, A., Hajjaji, N., 2016. Energetic, exergetic and
- 545 environmental life cycle assessment analyses as tools for optimization of hydrogen
- 546 production by autothermal reforming of bioethanol. Int. J. Hydrogen Energy 41, 17723–
- 547 17739. https://doi.org/10.1016/j.ijhydene.2016.07.225

- 548 Kumar, B., Kumar, S., Sinha, S., Kumar, S., 2018. Utilization of acetone-butanol-ethanol-water
- 549 mixture obtained from biomass fermentation as renewable feedstock for hydrogen
- 550 production via steam reforming: Thermodynamic and energy analyses. Bioresour.
- 551 Technol. 261, 385–393. https://doi.org/10.1016/j.biortech.2018.04.035
- Lee, Y.D., Ahn, K.Y., Morosuk, T., Tsatsaronis, G., 2015. Environmental impact assessment of a
- solid-oxide fuel-cell-based combined-heat-and-power-generation system. Energy 79,
- 554 455–466. https://doi.org/10.1016/j.energy.2014.11.035
- 555 López, E.R., Dorado, F., de Lucas-Consuegra, A., 2019. Electrochemical promotion for hydrogen
- 556 production via ethanol steam reforming reaction. Appl. Catal. B Environ. 243, 355–364.
- 557 https://doi.org/10.1016/j.apcatb.2018.10.062
- 558 Luo, L., van der Voet, E., Huppes, G., 2009. Life cycle assessment and life cycle costing of
- bioethanol from sugarcane in Brazil. Renew. Sustain. Energy Rev. 13, 1613–1619.
- 560 https://doi.org/10.1016/j.rser.2008.09.024
- 561 Menezes, J., Manfro, R., Souza, M., 2018. Hydrogen production from glycerol steam reforming
- 562 over nickel catalysts supported on alumina and niobia: Deactivation process, effect of
- reaction conditions and kinetic modeling. Int. J. Hydrogen Energy 43, 15064–15082.
- 564 https://doi.org/10.1016/j.ijhydene.2018.06.048
- 565 Menor, M., Sayas, S., Chica, A., 2017. Natural sepiolite promoted with Ni as new and efficient
- 566 catalyst for the sustainable production of hydrogen by steam reforming of the biodiesel
- 567 by-products glycerol. Fuel 193, 351–358. https://doi.org/10.1016/j.fuel.2016.12.068
- 568 Morales, M., Roa, J.J., Capdevila, X.G., Segarra, M., Piñol, S., 2010. Mechanical properties at
- 569 the nanometer scale of GDC and YSZ used as electrolytes for solid oxide fuel cells. Acta
- 570 Mater. 58, 2504–2509. https://doi.org/10.1016/j.actamat.2009.12.036
- 571 Muench, S., Guenther, E., 2013. A systematic review of bioenergy life cycle assessments. Appl.
- 572 Energy 112, 257–273. https://doi.org/10.1016/j.apenergy.2013.06.001

- 573 Ni, M., Leung, D.Y.C., Leung, M.K.H., 2007. A review on reforming bio-ethanol for hydrogen
- 574 production. Int. J. Hydrogen Energy 32, 3238–3247.
- 575 https://doi.org/10.1016/j.ijhydene.2007.04.038
- 576 Peters, J.F., Iribarren, D., Dufour, J., 2015. Simulation and life cycle assessment of biofuel
- 577 production via fast pyrolysis and hydroupgrading. Fuel 139, 441–456.
- 578 https://doi.org/https://doi.org/10.1016/j.fuel.2014.09.014
- 579 PRé Consultants, 2017. SimaPro Database Manual (No. Methods Library). The Netherlands.
- 580 Rabenstein, G., Hacker, V., 2008. Hydrogen for fuel cells from ethanol by steam-reforming,
- 581 partial-oxidation and combined auto-thermal reforming: A thermodynamic analysis. J.
- 582 Power Sources 185, 1293–1304. https://doi.org/10.1016/j.jpowsour.2008.08.010
- 583 Ramírez, P., Homs, N., 2008. Use of biofuels to produce hydrogen (reformation processes).
- 584 Chem. Soc. Rev. 37, 2459–2467. https://doi.org/10.1039/b712181b
- 585 Reyes-Valle, C., Villanueva-Perales, A.L., Vidal-Barrero, F., Ollero, P., 2015. Integrated economic
- and life cycle assessment of thermochemical production of bioethanol to reduce
- 587 production cost by exploiting excess of greenhouse gas savings. Appl. Energy 148, 466–
- 588 475. https://doi.org/10.1016/j.apenergy.2015.03.113
- 589 Rossetti, I., Compagnoni, M., Torli, M., 2015a. Process simulation and optimization of H2
- 590 production from ethanol steam reforming and its use in fuel cells. 1. Thermodynamic and
- 591 kinetic analysis. Chem. Eng. J. 281, 1024–1035. https://doi.org/10.1016/j.cej.2015.08.045
- 592 Rossetti, I., Compagnoni, M., Torli, M., 2015b. Process simulation and optimization of H2
- 593 production from ethanol steam reforming and its use in fuel cells. 2. Process analysis and
- 594 optimization. Chem. Eng. J. 281, 1036–1044. https://doi.org/10.1016/j.cej.2015.08.045
- 595 Salkuyeh, Y.K., Saville, B.A., MacLean, H.L., 2018. Techno-economic analysis and life cycle
- 596 assessment of hydrogen production from different biomass gasification processes. Int. J.

- 597 Hydrogen Energy 43, 9514–9528. https://doi.org/10.1016/j.ijhydene.2018.04.024
- 598 Spallina, V., Matturro, G., Ruocco, C., Meloni, E., Palma, V., Fernandez, E., Melendez, J.,
- 599 Pacheco-Tanaka, A.D., Viviente-Sole, J.L., van Sint-Annaland, M., Gallucci, F., 2018. Direct
- 600 route from ethanol to pure hydrogen through autothermal reforming in a membrane
- 601 reactor: Experimental demonstration, reactor modelling and design. Energy 143, 666–
- 602 681. https://doi.org/10.1016/j.energy.2017.11.031
- Spath, P.L., Mann, M.K., 2001. Life cycle assessment of hydrogen production via natural gas
 steam reforming, National Renewable Energy Laboratory.
- 605 Spiridon, I., Darie-Nita, R.N., Hitruc, G.E., Ludwiczak, J., Cianga, I.A., Niculaua, M., 2016. New
- 606 opportunities to valorize biomass wastes into green materials. J. Clean. Prod. 133, 235–
- 607 242. https://doi.org/10.1016/j.jclepro.2016.05.143
- 608 Strazza, C., Del Borghi, A., Costamagna, P., Gallo, M., Brignole, E., Girdinio, P., 2015. Life Cycle
- 609 Assessment and Life Cycle Costing of a SOFC system for distributed power generation.
- 610 Energy Convers. Manag. 100, 64–77. https://doi.org/10.1016/j.enconman.2015.04.068
- 611 Strazza, C., Del Borghi, A., Costamagna, P., Traverso, A., Santin, M., 2010. Comparative LCA of
- 612 methanol-fuelled SOFCs as auxiliary power systems on-board ships. Appl. Energy 87,
- 613 1670–1678. https://doi.org/10.1016/j.apenergy.2009.10.012
- 614 Susmozas, A., Iribarren, D., Dufour, J., 2015. Assessing the Life-Cycle Performance of Hydrogen
- 615 Production via Biofuel Reforming in Europe. Resources 4, 398–411.
- 616 https://doi.org/10.3390/resources4020398
- 617 Susmozas, A., Iribarren, D., Dufour, J., 2013. Life-cycle performance of indirect biomass
- 618 gasification as a green alternative to steam methane reforming for hydrogen production.
- 619 Int. J. Hydrogen Energy 38, 9961–9972. https://doi.org/10.1016/j.ijhydene.2013.06.012
- 620 Susmozas, A., Iribarren, D., Zapp, P., Linβen, J., Dufour, J., 2016. Life-cycle performance of

621 hydrogen production via indirect biomass gasification with CO2 capture. Int. J. Hydrogen

622 Energy 41, 19484–19491. https://doi.org/10.1016/j.ijhydene.2016.02.053

- Tian, J., Ke, Y., Kong, G., Tan, M., Wang, Y., Lin, J., Zhou, W., Wan, S., 2017. A novel structured
- 624 PdZnAl/Cu fiber catalyst for methanol steam reforming in microreactor. Renew. Energy
- 625 113, 30–42. https://doi.org/10.1016/j.renene.2017.04.070
- Tian, Y., Zhou, X., Lin, S., Ji, X., Bai, J., Xu, M., 2018. Syngas production from air-steam
- 627 gasification of biomass with natural catalysts. Sci. Total Environ. 645, 518–523.
- 628 https://doi.org/10.1016/j.scitotenv.2018.07.071
- Unrean, P., Lai Fui, B.C., Rianawati, E., Acda, M., 2018. Comparative techno-economic
- 630 assessment and environmental impacts of rice husk-to-fuel conversion technologies.

631 Energy 151, 581–593. https://doi.org/10.1016/j.energy.2018.03.112

- Uusitalo, V., Väisänen, S., Inkeri, E., Soukka, R., 2017. Potential for greenhouse gas emission
- 633 reductions using surplus electricity in hydrogen, methane and methanol production via
- 634 electrolysis. Energy Convers. Manag. 134, 125–134.
- 635 https://doi.org/10.1016/j.enconman.2016.12.031
- 636 Valente, A., Iribarren, D., Gálvez-Martos, J.L., Dufour, J., 2019. Robust eco-efficiency
- 637 assessment of hydrogen from biomass gasification as an alternative to conventional
- 638 hydrogen: A life-cycle study with and without external costs. Sci. Total Environ. 650,

639 1465–1475. https://doi.org/10.1016/j.scitotenv.2018.09.089

- 640 Wang, M., Au, C.T., Lai, S.Y., 2015. H2 production from catalytic steam reforming of n-propanol
- 641 over ruthenium and ruthenium-nickel bimetallic catalysts supported on ceria-alumina
- oxides with different ceria loadings. Int. J. Hydrogen Energy 40, 13926–13935.
- 643 https://doi.org/10.1016/j.ijhydene.2015.07.162
- Kue, Z., Shen, Y., Zhu, S., Li, P., Zeng, Y., Xi, Z., Cai, Y., 2017. Autothermal reforming of ethyl
- 645 acetate for hydrogen production over Ni3La7Oy/Al2O3catalyst. Energy Convers. Manag.

- 646 146, 34–42. https://doi.org/10.1016/j.enconman.2017.05.018
- 647 Zheng, T., Zhou, W., Yu, W., Ke, Y., Liu, Y., Liu, R., San Hui, K., 2019. Methanol steam reforming
- 648 performance optimisation of cylindrical microreactor for hydrogen production utilising
- 649 error backpropagation and genetic algorithm. Chem. Eng. J. 357, 641–654.
- 650 https://doi.org/10.1016/j.cej.2018.09.129