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CO₂ concentration measurements inside expansion-compression engine under high EGR conditions using an infrared absorption method

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ABSTRACT

The purpose of this study is to measure the high concentrations of CO₂ near a spark plug inside an internal combustion engine, and an infrared absorption method is used for the measurement. The spark plug sensor was adapted to a compression-expansion machine, and the CO₂ concentration near the spark plug was measured by adding a gas mixture, including CO₂ to imitate EGR. Next, the EGR ratio was changed from 10 to 40%, and the CO₂ concentration was measured. The effect of the CO₂ on the flame propagation was investigated by visualizing the bottom view of the compression-expansion machine. The measurements of CO₂ mass concentration are in agreement with those predicted by direct-absorption spectroscopy fundamental theory from the crank angle -60 to -15 deg ATDC. The error was less than 20%, and under the conditions with an EGR ratio of 20–40%.

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1. Introduction

Determination of species concentrations inside a combustion chamber provides vital knowledge about the combustion process. The gas mixture in a combustion chamber consists of two main components: The fresh air-fuel mixture and the remaining burned gas from the previous cycle. The former component, i.e. the air-fuel mixture, determines the quality of combustion. It is quite important to adjust the air-fuel mixture prior to ignition to get reliable, clean, and safe operation of the combustion process. The undesirable emissions associated with combustion processes includes carbon dioxide, carbon monoxide, nitrogen oxides, sulfur dioxide, and particulate matters. These emissions are facing increasingly stringent regulations. One of the most promising approaches to reduce pollution emissions is to dilute the air with recirculated gases from the previous ignition cycle. Exhaust gas recirculation (EGR) is a technology that is widely used to reduce and control nitrogen

oxide (NO_x) emissions [1,2]. In EGR method a portion of engine exhaust gases returns to the combustion chamber via the intake system. As a consequence, the available amount of oxygen in the intake mixture for combustion will be reduced. The effective air-fuel ratio is lowered as a result of the oxygen reduction, which substantially affects the exhaust emissions. Mixing the intake air with exhaust gases will increase the specific heat of the intake mixture, resulting in a flame temperature reduction. A lower oxygen quantity in the intake air and a lower flame temperature reduces the NO_x formation reaction rate [3,4]. Higher fraction of EGR may reduce NO_x emission to 25% [5]. In addition to this desirable effect, EGR introduce cycle-to-cycle variations which substantially increase ignition delay times. [5–7]. For a multi-cylinder engine, the insufficient mixing of the EGR-air charge coupled with cycle-to-cycle variations may produce different charge gas composition, i.e. different ratio of the fresh air-fuel mixture and the exhaust gases, among the combustion chambers. This may introduce cylinder-to-cylinder variations [8]. EGR addition might also decelerate the burning velocity of the mixture which in turn may introduce prolongation of the burn duration, poor combustion phasing, higher optimum heat loss, and partial burning for the fuel-air mixture [9,10]. There are two types of EGR technique internal EGR and external EGR, according to the exhaust recirculation strategy. Internal EGR requires some mechanisms or variable valve timing (VVT) to retain a certain amount of exhaust gases from a previous

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cycle, where an external EGR can be conducted by producing a pressure difference between the inlet air and exhaust gases through an external pip arrangement [11]. Although EGR has become important control technology for advanced combustion [12] and alternate fuelled engine applications [13,14], improper use of EGR may lead to a reduction in engine durability and unstable operation [9].

In order to optimize and control this complicated process, high-speed diagnostic techniques are needed to determine the amount of gas recirculated in an engine during the intake and compression cycle, especially the gas near the spark plug. Currently, there are many methods to measure the residual gas concentration in a combustion chamber [15]. Recent advances in laser-based techniques have achieved the required interest in many cases and various instruments have become commercially available. Laser-based combustion diagnostics techniques have been developed and are of great interest because of their *in situ* measurement capability and nonintrusive nature. For instance, the Laser-Induced Fluorescence (LIF) [16] is very efficient for temperature and air-fuel ratios measurements because it is based on a spatially resolved measurements technique. However it needs sufficient optical access. It is also demanding in terms of the time needed for measurements. Additionally, special care should be taken for choosing the fluorescent tracer molecule, and sometimes it does not permit real-time measurements [17,18]. Rayleigh and Raman scattering techniques (SRS) [19], can measure the concentration of the molecule by measuring Raman scattering generated by shifting the incident light of a specific wavelength by the vibration energy of the molecule, and it is also possible to measure spatial distribution. However, Raman spectroscopy needs to be measured through a visualization window. Another problem is that molecules with high concentration and large Raman scattering cross section are targeted to a very weak scattered light. For that purpose, Yamamoto et al. mainly used measurements in stationary flow fields and measured the CO₂ concentration in a steady flow field using CARS (Coherent Anti-Stokes Raman Scattering) with stronger light intensity [20].

One of the well-established strategies of spectroscopic diagnostic for flow parameters measurements is the absorption [21,22]. Absorption measurements are particularly helpful in combustion diagnostics since they are extremely quick and selective, up to 40 kHz using spectroscopy with second-harmonic detection of wavelength modulation [23]. They can be used to quantify parameters such as concentration, and temperature without any disturbing of the flow of interest [24,25]. Absorption-based measurements can be employed in a variety of applications such as basic parameters studies of chemical-kinetic in shock tubes [26], and commercial sensors for emission control [27]. Measurements can be demonstrated using many sources that ranges from vacuum-ultraviolet (below 200 nm) to mid-infrared (mid-IR, up to 20 μm) sources. For combustion applications, the mid-IR spectrum is of great interest since many combustion products have distinct absorption features in this region [28]. Advanced optical diagnostic techniques [29] can be used to conduct high-sensitivity absorption measurements. With the continuous development of mid-IR light sources and detectors, measurements techniques based on mid-IR absorption are highly developed for many applications.

Carbon dioxide is considered one of the main exhaust gas constituents. It received high interest because it is usually used to estimate EGR ratio. CO₂ shows three discrete absorption bands in the mid-IR spectrum: Near 4.3 μm, 2.7 μm, and 2.0 μm. Each band is characterized by numerous individual absorption features, which correlate with different rovibrational transitions. Kawahara et al. [30] used infrared laser absorption to perform cycle-resolved residual gas concentration measurements inside a heavy-duty diesel engine [30]. They estimated the internal exhaust gas recirculation

(EGR) ratio and quantified the CO₂ concentration in the residual gas. *In situ* measurements for residual gas concentrations, especially CO₂ and H₂O, have also been conducted using infrared absorption diagnostics [31,32]. Francqueville et al. [31] measured the CO₂ concentration in the combustion chamber of a spark-ignited engine. Grosch et al. measured CO₂ and gaseous H₂O concentrations using infrared spectroscopy in environments that was difficult for direct measurement using a fiber optical sensor [33]. They used an optical absorption sensor to conduct quantitatively *in-cylinder* transmission measurements. They analyzed spectrally the CO₂ and H₂O mixture (wavelength: 3700 cm⁻¹, temperatures: 573 K, and pressures: 1800 kPa). In spark-ignited engines, the sensors used for mixture formation analyses are usually optical absorption-based sensors. These sensors have the advantage that enabled the access of the cylinder without any optical window. Consequently, measurements can be performed under realistic conditions and the engine's mechanical and thermodynamic properties under study will not be changed by the measurement tools. Optical absorption-based sensors combined with gas sampling probes can analyze the gas mixture inside the cylinder. In high-pressure combustion environments, little advancement has been achieved for the practical absorption-based sensors developments for CO₂ measurements. Both the telecommunications diode lasers and the optical fiber, in the near-infrared (NIR) 1.3–1.6 μm wavelength) are used in many of the preceding high-pressure CO₂ sensors. By direct absorption, these sensors can access weak vibrational bands of CO₂ [34] by using direct absorption spectroscopy [35–37], wavelength modulation spectroscopy (WMS) [38,39], or NIR hyperspectral sources. A measurements of high-pressure CO₂ absorption have been conducted near 2.0 μm, which explore the importance of optical sensor design for high-pressure applications [40].

In this study, the infrared absorption method was used for CO₂ concentration measurements near a spark plug at different EGR ratios. A distributed feedback (DFB) laser diode was used as the infrared light source with a wavelength near 4.2 μm. Propane was used as the base fuel, and pure gases were used to simulate EGR compositions to approximate the combustion of ideal products and propane ideal reformer products. The wavelength of 4195.7 nm was chosen for high concentration CO₂ measurements at different EGR ratios. Additionally, the effect of the CO₂ concentration on flame propagation was investigated by visualization.

2. Theory

Absorption is a selective process, which occurs as a result of light-matter interaction when photon energy is transferred to the molecule. Absorption is strongly dependent on molecular structure so the fundamental absorption line spectrum is unique for each gas species. For example, SO₂, NO₂, and NO all share the same characteristic absorption lines in the ultraviolet region. Many combustion-related species have rovibrational (rotational-vibrational) transitions in the mid-IR spectrum. Carbon dioxide gas (CO₂), our main focus in this study, has three fundamental absorption bands at three wavelengths, 4.3, 2.7 and 2 μm, as a result of the C–O vibrational rotational band. The fundamental band centred near 4.3 μm shows many strong absorption lines, and this band is generally well isolated from absorption interference when combustion products, including water and carbon dioxide, are present [41]. For accurate gas concentration measurements in practical internal combustion engines, a strong absorption coefficient is essential because of the limitation of the measurement length. The infrared absorption bands of CO₂ from 2 to 5 μm in wavelength at 300 K calculated by the HITRAN database [42] are shown in Fig. 1.

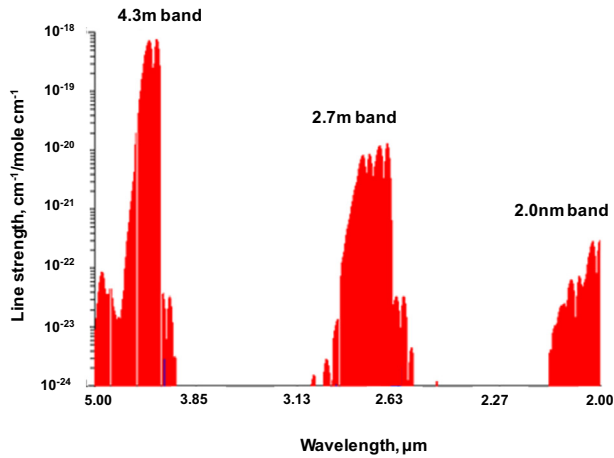


Fig. 1. Absorbance line strength of CO₂ at 300 K.

The direct-absorption spectroscopy fundamental theory has been explained in detail by many researchers [43,44] and it will be presented briefly to define our notation. When a beam of monochromatic light of intensity I_0 enters a homogeneous absorbing gas of length l , the intensity of the transmitted light I will be

$$I = I_0 e^{-kl} \quad (1)$$

where k is a constant called the gas absorption coefficient.

This law was discovered by J.H. Lambert in 1790 [45]. A. V. Beer [46] found that in many cases, the concentration coefficient is proportional to the concentration of the absorbing gas.

$$k = C^\epsilon \quad (2)$$

where C is the absorbing gas concentration and ϵ is the extinction coefficient of this gas.

The narrow-band laser absorption spectroscopy is governed by the basic physical relation stated in the Beer-Lambert law. It relates the intensity of light that enters an absorption medium I_0 to the transmitted intensity I as follows

$$\frac{I}{I_0} = e^{-\epsilon Cl} \quad (3)$$

The term $\frac{I}{I_0}$ is known as the transmissivity.

3. Experimental methods

3.1. Residual gas in a compression expansion machine

Fig. 2 Shows the compression-expansion machine, which can be fired once. This machine is specially designed for this study. The engine has a bore of 78 mm, stroke of 67 mm and compression ratio of 6.7:1. The spark timing was at 345 degrees and an engine speed of 600 rpm. The cylinder has a quartz window 52 mm in diameter at the centre, making it possible for visualization from below. For visualization, a high-speed video camera MEMRECAM GX-8 manufactured by NACK image technology with a camera speed of 3 kfps was used.

In this study, the measurements were carried out at different EGR ratios. Propane was used as a base fuel and pure gases were used to simulate the EGR compositions to approximate both the ideal combustion and reformer products of Propane

According to the stoichiometric combustion of propane, the EGR compositions were chosen.

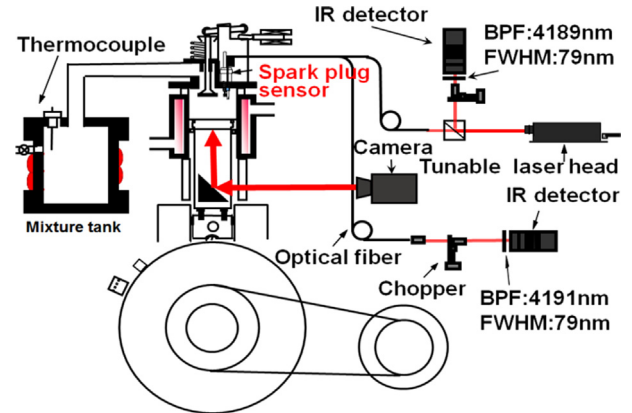
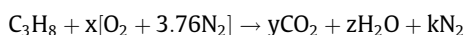


Fig. 2. Schematic of experiment set up with the compression- expansion machine.

We used 99% pure propane and dry compressed air. The EGR is simulated by a mixture of A% CO₂ and B% N₂ depending on the desired ratio. All the percentages were composition by volume. Since the addition of water to the combustion chamber was not practical, a mixture of CO₂ and N₂ was used to simulate the combustion product.

The EGR (%) in this study is defined as:

$$EGR\% = \frac{m_{EGR}}{m_{air+fuel} + m_{EGR}} * 100$$

where $m_{air+fuel}$ is the mass of fresh air and fuel, and m_{EGR} is the amount of exhaust gas that has the same volume of fresh air replaced. EGR ratio was changed from 10 to 40%.

A vacuum pump was used to evacuate the mixture tank and the chamber before each run. A pressure transducer was used to measure the pressure inside the combustion chamber. At every crank angle, the IR intensity signal in the cylinder pressure was recorded.

3.2. Optical sensor

An optical spark plug sensor (M14), which was modified from a commercial sensor [47,48] that allowed CO₂ concentration measurements near the spark plug under compression conditions, was used. Fig. 3 shows the construction of the modified optical sensor, which consists of three main optical parts: (1) two optical fibres, (2) a sapphire lens and (3) a metal mirror. Since the pressures and temperatures of the combustion gas are very high, the sapphire lens shields the fibres end faces from being damaged. The infrared light travelled from the laser source to the sensor using one of the optical fibres. The light passed through the sapphire lens and was then reflected by the mirror. The reflected light was transferred by the other optical fibre, passed through the sapphire lens again, and detected by a Hamamatsu Photonics

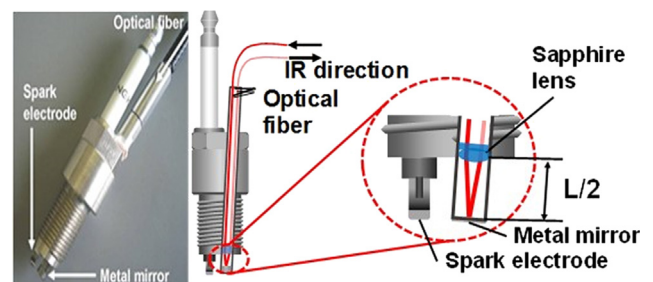


Fig. 3. Schematic diagram of spark plug sensor.

P4631_04 detector. As shown in the figure, the gap between the sapphire lens and the mirror was the measurement region. The measurement length was twice this gap, and since the light passes the gap twice in both directions, the measurement length was 11 mm. In this study a newly developed optical spark plug sensor (M12) was also used. The optical components is the same for both sensors, but the assembling method and the hole inlet is different as shown in Fig. 4.

3.3. Laser device and wavelength selection

In this experiment, a distributed feedback laser diode (DFB-LD) was used as an infrared light source, and a Hamamatsu Photonics P4631_04 detector was used as the IR detector. The laser device is shown in Fig. 5. The device uses mid-infrared (mid-IR) source radiation, which is based on difference frequency generation (DFG) in a periodically poled lithium niobate (PPLN) crystal. An additional wavelength oscillator power amplifier source was incorporated for simultaneous amplification of 1064 nm and 1426.5 nm signals in a fibre. The wavelengths in the range of 4175–4200 nm can be irradiated. The laser wavelength range can access the mid-range of the fundamental vibrational band of CO₂ near 4.2 μm. The upper graph in Fig. 5 represents the CO₂ absorption features in the range from 4170 nm to 4210 nm measured at temperature 300 K and 5% of CO₂. Further, the lower graph shows the reflected laser intensity, and wavelengths of 4175, 4190, 4195, and 4200 nm were selected.

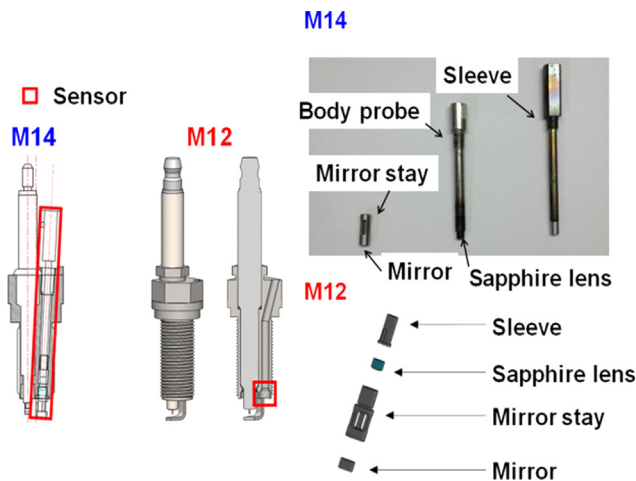


Fig. 4. Spark plug sensor M14 & M12.

The laser intensity and wavelengths were varied by changing the diode laser temperature and operating current [49,50]. A wave metre with a resolution of approximately 0.3 nm was used for the wavelength measurements

Since the intensity of absorption depends on the wavelength, it is necessary to select the suitable wavelength for measuring the CO₂ concentration under the experimental conditions. First the effect of pressure on the CO₂ absorption line was examined using HITRAN. Fig. 6 shows that the intensity of the absorption line greatly depends on the pressure.

When EGR increases, the engine operation reaches zones with higher instabilities and increased carbonaceous emissions. For this reason, the best wavelengths selection for the measurements was validated at EGR ratio of 40%. Fig. 7 shows the results of comparing the measurement results of the transmissivity measured at EGR 40% and the transmittance calculated from HITRAN at different wavelengths. I_0 can be obtained by measuring the intensity of infrared light through the beam splitter before entering the fibre. The solid lines indicate the measured value, and the symbols indicate the calculated value from HITRAN. The transmittance value calculated using HITRAN was obtained by using the pressure and the concentration value of CO₂ contained in EGR 40% at five points of -180, -135, -90, -45, 0 deg ATDC. From the transmittance history, it was confirmed that the CO₂ molar concentration increased as compression progressed, and more absorption occurred. From these five wavelengths, the wavelength of 4195.7 nm was selected

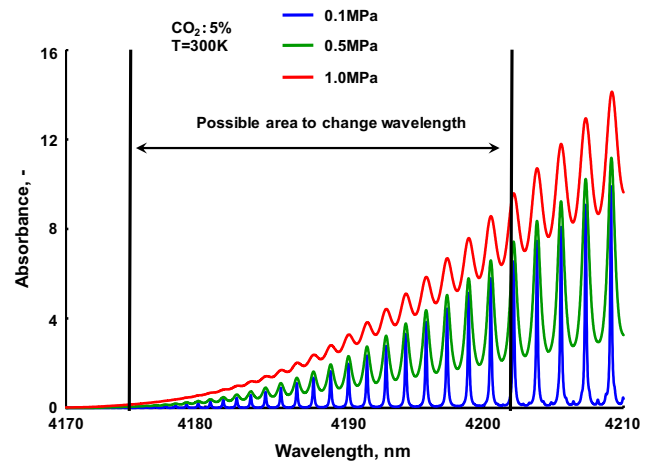


Fig. 6. Effect of pressure on CO₂ absorption line (4170–4210 nm).

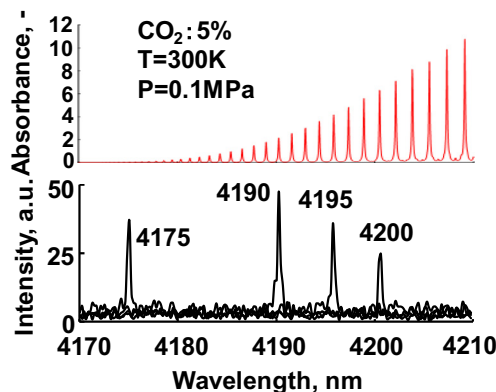
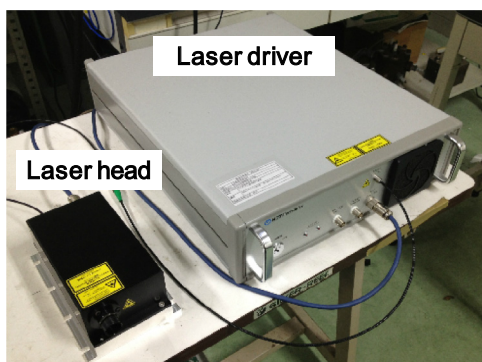


Fig. 5. Infrared light source and examples of the wavelength.

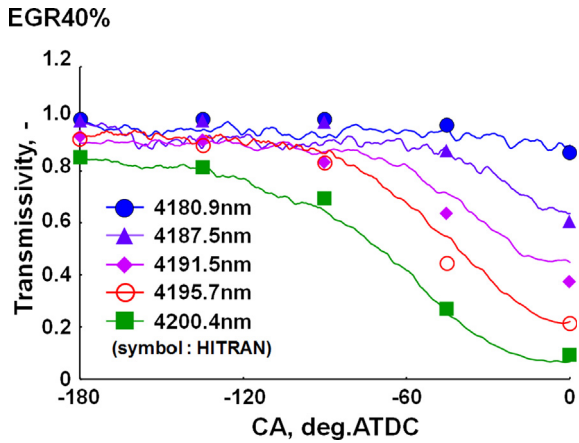


Fig. 7. Comparison between measured transmissivity and HITRAN at different wavelengths.

as the wavelength at which the absorption was too strong and the transmittance was not much less than 0.2, particularly in the vicinity of the compressed TDC. In addition, when examining the error of the calculated value from HITRAN, the error of 4200.4 nm at -45 deg for the ATDC is approximately 24%; for the errors of 4191.5 nm and 4200.4 nm at 0 deg, the ATDC increases to approximately 17% and 36%, respectively, although it was confirmed that the error was approximately 10% elsewhere.

Initially, The IR transmissivity was measured at wavelength 4195.7 nm using M12 and M14 optical sensor at EGR 10% and EGR 40% as shown in Fig. 8. The transmissivity data with M12 is the average value of 3 cycles, while that for M14 is the average value of 15 cycles. This may explain the fluctuation for the transmissivity measured using M14. The measurement was performed using M14 spark plug because of the limitation of accuracy of the initial light intensity measurement with the M12 spark plug.

Fig. 9 shows the pressure and temperature history, per crank angle degree at each EGR condition, the initial temperature inside the mixture tank was only measured, while the polytropic process equation is utilized to calculate the temperature during the compression. The pressure and temperature are changed inside the cylinder, especially in combustion and expansion stages. The pressure peak value was for lower EGR ratio (10%).

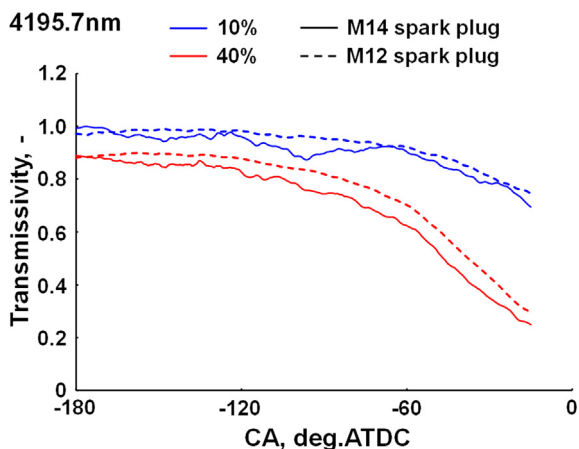


Fig. 8. Comparison of transmissivity with M12 & M14 using 4195.7 nm.

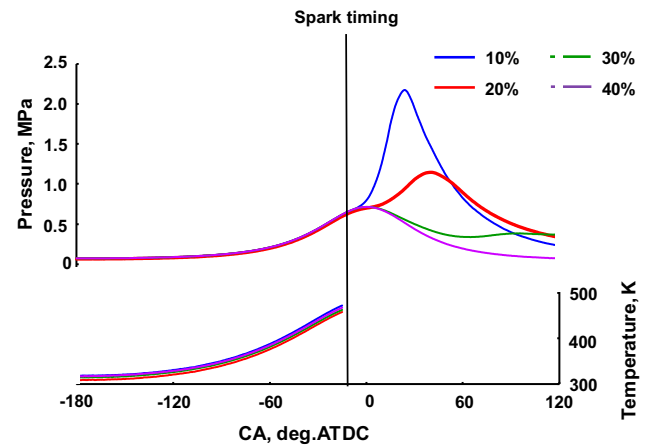


Fig. 9. Pressure and temperature history.

4. Results and discussion

The effect of the CO_2 influence on the flame propagation was investigated by visualizing from the bottom of the compression-expansion machine. A MEMRECAM GX-8 high speed camera with a speed of 3 kfps manufactured by NACK Image Technology was used. Fig. 10 shows the flame propagation change every 6 deg from -15 deg ATDC, which is the spark timing. It can be shown that the flame spread very quickly, which caused the combustion to finish quickly. For EGR 30%, the pressure showed a slight change, which resulted in the combustion slightly burning. Almost no combustion occurred at 40% EGR. At higher EGR, a reduction in the flame temperature as a result of the spatial broadening of the flame is caused as a result of displacement of oxygen by inert gases. This reduction of the peak combustion temperature slows down the combustion speed. Also heat capacity is changed, since the specific heat capacity of the exhaust gas is higher than that of air. So a mass of gas containing EGR will have a lower temperature than pure air for the combustion energy same amount.

Next, the measurement results for the pressure and temperature history from -180 to 0 deg ATDC and the transmittance under each EGR condition are shown in Fig. 11. The results of the transmittance shown in Fig. 11 show the average value for three cycles.

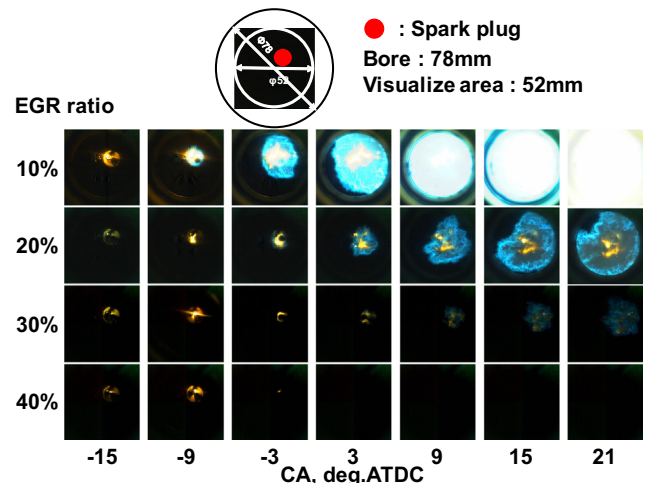


Fig. 10. Visualization of combustion in each EGR ratio.

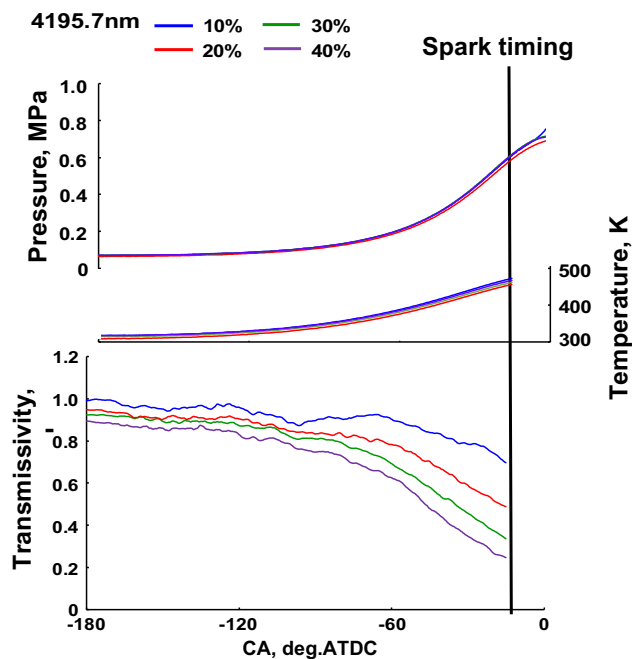


Fig. 11. Pressure, temperature and transmissivity history.

The result of the CO_2 concentration calculated from the transmittance result is shown in Fig. 12. The broken line is a value obtained by previously calculating the concentration of CO_2 contained in the premixed gas, and the solid line shows the measurement result. The maximum deviation between the calculated and measured values between -90 and 0 deg ATDC was approximately 54% at EGR 10%, 28% at EGR 20%, 10% at EGR 30% and 10% at EGR 40%. However, when looking at the maximum deviation between -60 and 15 deg, the ATDC was approximately 18% for EGR 10%, 8% for EGR 20%, 6% for EGR 30% and 10% for EGR 40%. For the overall EGR results, the deviation was less than 20%, and the maximum deviation under the condition of an EGR rate from 20 to 40% was less than approximately 10%. The deviation between the measured and the present values may be attributed to the small change in pressure and the large volume in the vicinity of -90 deg ATDC so that the molar concentration is small. The engine vibration which may also affect the light transmitted from the optical fibres. Also the measurement error resulting from noise and repeatability for any laser-based measurement system play a role in the deviation.

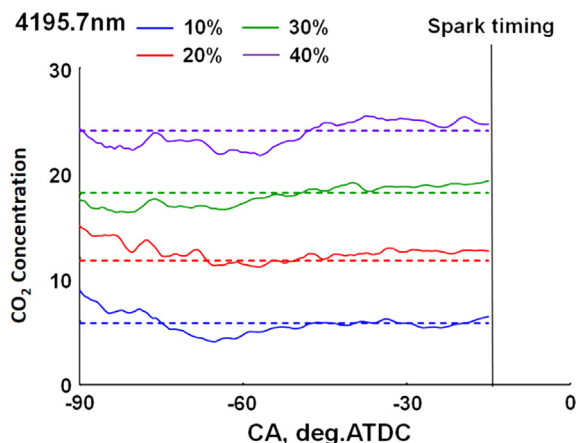


Fig. 12. Comparison of CO_2 mass from the transmittance results and that contained in the premixed gas.

5. Conclusion

In a compression-expansion engine, a premixed gas was prepared, and the CO_2 concentration near the spark plug was measured by the IR absorption method at different EGR ratios. A distributed feedback laser diode (DFB-LD) was used as the infrared light source with a wavelength near $4.2 \mu\text{m}$, which is the fundamental vibrational band of CO_2 . Propane was used as the base fuel, and pure gases were used to simulate the EGR compositions to approximate both the ideal combustion and propane reformer products. The wavelength at 4195.7 nm was chosen for high CO_2 concentration measurements at different EGR ratios. As a result, the following knowledge was obtained:

1. CO_2 concentration measurements near the spark plug can be performed at different EGR ratios by the IR absorption method.
2. When quantitatively measuring the CO_2 concentration in the vicinity of the spark plug, the maximum deviation between the measured and the present values was approximately 20% for the overall EGR ratio conditions.

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