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4-21-2020

## Renewable Ammonia

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## Renewable Ammonia

### Abstract

Ammonia is one of the most widely used chemicals that is commercially produced today given the wide need for fertilizer to sustain the world's ever-growing populations. Given the high world demand for ammonia, which increases every day, one can see how beneficial to the environment that a zero emission large-scale ammonia plant would be. Through the use of energy from Norwegian wind farms, which produce an excess of energy during off-peak hours, our plant design seeks to turn this wasted energy into useful ammonia products at a production rate of 67.2 kmol/hr.

The design of this ammonia synthesis plant can be split conceptually into two distinct halves. The first is the refinement of the hydrogen and nitrogen that are required for the Haber-Bosch synthesis from the raw inputs of air and water. This is done through the usage of solid oxide electrolytic cells which electrolyze the water into constituent hydrogen and oxygen atoms and separate the oxygen out of the air. The second half of the plant design is a typical Haber-Bosch ammonia synthesis that many plants today are utilizing. This section consists mainly of a reaction vessel at the correct operating conditions for the ammonia synthesis reaction to occur, and a series of separators that recoup the liquid ammonia product at the right conditions for storage while recycling the gaseous hydrogen and nitrogen reactants.

While this plant design provides a layout to accomplish the task of producing ammonia in an environmentally friendly way, it is less friendly to the wallet of the plant owner. Selling the ammonia product at current market rates of \$853/ton, it would take roughly 15 years for the plant to overcome the capital investment of the venture and become a monetarily net positive design. Current utility prices are projected to cost the plant over \$1.7 million dollars per year, which is another significant consideration why it takes such a large amount of time for the plant to become profitable.

It is our hope that ongoing refinement of solid oxide electrolytic units will enable their purchase at cheaper rates, and that as the environment worsens, a higher premium will be placed on chemical products that have been sourced renewably, both factors that could easily make this plant design a more viable option in the future than it currently is today.

### Disciplines

Biochemical and Biomolecular Engineering | Chemical Engineering | Engineering

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21 April 2020

Dear Mr. Bruce Vrana, Mr. Leonard Fabiano, and Dr. Raymond Gorte,

Please find attached our final report for CBE 459: Senior Design. Our project, titled “Renewable Ammonia”, was proposed by two of our group members, James Kwon and Dakota Wallach. This project design focuses on the utilization of excess wind energy produced in Norway to produce liquid ammonia, creating a useful chemical product with no carbon footprint.

In the body of the report you will find our preliminary design for this plant, including a full economic analysis and the projected future feasibility of this design. The size of this ammonia production is on the smaller scale of a full-size facility, producing 46 MT/day of liquid ammonia. The cost associated with construction of this plant is comparatively large, due to the high cost of the solid oxide electrolytic cells (SOECs) that are utilized. The calculated net present value (NPV) of this plant is USD -22M, and the return on investment (ROI) is -0.68%.

Based on the findings of our analysis, we found that it would require operation of the plant for a large number of years before plant operation would become profitable. A number of external considerations, such as SOECs becoming considerably cheaper over time, the price of green ammonia increasing, or an increased carbon tax on plants that are not operating renewably could shorten this time before profitability is reached. Unfortunately, as for now it appears that operation is not profitable enough to be pursued at this time, and we recommend that any interested parties carefully consider the following report before making a final decision on construction of this plant.

Sincerely,

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Kolbein Finsnes

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James Kwon

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Dakota Wallach

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# 1. Abstract

Ammonia is one of the most widely used chemicals that is commercially produced today given the wide need for fertilizer to sustain the world's ever-growing populations. Given the high world demand for ammonia, which increases every day, one can see how beneficial to the environment that a zero emission large-scale ammonia plant would be. Through the use of energy from Norwegian wind farms, which produce an excess of energy during off-peak hours, our plant design seeks to turn this wasted energy into useful ammonia products at a production rate of 67.2 kmol/hr.

The design of this ammonia synthesis plant can be split conceptually into two distinct halves. The first is the refinement of the hydrogen and nitrogen that are required for the Haber-Bosch synthesis from the raw inputs of air and water. This is done through the usage of solid oxide electrolytic cells which electrolyze the water into constituent hydrogen and oxygen atoms and separate the oxygen out of the air. The second half of the plant design is a typical Haber-Bosch ammonia synthesis that many plants today are utilizing. This section consists mainly of a reaction vessel at the correct operating conditions for the ammonia synthesis reaction to occur, and a series of separators that recoup the liquid ammonia product at the right conditions for storage while recycling the gaseous hydrogen and nitrogen reactants.

While this plant design provides a layout to accomplish the task of producing ammonia in an environmentally friendly way, it is less friendly to the wallet of the plant owner. Selling the ammonia product at current market rates of \$853/ton, it would take roughly 15 years for the plant to overcome the capital investment of the venture and become a monetarily net positive design. Current utility prices are projected to cost the plant over \$1.7 million dollars per year, which is



another significant consideration why it takes such a large amount of time for the plant to become profitable.

It is our hope that ongoing refinement of solid oxide electrolytic units will enable their purchase at cheaper rates, and that as the environment worsens, a higher premium will be placed on chemical products that have been sourced renewably, both factors that could easily make this plant design a more viable option in the future than it currently is today.

## 2. Introduction

### 2.1 Project Background

The Haber Bosch process (1910) is a fundamental chemical process that has fueled both economic and population growth. The invention brought about the mass production of ammonia, and both Haber and Bosch were awarded the Nobel Prize in Chemistry in 1918 and 1931 respectively. The process was first commercialized in 1913, proving instrumental to the growth of agricultural yields and more broadly sustenance of the human population. The inputs to the Haber Bosch processes are simple since it uses gaseous hydrogen and nitrogen reacted at high pressures and moderately high temperatures to produce gaseous ammonia which can subsequently then be cooled and liquefied. Nitrogen comprises 79% of the atmosphere by volume, and is generally obtained from air by separating oxygen. This is accomplished through a number of different air separation processes such as fractional distillation and pressure swing adsorption among others. Hydrogen, however, does not occur naturally and must be synthesized from some other source. Currently, most of the world's Hydrogen is synthesized using steam reforming, a process that converts methane (sourced from natural gas) into hydrogen and carbon dioxide.<sup>1</sup> However, one of the major drawbacks to this process is that it depends on fossil fuels that are not only unsustainable but harmful for the environment.

In recent years, there has been a large movement both in and outside of the scientific community to shift away from the use of fossil fuels. Consequently, this shift is not met without problems since major renewable energy sources continue to face issues of volatility, cost, and

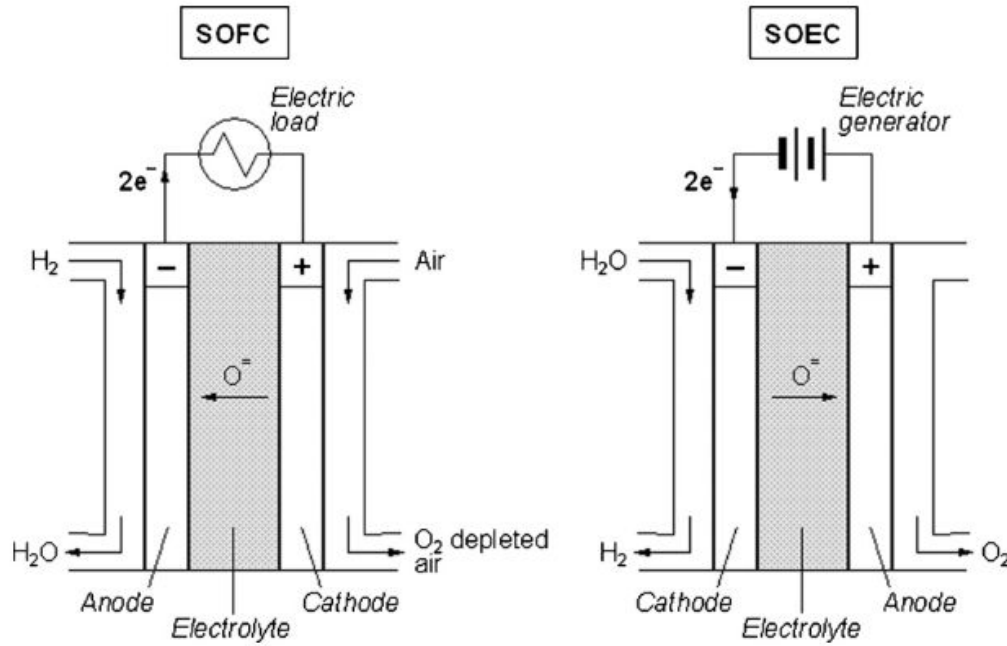
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<sup>1</sup> Holladay, J.D., Hu, J., King, D.L., Wang, Y. (2009)

implementation. For example, renewable sources of energy such as wind or solar are often highly unreliable, with energy generation directly linked to uncontrollable factors such as wind speed, or daily hours of sunshine. As a result, an excess of energy is produced at times; at other times, there is a lack of electricity available. Excess energy is typically wasted or sold to other locations and can be a problem for energy producers. Rather than selling this excess, many firms have begun exploring ways to better maximize its utility by using the energy to drive processes such as producing hydrogen gas through the electrolysis of water.

A significant technological innovation that our process utilizes is in the method in which it produces hydrogen. Compared to the most popular form of hydrogen production (steam reformation) utilization of the solid oxide electrolyzer eliminates carbon emissions. Typically, this sort of system is run as a fuel cell where fuel is consumed in order to produce energy. Fuel in a gaseous form is run on the anode side where molecules will react with the yttria stabilized zirconia (YSZ) based Ni catalyst and oxygen ions from an oxygen input in the cathode migrate to the other side producing water and electricity. Typical materials include nickel mixed with Yttria Stabilized Zirconia (Ni-YSZ) for the anode and lanthanum strontium manganate (LSM) for the cathode. However, in our system, the cell is essentially run in reverse taking electricity as an input to split water molecules. Water in the form of steam is run on the cathode side where it is electrolyzed to  $H_2$  and  $O^{2-}$  ions. These  $O^{2-}$  ions travel across the electrolyte and recombine on the anode side to produce oxygen. A diagram of this process versus standard fuel cells can be seen in the figure below.

Figure 2.1a: Visual depiction of how a solid oxide fuel cell (SOFC) and a solid oxide electrolyzer (SOEC) function.<sup>2</sup>



In addition, the system is able to achieve nitrogen separation with the oxygen as the potential at which the oxygen molecules react with the electrodes occur at a value close to 0V. The  $O_2$  pressure difference between the two electrodes serves as a driving force for the separation of the oxygen from the nitrogen as well. Both electrolyzers and fuel cells are fabricated as smaller cells and combined to form giant stacks to permit larger amounts to be processed.

Following the generation of hydrogen and separation of nitrogen, these materials will be put into the Haber Bosch process. The initial feed to the ammonia synthesis reaction vessel is a mix of nitrogen and hydrogen, along with trace amounts of argon. The reactants are fed into the vessel at relatively high temperatures, slightly above 200 degrees Celsius, and at an incredibly

<sup>2</sup> Iora, P., Chiesa, P. (2009)

high pressure of over 80 atmospheres of pressure. The reaction by which ammonia is synthesized is given below as *Equation 2.1a*.

*Equation 2.1a: Reaction of Hydrogen and Nitrogen to Form Ammonia*



As one may notice, this reaction is immensely exothermic, meaning that a large amount of heat energy is produced as a result of this reaction proceeding. This also explains why the reaction requires such extreme conditions in order to make the reaction proceed. In order to facilitate this reaction, an iron catalyst is added, which is usually made of magnetite or similar ore. In this process, an iron catalyst doped with sodium has been chosen, as this catalyst is sufficiently efficient for the needs of our process at a price point that is more reasonable than other catalysts made of precious minerals. The addition of a high surface area iron catalyst creates a surface to which the hydrogen and nitrogen can adsorb strongly to, which facilitates the slowest step of this reaction, the splitting of the diatomic nitrogen into singleton components. The largest concern regarding the catalyst is that care must be taken to ensure that no oxygen is allowed to enter the vessel where the catalyst is used. Oxygen reacts strongly with iron in order to form metal oxides, which effectively poisons the catalyst and renders it useless. In order to avoid this, precautions are taken to ensure that the air entering the process has been sufficiently separated into oxygen and nitrogen, with the oxygen being vented out and sold. It is important to note that it is possible to regenerate the iron catalyst under some circumstances, but would require shutting down plant operations, which comes at a significant cost.

## **2.2 Project Proposal**

The goal of this project was to design an ammonia plant that would utilize excess wind energy to drive electrolyzers which would produce the necessary inputs to the Haber Bosch process. Electrolysis of steam would form hydrogen while the nitrogen from the air would be separated through the electrolyzer as well. A solid oxide electrolyzer (SOEC) was chosen due its ability to utilize thermal and electrical processes to increase the efficiency of the overall process. One thing to note is that the scale to which we plan to use our SOECs currently do not exist but are expected to reach those sizes in the foreseeable future. All costs and various calculations were taken with values available as of today. The Haber Bosch process is typically a very energy and carbon intensive process due to the production of its feed streams but utilization of electrolysis largely eliminates both of these issues. The plant was designed with the goal of being as environmentally friendly as possible and carbon neutral. Extensive profitability and market analyses were conducted to determine necessary pricing measures for this process to become economically viable.

## 2.3 Project Timeline

Figure 2.3a: Graphical Depiction of Project Timeline

Activity	Jan	Feb	March	April
<b>RESEARCH</b>				
Identifying key markets for profitability	█	█		
Green hydrogen production and storage	█	█		
Review of relevant literature	█	█		
Review commercial products and processes	█	█		
<b>SCIENTIFIC MODELING AND ECONOMICS</b>				
ASPEN modeling of reactor		█	█	
Preparing financial model		█	█	█
Plant design		█	█	█
<b>DELIVERABLES</b>				
Mid-semester check in			█	
Final presentation				█
Final written report				█
Final full profitability analysis				█

Our project timeline can be seen in the figure depicted above. The bulk of our research and preparation took place in January and February where a plan for producing such hydrogen and the information relevant to the Haber Bosch process was determined. During February and March, the majority of the modelling of the entire process was initiated as the specific variable of plant operation and its various components were determined. The work in April mostly consisted of profitability analysis, the preparation of the final presentation, and the synthesis of the relevant findings into a final written report.

## 3. Market and Competitive Assessment

### 3.1 Uses

Ammonia (NH<sub>3</sub>) is a colorless gas at standard temperature and pressure. In 2019, more than 80% of ammonia produced was used by the agriculture industry as fertilizer.<sup>3</sup> This represents the largest industry use of ammonia by both mass and revenue.

Instead of only relying on farming techniques such as crop rotation and allowing land to lie fallow, fertilizer provides an alternative that drastically increases efficiency in farming. When crops grow in a field, nitrogen in the soil is depleted. Some plants, such as legumes, are nitrogen fixers, whose roots have bacteria that increase the amount of nitrogen present in the soil. Although nitrogen is highly present in the atmosphere (comprises 79% of air), it cannot be used in its elemental form. Ammonia as fertilizer has decreased the need for nitrogen fixers, and has drastically increased the efficiency of farms.

Ammonia can either be directly applied to soil or converted to a salt (such as ammonium nitrate) through a straightforward crystallization process and then applied. This report covers only the production of ammonia from raw materials. Although use of ammonia varies by farm and crop, a safe estimate is that 1 ton of anhydrous ammonia covers about 9.6 acres of farmland for standard application of fertilizers. Alternatively, 104kg of anhydrous ammonia is necessary per acre, per year.<sup>4</sup>

Ammonia is also used in cleaning products such as Windex and other glass cleaners.

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<sup>3</sup> Mordor Intelligence, Ammonia Market (2020), Retrieved April 9th, 2020 from <https://www.mordorintelligence.com/industry-reports/ammonia-market>

<sup>4</sup> Schnitkey, Gary, "Nitrogen Fertilizer Prices and Costs Lower for 2018", November 2017, Accessed April 10th, 2020 from <https://farmdocdaily.illinois.edu/2017/11/nitrogen-fertilizer-prices-and-costs-lower-for-2018.html>



### 3.2 Market Overview

In 2020, the global ammonia market size is projected to be worth roughly USD 72.8 billion, with a CAGR of ~1.1%.<sup>5</sup> The market is highly commodified and low growth (global GDP growth is projected to be ~3%). Nearly all hydrogen is currently sourced from natural gas via steam reforming. North America and Europe are classified as medium growth areas for demand of ammonia, for this industry.<sup>6</sup> High growth regions include China, Russia, Brazil and sub-Saharan Africa. (Mordor Intelligence)<sup>7</sup>. More than half of ammonia is consumed in Asia. This market share is expected to grow, as regions in Asia have high population growth rates and strong agricultural industries that rely on fertilizers.

### 3.3 Competitors

Due to the massive size of the ammonia market and uniformity of ammonia, the market is highly fragmented, with many players and high levels of competition. This is typical of highly commoditized markets, business to business markets. Margins are generally very small, and supply chains are fully integrated to cut costs. The world's largest ammonia producer is Norway based Yara. Other major players include BASF (the "firm that tasked Carl Bosch with the commercialization of Fritz Haber's ammonia synthesis process in 1910" - AmmoniaEnergy.org), CF Industries, Qatar Fertilizer Company, SABIC and EuroChem. (Mordor Intelligence).

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<sup>5</sup> MarketWatch, Ammonia Market 2020, March, 2020, Retrieved April 10th 2020, from <https://www.marketwatch.com/press-release/ammonia-market-size--industry-growth-analysis-2020-regional-outlook-trends-opportunity-revenue-share-forecasts-by-2025-2020-03-02>

<sup>6</sup> Mordor Intelligence, Ammonia Market (2020), Retrieved April 9th, 2020 from <https://www.mordorintelligence.com/industry-reports/ammonia-market>

<sup>7</sup> Ibid.

The above firms produce ammonia from fossil fuels, which produce greenhouse emissions and rely on the oil and gas industry. There are currently very few firms operating in the green ammonia space, and there are no wind-power green ammonia plants currently built. Many large ammonia players (such as Yara) are attempting to innovate and move into green ammonia should costs lessen and commercial viability increase. Even though ammonia produced from fossil fuels and wind farms is identical, if carbon tax credits were to make green ammonia more viable, it could disrupt the ammonia industry and become a space for mass innovation.

## 4. Preliminary Process Synthesis

### 4.1 Hydrogen Generation

While there are many different methods for producing hydrogen, hydrocarbon reforming is responsible for producing the vast majority of hydrogen consumed today. Hydrocarbon reforming can be performed by steam reforming, partial oxidation, or a combination of the two, autothermal reforming. These processes are essentially similar but still contain enough nuances to warrant different. For large-scale processes, steam reforming is the most practical since it does not require oxygen, has the lowest process temperatures and the best  $H_2/CO$  ratio for  $H_2$  production. These advantages are partially offset in regards to the process as a whole since the air emissions are the highest of the three.<sup>1</sup> The goal of the project was to produce hydrogen utilizing a greener method to produce the feedstock for the Haber Bosch process. This led to water electrolysis since this is the next most efficient method for producing hydrogen.

There are a number of different ways to accomplish water electrolysis, with commercialization proceeding on electrolyzers based on alkaline, polymer membrane, and solid oxide membranes. Solid oxide electrolyzers were chosen due to their high efficiencies, associated in part with their high operating temperatures. High temperatures greatly reduce electrode overpotentials and allow overall system efficiencies by using the waste heat to assist in the overall production of hydrogen. For modelling purposes, we use solid oxide fuel cells (SOFC) as a guideline as they are essentially SOECs run in reverse.

## 4.2 Nitrogen Separation

The nitrogen that is to be used in the process will be sourced from air. However, since nitrogen is not the only component present in air, extra steps must be taken to remove the other components (mainly oxygen) from the air. There are a number of different methods that are used in industry to separate air: fractional distillation, pressure swing adsorption, and vacuum swing adsorption. Out of these methods, fractional distillation in the form of cryogenic air separation is the most common. This process requires a tight integration of heat exchangers and separation columns to obtain an overall good efficiency for the process. One of the advantages of utilizing the SOECs is that the process of removing oxygen from the air comes at close to no energetic cost as the voltage at which this occurs is roughly around 0V. In our process, oxygen removal is accomplished partly due to the reaction between hydrogen and oxygen which generates water and the removal of the remaining oxygen across the electrolyzer. This eliminates the need for the purchase of the air separation and is integrated directly as a part of our process.

## 4.3 Utilization of Excess Wind Energy

To power the solid oxide electrolyzers, the standard approaches of utilizing traditional electricity sources were cast aside in favor of utilizing excess wind energy. Due to the intermittent nature of wind and solar energy, electricity generation varies depending on the position of the sun or the amount of wind that is blowing at any given moment. This leads to discrepancies in generation since there are times of the day (particularly at night when electricity

usage is low) when the electricity demand is less than the electricity generated by these sources. The excess electricity is typically sold off to other countries or stored in some form. As an alternative, it was decided that renewable excess energy should be used as the energy source for our electrolyzers. However, this by no means suggests that our process will be shut off when there is no wind available, the discrepancies will be supplied by electricity that is purchased and available on demand. Wind energy in particular was chosen as the source of energy as wind farms are typically located near bodies of water serving as a perfect location to source our water input to the process as well.

## 5. Assembly of Database

### 5.1 Cost of Chemicals

The raw materials utilized in this design are water and air. There is not an associated purchase price with either of these starting reagents, as they can both be sourced free of cost. The cost associated with separating these raw materials into the desired hydrogen and nitrogen inputs into the Haber-Bosch process are contained in the costs of the unit modules and electricity. Other costs, including water to be used as steam or for cooling throughout the process, are taken from standard pricing guidelines and included in Section 16.

The product that will be sold is liquid ammonia that will be stored at low temperatures and lightly pressurized. The market price for our ammonia will be \$500/ton, which is competitive in the current market. Considerations were made to theoretically include the price of ammonia sold per ton due to the fact that the ammonia produced by this process will be made exclusively using renewable energy, and, as such, could be worth the extra price to environmentally conscious purchasers. As of now, concerns over pricing our ammonia out of the market outweigh this potentially monetary benefit until it becomes clearer that there is enough demand for green ammonia to justify an increased price.

### 5.2 Catalyst Properties

Catalysts are frequently employed to increase the rate of reactions, typically by lowering some activation energy barrier without the catalyst being consumed in the process. For the Haber-Bosch reaction, a potassium-doped porous iron catalyst is the most common due to the

significant increase in reaction rate, along with the cheaper price of iron compared to more expensive catalyst materials. For this reaction, the Haldor Topsoe KM 111 magnetite catalyst was chosen for its proven success and stability in ammonia synthesis processes. This catalyst works by providing a surface to which the hydrogen and nitrogen will both strongly adsorb to. The fact that the catalyst is porous is of note because the increase in surface area allows for more catalysis to occur on the surface, increasing the reaction rate significantly.

### 5.3 Chemical Properties

Material Safety Data Sheets (MSDS) for each of the components of this process can be found in *Appendix C*. Considerations based on the safety of the chemicals in this process were obtained from the MSDS's, and can be found in *Appendix C*. The property data for the components of our process can be found in **Table 5.3a** and **Table 5.3b** below.

*Table 5.3a* Properties of Chemicals in Process (at STP)

Chemical Name	Molar Mass (lb/lbmol)	Density (lb/ft <sup>3</sup> )	Boiling Point (°F)	Heat Capacity (BTU/lb°F)
Water	18.02	62.43	212.0	1.001
Oxygen	15.99	0.08	-297.4	0.212
Hydrogen	2.02	0.01	-423.2	3.42
Nitrogen	32.00	0.07	-320.4	0.25
Argon	39.95	0.11	-302.5	0.12
Ammonia	17.02	0.044	-28.0	0.52

Table 5.3b Properties of Utilities in Process

Material	Inlet Temperature (°F)	Heat Capacity (BTU/lb°F)
Cooling Water	80	1.001
Chilled Water	45	1.001
Chilled Brine	0	1.001*

\*In our simulation, chilled brine was approximated to have the heat capacity of water

## 5.4 Aspen Simulation Specifications

The overall design was simulated in ASPEN Plus V11. The SRK property method was used throughout the simulation except for the SOEC and autothermal reactions which occurred in RSTOIC blocks which were manually input using calculations done in Excel and by hand.

The autothermal reaction was modelled in ASPEN using a mixer block to combine the streams and an RSTOIC block was used to show the extent of the reaction. The calculations regarding the amount of reactants formed and the temperature change that occurred was done by Excel using specific heats and enthalpy values at 800°C that were obtained from the NIST database.

The SOEC was modelled by taking the power and using a specified voltage and current to determine exactly how much hydrogen would be converted by the system. In ASPEN, these conversion values were input into an RSTOIC block and the molar flow rate of the reaction was used to convert the products. A SEP unit was used to split the stream into its two components because in a real system, the products of the reactions end up forming on the other side of the electrolyzer and never mixes with the cathode inputs to the process.



Coolers, heat exchangers, and condensers in the system were modelled using the HX block in ASPEN. Both the coolers and condenser had cold water running as the cooling fluid in the system. For the condenser however, since the process leads to two different phases being formed, an additional SEP unit was added to ensure that there was separation of the two phases.

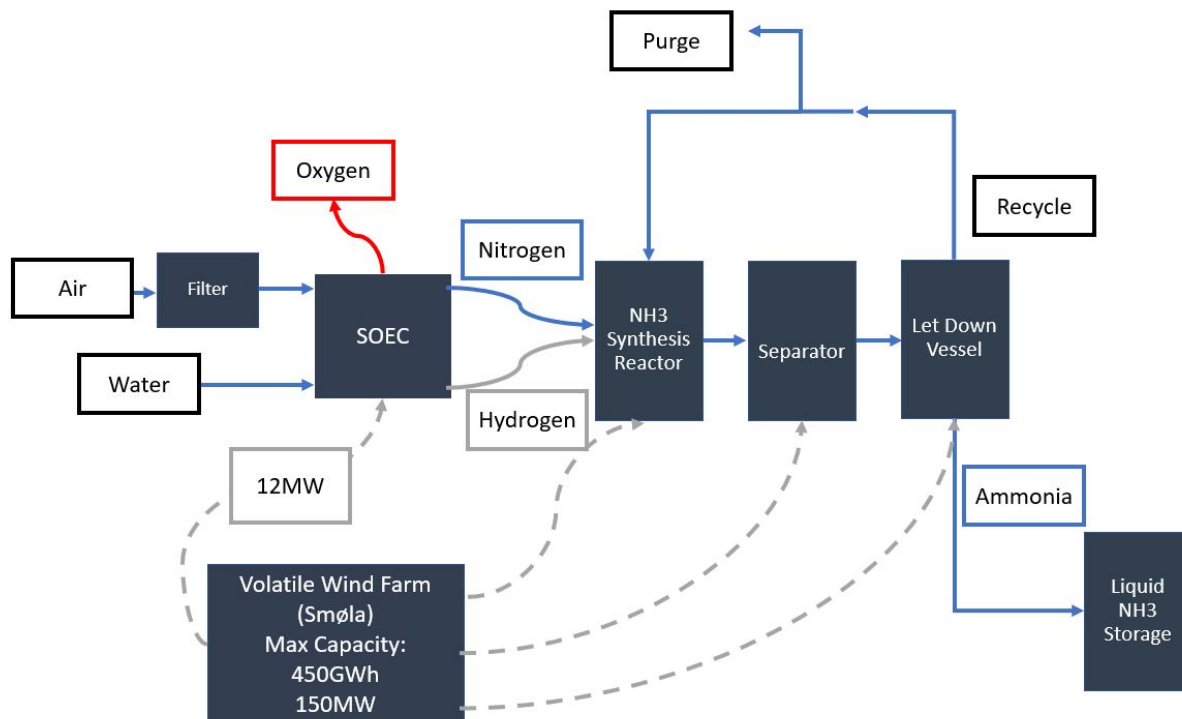
In the Haber Bosch process, the reaction vessel was modeled as an RSTOIC block as well with the reaction information input into the system to determine the conversion and the flow rates of the output. Both the primary separation vessel and the let-down vessel were modeled as SEP units.

## 6. Process Flow Diagram and Material Balances

### 6.1.1 Overall Simplified Process Flow Diagram

A simplified version of the overall process can be seen in **Figure 6.1.1**. This diagram incorporates all of the major components of the process and contains the input and exit streams of the process as well.

*Figure 6.1.1* Overall flow sheet which describes the major processes involved in ammonia synthesis, including reactants, intermediates, and ammonia product.



## 6.1.2 Overall Material Balance

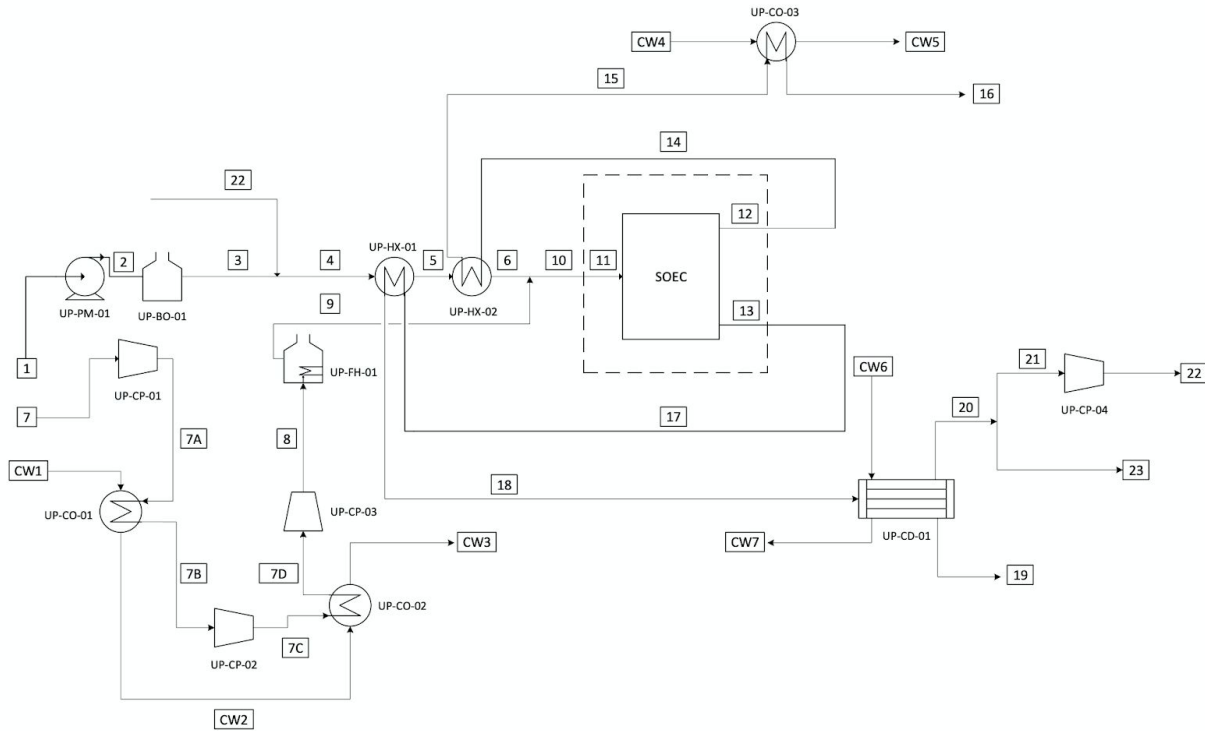
Table 6.1.2a Overall Material Balance Descriptions

Stream	Water In	N <sub>2</sub> In	O <sub>2</sub> In	Ar In	H <sub>2</sub> Out	N <sub>2</sub> Out	Ar Out	NH <sub>3</sub> Out	O <sub>2</sub> Out
Temp (°C)	25	25	25	25	20	20	20	20	35
Pressure (atm)	1	1	1	1	10.1	10.1	10.1	10.1	38.9
Mass Flow (kg/hr)	8858	1599	493	26	0.02	9.2	2.8	19448	2739
Mole flow (kmol/hr)	491.7	57.1	15.4	0.66	0.01	0.33	0.07	1144	84.4

## 6.2.1 Process Flow Diagram of the Solid Oxide Electrolytic Cell Processes

The overall process flow diagram for the generation of the inputs (hydrogen and nitrogen) to the Haber Bosch process is depicted in **Figure 6.2.1a**.

Figure 6.2.1a: Process flow diagram with all of the physical units involved in the process.



The process begins with water and air entering as streams 1 and 7 respectively. Both streams undergo a compression process to 40 bars and are heated then later mixed in the process. As this mixed temperature is moderately high, it undergoes the oxyhydrogen reaction and enters the SOEC system at 800°C. The remaining oxygen is separated out and the water is electrolyzed to hydrogen and oxygen. The stream entering the box with the dotted line will be split into 24 and enter 24 different SOEC stacks rated at 500kW. Streams 11 and 12 are the output of each of the 500kW SOEC units and combined to form streams 13 and 14. Effectively, the system will be run in parallel. Stream 14, which contains pure oxygen, will be cooled and sent for storage. Stream 17, which contains water, hydrogen, nitrogen, and argon will be condensed to eliminate the water and some of the gas will be used as inputs to the Haber Bosch process while the rest will be recycled in the process.

## 6.2.2 Material Balance of the Solid Oxide Electrolytic Cell Process

Table 6.2.2a summarizes the basic stream properties and material flow rates of all the streams pictured in Figure 6.2.1a

Table 6.2.2a: Summary of the streams properties and flow rates drawn in the PFD

Stream Number	1	2	3	4	5	6	7	7A
Temperature (°C)	25	26.2	420	379.9	590	610	25	197.9
Pressure (bar)	1	40	40	40	39.7	39.3	1	3.42
Mass Flow (kg/hr)	8858.1	8858.1	8858.1	9545.7	9545.7	9545.7	2118.7	2118.7
Molar Flow (kmol/hr)	491.7	491.7	491.7	563.1	563.1	563.1	73.2	73.2
<b>Components (kmol/hr)</b>								
H <sub>2</sub> O	491.7	491.7	491.7	491.7	491.7	491.7	0	0
H <sub>2</sub>	0	0	0	50.6	50.6	50.6	0	0
N <sub>2</sub>	0	0	0	20.6	20.6	20.6	57.1	57.1
O <sub>2</sub>	0	0	0	0	0	0	15.4	15.4
Ar	0	0	0	0.24	0.24	0.24	0.66	0.66

Stream Number	7B	7C	7D	8	9	10	11	12
Temperature (°C)	37.8	236.2	37.8	222.9	550	800	800	800
Pressure (bar)	3.1	11.7	11.4	40	40	39.3	39.3	39.3
Mass Flow (kg/hr)	2118.7	2118.7	2118.7	2118.7	2118.7	11664	486	114.1

<b>Molar Flow (kmol/hr)</b>	73.2	73.2	73.2	73.2	73.2	620.9	25.9	3.6
<b>Components (kmol/hr)</b>								
<b>H<sub>2</sub>O</b>	0	0	0	0	0	522.5	21.8	0
<b>H<sub>2</sub></b>	0	0	0	0	0	19.8	0.8	0
<b>N<sub>2</sub></b>	57.1	57.1	57.1	57.1	57.1	77.7	3.2	0
<b>O<sub>2</sub></b>	15.4	15.4	15.4	15.4	15.4	0.0	0	3.6
<b>Ar</b>	0.66	0.66	0.66	0.66	0.66	0.90	0.04	0

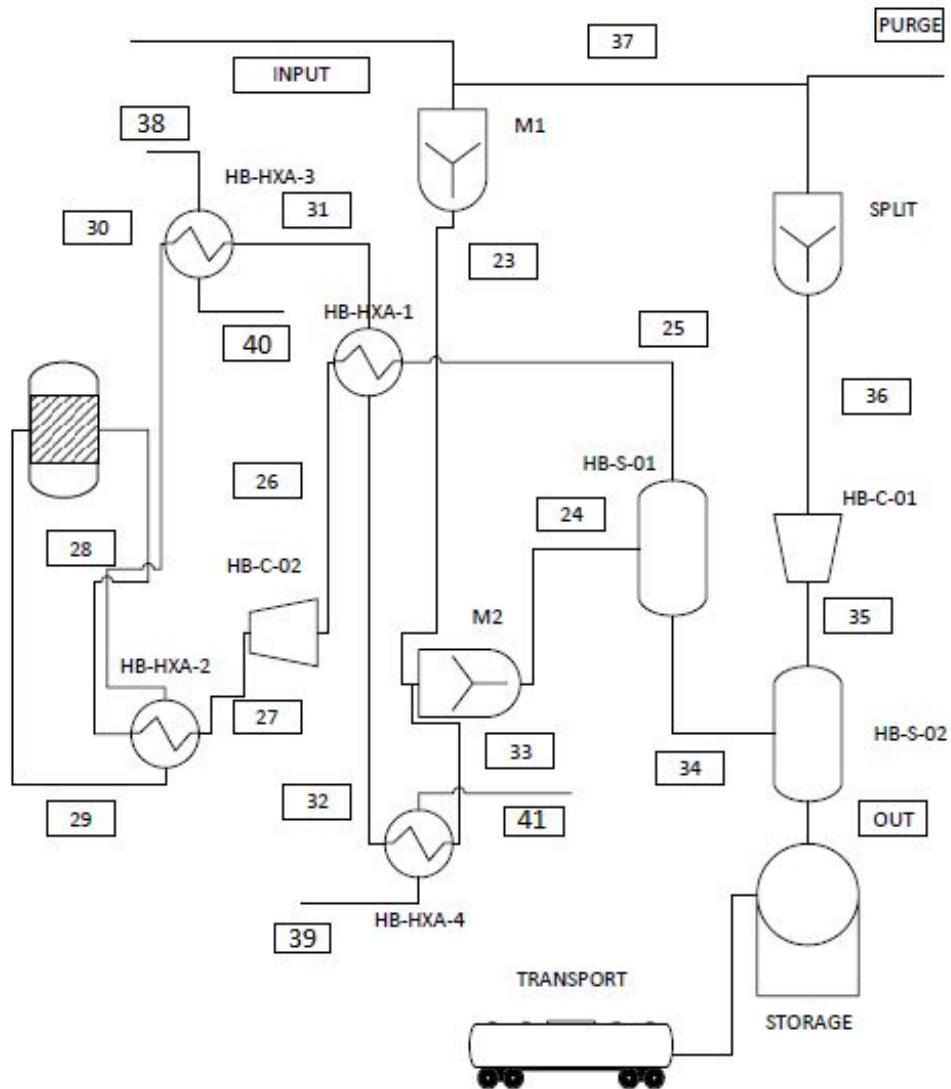
<b>Stream Number</b>	<b>13</b>	<b>14</b>	<b>15</b>	<b>16</b>	<b>17</b>	<b>18</b>	<b>19</b>	<b>20</b>
<b>Temperature (°C)</b>	800	800	649.6	35	800	598.2	35	35
<b>Pressure (bar)</b>	39.3	39.3	39.0	38.9	39.3	39.0	38.9	38.9
<b>Mass Flow (kg/hr)</b>	371.9	2739.1	2739.1	2739.1	8925.4	8925.4	6330.6	2594.8
<b>Molar Flow (kmol/hr)</b>	25.9	85.6	85.6	85.6	620.9	620.9	351.3	269.5
<b>Components (kmol/hr)</b>								
<b>H<sub>2</sub>O</b>	14.6	0	0	0	351.3	351.3	351.3	0
<b>H<sub>2</sub></b>	8.0	0	0	0	191.0	191.0	0	191.0
<b>N<sub>2</sub></b>	3.2	0	0	0	77.7	77.7	0	77.7
<b>O<sub>2</sub></b>	0	85.6	85.6	85.6	0	0	0	0
<b>Ar</b>	0.4	0	0	0	0.90	0.90	0	0

<b>Stream Number</b>	<b>21</b>	<b>22</b>	<b>23</b>
<b>Temperature (°C)</b>	35	38.4	35
<b>Pressure (bar)</b>	38.9	40	38.9

<b>Mass Flow (kg/hr)</b>	687.6	687.6	1907.2
<b>Molar Flow (kmol/hr)</b>	71.4	71.4	198.1
<b>Components (kmol/hr)</b>			
<b>H<sub>2</sub>O</b>	0	0	0
<b>H<sub>2</sub></b>	50.6	50.6	140.4
<b>N<sub>2</sub></b>	20.6	20.6	57.0
<b>O<sub>2</sub></b>	0	0	0
<b>Ar</b>	0.24	0.24	0.66

### 6.3.1 Process Flow Diagram of the Ammonia Synthesis Process

Figure 6.3.1 Process flow diagram which describes the unit operations and streams that are involved in the Haber-Bosch portion of the overall plant design.







<b>H<sub>2</sub></b>	513.2	513.2	513.2	513.2	0.2	0.2	0.2	0.2
<b>N<sub>2</sub></b>	283.6	283.6	283.6	283.6	0.2	0.2	0.2	0.2
<b>NH<sub>3</sub></b>	588.6	588.6	588.6	588.6	69	1.9	1.9	1.9
<b>Ar</b>	7.3	7.3	7.3	7.3	0.1	0	0	0

Table 6.3.2a: Haber Bosch Material Balance Descriptions

<b>Stream Number</b>	<b>38</b>	<b>39</b>	<b>40</b>	<b>41</b>	<b>OUT</b>	<b>PURGE</b>
<b>Temperature (°C)</b>	7.2	7.2	32.2	32.2	20	171
<b>Pressure (bar)</b>	1	1	1	1	10.1	39.6
<b>Mass Flow (kg/hr)</b>	1754	23,010	1754	23,010	1,145	0.8
<b>Molar Flow (kmol/hr)</b>	97.4	1277	97.4	1277	67.2	.02
<b>Components (kmol/hr)</b>						
<b>H<sub>2</sub>O</b>	97.4	1277	97.4	1277	0	0
<b>H<sub>2</sub></b>	0	0	0	0	.01	0.006
<b>N<sub>2</sub></b>	0	0	0	0	0.33	0.008
<b>NH<sub>3</sub></b>	0	0	0	0	1144	0.006
<b>Ar</b>	0	0	0	0	0.07	0.006

## 7. Process Descriptions

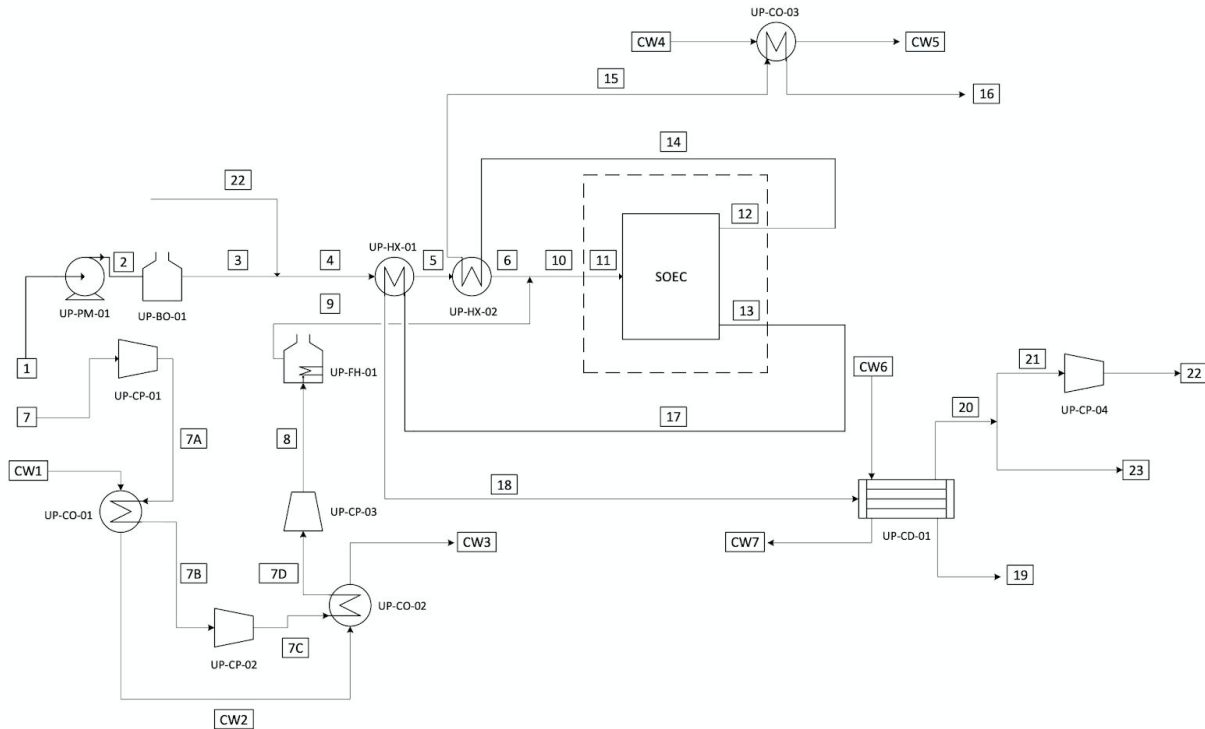
The overall process is broken down into two main sections: production of the reactants and the Haber Bosch process itself.

### 7.1.1 Feed Stream Sourcing and Preparation

Since the inputs to our process are simply air and water, we can source them directly from the environment. However, for the air, due to the presence of possible pollutants and solid particles present in the air, it will be run through a filtration system to avoid contamination and any possible issues to the system. The water does not necessarily need to go through such a process because the solids will fall out and instead remain in the boiler when the water is boiled. However, if clean water could be obtained that would be favorable as it would lower the frequency of required cleanings on the boilers. It will be assumed that the water has no solids. Both of the inputs will be heated and compressed prior to mixture with the  $H_2/N_2$  mixture that is recycled from the process. Argon is present all throughout the process and accounted for in the calculations but will not be dealt with until the Haber Bosch process where it will be purged.

**Figure 6.2.1a** is reprinted below for convenience.

Figure 6.2.1a: Process flow diagram with all of the physical units involved in the process.



### 7.1.2 Water Compression and Heating (UP-PM-01, UP-BO-01)

In order to produce hydrogen from water, the water must enter the SOEC system as compressed steam. To accomplish this, a pump with two stages (UP-PM-01) is used to first bring the input water at 25°C and 1bar to 40 bar. Following this process, the water is subsequently heated to 420°C by a boiler (UP-BO-01). This is in order to help achieve a reaction temperature that is able to support the reaction of hydrogen and oxygen in stream 6 and also ensures that the temperature at the end of the reaction will be at 800°C, the temperature at which our SOEC system is run. Prior to combination with the ar stream, the hydrogen + nitrogen is added from a recycle stream. This hydrogen + nitrogen stream is at a lower temperature (35°C) than the water stream and lowers the total stream temperature to about 380°C. The steam, hydrogen, and

nitrogen stream is elevated to higher temperatures by a series of two heat exchangers as well prior to the addition of the air stream.

### **7.1.3 Air Filtration, Compression, and Heating (UP-CP-01, UP-CO-01, UP-CP-02, UP-CO-02, UP-CP-03, UP-FH-01)**

The input air sourced from the environment is assumed to enter the process having passed a filter used to remove undesirable particles at 25°C and 1 bar similar to the water. It undergoes a compression process as well but is slightly different to the water as the air requires the use of compressors rather than a pump due to its physical state. After the first compressor (UP-CP-01), the air achieves a pressure of 3.42 bar. However, the temperature of the stream increases to 197.91°C. As this is undesirable due to more work needing to be exerted by the compressor to achieve the same pressure, before entry into the second compressor (UP-CP-02), the air stream enters a cooler (UP-CO-01) which decreases the temperature of the system to 37.8°C. This stream is then fed again into another compressor (UP-CP-02) which raises the pressure and temperature of the stream to 11.7 bar and 236.22°C. This stream enters another cooler (UP-CO-02) which cools the stream to 37.8°C and enters the final compressor (UP-CP-03) which brings the stream up to 40bar. Cooling water at 80°F or 26.67°C was used as the cold streams for the coolers. After this step however, the stream is not cooled again as having a higher temperature is desirable in our process due to the combination with the water stream needing to achieve temperatures higher than the oxyhydrogen reaction temperature which can be achieved at temperatures as low as 560°C.<sup>8</sup> The stream exits the final compressor at 40 bar and 222.91°C.

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<sup>8</sup> Airliquide Hydrogen Safety Data Sheet

This is not hot enough to maintain a temperature hot enough where the oxyhydrogen reaction or ignition of hydrogen will take place upon combination with the steam, hydrogen, and nitrogen stream. It will undergo an additional heating process in a fired heater (UP-FH-01) which heats the stream up to 550°C and afterwards gets combined with the other input stream.

#### **7.1.4 Heat Exchangers (UP-HX-01, UP-HX-02)**

Stream 4 passes through a series of heat exchangers in order to elevate the temperature of 610°C. This temperature is chosen so that when the air gets added to the process the change does not lower the temperature to a point where the oxyhydrogen reaction does not occur. Both heat exchangers utilize the products of the SOEC to heat up the reactants as they both leave the SOEC system at 800°C. These hot streams are both used to heat up the inputs and have a minimum approach temperature greater than 10°C. This was chosen to ensure that the driving force was large enough. A drop of 5 psi was assumed for each exit stream.

#### **7.1.5 Oxyhydrogen Reaction**

Hydrogen and oxygen will react when stream 6 combines with stream 9. The main components of this reaction involve oxygen from the air and the hydrogen from the recycle to undergo this process. Excess water is kept to ensure that the temperature increase caused by this reaction is not excessive as there are lower limits to which this reaction can get started. The water in addition is later hydrolyzed in the process to form more hydrogen and O<sub>2</sub> although from a strict stoichiometric perspective this seems intuitive but this process is crucial to the overall

system for a number of reasons. First, it is an excellent way to separate the oxygen from the air so that we may obtain nitrogen as a part of the process. This allows all the energy of the solid oxide electrolyzers to be utilized in producing hydrogen. In addition, it reduces heating costs of the system as more energy does not need to be spent to increase the temperature of the inputs of the SOEC to the operating temperature of the electrolyzer and the electrolyzer itself. Lastly, this process is advantageous as the oxygen cannot be exposed to the cathode side as it would degrade cell and thereby incur greater costs, Considering that the SOEC system to date is the most expensive units of the system, it is prudent to ensure the longevity of these systems at over others. For the process, it is assumed that all the oxygen that is input from the air into the process is reacted in this manner.

### **7.1.6 Solid Oxide Electrolyzer Network (SOEC)**

Each stack in our system was given a rating of 500kW in order to determine an appropriate price and current which would allow us to calculate the conversion of water to hydrogen within our system. 24 units each rated at 500kW would be put in parallel to process the hydrogen in the system. Taken at 1.285V, the thermoneutral voltage for the electrolysis of water at 800°C, this would lead to a current of  $9.231 \times 10^6$  amps to be run throughout the whole system.<sup>9</sup> Given that the current is used to electrolyze water, this would produce 171.2kmol H<sub>2</sub>/hr. Due to the system operating at the thermoneutral voltage, it will not experience a change in temperatures in the output and allows us to utilize the high temperature to heat up our inputs in UP-HX-01 and UP-HX-02. The calculations for the production of kmols H<sub>2</sub>/hr can be found in

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<sup>9</sup> High temperature electrolysis cell. Retrieved April 1, 2020 from <http://www.helmeth.eu/index.php/technologies/high-temperature-electrolysis-cell-soec>

*Appendix A.1.* The  $O_2$  partial pressure difference between the two electrodes will help any possible unreacted oxygen to be separated from the input stream.

### **7.1.7 Oxygen Cooler (UP-CO-03)**

One of the primary products of the SOEC is in the form of oxygen gas created from the electrolysis of water to produce hydrogen. The oxygen product is completely pure given that no air is run on the anode side of the SOEC to allow the oxygen to flow out of the electrolyte. This also allows there to be a greater  $O_2$  partial pressure difference to exist between the electrodes of the fuel cell system. As a result of the process, 85.6 kmol  $O_2$ /hr is produced and this stream leaves the anode side of the SOEC to be used as the hot fluid for UP-HX-02. The oxygen product leaves the heat exchanger at 649.6°C and enters a cooler that brings the temperature of the stream down to 35°C to permit the easier/safer storage of oxygen. The exact specifications of exactly how the oxygen was stored and sold were beyond the scope of the project. Cooling water at 26.7°C was used as the cold stream to this process.

### **7.1.8 SOEC Product Condenser (UP-CD-01)**

The gaseous stream containing hydrogen, nitrogen, and the remaining water leaves the cathode side of the electrolyzer and enters a heat exchanger (UP-HX-01) to heat up the inputs entering the SOEC. After this process, this stream is sent to a condenser for the removal of the water. It is much easier to do so when it exists in liquid form. By decreasing the temperature significantly, during this operation, the hydrogen and nitrogen will remain as a gas while the water condenses and exits the process as a liquid. The temperature that the streams leave the



condenser is 35°C as it is undesirable to leave hydrogen at high temperatures for safety reasons. Cooling water was once again used as the cold stream to the unit entering at 26.67°C. More cold water was added than necessary to allow the exit cooling water to remain below 30°C which preserves a reasonable driving force for the heat to be transferred across the two streams.

### **7.1.9 Recycle Stream Compressor (UP-CP-04)**

After condensing the water and eliminating it from the system, the gaseous stream consisting of primarily hydrogen and nitrogen is split with roughly 75% of the stream entering the next step of the process. The remaining 25% of the gas is sent to a compressor which raises the pressure back up to 40 bar for re-entry into the production of hydrogen and serves as the hydrogen component for the oxyhydrogen reaction.

### **7.2.1 Ammonia Synthesis Reaction Vessel (HB-RXN)**

For the given catalyst, the mass of catalyst required was calculated as a function of the GHSV and reactor size. The mass of catalyst required was found to be 316 kg at a price of \$20/kg of catalyst. The total amount of capital dedicated to purchasing the catalyst is \$20,000 to account for the 6-month cycle that the catalyst is functional for over the duration of the plant life.

It is further worth noting that the reaction has a relatively low single-pass conversion, only nearing 15-20% per pass through the reactor. However, repeated cycles through the entirety of the process is easily achieved and brings the total reaction rate close to completion. Through this recycle stream, a large amount of otherwise unreacted reagents are converted into the useful ammonia product.

The physical design of the reactor is that of a very tall tower with a relatively low pressure drop. There will be three catalyst beds, where the mixture will be allowed to react in separate layers to increase process efficiency. This gaseous ammonia product will be constantly removed to increase the reaction rate of the product in accordance with Le Chatelier's principle. This product mix will then be cooled slightly using chilled water and the incoming gas to the reactor. From this point, the gas will be sent to the separation column to recover the product.

### 7.2.2 Separation Column (HB-S-01)

The separation column, labeled HB-S-01 in **Figure 6.3.1a**, is a column that serves to separate the liquid ammonia product to be stored and shipped off from the gaseous reagents that failed to react in a previous pass through the reactor. It has been approximated as a flash vessel in ASPEN. HB-S-01 operates at 30 degrees Celsius and a pressure of 40 bar, taking in 968 kmol/hr of reagents, and outputting 69 kmol/hr of liquid ammonia product. HB-S-01 is the first column in the process loop, and as such is responsible for the bulk of the separation of ammonia from other gases. The distillate from HB-S-01 is recycled back into the main process loop after being heated by the reactor products. This occurs in heat exchangers HB-HX-01 and HB-HX-02. The stream is then pressurized by compressor HB-CP-02 to 80 atmospheres of pressure. Some of the unreacted hydrogen and nitrogen will inevitably leave as bottoms products from this first separation tower and enter the next stage. After the liquid product is depressurized in the let-down vessel HB-S-02 (see **Section 7.2.3**), the unreacted reagents (and trace amounts of ammonia) will leave as distillate and be repressurized by the compressor HB-CP-01. The distillate is also partially purged to remove the buildup of inert argon in the system, and the rest

of the distillate rejoins the initial feed stream. This rejoining of the two streams through a mixer completes the recycling process.

### **7.2.3 Let Down Vessel (HB-S-02)**

The let down vessel, which has been approximated as a flash vessel in ASPEN, is primarily utilized to lower the high pressure of the bottoms product of the separation columns, over 40 atmospheres, into a more manageable pressure for storage and shipment, roughly 10 atmospheres. The majority of the mass that flows through the vessel stays liquified at these conditions, given that almost exclusively liquid ammonia will exit as bottoms products from the columns. A small fraction of the liquid entering will be gasified upon pressure reduction, and will be sent to be repressurized and recycled throughout the process once more.

### **7.2.4 Compression of Gaseous Reactants (HB-C-01, HB-C-02)**

There are two separate compressors that are utilized in the ammonia synthesis portion of the process. In the first cycle through the reactor, there will be no ammonia to separate, and all the gas will flow through to the pre-reactor compressor HB-CP-02, where the gas is pressurized to the required 80 atmospheres of pressure that is required for the reaction to proceed at the desired rate. The second compressor, HB-CP-03, is used to compress the distillate of the let down vessel to return to the conditions needed to be reintroduced to the feed stream.

Due to the high pressures required for the reactants, centrifugal pumps were found to be appropriate. These compressors work through the use of an impeller that is shaped to force the gas to the rim of the impeller, which increases the velocity. This process is done through multiple

stages. These compressors are ideal as they are sufficiently large for this process and have comparatively greater efficiencies. They also weigh significantly less and occupy less space than other compressors of similar function, such as reciprocating compressors.

### **7.2.5 Heat Exchangers (HB-HX-01, HB-HX-02, HB-HX-03, HB-HX-04)**

In this process there are a number of situations where it is necessary to change the temperature of a given stream before the next process can be performed. Typically, in order to lower operation costs and purchases of utilities it is effective to exchange heat between a hotter stream that needs to be cooled, and a cooler stream that must be heated. Unfortunately, there are scenarios when no such heat integration opportunities are available, and in these cases a heater or cooler are used. An important note regarding the composition of the heat exchanger, along with the heaters and coolers, is that carbon steel is not an appropriate material choice. The hydrogen that is present all throughout the ammonia synthesis portion of the process is prone to reacting with the carbon in steel, causing hydrogen embrittlement to occur. This is a potential safety hazard because a pipe, or heat exchanger that has been made brittle could eventually burst. This result could be explosive and catastrophic. As such, the choice of material for these processes (and pipings) was chosen to be a Cr-Mo steel alloy that is far more resistant to this problem.

The most significant use of heat integration in this process are the usage of HB-HX-01 and HB-HX-02. The entry temperature of the reagents into the ammonia synthesis process from the SOEC section are high, but not enough to reach the desired reaction conditions. Preheating of these reagent streams is performed by heat exchangers HB-HX-01 and HB-HX-02, which utilize the high temperature of the reaction products to help reach the desired temperature for input into

the reaction vessel. The cold reagent stream enters HX-01 at 30 degrees Celsius, and exits at 90 degrees Celsius. After compression the temperature increases again, causing the stream to enter HX-02 at 193 degrees Celsius, and exiting at 225 degrees Celsius. The hot stream analogs to the aforementioned streams are the reaction products, which enter HX-02 at 400 degrees Celsius, and exit at 368 degrees Celsius. This stream is then cooled slightly by HX-03, which is cooled with cooling water, before entering HX-01, exiting at 300 degrees Celsius. Finally, the hot stream reaches HX-04, where it is once again cooled by cooling water until it reaches the final temperature of 250 degrees Celsius.

## 7.2.6 Storage

The liquid ammonia product, having met the quality criteria for proper sale, is stored in a very large-scale spherical tank. A spherical tank was chosen for the combination of volume, ability to minimize stress from the pressure in the storage vessel, and lack of heat transfer with the surroundings due to minimization of surface area. The tank will be pressurized at 10 atmospheres and held at a temperature of 20 degrees Celsius. The volume of the tank, roughly 47,000 gallons, was calculated to account for a three-day storage time, the longest amount of time that is expected for the tank to be emptied and for product to be shipped off by rail car. This calculation can be found in the *Appendix A.4*. For information regarding how transportation of product is expected to be undertaken can be found in **Section 14.5**.

## 8. Energy Balance and Utility Requirements

### 8.1 Description of Partitioning

In this section, the description of the energy balance and the energy requirements for utilities is split into discussions of the first and second “halves” of the process, similarly to what has been done in previous sections of this report, and will be continued in **Sections 9** and **10**. The first half involves the input of the air and water to the system and the utilization of the SOEC, culminating in the output of hydrogen and nitrogen into the Haber-Bosch ammonia synthesis portion, which is the second half of the process.

Overall, operation of this plant process involves a considerable amount of utilities and electricity, notably cooling water, high pressure steam, and electricity. There is also a fired heater that is operated in the first half of the process. While the utilities themselves are inexpensive, the volume that is required to achieve the desired output is considerable, and as such becomes a noticeable expense. Particularly, the incredible pressure requires significant investment in electricity, not to mention the large equipment cost for such a compressor. Yearly figures were calculated assuming that the plant operates for 350 days a year. It is assumed that the electricity will be obtained from renewable energy sources.

#### 8.2.1 Electricity Requirements for Overall Process

It is clear from **Table 8.2.1a** that the large majority of the electricity requirements stem from the hydrogen/nitrogen generation process. The overall amount of energy that the system requires is around 26.7MW.

Table 8.2.1a: Electricity Requirements for Overall Process

Process	Duty [cal/sec]	Usage Rate [kW]	Yearly Consumption [kW-hr]	Yearly Operation Cost [\$]
SOEC	4,952,066	20,719	174,043,374	0
HB	1,430,000	5986	50,281,652	0
Total Process	6,382,066	26,705	224,325,026	0

### 8.2.2 Breakdown of Electricity Requirements for SOEC Processes

A summary of the electricity requirements of the SOEC processes can be found in **Table 8.2.2a**. Some of the largest requirements of energy are the water boiler (UP-BO-01), the SOEC system (SOEC), and the condenser. Since it was assumed that the electricity to power these units and the water was essentially free, it was chosen to add excess water to provide ample quantities for reaction and also to absorb some of the heat released by the oxyhydrogen reaction. The SOEC has an especially high electricity requirement as it is the component directly responsible for producing the hydrogen to be fed into the next step of the overall process. Lastly, a large amount of energy is expended to cool and condense the cathode stream as to limit the dangers of working with hydrogen and eliminate the water.

Table 8.2.2a: Electricity Requirements for SOEC Processes

Unit Operation	Duty [cal/sec]	Usage Rate [kW]	Yearly Consumption [kW-hr]	Yearly Operation Cost [\$]
UP-PM-01	5,839	24	205,212	0
UP-BO-01	1,948,510	8,153	68,481,553	0
UP-CP-01	24,642	103	866,040	0
UP-CP-02	28,418	119	998,760	0
UP-CP-03	26,625	111	935,760	0
UP-FH-01	49,497	207	1,739,602	0
SOEC	2,868,069	12,000	100,800,000	0
UP-CP-04	466	2	16447	0
Total	4,952,066	20,719	174,043,374	0



## 8.2.3 Breakdown of Electricity Requirements for Ammonia Synthesis

### Processes

Table 8.2.2: Electricity Requirements for Ammonia Processes

Unit Operation	Duty [cal/sec]	Usage Rate [kW]	Yearly Consumption [kW-hr]	Yearly Operation Cost [\$]
HB-C-01	743	3.1	26,124	0
HB-C-02	327,500	1,371	11,520,000	0
HB-S-01	788,900	3,303	27,745,200	0
HB-S-02	1,772	7.4	62,328	0
HB-RXN	310,740	1,301	10,928,000	0
Total	1,430,000	5986	50,281,652	0

## 8.3 Cooling Water Requirements for Overall Process

Table 8.3a: Cooling Water Requirements for Overall Process

Process	Yearly Amount (MT/yr)	Yearly Cost (\$)
Cooling Water	280,534	8,000
Chilled Water	140,397	211,000
Chilled Brine	1,008,626	1,512,000
Total	1,429,557	1,731,000

## 9. Equipment List and Unit Descriptions

### 9.1 Heuristics for Equipment Determination

Generally, the equipment described and utilized here have had their costs determined through a number of common chemical engineering heuristics and equations. The specifics regarding each piece of equipment, including flow rates, energy usage, as well as temperature and pressure data can be found more clearly in **Section 10: Specification Sheets**.

### 9.2 Construction Materials

In general, the “cheapest first” heuristic was adhered to regarding our choice of materials for construction. This can be seen in our choice to use cheaper materials whenever possible in our design, such as in the pipes for the water input into the SOEC system where the complications regarding hydrogen are not a concern, stainless steel instead of Mo-Cr alloys can be used. Generally however, most of the processes in this operation involve hydrogen gas, meaning that embrittlement concerns dictate that alloys such as Mo-Cr or Monel (nickel alloy) must be used instead.

### 9.3 Specialized Equipment

Costing heuristics are very useful, and are implemented in this report for the majority of the processes in this design. However, there are specific pieces of equipment in this design which are too specialized to have a heuristic that allows for a rule-of-thumb calculation to be

performed. These non-standard pieces of equipment include the air filtration unit, and the solid oxide electrolytic cells. In order to find information and pricing, various online sources and quotes were found for these units, but should be considered to have significantly more variability in these estimations compared to the “actual” price of these units than the more conventional units will. In the ammonia synthesis reactor, information regarding retention time, sizing, and catalyst volume were found from literature.

## **9.4 Mixers and Splitters**

Mixers and splitters must be used throughout the whole process to ensure the system is able to run continuously. In these cases, mixing and splitting can be accomplished by a tee in the pipeline and utilizing a series of analyzers, controllers, and valves. These considerations are expected to be covered by the bare module costs and as such no specific analysis was conducted on these units.

### **9.5.1 Water Pump (UP-PM-01)**

UP-PM-01 will be used to bring liquid water at 25°C and 1 bar up to 40 bar so that it may be incorporated into the process. UP-PM-01 will be a pump with two stages operating at 3600rpm and has a horizontal split case. This pump will be constructed with cast iron. An electric motor that is able to provide 32.75hp will be used to drive these pumps. The cost of the pump itself and the electric motor are \$12,748 and \$1,733 respectively.

### **9.5.2 Water Boiler (UP-BO-01)**

Following the compression of the water, the water must be transformed to steam and raised to 420°C . The change in temperature is accomplished in a water boiler. Stainless steel will be the material of construction for this unit. The costing of this unit was given the same treatment as the fired heater and determined to be \$891,249 dollars.

### **9.5.3 Compressors (UP-CP-01, UP-CP-02, UP-CP-03, and UP-CP-04)**

In order to get the air to a suitable pressure, three different centrifugal compressors are used. The first compressor brings the air from 1 bar to 3.42 bar, the second compressor from 3.08 bar to 11.7 bar, and the third compressor from 11.36 bar to 40 bar. This was done in three different steps to avoid having the compression ratio extend beyond 4. These compressors will be constructed out of cast iron. The required power of these compressors are 138.3 hp, 159.5 hp, and 149.4 hp respectively. The fourth compressor in the system (UP-CP-04) will take the stream from 38.93 bar to 40 bar for re-entry into the process. This compressor will also be a centrifugal compressor but will be made of Cr-Mo steel alloy to prevent the embrittlement of the device. The compressor has a shaft power of 2.63 hp. The cost of the compressors is as follows: \$223,248; \$244,570; \$234,696; and \$25,785. These prices are in number order of the compressors.

### **9.5.4 Coolers (UP-CO-01, UP-CO-02, UP-CO-03)**

Throughout the SOEC system, streams must be cooled throughout to ensure optimal performance into the next unit or for convenience reasons. In each of these coolers which were

shell and tube heat exchangers, the hot stream is fed to the shell side while the coolant is fed through the pipes. UP-CO-01 and UP-CO-02 use cooling water as the coolant and UP-CO-03 uses chilled water. Each of the exchangers was designed with having a fixed head, tube lengths of 20ft, and made of carbon steel on both sides. UP-CO-01 and UP-CO-02 cool the air stream to 37.8°C following their respective compression processes. UP-CO-03 cools the oxygen stream to 35°C. The surface areas of the individual coolers in order are as follows: 2.01 m<sup>2</sup>, 3.80 m<sup>2</sup>, and 2.94 m<sup>2</sup>. The costs of the coolers are as follows: \$14,337; \$12,328; \$14,564,

### **9.5.5 Air Heater (UP-FH-01)**

Following the last compressor, the air must be heated so as not to decrease the temperature too far upon mixing with the water, hydrogen, and nitrogen stream. The air stream is raised to a temperature of 550°C from 222.9°C. Stainless steel will be used to construct this air heater. The cost of this unit is \$49,920.

### **9.5.6 Heat Exchangers (UP-HX-01, UP-HX-02)**

Heat exchangers are used in the system in order to maximize the extra energy remaining from the outputs from the SOEC systems. As they will exit the SOEC at 800°C and are to be cooled, this heat is used to heat up the water + recycle stream mixture to a temperature high enough (610°C) so that upon mixture with the air, the reaction of hydrogen will release enough heat to raise the temperature to 800°C. The exact nature of these calculations can be found in *Appendix A.2*. The first heat exchanger raises the temperature of the cool stream to 590°C and the second one raises the temperature to 610°C. Similar to the coolers, the heat exchangers are

fixed head and the hot stream is run along the shell side while the cold streams are fed through the tube side of the exchanger. The material of construction will be Cr-Mo steel to avoid hydrogen embrittlement problems. The tube length will be 20 ft. The surface areas of UP-HX-01 and UP-HX-02 are 7.06 m<sup>2</sup> and 1.31 m<sup>2</sup>. The price of UP-HX-01 is \$34,228 and UP-HX-02 is \$46,708.

### 9.5.7 500kW Solid Oxide Electrolyzer (SOEC)

The solid oxide electrolyzers are one of the most important and most expensive units of the process. Each cell stack was given a rating of 500kW to guide calculations. Since technology has not yet advanced this far, systems of these sizes do not yet exist but this model was derived with the assumption that technology will reach these sizes within the near future. Each stack will be run at 1.285V and 384,615 amps. 1.285V was chosen since it is the thermoneutral voltage for the reaction at 800°C. 24 units of 500kW stacks are necessary in order to achieve the hydrogen production desired. Materials used to build these units are going to be assumed to be standard: Ni-YSZ anode with a LSM anode. It is important to note that one of the main technological innovations to drive down costs of these units will be in the material in itself. The estimated bare modular cost of this unit will be \$15,000,000. From using a bare modular cost of 2, a purchase cost of \$7,500,000 was determined. This was chosen as a rough estimate to two significant figures by using some older SOFC costs as a basis. The authors understand that this number is low for an estimate and will instead focus on a sensitivity analysis on the cost that these units need to be in order for this operation to be profitable in **Section 15**.

### **9.5.8 Product Stream Condenser (UP-CD-01)**

The products exit the cathode side of the electrolyzer with steam needing to be eliminated from the stream prior input to the Haber Bosch process. This is accomplished in a condenser which removes the water as a liquid. The condenser will be made of Cr-Mo steel due to the hydrogen. The cooling fluid for the condenser is chilled brine. The hot stream temperature is lowered to 35°C from 598°C. Costing for this unit was assumed to be similar to a typical heat exchanger and was determined to be \$47,353.

### **9.6.1 Ammonia Synthesis Compressor Units (HB-C-01, HB-C-02, HB-CP-03)**

Each of these compressors in the ammonia synthesis process serve to pressurize the nitrogen, hydrogen, and argon that is used in the synthesis operation. Compressor HB-C-01 increases the pressure of its outgoing stream by 30 atmospheres, from 10 atm to 40 atm. HB-C-02 increases the pressure of its outgoing stream by 40 atmospheres, from 40 atm to 80 atm. These compressors will each be similar in function, and HB-C-01 will be operating at 150 horsepower. HB-CP-02 is the compressor that must put in the most work, and as such will be larger in size as well, and will operate at 1500 horsepower. Each compressor will utilize 8000-hour synthetic oil, and motors made of cast iron. HB-CP-01 will cost \$14,021 and HB-CP-02 will cost \$1,405,174 to purchase.

### 9.6.2 Heat Exchanger 1 (HB-HX-01, HB-HX-02, HB-HX-03, HB-HX-04)

Heat exchangers and associated pumps are required to facilitate the function of the synthesis process. The ammonia synthesis reactor output products are too hot to be placed in the separation column, and as such are cooled by contacting the input streams, heating them in the process to reaction conditions, which is done by heat exchangers HB-HX-01 and HB-HX-02. HB-HX-01 is 25 m<sup>2</sup> in surface area, and HB-HX-02 is 79 m<sup>2</sup> in surface area. Both are fixed head, shell-and-tube heat exchangers, 20 meters in length, and with both being made of Cr-Mo steel. In both cases, the hot stream is in the tube side, and the cold stream is in the shell side. HB-HX-01 cost \$33,407 and HB-HX-02 cost \$40,114 to purchase. The other two heat exchangers, HB-HX-03 and HB-HX-04 are similar in function to the previous exchangers, cooling the product stream to the proper temperatures to enter the separation units. They differ however in using cooling water instead of the colder reactant stream as the cooling fluid, and as such have the hot fluid in the shell. HB-HX-03 and HB-HX-04 are both 20 meters in length, and made of Cr-Mo steel on the gaseous product side, and carbon steel on the cooling water side. HB-HX-03 has a surface area of 25 m<sup>2</sup>, operates at 508 psig, and will cost \$37,992 to purchase. HB-HX-04 is identical to HB-HX-03 in terms of length and area, but operates at 1160 psig, and will cost \$48,292 to purchase.

### 9.6.3 Ammonia Synthesis Reaction Vessel (HB-RXN)

The ammonia synthesis reaction vessel is a packed bed reactor. The reaction that occurs is the conversion of gaseous nitrogen and hydrogen into ammonia, which is highly exothermic



and proceeds under pressure greater than 80 atmospheres. This reaction is catalyzed by the presence of a sodium-doped iron catalyst which facilitates the splitting of the diatomic hydrogen and nitrogen gas into constituent atoms. The reactor has a capacity of 2.63 m<sup>3</sup> and produces 84 kmol of ammonia per hour. This value was determined using residence time information about the reaction. To determine the catalyst mass, GHSV data and volume of catalyst in the reactor were taken from literature, and the final mass was determined to be 316 kg. The reactor vessel is a vertical pressure vessel that is 14.35 feet in height and 2.87 feet in diameter, and the vessel is made of Monel to account for the problem of hydrogen embrittlement. The total cost of this reaction vessel is \$81,929.

#### **9.6.4 Separation Columns (HB-S-01, HB-S-02)**

The first separation vessel, HB-S-01, is used to take in the input stream along with the product of the reaction vessel and separate the liquid ammonia off from the gaseous reactants. The liquid ammonia product is sent directly to HB-S-02, which serves as a let-down vessel. This vessel depressurizes the ammonia product and allows it to be safely stored at sale conditions in a spherical storage tank. There will be a small amount of distillate from HB-S-02, but not very much, as little H<sub>2</sub> or N<sub>2</sub> will have been liquified and carried to the let-down vessel. This minute amount of gaseous reactants will be recompressed and recycled back with the input stream to begin the cycle anew. HB-S-01 will be operated at 25 degrees Celsius and at a pressure of 40 atmospheres. HB-S-01 is a vertical pressure vessel with a diameter of 0.87 ft, and a height of 10.37 feet. This vessel, along with HB-S-02, is made of Monel-400 to prevent hydrogen embrittlement. HB-S-02 is operated at a slightly higher temperature, at around 50 degrees

Celsius, and at a lower pressure of 10 atmospheres. This column has a diameter of 0.78 feet and a length of 12.16 feet. HB-S-01 costs \$15,871 to purchase, and HB-S-02 costs \$13,735 to purchase.

### **9.6.5 Storage Vessel**

The ammonia storage vessel is a spherical vessel. The volume of the vessel was calculated by considering the retention time required to store the output of this process for a relatively long period of time, in case pickup and shipment of the product is halted for a few days. The calculations to determine this volume can be found in the *Appendix*. A spherical vessel was chosen due to the large volume of this storage vessel, but also the ability for a spherical vessel to withstand the pressure that the product is stored at, as well as to minimize heat transfer with the surroundings. The vessel is pressurized at 10 atmospheres, and is constructed of Monel to avoid hydrogen causing cracks in the storage vessel over time. The cost of this spherical storage vessel is \$235,000.

## 10. Specification Sheets

### Input Water Pump (UP-PM-01)

#### Description and Function

Increases the pressure of the water input stream from 1 bar to 40 bar.

#### Vendor

N/A

#### Operation

Continuous Output

#### Materials Handled

Water

#### Characteristics

Material: Cast Iron, Pump Type: Centrifugal pump, Number of Stages: 2 stages, Split Case Type:

Horizontal Split Case, Pump Specs: 3600 rpm, Power: 32.75 hp,

#### Operating Conditions/Design Data

Temperature: 25°C - 26.2°C

Pressure: 1 bar - 40 bar

#### Purchase Cost

\$ 12,748

#### Utilities

24.43 kW electricity

**Water Pump Motor (UP-EM-01)****Description and Function**

Electric motor used to drive the water pump.

**Vendor**

N/A

**Operation**

Continuous Output

**Materials Handled**

Water

**Characteristics**

Power: 32.75 hp

**Operating Conditions/Design Data**

N/A

**Purchase Cost**

\$1,733

**Utilities**

24.43 kW electricity

**Input Water Boiler (UP-BO-01)****Description and Function**

Following pressurization of the water, the water is transformed to steam and heated to 420°C.

**Vendor**

N/A

**Operation**

Continuous Output

**Materials Handled**

Water

**Characteristics**

Material: Stainless Steel, Process Volume: 2964.8 gal/min

**Operating Conditions/Design Data**

Temperature: 26.2°C - 420°C

**Purchase Cost**

\$891,249

**Utilities**

1,9948,510 kW electricity

## **Air Filter**

### **Description and Function**

Filters the air prior to entry into the system.

### **Vendor**

N/A

### **Operation**

Continuous Output

### **Materials Handled**

Nitrogen, Oxygen, Argon

### **Characteristics**

Process Volume: 3400 m<sup>3</sup>, Filter Media Material: Glass Fiber, Filter Class: M6, Media area: 8 m<sup>2</sup>, Filter Type: Vbank filter Dimensions: 0.6 x 0.6 x 0.2 m, Air flow: 3,400 m<sup>3</sup>/hr Frame: ABS,

Weight: 3 kg

### **Operating Conditions/Design Data**

Temperature: 25°C

Pressure: 1 bar

### **Purchase Cost**

\$4,000

### **Utilities**

N/A

## **Air Compressor 1 (UP-CP-01)**

### **Description and Function**

Compresses ambient air at 1 bar to 3.42 bar.

### **Vendor**

N/A

### **Operation**

Continuous Output

### **Materials Handled**

Nitrogen, Oxygen, Argon

### **Characteristics**

Material: Cast Iron, Type: Centrifugal Compressor, Power: 138.3 hp

### **Operating Conditions/Design Data**

Temperature: 25°C - 197.9°C

Pressure: 1 bar - 3.42 bar

### **Purchase Cost**

\$223,248

### **Utilities**

103 kW electricity

## **Air Compressor 2 (UP-CP-02)**

### **Description and Function**

Compresses the air from 3.08 bar to 11.7 bar following a decrease in temperature from a cooler.

### **Vendor**

N/A

### **Operation**

Continuous Output

### **Materials Handled**

Nitrogen, Oxygen, Argon

### **Characteristics**

Material: Cast Iron, Type: Centrifugal Compressor, Power: 159.5 hp

### **Operating Conditions/Design Data**

Temperature: 37.8°C - 236.2°C

Pressure: 3.08 bar - 11.7 bar

### **Purchase Cost**

\$244,570

### **Utilities**

119 kW electricity



## **Air Compressor 3 (UP-CP-03)**

### **Description and Function**

Compresses the air from 11.36 bar to 40 bar following a decrease in temperature from a cooler.

### **Vendor**

N/A

### **Operation**

Continuous Output

### **Materials Handled**

Nitrogen, Oxygen, Argon

### **Characteristics**

Material: Cast Iron, Type: Centrifugal Compressor, Power: 149.4 hp

### **Operating Conditions/Design Data**

Temperature: 37.8°C - 222.9°C

Pressure: 11.36 bar - 40 bar

### **Purchase Cost**

\$234,696

### **Utilities**

111 kW electricity

## **Recycle Stream Compressor (UP-CP-04)**

### **Description and Function**

Compresses the recycle stream back up to 40 bar following pressure drops throughout the process.

### **Vendor**

N/A

### **Operation**

Continuous Output

### **Materials Handled**

Hydrogen, Nitrogen, Argon

### **Characteristics**

Material: Cr-Mo Steel, Type: Centrifugal Compressor, Power: 2.63 hp

### **Operating Conditions/Design Data**

Temperature: 35°C - 36.2°C

Pressure: 38.9 bar - 40 bar

### **Purchase Cost**

\$25,785

### **Utilities**

1.95 kW electricity

**Air Cooler 1 (UP-CO-01)****Description and Function**

Cools the air exiting Air Compressor 1 (UP-CP-01) to 37.8°C to reduce energy requirements on subsequent compressor.

**Vendor**

N/A

**Operation**

Continuous Output

**Materials Handled**

Nitrogen, Oxygen, Argon

**Characteristics**

Type: Shell in tube, fixed head. Effective Surface Area: 2 m<sup>2</sup> Tube Side Material: Carbon Steel,  
Shell Side Material: Carbon Steel, Tube length: 20 m

**Operating Conditions/Design Data**

Hot Side Temperature: 197.9°C - 37.8°C

Hot Side Pressure: 3.42 bar - 3.08 bar

**Purchase Cost**

\$14,337

**Utilities**

63,601 MT/Year Cooling Water

**Air Cooler 2 (UP-CO-02)****Description and Function**

Cools the air exiting Air Compressor 2 (UP-CP-02) to 37.8°C to reduce energy requirements on subsequent compressor.

**Vendor**

N/A

**Operation**

Continuous Output

**Materials Handled**

Nitrogen, Oxygen, Argon

**Characteristics**

Type: Shell in tube, fixed head. Effective Surface Area: 3.8 m<sup>2</sup> Tube Side Material: Carbon Steel, Shell Side Material: Carbon Steel, Tube length: 20 m

**Operating Conditions/Design Data**

Hot Side Temperature: 236.2°C - 37.8°C

Hot Side Pressure: 11.7 bar - 11.36 bar

**Purchase Cost**

\$12,328

**Utilities**

63,601 MT/Year Cooling Water

## **Oxygen Cooler (UP-CO-03)**

### **Description and Function**

Cools oxygen product stream from the SOEC for easy storage.

### **Vendor**

N/A

### **Operation**

Continuous Output

### **Materials Handled**

Oxygen

### **Characteristics**

Type: Shell in tube, fixed head. Effective Surface Area: 2.9 m<sup>2</sup> Tube Side Material: Carbon

Steel, Shell Side Material: Carbon Steel, Tube length: 20 m

### **Operating Conditions/Design Data**

Hot Side Temperature: 650°C - 35.0°C

Pressure: 39.0 bar - 38.9 bar

### **Purchase Cost**

\$14,564

### **Utilities**

140,397 MT/Year Chilled Water

**Air Heater (UP-FH-01)****Description and Function**

Heats up the air following the compression steps.

**Vendor**

N/A

**Operation**

Continuous Output

**Materials Handled**

Nitrogen, Oxygen, Argon

**Characteristics**

Material: Stainless Steel, Volume Processed: 559.2 gal/min

**Operating Conditions/Design Data**

Temperature: 222.9°C - 550.0°C

**Purchase Cost**

\$49,920

**Utilities**

207 kW electricity

## Heat Exchanger 1 (UP-HX-01)

### Description and Function

Takes the compressed and heated water stream as the cold stream and the cathode product stream as the hot stream. Most of the heat exchange is done here.

### Vendor

N/A

### Operation

Continuous Output

### Materials Handled

Hot Stream: Water, Hydrogen, Nitrogen, Argon

Cold Stream: Water, Hydrogen, Nitrogen, Argon

### Characteristics

Type: Shell in tube, fixed head. Effective Surface Area: 7 m<sup>2</sup> Tube Side Material: Cr-Mo Steel,

Shell Side Material: Cr-Mo Steel, Tube length: 20 m

### Operating Conditions/Design Data

Cold Stream Temperature: 379.9°C - 590.0°C

Cold Stream Pressure: 40.0 bar - 39.7 bar

### Purchase Cost

\$34,228

### Utilities

N/A

**Heat Exchanger 2 (UP-HX-02)****Description and Function**

Takes the compressed and heated water stream as the cold stream and the oxygen product stream as the hot stream.

**Vendor**

N/A

**Operation**

Continuous Output

**Materials Handled**

Hot Stream: Oxygen

Cold Stream: Water, Hydrogen, Nitrogen, Argon

**Characteristics**

Type: Shell in tube, fixed head. Effective Surface Area: 1.3 m<sup>2</sup> Tube Side Material: Cr-Mo Steel,

Shell Side Material: Carbon Steel, Tube length: 20 m

**Operating Conditions/Design Data**

Cold Stream Temperature: 590.0°C - 610°C

Cold Stream Pressure: 39.7 bar - 39.3 bar

**Purchase Cost**

\$ 46,708

**Utilities**

N/A



## **500kW Solid Oxide Electrolyzer (SOEC)**

### **Description and Function**

This unit electrolyzes water to produce hydrogen. Each stack is input with 25.87 kmol/hr (14.63 kmol H<sub>2</sub>O/hr, 7.96 kmol H<sub>2</sub>/hr, 3.24 kmol O<sub>2</sub>/hr, 0.037 kmol Ar/hr). A total of 7.13 kmol H<sub>2</sub>/hr and 3.56 kmol O<sub>2</sub>/hr gets produced and within each stack. There are 24 stacks in the system.

### **Vendor**

N/A

### **Operation**

Continuous Output

### **Materials Handled**

Cathode Side: Water, Hydrogen, Nitrogen, Oxygen, Argon. Anode Side: Oxygen

### **Characteristics**

Anode: Ni-YSZ, Cathode: LSM

### **Operating Conditions/Design Data**

Temperature: 800°C

Voltage: 1.285V

Current: 384,615 Amps

### **Purchase Cost**

\$7,500,000 (estimation) Bare Module Cost: \$15,000,000

### **Utilities**

500 kW electricity per stack (12MW total)

**Product Stream Condenser (UP-CD-01)****Description and Function**

Condenses the product stream so the water can easily be separated and the hydrogen can be handled easier.

**Vendor**

N/A

**Operation**

Continuous Output

**Materials Handled**

Gaseous: Hydrogen, Nitrogen, Argon

Liquid: Water

**Characteristics**

Type: Shell in tube, fixed head. Effective Surface Area: 66 m<sup>2</sup> Tube Side Material: Carbon Steel,  
Shell Side Material: Cr-Mo Steel, Tube length: 20 m

**Operating Conditions/Design Data**

Hot Stream Temperature: 598.2°C - 35.0°C

Hot Stream Pressure: 39.0 bar - 38.9 bar

**Purchase Cost**

\$ 47,353

**Utilities**

1,008,626 MT/year Chilled Brine

## **Pre-Reaction Vessel Compressor (HB-CP-02)**

### **Description and Function**

This compressor serves to increase the pressure of the distillate of the first separation column to the required 80 atmospheres of pressure for the ammonia synthesis reaction to proceed.

### **Vendor**

N/A

### **Operation**

Continuous Output

### **Materials Handled**

Hydrogen, Nitrogen, Argon, Ammonia

### **Characteristics**

Material: Cr-Mo Steel, Weight: 2.5 MT, Compressor Type: Centrifugal Pump, Oil Type:  
8000-hour synthetic, 1500 hp

### **Operating Conditions/Design Data**

Temperature: 175°C

Pressure: 40 atm - 80 atm

### **Purchase Cost**

\$1,405,174

### **Utilities**

1371 kW electricity

**Let-Down Vessel Distillate Compressor (HB-CP-01)****Description and Function**

This compressor serves to increase the pressure of the distillate of the let down vessel to 10 atmospheres before entering the secondary separation unit.

**Vendor**

N/A

**Operation**

Continuous Output

**Materials Handled**

Hydrogen, Nitrogen, Argon, Ammonia

**Characteristics**

Material: Cr-Mo Steel, Weight: 1.5 MT, Compressor Type: Centrifugal Pump, Oil Type:  
8000-hour synthetic, 150 hp

**Operating Conditions/Design Data**

Temperature: 50°C

Pressure: 10 atm - 40 atm

**Purchase Cost**

\$14,021

**Utilities**

3.1 kW electricity

## **Separation Column (HB-S-01)**

### **Description and Function**

The first separation column removes the bulk of the unreacted inputs from the liquid ammonia product. The distillate of this column is recycled back to the reactor after subsequent heatings and repressurization. The bottoms product is piped to the let down vessel for further purification and depressurization.

### **Vendor**

N/A

### **Operation**

Continuous Output

### **Materials Handled**

Hydrogen, Nitrogen, Argon, Ammonia

### **Characteristics**

Material: Monel, Number of Trays: 8, Feed Stage: 4, Diameter: 0.87 ft, Height: 10.37 ft, Tray

Efficiency: 0.5, Reflux Ratio: 10.5, Condenser: Total

### **Operating Conditions/Design Data**

Temperature: 25°C, Pressure: 40 atm, Mass Flow Rate: 8,653 kg/hr

Mole Flow Rate: 1,119 kmol/hr Mass Flow Hydrogen: 1,251 kg/hr, Mass Flow Nitrogen: 5,800  
kg/hr,

Mass Flow Ammonia: 1,763 kg/hr. Mass flow Argon: 5 kg/hr

### **Purchase Cost**

\$15,871

**Utilities**

3,303 kW electricity

**Let Down Column (HB-S-02)****Description and Function**

This column serves to depressurize the bottoms product of HB-S-01 to allow the liquid ammonia to be removed for storage and later shipment

**Vendor**

N/A

**Operation**

Continuous Output

**Materials Handled**

Hydrogen, Nitrogen, Argon, Ammonia

**Characteristics**

Material: 304 Stainless Steel, Number of Trays: 6, Feed Stage: 3, Diameter: 0.78 ft, Height: 12.16 ft, Tray Efficiency: 0.5, Reflux Ratio: 7.5, Condenser: Total

**Operating Conditions/Design Data**

Temperature: 50°C, Pressure: 10 atm, Mass Flow Rate: 1873 kg/hr

Mole Flow Rate: 124 kmol/hr Mass Flow Hydrogen: 28 kg/hr, Mass Flow Nitrogen: 116 kg/hr,

Mass Flow Ammonia: 1729 kg/hr. Mass flow Argon: 0.05 kg/hr

**Purchase Cost**

\$13,735

**Utilities**

74 kW electricity

**Heat Exchanger (HB-HX-01)****Description and Function**

This first heat exchanger heats the distillate of the first separation column using heat energy from the reaction products.

**Vendor**

N/A

**Operation**

Continuous Output

**Materials Handled**

Hydrogen, Nitrogen, Argon, Ammonia

**Characteristics**

Type: Shell in tube, fixed head. Effective Surface Area: 24 m<sup>2</sup> Tube Side Material: Cr-Mo Steel,  
Shell Side Material: Cr-Mo Steel, Tube length: 20 m, Tube Diameter: 4.54 cm,

**Operating Conditions/Design Data**

Cold Side Output Temperature: 125°C

Pressure: 490 psig

**Purchase Cost**

\$40,114

**Utilities**

N/A



## Heat Exchanger (HB-HX-02)

### Description and Function

This second heat exchanger further heats the distillate of the first separation column using heat energy from the reaction products after compression to prepare the cooler stream for entry to the reaction vessel

### Vendor

N/A

### Operation

Continuous Output

### Materials Handled

Hydrogen, Nitrogen, Argon, Ammonia

### Characteristics

Type: Shell in tube, fixed head. Effective Surface Area: 79 m<sup>2</sup> Tube Side Material: Cr-Mo Steel, Shell Side Material: Cr-Mo Steel, Tube length: 20 m, Tube Diameter: 4.88 cm,

### Operating Conditions/Design Data

Cold Side Output Temperature: 225°C

Pressure: 1176 psig

### Purchase Cost

\$33,407 per unit

### Utilities

N/A

## **Heat Exchanger (HB-HX-03)**

### **Description and Function**

This heat exchanger serves as a cooler, further removing heat from the product stream after transferring some heat to the input to the reactor vessel, but before it must enter the separation vessel.

### **Vendor**

N/A

### **Operation**

Continuous Output

### **Materials Handled**

Hydrogen, Nitrogen, Argon, Ammonia

### **Characteristics**

Type: Shell in tube, fixed head. Effective Surface Area: 25 m<sup>2</sup> Tube Side Material: Cr-Mo Steel,  
Shell Side Material: Carbon Steel, Tube length: 20 m, Tube Diameter: 4.73 cm,

### **Operating Conditions/Design Data**

Cold Side Output Temperature: 300°C

Pressure: 490 psig

### **Purchase Cost**

\$37,992 per unit

### **Utilities**

120,272 MT/year of cooling water

**Heat Exchanger (HB-FH-03)****Description and Function**

This heat exchanger serves to even further cool the product of the reaction vessel, bringing the components close to the temperature required for separation.

**Vendor**

N/A

**Operation**

Continuous Output

**Materials Handled**

Hydrogen, Nitrogen, Argon, Ammonia

**Characteristics**

Type: Shell in tube, fixed head. Effective Surface Area: 25 m<sup>2</sup> Tube Side Material: Cr-Mo Steel,  
Shell Side Material: Carbon Steel, Tube length: 20 m, Tube Diameter: 5.31 cm,

**Operating Conditions/Design Data**

Cold Side Output Temperature: 150°C

Pressure: 490 psig

**Purchase Cost**

\$48,292 per unit

**Utilities**

160,262 MT/year of cooling water

## **Ammonia Storage Vessel**

### **Description and Function**

Spherical 47,000 gallon storage for anhydrous liquid ammonia product, held as a liquid under pressure prior to transportation via rail cart.

### **Vendor**

N/A

### **Operation**

Batch Output, Continuous Input

### **Materials Handled**

Ammonia

### **Characteristics**

Material: Monel, Volume: 48,000 gallons, Working Capacity 66%,

Flow Capability: 3500 kg NH<sub>3</sub>/hr

### **Operating Conditions/Design Data**

Temperature: 20°C

Pressure: 10 atm

Maximum retention time: 72 hours

### **Purchase Cost**

\$235,000 per unit

### **Utilities**

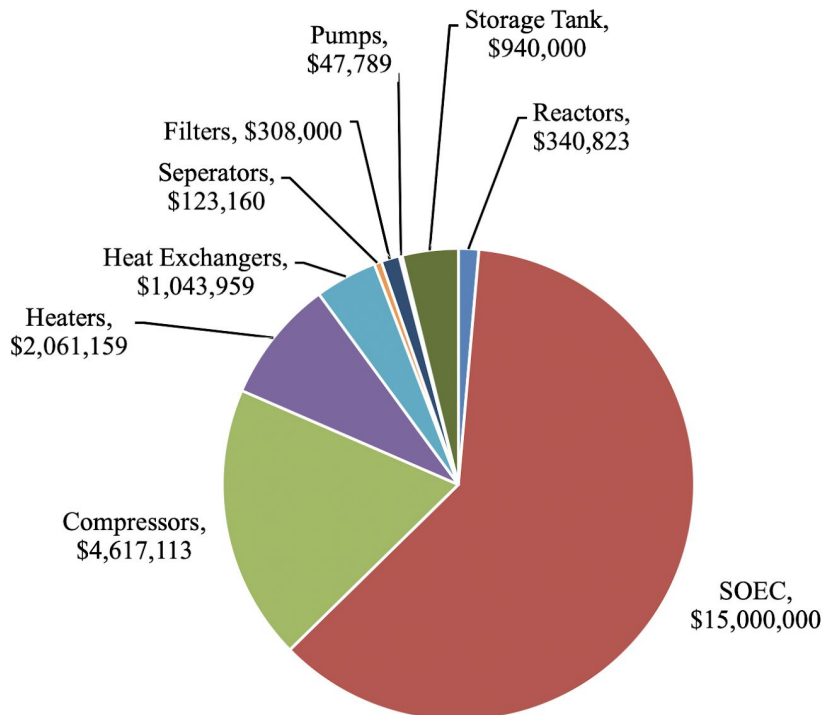
N/A

# 11. Equipment Cost Summary

## 11.1 Overview

Overall, equipment for the construction of the full green ammonia plant will cost \$24.5 million. For simplifying purposes, the process can be broken up into an upstream and downstream portion. The upstream portion includes the part of the process which converts air and water into a hydrogen and nitrogen mixed stream. The downstream portion of the plant includes the conversion of elemental hydrogen and nitrogen into ammonia via the Haber Bosch process.

Figure 11.1a: Breakdown of equipment costs by type of equipment



Equipment Type	Purchase Cost	Bare Module Factor	Bare Module Cost
Reactors	\$81,929	4.16	\$340,823
SOEC	\$7,500,000	2.00	\$15,000,000
Compressors	\$2,147,494	2.15	\$4,617,113
Heaters	\$941,169	2.19	\$2,061,159
Heat Exchangers	\$329,325	3.17	\$1,043,959
Seperators	\$29,606	4.16	\$123,160
Filters	\$154,000	2.00	\$308,000
Pumps	\$14,481	3.30	\$47,789
Storage Tank	\$235,000	4.00	\$940,000
<b>Total</b>	<b>\$11,433,003</b>		<b>\$24,482,003</b>

As seen in **Figure 11.1a**, the reactor and the SOECs make up the bulk of the equipment costs. As SOECs become cheaper, this process will become more economical.

## 11.2 Upstream Equipment Costs

*Table 11.2a: Overview of Upstream Equipment Costs*

Equipment Description	Type	Purchase Cost	Bare Module Factor	Bare Module Cost
SOEC	Process Machinery	\$7,500,000	2.00	\$15,000,000
UP-EM-01	Process Machinery	\$1,733	3.30	\$5,720
UP-PM-01	Process Machinery	\$12,748	3.30	\$42,068
UP-CP-01	Process Machinery	\$223,248	2.15	\$479,984
UP-CP-02	Process Machinery	\$244,570	2.15	\$525,826
UP-CP-03	Process Machinery	\$234,696	2.15	\$504,596
UP-CP-04	Process Machinery	\$25,785	2.15	\$55,437
UP-HX-01	Process Machinery	\$34,228	3.17	\$108,504
UP-HX-02	Process Machinery	\$46,708	3.17	\$148,064
UP-CO-01	Process Machinery	\$14,337	3.17	\$45,449
UP-CO-02	Process Machinery	\$12,328	3.17	\$39,081
UP-CO-03	Process Machinery	\$14,564	3.17	\$46,168
UP-CD-01	Process Machinery	\$47,353	3.17	\$150,110
UP-BO-01	Process Machinery	\$891,249	2.19	\$1,951,834
UP-FH-01	Process Machinery	\$49,920	2.19	\$109,325
M6 Filter	Process Machinery	\$4,000	2.00	\$8,000
Ion Exchange Unit	Process Machinery	\$150,000	2.00	\$300,000
<b>TOTAL</b>				<b>\$19,520,167</b>

The upstream part of the process is dominated by the SOEC units, whose projected bare module cost is \$15 million. All equipment sizing and bare module factors were consistent with Dr. Warren Seider's textbook: "Product and Process Design Principles", 4th edition, 2016..

### 11.3 Downstream Equipment Costs

Table 11.3a: Overview of Downstream Equipment Costs

Equipment Description	Type	Purchase Cost	Bare Module Factor	Bare Module Cost
Haber Bosch Reactor	Process Machinery	\$81,929	4.16	\$340,823
Sodium Doped Iron Catalyst	Catalysts	\$20,000	1.00	\$20,000
HB-CP-01	Process Machinery	\$14,021	2.15	\$30,146
HB-CP-02	Process Machinery	\$1,405,174	2.15	\$3,021,123
HB-HXA-01	Process Machinery	\$40,114	3.17	\$127,161
HB-HXA-02	Process Machinery	\$33,407	3.17	\$105,901
HB-HXA-03	Process Machinery	\$48,292	3.17	\$153,087
HB-HXA-04	Process Machinery	\$37,992	3.17	\$120,435
HB-S-01	Process Machinery	\$15,871	4.16	\$66,024
HB-S-02	Process Machinery	\$13,735	4.16	\$57,136
Storage Tank	Storage	\$235,000	4.00	\$940,000
<b>TOTAL</b>				<b>\$4,981,836</b>

Equipment in the downstream vertical is less expensive. The reactor itself costs \$340k, and the process requires multiple compressors that cost in excess \$1 million. As mentioned, all machinery in contact with high pressure hydrogen needs to be manufactured from Cr-Mo steel, which is 40% more expensive than carbon steel, adding an additional cost. A spherical storage tank is necessary for storing liquid ammonia, and is particularly expensive as well.

## 12. Fixed Capital Investment Summary

In order to consider the total permanent investment of this proposal, the cost of land, royalties and startup must be considered as well as equipment and installation costs (**Section 11**).

### 12.1 Land

In theory, this proposal is meant to be built on the existing site of a coastal windfarm's port. For this reason, it is assumed that a firm undertaking this project would already own the land on which this is meant to be built. For this reason, land was assumed to be 0.5% of total depreciable capital, one-fourth of the default value. This allotment is meant to allow for the purchase of additional land, which should be marginal and significantly less than if this project were designed to be standalone.

### 12.2 Royalties

No proprietary technology will be used in the production of ammonia. For this reason, royalties were assumed to be zero in calculating total permanent investment, as is most common.

### 12.3 Startup

Due to the massive nature of a factor producing 16,000 metric tonnes of ammonia per year, start up costs are significant and must be considered. It was assumed that start up costs



would be equal to 10% of total depreciable capital, which should be more than sufficient for starting the plant.

In order to lessen startup costs, the plant will be run constantly, which will lessen effects of startup and reduce costs.

*Table 12.3a: An overview of Fixed Capital Investment*

Cost of Land:	0.50%	of Total Depreciable Capital
Cost of Royalties:	\$0	
Cost of Plant Start-Up:	10.00%	of Total Depreciable Capital

## 13. Operating Cost

### 13.1 Raw Materials

Green ammonia is produced only from water, air and wind power. Air and water must be purified before being fed into the process. An air filter and an ion exchange system have been included in our process to be sure the raw material fed will not degrade any equipment or the ultimate product. Raw material costs are therefore assumed to be zero.

Although it has been found that only an ion exchange system will be necessary for this process, a unit that deionizes water may be necessary based on the water quality at the chosen site. Water could be particularly saline (or perhaps even sea water). A cost of such a unit would be minimal in comparison to the rest of the equipment, and could be easily sourced and entered into the process.

### 13.2 Utilities

Total utility costs come to \$1.7M/yr. Electricity is assumed to be free of charge from a nearby wind farm with excess amounts of electricity. For this reason, only cooling water, chilled water and chilled brine are expenses. For the annual production of 16,000 metric tons of ammonia, utility requirements and prices are below.

Table 13.2a: Yearly utility amounts and costs

Process	Yearly Amount (MT/yr)	Cost per MT	Yearly Cost (\$)
Cooling Water	280,534	\$0.027	8,000
Chilled Water	140,397	\$1.50	211,000
Chilled Brine	1,008,626	\$1.50	1,512,000
Total	1,429,557		1,731,000

### 13.3 Variable Cost and Working Capital

Additional variable costs were accounted for as follows in **Table 13.3a**. Typical values from Seider (2016) were used. Furthermore, working capital considerations and final figures are tabulated in 16.3.2 and 16.3.3. All working capital was expected to be wound down in the 15th and final year of production, 2036.

Table 13.3a: An overview of additional variable costs.

#### **Other Variable Costs**

##### General Expenses

Selling / Transfer Expenses:	3.00% of Sales
Direct Research:	4.80% of Sales
Allocated Research:	0.50% of Sales
Administrative Expense:	2.00% of Sales
Management Incentive Compensation:	1.25% of Sales

Table 13.3b: An overview of working capital considerations.

<b>Working Capital</b>		
Accounts Receivable	⇔	30 Days
Cash Reserves (excluding Raw Materials)	⇔	30 Days
Accounts Payable	⇔	30 Days
Ammonia Inventory	⇔	3 Days
Raw Materials	⇔	2 Days

Table 13.3c: Working capital figures.

<b>Working Capital</b>			
	<u>2021</u>	<u>2022</u>	<u>2023</u>
Accounts Receivable	\$ 329,109	\$ 164,554	\$ 164,554
Cash Reserves	\$ 279,770	\$ 139,885	\$ 139,885
Accounts Payable	\$ (64,029)	\$ (32,014)	\$ (32,014)
Ammonia Inventory	\$ 32,911	\$ 16,455	\$ 16,455
Raw Materials	\$ -	\$ -	\$ -
<b>Total</b>	<b>\$ 577,760</b>	<b>\$ 288,880</b>	<b>\$ 288,880</b>
<i>Present Value at 10%</i>	\$ 525,237	\$ 238,744	\$ 217,040
<b>Total Capital Investment</b>		<b>\$ 36,123,998</b>	

### 13.4 Total Variable Cost Summary

Variable costs were calculated to be \$2M annually. These costs were predominantly comprised of cooling water, chilled water and chilled brine requirements. Oxygen production was calculated to be a byproduct of ammonia production. \$700k of oxygen would be produced annually, which counted as a credit against variable costs.

Table 13.4a: Summary of variable costs.

#### Variable Cost Summary

##### Variable Costs at 100% Capacity:

##### General Expenses

Selling / Transfer Expenses:	\$	266,944
Direct Research:	\$	427,110
Allocated Research:	\$	44,491
Administrative Expense:	\$	177,962
Management Incentive Compensation:	\$	111,227
<b>Total General Expenses</b>	<b>\$</b>	<b>1,027,733</b>
<b><u>Raw Materials</u></b>	\$0.00 per ton of Ammonia	\$0
<b><u>Byproducts</u></b>	\$44.00 per ton of Ammonia	(\$711,850)
<b><u>Utilities</u></b>	\$107.00 per ton of Ammonia	\$1,731,152
<b><u>Total Variable Costs</u></b>	<b>\$</b>	<b><u>2,047,035</u></b>

### 13.5 Operations, Maintenance and Overhead

Per shift, 5 operators are needed to run the plant. This was calculated to be 2 operators in both the upstream and downstream verticals and an additional operator monitoring the overall

process and deliveries. Technical assistance and the control lab costs were calculated to be ~\$200k and ~\$300k respectively, consisting of one engineer and a part time lab employee. Default values from Seider (2016) were used in calculated maintenance and operating overhead costs.

*Table 13.5a: Overview of operations, maintenance and overhead costs.*

#### **Fixed Costs**

##### **Operations**

Operators per Shift:	5 (assuming 5 shifts)
Direct Wages and Benefits:	\$40 /operator hour
Direct Salaries and Benefits:	15% of Direct Wages and Benefits
Operating Supplies and Services:	6% of Direct Wages and Benefits
Technical Assistance to Manufacturing:	\$7,920.00 per year, for each Operator per Shift
Control Laboratory:	\$11,700.00 per year, for each Operator per Shift

##### **Maintenance**

Wages and Benefits:	2.00% of Total Depreciable Capital
Salaries and Benefits:	25.00% of Maintenance Wages and Benefits
Materials and Services:	100.00% of Maintenance Wages and Benefits
Maintenance Overhead:	5.00% of Maintenance Wages and Benefits

##### **Operating Overhead**

General Plant Overhead:	7.10% of Maintenance and Operations Wages and Benefits
Mechanical Department Services:	2.40% of Maintenance and Operations Wages and Benefits
Employee Relations Department	5.90% of Maintenance and Operations Wages and Benefits
Business Services	7.40% of Maintenance and Operations Wages and Benefits

## **13.6 Total Fixed Costs**

Final annual fixed costs resulting from operations maintenance and operating overhead are tabulated in table 13.6a. Due to the large amount of manpower to effectively run this plant, annual fixed costs are expensive at \$5.8M/yr. This is the second largest financial hurdle to this plant, after the cost of the SOECs. If the plant were to be scaled up, but was run with the same 25 weekly operators, margins would drastically improve, and the venture would be more profitable.

Table 13.6a: Overview of operations, maintenance and overhead costs.

**Fixed Cost Summary**

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**Operations**

Direct Wages and Benefits	\$	2,080,000
Direct Salaries and Benefits	\$	312,000
Operating Supplies and Services	\$	124,800
Technical Assistance to Manufacturing	\$	198,000
Control Laboratory	\$	292,500
<b>Total Operations</b>	<b>\$</b>	<b>3,007,300</b>

**Maintenance**

Wages and Benefits	\$	636,072
Salaries and Benefits	\$	159,018
Materials and Services	\$	636,072
Maintenance Overhead	\$	31,804
<b>Total Maintenance</b>	<b>\$</b>	<b>1,462,966</b>

**Operating Overhead**

General Plant Overhead:	\$	226,283
Mechanical Department Services:	\$	76,490
Employee Relations Department:	\$	188,038
Business Services:	\$	235,845
<b>Total Operating Overhead</b>	<b>\$</b>	<b>726,657</b>

**Property Taxes and Insurance**

Property Taxes and Insurance:	\$	636,072
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**Other Annual Expenses**

Rental Fees (Office and Laboratory Space):	\$	-
Licensing Fees:	\$	-
Miscellaneous:	\$	-
<b>Total Other Annual Expenses</b>	<b>\$</b>	<b>-</b>

<b><u>Total Fixed Costs</u></b>	<b>\$</b>	<b><u>5,832,994</u></b>
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## 14. Other Important Considerations

### 14.1 Location

One of the earliest and most crucial decisions that was made when researching this project was the choice of plant location. It was immediately obvious that the ending metrics of economic feasibility, plant size, and production capacity are all factors that are directly affected and can be optimized through careful consideration of optimal plant locations. We chose to locate our plant on the coast of Norway, as their agricultural market has sufficient demand such that our capacity of ammonia production would be purchased in its entirety. Furthermore, Norway has a long history of taxing carbon-heavy chemical production facilities at a very high rate. As a “green” ammonia production facility, our plant would avoid these taxes, and would qualify for a number of monetary rewards as a result of our zero-carbon emission plant design. These additional advantages that our plant design has over conventional ammonia synthesis facilities allows us to close the monetary gap that is created by our more expensive production methods.

Norway also has a climate that is conducive to the main reaction being performed in our plant. The synthesis of ammonia from hydrogen and nitrogen is an extremely exothermic reaction, performed at high pressures. With an average temperature of just 5 degrees Celsius, the environment will be a useful asset to lower the amount of work that must be put in by the cooling towers in the process.

The choice of our location to be coastal is a result of the input to our process, as well as our energy needs. One of the inputs into our process is water, and as such the plant will be built



coastally to lower transportation costs. Additionally, the coastal location allows for local utilization of the wind power that is stored on offshore, near coast windmills.

These windmills are perhaps the most important reason why Norway was chosen. Norway has massively invested in renewables energy sources, with wind energy at the forefront. The amount of wind energy produced is sufficiently large that it often exceeds energy demand in the country, and as such is simply wasted. Our process utilizes a tiny percentage of this excess wind energy and uses it to power our solid oxide electrolytic cell, which removes an incredible amount of energy that would otherwise need to be sourced through other, less environmentally friendly, means.

## **14.2 Environmental Impact**

One of the key considerations that was made when designing this plant was to ensure environmental friendliness wherever possible, while still reaching the desired output of 46 metric tons of ammonia per day. The ammonia that is produced from our process design utilizes nitrogen from air that has been separated from oxygen, and hydrogen that has been produced through electrolysis of water. Neither of these processes involve the output of pollutants, which is a noticeable environmental improvement over the typical method used to produce hydrogen, which is through steam reformation. Steam reformation outputs carbon monoxide and dioxide, which are greenhouse gases, whereas electrolysis outputs pure oxygen, which in our plant design will be sold as an additional revenue stream. Additionally, the energy requirements being met through the excess wind power that is available in Norway allows for the plant to produce no pollution, a vast upgrade to other traditional plants.

In order to facilitate the small environmental impact of this process, it is important to lower our energy costs as much as possible in order to diminish the need for energy outside of the excess wind power. This excess power would likely need to be produced in less environmentally agreeable ways such as through combustion of fuels like coal or natural gas. This was done by ensuring that the efficiencies of our processes were made as high as possible, through the addition of recycle streams and heat integration between disparate parts of the process. Most notably, the excess heat of the exothermic reaction was useful in lowering the energy required in the heater that powers the air and water coming into the SOEC. Furthermore, the heat of the reaction products were useful in getting the incoming reagents and recycled material up to the correct temperature in the reactor. The recycle stream was useful in increasing the conversion of our product from a single pass rate of ~15% to as high as 99% over extended periods of time. This benefit is mainly financial, as more product is undeniably best for the bottom line, but also environmental, as less energy would be going to waste in a higher conversion process.

### **14.3 Global, Social, and Cultural Factors**

Generally, when designing a large-scale industrial process, it is important to consider how the construction and operation of said process will affect the world around you. In this process, the product that is output is ammonia, which is primarily used for fertilizer, but also as a refrigerant or as a reagent in polymer synthesis in fringe cases. This process has been utilized since the early 1900s, and is one of the earliest chemical synthesis processes. As a result, there is likely little to no concern regarding social and cultural clashes with this process, as there might

be in the case of a new genetically modified food or product. Furthermore, there would potentially even be a positive cultural or social response given that a core value of our process is environmental safety. Many cultures and nations, like Norway, value respecting the environment, as can be seen by the investment of many nations in renewable energy sources. As such, it is reasonable to assume that this renewable ammonia synthesis process could be culturally and socially acceptable in most nations that we would be producing inside of, namely Norway.

The prime global factor that affects this process is the ammonia market. Due to the necessity of ammonia as a key component in fertilizer, it is incredibly unlikely that the demand for ammonia will decrease in the near future. In fact, unlike many markets, there are relatively few major European ammonia producers, meaning that a plant of the scale proposed here could reasonably expect to make a significant impact, especially if demand for cleanly produced ammonia increases, as it has for other products.

#### **14.4 Safety**

One of the defining characteristics of an ammonia processing plant is that great care must be taken to ensure that proper safety measures are taken into consideration- more so than many other plants of similar scale. This is due to the incredible pressures that the Haber-Bosch reaction is performed at. With pressures reaching upwards of 80 atmospheres, it is clear that if proper safety precautions are eschewed, then a catastrophe could potentially follow.

There are three most probable potential safety hazards that have been considered in this process design. The first is a fire or explosion caused by ignition of the hydrogen feed. The

second is an explosion as a result of uncontrolled buildup of temperature and pressure inside of the reaction vessel. Finally, there is a toxic hazard if any liquid ammonia is released from inside of the synthesis loop. There are also smaller potential hazards regarding the storing and handling of liquid ammonia.

Another significant safety concern is as a result of hydrogen embrittlement of carbon. This concern is largely mitigated by material choice regarding the piping and vessels, which are made of alloys that are resistant to reaction with the hydrogen, but due to the potential dangers associated with this embrittlement, it is worth frequently assessing the piping to ensure there are no imperfections or cracks.

To ensure that a disaster does not occur, this process will be following the guidelines set forth in the AIChE Safety in Ammonia Plants and Related Facilities Symposium. The plant will utilize a HAZOP (hazards and operability) study with a team of expert process engineers, contractors, and outside safety consultants. Trip systems and strategies for safe shut down in case of emergency will also be developed.

## **14.5 Transportation**

Transportation of the liquid ammonia product will be predominantly by rail cars and by river barges. Due to our location in Scandinavia, we will have a market that is accessible through landlocked transportation methods, but by utilizing the nearby ocean, we will be able to reach the larger European market.

The rail cars utilized will be outfitted with pressure vessels for anhydrous ammonia, with capacities in the range of 100-150 cubic meters of storage space. With this capacity, rail cars

would need to come daily, with the latest possible delay in shipments being three days, as that is the capacity of the liquid ammonia storage vessels. This distribution method will be used mainly to provide our supply to smaller fertilizer processing facilities or other wholesale suppliers and merchants.

Transportation through larger ocean and river vessels will also be necessary to reach a larger market. Due to the large size of barges, which have larger capacities than even the most massive rail carts, much more liquid ammonia could be shipped. This solution would likely not be implemented in the first year that the plant is operational, as demand for the ammonia product would need to be sufficient to justify the extra storage vessels that would be required to make shipping the product by barge to be a profitable venture.

## 14.6 Plant Startup

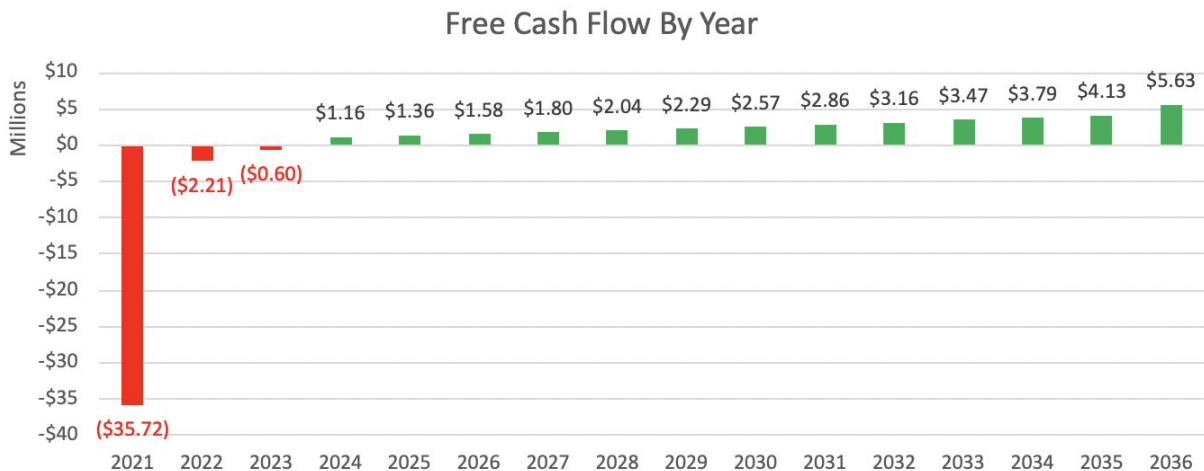
The design for this plant assumes that the cost of the reagents for the startup of the process is negligible, given that the only two inputs into the process are air and water, which are both available free of cost. The values given below describe the amount of these incoming reagents that are involved in the first “loop” through the process. The input into the first steps of the process are 203 kmol/hr of air and 563 kmol/hr of water. The air and water are separated into the desired constituents, which are 140 kmol/hr of nitrogen and 57 kmol/hr of hydrogen. Upon startup, either addition or regeneration of the iron catalyst that facilitates the Haber-Bosch reaction must be performed. Regeneration can be performed by drying the catalyst and heating to 300-400 degrees Celsius. A lifetime of six months is assumed for the iron catalyst. The total bare module cost, including this payment for catalyst is included in **Section 12.**

## 15. Profitability Analysis

In sum, this project does not represent a profitable venture. Once investment is complete, our product yields annual positive cash flows, but the total upfront investment as it currently stands is simply too large for commercial viability.

The NPV of this proposal was currently calculated as USD -22M (discount rate of 10%). The project lifetime was modeled as 15 years, after construction was complete in 2021. Investment in year one was roughly ~USD 35M, so only one third of capital outlays were recuperated. Net present value was calculated by project cash flows in 2021-2036. Terminal valuation beyond 2036 was not factored into profitability. Assuming a discount rate of 10% and a FCF growth rate of 3%, using the Gordon Growth Model and valuing further profits as a perpetuity, a discounted terminal value of <\$10M is attained. However, cashflows beyond this point would likely be hampered by additional capital expenditures.

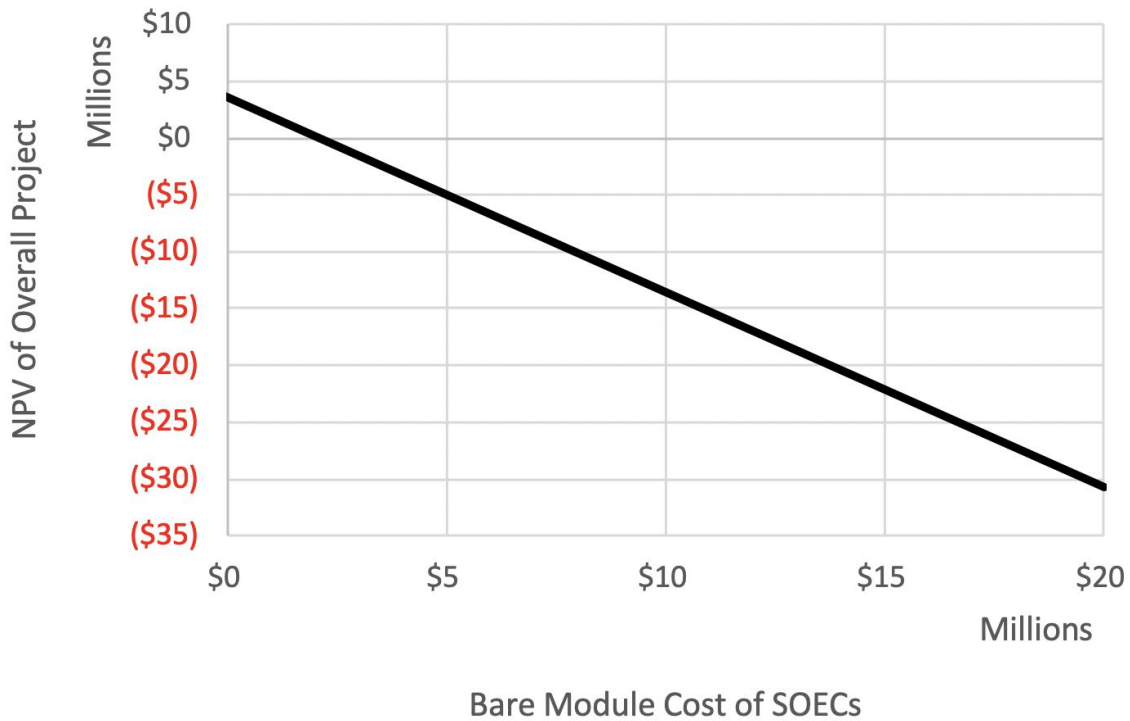
Figure 15.1a: Cash Flows



Using free cash flows, an internal rate of return of -0.68% was calculated. Neglecting the time value of money, this venture roughly repays initial outlays over the course of a 15 year lifetime.

The biggest obstacle to profitability is the cost of the SOEC, which represents ~60% of total permanent investment. If this price were to decrease from \$15m to \$2m, the project would become profitable. The SOEC is the most expensive unit purchased. Furthermore, few firms manufacture SOECs, and pricing information is hard to come by.

Figure 15.1b: NPV of overall project as a function of SOEC Bare Module Cost.



An additional consideration is the cost of ammonia. Ammonia’s price is highly correlated to the price of oil. If oil prices were to increase, this venture would likely benefit.

The below table shows ROI as a bivariate function of total permanent investment and price per metric ton of ammonia. The venture would become largely profitable should SOEC prices decrease and a bull market for oil emerge.

Figure 15.1c: ROI as a function of Ammonia price and TPI.

Product Price	Total Permanent Investment											
	\$17,571,489	\$21,085,787	\$24,600,085	\$28,114,382	\$31,628,680	\$35,142,978	\$38,657,276	\$42,171,574	\$45,685,871	\$49,200,169	\$52,714,467	
\$523	14.84%	9.92%	6.02%	2.82%	0.10%	-2.27%	-4.36%	-6.24%	-7.95%	-9.52%	-10.98%	
\$528	15.34%	10.35%	6.42%	3.18%	0.44%	-1.94%	-4.04%	-5.92%	-7.64%	-9.21%	-10.68%	
\$534	15.84%	10.78%	6.80%	3.53%	0.77%	-1.62%	-3.73%	-5.62%	-7.33%	-8.91%	-10.37%	
\$539	16.33%	11.21%	7.18%	3.89%	1.10%	-1.30%	-3.42%	-5.32%	-7.04%	-8.62%	-10.08%	
\$545	16.82%	11.63%	7.56%	4.23%	1.43%	-0.99%	-3.12%	-5.02%	-6.75%	-8.33%	-9.79%	
\$550	17.31%	12.05%	7.93%	4.57%	1.75%	-0.68%	-2.82%	-4.73%	-6.46%	-8.05%	-9.51%	
\$556	17.79%	12.46%	8.30%	4.91%	2.07%	-0.38%	-2.53%	-4.45%	-6.18%	-7.77%	-9.24%	
\$561	18.27%	12.87%	8.66%	5.24%	2.38%	-0.09%	-2.25%	-4.17%	-5.91%	-7.50%	-8.97%	
\$567	18.74%	13.27%	9.02%	5.57%	2.68%	0.21%	-1.97%	-3.90%	-5.64%	-7.24%	-8.70%	
\$572	19.21%	13.67%	9.37%	5.90%	2.99%	0.49%	-1.69%	-3.63%	-5.38%	-6.98%	-8.45%	
\$578	19.68%	14.07%	9.73%	6.22%	3.29%	0.78%	-1.42%	-3.37%	-5.12%	-6.72%	-8.19%	

Another major factor preventing profitability are the large annual fixed costs. Because the plant is relatively small (annual revenue of ~\$10m) and has so many operators (25), margins are relatively small. If the plant were to be expanded and could maintain the same number of operators and total maintenance expenses, the venture could become profitable. There are ammonia plants that manufacture well in excess of 50 times what this plant does. These plants do not have 50 times the manpower. By making use of economies of scale, it is possible that a fully green ammonia plant could be profitable in the future.

Further detailed calculations relating to profitability can be found in *Appendix D*.



## 16. Conclusions and Recommendations

With the effects of climate change growing more and more severe every year, it is hard to deny that green alternatives to current carbon-heavy processes would be of great use to the world, but as of this time it is difficult to make such ventures profitable. Unfortunately, we can not recommend that a plant with the given design be built, given that the profitability is currently negative. While after years of sustained operation the plant would turn a profit, the initial investment is currently too prohibitive to make the venture worthwhile. The cost of the purchased equipment is quite high because each of the main components of the plant must be made of expensive alloys, and is one of the most significant factors why the plant is unprofitable. The primary concern that has caused the profitability estimations to be so pessimistic is the cost of the reactor vessel and the cost of leasing the solid oxide electrolytic cells. Although the “free” energy that we would be able to obtain from wind power is a great boon, it is not enough to offset the massive cost of the electrolytic cells. Furthermore, the market for green ammonia is simply not profitable enough to overcome this deficit until the plant has operated for 15 years.

Though the process is not currently viable, it is reasonable to envision a future in which this exact process methodology would be usable in the coming years. Certain circumstances, such as the price of oil drastically increasing, a stark increase in tax for emissions, or a more lucrative green ammonia market, would enable our process to compete monetarily. A sensitivity analysis was performed to determine the degree to which altering these factors would allow us to overcome this barrier and to reach profitability sooner, and can be found in **Section 15**.

Despite the current lack of economic viability, this green ammonia process remains an interesting prospect given the benefits to society that could potentially be achieved if this process

were a primary way that ammonia was produced and sold across the world. However, given the current landscape, further consideration should be made before action is undertaken to create a plant similar to the one outlined in this report.

## **17. Acknowledgements**

We would like to thank Dr. Raymond Gorte, Professor Bruce Vrana, and Mr. Leonard Fabiano for their help throughout the project. In addition, we would like to thank the industrial consultants who met with us both in person and over Zoom. We would also like to thank the faculty in the University of Pennsylvania's Department of Chemical and Biomolecular Engineering.

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## Appendix A: Manual Calculations

### A.1 Hydrogen Production Calculations

To determine the extent of hydrogen able to be processed within the electrolyzer, a couple of assumptions were made: all the current will be used to electrolyze water, there are minimal to no voltage losses, the system is operating at its thermoneutral voltage. With these factors in mind, the calculation is as follows. For calculation purposes 1.285V was rounded to 1.3V.

#### Determining Current of the System

$$P = IV$$

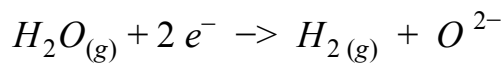
$$I = \frac{P}{V}$$

$$I = \frac{500,000W}{1.3V}$$

$$I = 384,615 \text{ Amps per SOEC Stack}$$

#### Determining moles of H<sub>2</sub> Produced

The reaction is as follows:



To determine mols of H<sub>2</sub> produced by the SOEC:

$$H_{2, produced} = \frac{I}{nF}$$

$$I = \text{current (amps)}$$

$$n = \text{mols of electrons}$$

$$F = \text{Faraday's Constant}$$

$$H_{2, produced} = \frac{384,615}{(2)(96485)} = 171200 \text{ mols } H_2 = 171.2 \text{ kmols } H_2$$

## A.2 Calculation of Water Input

The removal of oxygen is primarily driven by its reaction with hydrogen. The reaction is as follows:



As can be seen in the figure above, the oxyhydrogen reaction releases a significant amount of heat. Due to the operation of our SOEC stacks, the input must reach a temperature of 800°C prior to entry in order to maintain its thermoneutral operation at 1.285V. In addition, the temperature of the stream when it the hydrogen + air first mix must be high enough for this reaction to occur. The temperature at which this mixing occurs was taken to be about 600°C. Since water could be added to the process without raising the extent of the reaction, it was chosen to be the varying factor so that the process was able to absorb some of the excess heat produced by the reaction. This quantity was determined by the calculation detailed below.

Using coefficients from the NIST database, the specific heat values were determined using the Shomate Equation at 800°C for all of the components. It was assumed that the reaction took place at constant pressure.

Component	C <sub>p</sub> at 800°C (kJ/mol*K)
H <sub>2</sub> O	41.87
H <sub>2</sub>	30.84
N <sub>2</sub>	32.59
O <sub>2</sub>	34.60

Ar	20.79
----	-------

Assuming that all the oxygen reacted, the amount of heat released into the system was determined.

$$\Delta H_{rxn} = -247.2 \text{ kJ/mol of rxn}$$

$$\Delta H_{tot} = \Delta H_{rxn} * n_{o_2 \text{ reacted}}$$

$$\Delta H_{tot} = 3,806,172.97 \text{ kJ released/hr}$$

To determine the amount of water that needed to be flowed through the system, the heat released was set equal to the specific heat formula of all the components. It is assumed that no heat was lost to the environment.

$$Q = \Delta H_{tot} = 3,806,172.97 \text{ kJ/hr} = \sum_{i=1}^5 n_i C_{p,i} \Delta T$$

Since, all the other components had their molar flow rates set, we needed to solve for  $n_{H_2O}$  which was determined to be 522.5 kmol/hr. Since 30.8 kmol/hr was formed, it was determined that the amount of water that needed to be fed into the system was 491.7 kmol/hr.

### A.3 Calculation of Compression Ratios

Equations are taken from *Product and Process Design Principles* Chapter 16, Section 5, pg. 459-460

Sample calculation shown below:

$$\text{Net Work Required} = PC (Hp) = 1500 \text{ (From Aspen Block Results)}$$

Electric compressor  $FD = 1$  (From pg. 460)

Carbon steel material  $FM = 1$  (From pg. 460)

$FBM = 2.15$  (From Table 16.11 on pg. 441)

According to Heuristic 36 on pg. 150, the compression ratio must be calculated to determine the number of stages.

$Compression\ Ratio = Outlet\ Pressure / Inlet\ Pressure = 1160.3\ (psia) / 580.15\ (psia) = 2,$

$2 < 3 \therefore$  The number of gas compression stages is 1.

#### **A.4 Calculation of Storage Vessel Size**

Time Capacity is the amount of time the material will be stored.

Assuming a safety factor of 2, the volume of the tank must be double the volume of the material stored throughout the specified amount of time.

Time Capacity = 3 days

235000

$Volume\ of\ Tank = Volumetric\ Flow\ Rate * Time\ Capacity * Safety\ Factor$

Tank volume =  $(333\ gal/hr) * (0.134\ ft^3/gal) * (24\ hr/day) * (3\ days) * (2) = 6,426\ ft^3$

$Diameter = D = (Volume\ of\ Tank / 1.25 * \pi)^{1/3} = (6,426 / (1.25 * \pi))^{1/3} = 11.8\ f$

$Height = L = 2.5 * D = 29.5\ ft$

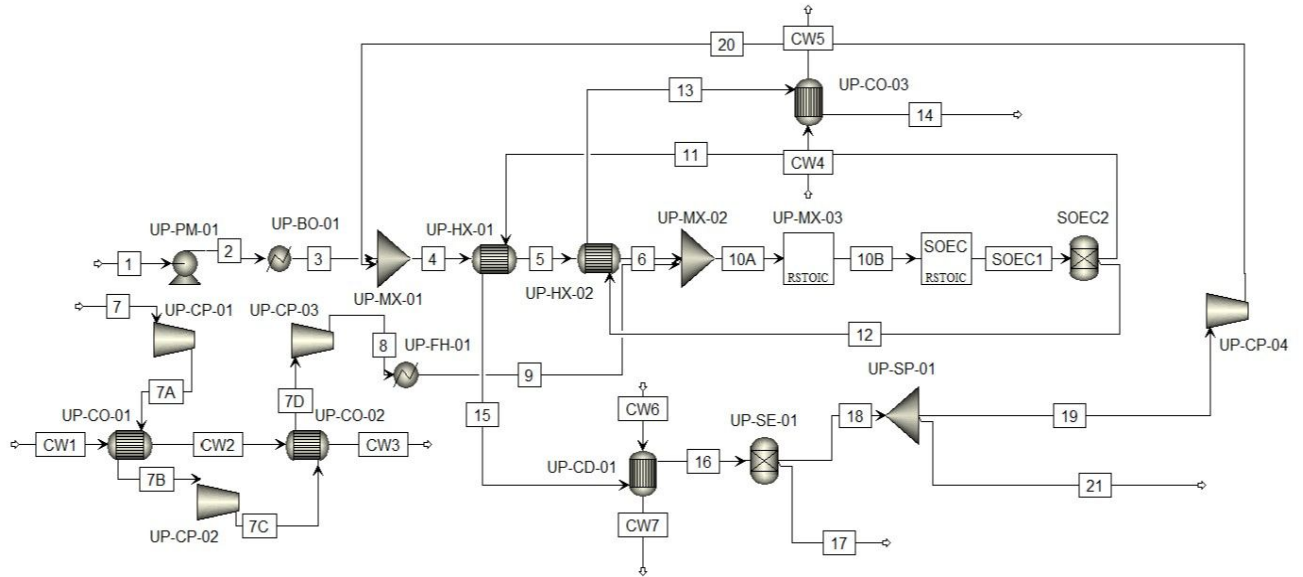


## A.5 Calculation of Reactor, HB-S-01 and HB-S-02 Vessel Sizes

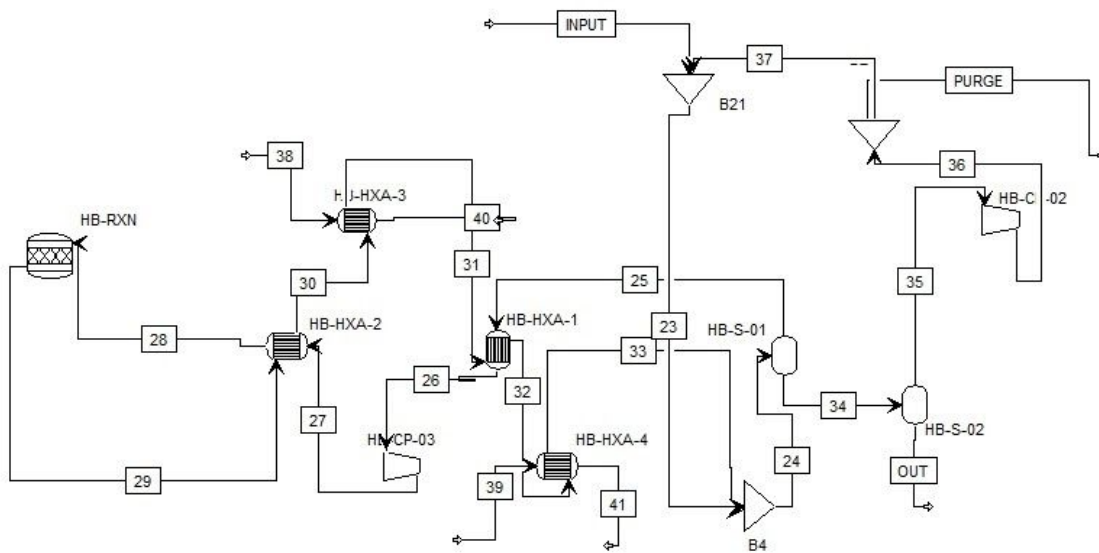
Reator Size			
Volumetric Flow Rate Out	15789	L/min	
Residence Time	10	s	
Volume	2.6315	m <sup>3</sup>	
Diameter	0.87508014	m	2.87 ft
Height	4.37540072	m	14.35 ft
Pressure	80	bar	1160 psi
HB-S-01 Size			
Liquid Volumetric Flow Rate Out	34.92	L/min	
Liquid Holdup Half Full	5	min	
Volume	0.1746	m <sup>3</sup>	
Gas Velocity	15	ft/s	274.39 m/s
Gas Flow Rate	15148	L/min	
Cross Sectional Area	0.05520604	m <sup>2</sup>	
Diameter	0.26512359	m	0.87 ft
Height	3.16269716	m	10.37 ft
Pressure	39	bar	565.5 psi
HB-S-02 Size			
Liquid Volumetric Flow Rate Out	32.84	L/min	
Liquid Holdup Half Full	5	min	
Volume	0.1642	m <sup>3</sup>	
Gas Velocity	0.1	ft/s	1.83 m/s
Gas Flow Rate	81	L/min	
Cross Sectional Area	0.04428	m <sup>2</sup>	
Diameter	0.23744272	m	0.78 ft
Height	3.70822042	m	12.16 ft
Pressure	10	bar	145 psi

# Appendix B: Aspen Flowsheet Information

## B.1.1 SOEC System ASPEN Flow Diagram



## B.2.1 Ammonia Synthesis ASPEN Flow Diagram



## B.1.2 SOEC ASPEN Inputs

```
;  
;Input Summary created by Aspen Plus Rel. 37.0 at 23:23:22 Sun Apr 19,  
2020  
;Directory \\nestor\jamekwon\SeniorDesignSOECv2_6 Filename  
C:\Users\jamekwon\AppData\Local\Temp\~apcce4.txt  
;
```

### DYNAMICS

```
DYNAMICS RESULTS=ON
```

```
IN-UNITS MET PRESSURE=bar TEMPERATURE=C DELTA-T=C PDROP=bar &  
INVERSE-PRES='1/bar' SHORT-LENGTH=mm
```

```
DEF-STREAMS CONVEN ALL
```

### MODEL-OPTION

```
DATABANKS 'APV110 PURE37' / 'APV110 AQUEOUS' / 'APV110 SOLIDS' &  
/ 'APV110 INORGANIC' / 'APESV110 AP-EOS' / &  
'NISTV110 NIST-TRC' / NOASPENPCD
```

```
PROP-SOURCES 'APV110 PURE37' / 'APV110 AQUEOUS' / &  
'APV110 SOLIDS' / 'APV110 INORGANIC' / 'APESV110 AP-EOS' &  
'NISTV110 NIST-TRC'
```

### COMPONENTS

```
WATER H2O /  
HYDROGEN H2 /  
NITROGEN N2 /  
OXYGEN O2 /  
ARGON AR
```

### SOLVE

```
RUN-MODE MODE=SIM
```

### FLOWSHEET

```
BLOCK UP-PM-01 IN=1 OUT=2  
BLOCK UP-BO-01 IN=2 OUT=3  
BLOCK UP-FH-01 IN=8 OUT=9  
BLOCK UP-HX-01 IN=11 4 OUT=15 5  
BLOCK UP-HX-02 IN=12 5 OUT=13 6  
BLOCK SOEC IN=10B OUT=SOEC1  
BLOCK UP-MX-01 IN=3 20 OUT=4  
BLOCK UP-SE-01 IN=16 OUT=18 17  
BLOCK UP-SP-01 IN=18 OUT=19 21  
BLOCK UP-CP-04 IN=19 OUT=20  
BLOCK UP-MX-03 IN=10A OUT=10B  
BLOCK UP-MX-02 IN=6 9 OUT=10A  
BLOCK SOEC2 IN=SOEC1 OUT=11 12  
BLOCK UP-CP-01 IN=7 OUT=7A  
BLOCK UP-CO-01 IN=7A CW1 OUT=7B CW2
```

BLOCK UP-CO-02 IN=7C CW2 OUT=7D CW3  
BLOCK UP-CP-02 IN=7B OUT=7C  
BLOCK UP-CP-03 IN=7D OUT=8  
BLOCK UP-CD-01 IN=15 CW6 OUT=16 CW7  
BLOCK UP-CO-03 IN=13 CW4 OUT=14 CW5

PROPERTIES SRK

STREAM 1

SUBSTREAM MIXED TEMP=25. PRES=1. MOLE-FLOW=491.7  
MOLE-FLOW WATER 491.7

STREAM 2

SUBSTREAM MIXED TEMP=25. PRES=40. MOLE-FLOW=522.5  
MOLE-FLOW WATER 522.5

STREAM 7

SUBSTREAM MIXED TEMP=25. PRES=1. MOLE-FLOW=73.16  
MOLE-FLOW NITROGEN 57.1 / OXYGEN 15.4 / ARGON 0.66

STREAM 9

SUBSTREAM MIXED TEMP=550. PRES=40. MOLE-FLOW=73.16 &  
FREE-WATER=NO NPHASE=2 PHASE=V  
MOLE-FLOW NITROGEN 57.1 / OXYGEN 15.4 / ARGON 0.66

STREAM 10B

SUBSTREAM MIXED TEMP=800. PRES=39.3 FREE-WATER=NO NPHASE=1 &  
PHASE=V

STREAM 11

SUBSTREAM MIXED TEMP=800. PRES=39.3

STREAM 12

SUBSTREAM MIXED TEMP=800. PRES=39.3

STREAM CW1

SUBSTREAM MIXED TEMP=80. <F> PRES=1. MOLE-FLOW=1000.  
MOLE-FLOW WATER 1000.

STREAM CW4

SUBSTREAM MIXED TEMP=45. <F> PRES=1. MOLE-FLOW=1000.  
MOLE-FLOW WATER 1000.

STREAM CW6

SUBSTREAM MIXED TEMP=0. <F> PRES=1. MOLE-FLOW=1000.  
MOLE-FLOW WATER 1000.

BLOCK UP-MX-01 MIXER

PARAM PRES=40. NPHASE=1 PHASE=V  
BLOCK-OPTION FREE-WATER=NO

BLOCK UP-MX-02 MIXER

PARAM

BLOCK UP-SP-01 FSPLIT  
FRAC 19 0.265

BLOCK SOEC2 SEP  
PARAM  
FRAC STREAM=12 SUBSTREAM=MIXED COMPS=WATER HYDROGEN &  
NITROGEN ARGON FRACS=0. 0. 0. 0.  
MOLE-FLOW STREAM=12 SUBSTREAM=MIXED COMPS=OXYGEN FLOWS= &  
85.6

BLOCK UP-SE-01 SEP  
PARAM  
MOLE-FLOW STREAM=18 SUBSTREAM=MIXED COMPS=WATER HYDROGEN &  
NITROGEN OXYGEN ARGON FLOWS=0. 232.8 77.6 0. 0.9  
FLASH-SPECS 18 PRES=38.9313 NPHASE=1 FREE-WATER=NO PHASE=V  
FLASH-SPECS 17 NPHASE=1 FREE-WATER=NO PHASE=L

BLOCK UP-BO-01 HEATER  
PARAM TEMP=420. PRES=40. DPPARMOPT=NO

BLOCK UP-FH-01 HEATER  
PARAM TEMP=550. PRES=40. NPHASE=1 PHASE=V DPPARMOPT=NO  
BLOCK-OPTION FREE-WATER=NO

BLOCK UP-CD-01 HEATX  
PARAM T-HOT=35. PRES-HOT=-0.5 <psi>  
FEEDS HOT=15 COLD=CW6  
OUTLETS-HOT 16  
OUTLETS-COLD CW7  
HOT-SIDE DPPARMOPT=NO  
COLD-SIDE DPPARMOPT=NO  
TQ-PARAM CURVE=YES

BLOCK UP-CO-01 HEATX  
PARAM T-HOT=100. <F> PRES-HOT=-0.3447  
FEEDS HOT=7A COLD=CW1  
OUTLETS-HOT 7B  
OUTLETS-COLD CW2  
HOT-SIDE DPPARMOPT=NO  
COLD-SIDE DPPARMOPT=NO  
TQ-PARAM CURVE=YES

BLOCK UP-CO-02 HEATX  
PARAM T-HOT=100. <F> PRES-HOT=-0.3447  
FEEDS HOT=7C COLD=CW2  
OUTLETS-HOT 7D  
OUTLETS-COLD CW3  
HOT-SIDE DPPARMOPT=NO  
COLD-SIDE DPPARMOPT=NO  
TQ-PARAM CURVE=YES

BLOCK UP-CO-03 HEATX  
PARAM T-HOT=35. PRES-HOT=-0.5 <psi>  
FEEDS HOT=13 COLD=CW4

OUTLETS-HOT 14  
OUTLETS-COLD CW5  
HOT-SIDE DPPARMOPT=NO  
COLD-SIDE DPPARMOPT=NO  
TQ-PARAM CURVE=YES

BLOCK UP-HX-01 HEATX  
PARAM T-COLD=590. PRES-HOT=-5. <psi> PRES-COLD=-5. <psi>  
FEEDS HOT=11 COLD=4  
OUTLETS-HOT 15  
OUTLETS-COLD 5  
HOT-SIDE DPPARMOPT=NO  
COLD-SIDE DPPARMOPT=NO  
TQ-PARAM CURVE=YES

BLOCK UP-HX-02 HEATX  
PARAM T-COLD=610. PRES-HOT=-5. <psi> PRES-COLD=-5. <psi>  
FEEDS HOT=12 COLD=5  
OUTLETS-HOT 13  
OUTLETS-COLD 6  
HOT-SIDE DPPARMOPT=NO  
COLD-SIDE DPPARMOPT=NO  
TQ-PARAM CURVE=YES

BLOCK SOEC RSTOIC  
PARAM TEMP=800. PRES=39.3105 NPHASE=2  
STOIC 1 MIXED WATER -1. / HYDROGEN 1. / OXYGEN 0.5  
EXTENT 1 171.2  
BLOCK-OPTION FREE-WATER=NO

BLOCK UP-MX-03 RSTOIC  
PARAM TEMP=800. PRES=39.3105 NPHASE=1 PHASE=V  
STOIC 1 MIXED HYDROGEN -1. / OXYGEN -0.5 / WATER 1.  
EXTENT 1 30.8  
BLOCK-OPTION FREE-WATER=NO

BLOCK UP-PM-01 PUMP  
PARAM PRES=40.

BLOCK UP-CP-01 COMPR  
PARAM TYPE=ISENTROPIC PRES=3.42 SB-MAXIT=30 SB-TOL=0.0001

BLOCK UP-CP-02 COMPR  
PARAM TYPE=ISENTROPIC PRES=11.7 SB-MAXIT=30 SB-TOL=0.0001

BLOCK UP-CP-03 COMPR  
PARAM TYPE=ISENTROPIC PRES=40. SB-MAXIT=30 SB-TOL=0.0001

BLOCK UP-CP-04 COMPR  
PARAM TYPE=ISENTROPIC PRES=40. SB-MAXIT=30 SB-TOL=0.0001

DESIGN-SPEC CWSYS1  
DEFINE CW3T STREAM-VAR STREAM=CW3 SUBSTREAM=MIXED &  
VARIABLE=TEMP UOM="F"

SPEC "CW3T" TO "120"  
TOL-SPEC "0.0001"  
VARY MOLE-FLOW STREAM=CW1 SUBSTREAM=MIXED COMPONENT=WATER &  
UOM="kmol/hr"  
LIMITS "400" "1000"

DESIGN-SPEC CWSYS2  
DEFINE CW5T STREAM-VAR STREAM=CW5 SUBSTREAM=MIXED &  
VARIABLE=TEMP UOM="F"  
SPEC "CW5T" TO "85"  
TOL-SPEC "0.0001"  
VARY MOLE-FLOW STREAM=CW4 SUBSTREAM=MIXED COMPONENT=WATER &  
UOM="kmol/hr"  
LIMITS "400" "50000"

DESIGN-SPEC CWSYS3  
DEFINE CW07T STREAM-VAR STREAM=CW7 SUBSTREAM=MIXED &  
VARIABLE=TEMP UOM="F"  
SPEC "CW07T" TO "90"  
TOL-SPEC "0.001"  
VARY MOLE-FLOW STREAM=CW6 SUBSTREAM=MIXED COMPONENT=WATER &  
UOM="kmol/hr"  
LIMITS "50" "500000"

EO-CONV-OPTI

STREAM-REPOR MOLEFLOW

PROPERTY-REP PCES

;  
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# B.1.3 SOEC Full Summary

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## ASPEN PLUS CALCULATION REPORT

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EUROPE (44) 1189-226555

PLATFORM: WIN-X64  
VERSION: 37.0 Build 395  
INSTALLATION:

APRIL 19, 2020  
SUNDAY  
11:21:21 P.M.



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HEATX COLD-TQCU UP-CO-02 TQCURV INLET.....	27
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BLOCK: UP-CO-03 MODEL: HEATX.....	28

HEATX COLD-TQCU UP-CO-03 TQCURV INLET.....	32
HEATX HOT-TQCUR UP-CO-03 TQCURV INLET.....	33
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RUN CONTROL SECTION

RUN CONTROL INFORMATION

-----

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TYPE OF RUN: EDIT

INPUT FILE NAME: \_2402dax.inm

INPUT PROBLEM DATA FILE NAME : \_2402dax

OUTPUT PROBLEM DATA FILE NAME: \_2000dhp

LOCATED IN:

PDF SIZE USED FOR INPUT TRANSLATION:

NUMBER OF FILE RECORDS (PSIZE) = 0  
NUMBER OF IN-CORE RECORDS = 256  
PSIZE NEEDED FOR SIMULATION = 1

CALLING PROGRAM NAME: apmain

LOCATED IN: C:\Program Files\AspenTech\Aspen Plus V11.0\Engine\XeQ

SIMULATION REQUESTED FOR ENTIRE FLOWSHEET

FLWSHEET SECTION

FLWSHEET CONNECTIVITY BY STREAMS

-----

STREAM	SOURCE	DEST	STREAM	SOURCE	DEST
1	----	UP-PM-01	7	----	UP-CP-01
CW1	----	UP-CO-01	CW6	----	UP-CD-01
CW4	----	UP-CO-03	2	UP-PM-01	UP-BO-01
3	UP-BO-01	UP-MX-01	9	UP-FH-01	UP-MX-02
15	UP-HX-01	UP-CD-01	5	UP-HX-01	UP-HX-02
13	UP-HX-02	UP-CO-03	6	UP-HX-02	UP-MX-02
SOEC1	SOEC	SOEC2	4	UP-MX-01	UP-HX-01
18	UP-SE-01	UP-SP-01	17	UP-SE-01	----
19	UP-SP-01	UP-CP-04	21	UP-SP-01	----
20	UP-CP-04	UP-MX-01	10B	UP-MX-03	SOEC
10A	UP-MX-02	UP-MX-03	11	SOEC2	UP-HX-01
12	SOEC2	UP-HX-02	7A	UP-CP-01	UP-CO-01
7B	UP-CO-01	UP-CP-02	CW2	UP-CO-01	UP-CO-02
7D	UP-CO-02	UP-CP-03	CW3	UP-CO-02	----
7C	UP-CP-02	UP-CO-02	8	UP-CP-03	UP-FH-01
16	UP-CD-01	UP-SE-01	CW7	UP-CD-01	----
14	UP-CO-03	----	CW5	UP-CO-03	----

FLWSHEET CONNECTIVITY BY BLOCKS

-----

BLOCK	INLETS	OUTLETS
UP-PM-01	1	2
UP-BO-01	2	3
UP-FH-01	8	9
UP-HX-01	11 4	15 5
UP-HX-02	12 5	13 6
SOEC	10B	SOEC1
UP-MX-01	3 20	4
UP-SE-01	16	18 17
UP-SP-01	18	19 21
UP-CP-04	19	20
UP-MX-03	10A	10B
UP-MX-02	6 9	10A
SOEC2	SOEC1	11 12
UP-CP-01	7	7A
UP-CO-01	7A CW1	7B CW2
UP-CO-02	7C CW2	7D CW3
UP-CP-02	7B	7C
UP-CP-03	7D	8
UP-CD-01	15 CW6	16 CW7
UP-CO-03	13 CW4	14 CW5

FLWSHEET SECTION

CONVERGENCE STATUS SUMMARY

-----

DESIGN-SPEC SUMMARY

=====

DESIGN SPEC BLOCK	ERROR	TOLERANCE	ERR/TOL	VARIABLE	STAT	CONV
-----	-----	-----	-----	-----	-----	-----
-						
CWSYS1 \$OLVER02	-0.62375E-08	0.10000E-03	-0.62375E-04	403.02	#	
CWSYS2 \$OLVER03	-0.16906E-04	0.10000E-03	-0.16906	889.66	#	
CWSYS3 \$OLVER04	-0.23763E-06	0.10000E-02	-0.23763E-03	6392.4	#	

TEAR STREAM SUMMARY

=====

STREAM CONV ID BLOCK	VARIABLE ID	MAXIMUM ERR/TOL	MAX. ERR. RELATIVE	ABSOLUTE ERROR	STAT
-----	-----	-----	-----	-----	-----
15 \$OLVER01	ARGON MOLEFLOW	0.47370E-01	0.47370E-05	0.11816E-08	#
10B \$OLVER01	WATER MOLEFLOW	0.0000	0.0000	0.0000	#

# = CONVERGED  
 \* = NOT CONVERGED  
 LB = AT LOWER BOUNDS  
 UB = AT UPPER BOUNDS

DESIGN-SPEC: CWSYS1

-----

SAMPLED VARIABLES:

CW3T : TEMPERATURE IN STREAM CW3 SUBSTREAM MIXED

SPECIFICATION:

MAKE CW3T APPROACH 120.000  
 WITHIN 0.000100000

MANIPULATED VARIABLES:

VARY : WATER MOLEFLOW IN STREAM CW1 SUBSTREAM MIXED  
LOWER LIMIT = 400.000 KMOL/HR  
UPPER LIMIT = 1,000.00 KMOL/HR  
FINAL VALUE = 403.018 KMOL/HR

VALUES OF ACCESSED FORTRAN VARIABLES:

VARIABLE	VALUE AT START OF LOOP	FINAL VALUE	UNITS
-----	-----	-----	-----
CW3T	96.1141	120.000	F

DESIGN-SPEC: CWSYS2

-----

SAMPLED VARIABLES:

CW5T : TEMPERATURE IN STREAM CW5 SUBSTREAM MIXED

FLWSHEET SECTION

DESIGN-SPEC: CWSYS2 (CONTINUED)

SPECIFICATION:

MAKE CW5T APPROACH 85.0000  
WITHIN 0.000100000

MANIPULATED VARIABLES:

VARY : WATER MOLEFLOW IN STREAM CW4 SUBSTREAM MIXED  
LOWER LIMIT = 400.000 KMOL/HR  
UPPER LIMIT = 50,000.0 KMOL/HR  
FINAL VALUE = 889.656 KMOL/HR

VALUES OF ACCESSED FORTRAN VARIABLES:

VARIABLE	VALUE AT START OF LOOP	FINAL VALUE	UNITS
-----	-----	-----	-----
CW5T	85.0000	85.0000	F

DESIGN-SPEC: CWSYS3  
-----

SAMPLED VARIABLES:

CW07T : TEMPERATURE IN STREAM CW7 SUBSTREAM MIXED

SPECIFICATION:

MAKE CW07T APPROACH 90.0000  
WITHIN 0.00100000

MANIPULATED VARIABLES:

VARY : WATER MOLEFLOW IN STREAM CW6 SUBSTREAM MIXED  
LOWER LIMIT = 50.0000 KMOL/HR  
UPPER LIMIT = 500,000. KMOL/HR  
FINAL VALUE = 6,392.41 KMOL/HR

VALUES OF ACCESSED FORTRAN VARIABLES:

VARIABLE	VALUE AT START OF LOOP	FINAL VALUE	UNITS
-----	-----	-----	-----
CW07T	90.0149	90.0000	F

CONVERGENCE BLOCK: \$SOLVER01  
-----

Tear Stream : 15 10B  
Tolerance used: 0.100D-03 0.100D-03  
Trace molefrac: 0.100D-05 0.100D-05

MAXIT= 30 WAIT 1 ITERATIONS BEFORE ACCELERATING  
QMAX = 0.0 QMIN = -5.0



FLWSHEET SECTION

CONVERGENCE BLOCK: \$OLVER01 (CONTINUED)  
 METHOD: WEGSTEIN STATUS: CONVERGED  
 TOTAL NUMBER OF ITERATIONS: 20  
 NUMBER OF ITERATIONS ON LAST OUTER LOOP: 1

\*\*\* FINAL VALUES \*\*\*

VAR#	TEAR STREAM	VAR	STREAM	SUBSTREA	COMPONEN	UNIT
VALUE	PREV VALUE	ERR/TOL				
1	TOTAL MOLEFLOW	15	MIXED			KMOL/HR
620.8822	620.8819	5.7749-03				
2	TOTAL MOLEFLOW	10B	MIXED			KMOL/HR
620.8822	620.8822	0.0				
3	MOLE-FLOW	15	MIXED	WATER		KMOL/HR
351.3000	351.3000	0.0				
4	MOLE-FLOW	15	MIXED	HYDROGEN		KMOL/HR
191.0203	191.0199	1.8548-02				
5	MOLE-FLOW	15	MIXED	NITROGEN		KMOL/HR
77.6640	77.6640	0.0				
6	MOLE-FLOW	15	MIXED	OXYGEN		KMOL/HR
0.0	0.0	0.0				
7	MOLE-FLOW	15	MIXED	ARGON		KMOL/HR
0.8980	0.8980	4.7370-02				
8	PRESSURE	15	MIXED			BAR
38.9658	38.9658	0.0				
9	MASS ENTHALPY	15	MIXED			CAL/GM
1958.3548	-1958.3552	2.1185-03				
10	MOLE-FLOW	10B	MIXED	WATER		KMOL/HR
522.5000	522.5000	0.0				
11	MOLE-FLOW	10B	MIXED	HYDROGEN		KMOL/HR
19.8203	19.8203	0.0				
12	MOLE-FLOW	10B	MIXED	NITROGEN		KMOL/HR
77.6640	77.6640	0.0				
13	MOLE-FLOW	10B	MIXED	OXYGEN		KMOL/HR
0.0	0.0	0.0				
14	MOLE-FLOW	10B	MIXED	ARGON		KMOL/HR
0.8980	0.8980	0.0				
15	PRESSURE	10B	MIXED			BAR
39.3105	39.3105	0.0				
16	MASS ENTHALPY	10B	MIXED			CAL/GM
2232.1863	-2232.1863	0.0				

\*\*\* ITERATION HISTORY \*\*\*

TEAR STREAMS AND TEAR VARIABLES:

ITERATION	MAX-ERR/TOL	VAR#	STREAM ID	VAR DESCRIPTION	SUBSTREA
COMPONEN	ATTRIBUT	ELEMENT			
1	0.4737E-01	7 15		MOLE-FLO	MIXED

ARGON

CONVERGENCE BLOCK: \$SOLVER02

-----

SPECS: CWSYS1

MAXIT= 30 STEP-SIZE= 1.0000 % OF RANGE

MAX-STEP= 100. % OF RANGE

XTOL= 1.000000E-08

THE NEW ALGORITHM WAS USED WITH BRACKETING=NO

METHOD: SECANT STATUS: CONVERGED

TOTAL NUMBER OF ITERATIONS: 7

NUMBER OF ITERATIONS ON LAST OUTER LOOP: 0

FLWSHEET SECTION

CONVERGENCE BLOCK: \$OLVER02 (CONTINUED)

\*\*\* FINAL VALUES \*\*\*

VAR#	VAR NAME	DESIGN SP		VARIABLE DESCRIPTION	UNIT
		CALCULATOR	ERR/TOL		
VALUE	PREV VALUE				
1	VARY	CWSYS1		CW1.MIXED.WATER.MOLEFLOW	KMOL/HR
403.0176	403.0208		-6.2375-05		

\*\*\* ITERATION HISTORY \*\*\*

DESIGN-SPEC ID: CWSYS1  
 ITERATED: WATER MOLEFLOW IN STREAM CW1 SUBSTREAM MIXED

ITERATION	VARIABLE		ERROR	ERR/TOL
1	1000.	UB	-23.89	-0.2389E+06
2	994.0		-23.79	-0.2379E+06
3	400.0	LB	0.3019	3019.
4	697.0		-16.88	-0.1688E+06
5	404.0		-0.1003	-1003.
6	403.0		-0.3183E-03	-3.183
7	403.0		-0.6237E-08	-0.6237E-04

CONVERGENCE BLOCK: \$OLVER03

-----  
 SPECS: CWSYS2  
 MAXIT= 30 STEP-SIZE= 1.0000 % OF RANGE  
 MAX-STEP= 100. % OF RANGE  
 XTOL= 1.000000E-08  
 THE NEW ALGORITHM WAS USED WITH BRACKETING=NO  
 METHOD: SECANT STATUS: CONVERGED  
 TOTAL NUMBER OF ITERATIONS: 25  
 NUMBER OF ITERATIONS ON LAST OUTER LOOP: 1

\*\*\* FINAL VALUES \*\*\*

VAR#	VAR NAME	DESIGN SP		VARIABLE DESCRIPTION	UNIT
		CALCULATOR	ERR/TOL		
VALUE	PREV VALUE				
1	VARY	CWSYS2		CW4.MIXED.WATER.MOLEFLOW	KMOL/HR
889.6555	889.6555		-0.1691		

\*\*\* ITERATION HISTORY \*\*\*

DESIGN-SPEC ID: CWSYS2

ITERATED: WATER MOLEFLOW IN STREAM CW4 SUBSTREAM MIXED

ITERATION	VARIABLE	ERROR	ERR/TOL
-----	-----	-----	-----
1	889.7	-0.1691E-04	-0.1691

FLWSHEET SECTION

CONVERGENCE BLOCK: \$OLVER04

```

-----
  SPECS: CWSYS3
  MAXIT= 30 STEP-SIZE= 1.0000 % OF RANGE
          MAX-STEP= 100. % OF RANGE
          XTOL= 1.000000E-08
  THE NEW ALGORITHM WAS USED WITH BRACKETING=NO
  METHOD: SECANT STATUS: CONVERGED
  TOTAL NUMBER OF ITERATIONS: 71
  NUMBER OF ITERATIONS ON LAST OUTER LOOP: 3
  
```

\*\*\* FINAL VALUES \*\*\*

VAR#	VAR NAME	DESIGN SP CALCULATOR	VARIABLE DESCRIPTION	UNIT
VALUE	PREV VALUE	ERR/TOL		
1	VARY	CWSYS3	CW6.MIXED.WATER.MOLEFLOW	KMOL/HR
6392.4052	6392.5064	-2.3763-04		

\*\*\* ITERATION HISTORY \*\*\*

DESIGN-SPEC ID: CWSYS3  
 ITERATED: WATER MOLEFLOW IN STREAM CW6 SUBSTREAM MIXED

ITERATION	VARIABLE	ERROR	ERR/TOL
1	6391.	0.1494E-01	14.94
2	6393.	-0.1434E-02	-1.434
3	6392.	-0.2376E-06	-0.2376E-03

COMPUTATIONAL SEQUENCE

SEQUENCE USED WAS:

```

UP-CP-01
$OLVER02 UP-CO-01 UP-CP-02 UP-CO-02
(RETURN $OLVER02)
UP-CP-03 UP-FH-01 UP-PM-01 UP-BO-01
$OLVER01 SOEC SOEC2
| $OLVER04 UP-CD-01
| (RETURN $OLVER04)
| *UP-SE-01 UP-SP-01 UP-CP-04 UP-MX-01 UP-HX-01 UP-HX-02 UP-MX-02
| UP-MX-03
(RETURN $OLVER01)
$OLVER03 UP-CO-03
(RETURN $OLVER03)
  
```

OVERALL FLOWSHEET BALANCE

-----

FLOWSHEET SECTION

OVERALL FLOWSHEET BALANCE (CONTINUED)

	*** MASS AND ENERGY BALANCE ***		***	
	IN	OUT	GENERATION	RELATIVE
DIFF.				
CONVENTIONAL COMPONENTS (KMOL/HR )				
WATER	8176.78	8036.38	-140.400	
0.00000				
HYDROGEN	0.00000	140.400	140.400	
0.252349E-05				
NITROGEN	57.1000	57.1000	0.00000	
0.248877E-15				
OXYGEN	15.4000	85.6000	70.2000	
0.166015E-15				
ARGON	0.660000	0.659996	0.00000	
0.644485E-05				
TOTAL BALANCE				
MOLE (KMOL/HR )	8249.94	8320.14	70.2000	
0.430943E-07				
MASS (KG/HR )	149426.	149426.		
0.591694E-08				
ENTHALPY (CAL/SEC )	-0.158378E+09	-0.153646E+09		-
0.298739E-01				

*** CO2 EQUIVALENT SUMMARY ***		
FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

PHYSICAL PROPERTIES SECTION

COMPONENTS

-----

ID	TYPE	ALIAS	NAME
WATER	C	H2O	WATER
HYDROGEN	C	H2	HYDROGEN
NITROGEN	C	N2	NITROGEN
OXYGEN	C	O2	OXYGEN
ARGON	C	AR	ARGON



U-O-S BLOCK SECTION

BLOCK: SOEC MODEL: RSTOIC

-----  
INLET STREAM: 10B  
OUTLET STREAM: SOEC1  
PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*  
IN OUT GENERATION RELATIVE  
DIFF.  
TOTAL BALANCE  
MOLE (KMOL/HR ) 620.882 706.482 85.6000  
0.00000  
MASS (KG/HR ) 11664.4 11664.4  
0.00000  
ENTHALPY (CAL/SEC ) -0.723256E+07 -0.440427E+07 -  
0.391050

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*  
FEED STREAMS CO2E 0.00000 KG/HR  
PRODUCT STREAMS CO2E 0.00000 KG/HR  
NET STREAMS CO2E PRODUCTION 0.00000 KG/HR  
UTILITIES CO2E PRODUCTION 0.00000 KG/HR  
TOTAL CO2E PRODUCTION 0.00000 KG/HR

\*\*\* INPUT DATA \*\*\*  
STOICHIOMETRY MATRIX:

REACTION # 1:  
SUBSTREAM MIXED :  
WATER -1.00 HYDROGEN 1.00 OXYGEN 0.500

REACTION EXTENT SPECS: NUMBER= 1  
REACTION # 1: EXTENT= 171.2 KMOL/HR

TWO PHASE TP FLASH  
SPECIFIED TEMPERATURE C 800.000  
SPECIFIED PRESSURE BAR 39.3105  
MAXIMUM NO. ITERATIONS 30  
CONVERGENCE TOLERANCE 0.000100000  
SIMULTANEOUS REACTIONS  
GENERATE COMBUSTION REACTIONS FOR FEED SPECIES NO

U-O-S BLOCK SECTION

BLOCK: SOEC MODEL: RSTOIC (CONTINUED)

\*\*\* RESULTS \*\*\*

OUTLET TEMPERATURE	C	800.00
OUTLET PRESSURE	BAR	39.311
HEAT DUTY	CAL/SEC	0.28283E+07
VAPOR FRACTION		1.0000

V-L PHASE EQUILIBRIUM :

COMP	F(I)	X(I)	Y(I)	K(I)
WATER	0.49725	0.49725	0.49725	
MISSING				
HYDROGEN	0.27038	0.27038	0.27038	
MISSING				
NITROGEN	0.10993	0.10993	0.10993	
MISSING				
OXYGEN	0.12116	0.12116	0.12116	
MISSING				
ARGON	0.12710E-02	0.12710E-02	0.12710E-02	
MISSING				

BLOCK: SOEC2 MODEL: SEP

-----

INLET STREAM:	SOEC1	
OUTLET STREAMS:	11	12
PROPERTY OPTION SET:	SRK	SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	706.482	706.482	0.00000
MASS (KG/HR )	11664.4	11664.4	0.00000
ENTHALPY (CAL/SEC )	-0.440427E+07	-0.440460E+07	
0.743308E-04			

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

U-O-S BLOCK SECTION

BLOCK: SOEC2 MODEL: SEP (CONTINUED)

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR STREAM 11  
TWO PHASE TP FLASH  
PRESSURE DROP BAR 0.0  
MAXIMUM NO. ITERATIONS 30  
CONVERGENCE TOLERANCE 0.000100000

FLASH SPECS FOR STREAM 12  
TWO PHASE TP FLASH  
PRESSURE DROP BAR 0.0  
MAXIMUM NO. ITERATIONS 30  
CONVERGENCE TOLERANCE 0.000100000

FRACTION OF FEED  
SUBSTREAM= MIXED  
STREAM= 12 CPT= WATER FRACTION= 0.0  
HYDROGEN 0.0  
NITROGEN 0.0  
ARGON 0.0

MOLE-FLOW (KMOL/HR )  
SUBSTREAM= MIXED  
STREAM= 12 CPT= OXYGEN FLOW= 85.6000

\*\*\* RESULTS \*\*\*

HEAT DUTY CAL/SEC -327.40

COMPONENT = WATER  
STREAM SUBSTREAM SPLIT FRACTION  
11 MIXED 1.00000

COMPONENT = HYDROGEN  
STREAM SUBSTREAM SPLIT FRACTION  
11 MIXED 1.00000

COMPONENT = NITROGEN  
STREAM SUBSTREAM SPLIT FRACTION  
11 MIXED 1.00000

COMPONENT = OXYGEN  
STREAM SUBSTREAM SPLIT FRACTION  
12 MIXED 1.00000

U-O-S BLOCK SECTION

BLOCK: SOEC2 MODEL: SEP (CONTINUED)

COMPONENT = ARGON

STREAM	SUBSTREAM	SPLIT FRACTION
11	MIXED	1.00000

BLOCK: UP-BO-01 MODEL: HEATER

-----  
INLET STREAM: 2  
OUTLET STREAM: 3  
PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*  
IN OUT RELATIVE

DIFF.

TOTAL BALANCE	IN	OUT	RELATIVE
MOLE (KMOL/HR )	491.700	491.700	0.00000
MASS (KG/HR )	8858.11	8858.11	0.00000
ENTHALPY (CAL/SEC )	-0.941751E+07	-0.746901E+07	-0.206903

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

TWO PHASE TP FLASH		
SPECIFIED TEMPERATURE	C	420.000
SPECIFIED PRESSURE	BAR	40.0000
MAXIMUM NO. ITERATIONS		30
CONVERGENCE TOLERANCE		

0.000100000

\*\*\* RESULTS \*\*\*

OUTLET TEMPERATURE	C	420.00
OUTLET PRESSURE	BAR	40.000
HEAT DUTY	CAL/SEC	0.19485E+07
OUTLET VAPOR FRACTION		1.0000

U-O-S BLOCK SECTION

BLOCK: UP-BO-01 MODEL: HEATER (CONTINUED)

V-L PHASE EQUILIBRIUM :

COMP	F(I)	X(I)	Y(I)	K(I)
WATER	1.0000	1.0000	1.0000	
MISSING				

BLOCK: UP-CD-01 MODEL: HEATX

-----  
 HOT SIDE:

-----  
 INLET STREAM: 15  
 OUTLET STREAM: 16  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 COLD SIDE:

-----  
 INLET STREAM: CW6  
 OUTLET STREAM: CW7  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*  
 IN OUT RELATIVE

DIFF.

TOTAL BALANCE	IN	OUT	RELATIVE
MOLE (KMOL/HR )	7013.29	7013.29	0.00000
MASS (KG/HR )	124086.	124086.	0.00000
ENTHALPY (CAL/SEC )	-0.128948E+09	-0.128948E+09	-

0.231119E-15

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR HOT SIDE:

TWO PHASE FLASH  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLASH SPECS FOR COLD SIDE:

TWO PHASE FLASH  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

U-O-S BLOCK SECTION

BLOCK: UP-CD-01 MODEL: HEATX (CONTINUED)

FLOW DIRECTION AND SPECIFICATION:

COUNTERCURRENT HEAT EXCHANGER  
 SPECIFIED HOT OUTLET TEMP  
 SPECIFIED VALUE C 35.0000  
 LMTD CORRECTION FACTOR 1.00000

PRESSURE SPECIFICATION:

HOT SIDE PRESSURE DROP BAR 0.0345  
 COLD SIDE PRESSURE DROP BAR 0.0000

HEAT TRANSFER COEFFICIENT SPECIFICATION:

HOT LIQUID	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD VAPOR	CAL/SEC-SQCM-K	0.0203

\*\*\* OVERALL RESULTS \*\*\*

STREAMS:

```

-----
15          -----> |          HOT          | -----> 16
T= 5.9845D+02 |          |          T=
3.5000D+01     |          |          P=
P= 3.8966D+01 |          |          P=
3.8931D+01     |          |          V=
V= 1.0000D+00 |          |          V=
4.3473D-01     |          |          |
              |          |          |
CW7          <----- |          COLD          | <----- CW6
T= 3.2222D+01 |          |          T= -
1.7778D+01     |          |          P=
P= 1.0000D+00 |          |          P=
1.0000D+00     |          |          V=
V= 0.0000D+00 |          |          V=
0.0000D+00     |          |          |
              |          |          |
-----

```

DUTY AND AREA:

CALCULATED HEAT DUTY	CAL/SEC	1849243.1706
CALCULATED (REQUIRED) AREA	SQM	65.9652
ACTUAL EXCHANGER AREA	SQM	65.9652

PER CENT OVER-DESIGN		0.0000
HEAT TRANSFER COEFFICIENT:		
AVERAGE COEFFICIENT (DIRTY)	CAL/SEC-SQCM-K	0.0203
UA (DIRTY)	CAL/SEC-K	13392.1917
LOG-MEAN TEMPERATURE DIFFERENCE:		
LMTD CORRECTION FACTOR		1.0000
LMTD (CORRECTED)	C	138.0837
NUMBER OF SHELLS IN SERIES		1
PRESSURE DROP:		
HOTSIDE, TOTAL	BAR	0.0345
COLD SIDE, TOTAL	BAR	0.0000

U-O-S BLOCK SECTION

BLOCK: UP-CD-01 MODEL: HEATX (CONTINUED)

\*\*\* ZONE RESULTS \*\*\*

TEMPERATURE LEAVING EACH ZONE:

		HOT			
HOT IN		VAP		COND	
HOT OUT					
----->					---
---					
598.5		213.7			
35.0					
COLDOUT		LIQ		LIQ	
COLDIN					
<-----					<--
----					
32.2		17.0			-
17.8					
		COLD			

ZONE HEAT TRANSFER AND AREA:

ZONE	HEAT DUTY CAL/SEC	AREA SQM	LMTD C	AVERAGE U CAL/SEC-SQCM-K	UA
CAL/SEC-K					
1	559364.539	7.8838	349.4788	0.0203	
1600.5680					
2	1289878.632	58.0814	109.3894	0.0203	
11791.6237					



U-O-S BLOCK SECTION

HEATX COLD-TQCU UP-CD-01 TQCURV INLET

-----  
 PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: 0.0 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

! DUTY	! PRES	! TEMP	! VFRAC	!
! CAL/SEC	! BAR	! C	!	!
! 0.0	! 1.0000	! 32.2222	! 0.0	!
! 8.8059+04	! 1.0000	! 29.8281	! 0.0	!
! 1.7612+05	! 1.0000	! 27.4346	! 0.0	!
! 2.6418+05	! 1.0000	! 25.0420	! 0.0	!
! 3.5224+05	! 1.0000	! 22.6501	! 0.0	!
! 4.4030+05	! 1.0000	! 20.2593	! 0.0	!
! 5.2836+05	! 1.0000	! 17.8695	! 0.0	!
! 5.5935+05	! 1.0000	! 17.0286	! 0.0	!
! 6.1641+05	! 1.0000	! 15.4810	! 0.0	!
! 7.0447+05	! 1.0000	! 13.0937	! 0.0	!
! 7.9253+05	! 1.0000	! 10.7078	! 0.0	!
! 8.8059+05	! 1.0000	! 8.3234	! 0.0	!
! 9.6865+05	! 1.0000	! 5.9405	! 0.0	!
! 1.0567+06	! 1.0000	! 3.5594	! 0.0	!
! 1.1448+06	! 1.0000	! 1.1801	! 0.0	!
! 1.2328+06	! 1.0000	! -1.1974	! 0.0	!
! 1.3209+06	! 1.0000	! -3.5728	! 0.0	!
! 1.4089+06	! 1.0000	! -5.9461	! 0.0	!
! 1.4970+06	! 1.0000	! -8.3173	! 0.0	!
! 1.5851+06	! 1.0000	! -10.6861	! 0.0	!
! 1.6731+06	! 1.0000	! -13.0525	! 0.0	!
! 1.7612+06	! 1.0000	! -15.4165	! 0.0	!
! 1.8492+06	! 1.0000	! -17.7778	! 0.0	!

U-O-S BLOCK SECTION

HEATX HOT-TQCUR UP-CD-01 TQCURV INLET

-----  
 PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: 0.0 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

! DUTY	! PRES	! TEMP	! VFRAC	!
! CAL/SEC	! BAR	! C	!	!
! 0.0	! 38.9658	! 598.4517	! 1.0000	!
! 8.8059+04	! 38.9658	! 539.0362	! 1.0000	!
! 1.7612+05	! 38.9658	! 478.9835	! 1.0000	!
! 2.6418+05	! 38.9658	! 418.3820	! 1.0000	!
! 3.5224+05	! 38.9658	! 357.3703	! 1.0000	!
! 4.4030+05	! 38.9658	! 296.1613	! 1.0000	!
! 5.2836+05	! 38.9658	! 235.0891	! 1.0000	!
! 5.5935+05	! 38.9658	! 213.7170	! DEW>1.0000	!
! 6.1641+05	! 38.9658	! 212.1274	! 0.9619	!
! 7.0447+05	! 38.9658	! 209.3752	! 0.9040	!
! 7.9253+05	! 38.9658	! 206.1884	! 0.8472	!
! 8.8059+05	! 38.9658	! 202.4636	! 0.7919	!
! 9.6865+05	! 38.9658	! 198.0651	! 0.7382	!
! 1.0567+06	! 38.9658	! 192.8126	! 0.6865	!
! 1.1448+06	! 38.9658	! 186.4635	! 0.6375	!
! 1.2328+06	! 38.9658	! 178.6899	! 0.5917	!
! 1.3209+06	! 38.9658	! 169.0453	! 0.5499	!
! 1.4089+06	! 38.9658	! 156.9273	! 0.5131	!
! 1.4970+06	! 38.9658	! 141.5472	! 0.4825	!
! 1.5851+06	! 38.9658	! 121.9693	! 0.4594	!
! 1.6731+06	! 38.9658	! 97.3929	! 0.4445	!
! 1.7612+06	! 38.9658	! 67.8882	! 0.4372	!
! 1.8492+06	! 38.9658	! 34.9997	! 0.4347	!

U-O-S BLOCK SECTION

BLOCK: UP-CO-01 MODEL: HEATX

-----  
 HOT SIDE:  
 -----

INLET STREAM: 7A  
 OUTLET STREAM: 7B  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 COLD SIDE:  
 -----

INLET STREAM: CW1  
 OUTLET STREAM: CW2  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

DIFF.	IN	OUT	RELATIVE
TOTAL BALANCE			
MOLE (KMOL/HR )	476.178	476.178	0.00000
MASS (KG/HR )	9379.19	9379.19	0.00000
ENTHALPY (CAL/SEC )	-0.769531E+07	-0.769531E+07	0.00000

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR HOT SIDE:

TWO PHASE FLASH  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLASH SPECS FOR COLD SIDE:

TWO PHASE FLASH  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLOW DIRECTION AND SPECIFICATION:

COUNTERCURRENT HEAT EXCHANGER  
 SPECIFIED HOT OUTLET TEMP  
 SPECIFIED VALUE C 37.7778  
 LMTD CORRECTION FACTOR 1.00000

U-O-S BLOCK SECTION

BLOCK: UP-CO-01 MODEL: HEATX (CONTINUED)

PRESSURE SPECIFICATION:

HOT SIDE PRESSURE DROP	BAR	0.3447
COLD SIDE PRESSURE DROP	BAR	0.0000

HEAT TRANSFER COEFFICIENT SPECIFICATION:

HOT LIQUID	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD VAPOR	CAL/SEC-SQCM-K	0.0203

\*\*\* OVERALL RESULTS \*\*\*

STREAMS:

```

-----
7A      ----->|          HOT          |-----> 7B
T= 1.9791D+02  |          |          |          T=
3.7778D+01     |          |          |
P= 3.4200D+00  |          |          |          P=
3.0753D+00     |          |          |
V= 1.0000D+00  |          |          |          V=
1.0000D+00     |          |          |
                |          |          |
CW2      <-----|          COLD          |<----- CW1
T= 3.6532D+01  |          |          |          T=
2.6667D+01     |          |          |
P= 1.0000D+00  |          |          |          P=
1.0000D+00     |          |          |
V= 0.0000D+00  |          |          |          V=
0.0000D+00     |          |          |
-----

```

DUTY AND AREA:

CALCULATED HEAT DUTY	CAL/SEC	22875.9612
CALCULATED (REQUIRED) AREA	SQM	2.0065
ACTUAL EXCHANGER AREA	SQM	2.0065
PER CENT OVER-DESIGN		0.0000

HEAT TRANSFER COEFFICIENT:

AVERAGE COEFFICIENT (DIRTY)	CAL/SEC-SQCM-K	0.0203
UA (DIRTY)	CAL/SEC-K	407.3491

LOG-MEAN TEMPERATURE DIFFERENCE:

LMTD CORRECTION FACTOR		1.0000
LMTD (CORRECTED)	C	56.1581
NUMBER OF SHELLS IN SERIES		1

PRESSURE DROP:

HOTSIDE, TOTAL	BAR	0.3447
COLD SIDE, TOTAL	BAR	0.0000

U-O-S BLOCK SECTION

BLOCK: UP-CO-01 MODEL: HEATX (CONTINUED)

\*\*\* ZONE RESULTS \*\*\*

TEMPERATURE LEAVING EACH ZONE:

HOT	
HOT IN	VAP
HOT OUT	
----->	
--->	
197.9	
37.8	
COLDOUT	LIQ
COLDIN	
<-----	
----	
36.5	
26.7	
COLD	

ZONE HEAT TRANSFER AND AREA:

ZONE	HEAT DUTY	AREA	LMTD	AVERAGE U	UA
CAL/SEC-K	CAL/SEC	SQM	C	CAL/SEC-SQCM-K	
1	22875.961	2.0065	56.1581	0.0203	
407.3491					

U-O-S BLOCK SECTION

HEATX COLD-TQCU UP-CO-01 TQCURV INLET

-----  
 PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: 0.0 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

! DUTY	! PRES	! TEMP	! VFRAC	!
! CAL/SEC	! BAR	! C	!	!
! 0.0	! 1.0000	! 36.5319	! 0.0	!
! 1089.3315	! 1.0000	! 36.0619	! 0.0	!
! 2178.6630	! 1.0000	! 35.5919	! 0.0	!
! 3267.9945	! 1.0000	! 35.1220	! 0.0	!
! 4357.3259	! 1.0000	! 34.6521	! 0.0	!
! 5446.6574	! 1.0000	! 34.1822	! 0.0	!
! 6535.9889	! 1.0000	! 33.7123	! 0.0	!
! 7625.3204	! 1.0000	! 33.2424	! 0.0	!
! 8714.6519	! 1.0000	! 32.7725	! 0.0	!
! 9803.9834	! 1.0000	! 32.3027	! 0.0	!
! 1.0893+04	! 1.0000	! 31.8329	! 0.0	!
! 1.1983+04	! 1.0000	! 31.3631	! 0.0	!
! 1.3072+04	! 1.0000	! 30.8934	! 0.0	!
! 1.4161+04	! 1.0000	! 30.4236	! 0.0	!
! 1.5251+04	! 1.0000	! 29.9539	! 0.0	!
! 1.6340+04	! 1.0000	! 29.4842	! 0.0	!
! 1.7429+04	! 1.0000	! 29.0146	! 0.0	!
! 1.8519+04	! 1.0000	! 28.5449	! 0.0	!
! 1.9608+04	! 1.0000	! 28.0753	! 0.0	!
! 2.0697+04	! 1.0000	! 27.6057	! 0.0	!
! 2.1787+04	! 1.0000	! 27.1362	! 0.0	!
! 2.2876+04	! 1.0000	! 26.6667	! 0.0	!

U-O-S BLOCK SECTION

HEATX HOT-TQCUR UP-CO-01 TQCURV INLET

-----  
 PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: 0.0 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

! DUTY	! PRES	! TEMP	! VFRAC	!
! CAL/SEC	! BAR	! C	!	!
! 0.0	! 3.4200	! 197.9118	! 1.0000	!
! 1089.3315	! 3.4200	! 190.3568	! 1.0000	!
! 2178.6630	! 3.4200	! 182.7929	! 1.0000	!
! 3267.9945	! 3.4200	! 175.2203	! 1.0000	!
! 4357.3259	! 3.4200	! 167.6394	! 1.0000	!
! 5446.6574	! 3.4200	! 160.0505	! 1.0000	!
! 6535.9889	! 3.4200	! 152.4540	! 1.0000	!
! 7625.3204	! 3.4200	! 144.8500	! 1.0000	!
! 8714.6519	! 3.4200	! 137.2391	! 1.0000	!
! 9803.9834	! 3.4200	! 129.6216	! 1.0000	!
! 1.0893+04	! 3.4200	! 121.9979	! 1.0000	!
! 1.1983+04	! 3.4200	! 114.3684	! 1.0000	!
! 1.3072+04	! 3.4200	! 106.7334	! 1.0000	!
! 1.4161+04	! 3.4200	! 99.0935	! 1.0000	!
! 1.5251+04	! 3.4200	! 91.4489	! 1.0000	!
! 1.6340+04	! 3.4200	! 83.8003	! 1.0000	!
! 1.7429+04	! 3.4200	! 76.1480	! 1.0000	!
! 1.8519+04	! 3.4200	! 68.4925	! 1.0000	!
! 1.9608+04	! 3.4200	! 60.8342	! 1.0000	!
! 2.0697+04	! 3.4200	! 53.1737	! 1.0000	!
! 2.1787+04	! 3.4200	! 45.5114	! 1.0000	!
! 2.2876+04	! 3.4200	! 37.8479	! 1.0000	!



U-O-S BLOCK SECTION

BLOCK: UP-CO-02 MODEL: HEATX

-----  
 HOT SIDE:  
 -----

INLET STREAM: 7C  
 OUTLET STREAM: 7D  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 COLD SIDE:  
 -----

INLET STREAM: CW2  
 OUTLET STREAM: CW3  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	476.178	476.178	0.00000
MASS (KG/HR )	9379.19	9379.19	0.00000
ENTHALPY (CAL/SEC )	-0.766691E+07	-0.766691E+07	
0.121473E-15			

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR HOT SIDE:

TWO PHASE FLASH  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLASH SPECS FOR COLD SIDE:

TWO PHASE FLASH  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLOW DIRECTION AND SPECIFICATION:

COUNTERCURRENT HEAT EXCHANGER  
 SPECIFIED HOT OUTLET TEMP  
 SPECIFIED VALUE C 37.7778  
 LMTD CORRECTION FACTOR 1.00000

U-O-S BLOCK SECTION

BLOCK: UP-CO-02 MODEL: HEATX (CONTINUED)

PRESSURE SPECIFICATION:

HOT SIDE PRESSURE DROP	BAR	0.3447
COLD SIDE PRESSURE DROP	BAR	0.0000

HEAT TRANSFER COEFFICIENT SPECIFICATION:

HOT LIQUID	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD VAPOR	CAL/SEC-SQCM-K	0.0203

\*\*\* OVERALL RESULTS \*\*\*

STREAMS:

```

-----
7C      -----> |                | |-----> 7D
T=  2.3622D+02 |                | |                T=
3.7778D+01     |                | |                P=
P=  1.1700D+01 |                | |                P=
1.1355D+01     |                | |                V=
V=  1.0000D+00 |                | |                V=
1.0000D+00     |                | |
CW3      <-----|                | |<----- CW2
T=  4.8889D+01 |                | |                T=
3.6532D+01     |                | |                P=
P=  1.0000D+00 |                | |                P=
1.0000D+00     |                | |                V=
V=  0.0000D+00 |                | |                V=
0.0000D+00     |                | |
-----
    
```

DUTY AND AREA:

CALCULATED HEAT DUTY	CAL/SEC	28635.0522
CALCULATED (REQUIRED) AREA	SQM	3.7997
ACTUAL EXCHANGER AREA	SQM	3.7997
PER CENT OVER-DESIGN		0.0000

HEAT TRANSFER COEFFICIENT:

AVERAGE COEFFICIENT (DIRTY)	CAL/SEC-SQCM-K	0.0203
UA (DIRTY)	CAL/SEC-K	771.4194

LOG-MEAN TEMPERATURE DIFFERENCE:

LMTD CORRECTION FACTOR		1.0000
LMTD (CORRECTED)	C	37.1200
NUMBER OF SHELLS IN SERIES		1

PRESSURE DROP:

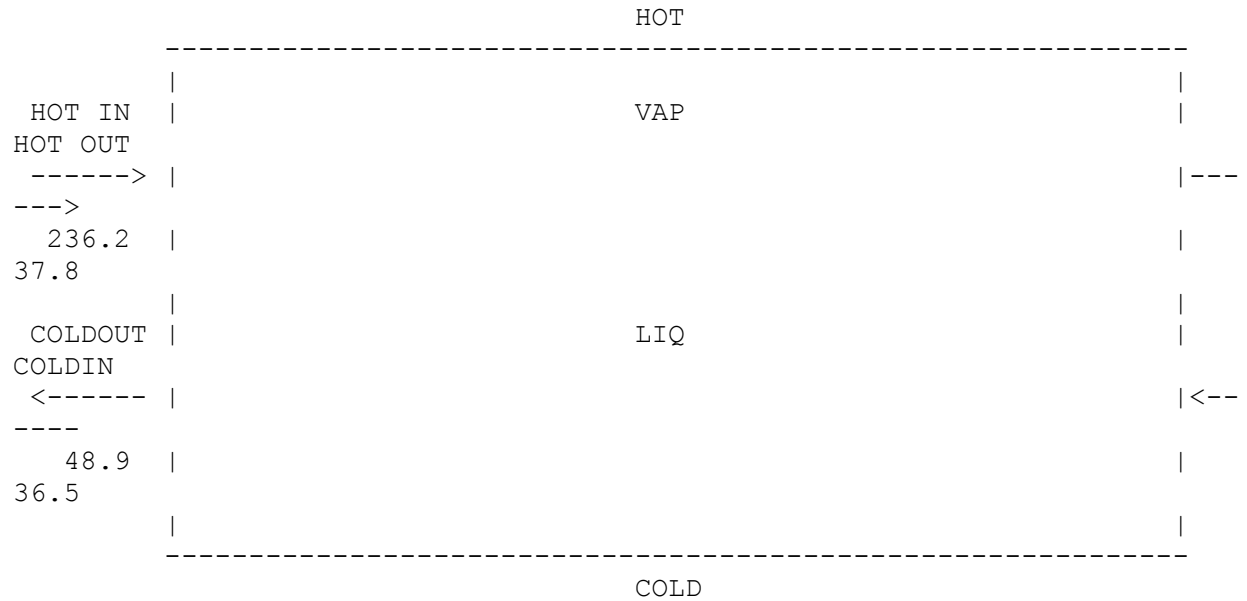
HOTSIDE, TOTAL	BAR	0.3447
COLD SIDE, TOTAL	BAR	0.0000

U-O-S BLOCK SECTION

BLOCK: UP-CO-02 MODEL: HEATX (CONTINUED)

\*\*\* ZONE RESULTS \*\*\*

TEMPERATURE LEAVING EACH ZONE:



ZONE HEAT TRANSFER AND AREA:

ZONE	HEAT DUTY	AREA	LMTD	AVERAGE U	UA
CAL/SEC-K	CAL/SEC	SQM	C	CAL/SEC-SQCM-K	
1	28635.052	3.7997	37.1200	0.0203	
771.4194					

U-O-S BLOCK SECTION

HEATX COLD-TQCU UP-CO-02 TQCURV INLET

-----  
 PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: 0.0 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

! DUTY	! PRES	! TEMP	! VFRAC	!
!	!	!	!	!
!	!	!	!	!
! CAL/SEC	! BAR	! C	!	!
!	!	!	!	!
! =====	! =====	! =====	! =====	! =====
! 0.0	! 1.0000	! 48.8889	! 0.0	!
! 1363.5739	! 1.0000	! 48.3004	! 0.0	!
! 2727.1478	! 1.0000	! 47.7120	! 0.0	!
! 4090.7217	! 1.0000	! 47.1235	! 0.0	!
! 5454.2957	! 1.0000	! 46.5351	! 0.0	!
! -----	! -----	! -----	! -----	! -----
! 6817.8696	! 1.0000	! 45.9466	! 0.0	!
! 8181.4435	! 1.0000	! 45.3581	! 0.0	!
! 9545.0174	! 1.0000	! 44.7696	! 0.0	!
! 1.0909+04	! 1.0000	! 44.1812	! 0.0	!
! 1.2272+04	! 1.0000	! 43.5927	! 0.0	!
! -----	! -----	! -----	! -----	! -----
! 1.3636+04	! 1.0000	! 43.0042	! 0.0	!
! 1.4999+04	! 1.0000	! 42.4158	! 0.0	!
! 1.6363+04	! 1.0000	! 41.8273	! 0.0	!
! 1.7726+04	! 1.0000	! 41.2389	! 0.0	!
! 1.9090+04	! 1.0000	! 40.6505	! 0.0	!
! -----	! -----	! -----	! -----	! -----
! 2.0454+04	! 1.0000	! 40.0620	! 0.0	!
! 2.1817+04	! 1.0000	! 39.4736	! 0.0	!
! 2.3181+04	! 1.0000	! 38.8853	! 0.0	!
! 2.4544+04	! 1.0000	! 38.2969	! 0.0	!
! 2.5908+04	! 1.0000	! 37.7085	! 0.0	!
! -----	! -----	! -----	! -----	! -----
! 2.7271+04	! 1.0000	! 37.1202	! 0.0	!
! 2.8635+04	! 1.0000	! 36.5319	! 0.0	!

U-O-S BLOCK SECTION

HEATX HOT-TQCUR UP-CO-02 TQCURV INLET

-----  
 PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: 0.0 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

! DUTY	! PRES	! TEMP	! VFRAC	!
! CAL/SEC	! BAR	! C	!	!
! 0.0	! 11.7000	! 236.2172	! 1.0000	!
! 1363.5739	! 11.7000	! 226.8587	! 1.0000	!
! 2727.1478	! 11.7000	! 217.4864	! 1.0000	!
! 4090.7217	! 11.7000	! 208.1009	! 1.0000	!
! 5454.2957	! 11.7000	! 198.7028	! 1.0000	!
! 6817.8696	! 11.7000	! 189.2927	! 1.0000	!
! 8181.4435	! 11.7000	! 179.8714	! 1.0000	!
! 9545.0174	! 11.7000	! 170.4396	! 1.0000	!
! 1.0909+04	! 11.7000	! 160.9980	! 1.0000	!
! 1.2272+04	! 11.7000	! 151.5476	! 1.0000	!
! 1.3636+04	! 11.7000	! 142.0893	! 1.0000	!
! 1.4999+04	! 11.7000	! 132.6240	! 1.0000	!
! 1.6363+04	! 11.7000	! 123.1527	! 1.0000	!
! 1.7726+04	! 11.7000	! 113.6767	! 1.0000	!
! 1.9090+04	! 11.7000	! 104.1968	! 1.0000	!
! 2.0454+04	! 11.7000	! 94.7145	! 1.0000	!
! 2.1817+04	! 11.7000	! 85.2310	! 1.0000	!
! 2.3181+04	! 11.7000	! 75.7476	! 1.0000	!
! 2.4544+04	! 11.7000	! 66.2658	! 1.0000	!
! 2.5908+04	! 11.7000	! 56.7871	! 1.0000	!
! 2.7271+04	! 11.7000	! 47.3130	! 1.0000	!
! 2.8635+04	! 11.7000	! 37.8454	! 1.0000	!

U-O-S BLOCK SECTION

BLOCK: UP-CO-03 MODEL: HEATX

-----  
 HOT SIDE:  
 -----

INLET STREAM: 13  
 OUTLET STREAM: 14  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 COLD SIDE:  
 -----

INLET STREAM: CW4  
 OUTLET STREAM: CW5  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

DIFF.	IN	OUT	RELATIVE
TOTAL BALANCE			
MOLE (KMOL/HR )	975.256	975.256	0.00000
MASS (KG/HR )	18766.5	18766.5	0.00000
ENTHALPY (CAL/SEC )	-0.170273E+08	-0.170273E+08	0.00000

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR HOT SIDE:

TWO PHASE FLASH  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLASH SPECS FOR COLD SIDE:

TWO PHASE FLASH  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLOW DIRECTION AND SPECIFICATION:

COUNTERCURRENT HEAT EXCHANGER  
 SPECIFIED HOT OUTLET TEMP  
 SPECIFIED VALUE C 35.0000  
 LMTD CORRECTION FACTOR 1.00000

U-O-S BLOCK SECTION

BLOCK: UP-CO-03 MODEL: HEATX (CONTINUED)

PRESSURE SPECIFICATION:

HOT SIDE PRESSURE DROP	BAR	0.0345
COLD SIDE PRESSURE DROP	BAR	0.0000

HEAT TRANSFER COEFFICIENT SPECIFICATION:

HOT LIQUID	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD VAPOR	CAL/SEC-SQCM-K	0.0203

\*\*\* OVERALL RESULTS \*\*\*

STREAMS:

```

-----
13      -----> |                | -----> 14
T= 6.4962D+02 |                | T=
3.5000D+01 |                |
P= 3.8966D+01 |                | P=
3.8931D+01 |                |
V= 1.0000D+00 |                | V=
1.0000D+00 |                |
          |                |
CW5      <----- |                | <----- CW4
T= 2.9444D+01 |                | T=
7.2222D+00 |                |
P= 1.0000D+00 |                | P=
1.0000D+00 |                |
V= 0.0000D+00 |                | V=
0.0000D+00 |                |
-----

```

DUTY AND AREA:

CALCULATED HEAT DUTY	CAL/SEC	113997.9145
CALCULATED (REQUIRED) AREA	SQM	2.9438
ACTUAL EXCHANGER AREA	SQM	2.9438
PER CENT OVER-DESIGN		0.0000

HEAT TRANSFER COEFFICIENT:

AVERAGE COEFFICIENT (DIRTY)	CAL/SEC-SQCM-K	0.0203
UA (DIRTY)	CAL/SEC-K	597.6554



LOG-MEAN TEMPERATURE DIFFERENCE:

LMTD CORRECTION FACTOR		1.0000
LMTD (CORRECTED)	C	190.7419
NUMBER OF SHELLS IN SERIES		1

PRESSURE DROP:

HOTSIDE, TOTAL	BAR	0.0345
COLD SIDE, TOTAL	BAR	0.0000

U-O-S BLOCK SECTION

BLOCK: UP-CO-03 MODEL: HEATX (CONTINUED)

\*\*\* ZONE RESULTS \*\*\*

TEMPERATURE LEAVING EACH ZONE:

HOT	
HOT IN	VAP
HOT OUT	
----->	
--->	
649.6	
35.0	
COLDOUT	LIQ
COLDIN	
<-----	
----	
29.4	
7.2	
-----	
COLD	

ZONE HEAT TRANSFER AND AREA:

ZONE	HEAT DUTY	AREA	LMTD	AVERAGE U	UA
CAL/SEC-K	CAL/SEC	SQM	C	CAL/SEC-SQCM-K	
1	113997.915	2.9438	190.7419	0.0203	
597.6554					

U-O-S BLOCK SECTION

HEATX COLD-TQCU UP-CO-03 TQCURV INLET

-----  
 PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: 0.0 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

! DUTY	! PRES	! TEMP	! VFRAC	!
! CAL/SEC	! BAR	! C	!	!
! 0.0	! 1.0000	! 29.4444	! 0.0	!
! 5428.4721	! 1.0000	! 28.3842	! 0.0	!
! 1.0857+04	! 1.0000	! 27.3242	! 0.0	!
! 1.6285+04	! 1.0000	! 26.2643	! 0.0	!
! 2.1714+04	! 1.0000	! 25.2045	! 0.0	!
! 2.7142+04	! 1.0000	! 24.1450	! 0.0	!
! 3.2571+04	! 1.0000	! 23.0856	! 0.0	!
! 3.7999+04	! 1.0000	! 22.0264	! 0.0	!
! 4.3428+04	! 1.0000	! 20.9674	! 0.0	!
! 4.8856+04	! 1.0000	! 19.9086	! 0.0	!
! 5.4285+04	! 1.0000	! 18.8500	! 0.0	!
! 5.9713+04	! 1.0000	! 17.7916	! 0.0	!
! 6.5142+04	! 1.0000	! 16.7335	! 0.0	!
! 7.0570+04	! 1.0000	! 15.6756	! 0.0	!
! 7.5999+04	! 1.0000	! 14.6179	! 0.0	!
! 8.1427+04	! 1.0000	! 13.5606	! 0.0	!
! 8.6856+04	! 1.0000	! 12.5034	! 0.0	!
! 9.2284+04	! 1.0000	! 11.4466	! 0.0	!
! 9.7712+04	! 1.0000	! 10.3901	! 0.0	!
! 1.0314+05	! 1.0000	! 9.3338	! 0.0	!
! 1.0857+05	! 1.0000	! 8.2779	! 0.0	!
! 1.1400+05	! 1.0000	! 7.2222	! 0.0	!

U-O-S BLOCK SECTION

HEATX HOT-TQCUR UP-CO-03 TQCURV INLET

-----  
 PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: 0.0 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

! DUTY	! PRES	! TEMP	! VFRAC	!
! CAL/SEC	! BAR	! C	!	!
! 0.0	! 38.9658	! 649.6228	! 1.0000	!
! 5428.4721	! 38.9658	! 621.9434	! 1.0000	!
! 1.0857+04	! 38.9658	! 594.1472	! 1.0000	!
! 1.6285+04	! 38.9658	! 566.2272	! 1.0000	!
! 2.1714+04	! 38.9658	! 538.1757	! 1.0000	!
! 2.7142+04	! 38.9658	! 509.9844	! 1.0000	!
! 3.2571+04	! 38.9658	! 481.6443	! 1.0000	!
! 3.7999+04	! 38.9658	! 453.1458	! 1.0000	!
! 4.3428+04	! 38.9658	! 424.4788	! 1.0000	!
! 4.8856+04	! 38.9658	! 395.6328	! 1.0000	!
! 5.4285+04	! 38.9658	! 366.5973	! 1.0000	!
! 5.9713+04	! 38.9658	! 337.3621	! 1.0000	!
! 6.5142+04	! 38.9658	! 307.9180	! 1.0000	!
! 7.0570+04	! 38.9658	! 278.2580	! 1.0000	!
! 7.5999+04	! 38.9658	! 248.3788	! 1.0000	!
! 8.1427+04	! 38.9658	! 218.2828	! 1.0000	!
! 8.6856+04	! 38.9658	! 187.9816	! 1.0000	!
! 9.2284+04	! 38.9658	! 157.4991	! 1.0000	!
! 9.7712+04	! 38.9658	! 126.8775	! 1.0000	!
! 1.0314+05	! 38.9658	! 96.1829	! 1.0000	!
! 1.0857+05	! 38.9658	! 65.5132	! 1.0000	!
! 1.1400+05	! 38.9658	! 35.0080	! 1.0000	!

BLOCK: UP-CP-01 MODEL: COMPR

-----  
 INLET STREAM: 7  
 OUTLET STREAM: 7A  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

DIFF.

IN

OUT

RELATIVE

U-O-S BLOCK SECTION

BLOCK: UP-CP-01 MODEL: COMPR (CONTINUED)

TOTAL BALANCE			
MOLE (KMOL/HR )	73.1600	73.1600	0.00000
MASS (KG/HR )	2118.72	2118.72	0.00000
ENTHALPY (CAL/SEC )	-32.2948	24591.9	-1.00131

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

ISENTROPIC CENTRIFUGAL COMPRESSOR

OUTLET PRESSURE BAR	3.42000
ISENTROPIC EFFICIENCY	0.72000
MECHANICAL EFFICIENCY	1.00000

\*\*\* RESULTS \*\*\*

INDICATED HORSEPOWER REQUIREMENT KW	103.097
BRAKE HORSEPOWER REQUIREMENT KW	103.097
NET WORK REQUIRED KW	103.097
POWER LOSSES KW	0.0
ISENTROPIC HORSEPOWER REQUIREMENT KW	74.2295
CALCULATED OUTLET TEMP C	197.912
ISENTROPIC TEMPERATURE C	149.950
EFFICIENCY (POLYTR/ISENTR) USED	0.72000
OUTLET VAPOR FRACTION	1.00000
HEAD DEVELOPED, M-KGF/KG	12,861.3
MECHANICAL EFFICIENCY USED	1.00000
INLET HEAT CAPACITY RATIO	1.40242
INLET VOLUMETRIC FLOW RATE , L/MIN	30,221.5
OUTLET VOLUMETRIC FLOW RATE, L/MIN	13,983.5
INLET COMPRESSIBILITY FACTOR	0.99984
OUTLET COMPRESSIBILITY FACTOR	1.00141
AV. ISENT. VOL. EXPONENT	1.40015
AV. ISENT. TEMP EXPONENT	1.39791
AV. ACTUAL VOL. EXPONENT	1.59553
AV. ACTUAL TEMP EXPONENT	1.59229

U-O-S BLOCK SECTION

BLOCK: UP-CP-02 MODEL: COMPR

-----  
INLET STREAM: 7B  
OUTLET STREAM: 7C  
PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	73.1600	73.1600	0.00000
MASS (KG/HR )	2118.72	2118.72	0.00000
ENTHALPY (CAL/SEC )	1715.93	30114.2	-0.943019

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

ISENTROPIC CENTRIFUGAL COMPRESSOR  
OUTLET PRESSURE BAR 11.7000  
ISENTROPIC EFFICIENCY 0.72000  
MECHANICAL EFFICIENCY 1.00000

U-O-S BLOCK SECTION

BLOCK: UP-CP-02 MODEL: COMPR (CONTINUED)

\*\*\* RESULTS \*\*\*

INDICATED HORSEPOWER REQUIREMENT	KW	118.898
BRAKE HORSEPOWER REQUIREMENT	KW	118.898
NET WORK REQUIRED	KW	118.898
POWER LOSSES	KW	0.0
ISENTROPIC HORSEPOWER REQUIREMENT	KW	85.6064
CALCULATED OUTLET TEMP	C	236.217
ISENTROPIC TEMPERATURE	C	181.461
EFFICIENCY (POLYTR/ISENTR) USED		0.72000
OUTLET VAPOR FRACTION		1.00000
HEAD DEVELOPED,	M-KGF/KG	14,832.5
MECHANICAL EFFICIENCY USED		1.00000
INLET HEAT CAPACITY RATIO		1.40517
INLET VOLUMETRIC FLOW RATE ,	L/MIN	10,248.4
OUTLET VOLUMETRIC FLOW RATE,	L/MIN	4,435.97
INLET COMPRESSIBILITY FACTOR		0.99985
OUTLET COMPRESSIBILITY FACTOR		1.00506
AV. ISENT. VOL. EXPONENT		1.40440
AV. ISENT. TEMP EXPONENT		1.39724
AV. ACTUAL VOL. EXPONENT		1.59568
AV. ACTUAL TEMP EXPONENT		1.58583

BLOCK: UP-CP-03 MODEL: COMPR

-----

INLET STREAM: 7D  
 OUTLET STREAM: 8  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	73.1600	73.1600	0.00000
MASS (KG/HR )	2118.72	2118.72	0.00000
ENTHALPY (CAL/SEC )	1479.11	28087.9	-0.947340

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR



U-O-S BLOCK SECTION

BLOCK: UP-CP-03 MODEL: COMPR (CONTINUED)

\*\*\* INPUT DATA \*\*\*

ISENTROPIC CENTRIFUGAL COMPRESSOR		
OUTLET PRESSURE	BAR	40.0000
ISENTROPIC EFFICIENCY		0.72000
MECHANICAL EFFICIENCY		1.00000

\*\*\* RESULTS \*\*\*

INDICATED HORSEPOWER REQUIREMENT	KW	111.405
BRAKE HORSEPOWER REQUIREMENT	KW	111.405
NET WORK REQUIRED	KW	111.405
POWER LOSSES	KW	0.0
ISENTROPIC HORSEPOWER REQUIREMENT	KW	80.2120
CALCULATED OUTLET TEMP	C	222.905
ISENTROPIC TEMPERATURE	C	172.329
EFFICIENCY (POLYTR/ISENTR) USED		0.72000
OUTLET VAPOR FRACTION		1.00000
HEAD DEVELOPED,	M-KGF/KG	13,897.9
MECHANICAL EFFICIENCY USED		1.00000
INLET HEAT CAPACITY RATIO		1.41832
INLET VOLUMETRIC FLOW RATE ,	L/MIN	2,774.96
OUTLET VOLUMETRIC FLOW RATE,	L/MIN	1,279.26
INLET COMPRESSIBILITY FACTOR		0.99965
OUTLET COMPRESSIBILITY FACTOR		1.01751
AV. ISENT. VOL. EXPONENT		1.42616
AV. ISENT. TEMP EXPONENT		1.39972
AV. ACTUAL VOL. EXPONENT		1.62612
AV. ACTUAL TEMP EXPONENT		1.58976

BLOCK: UP-CP-04 MODEL: COMPR

-----  
INLET STREAM: 19  
OUTLET STREAM: 20  
PROPERTY OPTION SET: SRK

SOAVE-REDLICH-KWONG EQUATION OF STATE

U-O-S BLOCK SECTION

BLOCK: UP-CP-04 MODEL: COMPR (CONTINUED)

*** MASS AND ENERGY BALANCE ***			
	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	71.4222	71.4222	0.00000
MASS (KG/HR )	687.620	687.620	-
0.165334E-15			
ENTHALPY (CAL/SEC )	1372.66	1840.32	-0.254120

*** CO2 EQUIVALENT SUMMARY ***		
FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

ISENTROPIC CENTRIFUGAL COMPRESSOR	
OUTLET PRESSURE BAR	40.0000
ISENTROPIC EFFICIENCY	0.72000
MECHANICAL EFFICIENCY	1.00000

\*\*\* RESULTS \*\*\*

INDICATED HORSEPOWER REQUIREMENT KW	1.95801
BRAKE HORSEPOWER REQUIREMENT KW	1.95801
NET WORK REQUIRED KW	1.95801
POWER LOSSES KW	0.0
ISENTROPIC HORSEPOWER REQUIREMENT KW	1.40977
CALCULATED OUTLET TEMP C	38.3557
ISENTROPIC TEMPERATURE C	37.4150
EFFICIENCY (POLYTR/ISENTR) USED	0.72000
OUTLET VAPOR FRACTION	1.00000
HEAD DEVELOPED, M-KGF/KG	752.630
MECHANICAL EFFICIENCY USED	1.00000
INLET HEAT CAPACITY RATIO	1.41657
INLET VOLUMETRIC FLOW RATE , L/MIN	798.958
OUTLET VOLUMETRIC FLOW RATE, L/MIN	786.496
INLET COMPRESSIBILITY FACTOR	1.01989
OUTLET COMPRESSIBILITY FACTOR	1.02043
AV. ISENT. VOL. EXPONENT	1.44519
AV. ISENT. TEMP EXPONENT	1.40503
AV. ACTUAL VOL. EXPONENT	1.72261
AV. ACTUAL TEMP EXPONENT	1.66651

U-O-S BLOCK SECTION

BLOCK: UP-CP-04 MODEL: COMPR (CONTINUED)

BLOCK: UP-FH-01 MODEL: HEATER

-----  
 INLET STREAM: 8  
 OUTLET STREAM: 9  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*  
 IN OUT RELATIVE

DIFF.

TOTAL BALANCE			
MOLE (KMOL/HR )	73.1600	73.1600	0.00000
MASS (KG/HR )	2118.72	2118.72	0.00000
ENTHALPY (CAL/SEC )	28087.9	77585.2	-0.637974

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

ONE PHASE TP FLASH	SPECIFIED PHASE IS	VAPOR	
SPECIFIED TEMPERATURE	C		550.000
SPECIFIED PRESSURE	BAR		40.0000
MAXIMUM NO. ITERATIONS			30
CONVERGENCE TOLERANCE			

0.000100000

\*\*\* RESULTS \*\*\*

OUTLET TEMPERATURE	C	550.00
OUTLET PRESSURE	BAR	40.000
HEAT DUTY	CAL/SEC	49497.

U-O-S BLOCK SECTION

BLOCK: UP-HX-01 MODEL: HEATX

-----  
 HOT SIDE:  
 -----

INLET STREAM: 11  
 OUTLET STREAM: 15  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 COLD SIDE:  
 -----

INLET STREAM: 4  
 OUTLET STREAM: 5  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	1184.00	1184.00	0.00000
MASS (KG/HR )	18471.1	18471.1	0.00000
ENTHALPY (CAL/SEC )	-0.120156E+08	-0.120156E+08	-
0.155019E-15			

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR HOT SIDE:

TWO PHASE FLASH  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLASH SPECS FOR COLD SIDE:

TWO PHASE FLASH  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLOW DIRECTION AND SPECIFICATION:

COUNTERCURRENT HEAT EXCHANGER  
 SPECIFIED COLD OUTLET TEMP  
 SPECIFIED VALUE C 590.0000  
 LMTD CORRECTION FACTOR 1.00000

U-O-S BLOCK SECTION

BLOCK: UP-HX-01 MODEL: HEATX (CONTINUED)

PRESSURE SPECIFICATION:

HOT SIDE PRESSURE DROP	BAR	0.3447
COLD SIDE PRESSURE DROP	BAR	0.3447

HEAT TRANSFER COEFFICIENT SPECIFICATION:

HOT LIQUID	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD VAPOR	CAL/SEC-SQCM-K	0.0203

\*\*\* OVERALL RESULTS \*\*\*

STREAMS:

```

-----
11      -----> |                | -----> 15
T= 8.0000D+02 |                | T=
5.9845D+02 |                |
P= 3.9311D+01 |                | P=
3.8966D+01 |                |
V= 1.0000D+00 |                | V=
1.0000D+00 |                |

5      <----- |                | <----- 4
T= 5.9000D+02 |                | T=
3.8012D+02 |                |
P= 3.9655D+01 |                | P=
4.0000D+01 |                |
V= 1.0000D+00 |                | V=
1.0000D+00 |                |
-----
  
```

DUTY AND AREA:

CALCULATED HEAT DUTY	CAL/SEC	306825.9444
CALCULATED (REQUIRED) AREA	SQM	7.0577
ACTUAL EXCHANGER AREA	SQM	7.0577
PER CENT OVER-DESIGN		0.0000

HEAT TRANSFER COEFFICIENT:

AVERAGE COEFFICIENT (DIRTY)	CAL/SEC-SQCM-K	0.0203
UA (DIRTY)	CAL/SEC-K	1432.8402

LOG-MEAN TEMPERATURE DIFFERENCE:

LMTD CORRECTION FACTOR		1.0000
LMTD (CORRECTED)	C	214.1383
NUMBER OF SHELLS IN SERIES		1

PRESSURE DROP:

HOTSIDE, TOTAL	BAR	0.3447
COLD SIDE, TOTAL	BAR	0.3447

U-O-S BLOCK SECTION

BLOCK: UP-HX-01 MODEL: HEATX (CONTINUED)

\*\*\* ZONE RESULTS \*\*\*

TEMPERATURE LEAVING EACH ZONE:

HOT	
HOT IN	VAP
HOT OUT	
----->	
--->	
800.0	
598.5	
COLDOUT	VAP
COLDIN	
<-----	
----	
590.0	
380.1	
COLD	

ZONE HEAT TRANSFER AND AREA:

ZONE	HEAT DUTY	AREA	LMTD	AVERAGE U	UA
CAL/SEC-K	CAL/SEC	SQM	C	CAL/SEC-SQCM-K	
1	306825.944	7.0577	214.1383	0.0203	
1432.8402					

U-O-S BLOCK SECTION

HEATX COLD-TQCU UP-HX-01 TQCURV INLET

-----  
 PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: -0.3447 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

! DUTY	! PRES	! TEMP	! VFRAC	!
!	!	!	!	!
!	!	!	!	!
!	!	!	!	!
! CAL/SEC	! BAR	! C	!	!
!	!	!	!	!
! =====	! =====	! =====	! =====	! =====
! 0.0	! 40.0000	! 590.1092	! 1.0000	!
! 1.4611+04	! 40.0000	! 580.2449	! 1.0000	!
! 2.9222+04	! 40.0000	! 570.3627	! 1.0000	!
! 4.3832+04	! 40.0000	! 560.4629	! 1.0000	!
! 5.8443+04	! 40.0000	! 550.5461	! 1.0000	!
! -----	! -----	! -----	! -----	! -----
! 7.3054+04	! 40.0000	! 540.6128	! 1.0000	!
! 8.7665+04	! 40.0000	! 530.6636	! 1.0000	!
! 1.0228+05	! 40.0000	! 520.6992	! 1.0000	!
! 1.1689+05	! 40.0000	! 510.7202	! 1.0000	!
! 1.3150+05	! 40.0000	! 500.7274	! 1.0000	!
! -----	! -----	! -----	! -----	! -----
! 1.4611+05	! 40.0000	! 490.7216	! 1.0000	!
! 1.6072+05	! 40.0000	! 480.7038	! 1.0000	!
! 1.7533+05	! 40.0000	! 470.6749	! 1.0000	!
! 1.8994+05	! 40.0000	! 460.6359	! 1.0000	!
! 2.0455+05	! 40.0000	! 450.5880	! 1.0000	!
! -----	! -----	! -----	! -----	! -----
! 2.1916+05	! 40.0000	! 440.5325	! 1.0000	!
! 2.3377+05	! 40.0000	! 430.4705	! 1.0000	!
! 2.4838+05	! 40.0000	! 420.4037	! 1.0000	!
! 2.6299+05	! 40.0000	! 410.3336	! 1.0000	!
! 2.7760+05	! 40.0000	! 400.2619	! 1.0000	!
! -----	! -----	! -----	! -----	! -----
! 2.9222+05	! 40.0000	! 390.1904	! 1.0000	!
! 3.0683+05	! 40.0000	! 380.1211	! 1.0000	!



U-O-S BLOCK SECTION

HEATX HOT-TQCUR UP-HX-01 TQCURV INLET

-----  
 PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: 0.0 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

! DUTY	! PRES	! TEMP	! VFRAC	!
! CAL/SEC	! BAR	! C	!	!
! 0.0	! 39.3105	! 800.0000	! 1.0000	!
! 1.4611+04	! 39.3105	! 790.6004	! 1.0000	!
! 2.9222+04	! 39.3105	! 781.1815	! 1.0000	!
! 4.3832+04	! 39.3105	! 771.7432	! 1.0000	!
! 5.8443+04	! 39.3105	! 762.2854	! 1.0000	!
! 7.3054+04	! 39.3105	! 752.8081	! 1.0000	!
! 8.7665+04	! 39.3105	! 743.3111	! 1.0000	!
! 1.0228+05	! 39.3105	! 733.7945	! 1.0000	!
! 1.1689+05	! 39.3105	! 724.2582	! 1.0000	!
! 1.3150+05	! 39.3105	! 714.7021	! 1.0000	!
! 1.4611+05	! 39.3105	! 705.1263	! 1.0000	!
! 1.6072+05	! 39.3105	! 695.5307	! 1.0000	!
! 1.7533+05	! 39.3105	! 685.9153	! 1.0000	!
! 1.8994+05	! 39.3105	! 676.2801	! 1.0000	!
! 2.0455+05	! 39.3105	! 666.6253	! 1.0000	!
! 2.1916+05	! 39.3105	! 656.9507	! 1.0000	!
! 2.3377+05	! 39.3105	! 647.2565	! 1.0000	!
! 2.4838+05	! 39.3105	! 637.5427	! 1.0000	!
! 2.6299+05	! 39.3105	! 627.8094	! 1.0000	!
! 2.7760+05	! 39.3105	! 618.0567	! 1.0000	!
! 2.9222+05	! 39.3105	! 608.2848	! 1.0000	!
! 3.0683+05	! 39.3105	! 598.4937	! 1.0000	!

U-O-S BLOCK SECTION

BLOCK: UP-HX-02 MODEL: HEATX

-----  
 HOT SIDE:  
 -----

INLET STREAM: 12  
 OUTLET STREAM: 13  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 COLD SIDE:  
 -----

INLET STREAM: 5  
 OUTLET STREAM: 6  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

DIFF.	IN	OUT	RELATIVE
TOTAL BALANCE			
MOLE (KMOL/HR )	648.722	648.722	0.00000
MASS (KG/HR )	12284.8	12284.8	0.00000
ENTHALPY (CAL/SEC )	-0.701648E+07	-0.701648E+07	0.00000

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR HOT SIDE:

TWO PHASE FLASH  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLASH SPECS FOR COLD SIDE:

TWO PHASE FLASH  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLOW DIRECTION AND SPECIFICATION:

COUNTERCURRENT HEAT EXCHANGER  
 SPECIFIED COLD OUTLET TEMP  
 SPECIFIED VALUE C 610.0000  
 LMTD CORRECTION FACTOR 1.00000

U-O-S BLOCK SECTION

BLOCK: UP-HX-02 MODEL: HEATX (CONTINUED)

PRESSURE SPECIFICATION:

HOT SIDE PRESSURE DROP	BAR	0.3447
COLD SIDE PRESSURE DROP	BAR	0.3447

HEAT TRANSFER COEFFICIENT SPECIFICATION:

HOT LIQUID	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD VAPOR	CAL/SEC-SQCM-K	0.0203

\*\*\* OVERALL RESULTS \*\*\*

STREAMS:

```

-----
12      -----> |                | |-----> 13
T= 8.0000D+02 |                | |      T=
6.4962D+02    |                | |
P= 3.9311D+01 |                | |      P=
3.8966D+01    |                | |
V= 1.0000D+00 |                | |      V=
1.0000D+00    |                | |

6      <----- |                | |<----- 5
T= 6.1000D+02 |                | |      T=
5.9000D+02    |                | |
P= 3.9311D+01 |                | |      P=
3.9655D+01    |                | |
V= 1.0000D+00 |                | |      V=
1.0000D+00    |                | |
-----
    
```

DUTY AND AREA:

CALCULATED HEAT DUTY	CAL/SEC	29852.2398
CALCULATED (REQUIRED) AREA	SQM	1.3071
ACTUAL EXCHANGER AREA	SQM	1.3071
PER CENT OVER-DESIGN		0.0000

HEAT TRANSFER COEFFICIENT:

AVERAGE COEFFICIENT (DIRTY)	CAL/SEC-SQCM-K	0.0203
UA (DIRTY)	CAL/SEC-K	265.3710

LOG-MEAN TEMPERATURE DIFFERENCE:

LMTD CORRECTION FACTOR		1.0000
LMTD (CORRECTED)	C	112.4925
NUMBER OF SHELLS IN SERIES		1

PRESSURE DROP:

HOTSIDE, TOTAL	BAR	0.3447
COLD SIDE, TOTAL	BAR	0.3447

U-O-S BLOCK SECTION

BLOCK: UP-HX-02 MODEL: HEATX (CONTINUED)

\*\*\* ZONE RESULTS \*\*\*

TEMPERATURE LEAVING EACH ZONE:

HOT	
HOT IN	VAP
HOT OUT	
----->	
--->	
800.0	
649.6	
COLDOUT	VAP
COLDIN	
<-----	
----	
610.0	
590.0	
COLD	

ZONE HEAT TRANSFER AND AREA:

ZONE	HEAT DUTY	AREA	LMTD	AVERAGE U	UA
CAL/SEC-K	CAL/SEC	SQM	C	CAL/SEC-SQCM-K	
1	29852.240	1.3071	112.4925	0.0203	
265.3710					

U-O-S BLOCK SECTION

HEATX COLD-TQCU UP-HX-02 TQCURV INLET

-----  
 PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: -0.3447 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

! DUTY	! PRES	! TEMP	! VFRAC	!
!	!	!	!	!
!	!	!	!	!
! CAL/SEC	! BAR	! C	!	!
!	!	!	!	!
! =====	! =====	! =====	! =====	! =====
! 0.0	! 39.6553	! 610.1030	! 1.0000	!
! 1421.5352	! 39.6553	! 609.1475	! 1.0000	!
! 2843.0705	! 39.6553	! 608.1919	! 1.0000	!
! 4264.6057	! 39.6553	! 607.2360	! 1.0000	!
! 5686.1409	! 39.6553	! 606.2800	! 1.0000	!
! -----	! -----	! -----	! -----	! -----
! 7107.6761	! 39.6553	! 605.3238	! 1.0000	!
! 8529.2114	! 39.6553	! 604.3674	! 1.0000	!
! 9950.7466	! 39.6553	! 603.4108	! 1.0000	!
! 1.1372+04	! 39.6553	! 602.4540	! 1.0000	!
! 1.2794+04	! 39.6553	! 601.4971	! 1.0000	!
! -----	! -----	! -----	! -----	! -----
! 1.4215+04	! 39.6553	! 600.5400	! 1.0000	!
! 1.5637+04	! 39.6553	! 599.5827	! 1.0000	!
! 1.7058+04	! 39.6553	! 598.6252	! 1.0000	!
! 1.8480+04	! 39.6553	! 597.6676	! 1.0000	!
! 1.9901+04	! 39.6553	! 596.7097	! 1.0000	!
! -----	! -----	! -----	! -----	! -----
! 2.1323+04	! 39.6553	! 595.7517	! 1.0000	!
! 2.2745+04	! 39.6553	! 594.7936	! 1.0000	!
! 2.4166+04	! 39.6553	! 593.8352	! 1.0000	!
! 2.5588+04	! 39.6553	! 592.8767	! 1.0000	!
! 2.7009+04	! 39.6553	! 591.9180	! 1.0000	!
! -----	! -----	! -----	! -----	! -----
! 2.8431+04	! 39.6553	! 590.9591	! 1.0000	!
! 2.9852+04	! 39.6553	! 590.0000	! 1.0000	!

U-O-S BLOCK SECTION

HEATX HOT-TQCUR UP-HX-02 TQCURV INLET

-----  
 PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: 0.0 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

! DUTY	! PRES	! TEMP	! VFRAC	!
! CAL/SEC	! BAR	! C	!	!
! 0.0	! 39.3105	! 800.0000	! 1.0000	!
! 1421.5352	! 39.3105	! 792.9010	! 1.0000	!
! 2843.0705	! 39.3105	! 785.7962	! 1.0000	!
! 4264.6057	! 39.3105	! 778.6856	! 1.0000	!
! 5686.1409	! 39.3105	! 771.5692	! 1.0000	!
! 7107.6761	! 39.3105	! 764.4468	! 1.0000	!
! 8529.2114	! 39.3105	! 757.3183	! 1.0000	!
! 9950.7466	! 39.3105	! 750.1838	! 1.0000	!
! 1.1372+04	! 39.3105	! 743.0430	! 1.0000	!
! 1.2794+04	! 39.3105	! 735.8960	! 1.0000	!
! 1.4215+04	! 39.3105	! 728.7426	! 1.0000	!
! 1.5637+04	! 39.3105	! 721.5827	! 1.0000	!
! 1.7058+04	! 39.3105	! 714.4163	! 1.0000	!
! 1.8480+04	! 39.3105	! 707.2433	! 1.0000	!
! 1.9901+04	! 39.3105	! 700.0635	! 1.0000	!
! 2.1323+04	! 39.3105	! 692.8769	! 1.0000	!
! 2.2745+04	! 39.3105	! 685.6834	! 1.0000	!
! 2.4166+04	! 39.3105	! 678.4829	! 1.0000	!
! 2.5588+04	! 39.3105	! 671.2753	! 1.0000	!
! 2.7009+04	! 39.3105	! 664.0604	! 1.0000	!
! 2.8431+04	! 39.3105	! 656.8382	! 1.0000	!
! 2.9852+04	! 39.3105	! 649.6086	! 1.0000	!

BLOCK: UP-MX-01 MODEL: MIXER

-----  
 INLET STREAMS: 3 20  
 OUTLET STREAM: 4  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

DIFF.

IN

OUT

RELATIVE



U-O-S BLOCK SECTION

BLOCK: UP-MX-01 MODEL: MIXER (CONTINUED)

TOTAL BALANCE  
 MOLE (KMOL/HR ) 563.122 563.122 0.00000  
 MASS (KG/HR ) 9545.73 9545.73 -  
 0.190555E-15  
 ENTHALPY (CAL/SEC ) -0.746717E+07 -0.746717E+07  
 0.124722E-15

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E 0.00000 KG/HR  
 PRODUCT STREAMS CO2E 0.00000 KG/HR  
 NET STREAMS CO2E PRODUCTION 0.00000 KG/HR  
 UTILITIES CO2E PRODUCTION 0.00000 KG/HR  
 TOTAL CO2E PRODUCTION 0.00000 KG/HR

\*\*\* INPUT DATA \*\*\*

ONE PHASE FLASH SPECIFIED PHASE IS VAPOR  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000  
 OUTLET PRESSURE BAR 40.0000

BLOCK: UP-MX-02 MODEL: MIXER

-----

INLET STREAMS: 6 9  
 OUTLET STREAM: 10A  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

DIFF.  
 TOTAL BALANCE  
 MOLE (KMOL/HR ) 636.282 636.282 0.00000  
 MASS (KG/HR ) 11664.4 11664.4  
 0.311886E-15  
 ENTHALPY (CAL/SEC ) -0.705290E+07 -0.705290E+07 -  
 0.132048E-15

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E 0.00000 KG/HR  
 PRODUCT STREAMS CO2E 0.00000 KG/HR  
 NET STREAMS CO2E PRODUCTION 0.00000 KG/HR  
 UTILITIES CO2E PRODUCTION 0.00000 KG/HR  
 TOTAL CO2E PRODUCTION 0.00000 KG/HR

\*\*\* INPUT DATA \*\*\*

TWO PHASE FLASH  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000  
 OUTLET PRESSURE: MINIMUM OF INLET STREAM PRESSURES

U-O-S BLOCK SECTION

BLOCK: UP-MX-03 MODEL: RSTOIC

-----  
 INLET STREAM: 10A  
 OUTLET STREAM: 10B  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	GENERATION	RELATIVE
DIFF.				
TOTAL BALANCE				
MOLE (KMOL/HR )	636.282	620.882	-15.4000	
0.00000				
MASS (KG/HR )	11664.4	11664.4		
0.00000				
ENTHALPY (CAL/SEC )	-0.705290E+07	-0.723256E+07		
0.248403E-01				

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*  
 STOICHIOMETRY MATRIX:

REACTION # 1:  
 SUBSTREAM MIXED :  
 WATER 1.00 HYDROGEN -1.00 OXYGEN -0.500

REACTION EXTENT SPECS: NUMBER= 1  
 REACTION # 1: EXTENT= 30.80 KMOL/HR

ONE PHASE TP FLASH SPECIFIED PHASE IS VAPOR  
 SPECIFIED TEMPERATURE C 800.000  
 SPECIFIED PRESSURE BAR 39.3105  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000  
 SIMULTANEOUS REACTIONS  
 GENERATE COMBUSTION REACTIONS FOR FEED SPECIES NO

\*\*\* RESULTS \*\*\*  
 OUTLET TEMPERATURE C 800.00  
 OUTLET PRESSURE BAR 39.311

HEAT DUTY

CAL/SEC

-0.17966E+06

U-O-S BLOCK SECTION

BLOCK: UP-PM-01 MODEL: PUMP

-----  
 INLET STREAM: 1  
 OUTLET STREAM: 2  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*  
 IN OUT RELATIVE

DIFF.

TOTAL BALANCE  
 MOLE (KMOL/HR ) 491.700 491.700 0.00000  
 MASS (KG/HR ) 8858.11 8858.11 0.00000  
 ENTHALPY (CAL/SEC ) -0.942335E+07 -0.941751E+07 -

0.619183E-03

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E 0.00000 KG/HR  
 PRODUCT STREAMS CO2E 0.00000 KG/HR  
 NET STREAMS CO2E PRODUCTION 0.00000 KG/HR  
 UTILITIES CO2E PRODUCTION 0.00000 KG/HR  
 TOTAL CO2E PRODUCTION 0.00000 KG/HR

\*\*\* INPUT DATA \*\*\*

OUTLET PRESSURE BAR 40.0000  
 DRIVER EFFICIENCY 1.00000

FLASH SPECIFICATIONS:

LIQUID PHASE CALCULATION  
 NO FLASH PERFORMED  
 MAXIMUM NUMBER OF ITERATIONS 30  
 TOLERANCE 0.000100000

\*\*\* RESULTS \*\*\*

VOLUMETRIC FLOW RATE L/MIN 153.615  
 PRESSURE CHANGE BAR 39.0000  
 NPSH AVAILABLE M-KGF/KG 10.3610  
 FLUID POWER KW 9.98495  
 BRAKE POWER KW 24.4291  
 ELECTRICITY KW 24.4291  
 PUMP EFFICIENCY USED 0.40873  
 NET WORK REQUIRED KW 24.4291  
 HEAD DEVELOPED M-KGF/KG 413.796

BLOCK: UP-SE-01 MODEL: SEP

-----  
 INLET STREAM: 16  
 OUTLET STREAMS: 17  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

U-O-S BLOCK SECTION

BLOCK: UP-SE-01 MODEL: SEP (CONTINUED)

\*\*\*\*\*  
 \*  
 \*  
 \* SUM OF SPLITS SPECIFIED IS ILLEGAL  
 \*  
 \*  
 \*  
 \*\*\*\*\*

*** MASS AND ENERGY BALANCE ***			
DIFF.	IN	OUT	RELATIVE
TOTAL BALANCE			
MOLE (KMOL/HR )	620.882	620.882	
0.577485E-06			
MASS (KG/HR )	8925.35	8925.35	
0.990596E-07			
ENTHALPY (CAL/SEC )	-0.670452E+07	-0.670542E+07	
0.134095E-03			

*** CO2 EQUIVALENT SUMMARY ***		
FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR STREAM 18  
 ONE PHASE TP FLASH SPECIFIED PHASE IS VAPOR  
 SPECIFIED PRESSURE BAR 38.9313  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLASH SPECS FOR STREAM 17  
 ONE PHASE TP FLASH SPECIFIED PHASE IS LIQUID  
 PRESSURE DROP BAR 0.0  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

U-O-S BLOCK SECTION

BLOCK: UP-SE-01 MODEL: SEP (CONTINUED)

MOLE-FLOW (KMOL/HR )

SUBSTREAM= MIXED

STREAM= 18

CPT= WATER	FLOW=	0.0
HYDROGEN		232.800
NITROGEN		77.6000
OXYGEN		0.0
ARGON		0.90000

\*\*\* RESULTS \*\*\*

HEAT DUTY	CAL/SEC	-899.15
-----------	---------	---------

COMPONENT = WATER

STREAM	SUBSTREAM	SPLIT FRACTION
17	MIXED	1.00000

COMPONENT = HYDROGEN

STREAM	SUBSTREAM	SPLIT FRACTION
18	MIXED	1.00000

COMPONENT = NITROGEN

STREAM	SUBSTREAM	SPLIT FRACTION
18	MIXED	0.99918
17	MIXED	0.00082406

COMPONENT = ARGON

STREAM	SUBSTREAM	SPLIT FRACTION
18	MIXED	1.00000

BLOCK: UP-SP-01 MODEL: FSPLIT

-----  
 INLET STREAM: 18  
 OUTLET STREAMS: 19 21  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*  
 IN OUT

DIFF.

TOTAL BALANCE			RELATIVE
MOLE (KMOL/HR )	269.518	269.518	0.00000
MASS (KG/HR )	2594.79	2594.79	0.00000
ENTHALPY (CAL/SEC )	5179.84	5179.84	0.00000

U-O-S BLOCK SECTION

BLOCK: UP-SP-01 MODEL: FSPLIT (CONTINUED)

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

FRACTION OF FLOW	STRM=19	FRAC=	0.26500
------------------	---------	-------	---------

\*\*\* RESULTS \*\*\*

STREAM= 19	SPLIT=	0.26500	KEY= 0	STREAM-
ORDER= 1				
21		0.73500	0	
2				

STREAM SECTION

1 10A 10B 11 12  
 -----

STREAM ID	1	10A	10B	11	12
FROM :	----	UP-MX-02	UP-MX-03	SOEC2	
SOEC2					
TO :	UP-PM-01	UP-MX-03	SOEC	UP-HX-01	UP-
HX-02					
SUBSTREAM: MIXED					
PHASE:	LIQUID	VAPOR	VAPOR	VAPOR	
VAPOR					
COMPONENTS: KMOL/HR					
WATER	491.7000	491.7000	522.5000	351.3000	0.0
HYDROGEN	0.0	50.6203	19.8203	191.0203	0.0
NITROGEN	0.0	77.6640	77.6640	77.6640	0.0
OXYGEN	0.0	15.4000	0.0	0.0	
85.6000					
ARGON	0.0	0.8980	0.8980	0.8980	0.0
TOTAL FLOW:					
KMOL/HR	491.7000	636.2822	620.8822	620.8822	
85.6000					
KG/HR	8858.1132	1.1664+04	1.1664+04	8925.3523	
2739.0973					
L/MIN	153.6146	1.9539+04	2.3484+04	2.3589+04	
3269.1917					
STATE VARIABLES:					
TEMP C	25.0000	603.3524	800.0000	800.0000	
800.0000					
PRES BAR	1.0000	39.3105	39.3105	39.3105	
39.3105					
VFRAC	0.0	1.0000	1.0000	1.0000	
1.0000					
LFRAC	1.0000	0.0	0.0	0.0	0.0
SFRAC	0.0	0.0	0.0	0.0	0.0
ENTHALPY:					
CAL/MOL	-6.8993+04	-3.9904+04	-4.1936+04	-2.6373+04	
6050.0777					
CAL/GM	-3829.7161	-2176.7382	-2232.1863	-1834.5980	
189.0720					
CAL/SEC	-9.4233+06	-7.0529+06	-7.2326+06	-4.5485+06	
1.4386+05					
ENTROPY:					
CAL/MOL-K	-38.9834	-5.1890	-4.3373	-1.1313	
2.4981					
CAL/GM-K	-2.1639	-0.2831	-0.2309	-7.8699-02	
7.8067-02					
DENSITY:					



MOL/CC	5.3348-02	5.4275-04	4.4064-04	4.3868-04
4.3640-04				
GM/CC	0.9611	9.9499-03	8.2783-03	6.3062-03
1.3964-02				
AVG MW	18.0153	18.3322	18.7869	14.3753
31.9988				

STREAM SECTION

	13	14	15	16	17
STREAM ID	13	14	15	16	17
FROM :	UP-HX-02	UP-CO-03	UP-HX-01	UP-CD-01	UP-
SE-01					
TO :	UP-CO-03	----	UP-CD-01	UP-SE-01	----
CONV. MAX. REL. ERR:	0.0	0.0	4.7370-06	0.0	0.0
SUBSTREAM: MIXED					
PHASE:	VAPOR	VAPOR	VAPOR	MIXED	
LIQUID					
COMPONENTS: KMOL/HR					
WATER	0.0	0.0	351.3000	351.3000	
351.3000					
HYDROGEN	0.0	0.0	191.0203	191.0203	0.0
NITROGEN	0.0	0.0	77.6640	77.6640	
6.4000-02					
OXYGEN	85.6000	85.6000	0.0	0.0	0.0
ARGON	0.0	0.0	0.8980	0.8980	0.0
TOTAL FLOW:					
KMOL/HR	85.6000	85.6000	620.8822	620.8822	
351.3640					
KG/HR	2739.0973	2739.0973	8925.3523	8925.3523	
6330.5607					
L/MIN	2838.9851	924.6971	1.9265+04	3129.5856	
110.7025					
STATE VARIABLES:					
TEMP C	649.6228	35.0000	598.4517	35.0000	
35.0000					
PRES BAR	38.9658	38.9313	38.9658	38.9313	
38.9313					
VFRAC	1.0000	1.0000	1.0000	0.4347	0.0
LFRAC	0.0	0.0	0.0	0.5653	
1.0000					
SFRAC	0.0	0.0	0.0	0.0	0.0
ENTHALPY:					
CAL/MOL	4794.6097	0.3049	-2.8152+04	-3.8874+04	-
6.8755+04					
CAL/GM	149.8372	9.5286-03	-1958.3548	-2704.2386	-
3816.1179					
CAL/SEC	1.1401+05	7.2499	-4.8553+06	-6.7045+06	-
6.7106+06					
ENTROPY:					
CAL/MOL-K	1.2556	-7.2082	-2.9486	-24.2343	-
38.3942					
CAL/GM-K	3.9239-02	-0.2253	-0.2051	-1.6858	-
2.1310					

DENSITY:				
MOL/CC	5.0253-04	1.5428-03	5.3715-04	3.3065-03
5.2899-02				
GM/CC	1.6080-02	4.9369-02	7.7216-03	4.7532-02
0.9531				
AVG MW	31.9988	31.9988	14.3753	14.3753
18.0171				

STREAM SECTION

	18	19	2	20	21
18 19 2 20 21 -----					
STREAM ID	18	19	2	20	21
FROM :	UP-SE-01	UP-SP-01	UP-PM-01	UP-CP-04	UP-
SP-01					
TO :	UP-SP-01	UP-CP-04	UP-BO-01	UP-MX-01	----
SUBSTREAM: MIXED					
PHASE:	VAPOR	VAPOR	LIQUID	VAPOR	
VAPOR					
COMPONENTS: KMOL/HR					
WATER	0.0	0.0	491.7000	0.0	0.0
HYDROGEN	191.0199	50.6203	0.0	50.6203	
140.3996					
NITROGEN	77.6000	20.5640	0.0	20.5640	
57.0360					
OXYGEN	0.0	0.0	0.0	0.0	0.0
ARGON	0.8980	0.2380	0.0	0.2380	
0.6600					
TOTAL FLOW:					
KMOL/HR	269.5179	71.4222	491.7000	71.4222	
198.0956					
KG/HR	2594.7907	687.6195	8858.1132	687.6195	
1907.1712					
L/MIN	3014.9374	798.9584	153.6654	786.4963	
2215.9790					
STATE VARIABLES:					
TEMP C	35.0000	35.0000	26.2138	38.3557	
35.0000					
PRES BAR	38.9313	38.9313	40.0000	40.0000	
38.9313					
VFRAC	1.0000	1.0000	0.0	1.0000	
1.0000					
LFRAC	0.0	0.0	1.0000	0.0	0.0
SFRAC	0.0	0.0	0.0	0.0	0.0
ENTHALPY:					
CAL/MOL	69.1881	69.1881	-6.8951+04	92.7604	
69.1881					
CAL/GM	7.1865	7.1865	-3827.3448	9.6349	
7.1865					
CAL/SEC	5179.8437	1372.6586	-9.4175+06	1840.3216	
3807.1851					
ENTROPY:					
CAL/MOL-K	-5.8222	-5.8222	-38.9164	-5.8010	-
5.8222					
CAL/GM-K	-0.6047	-0.6047	-2.1602	-0.6025	-
0.6047					
DENSITY:					

MOL/CC	1.4899-03	1.4899-03	5.3330-02	1.5135-03
1.4899-03				
GM/CC	1.4344-02	1.4344-02	0.9608	1.4571-02
1.4344-02				
AVG MW	9.6275	9.6275	18.0153	9.6275
9.6275				

STREAM SECTION

	3	4	5	6	7
3 4 5 6 7 -----					
STREAM ID	3	4	5	6	7
FROM :	UP-BO-01	UP-MX-01	UP-HX-01	UP-HX-02	----
TO :	UP-MX-01	UP-HX-01	UP-HX-02	UP-MX-02	UP-
CP-01					
SUBSTREAM: MIXED					
PHASE:	VAPOR	VAPOR	VAPOR	VAPOR	
VAPOR					
COMPONENTS: KMOL/HR					
WATER	491.7000	491.7000	491.7000	491.7000	0.0
HYDROGEN	0.0	50.6203	50.6203	50.6203	0.0
NITROGEN	0.0	20.5640	20.5640	20.5640	
57.1000					
OXYGEN	0.0	0.0	0.0	0.0	
15.4000					
ARGON	0.0	0.2380	0.2380	0.2380	
0.6600					
TOTAL FLOW:					
KMOL/HR	491.7000	563.1222	563.1222	563.1222	
73.1600					
KG/HR	8858.1132	9545.7327	9545.7327	9545.7327	
2118.7169					
L/MIN	1.1223+04	1.2184+04	1.6781+04	1.7349+04	
3.0222+04					
STATE VARIABLES:					
TEMP C	420.0000	380.1211	590.0000	610.0000	
25.0000					
PRES BAR	40.0000	40.0000	39.6553	39.3105	
1.0000					
VFRAC	1.0000	1.0000	1.0000	1.0000	
1.0000					
LFRAC	0.0	0.0	0.0	0.0	0.0
SFRAC	0.0	0.0	0.0	0.0	0.0
ENTHALPY:					
CAL/MOL	-5.4685+04	-4.7737+04	-4.5776+04	-4.5585+04	-
1.5891					
CAL/GM	-3035.4576	-2816.1067	-2700.3928	-2689.1346	-
5.4873-02					
CAL/SEC	-7.4690+06	-7.4672+06	-7.1603+06	-7.1305+06	-
32.2948					
ENTROPY:					
CAL/MOL-K	-11.1286	-9.5045	-6.8853	-6.6495	
1.1410					
CAL/GM-K	-0.6177	-0.5607	-0.4062	-0.3923	
3.9399-02					
DENSITY:					

MOL/CC	7.3021-04	7.7029-04	5.5928-04	5.4097-04
4.0347-05				
GM/CC	1.3155-02	1.3058-02	9.4805-03	9.1703-03
1.1684-03				
AVG MW	18.0153	16.9514	16.9514	16.9514
28.9600				

STREAM SECTION

	7A	7B	7C	7D	8
7A 7B 7C 7D 8 -----					
STREAM ID	7A	7B	7C	7D	8
FROM :	UP-CP-01	UP-CO-01	UP-CP-02	UP-CO-02	UP-
CP-03					
TO :	UP-CO-01	UP-CP-02	UP-CO-02	UP-CP-03	UP-
FH-01					
SUBSTREAM: MIXED					
PHASE:	VAPOR	VAPOR	VAPOR	VAPOR	
VAPOR					
COMPONENTS: KMOL/HR					
WATER	0.0	0.0	0.0	0.0	0.0
HYDROGEN	0.0	0.0	0.0	0.0	0.0
NITROGEN	57.1000	57.1000	57.1000	57.1000	
57.1000					
OXYGEN	15.4000	15.4000	15.4000	15.4000	
15.4000					
ARGON	0.6600	0.6600	0.6600	0.6600	
0.6600					
TOTAL FLOW:					
KMOL/HR	73.1600	73.1600	73.1600	73.1600	
73.1600					
KG/HR	2118.7169	2118.7169	2118.7169	2118.7169	
2118.7169					
L/MIN	1.3983+04	1.0248+04	4435.9706	2774.9582	
1279.2606					
STATE VARIABLES:					
TEMP C	197.9118	37.7778	236.2172	37.7778	
222.9051					
PRES BAR	3.4200	3.0753	11.7000	11.3553	
40.0000					
VFRAC	1.0000	1.0000	1.0000	1.0000	
1.0000					
LFRAC	0.0	0.0	0.0	0.0	0.0
SFRAC	0.0	0.0	0.0	0.0	0.0
ENTHALPY:					
CAL/MOL	1210.0985	84.4361	1481.8340	72.7828	
1382.1251					
CAL/GM	41.7851	2.9156	51.1682	2.5132	
47.7252					
CAL/SEC	2.4592+04	1715.9285	3.0114+04	1479.1084	
2.8088+04					
ENTROPY:					
CAL/MOL-K	1.9005	-0.8070	5.6172-03	-3.4379	-
2.6584					
CAL/GM-K	6.5626-02	-2.7865-02	1.9396-04	-0.1187	-
9.1795-02					



DENSITY:				
MOL/CC	8.7198-05	1.1898-04	2.7487-04	4.3941-04
9.5315-04				
GM/CC	2.5253-03	3.4456-03	7.9604-03	1.2725-02
2.7603-02				
AVG MW	28.9600	28.9600	28.9600	28.9600
28.9600				

STREAM SECTION

9 CW1 CW2 CW3 CW4  
 -----

STREAM ID	9	CW1	CW2	CW3	CW4
FROM :	UP-FH-01	----	UP-CO-01	UP-CO-02	----
TO :	UP-MX-02	UP-CO-01	UP-CO-02	----	UP-
CO-03					
SUBSTREAM: MIXED					
PHASE:	VAPOR	LIQUID	LIQUID	LIQUID	
LIQUID					
COMPONENTS: KMOL/HR					
WATER	0.0	403.0176	403.0176	403.0176	
889.6555					
HYDROGEN	0.0	0.0	0.0	0.0	0.0
NITROGEN	57.1000	0.0	0.0	0.0	0.0
OXYGEN	15.4000	0.0	0.0	0.0	0.0
ARGON	0.6600	0.0	0.0	0.0	0.0
TOTAL FLOW:					
KMOL/HR	73.1600	403.0176	403.0176	403.0176	
889.6555					
KG/HR	2118.7169	7260.4752	7260.4752	7260.4752	
1.6027+04					
L/MIN	2116.7436	126.0963	127.2374	128.7475	
273.7279					
STATE VARIABLES:					
TEMP C	550.0000	26.6667	36.5319	48.8889	
7.2222					
PRES BAR	40.0000	1.0000	1.0000	1.0000	
1.0000					
VFRAC	1.0000	0.0	0.0	0.0	0.0
LFRAC	0.0	1.0000	1.0000	1.0000	
1.0000					
SFRAC	0.0	0.0	0.0	0.0	0.0
ENTHALPY:					
CAL/MOL	3817.7504	-6.8959+04	-6.8755+04	-6.8499+04	-
6.9363+04					
CAL/GM	131.8282	-3827.7985	-3816.4558	-3802.2575	-
3850.2092					
CAL/SEC	7.7585+04	-7.7199+06	-7.6970+06	-7.6684+06	-
1.7141+07					
ENTROPY:					
CAL/MOL-K	1.1037	-38.8832	-38.3020	-37.5995	-
40.0894					
CAL/GM-K	3.8112-02	-2.1583	-2.1261	-2.0871	-
2.2253					
DENSITY:					
MOL/CC	5.7604-04	5.3269-02	5.2791-02	5.2172-02	
5.4169-02					

GM/CC	1.6682-02	0.9596	0.9510	0.9399
0.9759				
AVG MW	28.9600	18.0153	18.0153	18.0153
18.0153				

STREAM SECTION

CW5 CW6 CW7 SOEC1  
 -----

STREAM ID	CW5	CW6	CW7	SOEC1
FROM :	UP-CO-03	----	UP-CD-01	SOEC
TO :	----	UP-CD-01	----	SOEC2
SUBSTREAM: MIXED				
PHASE:	LIQUID	LIQUID	LIQUID	VAPOR
COMPONENTS: KMOL/HR				
WATER	889.6555	6392.4052	6392.4052	351.3000
HYDROGEN	0.0	0.0	0.0	191.0203
NITROGEN	0.0	0.0	0.0	77.6640
OXYGEN	0.0	0.0	0.0	85.6000
ARGON	0.0	0.0	0.0	0.8980
TOTAL FLOW:				
KMOL/HR	889.6555	6392.4052	6392.4052	706.4822
KG/HR	1.6027+04	1.1516+05	1.1516+05	1.1664+04
L/MIN	279.0528	1928.2758	2010.1432	2.6866+04
STATE VARIABLES:				
TEMP C	29.4444	-17.7778	32.2222	800.0000
PRES BAR	1.0000	1.0000	1.0000	39.3105
VFRAC	0.0	0.0	0.0	1.0000
LFRAC	1.0000	1.0000	1.0000	0.0
SFRAC	0.0	0.0	0.0	0.0
ENTHALPY:				
CAL/MOL	-6.8901+04	-6.9885+04	-6.8844+04	-2.2443+04
CAL/GM	-3824.6035	-3879.2179	-3821.4095	-1359.2898
CAL/SEC	-1.7027+07	-1.2409+08	-1.2224+08	-4.4043+06
ENTROPY:				
CAL/MOL-K	-38.7176	-41.7323	-38.5536	4.2610-02
CAL/GM-K	-2.1492	-2.3165	-2.1400	2.5808-03
DENSITY:				
MOL/CC	5.3135-02	5.5251-02	5.3001-02	4.3827-04
GM/CC	0.9572	0.9954	0.9548	7.2361-03
AVG MW	18.0153	18.0153	18.0153	16.5106

PROBLEM STATUS SECTION

BLOCK STATUS

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```
*****
***
*
*
* Calculations were completed with warnings
*
*
* The following Unit Operation blocks were
*
* completed with warnings:
*
*   UP-SE-01
*
*
* All streams were flashed normally
*
*
* All Convergence blocks were completed normally
*
*
*****
***
```

# B.1.4 SOEC Block Summary

BLOCK: SOEC MODEL: RSTOIC

-----  
 INLET STREAM: 10B  
 OUTLET STREAM: SOEC1  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	GENERATION	RELATIVE
DIFF.				
TOTAL BALANCE				
MOLE (KMOL/HR )	620.882	706.482	85.6000	
0.00000				
MASS (KG/HR )	11664.4	11664.4		
0.00000				
ENTHALPY (CAL/SEC )	-0.723256E+07	-0.440427E+07		-
0.391050				

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*  
 STOICHIOMETRY MATRIX:

REACTION # 1:  
 SUBSTREAM MIXED :  
 WATER -1.00 HYDROGEN 1.00 OXYGEN 0.500

REACTION EXTENT SPECS: NUMBER= 1  
 REACTION # 1: EXTENT= 171.2 KMOL/HR

TWO PHASE TP FLASH  
 SPECIFIED TEMPERATURE C 800.000  
 SPECIFIED PRESSURE BAR 39.3105  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000  
 SIMULTANEOUS REACTIONS  
 GENERATE COMBUSTION REACTIONS FOR FEED SPECIES NO

\*\*\* RESULTS \*\*\*  
 OUTLET TEMPERATURE C 800.00  
 OUTLET PRESSURE BAR 39.311  
 HEAT DUTY CAL/SEC 0.28283E+07  
 VAPOR FRACTION 1.0000

V-L PHASE EQUILIBRIUM :

	COMP	F(I)	X(I)	Y(I)	K(I)
	WATER	0.49725	0.49725	0.49725	
MISSING					
	HYDROGEN	0.27038	0.27038	0.27038	
MISSING					
	NITROGEN	0.10993	0.10993	0.10993	
MISSING					
	OXYGEN	0.12116	0.12116	0.12116	
MISSING					
	ARGON	0.12710E-02	0.12710E-02	0.12710E-02	
MISSING					

BLOCK: SOEC2 MODEL: SEP

-----  
 INLET STREAM: SOEC1  
 OUTLET STREAMS: 11 12  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*  
 IN OUT

DIFF.		IN	OUT	RELATIVE
	TOTAL BALANCE			
	MOLE (KMOL/HR )	706.482	706.482	0.00000
	MASS (KG/HR )	11664.4	11664.4	0.00000
	ENTHALPY (CAL/SEC )	-0.440427E+07	-0.440460E+07	
0.743308E-04				

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR STREAM 11  
 TWO PHASE TP FLASH  
 PRESSURE DROP BAR 0.0  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLASH SPECS FOR STREAM 12  
 TWO PHASE TP FLASH  
 PRESSURE DROP BAR 0.0  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FRACTION OF FEED

SUBSTREAM= MIXED  
 STREAM= 12           CPT= WATER       FRACTION=           0.0  
                           HYDROGEN               0.0  
                           NITROGEN               0.0  
                           ARGON                    0.0

MOLE-FLOW (KMOL/HR )  
 SUBSTREAM= MIXED  
 STREAM= 12           CPT= OXYGEN       FLOW=               85.6000

\*\*\* RESULTS \*\*\*

HEAT DUTY                   CAL/SEC                               -327.40

COMPONENT = WATER  
 STREAM       SUBSTREAM       SPLIT FRACTION  
 11           MIXED               1.00000

COMPONENT = HYDROGEN  
 STREAM       SUBSTREAM       SPLIT FRACTION  
 11           MIXED               1.00000

COMPONENT = NITROGEN  
 STREAM       SUBSTREAM       SPLIT FRACTION  
 11           MIXED               1.00000

COMPONENT = OXYGEN  
 STREAM       SUBSTREAM       SPLIT FRACTION  
 12           MIXED               1.00000

COMPONENT = ARGON  
 STREAM       SUBSTREAM       SPLIT FRACTION  
 11           MIXED               1.00000

BLOCK: UP-BO-01 MODEL: HEATER

-----

INLET STREAM:               2  
 OUTLET STREAM:              3  
 PROPERTY OPTION SET:       SRK           SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	491.700	491.700	0.00000
MASS (KG/HR )	8858.11	8858.11	0.00000
ENTHALPY (CAL/SEC )	-0.941751E+07	-0.746901E+07	-0.206903

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR



TOTAL CO2E PRODUCTION 0.00000 KG/HR

\*\*\* INPUT DATA \*\*\*

TWO PHASE TP FLASH
SPECIFIED TEMPERATURE C 420.000
SPECIFIED PRESSURE BAR 40.0000
MAXIMUM NO. ITERATIONS 30
CONVERGENCE TOLERANCE 0.000100000

\*\*\* RESULTS \*\*\*

OUTLET TEMPERATURE C 420.00
OUTLET PRESSURE BAR 40.000
HEAT DUTY CAL/SEC 0.19485E+07
OUTLET VAPOR FRACTION 1.0000

V-L PHASE EQUILIBRIUM :

COMP F(I) X(I) Y(I) K(I)
WATER 1.0000 1.0000 1.0000
MISSING

BLOCK: UP-CD-01 MODEL: HEATX

HOT SIDE:

INLET STREAM: 15
OUTLET STREAM: 16
PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE
COLD SIDE:

INLET STREAM: CW6
OUTLET STREAM: CW7
PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

DIFF. IN OUT RELATIVE
TOTAL BALANCE
MOLE (KMOL/HR ) 7013.29 7013.29 0.00000
MASS (KG/HR ) 124086. 124086. 0.00000
ENTHALPY (CAL/SEC ) -0.128948E+09 -0.128948E+09 -
0.231119E-15

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E 0.00000 KG/HR
PRODUCT STREAMS CO2E 0.00000 KG/HR
NET STREAMS CO2E PRODUCTION 0.00000 KG/HR
UTILITIES CO2E PRODUCTION 0.00000 KG/HR
TOTAL CO2E PRODUCTION 0.00000 KG/HR

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR HOT SIDE:

TWO PHASE FLASH  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLASH SPECS FOR COLD SIDE:

TWO PHASE FLASH  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLOW DIRECTION AND SPECIFICATION:

COUNTERCURRENT HEAT EXCHANGER  
 SPECIFIED HOT OUTLET TEMP  
 SPECIFIED VALUE C 35.0000  
 LMTD CORRECTION FACTOR 1.00000

PRESSURE SPECIFICATION:

HOT SIDE PRESSURE DROP BAR 0.0345  
 COLD SIDE PRESSURE DROP BAR 0.0000

HEAT TRANSFER COEFFICIENT SPECIFICATION:

HOT LIQUID	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD VAPOR	CAL/SEC-SQCM-K	0.0203

\*\*\* OVERALL RESULTS \*\*\*

STREAMS:

```

-----
15      -----> |                | |-----> 16
T= 5.9845D+02 |                | | T=
3.5000D+01 |                | |
P= 3.8966D+01 |                | | P=
3.8931D+01 |                | |
V= 1.0000D+00 |                | | V=
4.3473D-01 |                | |
CW7      <----- |                | |----- CW6
T= 3.2222D+01 |                | | T= -
1.7778D+01 |                | |
P= 1.0000D+00 |                | | P=
1.0000D+00 |                | |
V= 0.0000D+00 |                | | V=
0.0000D+00 |                | |
    
```

DUTY AND AREA:

CALCULATED HEAT DUTY	CAL/SEC	1849243.1706
CALCULATED (REQUIRED) AREA	SQM	65.9652
ACTUAL EXCHANGER AREA	SQM	65.9652
PER CENT OVER-DESIGN		0.0000

HEAT TRANSFER COEFFICIENT:

AVERAGE COEFFICIENT (DIRTY)	CAL/SEC-SQCM-K	0.0203
UA (DIRTY)	CAL/SEC-K	13392.1917

LOG-MEAN TEMPERATURE DIFFERENCE:

LMTD CORRECTION FACTOR		1.0000
LMTD (CORRECTED)	C	138.0837
NUMBER OF SHELLS IN SERIES		1

PRESSURE DROP:

HOTSIDE, TOTAL	BAR	0.0345
COLD SIDE, TOTAL	BAR	0.0000

\*\*\* ZONE RESULTS \*\*\*

TEMPERATURE LEAVING EACH ZONE:

		HOT			
HOT IN		VAP		COND	
HOT OUT					
----->					---
---					
598.5		213.7			
35.0					
COLDOUT		LIQ		LIQ	
COLDIN					
<-----					<---
----					
32.2		17.0			-
17.8					
		COLD			

ZONE HEAT TRANSFER AND AREA:

ZONE	HEAT DUTY CAL/SEC	AREA SQM	LMTD C	AVERAGE U CAL/SEC-SQCM-K	UA
CAL/SEC-K					
1	559364.539	7.8838	349.4788	0.0203	
1600.5680					
2	1289878.632	58.0814	109.3894	0.0203	
11791.6237					

HEATX COLD-TQCU UP-CD-01 TQCURV INLET

-----  
 PRESSURE PROFILE:           CONSTANT2  
 PRESSURE DROP:             0.0            BAR  
 PROPERTY OPTION SET:     SRK            SOAVE-REDLICH-KWONG EQUATION OF STATE

! DUTY	! PRES	! TEMP	! VFRAC	!
!	!	!	!	!
!	!	!	!	!
! CAL/SEC	! BAR	! C	!	!
!	!	!	!	!
!=====!	!=====!	!=====!	!=====!	!
! 0.0	! 1.0000	! 32.2222	! 0.0	!
! 8.8059+04	! 1.0000	! 29.8281	! 0.0	!
! 1.7612+05	! 1.0000	! 27.4346	! 0.0	!
! 2.6418+05	! 1.0000	! 25.0420	! 0.0	!
! 3.5224+05	! 1.0000	! 22.6501	! 0.0	!
!-----!	!-----!	!-----!	!-----!	!
! 4.4030+05	! 1.0000	! 20.2593	! 0.0	!
! 5.2836+05	! 1.0000	! 17.8695	! 0.0	!
! 5.5935+05	! 1.0000	! 17.0286	! 0.0	!
! 6.1641+05	! 1.0000	! 15.4810	! 0.0	!
! 7.0447+05	! 1.0000	! 13.0937	! 0.0	!
!-----!	!-----!	!-----!	!-----!	!
! 7.9253+05	! 1.0000	! 10.7078	! 0.0	!
! 8.8059+05	! 1.0000	! 8.3234	! 0.0	!
! 9.6865+05	! 1.0000	! 5.9405	! 0.0	!
! 1.0567+06	! 1.0000	! 3.5594	! 0.0	!
! 1.1448+06	! 1.0000	! 1.1801	! 0.0	!
!-----!	!-----!	!-----!	!-----!	!
! 1.2328+06	! 1.0000	! -1.1974	! 0.0	!
! 1.3209+06	! 1.0000	! -3.5728	! 0.0	!
! 1.4089+06	! 1.0000	! -5.9461	! 0.0	!
! 1.4970+06	! 1.0000	! -8.3173	! 0.0	!
! 1.5851+06	! 1.0000	! -10.6861	! 0.0	!
!-----!	!-----!	!-----!	!-----!	!
! 1.6731+06	! 1.0000	! -13.0525	! 0.0	!
! 1.7612+06	! 1.0000	! -15.4165	! 0.0	!
! 1.8492+06	! 1.0000	! -17.7778	! 0.0	!
!-----!	!-----!	!-----!	!-----!	!

HEATX HOT-TQCUR UP-CD-01 TQCURV INLET

-----  
 PRESSURE PROFILE:           CONSTANT2  
 PRESSURE DROP:             0.0            BAR  
 PROPERTY OPTION SET:     SRK            SOAVE-REDLICH-KWONG EQUATION OF STATE

! DUTY	! PRES	! TEMP	! VFRAC	!
!	!	!	!	!
!	!	!	!	!
!	!	!	!	!
!	!	!	!	!

CAL/SEC	BAR	C	
0.0	38.9658	598.4517	1.0000
8.8059+04	38.9658	539.0362	1.0000
1.7612+05	38.9658	478.9835	1.0000
2.6418+05	38.9658	418.3820	1.0000
3.5224+05	38.9658	357.3703	1.0000
4.4030+05	38.9658	296.1613	1.0000
5.2836+05	38.9658	235.0891	1.0000
5.5935+05	38.9658	213.7170	DEW>1.0000
6.1641+05	38.9658	212.1274	0.9619
7.0447+05	38.9658	209.3752	0.9040
7.9253+05	38.9658	206.1884	0.8472
8.8059+05	38.9658	202.4636	0.7919
9.6865+05	38.9658	198.0651	0.7382
1.0567+06	38.9658	192.8126	0.6865
1.1448+06	38.9658	186.4635	0.6375
1.2328+06	38.9658	178.6899	0.5917
1.3209+06	38.9658	169.0453	0.5499
1.4089+06	38.9658	156.9273	0.5131
1.4970+06	38.9658	141.5472	0.4825
1.5851+06	38.9658	121.9693	0.4594
1.6731+06	38.9658	97.3929	0.4445
1.7612+06	38.9658	67.8882	0.4372
1.8492+06	38.9658	34.9997	0.4347

BLOCK: UP-CO-01 MODEL: HEATX

HOT SIDE:

INLET STREAM: 7A  
 OUTLET STREAM: 7B  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 COLD SIDE:

INLET STREAM: CW1  
 OUTLET STREAM: CW2  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

DIFF.	IN	OUT	RELATIVE
TOTAL BALANCE			
MOLE (KMOL/HR )	476.178	476.178	0.00000
MASS (KG/HR )	9379.19	9379.19	0.00000
ENTHALPY (CAL/SEC )	-0.769531E+07	-0.769531E+07	0.00000

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR HOT SIDE:

TWO PHASE FLASH	
MAXIMUM NO. ITERATIONS	30
CONVERGENCE TOLERANCE	0.000100000

FLASH SPECS FOR COLD SIDE:

TWO PHASE FLASH	
MAXIMUM NO. ITERATIONS	30
CONVERGENCE TOLERANCE	0.000100000

FLOW DIRECTION AND SPECIFICATION:

COUNTERCURRENT HEAT EXCHANGER	
SPECIFIED HOT OUTLET TEMP	
SPECIFIED VALUE	C 37.7778
LMTD CORRECTION FACTOR	1.00000

PRESSURE SPECIFICATION:

HOT SIDE PRESSURE DROP	BAR	0.3447
COLD SIDE PRESSURE DROP	BAR	0.0000

HEAT TRANSFER COEFFICIENT SPECIFICATION:

HOT LIQUID	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD VAPOR	CAL/SEC-SQCM-K	0.0203

\*\*\* OVERALL RESULTS \*\*\*

STREAMS :

```

-----|-----
7A      ----->|          HOT          |-----> 7B
T= 1.9791D+02 |          |          |          |          |
3.7778D+01     |          |          |          |          |
P= 3.4200D+00 |          |          |          |          |
3.0753D+00     |          |          |          |          |
V= 1.0000D+00 |          |          |          |          |
1.0000D+00     |          |          |          |          |
          |          |          |          |          |
CW2      <-----|          COLD          |<----- CW1
  
```

T= 3.6532D+01 | | T=  
 2.6667D+01  
 P= 1.0000D+00 | | P=  
 1.0000D+00  
 V= 0.0000D+00 | | V=  
 0.0000D+00

-----

DUTY AND AREA:

CALCULATED HEAT DUTY	CAL/SEC	22875.9612
CALCULATED (REQUIRED) AREA	SQM	2.0065
ACTUAL EXCHANGER AREA	SQM	2.0065
PER CENT OVER-DESIGN		0.0000

HEAT TRANSFER COEFFICIENT:

AVERAGE COEFFICIENT (DIRTY)	CAL/SEC-SQCM-K	0.0203
UA (DIRTY)	CAL/SEC-K	407.3491

LOG-MEAN TEMPERATURE DIFFERENCE:

LMTD CORRECTION FACTOR		1.0000
LMTD (CORRECTED)	C	56.1581
NUMBER OF SHELLS IN SERIES		1

PRESSURE DROP:

HOTSIDE, TOTAL	BAR	0.3447
COLD SIDE, TOTAL	BAR	0.0000

\*\*\* ZONE RESULTS \*\*\*

TEMPERATURE LEAVING EACH ZONE:

	HOT		
	-----		
HOT IN		VAP	
HOT OUT			
----->			---
--->			
197.9			
37.8			
COLDOUT		LIQ	
COLDIN			
<-----			<---
----			
36.5			
26.7			
	-----		
	COLD		

ZONE HEAT TRANSFER AND AREA:

ZONE	HEAT DUTY	AREA	LMTD	AVERAGE U	UA
------	-----------	------	------	-----------	----

CAL/SEC                      SQM                      C                      CAL/SEC-SQCM-K  
 CAL/SEC-K  
 1                      22875.961                      2.0065                      56.1581                      0.0203  
 407.3491

HEATX COLD-TQCU UP-CO-01 TQCURV INLET

-----  
 PRESSURE PROFILE:                      CONSTANT2  
 PRESSURE DROP:                      0.0                      BAR  
 PROPERTY OPTION SET:                      SRK                      SOAVE-REDLICH-KWONG EQUATION OF STATE

-----

! DUTY	! PRES	! TEMP	! VFRAC	!
!	!	!	!	!
!	!	!	!	!
! CAL/SEC	! BAR	! C	!	!
!	!	!	!	!
! =====	! =====	! =====	! =====	! =====
! 0.0	! 1.0000	! 36.5319	! 0.0	!
! 1089.3315	! 1.0000	! 36.0619	! 0.0	!
! 2178.6630	! 1.0000	! 35.5919	! 0.0	!
! 3267.9945	! 1.0000	! 35.1220	! 0.0	!
! 4357.3259	! 1.0000	! 34.6521	! 0.0	!
! -----	! -----	! -----	! -----	! -----
! 5446.6574	! 1.0000	! 34.1822	! 0.0	!
! 6535.9889	! 1.0000	! 33.7123	! 0.0	!
! 7625.3204	! 1.0000	! 33.2424	! 0.0	!
! 8714.6519	! 1.0000	! 32.7725	! 0.0	!
! 9803.9834	! 1.0000	! 32.3027	! 0.0	!
! -----	! -----	! -----	! -----	! -----
! 1.0893+04	! 1.0000	! 31.8329	! 0.0	!
! 1.1983+04	! 1.0000	! 31.3631	! 0.0	!
! 1.3072+04	! 1.0000	! 30.8934	! 0.0	!
! 1.4161+04	! 1.0000	! 30.4236	! 0.0	!
! 1.5251+04	! 1.0000	! 29.9539	! 0.0	!
! -----	! -----	! -----	! -----	! -----
! 1.6340+04	! 1.0000	! 29.4842	! 0.0	!
! 1.7429+04	! 1.0000	! 29.0146	! 0.0	!
! 1.8519+04	! 1.0000	! 28.5449	! 0.0	!
! 1.9608+04	! 1.0000	! 28.0753	! 0.0	!
! 2.0697+04	! 1.0000	! 27.6057	! 0.0	!
! -----	! -----	! -----	! -----	! -----
! 2.1787+04	! 1.0000	! 27.1362	! 0.0	!
! 2.2876+04	! 1.0000	! 26.6667	! 0.0	!

-----

HEATX HOT-TQCUR UP-CO-01 TQCURV INLET

-----  
 PRESSURE PROFILE:                      CONSTANT2  
 PRESSURE DROP:                      0.0                      BAR  
 PROPERTY OPTION SET:                      SRK                      SOAVE-REDLICH-KWONG EQUATION OF STATE

-----



DUTY	PRES	TEMP	VFRAC
CAL/SEC	BAR	C	
0.0	3.4200	197.9118	1.0000
1089.3315	3.4200	190.3568	1.0000
2178.6630	3.4200	182.7929	1.0000
3267.9945	3.4200	175.2203	1.0000
4357.3259	3.4200	167.6394	1.0000
5446.6574	3.4200	160.0505	1.0000
6535.9889	3.4200	152.4540	1.0000
7625.3204	3.4200	144.8500	1.0000
8714.6519	3.4200	137.2391	1.0000
9803.9834	3.4200	129.6216	1.0000
1.0893+04	3.4200	121.9979	1.0000
1.1983+04	3.4200	114.3684	1.0000
1.3072+04	3.4200	106.7334	1.0000
1.4161+04	3.4200	99.0935	1.0000
1.5251+04	3.4200	91.4489	1.0000
1.6340+04	3.4200	83.8003	1.0000
1.7429+04	3.4200	76.1480	1.0000
1.8519+04	3.4200	68.4925	1.0000
1.9608+04	3.4200	60.8342	1.0000
2.0697+04	3.4200	53.1737	1.0000
2.1787+04	3.4200	45.5114	1.0000
2.2876+04	3.4200	37.8479	1.0000

BLOCK: UP-CO-02 MODEL: HEATX

HOT SIDE:

INLET STREAM: 7C  
 OUTLET STREAM: 7D  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 COLD SIDE:

INLET STREAM: CW2  
 OUTLET STREAM: CW3  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	476.178	476.178	0.00000
MASS (KG/HR )	9379.19	9379.19	0.00000

ENTHALPY (CAL/SEC )            -0.766691E+07    -0.766691E+07  
0.121473E-15

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR HOT SIDE:

TWO PHASE FLASH	
MAXIMUM NO. ITERATIONS	30
CONVERGENCE TOLERANCE	0.000100000

FLASH SPECS FOR COLD SIDE:

TWO PHASE FLASH	
MAXIMUM NO. ITERATIONS	30
CONVERGENCE TOLERANCE	0.000100000

FLOW DIRECTION AND SPECIFICATION:

COUNTERCURRENT HEAT EXCHANGER	
SPECIFIED HOT OUTLET TEMP	
SPECIFIED VALUE	C 37.7778
LMTD CORRECTION FACTOR	1.00000

PRESSURE SPECIFICATION:

HOT SIDE PRESSURE DROP	BAR	0.3447
COLD SIDE PRESSURE DROP	BAR	0.0000

HEAT TRANSFER COEFFICIENT SPECIFICATION:

HOT LIQUID	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD VAPOR	CAL/SEC-SQCM-K	0.0203

\*\*\* OVERALL RESULTS \*\*\*

STREAMS :

7C	----->	HOT		-----> 7D
T= 2.3622D+02				T=
3.7778D+01				
P= 1.1700D+01				P=
1.1355D+01				

```

V= 1.0000D+00 | | V=
1.0000D+00
| |
CW3 <-----| | COLD |<----- CW2
T= 4.8889D+01 | | T=
3.6532D+01
P= 1.0000D+00 | | P=
1.0000D+00
V= 0.0000D+00 | | V=
0.0000D+00

```

-----

DUTY AND AREA:

CALCULATED HEAT DUTY	CAL/SEC	28635.0522
CALCULATED (REQUIRED) AREA	SQM	3.7997
ACTUAL EXCHANGER AREA	SQM	3.7997
PER CENT OVER-DESIGN		0.0000

HEAT TRANSFER COEFFICIENT:

AVERAGE COEFFICIENT (DIRTY)	CAL/SEC-SQCM-K	0.0203
UA (DIRTY)	CAL/SEC-K	771.4194

LOG-MEAN TEMPERATURE DIFFERENCE:

LMTD CORRECTION FACTOR		1.0000
LMTD (CORRECTED)	C	37.1200
NUMBER OF SHELLS IN SERIES		1

PRESSURE DROP:

HOTSIDE, TOTAL	BAR	0.3447
COLD SIDE, TOTAL	BAR	0.0000

\*\*\* ZONE RESULTS \*\*\*

TEMPERATURE LEAVING EACH ZONE:

```

HOT
-----
HOT IN | | |
HOT OUT | | |
-----> | | |
---> | | |
236.2 | | |
37.8 | | |
| | |
COLDOUT | | |
COLDIN | | |
<----- | | |
----- | | |
48.9 | | |
36.5 | | |
-----
COLD

```

ZONE HEAT TRANSFER AND AREA:

ZONE	HEAT DUTY CAL/SEC	AREA SQM	LMTD C	AVERAGE U CAL/SEC-SQCM-K	UA
CAL/SEC-K 1	28635.052	3.7997	37.1200	0.0203	
771.4194					

HEATX COLD-TQCU UP-CO-02 TQCURV INLET

-----  
 PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: 0.0 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

! DUTY	! PRES	! TEMP	! VFRAC	!
! CAL/SEC	! BAR	! C	!	!
! 0.0	! 1.0000	! 48.8889	! 0.0	!
! 1363.5739	! 1.0000	! 48.3004	! 0.0	!
! 2727.1478	! 1.0000	! 47.7120	! 0.0	!
! 4090.7217	! 1.0000	! 47.1235	! 0.0	!
! 5454.2957	! 1.0000	! 46.5351	! 0.0	!
! 6817.8696	! 1.0000	! 45.9466	! 0.0	!
! 8181.4435	! 1.0000	! 45.3581	! 0.0	!
! 9545.0174	! 1.0000	! 44.7696	! 0.0	!
! 1.0909+04	! 1.0000	! 44.1812	! 0.0	!
! 1.2272+04	! 1.0000	! 43.5927	! 0.0	!
! 1.3636+04	! 1.0000	! 43.0042	! 0.0	!
! 1.4999+04	! 1.0000	! 42.4158	! 0.0	!
! 1.6363+04	! 1.0000	! 41.8273	! 0.0	!
! 1.7726+04	! 1.0000	! 41.2389	! 0.0	!
! 1.9090+04	! 1.0000	! 40.6505	! 0.0	!
! 2.0454+04	! 1.0000	! 40.0620	! 0.0	!
! 2.1817+04	! 1.0000	! 39.4736	! 0.0	!
! 2.3181+04	! 1.0000	! 38.8853	! 0.0	!
! 2.4544+04	! 1.0000	! 38.2969	! 0.0	!
! 2.5908+04	! 1.0000	! 37.7085	! 0.0	!
! 2.7271+04	! 1.0000	! 37.1202	! 0.0	!
! 2.8635+04	! 1.0000	! 36.5319	! 0.0	!

HEATX HOT-TQCUR UP-CO-02 TQCURV INLET

-----  
 PRESSURE PROFILE: CONSTANT2

PRESSURE DROP: 0.0 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

```

-----
! DUTY      ! PRES      ! TEMP      ! VFRAC     !
!           !           !           !           !
!           !           !           !           !
!           !           !           !           !
! CAL/SEC   ! BAR       ! C         !           !
!           !           !           !           !
!=====!=====!=====!=====!
! 0.0       ! 11.7000  ! 236.2172 ! 1.0000  !
! 1363.5739 ! 11.7000  ! 226.8587 ! 1.0000  !
! 2727.1478 ! 11.7000  ! 217.4864 ! 1.0000  !
! 4090.7217 ! 11.7000  ! 208.1009 ! 1.0000  !
! 5454.2957 ! 11.7000  ! 198.7028 ! 1.0000  !
!-----+-----+-----+-----!
! 6817.8696 ! 11.7000  ! 189.2927 ! 1.0000  !
! 8181.4435 ! 11.7000  ! 179.8714 ! 1.0000  !
! 9545.0174 ! 11.7000  ! 170.4396 ! 1.0000  !
! 1.0909+04 ! 11.7000  ! 160.9980 ! 1.0000  !
! 1.2272+04 ! 11.7000  ! 151.5476 ! 1.0000  !
!-----+-----+-----+-----!
! 1.3636+04 ! 11.7000  ! 142.0893 ! 1.0000  !
! 1.4999+04 ! 11.7000  ! 132.6240 ! 1.0000  !
! 1.6363+04 ! 11.7000  ! 123.1527 ! 1.0000  !
! 1.7726+04 ! 11.7000  ! 113.6767 ! 1.0000  !
! 1.9090+04 ! 11.7000  ! 104.1968 ! 1.0000  !
!-----+-----+-----+-----!
! 2.0454+04 ! 11.7000  ! 94.7145  ! 1.0000  !
! 2.1817+04 ! 11.7000  ! 85.2310  ! 1.0000  !
! 2.3181+04 ! 11.7000  ! 75.7476  ! 1.0000  !
! 2.4544+04 ! 11.7000  ! 66.2658  ! 1.0000  !
! 2.5908+04 ! 11.7000  ! 56.7871  ! 1.0000  !
!-----+-----+-----+-----!
! 2.7271+04 ! 11.7000  ! 47.3130  ! 1.0000  !
! 2.8635+04 ! 11.7000  ! 37.8454  ! 1.0000  !
-----
  
```

BLOCK: UP-CO-03 MODEL: HEATX

HOT SIDE:

```

-----
INLET STREAM: 13
OUTLET STREAM: 14
PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE
COLD SIDE:
-----
  
```

```

INLET STREAM: CW4
OUTLET STREAM: CW5
PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE
  
```

\*\*\* MASS AND ENERGY BALANCE \*\*\*

DIFF.	IN	OUT	RELATIVE
TOTAL BALANCE			
MOLE (KMOL/HR )	975.256	975.256	0.00000
MASS (KG/HR )	18766.5	18766.5	0.00000
ENTHALPY (CAL/SEC )	-0.170273E+08	-0.170273E+08	0.00000

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR HOT SIDE:

TWO PHASE FLASH	
MAXIMUM NO. ITERATIONS	30
CONVERGENCE TOLERANCE	0.000100000

FLASH SPECS FOR COLD SIDE:

TWO PHASE FLASH	
MAXIMUM NO. ITERATIONS	30
CONVERGENCE TOLERANCE	0.000100000

FLOW DIRECTION AND SPECIFICATION:

COUNTERCURRENT HEAT EXCHANGER	
SPECIFIED HOT OUTLET TEMP	
SPECIFIED VALUE	C 35.0000
LMTD CORRECTION FACTOR	1.00000

PRESSURE SPECIFICATION:

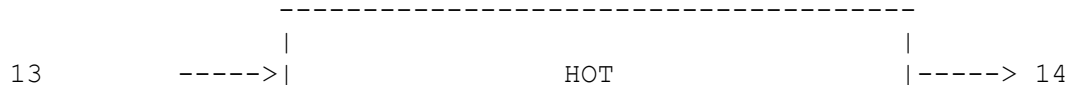
HOT SIDE PRESSURE DROP	BAR	0.0345
COLD SIDE PRESSURE DROP	BAR	0.0000

HEAT TRANSFER COEFFICIENT SPECIFICATION:

HOT LIQUID	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD VAPOR	CAL/SEC-SQCM-K	0.0203

\*\*\* OVERALL RESULTS \*\*\*

STREAMS:



```

T= 6.4962D+02 | | T=
3.5000D+01
P= 3.8966D+01 | | P=
3.8931D+01
V= 1.0000D+00 | | V=
1.0000D+00
| |
CW5 <-----| COLD |<----- CW4
T= 2.9444D+01 | | T=
7.2222D+00
P= 1.0000D+00 | | P=
1.0000D+00
V= 0.0000D+00 | | V=
0.0000D+00
-----

```

DUTY AND AREA:

CALCULATED HEAT DUTY	CAL/SEC	113997.9145
CALCULATED (REQUIRED) AREA	SQM	2.9438
ACTUAL EXCHANGER AREA	SQM	2.9438
PER CENT OVER-DESIGN		0.0000

HEAT TRANSFER COEFFICIENT:

AVERAGE COEFFICIENT (DIRTY)	CAL/SEC-SQCM-K	0.0203
UA (DIRTY)	CAL/SEC-K	597.6554

LOG-MEAN TEMPERATURE DIFFERENCE:

LMTD CORRECTION FACTOR		1.0000
LMTD (CORRECTED)	C	190.7419
NUMBER OF SHELLS IN SERIES		1

PRESSURE DROP:

HOTSIDE, TOTAL	BAR	0.0345
COLD SIDE, TOTAL	BAR	0.0000

\*\*\* ZONE RESULTS \*\*\*

TEMPERATURE LEAVING EACH ZONE:

```

HOT
-----
HOT IN | |
HOT OUT | VAP |
-----> | |
---> | |
649.6 | |
35.0 | |
COLDOUT | |
COLDIN | LIQ |
<----- | |
----- |<--

```

29.4 |  
7.2

COLD

ZONE HEAT TRANSFER AND AREA:

ZONE	HEAT DUTY CAL/SEC	AREA SQM	LMTD C	AVERAGE U CAL/SEC-SQCM-K	UA
1	113997.915	2.9438	190.7419	0.0203	
CAL/SEC-K					
597.6554					

HEATX COLD-TQCU UP-CO-03 TQCURV INLET

-----  
 PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: 0.0 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

DUTY	PRES	TEMP	VFRAC
CAL/SEC	BAR	C	
0.0	1.0000	29.4444	0.0
5428.4721	1.0000	28.3842	0.0
1.0857+04	1.0000	27.3242	0.0
1.6285+04	1.0000	26.2643	0.0
2.1714+04	1.0000	25.2045	0.0
2.7142+04	1.0000	24.1450	0.0
3.2571+04	1.0000	23.0856	0.0
3.7999+04	1.0000	22.0264	0.0
4.3428+04	1.0000	20.9674	0.0
4.8856+04	1.0000	19.9086	0.0
5.4285+04	1.0000	18.8500	0.0
5.9713+04	1.0000	17.7916	0.0
6.5142+04	1.0000	16.7335	0.0
7.0570+04	1.0000	15.6756	0.0
7.5999+04	1.0000	14.6179	0.0
8.1427+04	1.0000	13.5606	0.0
8.6856+04	1.0000	12.5034	0.0
9.2284+04	1.0000	11.4466	0.0
9.7712+04	1.0000	10.3901	0.0
1.0314+05	1.0000	9.3338	0.0
1.0857+05	1.0000	8.2779	0.0
1.1400+05	1.0000	7.2222	0.0



-----  
 HEATX HOT-TQCUR UP-CO-03 TQCURV INLET  
 -----

PRESSURE PROFILE:       CONSTANT2  
 PRESSURE DROP:         0.0            BAR  
 PROPERTY OPTION SET:   SRK            SOAVE-REDLICH-KWONG EQUATION OF STATE

! DUTY	! PRES	! TEMP	! VFRAC	!
! CAL/SEC	! BAR	! C	!	!
! 0.0	! 38.9658	! 649.6228	! 1.0000	!
! 5428.4721	! 38.9658	! 621.9434	! 1.0000	!
! 1.0857+04	! 38.9658	! 594.1472	! 1.0000	!
! 1.6285+04	! 38.9658	! 566.2272	! 1.0000	!
! 2.1714+04	! 38.9658	! 538.1757	! 1.0000	!
! 2.7142+04	! 38.9658	! 509.9844	! 1.0000	!
! 3.2571+04	! 38.9658	! 481.6443	! 1.0000	!
! 3.7999+04	! 38.9658	! 453.1458	! 1.0000	!
! 4.3428+04	! 38.9658	! 424.4788	! 1.0000	!
! 4.8856+04	! 38.9658	! 395.6328	! 1.0000	!
! 5.4285+04	! 38.9658	! 366.5973	! 1.0000	!
! 5.9713+04	! 38.9658	! 337.3621	! 1.0000	!
! 6.5142+04	! 38.9658	! 307.9180	! 1.0000	!
! 7.0570+04	! 38.9658	! 278.2580	! 1.0000	!
! 7.5999+04	! 38.9658	! 248.3788	! 1.0000	!
! 8.1427+04	! 38.9658	! 218.2828	! 1.0000	!
! 8.6856+04	! 38.9658	! 187.9816	! 1.0000	!
! 9.2284+04	! 38.9658	! 157.4991	! 1.0000	!
! 9.7712+04	! 38.9658	! 126.8775	! 1.0000	!
! 1.0314+05	! 38.9658	! 96.1829	! 1.0000	!
! 1.0857+05	! 38.9658	! 65.5132	! 1.0000	!
! 1.1400+05	! 38.9658	! 35.0080	! 1.0000	!

BLOCK: UP-CP-01 MODEL: COMPR  
 -----

INLET STREAM:           7  
 OUTLET STREAM:         7A  
 PROPERTY OPTION SET:   SRK            SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*  
                           IN                    OUT                    RELATIVE  
 DIFF.  
 TOTAL BALANCE

MOLE (KMOL/HR )	73.1600	73.1600	0.00000
MASS (KG/HR )	2118.72	2118.72	0.00000
ENTHALPY (CAL/SEC )	-32.2948	24591.9	-1.00131

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

ISENTROPIC CENTRIFUGAL COMPRESSOR

OUTLET PRESSURE BAR	3.42000
ISENTROPIC EFFICIENCY	0.72000
MECHANICAL EFFICIENCY	1.00000

\*\*\* RESULTS \*\*\*

INDICATED HORSEPOWER REQUIREMENT KW	103.097
BRAKE HORSEPOWER REQUIREMENT KW	103.097
NET WORK REQUIRED KW	103.097
POWER LOSSES KW	0.0
ISENTROPIC HORSEPOWER REQUIREMENT KW	74.2295
CALCULATED OUTLET TEMP C	197.912
ISENTROPIC TEMPERATURE C	149.950
EFFICIENCY (POLYTR/ISENTR) USED	0.72000
OUTLET VAPOR FRACTION	1.00000
HEAD DEVELOPED, M-KGF/KG	12,861.3
MECHANICAL EFFICIENCY USED	1.00000
INLET HEAT CAPACITY RATIO	1.40242
INLET VOLUMETRIC FLOW RATE , L/MIN	30,221.5
OUTLET VOLUMETRIC FLOW RATE, L/MIN	13,983.5
INLET COMPRESSIBILITY FACTOR	0.99984
OUTLET COMPRESSIBILITY FACTOR	1.00141
AV. ISENT. VOL. EXPONENT	1.40015
AV. ISENT. TEMP EXPONENT	1.39791
AV. ACTUAL VOL. EXPONENT	1.59553
AV. ACTUAL TEMP EXPONENT	1.59229

BLOCK: UP-CP-02 MODEL: COMPR

-----  
 INLET STREAM: 7B  
 OUTLET STREAM: 7C  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	73.1600	73.1600	0.00000
MASS (KG/HR )	2118.72	2118.72	0.00000
ENTHALPY (CAL/SEC )	1715.93	30114.2	-0.943019

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

ISENTROPIC CENTRIFUGAL COMPRESSOR

OUTLET PRESSURE BAR	11.7000
ISENTROPIC EFFICIENCY	0.72000
MECHANICAL EFFICIENCY	1.00000

\*\*\* RESULTS \*\*\*

INDICATED HORSEPOWER REQUIREMENT	KW	118.898
BRAKE HORSEPOWER REQUIREMENT	KW	118.898
NET WORK REQUIRED	KW	118.898
POWER LOSSES	KW	0.0
ISENTROPIC HORSEPOWER REQUIREMENT	KW	85.6064
CALCULATED OUTLET TEMP	C	236.217
ISENTROPIC TEMPERATURE	C	181.461
EFFICIENCY (POLYTR/ISENTR) USED		0.72000
OUTLET VAPOR FRACTION		1.00000
HEAD DEVELOPED,	M-KGF/KG	14,832.5
MECHANICAL EFFICIENCY USED		1.00000
INLET HEAT CAPACITY RATIO		1.40517
INLET VOLUMETRIC FLOW RATE ,	L/MIN	10,248.4
OUTLET VOLUMETRIC FLOW RATE,	L/MIN	4,435.97
INLET COMPRESSIBILITY FACTOR		0.99985
OUTLET COMPRESSIBILITY FACTOR		1.00506
AV. ISENT. VOL. EXPONENT		1.40440
AV. ISENT. TEMP EXPONENT		1.39724
AV. ACTUAL VOL. EXPONENT		1.59568
AV. ACTUAL TEMP EXPONENT		1.58583

BLOCK: UP-CP-03 MODEL: COMPR

-----

INLET STREAM:	7D
OUTLET STREAM:	8
PROPERTY OPTION SET:	SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	73.1600	73.1600	0.00000
MASS (KG/HR )	2118.72	2118.72	0.00000
ENTHALPY (CAL/SEC )	1479.11	28087.9	-0.947340

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
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PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

ISENTROPIC CENTRIFUGAL COMPRESSOR		
OUTLET PRESSURE BAR		40.0000
ISENTROPIC EFFICIENCY		0.72000
MECHANICAL EFFICIENCY		1.00000

\*\*\* RESULTS \*\*\*

INDICATED HORSEPOWER REQUIREMENT	KW	111.405
BRAKE HORSEPOWER REQUIREMENT	KW	111.405
NET WORK REQUIRED	KW	111.405
POWER LOSSES	KW	0.0
ISENTROPIC HORSEPOWER REQUIREMENT	KW	80.2120
CALCULATED OUTLET TEMP	C	222.905
ISENTROPIC TEMPERATURE	C	172.329
EFFICIENCY (POLYTR/ISENTR) USED		0.72000
OUTLET VAPOR FRACTION		1.00000
HEAD DEVELOPED,	M-KGF/KG	13,897.9
MECHANICAL EFFICIENCY USED		1.00000
INLET HEAT CAPACITY RATIO		1.41832
INLET VOLUMETRIC FLOW RATE ,	L/MIN	2,774.96
OUTLET VOLUMETRIC FLOW RATE,	L/MIN	1,279.26
INLET COMPRESSIBILITY FACTOR		0.99965
OUTLET COMPRESSIBILITY FACTOR		1.01751
AV. ISENT. VOL. EXPONENT		1.42616
AV. ISENT. TEMP EXPONENT		1.39972
AV. ACTUAL VOL. EXPONENT		1.62612
AV. ACTUAL TEMP EXPONENT		1.58976

BLOCK: UP-CP-04 MODEL: COMPR

-----

INLET STREAM:	19	
OUTLET STREAM:	20	
PROPERTY OPTION SET:	SRK	SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

DIFF.	IN	OUT	RELATIVE
TOTAL BALANCE			
MOLE (KMOL/HR )	71.4222	71.4222	0.00000
MASS (KG/HR )	687.620	687.620	-
0.165334E-15			
ENTHALPY (CAL/SEC )	1372.66	1840.32	-0.254120

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR

UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

ISENTROPIC CENTRIFUGAL COMPRESSOR		
OUTLET PRESSURE BAR		40.0000
ISENTROPIC EFFICIENCY		0.72000
MECHANICAL EFFICIENCY		1.00000

\*\*\* RESULTS \*\*\*

INDICATED HORSEPOWER REQUIREMENT	KW	1.95801
BRAKE HORSEPOWER REQUIREMENT	KW	1.95801
NET WORK REQUIRED	KW	1.95801
POWER LOSSES	KW	0.0
ISENTROPIC HORSEPOWER REQUIREMENT	KW	1.40977
CALCULATED OUTLET TEMP	C	38.3557
ISENTROPIC TEMPERATURE	C	37.4150
EFFICIENCY (POLYTR/ISENTR) USED		0.72000
OUTLET VAPOR FRACTION		1.00000
HEAD DEVELOPED,	M-KGF/KG	752.630
MECHANICAL EFFICIENCY USED		1.00000
INLET HEAT CAPACITY RATIO		1.41657
INLET VOLUMETRIC FLOW RATE ,	L/MIN	798.958
OUTLET VOLUMETRIC FLOW RATE,	L/MIN	786.496
INLET COMPRESSIBILITY FACTOR		1.01989
OUTLET COMPRESSIBILITY FACTOR		1.02043
AV. ISENT. VOL. EXPONENT		1.44519
AV. ISENT. TEMP EXPONENT		1.40503
AV. ACTUAL VOL. EXPONENT		1.72261
AV. ACTUAL TEMP EXPONENT		1.66651

BLOCK: UP-FH-01 MODEL: HEATER

-----

INLET STREAM:	8	
OUTLET STREAM:	9	
PROPERTY OPTION SET:	SRK	SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	73.1600	73.1600	0.00000
MASS (KG/HR )	2118.72	2118.72	0.00000
ENTHALPY (CAL/SEC )	28087.9	77585.2	-0.637974

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

ONE PHASE TP FLASH SPECIFIED PHASE IS VAPOR  
 SPECIFIED TEMPERATURE C 550.000  
 SPECIFIED PRESSURE BAR 40.0000  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE  
 0.000100000

\*\*\* RESULTS \*\*\*

OUTLET TEMPERATURE C 550.00  
 OUTLET PRESSURE BAR 40.000  
 HEAT DUTY CAL/SEC 49497.

BLOCK: UP-HX-01 MODEL: HEATX

-----  
 HOT SIDE:  
 -----

INLET STREAM: 11  
 OUTLET STREAM: 15  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 COLD SIDE:  
 -----

INLET STREAM: 4  
 OUTLET STREAM: 5  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	1184.00	1184.00	0.00000
MASS (KG/HR )	18471.1	18471.1	0.00000
ENTHALPY (CAL/SEC )	-0.120156E+08	-0.120156E+08	-

0.155019E-15

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR HOT SIDE:

TWO PHASE FLASH  
 MAXIMUM NO. ITERATIONS 30

CONVERGENCE TOLERANCE 0.000100000

FLASH SPECS FOR COLD SIDE:

TWO PHASE FLASH  
MAXIMUM NO. ITERATIONS 30  
CONVERGENCE TOLERANCE 0.000100000

FLOW DIRECTION AND SPECIFICATION:

COUNTERCURRENT HEAT EXCHANGER  
SPECIFIED COLD OUTLET TEMP  
SPECIFIED VALUE C 590.0000  
LMTD CORRECTION FACTOR 1.00000

PRESSURE SPECIFICATION:

HOT SIDE PRESSURE DROP BAR 0.3447  
COLD SIDE PRESSURE DROP BAR 0.3447

HEAT TRANSFER COEFFICIENT SPECIFICATION:

HOT LIQUID COLD LIQUID CAL/SEC-SQCM-K 0.0203  
HOT 2-PHASE COLD LIQUID CAL/SEC-SQCM-K 0.0203  
HOT VAPOR COLD LIQUID CAL/SEC-SQCM-K 0.0203  
HOT LIQUID COLD 2-PHASE CAL/SEC-SQCM-K 0.0203  
HOT 2-PHASE COLD 2-PHASE CAL/SEC-SQCM-K 0.0203  
HOT VAPOR COLD 2-PHASE CAL/SEC-SQCM-K 0.0203  
HOT LIQUID COLD VAPOR CAL/SEC-SQCM-K 0.0203  
HOT 2-PHASE COLD VAPOR CAL/SEC-SQCM-K 0.0203  
HOT VAPOR COLD VAPOR CAL/SEC-SQCM-K 0.0203

\*\*\* OVERALL RESULTS \*\*\*

STREAMS:

-----  
11 -----> | | |-----> 15  
T= 8.0000D+02 | | | T=  
5.9845D+02  
P= 3.9311D+01 | | | P=  
3.8966D+01  
V= 1.0000D+00 | | | V=  
1.0000D+00  
5 <----- | | | <----- 4  
T= 5.9000D+02 | | | T=  
3.8012D+02  
P= 3.9655D+01 | | | P=  
4.0000D+01  
V= 1.0000D+00 | | | V=  
1.0000D+00  
-----

DUTY AND AREA:

CALCULATED HEAT DUTY CAL/SEC 306825.9444  
CALCULATED (REQUIRED) AREA SQM 7.0577  
ACTUAL EXCHANGER AREA SQM 7.0577

PER CENT OVER-DESIGN 0.0000

HEAT TRANSFER COEFFICIENT:

AVERAGE COEFFICIENT (DIRTY)	CAL/SEC-SQCM-K	0.0203
UA (DIRTY)	CAL/SEC-K	1432.8402

LOG-MEAN TEMPERATURE DIFFERENCE:

LMTD CORRECTION FACTOR		1.0000
LMTD (CORRECTED)	C	214.1383
NUMBER OF SHELLS IN SERIES		1

PRESSURE DROP:

HOTSIDE, TOTAL	BAR	0.3447
COLD SIDE, TOTAL	BAR	0.3447

\*\*\* ZONE RESULTS \*\*\*

TEMPERATURE LEAVING EACH ZONE:

	HOT	
	-----	
HOT IN	VAP	
HOT OUT		
----->		---
--->		
800.0		
598.5		
	VAP	
COLDOUT		
COLDIN		
<-----		<--
----		
590.0		
380.1		
	COLD	
	-----	

ZONE HEAT TRANSFER AND AREA:

ZONE	HEAT DUTY CAL/SEC	AREA SQM	LMTD C	AVERAGE U CAL/SEC-SQCM-K	UA
CAL/SEC-K					
1	306825.944	7.0577	214.1383	0.0203	
1432.8402					

HEATX COLD-TQCU UP-HX-01 TQCURV INLET

-----

PRESSURE PROFILE:	CONSTANT2
PRESSURE DROP:	-0.3447 BAR
PROPERTY OPTION SET:	SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

-----



DUTY	PRES	TEMP	VFRAC
CAL/SEC	BAR	C	
0.0	40.0000	590.1092	1.0000
1.4611+04	40.0000	580.2449	1.0000
2.9222+04	40.0000	570.3627	1.0000
4.3832+04	40.0000	560.4629	1.0000
5.8443+04	40.0000	550.5461	1.0000
7.3054+04	40.0000	540.6128	1.0000
8.7665+04	40.0000	530.6636	1.0000
1.0228+05	40.0000	520.6992	1.0000
1.1689+05	40.0000	510.7202	1.0000
1.3150+05	40.0000	500.7274	1.0000
1.4611+05	40.0000	490.7216	1.0000
1.6072+05	40.0000	480.7038	1.0000
1.7533+05	40.0000	470.6749	1.0000
1.8994+05	40.0000	460.6359	1.0000
2.0455+05	40.0000	450.5880	1.0000
2.1916+05	40.0000	440.5325	1.0000
2.3377+05	40.0000	430.4705	1.0000
2.4838+05	40.0000	420.4037	1.0000
2.6299+05	40.0000	410.3336	1.0000
2.7760+05	40.0000	400.2619	1.0000
2.9222+05	40.0000	390.1904	1.0000
3.0683+05	40.0000	380.1211	1.0000

HEATX HOT-TQCUR UP-HX-01 TQCURV INLET

PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: 0.0 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

DUTY	PRES	TEMP	VFRAC
CAL/SEC	BAR	C	
0.0	39.3105	800.0000	1.0000
1.4611+04	39.3105	790.6004	1.0000
2.9222+04	39.3105	781.1815	1.0000
4.3832+04	39.3105	771.7432	1.0000
5.8443+04	39.3105	762.2854	1.0000

```

!-----+-----+-----+-----!
! 7.3054+04 ! 39.3105 ! 752.8081 ! 1.0000 !
! 8.7665+04 ! 39.3105 ! 743.3111 ! 1.0000 !
! 1.0228+05 ! 39.3105 ! 733.7945 ! 1.0000 !
! 1.1689+05 ! 39.3105 ! 724.2582 ! 1.0000 !
! 1.3150+05 ! 39.3105 ! 714.7021 ! 1.0000 !
!-----+-----+-----+-----!
! 1.4611+05 ! 39.3105 ! 705.1263 ! 1.0000 !
! 1.6072+05 ! 39.3105 ! 695.5307 ! 1.0000 !
! 1.7533+05 ! 39.3105 ! 685.9153 ! 1.0000 !
! 1.8994+05 ! 39.3105 ! 676.2801 ! 1.0000 !
! 2.0455+05 ! 39.3105 ! 666.6253 ! 1.0000 !
!-----+-----+-----+-----!
! 2.1916+05 ! 39.3105 ! 656.9507 ! 1.0000 !
! 2.3377+05 ! 39.3105 ! 647.2565 ! 1.0000 !
! 2.4838+05 ! 39.3105 ! 637.5427 ! 1.0000 !
! 2.6299+05 ! 39.3105 ! 627.8094 ! 1.0000 !
! 2.7760+05 ! 39.3105 ! 618.0567 ! 1.0000 !
!-----+-----+-----+-----!
! 2.9222+05 ! 39.3105 ! 608.2848 ! 1.0000 !
! 3.0683+05 ! 39.3105 ! 598.4937 ! 1.0000 !
!-----+-----+-----+-----!

```

BLOCK: UP-HX-02 MODEL: HEATX

-----  
HOT SIDE:

-----  
INLET STREAM: 12  
OUTLET STREAM: 13  
PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
COLD SIDE:

-----  
INLET STREAM: 5  
OUTLET STREAM: 6  
PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	648.722	648.722	0.00000
MASS (KG/HR )	12284.8	12284.8	0.00000
ENTHALPY (CAL/SEC )	-0.701648E+07	-0.701648E+07	0.00000

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR HOT SIDE:

TWO PHASE FLASH  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLASH SPECS FOR COLD SIDE:  
 TWO PHASE FLASH  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

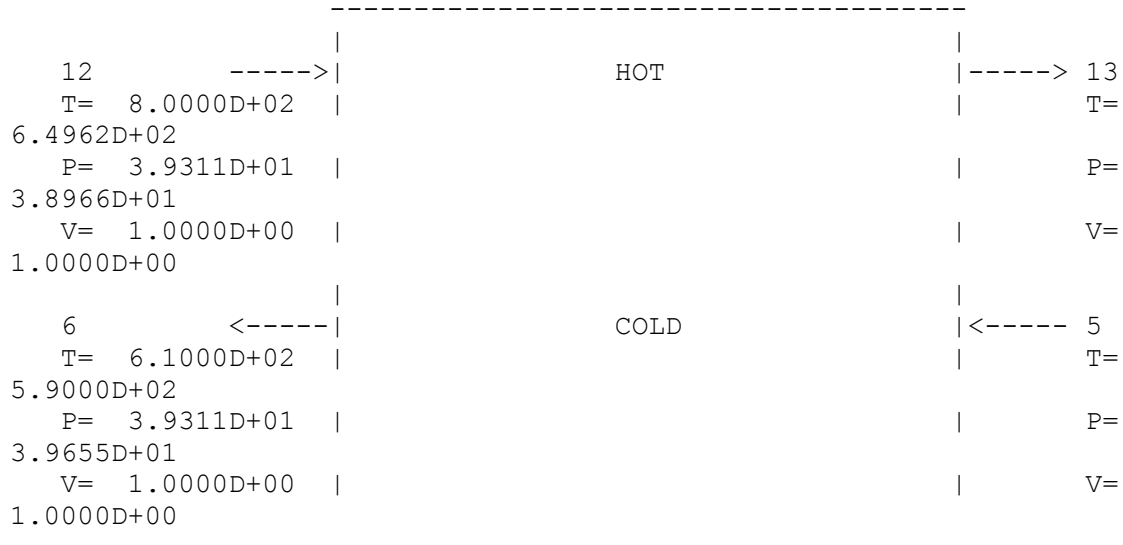
FLOW DIRECTION AND SPECIFICATION:  
 COUNTERCURRENT HEAT EXCHANGER  
 SPECIFIED COLD OUTLET TEMP  
 SPECIFIED VALUE C 610.0000  
 LMTD CORRECTION FACTOR 1.00000

PRESSURE SPECIFICATION:  
 HOT SIDE PRESSURE DROP BAR 0.3447  
 COLD SIDE PRESSURE DROP BAR 0.3447

HEAT TRANSFER COEFFICIENT SPECIFICATION:  
 HOT LIQUID COLD LIQUID CAL/SEC-SQCM-K 0.0203  
 HOT 2-PHASE COLD LIQUID CAL/SEC-SQCM-K 0.0203  
 HOT VAPOR COLD LIQUID CAL/SEC-SQCM-K 0.0203  
 HOT LIQUID COLD 2-PHASE CAL/SEC-SQCM-K 0.0203  
 HOT 2-PHASE COLD 2-PHASE CAL/SEC-SQCM-K 0.0203  
 HOT VAPOR COLD 2-PHASE CAL/SEC-SQCM-K 0.0203  
 HOT LIQUID COLD VAPOR CAL/SEC-SQCM-K 0.0203  
 HOT 2-PHASE COLD VAPOR CAL/SEC-SQCM-K 0.0203  
 HOT VAPOR COLD VAPOR CAL/SEC-SQCM-K 0.0203

\*\*\* OVERALL RESULTS \*\*\*

STREAMS:



DUTY AND AREA:  
 CALCULATED HEAT DUTY CAL/SEC 29852.2398

CALCULATED (REQUIRED) AREA	SQM	1.3071
ACTUAL EXCHANGER AREA	SQM	1.3071
PER CENT OVER-DESIGN		0.0000
HEAT TRANSFER COEFFICIENT:		
AVERAGE COEFFICIENT (DIRTY)	CAL/SEC-SQCM-K	0.0203
UA (DIRTY)	CAL/SEC-K	265.3710
LOG-MEAN TEMPERATURE DIFFERENCE:		
LMTD CORRECTION FACTOR		1.0000
LMTD (CORRECTED)	C	112.4925
NUMBER OF SHELLS IN SERIES		1
PRESSURE DROP:		
HOTSIDE, TOTAL	BAR	0.3447
COLD SIDE, TOTAL	BAR	0.3447

\*\*\* ZONE RESULTS \*\*\*

TEMPERATURE LEAVING EACH ZONE:

	HOT	
	-----	
HOT IN	VAP	
HOT OUT		
----->		---
--->		
800.0		
649.6		
COLDOUT	VAP	
COLDIN		
<-----		<--
----		
610.0		
590.0		
	-----	
	COLD	

ZONE HEAT TRANSFER AND AREA:

ZONE	HEAT DUTY CAL/SEC	AREA SQM	LMTD C	AVERAGE U CAL/SEC-SQCM-K	UA
1	29852.240	1.3071	112.4925	0.0203	
	265.3710				

HEATX COLD-TQCU UP-HX-02 TQCURV INLET

-----

PRESSURE PROFILE:	CONSTANT2
PRESSURE DROP:	-0.3447 BAR
PROPERTY OPTION SET:	SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

DUTY	PRES	TEMP	VFRAC
CAL/SEC	BAR	C	
0.0	39.6553	610.1030	1.0000
1421.5352	39.6553	609.1475	1.0000
2843.0705	39.6553	608.1919	1.0000
4264.6057	39.6553	607.2360	1.0000
5686.1409	39.6553	606.2800	1.0000
7107.6761	39.6553	605.3238	1.0000
8529.2114	39.6553	604.3674	1.0000
9950.7466	39.6553	603.4108	1.0000
1.1372+04	39.6553	602.4540	1.0000
1.2794+04	39.6553	601.4971	1.0000
1.4215+04	39.6553	600.5400	1.0000
1.5637+04	39.6553	599.5827	1.0000
1.7058+04	39.6553	598.6252	1.0000
1.8480+04	39.6553	597.6676	1.0000
1.9901+04	39.6553	596.7097	1.0000
2.1323+04	39.6553	595.7517	1.0000
2.2745+04	39.6553	594.7936	1.0000
2.4166+04	39.6553	593.8352	1.0000
2.5588+04	39.6553	592.8767	1.0000
2.7009+04	39.6553	591.9180	1.0000
2.8431+04	39.6553	590.9591	1.0000
2.9852+04	39.6553	590.0000	1.0000

HEATX HOT-TQCUR UP-HX-02 TQCURV INLET

PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: 0.0 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

DUTY	PRES	TEMP	VFRAC
CAL/SEC	BAR	C	
0.0	39.3105	800.0000	1.0000
1421.5352	39.3105	792.9010	1.0000
2843.0705	39.3105	785.7962	1.0000

! 4264.6057 !	39.3105 !	778.6856 !	1.0000 !
! 5686.1409 !	39.3105 !	771.5692 !	1.0000 !
! 7107.6761 !	39.3105 !	764.4468 !	1.0000 !
! 8529.2114 !	39.3105 !	757.3183 !	1.0000 !
! 9950.7466 !	39.3105 !	750.1838 !	1.0000 !
! 1.1372+04 !	39.3105 !	743.0430 !	1.0000 !
! 1.2794+04 !	39.3105 !	735.8960 !	1.0000 !
! 1.4215+04 !	39.3105 !	728.7426 !	1.0000 !
! 1.5637+04 !	39.3105 !	721.5827 !	1.0000 !
! 1.7058+04 !	39.3105 !	714.4163 !	1.0000 !
! 1.8480+04 !	39.3105 !	707.2433 !	1.0000 !
! 1.9901+04 !	39.3105 !	700.0635 !	1.0000 !
! 2.1323+04 !	39.3105 !	692.8769 !	1.0000 !
! 2.2745+04 !	39.3105 !	685.6834 !	1.0000 !
! 2.4166+04 !	39.3105 !	678.4829 !	1.0000 !
! 2.5588+04 !	39.3105 !	671.2753 !	1.0000 !
! 2.7009+04 !	39.3105 !	664.0604 !	1.0000 !
! 2.8431+04 !	39.3105 !	656.8382 !	1.0000 !
! 2.9852+04 !	39.3105 !	649.6086 !	1.0000 !

BLOCK: UP-MX-01 MODEL: MIXER

-----  
 INLET STREAMS: 3 20  
 OUTLET STREAM: 4  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	563.122	563.122	0.00000
MASS (KG/HR )	9545.73	9545.73	-
0.190555E-15			
ENTHALPY (CAL/SEC )	-0.746717E+07	-0.746717E+07	
0.124722E-15			

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

ONE PHASE FLASH SPECIFIED PHASE IS VAPOR	
MAXIMUM NO. ITERATIONS	30
CONVERGENCE TOLERANCE	0.000100000
OUTLET PRESSURE BAR	40.0000

BLOCK: UP-MX-02 MODEL: MIXER

-----  
INLET STREAMS: 6 9  
OUTLET STREAM: 10A  
PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	636.282	636.282	0.00000
MASS (KG/HR )	11664.4	11664.4	
0.311886E-15			
ENTHALPY (CAL/SEC )	-0.705290E+07	-0.705290E+07	-
0.132048E-15			

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

TWO PHASE FLASH  
MAXIMUM NO. ITERATIONS 30  
CONVERGENCE TOLERANCE 0.000100000  
OUTLET PRESSURE: MINIMUM OF INLET STREAM PRESSURES

BLOCK: UP-MX-03 MODEL: RSTOIC

-----  
INLET STREAM: 10A  
OUTLET STREAM: 10B  
PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	GENERATION	RELATIVE
DIFF.				
TOTAL BALANCE				
MOLE (KMOL/HR )	636.282	620.882	-15.4000	
0.00000				
MASS (KG/HR )	11664.4	11664.4		
0.00000				
ENTHALPY (CAL/SEC )	-0.705290E+07	-0.723256E+07		
0.248403E-01				

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

STOICHIOMETRY MATRIX:

REACTION # 1:  
 SUBSTREAM MIXED :  
 WATER 1.00 HYDROGEN -1.00 OXYGEN -0.500

REACTION EXTENT SPECS: NUMBER= 1  
 REACTION # 1: EXTENT= 30.80 KMOL/HR

ONE PHASE TP FLASH SPECIFIED PHASE IS VAPOR  
 SPECIFIED TEMPERATURE C 800.000  
 SPECIFIED PRESSURE BAR 39.3105  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000  
 SIMULTANEOUS REACTIONS  
 GENERATE COMBUSTION REACTIONS FOR FEED SPECIES NO

\*\*\* RESULTS \*\*\*

OUTLET TEMPERATURE C 800.00  
 OUTLET PRESSURE BAR 39.311  
 HEAT DUTY CAL/SEC -0.17966E+06

BLOCK: UP-PM-01 MODEL: PUMP

-----

INLET STREAM: 1  
 OUTLET STREAM: 2  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	491.700	491.700	0.00000
MASS (KG/HR )	8858.11	8858.11	0.00000
ENTHALPY (CAL/SEC )	-0.942335E+07	-0.941751E+07	-
0.619183E-03			

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

OUTLET PRESSURE BAR 40.0000  
 DRIVER EFFICIENCY 1.00000



FLASH SPECIFICATIONS:  
 LIQUID PHASE CALCULATION  
 NO FLASH PERFORMED  
 MAXIMUM NUMBER OF ITERATIONS 30  
 TOLERANCE 0.000100000

\*\*\* RESULTS \*\*\*

VOLUMETRIC FLOW RATE	L/MIN	153.615
PRESSURE CHANGE	BAR	39.0000
NPSH AVAILABLE	M-KGF/KG	10.3610
FLUID POWER	KW	9.98495
BRAKE POWER	KW	24.4291
ELECTRICITY	KW	24.4291
PUMP EFFICIENCY USED		0.40873
NET WORK REQUIRED	KW	24.4291
HEAD DEVELOPED	M-KGF/KG	413.796

BLOCK: UP-SE-01 MODEL: SEP

-----

INLET STREAM:	16	
OUTLET STREAMS:	18	17
PROPERTY OPTION SET:	SRK	SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\*\*\*

\*  
 \*  
 \* SUM OF SPLITS SPECIFIED IS ILLEGAL  
 \*  
 \*

\*\*\*\*\*

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	620.882	620.882	
0.577485E-06			
MASS (KG/HR )	8925.35	8925.35	
0.990596E-07			
ENTHALPY (CAL/SEC )	-0.670452E+07	-0.670542E+07	
0.134095E-03			

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR STREAM 18  
 ONE PHASE TP FLASH SPECIFIED PHASE IS VAPOR  
 SPECIFIED PRESSURE BAR 38.9313  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLASH SPECS FOR STREAM 17  
 ONE PHASE TP FLASH SPECIFIED PHASE IS LIQUID  
 PRESSURE DROP BAR 0.0  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

MOLE-FLOW (KMOL/HR )  
 SUBSTREAM= MIXED  
 STREAM= 18 CPT= WATER FLOW= 0.0  
 HYDROGEN 232.800  
 NITROGEN 77.6000  
 OXYGEN 0.0  
 ARGON 0.90000

\*\*\* RESULTS \*\*\*

HEAT DUTY CAL/SEC -899.15

COMPONENT = WATER  
 STREAM SUBSTREAM SPLIT FRACTION  
 17 MIXED 1.00000

COMPONENT = HYDROGEN  
 STREAM SUBSTREAM SPLIT FRACTION  
 18 MIXED 1.00000

COMPONENT = NITROGEN  
 STREAM SUBSTREAM SPLIT FRACTION  
 18 MIXED 0.99918  
 17 MIXED 0.00082406

COMPONENT = ARGON  
 STREAM SUBSTREAM SPLIT FRACTION  
 18 MIXED 1.00000

BLOCK: UP-SP-01 MODEL: FSPLIT

-----  
 INLET STREAM: 18  
 OUTLET STREAMS: 19 21  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE

\*\*\* MASS AND ENERGY BALANCE \*\*\*  
 IN OUT

DIFF.

RELATIVE

TOTAL BALANCE			
MOLE (KMOL/HR )	269.518	269.518	0.00000
MASS (KG/HR )	2594.79	2594.79	0.00000
ENTHALPY (CAL/SEC )	5179.84	5179.84	0.00000

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

FRACTION OF FLOW	STRM=19	FRAC=	0.26500
------------------	---------	-------	---------

\*\*\* RESULTS \*\*\*

STREAM= 19	SPLIT=	0.26500	KEY= 0	STREAM-
ORDER= 1				
2		0.73500	0	

## B.1.5 SOEC Stream Summary

1 10A 10B 11 12  
-----

STREAM ID	1	10A	10B	11	12
FROM :	----	UP-MX-02	UP-MX-03	SOEC2	
SOEC2					
TO :	UP-PM-01	UP-MX-03	SOEC	UP-HX-01	UP-
HX-02					
SUBSTREAM: MIXED					
PHASE:	LIQUID	VAPOR	VAPOR	VAPOR	
VAPOR					
COMPONENTS: KMOL/HR					
WATER	491.7000	491.7000	522.5000	351.3000	0.0
HYDROGEN	0.0	50.6203	19.8203	191.0203	0.0
NITROGEN	0.0	77.6640	77.6640	77.6640	0.0
OXYGEN	0.0	15.4000	0.0	0.0	
85.6000					
ARGON	0.0	0.8980	0.8980	0.8980	0.0
TOTAL FLOW:					
KMOL/HR	491.7000	636.2822	620.8822	620.8822	
85.6000					
KG/HR	8858.1132	1.1664+04	1.1664+04	8925.3523	
2739.0973					
L/MIN	153.6146	1.9539+04	2.3484+04	2.3589+04	
3269.1917					
STATE VARIABLES:					
TEMP C	25.0000	603.3524	800.0000	800.0000	
800.0000					
PRES BAR	1.0000	39.3105	39.3105	39.3105	
39.3105					
VFRAC	0.0	1.0000	1.0000	1.0000	
1.0000					
LFRAC	1.0000	0.0	0.0	0.0	0.0
SFRAC	0.0	0.0	0.0	0.0	0.0
ENTHALPY:					
CAL/MOL	-6.8993+04	-3.9904+04	-4.1936+04	-2.6373+04	
6050.0777					
CAL/GM	-3829.7161	-2176.7382	-2232.1863	-1834.5980	
189.0720					
CAL/SEC	-9.4233+06	-7.0529+06	-7.2326+06	-4.5485+06	
1.4386+05					
ENTROPY:					
CAL/MOL-K	-38.9834	-5.1890	-4.3373	-1.1313	
2.4981					
CAL/GM-K	-2.1639	-0.2831	-0.2309	-7.8699-02	
7.8067-02					
DENSITY:					
MOL/CC	5.3348-02	5.4275-04	4.4064-04	4.3868-04	
4.3640-04					

GM/CC	0.9611	9.9499-03	8.2783-03	6.3062-03	
1.3964-02					
AVG MW	18.0153	18.3322	18.7869	14.3753	
31.9988					
13 14 15 16 17					
-----					
STREAM ID	13	14	15	16	17
FROM :	UP-HX-02	UP-CO-03	UP-HX-01	UP-CD-01	UP-
SE-01					
TO :	UP-CO-03	----	UP-CD-01	UP-SE-01	----
CONV. MAX. REL. ERR:	0.0	0.0	4.7370-06	0.0	0.0
SUBSTREAM: MIXED					
PHASE:	VAPOR	VAPOR	VAPOR	MIXED	
LIQUID					
COMPONENTS: KMOL/HR					
WATER	0.0	0.0	351.3000	351.3000	
351.3000					
HYDROGEN	0.0	0.0	191.0203	191.0203	0.0
NITROGEN	0.0	0.0	77.6640	77.6640	
6.4000-02					
OXYGEN	85.6000	85.6000	0.0	0.0	0.0
ARGON	0.0	0.0	0.8980	0.8980	0.0
TOTAL FLOW:					
KMOL/HR	85.6000	85.6000	620.8822	620.8822	
351.3640					
KG/HR	2739.0973	2739.0973	8925.3523	8925.3523	
6330.5607					
L/MIN	2838.9851	924.6971	1.9265+04	3129.5856	
110.7025					
STATE VARIABLES:					
TEMP C	649.6228	35.0000	598.4517	35.0000	
35.0000					
PRES BAR	38.9658	38.9313	38.9658	38.9313	
38.9313					
VFRAC	1.0000	1.0000	1.0000	0.4347	0.0
LFRAC	0.0	0.0	0.0	0.5653	
1.0000					
SFRAC	0.0	0.0	0.0	0.0	0.0
ENTHALPY:					
CAL/MOL	4794.6097	0.3049	-2.8152+04	-3.8874+04	-
6.8755+04					
CAL/GM	149.8372	9.5286-03	-1958.3548	-2704.2386	-
3816.1179					
CAL/SEC	1.1401+05	7.2499	-4.8553+06	-6.7045+06	-
6.7106+06					
ENTROPY:					
CAL/MOL-K	1.2556	-7.2082	-2.9486	-24.2343	-
38.3942					
CAL/GM-K	3.9239-02	-0.2253	-0.2051	-1.6858	-
2.1310					

DENSITY:					
MOL/CC	5.0253-04	1.5428-03	5.3715-04	3.3065-03	
5.2899-02					
GM/CC	1.6080-02	4.9369-02	7.7216-03	4.7532-02	
0.9531					
AVG MW	31.9988	31.9988	14.3753	14.3753	
18.0171					

18 19 2 20 21  
-----

STREAM ID	18	19	2	20	21
FROM :	UP-SE-01	UP-SP-01	UP-PM-01	UP-CP-04	UP-
SP-01					
TO :	UP-SP-01	UP-CP-04	UP-BO-01	UP-MX-01	----

SUBSTREAM: MIXED  
PHASE:  
VAPOR

COMPONENTS: KMOL/HR					
WATER	0.0	0.0	491.7000	0.0	0.0
HYDROGEN	191.0199	50.6203	0.0	50.6203	
140.3996					
NITROGEN	77.6000	20.5640	0.0	20.5640	
57.0360					
OXYGEN	0.0	0.0	0.0	0.0	0.0
ARGON	0.8980	0.2380	0.0	0.2380	
0.6600					

TOTAL FLOW:					
KMOL/HR	269.5179	71.4222	491.7000	71.4222	
198.0956					
KG/HR	2594.7907	687.6195	8858.1132	687.6195	
1907.1712					
L/MIN	3014.9374	798.9584	153.6654	786.4963	
2215.9790					

STATE VARIABLES:					
TEMP C	35.0000	35.0000	26.2138	38.3557	
35.0000					
PRES BAR	38.9313	38.9313	40.0000	40.0000	
38.9313					
VFRAC	1.0000	1.0000	0.0	1.0000	
1.0000					
LFRAC	0.0	0.0	1.0000	0.0	0.0
SFRAC	0.0	0.0	0.0	0.0	0.0

ENTHALPY:					
CAL/MOL	69.1881	69.1881	-6.8951+04	92.7604	
69.1881					
CAL/GM	7.1865	7.1865	-3827.3448	9.6349	
7.1865					
CAL/SEC	5179.8437	1372.6586	-9.4175+06	1840.3216	
3807.1851					

ENTROPY:					
CAL/MOL-K	-5.8222	-5.8222	-38.9164	-5.8010	-
5.8222					

CAL/GM-K	-0.6047	-0.6047	-2.1602	-0.6025	-
0.6047					
DENSITY:					
MOL/CC	1.4899-03	1.4899-03	5.3330-02	1.5135-03	
1.4899-03					
GM/CC	1.4344-02	1.4344-02	0.9608	1.4571-02	
1.4344-02					
AVG MW	9.6275	9.6275	18.0153	9.6275	
9.6275					

3 4 5 6 7  
-----

STREAM ID	3	4	5	6	7
FROM :	UP-BO-01	UP-MX-01	UP-HX-01	UP-HX-02	----
TO :	UP-MX-01	UP-HX-01	UP-HX-02	UP-MX-02	UP-
CP-01					

SUBSTREAM: MIXED

PHASE:	VAPOR	VAPOR	VAPOR	VAPOR	
VAPOR					

COMPONENTS: KMOL/HR

WATER	491.7000	491.7000	491.7000	491.7000	0.0
HYDROGEN	0.0	50.6203	50.6203	50.6203	0.0
NITROGEN	0.0	20.5640	20.5640	20.5640	
57.1000					
OXYGEN	0.0	0.0	0.0	0.0	
15.4000					
ARGON	0.0	0.2380	0.2380	0.2380	
0.6600					

TOTAL FLOW:

KMOL/HR	491.7000	563.1222	563.1222	563.1222	
73.1600					
KG/HR	8858.1132	9545.7327	9545.7327	9545.7327	
2118.7169					
L/MIN	1.1223+04	1.2184+04	1.6781+04	1.7349+04	
3.0222+04					

STATE VARIABLES:

TEMP C	420.0000	380.1211	590.0000	610.0000	
25.0000					
PRES BAR	40.0000	40.0000	39.6553	39.3105	
1.0000					
VFRAC	1.0000	1.0000	1.0000	1.0000	
1.0000					
LFRAC	0.0	0.0	0.0	0.0	0.0
SFRAC	0.0	0.0	0.0	0.0	0.0

ENTHALPY:

CAL/MOL	-5.4685+04	-4.7737+04	-4.5776+04	-4.5585+04	-
1.5891					
CAL/GM	-3035.4576	-2816.1067	-2700.3928	-2689.1346	-
5.4873-02					
CAL/SEC	-7.4690+06	-7.4672+06	-7.1603+06	-7.1305+06	-
32.2948					

ENTROPY:

CAL/MOL-K	-11.1286	-9.5045	-6.8853	-6.6495
1.1410				
CAL/GM-K	-0.6177	-0.5607	-0.4062	-0.3923
3.9399-02				
DENSITY:				
MOL/CC	7.3021-04	7.7029-04	5.5928-04	5.4097-04
4.0347-05				
GM/CC	1.3155-02	1.3058-02	9.4805-03	9.1703-03
1.1684-03				
AVG MW	18.0153	16.9514	16.9514	16.9514
28.9600				

7A 7B 7C 7D 8

-----

STREAM ID	7A	7B	7C	7D	8
FROM :	UP-CP-01	UP-CO-01	UP-CP-02	UP-CO-02	UP-
CP-03					
TO :	UP-CO-01	UP-CP-02	UP-CO-02	UP-CP-03	UP-
FH-01					
SUBSTREAM: MIXED					
PHASE:	VAPOR	VAPOR	VAPOR	VAPOR	
VAPOR					
COMPONENTS: KMOL/HR					
WATER	0.0	0.0	0.0	0.0	0.0
HYDROGEN	0.0	0.0	0.0	0.0	0.0
NITROGEN	57.1000	57.1000	57.1000	57.1000	
57.1000					
OXYGEN	15.4000	15.4000	15.4000	15.4000	
15.4000					
ARGON	0.6600	0.6600	0.6600	0.6600	
0.6600					
TOTAL FLOW:					
KMOL/HR	73.1600	73.1600	73.1600	73.1600	
73.1600					
KG/HR	2118.7169	2118.7169	2118.7169	2118.7169	
2118.7169					
L/MIN	1.3983+04	1.0248+04	4435.9706	2774.9582	
1279.2606					
STATE VARIABLES:					
TEMP C	197.9118	37.7778	236.2172	37.7778	
222.9051					
PRES BAR	3.4200	3.0753	11.7000	11.3553	
40.0000					
VFRAC	1.0000	1.0000	1.0000	1.0000	
1.0000					
LFRAC	0.0	0.0	0.0	0.0	0.0
SFRAC	0.0	0.0	0.0	0.0	0.0
ENTHALPY:					
CAL/MOL	1210.0985	84.4361	1481.8340	72.7828	
1382.1251					
CAL/GM	41.7851	2.9156	51.1682	2.5132	
47.7252					



CAL/SEC	2.4592+04	1715.9285	3.0114+04	1479.1084	
2.8088+04					
ENTROPY:					
CAL/MOL-K	1.9005	-0.8070	5.6172-03	-3.4379	-
2.6584					
CAL/GM-K	6.5626-02	-2.7865-02	1.9396-04	-0.1187	-
9.1795-02					
DENSITY:					
MOL/CC	8.7198-05	1.1898-04	2.7487-04	4.3941-04	
9.5315-04					
GM/CC	2.5253-03	3.4456-03	7.9604-03	1.2725-02	
2.7603-02					
AVG MW	28.9600	28.9600	28.9600	28.9600	
28.9600					

9 CW1 CW2 CW3 CW4

STREAM ID	9	CW1	CW2	CW3	CW4
FROM :	UP-FH-01	----	UP-CO-01	UP-CO-02	----
TO :	UP-MX-02	UP-CO-01	UP-CO-02	----	UP-
CO-03					

SUBSTREAM: MIXED

PHASE:	VAPOR	LIQUID	LIQUID	LIQUID	
--------	-------	--------	--------	--------	--

LIQUID

COMPONENTS: KMOL/HR

WATER	0.0	403.0176	403.0176	403.0176	
889.6555					
HYDROGEN	0.0	0.0	0.0	0.0	0.0
NITROGEN	57.1000	0.0	0.0	0.0	0.0
OXYGEN	15.4000	0.0	0.0	0.0	0.0
ARGON	0.6600	0.0	0.0	0.0	0.0

TOTAL FLOW:

KMOL/HR	73.1600	403.0176	403.0176	403.0176	
---------	---------	----------	----------	----------	--

889.6555

KG/HR	2118.7169	7260.4752	7260.4752	7260.4752	
-------	-----------	-----------	-----------	-----------	--

1.6027+04

L/MIN	2116.7436	126.0963	127.2374	128.7475	
-------	-----------	----------	----------	----------	--

273.7279

STATE VARIABLES:

TEMP C	550.0000	26.6667	36.5319	48.8889	
--------	----------	---------	---------	---------	--

7.2222

PRES BAR	40.0000	1.0000	1.0000	1.0000	
----------	---------	--------	--------	--------	--

1.0000

VFRAC	1.0000	0.0	0.0	0.0	0.0
-------	--------	-----	-----	-----	-----

LFRAC	0.0	1.0000	1.0000	1.0000	
-------	-----	--------	--------	--------	--

1.0000

SFRAC	0.0	0.0	0.0	0.0	0.0
-------	-----	-----	-----	-----	-----

ENTHALPY:

CAL/MOL	3817.7504	-6.8959+04	-6.8755+04	-6.8499+04	-
---------	-----------	------------	------------	------------	---

6.9363+04

CAL/GM	131.8282	-3827.7985	-3816.4558	-3802.2575	-
--------	----------	------------	------------	------------	---

3850.2092

CAL/SEC	7.7585+04	-7.7199+06	-7.6970+06	-7.6684+06	-
1.7141+07					
ENTROPY:					
CAL/MOL-K	1.1037	-38.8832	-38.3020	-37.5995	-
40.0894					
CAL/GM-K	3.8112-02	-2.1583	-2.1261	-2.0871	-
2.2253					
DENSITY:					
MOL/CC	5.7604-04	5.3269-02	5.2791-02	5.2172-02	
5.4169-02					
GM/CC	1.6682-02	0.9596	0.9510	0.9399	
0.9759					
AVG MW	28.9600	18.0153	18.0153	18.0153	
18.0153					

CW5 CW6 CW7 SOEC1  
-----

STREAM ID	CW5	CW6	CW7	SOEC1
FROM :	UP-CO-03	----	UP-CD-01	SOEC
TO :	----	UP-CD-01	----	SOEC2
SUBSTREAM: MIXED				
PHASE:	LIQUID	LIQUID	LIQUID	VAPOR
COMPONENTS: KMOL/HR				
WATER	889.6555	6392.4052	6392.4052	351.3000
HYDROGEN	0.0	0.0	0.0	191.0203
NITROGEN	0.0	0.0	0.0	77.6640
OXYGEN	0.0	0.0	0.0	85.6000
ARGON	0.0	0.0	0.0	0.8980
TOTAL FLOW:				
KMOL/HR	889.6555	6392.4052	6392.4052	706.4822
KG/HR	1.6027+04	1.1516+05	1.1516+05	1.1664+04
L/MIN	279.0528	1928.2758	2010.1432	2.6866+04
STATE VARIABLES:				
TEMP C	29.4444	-17.7778	32.2222	800.0000
PRES BAR	1.0000	1.0000	1.0000	39.3105
VFRAC	0.0	0.0	0.0	1.0000
LFRAC	1.0000	1.0000	1.0000	0.0
SFRAC	0.0	0.0	0.0	0.0
ENTHALPY:				
CAL/MOL	-6.8901+04	-6.9885+04	-6.8844+04	-2.2443+04
CAL/GM	-3824.6035	-3879.2179	-3821.4095	-1359.2898
CAL/SEC	-1.7027+07	-1.2409+08	-1.2224+08	-4.4043+06
ENTROPY:				
CAL/MOL-K	-38.7176	-41.7323	-38.5536	4.2610-02
CAL/GM-K	-2.1492	-2.3165	-2.1400	2.5808-03
DENSITY:				
MOL/CC	5.3135-02	5.5251-02	5.3001-02	4.3827-04
GM/CC	0.9572	0.9954	0.9548	7.2361-03
AVG MW	18.0153	18.0153	18.0153	16.5106

## B.2.2 Ammonia Synthesis ASPEN Inputs

```
;  
;Input Summary created by Aspen Plus Rel. 37.0 at 03:40:05 Mon Apr 20,  
2020  
;Directory C:\Users\dakotaw\Downloads Filename  
C:\Users\dakotaw\AppData\Local\Temp\~ap5ca7.txt  
;
```

### DYNAMICS

```
DYNAMICS RESULTS=ON
```

```
IN-UNITS MET PRESSURE=bar TEMPERATURE=C DELTA-T=C PDROP=bar &  
INVERSE-PRES='1/bar' SHORT-LENGTH=mm
```

```
DEF-STREAMS CONVEN ALL
```

```
SIM-OPTIONS MASS-BAL-CHE=YES FREE-WATER=YES
```

### MODEL-OPTION

```
DATABANKS 'APV110 PURE37' / 'APV110 AQUEOUS' / 'APV110 SOLIDS' &  
/ 'APV110 INORGANIC' / 'APESV110 AP-EOS' / &  
'NISTV110 NIST-TRC' / NOASPENPCD
```

```
PROP-SOURCES 'APV110 PURE37' / 'APV110 AQUEOUS' / &  
'APV110 SOLIDS' / 'APV110 INORGANIC' / 'APESV110 AP-EOS' &  
'NISTV110 NIST-TRC'
```

### COMPONENTS

```
AMMONIA H3N /  
N2 N2 /  
H2 H2 /  
ARGON AR /  
WATER H2O
```

### SOLVE

```
RUN-MODE MODE=SIM
```

### FLOWSHEET

```
BLOCK B4 IN=33 23 OUT=24  
BLOCK HB-RXN IN=28 OUT=29  
BLOCK HB-HXA-1 IN=31 25 OUT=32 26  
BLOCK HB-HXA-2 IN=29 27 OUT=30 28  
BLOCK HB-S-01 IN=24 OUT=25 34  
BLOCK HB-CP-03 IN=26 OUT=27  
BLOCK HB-S-02 IN=34 OUT=35 OUT  
BLOCK HB-CP-02 IN=35 OUT=36  
BLOCK B20 IN=36 OUT=PURGE 37  
BLOCK B21 IN=37 INPUT OUT=23  
BLOCK HB-HXA-3 IN=30 38 OUT=31 40  
BLOCK HB-HXA-4 IN=32 39 OUT=33 41
```

PROPERTIES SRK

STREAM 38

SUBSTREAM MIXED TEMP=45. <F> PRES=1. MASS-FLOW=1754.  
MASS-FRAC WATER 1.

STREAM 39

SUBSTREAM MIXED TEMP=45. <F> PRES=1. MASS-FLOW=23010.  
MASS-FRAC WATER 1.

STREAM 40

SUBSTREAM MIXED TEMP=90. <F> PRES=1. MASS-FLOW=1754.  
MASS-FRAC WATER 1.

STREAM 41

SUBSTREAM MIXED TEMP=90. <F> PRES=1. MASS-FLOW=23010.  
MASS-FRAC WATER 1.

STREAM INPUT

SUBSTREAM MIXED TEMP=35. PRES=39.6 MOLE-FLOW=198.1  
MOLE-FLOW AMMONIA 0.0 / N2 57.04 / H2 140.4 / ARGON &  
0.66 / WATER 0.

BLOCK B4 MIXER

PARAM

BLOCK B21 MIXER

PARAM

BLOCK B20 FSPLIT

FRAC PURGE 0.02

BLOCK HB-S-01 FLASH2

PARAM TEMP=30. PRES=39.6  
UTILITY UTILITY-ID=U-3

BLOCK HB-S-02 FLASH2

PARAM TEMP=20.00000000 PRES=10.13250000  
UTILITY UTILITY-ID=U-3

BLOCK HB-HXA-1 HEATX

PARAM INCR-COLD=60. CALC-TYPE=DESIGN PRES-HOT=35.46375000 &  
PRES-COLD=-5. <psi> MIN-TAPP=10.00000000 &  
CALC-METHOD=SHORTCUT  
FEEDS HOT=31 COLD=25  
OUTLETS-HOT 32  
OUTLETS-COLD 26  
HOT-SIDE DPPARMOPT=NO  
COLD-SIDE DPPARMOPT=NO  
TQ-PARAM CURVE=YES

BLOCK HB-HXA-2 HEATX

PARAM T-COLD=225. PRES-COLD=-5. <psi>  
FEEDS HOT=29 COLD=27

OUTLETS-HOT 30  
OUTLETS-COLD 28  
HOT-SIDE DPPARMOPT=NO  
COLD-SIDE DPPARMOPT=NO  
TQ-PARAM CURVE=YES

BLOCK HB-HXA-3 HEATX  
PARAM T-COLD=90. <F> TYPE=COUNTERCURRE PRES-HOT=-5. <psi> &  
CALC-METHOD=SHORTCUT  
FEEDS HOT=30 COLD=38  
OUTLETS-HOT 31  
OUTLETS-COLD 40  
HOT-SIDE DPPARMOPT=NO  
COLD-SIDE DPPARMOPT=NO  
TQ-PARAM CURVE=YES

BLOCK HB-HXA-4 HEATX  
PARAM T-COLD=90. <F> PRES-HOT=-5. <psi>  
FEEDS HOT=32 COLD=39  
OUTLETS-HOT 33  
OUTLETS-COLD 41  
HOT-SIDE DPPARMOPT=NO  
COLD-SIDE DPPARMOPT=NO  
TQ-PARAM CURVE=YES

BLOCK HB-RXN RSTOIC  
PARAM TEMP=400.0000000 PRES=81.06000000  
STOIC 1 MIXED N2 -1. / H2 -3. / AMMONIA 2.  
CONV 1 MIXED H2 0.2  
UTILITY UTILITY-ID=U-3

BLOCK HB-CP-02 COMPR  
PARAM TYPE=ISENTROPIC PRES=39.6 SB-MAXIT=30 SB-TOL=0.0001  
UTILITY UTILITY-ID=U-3

BLOCK HB-CP-03 COMPR  
PARAM TYPE=ISENTROPIC PRES=81.06000000 SB-MAXIT=30 &  
SB-TOL=0.0001  
UTILITY UTILITY-ID=U-3

UTILITY U-1 GENERAL  
COST PRICE=1.000000000  
PARAM UTILITY-TYPE=WATER COOLING-VALU=1.000000000

UTILITY U-2 GENERAL  
DESCRIPTION &  
"High Pressure Steam, Inlet Temp=250 C, Outlet Temp=249 C,  
Pres=572 psia"  
COST ENERGY-PRICE=1.04670000E-8  
PARAM UTILITY-TYPE=STEAM TIN=250.0000000 TOUT=249.0000000 &  
VFRAC=1. VFR-OUT=0. CALOPT=FLASH MIN-TAPP=10.00000000 &  
CALCCO2=YES FACTORSOURCE="US-EPA-Rule-E9-5711" FUELSOURCE= &  
"Natural\_gas" CO2FACTOR=2.34000000E-7 EFFICIENCY=0.85 &  
HTC=.1433075380

UTILITY U-3 GENERAL

DESCRIPTION "Electrical Utility"

COST ELEC-PRICE=.0775000000

PARAM UTILITY-TYPE=ELECTRICITY CALCCO2=YES FACTORSOURCE= &  
"US-EPA-Rule-E9-5711" FUELSOURCE="Natural\_gas" &  
CO2FACTOR=2.34000000E-7 EFFICIENCY=0.58

UTILITY U-4 GENERAL

DESCRIPTION "Cooling Water, Inlet Temp=20 C, Outlet Temp=25 C"

COST ENERGY-PRICE=8.8760160E-10

PARAM UTILITY-TYPE=WATER PRES=1.013250000 &  
PRES-OUT=1.013250000 TIN=20.00000000 TOUT=25.00000000 &  
CALOPT=FLASH MIN-TAPP=5.000000000 HTC=.0895672112

EO-CONV-OPTI

CONV-OPTIONS

PARAM TOL=0.005

STREAM-REPOR MOLEFLOW MASSFLOW

PROPERTY-REP PCES

;  
;  
;  
;  
;



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HEATX COLD-TQCU HB-HXA-1 TQCURV INLET.....	15
HEATX HOT-TQCUR HB-HXA-1 TQCURV INLET.....	16
BLOCK: HB-HXA-2 MODEL: HEATX.....	16
HEATX COLD-TQCU HB-HXA-2 TQCURV INLET.....	20
HEATX HOT-TQCUR HB-HXA-2 TQCURV INLET.....	21
BLOCK: HB-HXA-3 MODEL: HEATX.....	21
HEATX COLD-TQCU HB-HXA-3 TQCURV INLET.....	25
HEATX HOT-TQCUR HB-HXA-3 TQCURV INLET.....	26
BLOCK: HB-HXA-4 MODEL: HEATX.....	26
HEATX COLD-TQCU HB-HXA-4 TQCURV INLET.....	30
HEATX HOT-TQCUR HB-HXA-4 TQCURV INLET.....	31
BLOCK: HB-RXN MODEL: RSTOIC.....	31
BLOCK: HB-S-01 MODEL: FLASH2.....	33



BLOCK: HB-S-02 MODEL: FLASH2..... 34

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RUN CONTROL SECTION

RUN CONTROL INFORMATION

-----

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TYPE OF RUN: NEW

INPUT FILE NAME: \_3457zuo.inm

OUTPUT PROBLEM DATA FILE NAME: \_3457zuo  
LOCATED IN:

PDF SIZE USED FOR INPUT TRANSLATION:

NUMBER OF FILE RECORDS (PSIZE) = 0  
NUMBER OF IN-CORE RECORDS = 256  
PSIZE NEEDED FOR SIMULATION = 256

CALLING PROGRAM NAME: apmain  
LOCATED IN: C:\Program Files\AspenTech\Aspen Plus V11.0\Engine\Xe

SIMULATION REQUESTED FOR ENTIRE FLOWSHEET

FLWSHEET SECTION

FLWSHEET CONNECTIVITY BY STREAMS

STREAM	SOURCE	DEST	STREAM	SOURCE	DEST
INPUT	----	B21	38	----	HB-HXA-3
39	----	HB-HXA-4	24	B4	HB-S-01
29	HB-RXN	HB-HXA-2	32	HB-HXA-1	HB-HXA-4
26	HB-HXA-1	HB-CP-03	30	HB-HXA-2	HB-HXA-3
28	HB-HXA-2	HB-RXN	25	HB-S-01	HB-HXA-1
34	HB-S-01	HB-S-02	27	HB-CP-03	HB-HXA-2
35	HB-S-02	HB-CP-02	OUT	HB-S-02	----
36	HB-CP-02	B20	PURGE	B20	----
37	B20	B21	23	B21	B4
31	HB-HXA-3	HB-HXA-1	40	HB-HXA-3	----
33	HB-HXA-4	B4	41	HB-HXA-4	----

FLWSHEET CONNECTIVITY BY BLOCKS

BLOCK	INLETS	OUTLETS
B4	33 23	24
HB-RXN	28	29
HB-HXA-1	31 25	32 26
HB-HXA-2	29 27	30 28
HB-S-01	24	25 34
HB-CP-03	26	27
HB-S-02	34	35 OUT
HB-CP-02	35	36
B20	36	PURGE 37
B21	37 INPUT	23
HB-HXA-3	30 38	31 40
HB-HXA-4	32 39	33 41

CONVERGENCE STATUS SUMMARY

TEAR STREAM SUMMARY  
 =====

STREAM	VARIABLE	MAXIMUM	MAX. ERR.	ABSOLUTE	
CONV	ID	ERR/TOL	RELATIVE	ERROR	STAT
BLOCK	ID				
-----	-----	-----	-----	-----	-----
28	N2 MOLEFLOW	13.163	0.65813E-01	0.13621E-01	#
\$OLVER05					

24	MASS ENTHALPY	0.68356	-0.34178E-02	0.19311E-04	#
\$OLVER05					
31	N2 MOLEFLOW	10.562	-0.52808E-01	0.10814E-01	#
\$OLVER05					

# = CONVERGED  
\* = NOT CONVERGED

CONVERGENCE BLOCK: \$OLVER05

-----

Tear Stream :	28	24	31
Tolerance used:	0.500D-02	0.500D-02	0.500D-02
Trace molefrac:	0.500D-04	0.500D-04	0.500D-04

FLWSHEET SECTION

CONVERGENCE BLOCK: \$OLVER05 (CONTINUED)

MAXIT= 30 WAIT 1 ITERATIONS BEFORE ACCELERATING  
 QMAX = 0.0 QMIN = -5.0  
 METHOD: WEGSTEIN STATUS: CONVERGED  
 TOTAL NUMBER OF ITERATIONS: 30

\*\*\* FINAL VALUES \*\*\*

VAR#	TEAR STREAM VAR	STREAM VAR	SUBSTREA	COMPONEN	UNIT
VALUE	PREV VALUE	ERR/TOL			
1	TOTAL MOLEFLOW	28	MIXED		KMOL/HR
2337.7977	2259.7175	6.9106-02			
2	TOTAL MOLEFLOW	24	MIXED		KMOL/HR
2428.9364	2428.7642	1.4184-02			
3	TOTAL MOLEFLOW	31	MIXED		KMOL/HR
2166.1259	2227.4499	-5.5062-02			
4	MOLE-FLOW	28	MIXED	AMMONIA	KMOL/HR
807.8182	779.9406	7.1486-02			
5	MOLE-FLOW	28	MIXED	N2	KMOL/HR
794.0931	745.0587	3.1626-02			
6	MOLE-FLOW	28	MIXED	H2	KMOL/HR
702.0008	701.9366	1.8281-02			
7	MOLE-FLOW	28	MIXED	ARGON	KMOL/HR
33.8856	32.7816	6.7358			
8	MOLE-FLOW	28	MIXED	WATER	KMOL/HR
0.0	0.0	0.0			
9	PRESSURE	28	MIXED		BAR
80.7153	80.7153	0.0			
10	MASS ENTHALPY	28	MIXED		CAL/GM
139.3753	-141.3079	2.7353			
11	MOLE-FLOW	24	MIXED	AMMONIA	KMOL/HR
898.3425	898.2631	1.7674-02			
12	MOLE-FLOW	24	MIXED	N2	KMOL/HR
794.5430	794.4302	2.8409-02			
13	MOLE-FLOW	24	MIXED	H2	KMOL/HR
702.1252	702.1462	-6.0011-03			
14	MOLE-FLOW	24	MIXED	ARGON	KMOL/HR
33.9257	33.9247	6.4298-03			
15	MOLE-FLOW	24	MIXED	WATER	KMOL/HR
0.0	0.0	0.0			
16	PRESSURE	24	MIXED		BAR
35.1190	35.1190	0.0			
17	MASS ENTHALPY	24	MIXED		CAL/GM
135.4096	-134.9484	-0.6836			

18	MOLE-FLOW	31	MIXED	AMMONIA	KMOL/HR	
873.5322	895.4369	-0.8925				
19	MOLE-FLOW	31	MIXED	N2	KMOL/HR	
698.2629	737.1927	-0.5616				
20	MOLE-FLOW	31	MIXED	H2	KMOL/HR	
561.5493	561.5867	-1.3303-02				
21	MOLE-FLOW	31	MIXED	ARGON	KMOL/HR	
32.7816	33.2336	-0.7205				
22	MOLE-FLOW	31	MIXED	WATER	KMOL/HR	
0.0	0.0	0.0				
23	PRESSURE	31	MIXED		BAR	
80.7153	80.7153	0.0				
24	MASS ENTHALPY	31	MIXED		CAL/GM	-
100.0722	-97.0018	-0.3307				

\*\*\* ITERATION HISTORY \*\*\*

FLWSHEET SECTION

CONVERGENCE BLOCK: \$OLVER05 (CONTINUED)

TEAR STREAMS AND TEAR VARIABLES:

ITERATION COMPONEN	MAX-ERR/TOL ATTRIBUT ELEMENT	VAR#	STREAM ID	VAR DESCRIPTION	SUBSTREA
1	16.54	19 31		MOLE-FLO	MIXED N2
2	15.09	12 24		MOLE-FLO	MIXED N2
3	15.09	5 28		MOLE-FLO	MIXED N2
4	16.25	19 31		MOLE-FLO	MIXED N2
5	14.85	12 24		MOLE-FLO	MIXED N2
6	14.85	5 28		MOLE-FLO	MIXED N2
7	15.97	19 31		MOLE-FLO	MIXED N2
8	14.61	12 24		MOLE-FLO	MIXED N2
9	14.61	5 28		MOLE-FLO	MIXED N2
10	15.70	19 31		MOLE-FLO	MIXED N2
11	14.38	12 24		MOLE-FLO	MIXED N2
12	14.39	5 28		MOLE-FLO	MIXED N2
13	15.44	19 31		MOLE-FLO	MIXED N2
14	14.16	12 24		MOLE-FLO	MIXED N2
15	14.17	5 28		MOLE-FLO	MIXED N2
16	15.19	19 31		MOLE-FLO	MIXED N2
17	13.95	12 24		MOLE-FLO	MIXED N2
18	13.95	5 28		MOLE-FLO	MIXED N2
19	14.95	19 31		MOLE-FLO	MIXED N2
20	13.74	12 24		MOLE-FLO	MIXED N2
21	13.75	5 28		MOLE-FLO	MIXED N2
22	14.71	19 31		MOLE-FLO	MIXED N2
23	13.54	12 24		MOLE-FLO	MIXED N2
24	13.55	5 28		MOLE-FLO	MIXED N2
25	14.48	19 31		MOLE-FLO	MIXED N2
26	13.35	12 24		MOLE-FLO	MIXED N2
27	13.35	5 28		MOLE-FLO	MIXED N2
28	14.26	19 31		MOLE-FLO	MIXED N2
29	13.16	12 24		MOLE-FLO	MIXED N2
30	13.16	5 28		MOLE-FLO	MIXED N2

COMPUTATIONAL SEQUENCE

SEQUENCE USED WAS:

U-3  
 \*\$OLVER05 \*HB-RXN HB-S-01 \*HB-HXA-1 HB-HXA-4 HB-CP-03 HB-HXA-2 HB-  
 HXA-3  
 | HB-S-02 HB-CP-02 B20 B21 \*B4  
 (RETURN \*\$OLVER05)  
 U-1 U-2 U-4



OVERALL FLOWSHEET BALANCE

-----

FLOWSHEET SECTION

OVERALL FLOWSHEET BALANCE (CONTINUED)

	*** MASS AND ENERGY BALANCE ***		***	
	IN	OUT	GENERATION	RELATIVE
DIFF.				
CONVENTIONAL COMPONENTS (KMOL/HR )				
AMMONIA	0.00000	87.5393	93.5916	
0.691371E-01				
N2	57.0400	0.267413E-01	-46.7958	
0.179128				
H2	140.400	0.693437E-02	-140.387	
0.408834E-04				
ARGON	0.660000	0.692198E-02	0.00000	
0.989512				
WATER	1374.61	1374.61	0.00000	
0.00000				
TOTAL BALANCE				
MOLE (KMOL/HR )	1572.71	1462.19	-93.5916	
0.107639E-01				
MASS (KG/HR )	26671.3	26255.9		
0.155748E-01				
ENTHALPY (CAL/SEC )	-0.261857E+08	-0.264110E+08		
0.852834E-02				

*** CO2 EQUIVALENT SUMMARY ***		
FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	3683.15	KG/HR
TOTAL CO2E PRODUCTION	3683.15	KG/HR

PHYSICAL PROPERTIES SECTION

COMPONENTS

-----

ID	TYPE	ALIAS	NAME
AMMONIA	C	H3N	AMMONIA
N2	C	N2	NITROGEN
H2	C	H2	HYDROGEN
ARGON	C	AR	ARGON
WATER	C	H2O	WATER

UTILITY SECTION

UTILITY USAGE: U-1 (WATER)  
-----

INPUT DATA:

HEATING VALUE	1.0000	CAL/GM
PRICE	1.0000	\$/KG
INDEX TYPE		FUEL

RESULT:

HEATING VALUE	1.0000	CAL/GM
INDEXED PRICE	MISSING	\$/KG

THIS UTILITY IS PURCHASED

THIS UTILITY IS NOT USED BY ANY COST OR UOS BLOCKS

UTILITY SECTION

UTILITY USAGE: U-2 (STEAM)  
-----

HIGH PRESSURE STEAM, INLET TEMP=250 C, OUTLET TEMP=249 C, PRES=572 PSIA  
INPUT DATA:

INLET TEMPERATURE	250.0000	C
OUTLET TEMPERATURE	249.0000	C
INLET VAPOR FRACTION	1.0000	
OUTLET VAPOR FRACTION	0.0	
HEAT TRANSFER COEFFICIENT	0.1433	CAL/SEC-SQCM-K
CO2 DATA SOURCE		US-EPA-RULE-E9-5711
CO2 FUEL SOURCE		NATURAL_GAS
CO2 EMISSION FACTOR	2.3400-07	KG/CAL
THERMAL EFFICIENCY	0.8500	
PRICE	1.0467-08	\$/CAL
INDEX TYPE		FUEL

RESULT:

HEATING VALUE	410.6534	CAL/GM
INDEXED PRICE	MISSING	\$/KG
CO2 EMISSION FACTOR	2.3400-07	KG/CAL

THIS UTILITY IS PURCHASED

THIS UTILITY IS NOT USED BY ANY COST OR UOS BLOCKS

UTILITY SECTION

UTILITY USAGE: U-3 (ELECTRICITY)  
 -----

ELECTRICAL UTILITY  
 INPUT DATA:

CO2 DATA SOURCE	US-EPA-RULE-E9-5711
CO2 FUEL SOURCE	NATURAL GAS
CO2 EMISSION FACTOR	2.3400-07 KG/CAL
THERMAL EFFICIENCY	0.5800
PRICE	7.7500-02 \$/KWHR
INDEX TYPE	FUEL

RESULT:

INDEXED PRICE	7.7500-02 \$/KWHR
CO2 EMISSION FACTOR	2.3400-07 KG/CAL
TOTAL CO2 EMISSIONS	3683.1472 KG/HR

THIS UTILITY IS PURCHASED

USAGE:

BLOCK ID	MODEL	DUTY	USAGE RATE	COST
CO2E EMISSIONS		CAL/SEC	KW	\$/HR
KG/HR				
-----	-----	-----	-----	-----
HB-S-01	FLASH2	1.4040+06	5878.4438	
455.5794	2039.2502			
HB-S-02	FLASH2	1688.9115	7.0711	
0.5480	2.4530			
HB-RXN	RSTOIC	6.1354+05	2568.7607	
199.0790	891.1110			
HB-CP-02	COMPR	1159.9468	4.8565	
0.3764	1.6847			
HB-CP-03	COMPR	5.1545+05	2158.0905	
167.2520	748.6482			
		-----	-----	-----
	TOTAL:	2.5359+06	1.0617+04	
822.8348	3683.1472			
		=====	=====	
=====	=====			

UTILITY SECTION

UTILITY USAGE: U-4 (WATER)  
-----

COOLING WATER, INLET TEMP=20 C, OUTLET TEMP=25 C  
INPUT DATA:

INLET TEMPERATURE	20.0000	C
OUTLET TEMPERATURE	25.0000	C
INLET PRESSURE	1.0133	BAR
OUTLET PRESSURE	1.0133	BAR
HEAT TRANSFER COEFFICIENT	8.9567-02	CAL/SEC-SQCM-K
PRICE	8.8760-10	\$/CAL
INDEX TYPE		FUEL

RESULT:

COOLING VALUE	4.9861	CAL/GM
INDEXED PRICE	MISSING	\$/KG

THIS UTILITY IS PURCHASED

THIS UTILITY IS NOT USED BY ANY COST OR UOS BLOCKS









FREE WATER OPTION SET: SYSOP12 ASME STEAM TABLE  
 SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK ) .

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	3.45561	3.45561	0.00000
MASS (KG/HR )	60.9575	60.9575	-
0.116564E-15			
ENTHALPY (CAL/SEC )	-9182.34	-8022.40	-0.126324

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	1.68472	KG/HR
TOTAL CO2E PRODUCTION	1.68472	KG/HR

\*\*\* INPUT DATA \*\*\*

ISENTROPIC CENTRIFUGAL COMPRESSOR

OUTLET PRESSURE BAR	39.6000
ISENTROPIC EFFICIENCY	0.72000
MECHANICAL EFFICIENCY	1.00000

\*\*\* RESULTS \*\*\*

INDICATED HORSEPOWER REQUIREMENT KW	4.85647
BRAKE HORSEPOWER REQUIREMENT KW	4.85647
NET WORK REQUIRED KW	4.85647
POWER LOSSES KW	0.0
ISENTROPIC HORSEPOWER REQUIREMENT KW	3.49666
CALCULATED OUTLET TEMP C	171.026
ISENTROPIC TEMPERATURE C	138.310
EFFICIENCY (POLYTR/ISENTR) USED	0.72000
OUTLET VAPOR FRACTION	1.00000
HEAD DEVELOPED, M-KGF/KG	21,057.5
MECHANICAL EFFICIENCY USED	1.00000
INLET HEAT CAPACITY RATIO	1.41355
INLET VOLUMETRIC FLOW RATE , L/MIN	128.997
OUTLET VOLUMETRIC FLOW RATE, L/MIN	50.2032
INLET COMPRESSIBILITY FACTOR	0.93112
OUTLET COMPRESSIBILITY FACTOR	0.93470
AV. ISENT. VOL. EXPONENT	1.30351
AV. ISENT. TEMP EXPONENT	1.33106
AV. ACTUAL VOL. EXPONENT	1.44439
AV. ACTUAL TEMP EXPONENT	1.43854

\*\*\* ASSOCIATED UTILITIES \*\*\*

UTILITY ID FOR ELECTRICITY	U-3
RATE OF CONSUMPTION	4.8565 KW
COST	0.3764 \$/HR

CO2 EQUIVALENT EMISSIONS

1.6847 KG/HR

BLOCK: HB-CP-03 MODEL: COMPR

-----  
INLET STREAM: 26  
OUTLET STREAM: 27  
PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
FREE WATER OPTION SET: SYSOP12 ASME STEAM TABLE  
SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK ).

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	2337.80	2337.80	0.00000
MASS (KG/HR )	38771.7	38771.7	0.00000
ENTHALPY (CAL/SEC )	-0.219547E+07	-0.168002E+07	-0.234779

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	748.648	KG/HR
TOTAL CO2E PRODUCTION	748.648	KG/HR

\*\*\* INPUT DATA \*\*\*

ISENTROPIC CENTRIFUGAL COMPRESSOR

OUTLET PRESSURE BAR	81.0600
ISENTROPIC EFFICIENCY	0.72000
MECHANICAL EFFICIENCY	1.00000

\*\*\* RESULTS \*\*\*

INDICATED HORSEPOWER REQUIREMENT KW	2,158.09
BRAKE HORSEPOWER REQUIREMENT KW	2,158.09
NET WORK REQUIRED KW	2,158.09
POWER LOSSES KW	0.0
ISENTROPIC HORSEPOWER REQUIREMENT KW	1,553.83
CALCULATED OUTLET TEMP C	192.595
ISENTROPIC TEMPERATURE C	166.431
EFFICIENCY (POLYTR/ISENTR) USED	0.72000
OUTLET VAPOR FRACTION	1.00000
HEAD DEVELOPED, M-KGF/KG	14,711.9
MECHANICAL EFFICIENCY USED	1.00000
INLET HEAT CAPACITY RATIO	1.41573
INLET VOLUMETRIC FLOW RATE , L/MIN	29,474.6
OUTLET VOLUMETRIC FLOW RATE, L/MIN	18,736.7
INLET COMPRESSIBILITY FACTOR	0.98351
OUTLET COMPRESSIBILITY FACTOR	1.00663
AV. ISENT. VOL. EXPONENT	1.40390
AV. ISENT. TEMP EXPONENT	1.35763
AV. ACTUAL VOL. EXPONENT	1.60051
AV. ACTUAL TEMP EXPONENT	1.52243

\*\*\* ASSOCIATED UTILITIES \*\*\*

UTILITY ID FOR ELECTRICITY U-3  
 RATE OF CONSUMPTION 2158.0905 KW  
 COST 167.2520 \$/HR  
 CO2 EQUIVALENT EMISSIONS 748.6482 KG/HR

BLOCK: HB-HXA-1 MODEL: HEATX

-----  
 HOT SIDE:  
 -----

INLET STREAM: 31  
 OUTLET STREAM: 32  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 FREE WATER OPTION SET: SYSOP12 ASME STEAM TABLE  
 SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK ).  
 COLD SIDE:  
 -----

INLET STREAM: 25  
 OUTLET STREAM: 26  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 FREE WATER OPTION SET: SYSOP12 ASME STEAM TABLE  
 SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK ).

\*\*\* MASS AND ENERGY BALANCE \*\*\*

DIFF.	IN	OUT	RELATIVE
TOTAL BALANCE			
MOLE (KMOL/HR )	4503.92	4565.25	-
0.134328E-01			
MASS (KG/HR )	75650.8	77132.6	-
0.192104E-01			
ENTHALPY (CAL/SEC )	-0.354034E+07	-0.354881E+07	
0.238712E-02			

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR HOT SIDE:

TWO PHASE FLASH  
 FREE WATER CONSIDERED  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLASH SPECS FOR COLD SIDE:

TWO PHASE FLASH

FREE WATER CONSIDERED  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLOW DIRECTION AND SPECIFICATION:  
 COUNTERCURRENT HEAT EXCHANGER  
 SPECIFIED COLD TEMP CHANGE  
 SPECIFIED VALUE C 60.0000  
 LMTD CORRECTION FACTOR 1.00000

PRESSURE SPECIFICATION:  
 HOT SIDE OUTLET PRESSURE BAR 35.4638  
 COLD SIDE PRESSURE DROP BAR 0.3447

HEAT TRANSFER COEFFICIENT SPECIFICATION:  
 HOT LIQUID COLD LIQUID CAL/SEC-SQCM-K 0.0203  
 HOT 2-PHASE COLD LIQUID CAL/SEC-SQCM-K 0.0203  
 HOT VAPOR COLD LIQUID CAL/SEC-SQCM-K 0.0203  
 HOT LIQUID COLD 2-PHASE CAL/SEC-SQCM-K 0.0203  
 HOT 2-PHASE COLD 2-PHASE CAL/SEC-SQCM-K 0.0203  
 HOT VAPOR COLD 2-PHASE CAL/SEC-SQCM-K 0.0203  
 HOT LIQUID COLD VAPOR CAL/SEC-SQCM-K 0.0203  
 HOT 2-PHASE COLD VAPOR CAL/SEC-SQCM-K 0.0203  
 HOT VAPOR COLD VAPOR CAL/SEC-SQCM-K 0.0203

\*\*\* OVERALL RESULTS \*\*\*

STREAMS:

```

-----|-----
31      ----->|          HOT          |-----> 32
T=  3.6480D+02 |          |          T=
3.0560D+02     |          |          P=
P=  8.0715D+01 |          |          V=
3.5464D+01     |          |          V=
V=  1.0000D+00 |          |          V=
1.0000D+00     |          |          V=
26      <-----|          COLD          |<----- 25
T=  9.0000D+01 |          |          T=
3.0000D+01     |          |          P=
P=  3.9255D+01 |          |          P=
3.9600D+01     |          |          V=
V=  1.0000D+00 |          |          V=
1.0000D+00     |          |          V=
-----|-----

```

DUTY AND AREA:  
 CALCULATED HEAT DUTY CAL/SEC 319717.4714  
 CALCULATED (REQUIRED) AREA SQM 5.6991  
 ACTUAL EXCHANGER AREA SQM 5.6991  
 PER CENT OVER-DESIGN 0.0000

HEAT TRANSFER COEFFICIENT:

AVERAGE COEFFICIENT (DIRTY)      CAL/SEC-SQCM-K      0.0203  
 UA (DIRTY)      CAL/SEC-K      1157.0230

LOG-MEAN TEMPERATURE DIFFERENCE:  
 LMTD CORRECTION FACTOR      1.0000  
 LMTD (CORRECTED)      C      276.3277  
 NUMBER OF SHELLS IN SERIES      1

PRESSURE DROP:  
 HOTSIDE, TOTAL      BAR      45.2515  
 COLDSIDE, TOTAL      BAR      0.3447

\*\*\* ZONE RESULTS \*\*\*

TEMPERATURE LEAVING EACH ZONE:

```

                                HOT
-----
HOT IN |                               |
HOT OUT |                               |
-----> |                               |
---> |                               |
 364.8 |                               |
305.6 |                               |
      |                               |
COLDOUT |                               |
COLDIN |                               |
<----- |                               |
---- |                               |
  90.0 |                               |
30.0 |                               |
      |                               |
-----
                                COLD
  
```

ZONE HEAT TRANSFER AND AREA:

ZONE	HEAT DUTY CAL/SEC	AREA SQM	LMTD C	AVERAGE U CAL/SEC-SQCM-K	UA
1	319717.471	5.6991	276.3277	0.0203	1157.0230

HEATX COLD-TQCU HB-HXA-1 TQCURV INLET

```

-----
PRESSURE PROFILE:      CONSTANT2
PRESSURE DROP:      -0.3447      BAR
PROPERTY OPTION SET:      SRK      SOAVE-REDLICH-KWONG EQUATION OF STATE
FREE WATER OPTION SET:      SYSOP12      ASME STEAM TABLE
SOLUBLE WATER OPTION:      THE MAIN PROPERTY OPTION SET (SRK      ).
  
```

-----  
 ! DUTY      ! PRES      ! TEMP      ! VFRAC      !

CAL/SEC	BAR	C	
0.0	39.6000	90.0869	1.0000
1.5225+04	39.6000	87.2080	1.0000
3.0449+04	39.6000	84.3298	1.0000
4.5674+04	39.6000	81.4525	1.0000
6.0899+04	39.6000	78.5762	1.0000
7.6123+04	39.6000	75.7010	1.0000
9.1348+04	39.6000	72.8271	1.0000
1.0657+05	39.6000	69.9547	1.0000
1.2180+05	39.6000	67.0839	1.0000
1.3702+05	39.6000	64.2148	1.0000
1.5225+05	39.6000	61.3478	1.0000
1.6747+05	39.6000	58.4828	1.0000
1.8270+05	39.6000	55.6203	1.0000
1.9792+05	39.6000	52.7603	1.0000
2.1314+05	39.6000	49.9030	1.0000
2.2837+05	39.6000	47.0487	1.0000
2.4359+05	39.6000	44.1977	1.0000
2.5882+05	39.6000	41.3501	1.0000
2.7404+05	39.6000	38.5063	1.0000
2.8927+05	39.6000	35.6665	1.0000
3.0449+05	39.6000	32.8309	1.0000
3.1972+05	39.6000	30.0000	1.0000

HEATX HOT-TQCUR HB-HXA-1 TQCURV INLET

PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: 0.0 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 FREE WATER OPTION SET: SYSOP12 ASME STEAM TABLE  
 SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK ).

DUTY	PRES	TEMP	VFRAC
CAL/SEC	BAR	C	
0.0	80.7153	367.0603	1.0000
1.5225+04	80.7153	364.3226	1.0000
3.0449+04	80.7153	361.5829	1.0000
4.5674+04	80.7153	358.8415	1.0000



! 6.0899+04 !	80.7153 !	356.0981 !	1.0000 !
! 7.6123+04 !	80.7153 !	353.3530 !	1.0000 !
! 9.1348+04 !	80.7153 !	350.6060 !	1.0000 !
! 1.0657+05 !	80.7153 !	347.8572 !	1.0000 !
! 1.2180+05 !	80.7153 !	345.1067 !	1.0000 !
! 1.3702+05 !	80.7153 !	342.3543 !	1.0000 !
! 1.5225+05 !	80.7153 !	339.6002 !	1.0000 !
! 1.6747+05 !	80.7153 !	336.8444 !	1.0000 !
! 1.8270+05 !	80.7153 !	334.0868 !	1.0000 !
! 1.9792+05 !	80.7153 !	331.3275 !	1.0000 !
! 2.1314+05 !	80.7153 !	328.5665 !	1.0000 !
! 2.2837+05 !	80.7153 !	325.8038 !	1.0000 !
! 2.4359+05 !	80.7153 !	323.0395 !	1.0000 !
! 2.5882+05 !	80.7153 !	320.2735 !	1.0000 !
! 2.7404+05 !	80.7153 !	317.5058 !	1.0000 !
! 2.8927+05 !	80.7153 !	314.7366 !	1.0000 !
! 3.0449+05 !	80.7153 !	311.9658 !	1.0000 !
! 3.1972+05 !	80.7153 !	309.1934 !	1.0000 !

BLOCK: HB-HXA-2 MODEL: HEATX

HOT SIDE:

INLET STREAM: 29  
 OUTLET STREAM: 30  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 FREE WATER OPTION SET: SYSOP12 ASME STEAM TABLE  
 SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK ).

COLD SIDE:  
 INLET STREAM: 27  
 OUTLET STREAM: 28  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 FREE WATER OPTION SET: SYSOP12 ASME STEAM TABLE  
 SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK ).

	*** MASS AND ENERGY BALANCE ***	***	RELATIVE
DIFF.	IN	OUT	
TOTAL BALANCE			
MOLE (KMOL/HR )	4503.92	4503.92	0.00000
MASS (KG/HR )	75650.8	75650.8	0.00000
ENTHALPY (CAL/SEC )	-0.251406E+07	-0.251406E+07	

0.185223E-15

*** CO2 EQUIVALENT SUMMARY ***		
FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR

UTILITIES CO2E PRODUCTION 0.00000 KG/HR  
 TOTAL CO2E PRODUCTION 0.00000 KG/HR

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR HOT SIDE:

TWO PHASE FLASH  
 FREE WATER CONSIDERED  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLASH SPECS FOR COLD SIDE:

TWO PHASE FLASH  
 FREE WATER CONSIDERED  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLOW DIRECTION AND SPECIFICATION:

COUNTERCURRENT HEAT EXCHANGER  
 SPECIFIED COLD OUTLET TEMP  
 SPECIFIED VALUE C 225.0000  
 LMTD CORRECTION FACTOR 1.00000

PRESSURE SPECIFICATION:

HOT SIDE PRESSURE DROP BAR 0.0000  
 COLD SIDE PRESSURE DROP BAR 0.3447

HEAT TRANSFER COEFFICIENT SPECIFICATION:

HOT LIQUID	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD VAPOR	CAL/SEC-SQCM-K	0.0203

\*\*\* OVERALL RESULTS \*\*\*

STREAMS:

```

-----|-----|-----
29      ----->|          HOT          |-----> 30
T= 4.0000D+02 |          |          |          T=
3.6707D+02     |          |          |
P= 8.1060D+01 |          |          |          P=
8.1060D+01     |          |          |
V= 1.0000D+00 |          |          |          V=
1.0000D+00     |          |          |
28      <-----|          COLD          |<----- 27
T= 2.2500D+02 |          |          |          T=
1.9260D+02     |          |          |

```

P= 8.0715D+01 | | P=  
8.1060D+01  
V= 1.0000D+00 | | V=  
1.0000D+00

DUTY AND AREA:

CALCULATED HEAT DUTY	CAL/SEC	178955.3759
CALCULATED (REQUIRED) AREA	SQM	5.0446
ACTUAL EXCHANGER AREA	SQM	5.0446
PER CENT OVER-DESIGN		0.0000

HEAT TRANSFER COEFFICIENT:

AVERAGE COEFFICIENT (DIRTY)	CAL/SEC-SQCM-K	0.0203
UA (DIRTY)	CAL/SEC-K	1024.1444

LOG-MEAN TEMPERATURE DIFFERENCE:

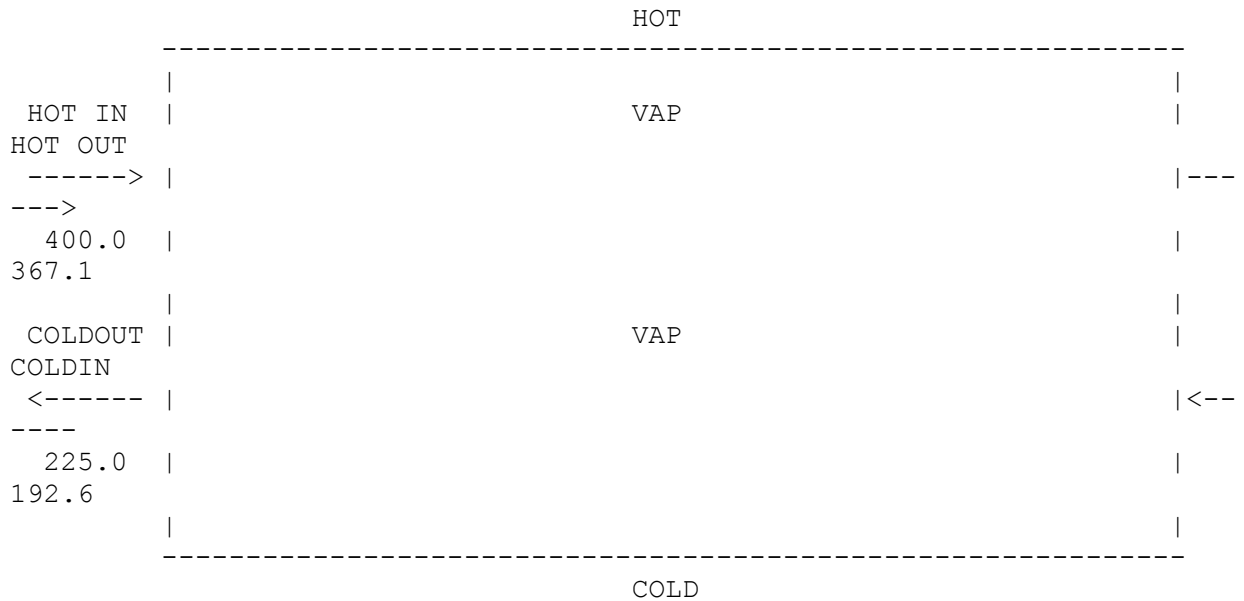
LMTD CORRECTION FACTOR		1.0000
LMTD (CORRECTED)	C	174.7365
NUMBER OF SHELLS IN SERIES		1

PRESSURE DROP:

HOTSIDE, TOTAL	BAR	0.0000
COLD SIDE, TOTAL	BAR	0.3447

\*\*\* ZONE RESULTS \*\*\*

TEMPERATURE LEAVING EACH ZONE:



ZONE HEAT TRANSFER AND AREA:

ZONE	HEAT DUTY	AREA	LMTD	AVERAGE U	UA
CAL/SEC-K	CAL/SEC	SQM	C	CAL/SEC-SQCM-K	

1 178955.376 5.0446 174.7365 0.0203  
 1024.1444

HEATX COLD-TQCU HB-HXA-2 TQCURV INLET

-----  
 PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: -0.3447 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 FREE WATER OPTION SET: SYSOP12 ASME STEAM TABLE  
 SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK ).

-----

! DUTY	! PRES	! TEMP	! VFRAC	!
!	!	!	!	!
!	!	!	!	!
!	!	!	!	!
! CAL/SEC	! BAR	! C	!	!
!	!	!	!	!
! =====	! =====	! =====	! =====	! =====
! 0.0	! 81.0600	! 225.0326	! 1.0000	!
! 8521.6846	! 81.0600	! 223.4893	! 1.0000	!
! 1.7043+04	! 81.0600	! 221.9457	! 1.0000	!
! 2.5565+04	! 81.0600	! 220.4020	! 1.0000	!
! 3.4087+04	! 81.0600	! 218.8581	! 1.0000	!
! -----	! -----	! -----	! -----	! -----
! 4.2608+04	! 81.0600	! 217.3141	! 1.0000	!
! 5.1130+04	! 81.0600	! 215.7699	! 1.0000	!
! 5.9652+04	! 81.0600	! 214.2256	! 1.0000	!
! 6.8173+04	! 81.0600	! 212.6812	! 1.0000	!
! 7.6695+04	! 81.0600	! 211.1366	! 1.0000	!
! -----	! -----	! -----	! -----	! -----
! 8.5217+04	! 81.0600	! 209.5919	! 1.0000	!
! 9.3739+04	! 81.0600	! 208.0471	! 1.0000	!
! 1.0226+05	! 81.0600	! 206.5022	! 1.0000	!
! 1.1078+05	! 81.0600	! 204.9573	! 1.0000	!
! 1.1930+05	! 81.0600	! 203.4122	! 1.0000	!
! -----	! -----	! -----	! -----	! -----
! 1.2783+05	! 81.0600	! 201.8671	! 1.0000	!
! 1.3635+05	! 81.0600	! 200.3219	! 1.0000	!
! 1.4487+05	! 81.0600	! 198.7766	! 1.0000	!
! 1.5339+05	! 81.0600	! 197.2314	! 1.0000	!
! 1.6191+05	! 81.0600	! 195.6860	! 1.0000	!
! -----	! -----	! -----	! -----	! -----
! 1.7043+05	! 81.0600	! 194.1407	! 1.0000	!
! 1.7896+05	! 81.0600	! 192.5954	! 1.0000	!

-----

HEATX HOT-TQCUR HB-HXA-2 TQCURV INLET

-----  
 PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: 0.0 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 FREE WATER OPTION SET: SYSOP12 ASME STEAM TABLE  
 SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK ).

DUTY	PRES	TEMP	VFRAC
CAL/SEC	BAR	C	
0.0	81.0600	400.0000	1.0000
8521.6846	81.0600	398.4383	1.0000
1.7043+04	81.0600	396.8759	1.0000
2.5565+04	81.0600	395.3129	1.0000
3.4087+04	81.0600	393.7493	1.0000
4.2608+04	81.0600	392.1850	1.0000
5.1130+04	81.0600	390.6200	1.0000
5.9652+04	81.0600	389.0544	1.0000
6.8173+04	81.0600	387.4881	1.0000
7.6695+04	81.0600	385.9212	1.0000
8.5217+04	81.0600	384.3537	1.0000
9.3739+04	81.0600	382.7855	1.0000
1.0226+05	81.0600	381.2166	1.0000
1.1078+05	81.0600	379.6472	1.0000
1.1930+05	81.0600	378.0771	1.0000
1.2783+05	81.0600	376.5063	1.0000
1.3635+05	81.0600	374.9349	1.0000
1.4487+05	81.0600	373.3629	1.0000
1.5339+05	81.0600	371.7903	1.0000
1.6191+05	81.0600	370.2170	1.0000
1.7043+05	81.0600	368.6431	1.0000
1.7896+05	81.0600	367.0686	1.0000

BLOCK: HB-HXA-3 MODEL: HEATX

HOT SIDE:

INLET STREAM: 30  
 OUTLET STREAM: 31  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 FREE WATER OPTION SET: SYSOP12 ASME STEAM TABLE  
 SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK ).  
 COLD SIDE:

INLET STREAM: 38  
 OUTLET STREAM: 40  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 FREE WATER OPTION SET: SYSOP12 ASME STEAM TABLE  
 SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK ).

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	2263.49	2263.49	0.00000
MASS (KG/HR )	38633.1	38633.1	0.00000
ENTHALPY (CAL/SEC )	-0.286797E+07	-0.286797E+07	
0.324732E-15			

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR HOT SIDE:

TWO PHASE FLASH	
FREE WATER CONSIDERED	
MAXIMUM NO. ITERATIONS	30
CONVERGENCE TOLERANCE	0.000100000

FLASH SPECS FOR COLD SIDE:

TWO PHASE FLASH	
FREE WATER CONSIDERED	
MAXIMUM NO. ITERATIONS	30
CONVERGENCE TOLERANCE	0.000100000

FLOW DIRECTION AND SPECIFICATION:

COUNTERCURRENT HEAT EXCHANGER	
SPECIFIED COLD OUTLET TEMP	
SPECIFIED VALUE	C 32.2222
LMTD CORRECTION FACTOR	1.00000

PRESSURE SPECIFICATION:

HOT SIDE PRESSURE DROP	BAR	0.3447
COLD SIDE PRESSURE DROP	BAR	0.0000

HEAT TRANSFER COEFFICIENT SPECIFICATION:

HOT LIQUID	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD VAPOR	CAL/SEC-SQCM-K	0.0203

\*\*\* OVERALL RESULTS \*\*\*

STREAMS :

```

-----
      30      -----> |                | |-----> 31
      T= 3.6707D+02 |                | |                | T=
3.6480D+02          |                | |                |
      P= 8.1060D+01 |                | |                | P=
8.0715D+01          |                | |                |
      V= 1.0000D+00 |                | |                | V=
1.0000D+00          |                | |                |
      40      <----- |                | |<----- 38
      T= 3.2222D+01 |                | |                | T=
7.2222D+00          |                | |                |
      P= 1.0000D+00 |                | |                | P=
1.0000D+00          |                | |                |
      V= 0.0000D+00 |                | |                | V=
0.0000D+00          |                | |                |
-----

```

```

DUTY AND AREA:
CALCULATED HEAT DUTY          CAL/SEC          12156.9779
CALCULATED (REQUIRED) AREA    SQM              0.1730
ACTUAL EXCHANGER AREA        SQM              0.1730
PER CENT OVER-DESIGN          0.0000

```

```

HEAT TRANSFER COEFFICIENT:
AVERAGE COEFFICIENT (DIRTY)  CAL/SEC-SQCM-K   0.0203
UA (DIRTY)                    CAL/SEC-K        35.1267

```

```

LOG-MEAN TEMPERATURE DIFFERENCE:
LMTD CORRECTION FACTOR              1.0000
LMTD (CORRECTED)                     C          346.0898
NUMBER OF SHELLS IN SERIES            1

```

```

PRESSURE DROP:
HOTSIDE, TOTAL                      BAR          0.3447
COLD SIDE, TOTAL                     BAR          0.0000

```

\*\*\* ZONE RESULTS \*\*\*

TEMPERATURE LEAVING EACH ZONE:

```

                                HOT
-----
HOT IN |                | |
HOT OUT |                | |
-----> |                | |-----
---> |                | |
 367.1 |                | |
364.8  |                | |
      |                | |
COLDOUT |                | |
COLDIN  |                | |
                                LIQ

```

```

<----- | |<--
-----
32.2 | |
7.2 | |
| |
-----

```

COLD

ZONE HEAT TRANSFER AND AREA:

ZONE	HEAT DUTY CAL/SEC	AREA SQM	LMTD C	AVERAGE U CAL/SEC-SQCM-K	UA
1	12156.978	0.1730	346.0898	0.0203	
CAL/SEC-K	35.1267				

HEATX COLD-TQCU HB-HXA-3 TQCURV INLET

```

-----
PRESSURE PROFILE:      CONSTANT2
PRESSURE DROP:        0.0          BAR
PROPERTY OPTION SET:  SRK          SOAVE-REDLICH-KWONG EQUATION OF STATE
FREE WATER OPTION SET: SYSOP12    ASME STEAM TABLE
SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK      ).

```

```

-----
! DUTY      ! PRES      ! TEMP      ! VFRAC     !
!           !           !           !           !
!           !           !           !           !
! CAL/SEC   ! BAR       ! C         !           !
!           !           !           !           !
!=====!=====!=====!=====!
! 0.0       ! 1.0000   ! 32.2222  ! 0.0       !
! 578.9037  ! 1.0000   ! 31.0299  ! 0.0       !
! 1157.8074 ! 1.0000   ! 29.8377  ! 0.0       !
! 1736.7111 ! 1.0000   ! 28.6455  ! 0.0       !
! 2315.6148 ! 1.0000   ! 27.4534  ! 0.0       !
!-----!-----!-----!-----!
! 2894.5185 ! 1.0000   ! 26.2614  ! 0.0       !
! 3473.4223 ! 1.0000   ! 25.0695  ! 0.0       !
! 4052.3260 ! 1.0000   ! 23.8778  ! 0.0       !
! 4631.2297 ! 1.0000   ! 22.6862  ! 0.0       !
! 5210.1334 ! 1.0000   ! 21.4947  ! 0.0       !
!-----!-----!-----!-----!
! 5789.0371 ! 1.0000   ! 20.3035  ! 0.0       !
! 6367.9408 ! 1.0000   ! 19.1125  ! 0.0       !
! 6946.8445 ! 1.0000   ! 17.9217  ! 0.0       !
! 7525.7482 ! 1.0000   ! 16.7312  ! 0.0       !
! 8104.6519 ! 1.0000   ! 15.5411  ! 0.0       !
!-----!-----!-----!-----!
! 8683.5556 ! 1.0000   ! 14.3512  ! 0.0       !
! 9262.4593 ! 1.0000   ! 13.1618  ! 0.0       !
! 9841.3630 ! 1.0000   ! 11.9728  ! 0.0       !
! 1.0420+04 ! 1.0000   ! 10.7843  ! 0.0       !

```



! 1.0999+04 !	1.0000 !	9.5964 !	0.0 !
! 1.1578+04 !	1.0000 !	8.4090 !	0.0 !
! 1.2157+04 !	1.0000 !	7.2222 !	0.0 !

HEATX HOT-TQCUR HB-HXA-3 TQCURV INLET

PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: 0.0 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 FREE WATER OPTION SET: SYSOP12 ASME STEAM TABLE  
 SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK ).

DUTY	PRES	TEMP	VFRAC
CAL/SEC	BAR	C	
0.0	81.0600	367.0686	1.0000
578.9037	81.0600	366.9616	1.0000
1157.8074	81.0600	366.8546	1.0000
1736.7111	81.0600	366.7476	1.0000
2315.6148	81.0600	366.6407	1.0000
2894.5185	81.0600	366.5337	1.0000
3473.4223	81.0600	366.4267	1.0000
4052.3260	81.0600	366.3197	1.0000
4631.2297	81.0600	366.2127	1.0000
5210.1334	81.0600	366.1056	1.0000
5789.0371	81.0600	365.9986	1.0000
6367.9408	81.0600	365.8916	1.0000
6946.8445	81.0600	365.7846	1.0000
7525.7482	81.0600	365.6776	1.0000
8104.6519	81.0600	365.5706	1.0000
8683.5556	81.0600	365.4635	1.0000
9262.4593	81.0600	365.3565	1.0000
9841.3630	81.0600	365.2495	1.0000
1.0420+04	81.0600	365.1425	1.0000
1.0999+04	81.0600	365.0354	1.0000
1.1578+04	81.0600	364.9284	1.0000
1.2157+04	81.0600	364.8213	1.0000

BLOCK: HB-HXA-4 MODEL: HEATX

HOT SIDE:

INLET STREAM: 32  
 OUTLET STREAM: 33  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 FREE WATER OPTION SET: SYSOP12 ASME STEAM TABLE  
 SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK ).  
 COLD SIDE:  
 -----

INLET STREAM: 39  
 OUTLET STREAM: 41  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 FREE WATER OPTION SET: SYSOP12 ASME STEAM TABLE  
 SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK ).

\*\*\* MASS AND ENERGY BALANCE \*\*\*  
 IN OUT RELATIVE

DIFF.

TOTAL BALANCE			
MOLE (KMOL/HR )	3504.70	3504.70	0.00000
MASS (KG/HR )	61370.8	61370.8	0.00000
ENTHALPY (CAL/SEC )	-0.256879E+08	-0.256879E+08	-

0.145021E-15

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	0.00000	KG/HR
TOTAL CO2E PRODUCTION	0.00000	KG/HR

\*\*\* INPUT DATA \*\*\*

FLASH SPECS FOR HOT SIDE:

TWO PHASE FLASH  
 FREE WATER CONSIDERED  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLASH SPECS FOR COLD SIDE:

TWO PHASE FLASH  
 FREE WATER CONSIDERED  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

FLOW DIRECTION AND SPECIFICATION:

COUNTERCURRENT HEAT EXCHANGER  
 SPECIFIED COLD OUTLET TEMP  
 SPECIFIED VALUE C 32.2222  
 LMTD CORRECTION FACTOR 1.00000

PRESSURE SPECIFICATION:

HOT SIDE PRESSURE DROP BAR 0.3447  
 COLD SIDE PRESSURE DROP BAR 0.0000

HEAT TRANSFER COEFFICIENT SPECIFICATION:

HOT LIQUID	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD LIQUID	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD 2-PHASE	CAL/SEC-SQCM-K	0.0203
HOT LIQUID	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT 2-PHASE	COLD VAPOR	CAL/SEC-SQCM-K	0.0203
HOT VAPOR	COLD VAPOR	CAL/SEC-SQCM-K	0.0203

\*\*\* OVERALL RESULTS \*\*\*

STREAMS:

```

-----|-----|-----
32      <----->|          HOT          |>-----> 33
T=  3.0560D+02 |          |          |          T=
2.7567D+02      |          |          |          P=
P=  3.5464D+01 |          |          |          V=
3.5119D+01      |          |          |          V=
V=  1.0000D+00 |          |          |          V=
1.0000D+00      |          |          |          V=

41      <----->|          COLD          |<-----> 39
T=  3.2222D+01 |          |          |          T=
7.2222D+00      |          |          |          P=
P=  1.0000D+00 |          |          |          P=
1.0000D+00      |          |          |          V=
V=  0.0000D+00 |          |          |          V=
0.0000D+00      |          |          |          V=
-----|-----|-----

```

DUTY AND AREA:

CALCULATED HEAT DUTY	CAL/SEC	159482.3609
CALCULATED (REQUIRED) AREA	SQM	2.8997
ACTUAL EXCHANGER AREA	SQM	2.8997
PER CENT OVER-DESIGN		0.0000

HEAT TRANSFER COEFFICIENT:

AVERAGE COEFFICIENT (DIRTY)	CAL/SEC-SQCM-K	0.0203
UA (DIRTY)	CAL/SEC-K	588.7042

LOG-MEAN TEMPERATURE DIFFERENCE:

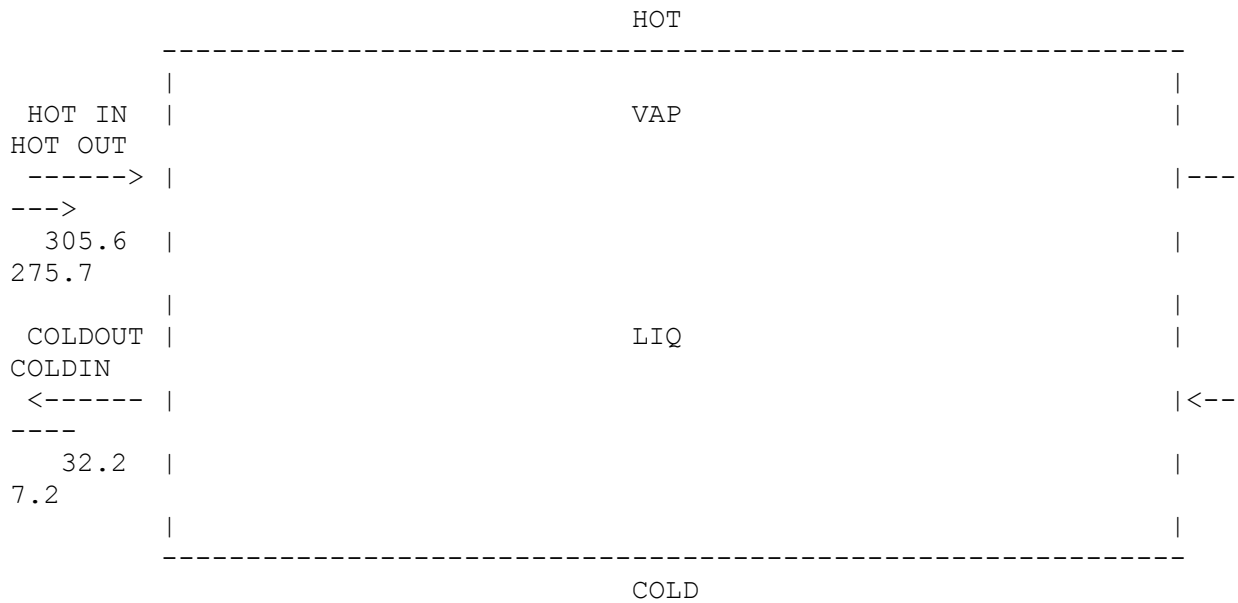
LMTD CORRECTION FACTOR		1.0000
LMTD (CORRECTED)	C	270.9040
NUMBER OF SHELLS IN SERIES		1

PRESSURE DROP:

HOTSIDE, TOTAL	BAR	0.3447
COLD SIDE, TOTAL	BAR	0.0000

\*\*\* ZONE RESULTS \*\*\*

TEMPERATURE LEAVING EACH ZONE:



ZONE HEAT TRANSFER AND AREA:

ZONE	HEAT DUTY CAL/SEC	AREA SQM	LMTD C	AVERAGE U CAL/SEC-SQCM-K	UA
1	159482.361	2.8997	270.9040	0.0203	588.7042

HEATX COLD-TQCU HB-HXA-4 TQCURV INLET

```

-----
PRESSURE PROFILE:      CONSTANT2
PRESSURE DROP:        0.0      BAR
PROPERTY OPTION SET:  SRK      SOAVE-REDLICH-KWONG EQUATION OF STATE
FREE WATER OPTION SET: SYSOP12 ASME STEAM TABLE
SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK      ).

```

```

-----
! DUTY      ! PRES      ! TEMP      ! VFRAC     !
!           !           !           !           !
!           !           !           !           !
! CAL/SEC   ! BAR       ! C         !           !
!           !           !           !           !
!=====!=====!=====!=====!
! 0.0      ! 1.0000   ! 32.2222  ! 0.0       !
! 7594.3981 ! 1.0000   ! 31.0299  ! 0.0       !
! 1.5189+04 ! 1.0000   ! 29.8377  ! 0.0       !
! 2.2783+04 ! 1.0000   ! 28.6455  ! 0.0       !
! 3.0378+04 ! 1.0000   ! 27.4534  ! 0.0       !
!-----!-----!-----!-----!
! 3.7972+04 ! 1.0000   ! 26.2614  ! 0.0       !
! 4.5566+04 ! 1.0000   ! 25.0695  ! 0.0       !
! 5.3161+04 ! 1.0000   ! 23.8778  ! 0.0       !

```

! 6.0755+04 !	1.0000 !	22.6862 !	0.0 !
! 6.8350+04 !	1.0000 !	21.4947 !	0.0 !
! 7.5944+04 !	1.0000 !	20.3035 !	0.0 !
! 8.3538+04 !	1.0000 !	19.1125 !	0.0 !
! 9.1133+04 !	1.0000 !	17.9217 !	0.0 !
! 9.8727+04 !	1.0000 !	16.7312 !	0.0 !
! 1.0632+05 !	1.0000 !	15.5411 !	0.0 !
! 1.1392+05 !	1.0000 !	14.3512 !	0.0 !
! 1.2151+05 !	1.0000 !	13.1618 !	0.0 !
! 1.2910+05 !	1.0000 !	11.9728 !	0.0 !
! 1.3670+05 !	1.0000 !	10.7843 !	0.0 !
! 1.4429+05 !	1.0000 !	9.5964 !	0.0 !
! 1.5189+05 !	1.0000 !	8.4090 !	0.0 !
! 1.5948+05 !	1.0000 !	7.2222 !	0.0 !

HEATX HOT-TQCUR HB-HXA-4 TQCURV INLET

PRESSURE PROFILE: CONSTANT2  
 PRESSURE DROP: 0.0 BAR  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 FREE WATER OPTION SET: SYSOP12 ASME STEAM TABLE  
 SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK ).

! DUTY !	! PRES !	! TEMP !	! VFRAC !
! CAL/SEC !	! BAR !	! C !	! !
! 0.0 !	35.4637 !	305.5963 !	1.0000 !
! 7594.3981 !	35.4637 !	304.1792 !	1.0000 !
! 1.5189+04 !	35.4637 !	302.7614 !	1.0000 !
! 2.2783+04 !	35.4637 !	301.3430 !	1.0000 !
! 3.0378+04 !	35.4637 !	299.9240 !	1.0000 !
! 3.7972+04 !	35.4637 !	298.5043 !	1.0000 !
! 4.5566+04 !	35.4637 !	297.0841 !	1.0000 !
! 5.3161+04 !	35.4637 !	295.6632 !	1.0000 !
! 6.0755+04 !	35.4637 !	294.2417 !	1.0000 !
! 6.8350+04 !	35.4637 !	292.8196 !	1.0000 !
! 7.5944+04 !	35.4637 !	291.3969 !	1.0000 !
! 8.3538+04 !	35.4637 !	289.9736 !	1.0000 !
! 9.1133+04 !	35.4637 !	288.5497 !	1.0000 !
! 9.8727+04 !	35.4637 !	287.1251 !	1.0000 !
! 1.0632+05 !	35.4637 !	285.7000 !	1.0000 !
! 1.1392+05 !	35.4637 !	284.2742 !	1.0000 !

```

! 1.2151+05 ! 35.4637 ! 282.8478 ! 1.0000 !
! 1.2910+05 ! 35.4637 ! 281.4209 ! 1.0000 !
! 1.3670+05 ! 35.4637 ! 279.9933 ! 1.0000 !
! 1.4429+05 ! 35.4637 ! 278.5651 ! 1.0000 !
!-----+-----+-----+-----!
! 1.5189+05 ! 35.4637 ! 277.1363 ! 1.0000 !
! 1.5948+05 ! 35.4637 ! 275.7069 ! 1.0000 !
-----

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BLOCK: HB-RXN MODEL: RSTOIC

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-----
INLET STREAM:      28
OUTLET STREAM:    29
PROPERTY OPTION SET: SRK          SOAVE-REDLICH-KWONG EQUATION OF STATE
FREE WATER OPTION SET: SYSOP12   ASME STEAM TABLE
SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK      ).

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*** MASS AND ENERGY BALANCE ***
          IN          OUT          GENERATION    RELATIVE
DIFF.
TOTAL BALANCE
MOLE (KMOL/HR )          2337.80          2166.13          -93.5916
0.333991E-01
MASS (KG/HR )           38771.7           36879.1
0.488147E-01
ENTHALPY (CAL/SEC )     -0.150106E+07    -834047.          -
0.444362

```

```

*** CO2 EQUIVALENT SUMMARY ***
FEED STREAMS CO2E          0.00000          KG/HR
PRODUCT STREAMS CO2E       0.00000          KG/HR
NET STREAMS CO2E PRODUCTION 0.00000          KG/HR
UTILITIES CO2E PRODUCTION  891.111          KG/HR
TOTAL CO2E PRODUCTION      891.111          KG/HR

```

```

*** INPUT DATA ***
STOICHIOMETRY MATRIX:

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REACTION # 1:
SUBSTREAM MIXED :
AMMONIA 2.00 N2 -1.00 H2 -3.00

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REACTION CONVERSION SPECS: NUMBER= 1
REACTION # 1:
SUBSTREAM:MIXED KEY COMP:H2 CONV FRAC: 0.2000

```

```

TWO PHASE TP FLASH
FREE WATER CONSIDERED
SPECIFIED TEMPERATURE C 400.000
SPECIFIED PRESSURE BAR 81.0600

```

MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000  
 SIMULTANEOUS REACTIONS  
 GENERATE COMBUSTION REACTIONS FOR FEED SPECIES NO

\*\*\* RESULTS \*\*\*

OUTLET TEMPERATURE C 400.00  
 OUTLET PRESSURE BAR 81.060  
 HEAT DUTY CAL/SEC 0.61354E+06  
 VAPOR FRACTION 1.0000  
 1ST LIQUID/TOTAL LIQUID 1.0000

REACTION EXTENTS:

REACTION NUMBER	REACTION EXTENT KMOL/HR
1	46.796

V-L1-L2 PHASE EQUILIBRIUM :

K2 (I)	COMP	F (I)	X1 (I)	X2 (I)	Y (I)	K1 (I)
	AMMONIA	0.403	0.403	0.00	0.403	
	N2	0.322	0.322	0.00	0.322	
	H2	0.259	0.259	0.00	0.259	
	ARGON	0.151E-01	0.151E-01	0.00	0.151E-01	

\*\*\* ASSOCIATED UTILITIES \*\*\*

UTILITY ID FOR ELECTRICITY	U-3
RATE OF CONSUMPTION	2568.7607 KW
COST	199.0790 \$/HR
CO2 EQUIVALENT EMISSIONS	891.1110 KG/HR

BLOCK: HB-S-01 MODEL: FLASH2

-----  
 INLET STREAM: 24  
 OUTLET VAPOR STREAM: 25  
 OUTLET LIQUID STREAM: 34  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 FREE WATER OPTION SET: SYSOP12 ASME STEAM TABLE  
 SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK ).

\*\*\* MASS AND ENERGY BALANCE \*\*\*

DIFF.	IN	OUT	RELATIVE
TOTAL BALANCE			
MOLE (KMOL/HR )	2428.76	2428.76	
0.187234E-15			
MASS (KG/HR )	40323.3	40323.3	-
0.858535E-12			
ENTHALPY (CAL/SEC )	-0.151155E+07	-0.291559E+07	0.481564

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	2039.25	KG/HR
TOTAL CO2E PRODUCTION	2039.25	KG/HR

\*\*\* INPUT DATA \*\*\*

TWO PHASE TP FLASH  
 FREE WATER CONSIDERED  
 SPECIFIED TEMPERATURE C 30.0000  
 SPECIFIED PRESSURE BAR 39.6000  
 MAXIMUM NO. ITERATIONS 30  
 CONVERGENCE TOLERANCE 0.000100000

\*\*\* RESULTS \*\*\*

OUTLET TEMPERATURE C 30.000  
 OUTLET PRESSURE BAR 39.600  
 HEAT DUTY CAL/SEC -0.14040E+07  
 VAPOR FRACTION 0.96255  
 1ST LIQUID/TOTAL LIQUID 1.0000

V-L1-L2 PHASE EQUILIBRIUM :

COMP	F(I)	X1(I)	X2(I)	Y(I)	K1(I)
K2(I)					
AMMONIA	0.370	0.994	0.00	0.346	0.348
N2	0.327	0.370E-02	0.00	0.340	91.7
H2	0.289	0.160E-02	0.00	0.300	188.
ARGON	0.140E-01	0.429E-03	0.00	0.145E-01	33.8

\*\*\* ASSOCIATED UTILITIES \*\*\*

UTILITY ID FOR ELECTRICITY U-3  
 RATE OF CONSUMPTION 5878.4438 KW  
 COST 455.5794 \$/HR  
 CO2 EQUIVALENT EMISSIONS 2039.2502 KG/HR

BLOCK: HB-S-02 MODEL: FLASH2

-----  
 INLET STREAM: 34  
 OUTLET VAPOR STREAM: 35  
 OUTLET LIQUID STREAM: OUT  
 PROPERTY OPTION SET: SRK SOAVE-REDLICH-KWONG EQUATION OF STATE  
 FREE WATER OPTION SET: SYSOP12 ASME STEAM TABLE  
 SOLUBLE WATER OPTION: THE MAIN PROPERTY OPTION SET (SRK ).

\*\*\* MASS AND ENERGY BALANCE \*\*\*

	IN	OUT	RELATIVE
DIFF.			
TOTAL BALANCE			
MOLE (KMOL/HR )	90.9664	90.9664	0.00000
MASS (KG/HR )	1551.62	1551.62	

0.735774E-12



ENTHALPY (CAL/SEC ) -400406. -402095.  
0.420028E-02

\*\*\* CO2 EQUIVALENT SUMMARY \*\*\*

FEED STREAMS CO2E	0.00000	KG/HR
PRODUCT STREAMS CO2E	0.00000	KG/HR
NET STREAMS CO2E PRODUCTION	0.00000	KG/HR
UTILITIES CO2E PRODUCTION	2.45300	KG/HR
TOTAL CO2E PRODUCTION	2.45300	KG/HR

\*\*\* INPUT DATA \*\*\*

TWO PHASE TP FLASH	
FREE WATER CONSIDERED	
SPECIFIED TEMPERATURE C	20.0000
SPECIFIED PRESSURE BAR	10.1325
MAXIMUM NO. ITERATIONS	30
CONVERGENCE TOLERANCE	0.000100000

\*\*\* RESULTS \*\*\*

OUTLET TEMPERATURE C	20.000
OUTLET PRESSURE BAR	10.133
HEAT DUTY CAL/SEC	-1688.9
VAPOR FRACTION	0.37988E-01
1ST LIQUID/TOTAL LIQUID	1.0000

V-L1-L2 PHASE EQUILIBRIUM :

K2(I)	COMP	F(I)	X1(I)	X2(I)	Y(I)	K1(I)
	AMMONIA	0.994	1.00	0.00	0.858	0.858
	N2	0.370E-02	0.233E-03	0.00	0.916E-01	393.
	H2	0.160E-02	0.469E-04	0.00	0.409E-01	871.
	ARGON	0.429E-03	0.716E-04	0.00	0.948E-02	132.

\*\*\* ASSOCIATED UTILITIES \*\*\*

UTILITY ID FOR ELECTRICITY	U-3
RATE OF CONSUMPTION	7.0711 KW
COST	0.5480 \$/HR
CO2 EQUIVALENT EMISSIONS	2.4530 KG/HR

## B.2.5 Ammonia Synthesis Stream Summary

23 24 25 26 27  
-----

STREAM ID	23	24	25	26	27
FROM :	B21	B4	HB-S-01	HB-HXA-1	HB-
CP-03					
TO :	B4	HB-S-01	HB-HXA-1	HB-CP-03	HB-
HXA-2					
CONV. MAX. REL. ERR:	0.0	-3.4178-03	0.0	0.0	0.0
SUBSTREAM: MIXED					
PHASE:	VAPOR	VAPOR	VAPOR	VAPOR	
VAPOR					
COMPONENTS: KMOL/HR					
AMMONIA	2.9056	898.2631	807.8182	807.8182	
807.8182					
N2	57.3503	794.4302	794.0931	794.0931	
794.0931					
H2	140.5385	702.1462	702.0008	702.0008	
702.0008					
ARGON	0.6921	33.9247	33.8856	33.8856	
33.8856					
WATER	0.0	0.0	0.0	0.0	0.0
COMPONENTS: KG/HR					
AMMONIA	49.4840	1.5298+04	1.3758+04	1.3758+04	
1.3758+04					
N2	1606.5811	2.2255+04	2.2245+04	2.2245+04	
2.2245+04					
H2	283.3087	1415.4425	1415.1494	1415.1494	
1415.1494					
ARGON	27.6487	1355.2220	1353.6625	1353.6625	
1353.6625					
WATER	0.0	0.0	0.0	0.0	0.0
TOTAL FLOW:					
KMOL/HR	201.4865	2428.7642	2337.7977	2337.7977	
2337.7977					
KG/HR	1967.0225	4.0323+04	3.8772+04	3.8772+04	
3.8772+04					
L/MIN	2233.1981	5.1244+04	2.3697+04	2.9475+04	
1.8737+04					
STATE VARIABLES:					
TEMP C	37.6133	258.8760	30.0000	90.0000	
192.5954					
PRES BAR	39.6000	35.1190	39.6000	39.2553	
81.0600					
VFRAC	1.0000	1.0000	1.0000	1.0000	
1.0000					
LFRAC	0.0	0.0	0.0	0.0	0.0
SFRAC	0.0	0.0	0.0	0.0	0.0
ENTHALPY:					

CAL/MOL	-72.4303	-2240.4691	-3873.1588	-3380.8224	-
2587.0749					
CAL/GM	-7.4192	-134.9484	-233.5378	-203.8516	-
155.9915					
CAL/SEC	-4053.8108	-1.5115+06	-2.5152+06	-2.1955+06	-
1.6800+06					
ENTROPY:					
CAL/MOL-K	-6.0069	-9.0337	-13.3370	-11.8379	-
11.3468					
CAL/GM-K	-0.6153	-0.5441	-0.8042	-0.7138	-
0.6842					
DENSITY:					
MOL/CC	1.5037-03	7.8994-04	1.6442-03	1.3219-03	
2.0795-03					
GM/CC	1.4680-02	1.3115-02	2.7269-02	2.1924-02	
3.4488-02					
AVG MW	9.7626	16.6024	16.5847	16.5847	
16.5847					

28 29 30 31 32  
 -----

STREAM ID	28	29	30	31	32
FROM :	HB-HXA-2	HB-RXN	HB-HXA-2	HB-HXA-3	HB-
HXA-1					
TO :	HB-RXN	HB-HXA-2	HB-HXA-3	HB-HXA-1	HB-
HXA-4					
CONV. MAX. REL. ERR:	6.5813-02	0.0	0.0	-5.2808-02	0.0
SUBSTREAM: MIXED					
PHASE:	VAPOR	VAPOR	VAPOR	VAPOR	
VAPOR					
COMPONENTS: KMOL/HR					
AMMONIA	807.8182	873.5322	873.5322	873.5322	
895.4369					
N2	794.0931	698.2629	698.2629	698.2629	
737.1927					
H2	702.0008	561.5493	561.5493	561.5493	
561.5867					
ARGON	33.8856	32.7816	32.7816	32.7816	
33.2336					
WATER	0.0	0.0	0.0	0.0	0.0
COMPONENTS: KG/HR					
AMMONIA	1.3758+04	1.4877+04	1.4877+04	1.4877+04	
1.5250+04					
N2	2.2245+04	1.9561+04	1.9561+04	1.9561+04	
2.0651+04					
H2	1415.1494	1132.0160	1132.0160	1132.0160	
1132.0913					
ARGON	1353.6625	1309.5581	1309.5581	1309.5581	
1327.6169					
WATER	0.0	0.0	0.0	0.0	0.0
TOTAL FLOW:					

KMOL/HR	2337.7977	2166.1259	2166.1259	2166.1259	
2227.4499					
KG/HR	3.8772+04	3.6879+04	3.6879+04	3.6879+04	
3.8361+04					
L/MIN	2.0227+04	2.5421+04	2.4149+04	2.4162+04	
5.0674+04					
STATE VARIABLES:					
TEMP C	225.0000	400.0000	367.0686	364.8045	
305.5963					
PRES BAR	80.7153	81.0600	81.0600	80.7153	
35.4637					
VFRAC	1.0000	1.0000	1.0000	1.0000	
1.0000					
LFRAC	0.0	0.0	0.0	0.0	0.0
SFRAC	0.0	0.0	0.0	0.0	0.0
ENTHALPY:					
CAL/MOL	-2311.4996	-1386.1469	-1683.5624	-1703.7667	-
2187.2785					
CAL/GM	-139.3753	-81.4166	-98.8855	-100.0722	-
127.0059					
CAL/SEC	-1.5011+06	-8.3405+05	-1.0130+06	-1.0252+06	-
1.3533+06					
ENTROPY:					
CAL/MOL-K	-10.7663	-9.4569	-9.9099	-9.9329	-
9.0742					
CAL/GM-K	-0.6492	-0.5555	-0.5821	-0.5834	-
0.5269					
DENSITY:					
MOL/CC	1.9263-03	1.4202-03	1.4950-03	1.4942-03	
7.3260-04					
GM/CC	3.1947-02	2.4179-02	2.5453-02	2.5439-02	
1.2617-02					
AVG MW	16.5847	17.0254	17.0254	17.0254	
17.2219					

33 34 35 36 37  
-----

STREAM ID	33	34	35	36	37
FROM :	HB-HXA-4	HB-S-01	HB-S-02	HB-CP-02	B20
TO :	B4	HB-S-02	HB-CP-02	B20	B21
SUBSTREAM: MIXED					
PHASE:	VAPOR	LIQUID	VAPOR	VAPOR	
VAPOR					
COMPONENTS: KMOL/HR					
AMMONIA	895.4369	90.4449	2.9649	2.9649	
2.9056					
N2	737.1927	0.3370	0.3166	0.3166	
0.3103					
H2	561.5867	0.1454	0.1413	0.1413	
0.1385					
ARGON	33.2336	3.9038-02	3.2772-02	3.2772-02	
3.2116-02					

WATER	0.0	0.0	0.0	0.0	0.0
COMPONENTS: KG/HR					
AMMONIA	1.5250+04	1540.3279	50.4939	50.4939	
49.4840					
N2	2.0651+04	9.4413	8.8696	8.8696	
8.6922					
H2	1132.0913	0.2932	0.2849	0.2849	
0.2792					
ARGON	1327.6169	1.5595	1.3092	1.3092	
1.2830					
WATER	0.0	0.0	0.0	0.0	0.0
TOTAL FLOW:					
KMOL/HR	2227.4499	90.9664	3.4556	3.4556	
3.3865					
KG/HR	3.8361+04	1551.6219	60.9575	60.9575	
59.7383					
L/MIN	4.8457+04	46.4395	128.9968	50.2032	
49.1991					
STATE VARIABLES:					
TEMP C	275.6711	30.0000	20.0000	171.0260	
171.0259					
PRES BAR	35.1190	39.6000	10.1325	39.6000	
39.6000					
VFRAC	1.0000	0.0	1.0000	1.0000	
1.0000					
LFRAC	0.0	1.0000	0.0	0.0	0.0
SFRAC	0.0	0.0	0.0	0.0	0.0
ENTHALPY:					
CAL/MOL	-2445.0335	-1.5846+04	-9566.0182	-8357.6044	-
8357.6044					
CAL/GM	-141.9727	-929.0029	-542.2868	-473.7832	-
473.7832					
CAL/SEC	-1.5128+06	-4.0041+05	-9182.3445	-8022.3977	-
7861.9497					
ENTROPY:					
CAL/MOL-K	-9.5120	-44.5577	-24.2168	-23.4255	-
23.4255					
CAL/GM-K	-0.5523	-2.6123	-1.3728	-1.3280	-
1.3280					
DENSITY:					
MOL/CC	7.6612-04	3.2647-02	4.4647-04	1.1472-03	
1.1472-03					
GM/CC	1.3194-02	0.5569	7.8758-03	2.0237-02	
2.0237-02					
AVG MW	17.2219	17.0571	17.6401	17.6401	
17.6401					

38 39 40 41 INPUT

STREAM ID	38	39	40	41	
INPUT					
FROM :	----	----	HB-HXA-3	HB-HXA-4	----
TO :	HB-HXA-3	HB-HXA-4	----	----	B21

SUBSTREAM: MIXED					
PHASE:	LIQUID	LIQUID	LIQUID	LIQUID	
VAPOR					
COMPONENTS: KMOL/HR					
AMMONIA	0.0	0.0	0.0	0.0	0.0
N2	0.0	0.0	0.0	0.0	
57.0400					
H2	0.0	0.0	0.0	0.0	
140.4000					
ARGON	0.0	0.0	0.0	0.0	
0.6600					
WATER	97.3618	1277.2491	97.3618	1277.2491	0.0
COMPONENTS: KG/HR					
AMMONIA	0.0	0.0	0.0	0.0	0.0
N2	0.0	0.0	0.0	0.0	
1597.8889					
H2	0.0	0.0	0.0	0.0	
283.0296					
ARGON	0.0	0.0	0.0	0.0	
26.3657					
WATER	1754.0000	2.3010+04	1754.0000	2.3010+04	0.0
TOTAL FLOW:					
KMOL/HR	97.3618	1277.2491	97.3618	1277.2491	
198.1000					
KG/HR	1754.0000	2.3010+04	1754.0000	2.3010+04	
1907.2841					
L/MIN	29.2341	383.5102	29.3784	385.4031	
2179.3562					
STATE VARIABLES:					
TEMP C	7.2222	7.2222	32.2222	32.2222	
35.0000					
PRES BAR	1.0000	1.0000	1.0000	1.0000	
39.6000					
VFRAC	0.0	0.0	0.0	0.0	
1.0000					
LFRAC	1.0000	1.0000	1.0000	1.0000	0.0
SFRAC	0.0	0.0	0.0	0.0	0.0
ENTHALPY:					
CAL/MOL	-6.8588+04	-6.8588+04	-6.8139+04	-6.8139+04	
69.2039					
CAL/GM	-3807.2336	-3807.2336	-3782.2820	-3782.2820	
7.1879					
CAL/SEC	-1.8550+06	-2.4335+07	-1.8428+06	-2.4175+07	
3808.1389					
ENTROPY:					
CAL/MOL-K	-40.0894	-40.0894	-38.5536	-38.5536	-
5.8566					
CAL/GM-K	-2.2253	-2.2253	-2.1400	-2.1400	-
0.6083					
DENSITY:					
MOL/CC	5.5507-02	5.5507-02	5.5234-02	5.5234-02	
1.5150-03					

GM/CC	1.0000	1.0000	0.9951	0.9951
1.4586-02				
AVG MW	18.0153	18.0153	18.0153	18.0153
9.6279				

OUT PURGE  
-----

STREAM ID	OUT	PURGE
FROM :	HB-S-02	B20
TO :	----	----

SUBSTREAM: MIXED

PHASE:	LIQUID	VAPOR
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COMPONENTS: KMOL/HR

AMMONIA	87.4800	5.9298-02
N2	2.0409-02	6.3324-03
H2	4.1079-03	2.8265-03
ARGON	6.2665-03	6.5543-04
WATER	0.0	0.0

COMPONENTS: KG/HR

AMMONIA	1489.8341	1.0099
N2	0.5717	0.1774
H2	8.2810-03	5.6979-03
ARGON	0.2503	2.6183-02
WATER	0.0	0.0

TOTAL FLOW:

KMOL/HR	87.5108	6.9112-02
KG/HR	1490.6644	1.2191
L/MIN	43.3357	1.0041

STATE VARIABLES:

TEMP C	20.0000	171.0259
PRES BAR	10.1325	39.6000
VFRAC	0.0	1.0000
LFRAC	1.0000	0.0
SFRAC	0.0	0.0

ENTHALPY:

CAL/MOL	-1.6164+04	-8357.6044
CAL/GM	-948.8955	-473.7832
CAL/SEC	-3.9291+05	-160.4480

ENTROPY:

CAL/MOL-K	-45.4736	-23.4255
CAL/GM-K	-2.6696	-1.3280

DENSITY:

MOL/CC	3.3656-02	1.1472-03
GM/CC	0.5733	2.0237-02
AVG MW	17.0341	17.6401

23  
--

STREAM ID	23
FROM :	B21
TO :	B4

SUBSTREAM: MIXED  
 PHASE: VAPOR  
 COMPONENTS: KMOL/HR  
   AMMONIA 2.9056  
   N2 57.3503  
   H2 140.5385  
   ARGON 0.6921  
   WATER 0.0  
 COMPONENTS: KG/HR  
   AMMONIA 49.4840  
   N2 1606.5811  
   H2 283.3087  
   ARGON 27.6487  
   WATER 0.0  
 TOTAL FLOW:  
   KMOL/HR 201.4865  
   KG/HR 1967.0225  
   L/MIN 2233.1981  
 STATE VARIABLES:  
   TEMP C 37.6133  
   PRES BAR 39.6000  
   VFRAC 1.0000  
   LFRAC 0.0  
   SFRAC 0.0  
 ENTHALPY:  
   CAL/MOL -72.4303  
   CAL/GM -7.4192  
   CAL/SEC -4053.8108  
 ENTROPY:  
   CAL/MOL-K -6.0069  
   CAL/GM-K -0.6153  
 DENSITY:  
   MOL/CC 1.5037-03  
   GM/CC 1.4680-02  
 AVG MW 9.7626

24  
--

STREAM ID 24  
 FROM : B4  
 TO : HB-S-01

CONV. MAX. REL. ERR: -3.4178-03  
 SUBSTREAM: MIXED  
 PHASE: VAPOR  
 COMPONENTS: KMOL/HR  
   AMMONIA 898.2631  
   N2 794.4302  
   H2 702.1462  
   ARGON 33.9247  
   WATER 0.0



COMPONENTS: KG/HR

AMMONIA	1.5298+04
N2	2.2255+04
H2	1415.4425
ARGON	1355.2220
WATER	0.0

TOTAL FLOW:

KMOL/HR	2428.7642
KG/HR	4.0323+04
L/MIN	5.1244+04

STATE VARIABLES:

TEMP C	258.8760
PRES BAR	35.1190
VFRAC	1.0000
LFRAC	0.0
SFRAC	0.0

ENTHALPY:

CAL/MOL	-2240.4691
CAL/GM	-134.9484
CAL/SEC	-1.5115+06

ENTROPY:

CAL/MOL-K	-9.0337
CAL/GM-K	-0.5441

DENSITY:

MOL/CC	7.8994-04
GM/CC	1.3115-02

AVG MW 16.6024

25  
--

STREAM ID 25  
FROM : HB-S-01  
TO : HB-HXA-1

SUBSTREAM: MIXED

PHASE: VAPOR

COMPONENTS: KMOL/HR

AMMONIA	807.8182
N2	794.0931
H2	702.0008
ARGON	33.8856
WATER	0.0

COMPONENTS: KG/HR

AMMONIA	1.3758+04
N2	2.2245+04
H2	1415.1494
ARGON	1353.6625
WATER	0.0

TOTAL FLOW:

KMOL/HR	2337.7977
KG/HR	3.8772+04
L/MIN	2.3697+04

STATE VARIABLES:

TEMP	C	30.0000
PRES	BAR	39.6000
VFRAC		1.0000
LFRAC		0.0
SFRAC		0.0
ENTHALPY:		
CAL/MOL		-3873.1588
CAL/GM		-233.5378
CAL/SEC		-2.5152+06
ENTROPY:		
CAL/MOL-K		-13.3370
CAL/GM-K		-0.8042
DENSITY:		
MOL/CC		1.6442-03
GM/CC		2.7269-02
AVG MW		16.5847

26  
--

STREAM ID	26
FROM :	HB-HXA-1
TO :	HB-CP-03

SUBSTREAM: MIXED  
PHASE: VAPOR  
COMPONENTS: KMOL/HR

AMMONIA	807.8182
N2	794.0931
H2	702.0008
ARGON	33.8856
WATER	0.0

COMPONENTS: KG/HR

AMMONIA	1.3758+04
N2	2.2245+04
H2	1415.1494
ARGON	1353.6625
WATER	0.0

TOTAL FLOW:

KMOL/HR	2337.7977
KG/HR	3.8772+04
L/MIN	2.9475+04

STATE VARIABLES:

TEMP	C	90.0000
PRES	BAR	39.2553
VFRAC		1.0000
LFRAC		0.0
SFRAC		0.0

ENTHALPY:

CAL/MOL	-3380.8224
CAL/GM	-203.8516
CAL/SEC	-2.1955+06

ENTROPY:

CAL/MOL-K	-11.8379
-----------	----------

CAL/GM-K	-0.7138
DENSITY:	
MOL/CC	1.3219-03
GM/CC	2.1924-02
AVG MW	16.5847

27

--

STREAM ID	27
FROM :	HB-CP-03
TO :	HB-HXA-2

SUBSTREAM: MIXED

PHASE: VAPOR

COMPONENTS: KMOL/HR

AMMONIA	807.8182
N2	794.0931
H2	702.0008
ARGON	33.8856
WATER	0.0

COMPONENTS: KG/HR

AMMONIA	1.3758+04
N2	2.2245+04
H2	1415.1494
ARGON	1353.6625
WATER	0.0

TOTAL FLOW:

KMOL/HR	2337.7977
KG/HR	3.8772+04
L/MIN	1.8737+04

STATE VARIABLES:

TEMP C	192.5954
PRES BAR	81.0600
VFRAC	1.0000
LFRAC	0.0
SFRAC	0.0

ENTHALPY:

CAL/MOL	-2587.0749
CAL/GM	-155.9915
CAL/SEC	-1.6800+06

ENTROPY:

CAL/MOL-K	-11.3468
CAL/GM-K	-0.6842

DENSITY:

MOL/CC	2.0795-03
GM/CC	3.4488-02
AVG MW	16.5847

28

--

STREAM ID	28
FROM :	HB-HXA-2

TO : HB-RXN

CONV. MAX. REL. ERR: 6.5813-02

SUBSTREAM: MIXED

PHASE: VAPOR

COMPONENTS: KMOL/HR

AMMONIA	807.8182
N2	794.0931
H2	702.0008
ARGON	33.8856
WATER	0.0

COMPONENTS: KG/HR

AMMONIA	1.3758+04
N2	2.2245+04
H2	1415.1494
ARGON	1353.6625
WATER	0.0

TOTAL FLOW:

KMOL/HR	2337.7977
KG/HR	3.8772+04
L/MIN	2.0227+04

STATE VARIABLES:

TEMP C	225.0000
PRES BAR	80.7153
VFRAC	1.0000
LFRAC	0.0
SFRAC	0.0

ENTHALPY:

CAL/MOL	-2311.4996
CAL/GM	-139.3753
CAL/SEC	-1.5011+06

ENTROPY:

CAL/MOL-K	-10.7663
CAL/GM-K	-0.6492

DENSITY:

MOL/CC	1.9263-03
GM/CC	3.1947-02

AVG MW 16.5847

29

--

STREAM ID 29  
FROM : HB-RXN  
TO : HB-HXA-2

SUBSTREAM: MIXED

PHASE: VAPOR

COMPONENTS: KMOL/HR

AMMONIA	873.5322
N2	698.2629
H2	561.5493
ARGON	32.7816

WATER	0.0
COMPONENTS: KG/HR	
AMMONIA	1.4877+04
N2	1.9561+04
H2	1132.0160
ARGON	1309.5581
WATER	0.0
TOTAL FLOW:	
KMOL/HR	2166.1259
KG/HR	3.6879+04
L/MIN	2.5421+04
STATE VARIABLES:	
TEMP C	400.0000
PRES BAR	81.0600
VFRAC	1.0000
LFRAC	0.0
SFRAC	0.0
ENTHALPY:	
CAL/MOL	-1386.1469
CAL/GM	-81.4166
CAL/SEC	-8.3405+05
ENTROPY:	
CAL/MOL-K	-9.4569
CAL/GM-K	-0.5555
DENSITY:	
MOL/CC	1.4202-03
GM/CC	2.4179-02
AVG MW	17.0254

30  
--

STREAM ID	30
FROM :	HB-HXA-2
TO :	HB-HXA-3

SUBSTREAM: MIXED

PHASE:	VAPOR
COMPONENTS: KMOL/HR	
AMMONIA	873.5322
N2	698.2629
H2	561.5493
ARGON	32.7816
WATER	0.0
COMPONENTS: KG/HR	
AMMONIA	1.4877+04
N2	1.9561+04
H2	1132.0160
ARGON	1309.5581
WATER	0.0
TOTAL FLOW:	
KMOL/HR	2166.1259
KG/HR	3.6879+04
L/MIN	2.4149+04

## STATE VARIABLES:

TEMP	C	367.0686
PRES	BAR	81.0600
VFRAC		1.0000
LFRAC		0.0
SFRAC		0.0
ENTHALPY:		
CAL/MOL		-1683.5624
CAL/GM		-98.8855
CAL/SEC		-1.0130+06
ENTROPY:		
CAL/MOL-K		-9.9099
CAL/GM-K		-0.5821
DENSITY:		
MOL/CC		1.4950-03
GM/CC		2.5453-02
AVG MW		17.0254

31

--

STREAM ID	31
FROM :	HB-HXA-3
TO :	HB-HXA-1

CONV. MAX. REL. ERR: -5.2808-02

SUBSTREAM: MIXED

PHASE: VAPOR

COMPONENTS: KMOL/HR

AMMONIA	873.5322
N2	698.2629
H2	561.5493
ARGON	32.7816
WATER	0.0

COMPONENTS: KG/HR

AMMONIA	1.4877+04
N2	1.9561+04
H2	1132.0160
ARGON	1309.5581
WATER	0.0

TOTAL FLOW:

KMOL/HR	2166.1259
KG/HR	3.6879+04
L/MIN	2.4162+04

## STATE VARIABLES:

TEMP	C	364.8045
PRES	BAR	80.7153
VFRAC		1.0000
LFRAC		0.0
SFRAC		0.0
ENTHALPY:		
CAL/MOL		-1703.7667
CAL/GM		-100.0722

CAL/SEC	-1.0252+06
ENTROPY:	
CAL/MOL-K	-9.9329
CAL/GM-K	-0.5834
DENSITY:	
MOL/CC	1.4942-03
GM/CC	2.5439-02
AVG MW	17.0254

32  
--

STREAM ID	32
FROM :	HB-HXA-1
TO :	HB-HXA-4

SUBSTREAM: MIXED

PHASE: VAPOR

COMPONENTS: KMOL/HR

AMMONIA	895.4369
N2	737.1927
H2	561.5867
ARGON	33.2336
WATER	0.0

COMPONENTS: KG/HR

AMMONIA	1.5250+04
N2	2.0651+04
H2	1132.0913
ARGON	1327.6169
WATER	0.0

TOTAL FLOW:

KMOL/HR	2227.4499
KG/HR	3.8361+04
L/MIN	5.0674+04

STATE VARIABLES:

TEMP C	305.5963
PRES BAR	35.4637
VFRAC	1.0000
LFRAC	0.0
SFRAC	0.0

ENTHALPY:

CAL/MOL	-2187.2785
CAL/GM	-127.0059
CAL/SEC	-1.3533+06

ENTROPY:

CAL/MOL-K	-9.0742
CAL/GM-K	-0.5269

DENSITY:

MOL/CC	7.3260-04
GM/CC	1.2617-02
AVG MW	17.2219

33  
--

STREAM ID 33  
FROM : HB-HXA-4  
TO : B4

SUBSTREAM: MIXED

PHASE: VAPOR

COMPONENTS: KMOL/HR

AMMONIA	895.4369
N2	737.1927
H2	561.5867
ARGON	33.2336
WATER	0.0

COMPONENTS: KG/HR

AMMONIA	1.5250+04
N2	2.0651+04
H2	1132.0913
ARGON	1327.6169
WATER	0.0

TOTAL FLOW:

KMOL/HR	2227.4499
KG/HR	3.8361+04
L/MIN	4.8457+04

STATE VARIABLES:

TEMP C	275.6711
PRES BAR	35.1190
VFRAC	1.0000
LFRAC	0.0
SFRAC	0.0

ENTHALPY:

CAL/MOL	-2445.0335
CAL/GM	-141.9727
CAL/SEC	-1.5128+06

ENTROPY:

CAL/MOL-K	-9.5120
CAL/GM-K	-0.5523

DENSITY:

MOL/CC	7.6612-04
GM/CC	1.3194-02

AVG MW 17.2219

34

--

STREAM ID 34  
FROM : HB-S-01  
TO : HB-S-02

SUBSTREAM: MIXED

PHASE: LIQUID

COMPONENTS: KMOL/HR

AMMONIA	90.4449
N2	0.3370
H2	0.1454



ARGON	3.9038-02
WATER	0.0
COMPONENTS: KG/HR	
AMMONIA	1540.3279
N2	9.4413
H2	0.2932
ARGON	1.5595
WATER	0.0
TOTAL FLOW:	
KMOL/HR	90.9664
KG/HR	1551.6219
L/MIN	46.4395
STATE VARIABLES:	
TEMP C	30.0000
PRES BAR	39.6000
VFRAC	0.0
LFRAC	1.0000
SFRAC	0.0
ENTHALPY:	
CAL/MOL	-1.5846+04
CAL/GM	-929.0029
CAL/SEC	-4.0041+05
ENTROPY:	
CAL/MOL-K	-44.5577
CAL/GM-K	-2.6123
DENSITY:	
MOL/CC	3.2647-02
GM/CC	0.5569
AVG MW	17.0571

35  
--

STREAM ID	35
FROM :	HB-S-02
TO :	HB-CP-02

SUBSTREAM: MIXED

PHASE:	VAPOR
COMPONENTS: KMOL/HR	
AMMONIA	2.9649
N2	0.3166
H2	0.1413
ARGON	3.2772-02
WATER	0.0
COMPONENTS: KG/HR	
AMMONIA	50.4939
N2	8.8696
H2	0.2849
ARGON	1.3092
WATER	0.0
TOTAL FLOW:	
KMOL/HR	3.4556
KG/HR	60.9575

L/MIN		128.9968
STATE VARIABLES:		
TEMP	C	20.0000
PRES	BAR	10.1325
VFRAC		1.0000
LFRAC		0.0
SFRAC		0.0
ENTHALPY:		
CAL/MOL		-9566.0182
CAL/GM		-542.2868
CAL/SEC		-9182.3445
ENTROPY:		
CAL/MOL-K		-24.2168
CAL/GM-K		-1.3728
DENSITY:		
MOL/CC		4.4647-04
GM/CC		7.8758-03
AVG MW		17.6401

36

--

STREAM ID		36
FROM :		HB-CP-02
TO :		B20

SUBSTREAM: MIXED

PHASE: VAPOR

COMPONENTS: KMOL/HR

AMMONIA	2.9649
N2	0.3166
H2	0.1413
ARGON	3.2772-02
WATER	0.0

COMPONENTS: KG/HR

AMMONIA	50.4939
N2	8.8696
H2	0.2849
ARGON	1.3092
WATER	0.0

TOTAL FLOW:

KMOL/HR	3.4556
KG/HR	60.9575
L/MIN	50.2032

STATE VARIABLES:

TEMP	C	171.0260
PRES	BAR	39.6000
VFRAC		1.0000
LFRAC		0.0
SFRAC		0.0

ENTHALPY:

CAL/MOL		-8357.6044
CAL/GM		-473.7832
CAL/SEC		-8022.3977

ENTROPY:  
CAL/MOL-K -23.4255  
CAL/GM-K -1.3280  
DENSITY:  
MOL/CC 1.1472-03  
GM/CC 2.0237-02  
AVG MW 17.6401

37  
--

STREAM ID 37  
FROM : B20  
TO : B21

SUBSTREAM: MIXED  
PHASE: VAPOR  
COMPONENTS: KMOL/HR  
AMMONIA 2.9056  
N2 0.3103  
H2 0.1385  
ARGON 3.2116-02  
WATER 0.0

COMPONENTS: KG/HR  
AMMONIA 49.4840  
N2 8.6922  
H2 0.2792  
ARGON 1.2830  
WATER 0.0

TOTAL FLOW:  
KMOL/HR 3.3865  
KG/HR 59.7383  
L/MIN 49.1991

STATE VARIABLES:  
TEMP C 171.0259  
PRES BAR 39.6000  
VFRAC 1.0000  
LFRAC 0.0  
SFRAC 0.0

ENTHALPY:  
CAL/MOL -8357.6044  
CAL/GM -473.7832  
CAL/SEC -7861.9497

ENTROPY:  
CAL/MOL-K -23.4255  
CAL/GM-K -1.3280  
DENSITY:  
MOL/CC 1.1472-03  
GM/CC 2.0237-02  
AVG MW 17.6401

38  
--

STREAM ID 38  
FROM : ----  
TO : HB-HXA-3

SUBSTREAM: MIXED

PHASE: LIQUID

COMPONENTS: KMOL/HR

AMMONIA	0.0
N2	0.0
H2	0.0
ARGON	0.0
WATER	97.3618

COMPONENTS: KG/HR

AMMONIA	0.0
N2	0.0
H2	0.0
ARGON	0.0
WATER	1754.0000

TOTAL FLOW:

KMOL/HR	97.3618
KG/HR	1754.0000
L/MIN	29.2341

STATE VARIABLES:

TEMP C	7.2222
PRES BAR	1.0000
VFRAC	0.0
LFRAC	1.0000
SFRAC	0.0

ENTHALPY:

CAL/MOL	-6.8588+04
CAL/GM	-3807.2336
CAL/SEC	-1.8550+06

ENTROPY:

CAL/MOL-K	-40.0894
CAL/GM-K	-2.2253

DENSITY:

MOL/CC	5.5507-02
GM/CC	1.0000

AVG MW 18.0153

39

--

STREAM ID 39  
FROM : ----  
TO : HB-HXA-4

SUBSTREAM: MIXED

PHASE: LIQUID

COMPONENTS: KMOL/HR

AMMONIA	0.0
N2	0.0
H2	0.0
ARGON	0.0

WATER	1277.2491
COMPONENTS: KG/HR	
AMMONIA	0.0
N2	0.0
H2	0.0
ARGON	0.0
WATER	2.3010+04
TOTAL FLOW:	
KMOL/HR	1277.2491
KG/HR	2.3010+04
L/MIN	383.5102
STATE VARIABLES:	
TEMP C	7.2222
PRES BAR	1.0000
VFRAC	0.0
LFRAC	1.0000
SFRAC	0.0
ENTHALPY:	
CAL/MOL	-6.8588+04
CAL/GM	-3807.2336
CAL/SEC	-2.4335+07
ENTROPY:	
CAL/MOL-K	-40.0894
CAL/GM-K	-2.2253
DENSITY:	
MOL/CC	5.5507-02
GM/CC	1.0000
AVG MW	18.0153

40  
--

STREAM ID	40
FROM :	HB-HXA-3
TO :	----

SUBSTREAM: MIXED	
PHASE:	LIQUID
COMPONENTS: KMOL/HR	
AMMONIA	0.0
N2	0.0
H2	0.0
ARGON	0.0
WATER	97.3618
COMPONENTS: KG/HR	
AMMONIA	0.0
N2	0.0
H2	0.0
ARGON	0.0
WATER	1754.0000
TOTAL FLOW:	
KMOL/HR	97.3618
KG/HR	1754.0000
L/MIN	29.3784

STATE VARIABLES:

TEMP	C	32.2222
PRES	BAR	1.0000
VFRAC		0.0
LFRAC		1.0000
SFRAC		0.0

ENTHALPY:

CAL/MOL	-6.8139+04
CAL/GM	-3782.2820
CAL/SEC	-1.8428+06

ENTROPY:

CAL/MOL-K	-38.5536
CAL/GM-K	-2.1400

DENSITY:

MOL/CC	5.5234-02
GM/CC	0.9951

AVG MW 18.0153

41  
--

STREAM ID 41  
FROM : HB-HXA-4  
TO : ----

SUBSTREAM: MIXED  
PHASE: LIQUID  
COMPONENTS: KMOL/HR

AMMONIA	0.0
N2	0.0
H2	0.0
ARGON	0.0
WATER	1277.2491

COMPONENTS: KG/HR

AMMONIA	0.0
N2	0.0
H2	0.0
ARGON	0.0
WATER	2.3010+04

TOTAL FLOW:

KMOL/HR	1277.2491
KG/HR	2.3010+04
L/MIN	385.4031

STATE VARIABLES:

TEMP	C	32.2222
PRES	BAR	1.0000
VFRAC		0.0
LFRAC		1.0000
SFRAC		0.0

ENTHALPY:

CAL/MOL	-6.8139+04
CAL/GM	-3782.2820
CAL/SEC	-2.4175+07

ENTROPY:

CAL/MOL-K	-38.5536
CAL/GM-K	-2.1400
DENSITY:	
MOL/CC	5.5234-02
GM/CC	0.9951
AVG MW	18.0153

INPUT  
-----

STREAM ID	INPUT
FROM :	----
TO :	B21

SUBSTREAM: MIXED	
PHASE:	VAPOR
COMPONENTS: KMOL/HR	
AMMONIA	0.0
N2	57.0400
H2	140.4000
ARGON	0.6600
WATER	0.0

COMPONENTS: KG/HR	
AMMONIA	0.0
N2	1597.8889
H2	283.0296
ARGON	26.3657
WATER	0.0

TOTAL FLOW:	
KMOL/HR	198.1000
KG/HR	1907.2841
L/MIN	2179.3562

STATE VARIABLES:	
TEMP C	35.0000
PRES BAR	39.6000
VFRAC	1.0000
LFRAC	0.0
SFRAC	0.0

ENTHALPY:	
CAL/MOL	69.2039
CAL/GM	7.1879
CAL/SEC	3808.1389

ENTROPY:	
CAL/MOL-K	-5.8566
CAL/GM-K	-0.6083

DENSITY:	
MOL/CC	1.5150-03
GM/CC	1.4586-02
AVG MW	9.6279

OUT  
---

STREAM ID	OUT
-----------	-----

FROM : HB-S-02  
TO : ----

SUBSTREAM: MIXED

PHASE: LIQUID

COMPONENTS: KMOL/HR

AMMONIA	87.4800
N2	2.0409-02
H2	4.1079-03
ARGON	6.2665-03
WATER	0.0

COMPONENTS: KG/HR

AMMONIA	1489.8341
N2	0.5717
H2	8.2810-03
ARGON	0.2503
WATER	0.0

TOTAL FLOW:

KMOL/HR	87.5108
KG/HR	1490.6644
L/MIN	43.3357

STATE VARIABLES:

TEMP C	20.0000
PRES BAR	10.1325
VFRAC	0.0
LFRAC	1.0000
SFRAC	0.0

ENTHALPY:

CAL/MOL	-1.6164+04
CAL/GM	-948.8955
CAL/SEC	-3.9291+05

ENTROPY:

CAL/MOL-K	-45.4736
CAL/GM-K	-2.6696

DENSITY:

MOL/CC	3.3656-02
GM/CC	0.5733
AVG MW	17.0341

PURGE

-----

STREAM ID PURGE  
FROM : B20  
TO : ----

SUBSTREAM: MIXED

PHASE: VAPOR

COMPONENTS: KMOL/HR

AMMONIA	5.9298-02
N2	6.3324-03
H2	2.8265-03
ARGON	6.5543-04
WATER	0.0



COMPONENTS: KG/HR		
AMMONIA		1.0099
N2		0.1774
H2		5.6979-03
ARGON		2.6183-02
WATER		0.0
TOTAL FLOW:		
KMOL/HR		6.9112-02
KG/HR		1.2191
L/MIN		1.0041
STATE VARIABLES:		
TEMP	C	171.0259
PRES	BAR	39.6000
VFRAC		1.0000
LFRAC		0.0
SFRAC		0.0
ENTHALPY:		
CAL/MOL		-8357.6044
CAL/GM		-473.7832
CAL/SEC		-160.4480
ENTROPY:		
CAL/MOL-K		-23.4255
CAL/GM-K		-1.3280
DENSITY:		
MOL/CC		1.1472-03
GM/CC		2.0237-02
AVG MW		17.6401

# C.1.1: Compressed Air

## Safety Data Sheet

according to Regulation (EU) 2015/830



## Compressed Air

Date of issue: 20/12/2010

Supersedes: 18/12/2015

Revision date: 10/07/2019

Version: 1.2

SDS reference: 2010492

**Warning**



### SECTION 1: Identification of the substance/mixture and of the company/undertaking

#### 1.1. Product identifier

Trade name : Compressed Air, Alphahaz™ Air, Smartop™ Air, Purified Air, Medical Air  
SDS no : 2010492

#### 1.2. Relevant identified uses of the substance or mixture and uses advised against

Relevant identified uses : Industrial and professional. Perform risk assessment prior to use.  
Contact supplier for more information on uses.  
Test gas/Calibration gas.  
Purging.  
Laboratory use.

Uses advised against : None.

#### 1.3. Details of the supplier of the safety data sheet

Company identification : AIR LIQUIDE SINGAPORE PTE LTD  
HEAD OFFICE : 2 VENTURE DRIVE, VISION EXCHANGE, #22-28, SINGAPORE 608526  
SPECIALGASES OFFICE, NO 24 JALAN BUROH SINGAPORE 619480  
T +65 6 265 3788  
<https://industry.airliquide.sg/resources/safety-data-sheets-sds>  
Sg-info@airliquide.com

#### 1.4. Emergency telephone number

Emergency telephone number : +65 6265 3788, +65 9619 9229 (After Office Hour)

### SECTION 2: Hazards identification

#### 2.1. Classification of the substance or mixture

##### Classification according to Regulation (EC) No. 1272/2008 [CLP]

Physical hazards : Gases under pressure : Compressed gas H280

#### 2.2. Label elements

##### Labelling according to Regulation (EC) No. 1272/2008 [CLP]

Hazard pictograms (CLP) :



GHS04

Signal word (CLP) : Warning

Hazard statements (CLP) : H280 - Contains gas under pressure; may explode if heated.

Precautionary statements (CLP)

- Storage : P403 - Store in a well-ventilated place.

**2.3. Other hazards**

: None.

**SECTION 3: Composition/information on ingredients****3.1. Substances** : Not applicable**3.2. Mixtures**

Name	Product identifier	%	Classification according to Regulation (EC) No. 1272/2008 [CLP]
Nitrogen	(CAS-No.) 7727-37-9 (EC-No.) 231-783-9 (EC Index-No.) (REACH-no) *1	79	Press. Gas (Comp.), H280
Oxygen	(CAS-No.) 7782-44-7 (EC-No.) 231-956-9 (EC Index-No.) 008-001-00-8 (REACH-no) *1	21	Ox. Gas 1, H270 Press. Gas (Comp.), H280

Full text of H-statements: see section 16

*Contains no other components or impurities which will influence the classification of the product.*

\*1: Listed in Annex IV / V REACH, exempted from registration.

\*2: Registration deadline not expired.

\*3: Registration not required: Substance manufactured or imported &lt; 1t/y.

**SECTION 4: First aid measures****4.1. Description of first aid measures**

- Inhalation : Remove victim to uncontaminated area wearing self contained breathing apparatus. Keep victim warm and rested. Call a doctor. Apply artificial respiration if breathing stopped.
- Skin contact : Adverse effects not expected from this product.
- Eye contact : Adverse effects not expected from this product.
- Ingestion : Ingestion is not considered a potential route of exposure.

**4.2. Most important symptoms and effects, both acute and delayed**

- : No effect on living tissue.
- Refer to section 11.

**4.3. Indication of any immediate medical attention and special treatment needed**

: None.

**SECTION 5: Firefighting measures****5.1. Extinguishing media**

- Suitable extinguishing media : Water spray or fog.
- Unsuitable extinguishing media : Do not use water jet to extinguish.

**5.2. Special hazards arising from the substance or mixture**

Specific hazards : Exposure to fire may cause containers to rupture/explode.  
Supports combustion.

Hazardous combustion products : None.

**5.3. Advice for firefighters**

Specific methods : Use fire control measures appropriate for the surrounding fire. Exposure to fire and heat radiation may cause gas receptacles to rupture. Cool endangered receptacles with water spray jet from a protected position. Prevent water used in emergency cases from entering sewers and drainage systems.

If possible, stop flow of product.

Use water spray or fog to knock down fire fumes if possible.

Move containers away from the fire area if this can be done without risk.

In confined space use self-contained breathing apparatus.

Standard EN 137 - Self-contained open-circuit compressed air breathing apparatus with full face mask.

Special protective equipment for fire fighters : Standard protective clothing and equipment (Self Contained Breathing Apparatus) for fire fighters.

Standard EN 469 - Protective clothing for firefighters. Standard - EN 659: Protective gloves for firefighters.

Standard EN 137 - Self-contained open-circuit compressed air breathing apparatus with full face mask.

In confined space use self-contained breathing apparatus.

**SECTION 6: Accidental release measures****6.1. Personal precautions, protective equipment and emergency procedures**

: Ensure adequate air ventilation.

Act in accordance with local emergency plan.

Stay upwind.

Try to stop release.

Evacuate area.

Wear self-contained breathing apparatus when entering area unless atmosphere is proved to be safe.

Oxygen detectors should be used when asphyxiating gases may be released.

**6.2. Environmental precautions**

: Try to stop release.

None.

**6.3. Methods and material for containment and cleaning up**

: Ventilate area.

None.

**6.4. Reference to other sections**

: See also sections 8 and 13.

**SECTION 7: Handling and storage**

**7.1. Precautions for safe handling**

- Safe use of the product : The product must be handled in accordance with good industrial hygiene and safety procedures.
- Only experienced and properly instructed persons should handle gases under pressure.
  - Consider pressure relief device(s) in gas installations.
  - Ensure the complete gas system was (or is regularly) checked for leaks before use.
  - Do not smoke while handling product.
  - Use only properly specified equipment which is suitable for this product, its supply pressure and temperature. Contact your gas supplier if in doubt.
  - Use only oxygen approved lubricants and oxygen approved sealings.
  - Avoid suck back of water, acid and alkalis.
  - Do not breathe gas.
  - Avoid release of product into work area.
- Safe handling of the gas receptacle : Refer to supplier's container handling instructions.
- Do not allow backfeed into the container.
  - Protect cylinders from physical damage; do not drag, roll, slide or drop.
  - When moving cylinders, even for short distances, use a cart (trolley, hand truck, etc.) designed to transport cylinders.
  - Leave valve protection caps in place until the container has been secured against either a wall or bench or placed in a container stand and is ready for use.
  - If user experiences any difficulty operating cylinder valve discontinue use and contact supplier.
  - Never attempt to repair or modify container valves or safety relief devices.
  - Damaged valves should be reported immediately to the supplier.
  - Keep container valve outlets clean and free from contaminants particularly oil and water.
  - Replace valve outlet caps or plugs and container caps where supplied as soon as container is disconnected from equipment.
  - Close container valve after each use and when empty, even if still connected to equipment.
  - Never attempt to transfer gases from one cylinder/container to another.
  - Never use direct flame or electrical heating devices to raise the pressure of a container.
  - Do not remove or deface labels provided by the supplier for the identification of the cylinder contents.
  - Suck back of water into the container must be prevented.
  - Open valve slowly to avoid pressure shock.

**7.2. Conditions for safe storage, including any incompatibilities**

- Observe all regulations and local requirements regarding storage of containers.
- Containers should not be stored in conditions likely to encourage corrosion.
- Container valve guards or caps should be in place.
- Containers should be stored in the vertical position and properly secured to prevent them from falling over.
- Stored containers should be periodically checked for general condition and leakage.
- Keep container below 50°C in a well ventilated place.
- Store containers in location free from fire risk and away from sources of heat and ignition.
- Keep away from combustible materials.

**7.3. Specific end use(s)**

- None.

**SECTION 8: Exposure controls/personal protection****8.1. Control parameters**

OEL (Occupational Exposure Limits)	:	None available.
DNEL (Derived-No Effect Level)	:	None available.
PNEC (Predicted No-Effect Concentration)	:	None available.

## **8.2. Exposure controls**

### **8.2.1. Appropriate engineering controls**

- : Systems under pressure should be regularly checked for leakages.  
Consider the use of a work permit system e.g. for maintenance activities.  
Provide adequate general and local exhaust ventilation.  
Oxygen detectors should be used when asphyxiating gases may be released.

### **8.2.2. Individual protection measures, e.g. personal protective equipment**

- : A risk assessment should be conducted and documented in each work area to assess the risks related to the use of the product and to select the PPE that matches the relevant risk. The following recommendations should be considered:  
PPE compliant to the recommended EN/ISO standards should be selected.

- Eye/face protection : Wear safety glasses with side shields.  
Standard EN 166 - Personal eye-protection - specifications.
- Skin protection
  - Hand protection : Wear working gloves when handling gas containers.  
Standard EN 388 - Protective gloves against mechanical risk.
  - Other : Wear safety shoes while handling containers.  
Standard EN ISO 20345 - Personal protective equipment - Safety footwear.
- Respiratory protection : Self contained breathing apparatus (SCBA) or positive pressure airline with mask are to be used in oxygen-deficient atmospheres.  
Standard EN 137 - Self-contained open-circuit compressed air breathing apparatus with full face mask.  
None necessary.
- Thermal hazards : None in addition to the above sections.

### **8.2.3. Environmental exposure controls**

- : Refer to local regulations for restriction of emissions to the atmosphere. See section 13 for specific methods for waste gas treatment.  
None necessary.

## **SECTION 9: Physical and chemical properties**

### **9.1. Information on basic physical and chemical properties**

#### Appearance

- Physical state at 20°C / 101.3kPa : Gas
- Colour : Mixture contains one or more component(s) which have the following colour(s):  
Colourless.

Odour : Odourless.

Odour threshold : Odour threshold is subjective and inadequate to warn of overexposure.

pH : Not applicable for gases and gas mixtures.

Melting point / Freezing point : Not known

Boiling point	: Not known
Flash point	: Not applicable for gases and gas mixtures.
Evaporation rate	: Not applicable for gases and gas mixtures.
Flammability (solid, gas)	: Non flammable.
Explosive limits	: Non flammable.
Vapour pressure [20°C]	: Not applicable.
Vapour pressure [50°C]	: Not applicable.
Vapour density	: Not applicable.
Relative density, gas (air=1)	: 1
Partition coefficient n-octanol/water (Log Kow)	: Not applicable for inorganic products.
Auto-ignition temperature	: Non flammable.
Decomposition temperature	: Not applicable.
Viscosity, kinematic	: No reliable data available.
Explosive properties	: Not applicable.
Oxidising properties	: Not applicable.

**9.2. Other information**

Molar mass	: 29 g/mol
Other data	: None.

**SECTION 10: Stability and reactivity****10.1. Reactivity**

: No reactivity hazard other than the effects described in sub-sections below.

**10.2. Chemical stability**

: Stable under normal conditions.

**10.3. Possibility of hazardous reactions**

: None.

**10.4. Conditions to avoid**

: Avoid moisture in installation systems.

**10.5. Incompatible materials**

: For additional information on compatibility refer to ISO 11114.  
None.

**10.6. Hazardous decomposition products**

: Under normal conditions of storage and use, hazardous decomposition products should not be produced.

**SECTION 11: Toxicological information****11.1. Information on toxicological effects**

<b>Acute toxicity</b>	: No toxicological effects from this product.
<b>Skin corrosion/irritation</b>	: No known effects from this product.
<b>Serious eye damage/irritation</b>	: No known effects from this product.
<b>Respiratory or skin sensitisation</b>	: No known effects from this product.
<b>Germ cell mutagenicity</b>	: No known effects from this product.
<b>Carcinogenicity</b>	: No known effects from this product.

<b>Toxic for reproduction : Fertility</b>	: No known effects from this product.
<b>Toxic for reproduction : unborn child</b>	: No known effects from this product.
<b>STOT-single exposure</b>	: No known effects from this product.
<b>STOT-repeated exposure</b>	: No known effects from this product.
<b>Aspiration hazard</b>	: Not applicable for gases and gas mixtures.

## SECTION 12: Ecological information

### 12.1. Toxicity

Assessment	: No ecological damage caused by this product.
EC50 48h - Daphnia magna [mg/l]	: No data available.
EC50 72h - Algae [mg/l]	: No data available.
LC50 96 h - Fish [mg/l]	: No data available.

### 12.2. Persistence and degradability

Assessment	: No ecological damage caused by this product.
------------	--

### 12.3. Bioaccumulative potential

Assessment	: No data available.
------------	----------------------

### 12.4. Mobility in soil

Assessment	: Because of its high volatility, the product is unlikely to cause ground or water pollution. Partition into soil is unlikely.
------------	---

### 12.5. Results of PBT and vPvB assessment

Assessment	: No data available.
------------	----------------------

### 12.6. Other adverse effects

Other adverse effects	: No known effects from this product.
Effect on the ozone layer	: None.
Effect on global warming	: No known effects from this product.

## SECTION 13: Disposal considerations

### 13.1. Waste treatment methods

Contact supplier if guidance is required.  
Do not discharge into any place where its accumulation could be dangerous.  
Ensure that the emission levels from local regulations or operating permits are not exceeded.  
Refer to the EIGA code of practice Doc.30 "Disposal of Gases", downloadable at <http://www.eiga.eu> for more guidance on suitable disposal methods.  
Return unused product in original cylinder to supplier.  
May be vented to atmosphere in a well ventilated place.  
May be vented to atmosphere.  
16 05 05 : Gases in pressure containers other than those mentioned in 16 05 04.

List of hazardous waste codes (from Commission Decision 2000/532/EC as amended)



**13.2. Additional information**

: External treatment and disposal of waste should comply with applicable local and/or national regulations.

**SECTION 14: Transport information**

**14.1. UN number**

UN-No. : 1002

**14.2. UN proper shipping name**

Transport by road/rail (ADR/RID) : AIR, COMPRESSED

Transport by air (ICAO-TI / IATA-DGR) : Air, compressed

Transport by sea (IMDG) : AIR, COMPRESSED

**14.3. Transport hazard class(es)**

Labelling :



2.2 : Non-flammable, non-toxic gases.

**Transport by road/rail (ADR/RID)**

Class : 2  
 Classification code : 1A  
 Hazard identification number : 20  
 Tunnel Restriction : E - Passage forbidden through tunnels of category E

**Transport by air (ICAO-TI / IATA-DGR)**

Class / Div. (Sub. risk(s)) : 2.2

**Transport by sea (IMDG)**

Class / Div. (Sub. risk(s)) : 2.2  
 Emergency Schedule (EmS) - Fire : F-C  
 Emergency Schedule (EmS) - Spillage : S-V

**14.4. Packing group**

Transport by road/rail (ADR/RID) : Not applicable  
 Transport by air (ICAO-TI / IATA-DGR) : Not applicable  
 Transport by sea (IMDG) : Not applicable

**14.5. Environmental hazards**

Transport by road/rail (ADR/RID) : None.  
 Transport by air (ICAO-TI / IATA-DGR) : None.  
 Transport by sea (IMDG) : None.

**14.6. Special precautions for user**

**Packing Instruction(s)**

Transport by road/rail (ADR/RID) : P200  
 Transport by air (ICAO-TI / IATA-DGR)

Passenger and Cargo Aircraft : 200.  
Cargo Aircraft only : 200.  
Transport by sea (IMDG) : P200

Special transport precautions : Avoid transport on vehicles where the load space is not separated from the driver's compartment.  
Ensure vehicle driver is aware of the potential hazards of the load and knows what to do in the event of an accident or an emergency.  
Before transporting product containers:  
- Ensure there is adequate ventilation.  
- Ensure that containers are firmly secured.  
- Ensure cylinder valve is closed and not leaking.  
- Ensure valve outlet cap nut or plug (where provided) is correctly fitted.  
- Ensure valve protection device (where provided) is correctly fitted.

#### **14.7. Transport in bulk according to Annex II of Marpol and the IBC Code**

: Not applicable.

### **SECTION 15: Regulatory information**

#### **15.1. Safety, health and environmental regulations/legislation specific for the substance or mixture**

##### **EU-Regulations**

Restrictions on use : None.  
Seveso Directive : 2012/18/EU (Seveso III) : Not covered.

##### **National regulations**

National legislation : Ensure all national/local regulations are observed.

#### **15.2. Chemical safety assessment**

: A CSA does not need to be carried out for this product.

### **SECTION 16: Other information**

Indication of changes : Revised safety data sheet in accordance with commission regulation (EU) No 2015/830.

- Abbreviations and acronyms : ATE - Acute Toxicity Estimate  
CLP - Classification Labelling Packaging Regulation; Regulation (EC) No 1272/2008  
REACH - Registration, Evaluation, Authorisation and Restriction of Chemicals Regulation (EC) No 1907/2006  
EINECS - European Inventory of Existing Commercial Chemical Substances  
CAS# - Chemical Abstract Service number  
PPE - Personal Protection Equipment  
LC50 - Lethal Concentration to 50 % of a test population  
RMM - Risk Management Measures  
PBT - Persistent, Bioaccumulative and Toxic  
vPvB - Very Persistent and Very Bioaccumulative  
STOT- SE : Specific Target Organ Toxicity - Single Exposure  
CSA - Chemical Safety Assessment  
EN - European Standard  
UN - United Nations  
ADR - European Agreement concerning the International Carriage of Dangerous Goods by Road  
IATA - International Air Transport Association  
IMDG code - International Maritime Dangerous Goods  
RID - Regulations concerning the International Carriage of Dangerous Goods by Rail  
WGK - Water Hazard Class  
STOT - RE : Specific Target Organ Toxicity - Repeated Exposure
- Training advice : The hazard of asphyxiation is often overlooked and must be stressed during operator training.
- Further information : Classification using data from databases maintained by the European Industrial Gases Association (EIGA).  
Classification in accordance with the calculation methods of Regulation (EC) 1272/2008 CLP.


## Full text of H- and EUH-statements

Ox. Gas 1	Oxidising Gases, Category 1
Press. Gas (Comp.)	Gases under pressure : Compressed gas
H270	May cause or intensify fire; oxidiser.
H280	Contains gas under pressure; may explode if heated.

- DISCLAIMER OF LIABILITY : Before using this product in any new process or experiment, a thorough material compatibility and safety study should be carried out.  
Details given in this document are believed to be correct at the time of going to press.  
Whilst proper care has been taken in the preparation of this document, no liability for injury or damage resulting from its use can be accepted.

End of document

## C.1.2: Hydrogen

	<b>SAFETY DATA SHEET</b>	Page : 1/11
		Revised edition no : 1
		Compilation date : 17 / 9 / 2018
		Supersedes : 4 / 10 / 2017
<b>Hydrogen</b>		<b>NOAL_0067A</b>
		Country : SE / Language : EN

### SECTION 1: Identification of the substance/mixture and of the company/undertaking

#### 1.1. Product identifier

Trade name : Hydrogen, Alphagaz 1 Hydrogen, Alphagaz 2 Hydrogen, Hydrogen N35, Hydrogen N50, Hydrogen N56  
SDS no : NOAL\_0067A  
Chemical description : Hydrogen  
CAS-No. : 1333-74-0  
EC-No. : 215-605-7  
EC Index-No. : 001-001-00-9  
Registration-No. : Listed in Annex IV / V REACH, exempted from registration.  
Chemical formula : H<sub>2</sub>

#### 1.2. Relevant identified uses of the substance or mixture and uses advised against

Relevant identified uses : Industrial and professional. Perform risk assessment prior to use.  
Test gas/Calibration gas.  
Laboratory use.  
Chemical reaction / Synthesis.  
Use as a fuel.  
Shield gas for welding processes.  
Use for manufacture of electronic/photovoltaic components.  
Laser gas.  
Contact supplier for more information on uses.

Uses advised against : Do not inflate in party balloons because of the risk of explosion.  
Consumer use.

#### 1.3. Details of the supplier of the safety data sheet

##### Company identification

AIR LIQUIDE GAS AB  
Lundavägen 151  
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#### 1.4. Emergency telephone number

Emergency telephone number : 112  
Availability  
( 24 / 7 )

### SECTION 2: Hazards identification

#### 2.1. Classification of the substance or mixture

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		Country : SE / Language : EN

**Classification according to Regulation (EC) No. 1272/2008 [CLP]**

Physical hazards                      Flammable gases, Category 1                      H220  
 Gases under pressure : Compressed gas                      H280

**2.2. Label elements**
**Labelling according to Regulation (EC) No. 1272/2008 [CLP]**

Hazard pictograms (CLP)



Signal word (CLP)

: Danger

Hazard statements (CLP)

 : H220 - Extremely flammable gas..  
 H280 - Contains gas under pressure; may explode if heated..

Precautionary statements (CLP)

- Prevention : P210 - Keep away from heat, hot surfaces, sparks, open flames and other ignition sources. No smoking..
- Response : P377 - Leaking gas fire: Do not extinguish, unless leak can be stopped safely..  
 P381 - In case of leakage, eliminate all ignition sources.
- Storage : P403 - Store in a well-ventilated place..

**2.3. Other hazards**

: None.


**SECTION 3: Composition/information on ingredients**
**3.1. Substances**

Name	Product identifier	Composition [V-%]:	Classification according to Regulation (EC) No. 1272/2008 [CLP]
Hydrogen	(CAS-No.) 1333-74-0  (EC-No.) 215-605-7  (EC Index-No.) 001-001-00-9  (Registration-No.) *1	100	Flam. Gas 1, H220 Press. Gas (Comp.), H280

*Contains no other components or impurities which will influence the classification of the product.*
*\*1: Listed in Annex IV / V REACH, exempted from registration.*
*\*2: Registration deadline not expired.*
*\*3: Registration not required: Substance manufactured or imported < 1t/y.*
**3.2. Mixtures**

: Not established.

**SECTION 4: First aid measures**

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#### **4.1. Description of first aid measures**

- Inhalation : Remove victim to uncontaminated area wearing self contained breathing apparatus. Keep victim warm and rested. Call a doctor. Apply artificial respiration if breathing stopped.
- Skin contact : Adverse effects not expected from this product.
- Eye contact : Adverse effects not expected from this product.
- Ingestion : Ingestion is not considered a potential route of exposure.

#### **4.2. Most important symptoms and effects, both acute and delayed**

: Refer to section 11.

#### **4.3. Indication of any immediate medical attention and special treatment needed**

: None.

### **SECTION 5: Firefighting measures**

#### **5.1. Extinguishing media**

- Suitable extinguishing media : Water spray or fog.  
Dry powder.
- Unsuitable extinguishing media : Carbon dioxide.  
Do not use water jet to extinguish.

#### **5.2. Special hazards arising from the substance or mixture**

- Specific hazards : Exposure to fire may cause containers to rupture/explode.
- Hazardous combustion products : None.


#### **5.3. Advice for firefighters**

- Specific methods : Use fire control measures appropriate for the surrounding fire. Exposure to fire and heat radiation may cause gas receptacles to rupture. Cool endangered receptacles with water spray jet from a protected position. Prevent water used in emergency cases from entering sewers and drainage systems.  
If possible, stop flow of product.  
Use water spray or fog to knock down fire fumes if possible.  
Do not extinguish a leaking gas flame unless absolutely necessary. Spontaneous/explosive re-ignition may occur. Extinguish any other fire.  
Move containers away from the fire area if this can be done without risk.
- Special protective equipment for fire fighters : In confined space use self-contained breathing apparatus.  
Standard protective clothing and equipment (Self Contained Breathing Apparatus) for fire fighters.  
Standard EN 137 - Self-contained open-circuit compressed air breathing apparatus with full face mask.  
Standard EN 469 - Protective clothing for firefighters. Standard - EN 659: Protective gloves for firefighters.

### **SECTION 6: Accidental release measures**

#### **6.1. Personal precautions, protective equipment and emergency procedures**

: Try to stop release.

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		Country : SE / Language : EN

Evacuate area.  
 Monitor concentration of released product.  
 Consider the risk of potentially explosive atmospheres.  
 Wear self-contained breathing apparatus when entering area unless atmosphere is proved to be safe.  
 Eliminate ignition sources.  
 Ensure adequate air ventilation.  
 Act in accordance with local emergency plan.  
 Stay upwind.

### **6.2. Environmental precautions**

: Try to stop release.

### **6.3. Methods and material for containment and cleaning up**

: Ventilate area.

### **6.4. Reference to other sections**


: See also sections 8 and 13.

## **SECTION 7: Handling and storage**

### **7.1. Precautions for safe handling**

Safe use of the product : The product must be handled in accordance with good industrial hygiene and safety procedures.  
 Only experienced and properly instructed persons should handle gases under pressure.  
 Consider pressure relief device(s) in gas installations.  
 Ensure the complete gas system was (or is regularly) checked for leaks before use.  
 Do not smoke while handling product.  
 Use only properly specified equipment which is suitable for this product, its supply pressure and temperature. Contact your gas supplier if in doubt.  
 Avoid suck back of water, acid and alkalis.  
 Assess the risk of potentially explosive atmospheres and the need for explosion-proof equipment.  
 Purge air from system before introducing gas.  
 Take precautionary measures against static discharge.  
 Keep away from ignition sources (including static discharges).  
 Consider the use of only non-sparking tools.  
 Do not breathe gas.  
 Avoid release of product into atmosphere.  
 Ensure equipment is adequately earthed.

Safe handling of the gas receptacle : Refer to supplier's container handling instructions.  
 Do not allow backfeed into the container.  
 Protect cylinders from physical damage; do not drag, roll, slide or drop.  
 When moving cylinders, even for short distances, use a cart (trolley, hand truck, etc.) designed to transport cylinders.  
 Leave valve protection caps in place until the container has been secured against either a wall or bench or placed in a container stand and is ready for use.  
 If user experiences any difficulty operating cylinder valve discontinue use and contact supplier.  
 Never attempt to repair or modify container valves or safety relief devices.

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Damaged valves should be reported immediately to the supplier.

Keep container valve outlets clean and free from contaminants particularly oil and water.

Replace valve outlet caps or plugs and container caps where supplied as soon as container is disconnected from equipment.

Close container valve after each use and when empty, even if still connected to equipment.

Never attempt to transfer gases from one cylinder/container to another.

Never use direct flame or electrical heating devices to raise the pressure of a container.

Do not remove or deface labels provided by the supplier for the identification of the cylinder contents.

Suck back of water into the container must be prevented.

Open valve slowly to avoid pressure shock.

### 7.2. Conditions for safe storage, including any incompatibilities

: Observe all regulations and local requirements regarding storage of containers.

Containers should not be stored in conditions likely to encourage corrosion.

Container valve guards or caps should be in place.

Containers should be stored in the vertical position and properly secured to prevent them from falling over.

Stored containers should be periodically checked for general condition and leakage.

Keep container below 50°C in a well ventilated place.

Store containers in location free from fire risk and away from sources of heat and ignition.

Keep away from combustible materials.

Segregate from oxidant gases and other oxidants in store.

All electrical equipment in the storage areas should be compatible with the risk of a potentially explosive atmosphere.

### 7.3. Specific end use(s)

: None.

## SECTION 8: Exposure controls/personal protection

### 8.1. Control parameters

OEL (Occupational Exposure Limits) : No data available.

DNEL (Derived-No Effect Level) : No data available.

PNEC (Predicted No-Effect Concentration) : No data available.

### 8.2. Exposure controls

#### **8.2.1. Appropriate engineering controls**

: Provide adequate general and local exhaust ventilation.

Product to be handled in a closed system.

Systems under pressure should be regularly checked for leakages.

Gas detectors should be used when flammable gases/vapours may be released.


Consider the use of a work permit system e.g. for maintenance activities.

#### **8.2.2. Individual protection measures, e.g. personal protective equipment**

: A risk assessment should be conducted and documented in each work area to assess the risks related to the use of the product and to select the PPE that matches the relevant risk. The following recommendations should be considered:

PPE compliant to the recommended EN/ISO standards should be selected.



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- Eye/face protection : Wear safety glasses with side shields.  
Standard EN 166 - Personal eye-protection - specifications.
- Skin protection
  - Hand protection : Wear working gloves when handling gas containers.  
Standard EN 388 - Protective gloves against mechanical risk.
  - Other : Consider the use of flame resistant anti-static safety clothing.  
Standard EN ISO 14116 - Limited flame spread materials.  
Standard EN ISO 1149-5 - Protective clothing: Electrostatic properties.  
Wear safety shoes while handling containers.  
Standard EN ISO 20345 - Personal protective equipment - Safety footwear.
- Respiratory protection : None necessary.
- Thermal hazards : None in addition to the above sections.

### 8.2.3. Environmental exposure controls

: Refer to local regulations for restriction of emissions to the atmosphere. See section 13 for specific methods for waste gas treatment.

## SECTION 9: Physical and chemical properties

### 9.1. Information on basic physical and chemical properties

#### Appearance

- Physical state at 20°C / 101.3kPa : Gas.
- Colour : Colourless.

Odour : Odourless.

Odour threshold : Odour threshold is subjective and inadequate to warn of overexposure.

pH value : Not applicable for gases and gas mixtures.

Molar mass : 2 g/mol

Melting point : -259 °C

Boiling point : -253 °C

Flash point : Not applicable for gases and gas mixtures.

Critical temperature [°C] : -240 °C

Evaporation rate (ether=1) : Not applicable for gases and gas mixtures.

Flammability range : 4 - 77 vol %

Vapour pressure [20°C] : Not applicable.

Vapour pressure [50°C] : Not applicable.

Relative density, gas (air=1) : 0.07

Relative density, liquid (water=1) : 0.07

Solubility in water : 1.6 mg/l

Partition coefficient n-octanol/water [log Kow] : Not applicable for inorganic gases.

Auto-ignition temperature : 560 °C


Decomposition point [°C] : Not applicable.

Viscosity [20°C] : No reliable data available.

Explosive Properties : Not applicable.

Oxidising Properties : Not applicable.

### 9.2. Other information

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Other data : Burns with an invisible flame.

## SECTION 10: Stability and reactivity

### 10.1. Reactivity

: No reactivity hazard other than the effects described in sub-sections below.

### 10.2. Chemical stability

: Stable under normal conditions.

### 10.3. Possibility of hazardous reactions

: Can form explosive mixture with air.  
May react violently with oxidants.

### 10.4. Conditions to avoid

: Keep away from heat/sparks/open flames/hot surfaces. – No smoking.  
Avoid moisture in installation systems.

### 10.5. Incompatible materials

: Air, Oxidisers.  
For additional information on compatibility refer to ISO 11114.

### 10.6. Hazardous decomposition products

: Under normal conditions of storage and use, hazardous decomposition products should not be produced.

## SECTION 11: Toxicological information

### 11.1. Information on toxicological effects

**Acute toxicity** : No known toxicological effects from this product.

**Skin corrosion/irritation** : No known effects from this product.

**Serious eye damage/irritation** : No known effects from this product.

**Respiratory or skin sensitisation** : No known effects from this product.

**Germ cell mutagenicity** : No known effects from this product.

**Carcinogenicity** : No known effects from this product.

**Reproductive toxicity** : No known effects from this product.  
No known effects from this product.

**STOT-single exposure** : No known effects from this product.

**STOT-repeated exposure** : No known effects from this product.

**Aspiration hazard** : Not applicable for gases and gas mixtures.

## SECTION 12: Ecological information

### 12.1. Toxicity


Assessment : No ecological damage caused by this product.

EC50 48h - Daphnia magna [mg/l] : No data available.

EC50 72h - Algae [mg/l] : No data available.

LC50 96 h - Fish [mg/l] : No data available.

### 12.2. Persistence and degradability

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Assessment : No ecological damage caused by this product.

**12.3. Bioaccumulative potential**

Assessment : No data available.

**12.4. Mobility in soil**

Assessment : Because of its high volatility, the product is unlikely to cause ground or water pollution.  
Partition into soil is unlikely.

**12.5. Results of PBT and vPvB assessment**

Assessment : No data available.

**12.6. Other adverse effects**

Other adverse effects : No known effects from this product.  
Effect on the ozone layer : None.  
Global warming potential [CO<sub>2</sub>=1] : 6  
Effect on global warming : Contains greenhouse gas(es).  
When discharged in large quantities may contribute to the greenhouse effect.

**SECTION 13: Disposal considerations**

**13.1. Waste treatment methods**

Contact supplier if guidance is required.  
Do not discharge into areas where there is a risk of forming an explosive mixture with air.  
Waste gas should be flared through a suitable burner with flash back arrestor.  
Do not discharge into any place where its accumulation could be dangerous.  
Ensure that the emission levels from local regulations or operating permits are not exceeded.  
Refer to the EIGA code of practice Doc.30 "Disposal of Gases", downloadable at <http://www.eiga.org> for more guidance on suitable disposal methods.  
Return unused product in original cylinder to supplier.

List of hazardous waste codes (from Commission Decision 2001/118/EC) : 16 05 04 \*: Gases in pressure containers (including halons) containing dangerous substances.

**13.2. Additional information**

: External treatment and disposal of waste should comply with applicable local and/or national regulations.


**SECTION 14: Transport information**

**14.1. UN number**

UN-No. : 1049

**14.2. UN proper shipping name**

Transport by road/rail (ADR/RID) : HYDROGEN, COMPRESSED  
Transport by air (ICAO-TI / IATA-DGR) : Hydrogen, compressed  
Transport by sea (IMDG) : HYDROGEN, COMPRESSED

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		Country : SE / Language : EN

### 14.3. Transport hazard class(es)

**Labelling** :



2.1 : Flammable gases.

**Transport by road/rail (ADR/RID)**

Class : 2.  
Classification code : 1F.  
Hazard identification number : 23.  
Tunnel Restriction : B/D - Tank carriage : Passage forbidden through tunnels of category B, C, D and E. Other carriage : Passage forbidden through tunnels of category D and E.

**Transport by air (ICAO-TI / IATA-DGR)**

Class / Div. (Sub. risk(s)) : 2.1

**Transport by sea (IMDG)**

Class / Div. (Sub. risk(s)) : 2.1  
Emergency Schedule (EmS) - Fire : F-D.  
Emergency Schedule (EmS) - Spillage : S-U.

### 14.4. Packing group

Transport by road/rail (ADR/RID) : Not established.  
Transport by air (ICAO-TI / IATA-DGR) : Not established.  
Transport by sea (IMDG) : Not established.

### 14.5. Environmental hazards


Transport by road/rail (ADR/RID) : None.  
Transport by air (ICAO-TI / IATA-DGR) : None.  
Transport by sea (IMDG) : None.

### 14.6. Special precautions for user

**Packing Instruction(s)**

Transport by road/rail (ADR/RID) : P200.  
Transport by air (ICAO-TI / IATA-DGR)  
    Passenger and Cargo Aircraft : Forbidden.  
    Cargo Aircraft only : 200.  
Transport by sea (IMDG) : P200.

Special transport precautions : Avoid transport on vehicles where the load space is not separated from the driver's compartment.  
Ensure vehicle driver is aware of the potential hazards of the load and knows what to do in the event of an accident or an emergency.  
Before transporting product containers:  
- Ensure there is adequate ventilation.  
- Ensure that containers are firmly secured.  
- Ensure cylinder valve is closed and not leaking.

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- Ensure valve outlet cap nut or plug (where provided) is correctly fitted.
- Ensure valve protection device (where provided) is correctly fitted.

#### 14.7. Transport in bulk according to Annex II of Marpol and the IBC Code

: Not applicable.

### **SECTION 15: Regulatory information**

#### 15.1. Safety, health and environmental regulations/legislation specific for the substance or mixture

##### **EU-Regulations**

Restrictions on use : None.  
Seveso Directive : 2012/18/EU (Seveso III) : Listed.

##### **National regulations**

National legislation : Ensure all national/local regulations are observed.

#### 15.2. Chemical safety assessment

A CSA does not need to be carried out for this product.


### **SECTION 16: Other information**

Indication of changes : Revised safety data sheet in accordance with commission regulation (EU) No 453/2010.

Abbreviations and acronyms : ATE - Acute Toxicity Estimate  
CLP - Classification Labelling Packaging Regulation; Regulation (EC) No 1272/2008  
REACH - Registration, Evaluation, Authorisation and Restriction of Chemicals Regulation (EC) No 1907/2006  
EINECS - European Inventory of Existing Commercial Chemical Substances  
CAS# - Chemical Abstract Service number  
PPE - Personal Protection Equipment  
LC50 - Lethal Concentration to 50 % of a test population  
RMM - Risk Management Measures  
PBT - Persistent, Bioaccumulative and Toxic  
vPvB - Very Persistent and Very Bioaccumulative  
STOT- SE : Specific Target Organ Toxicity - Single Exposure  
CSA - Chemical Safety Assessment  
EN - European Standard  
UN - United Nations  
ADR - European Agreement concerning the International Carriage of Dangerous Goods by Road  
IATA - International Air Transport Association  
IMDG code - International Maritime Dangerous Goods  
RID - Regulations concerning the International Carriage of Dangerous Goods by Rail  
WGK - Water Hazard Class

Training advice : Ensure operators understand the flammability hazard.

Full text of H- and EUH-statements

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		Country : SE / Language : EN

Flam. Gas 1	Flammable gases, Category 1
Press. Gas (Comp.)	Gases under pressure : Compressed gas
H220	Extremely flammable gas.
H280	Contains gas under pressure; may explode if heated.

DISCLAIMER OF LIABILITY

: Before using this product in any new process or experiment, a thorough material compatibility and safety study should be carried out.

Details given in this document are believed to be correct at the time of going to press.

Whilst proper care has been taken in the preparation of this document, no liability for injury or damage resulting from its use can be accepted.

## C.1.3: Nitrogen

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		Country : DK / Language : EN

### SECTION 1: Identification of the substance/mixture and of the company/undertaking

#### 1.1. Product identifier

Trade name : Nitrogen, Nitrogen compressed, Nitrogen N48, Nitrogen N52, Nitrogen HG, Lasal 1, Lasal 2001, Aligal 1, Alphagaz N2 1, Alphagaz N2 2, Alphagaz 1 Nitrogen, Alphagaz 2 Nitrogen, Lasal 1, Phargalis 1, Albee Cool N2

SDS no : NOAL\_0089A

Chemical description : Nitrogen  
CAS-No. : 7727-37-9  
EC-No. : 231-783-9  
EC Index-No. : ---

Registration-No. : Listed in Annex IV / V REACH, exempted from registration.

Chemical formula : N<sub>2</sub>

#### 1.2. Relevant identified uses of the substance or mixture and uses advised against

Relevant identified uses : Industrial and professional. Perform risk assessment prior to use.  
Test gas/Calibration gas.  
Laboratory use.  
Purge gas, diluting gas, inerting gas.  
Shield gas for welding processes.  
Use for manufacture of electronic/photovoltaic components.  
Contact supplier for more information on uses.

Uses advised against : Consumer use.

#### 1.3. Details of the supplier of the safety data sheet

##### Company identification

AIR LIQUIDE Denmark A/S  
Høje Taastrupvej 42  
2630 Taastrup - DENMARK  
T +45 76 25 25 25  
[eunordic-sds@airliquide.com](mailto:eunordic-sds@airliquide.com)

E-Mail address (competent person) : eunordic-sds@airliquide.com

#### 1.4. Emergency telephone number


Emergency telephone number : 112  
Availability  
( 24 / 7 )

### SECTION 2: Hazards identification

#### 2.1. Classification of the substance or mixture

##### Classification according to Regulation (EC) No. 1272/2008 [CLP]

Physical hazards                      Gases under pressure : Compressed gas                      H280

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		Country : DK / Language : EN

## 2.2. Label elements

### Labelling according to Regulation (EC) No. 1272/2008 [CLP]

Hazard pictograms (CLP) :



GHS04

Signal word (CLP) :

Warning

Hazard statements (CLP) :

H280 - Contains gas under pressure; may explode if heated..

Precautionary statements (CLP)

- Storage : P403 - Store in a well-ventilated place..

## 2.3. Other hazards

: Asphyxiant in high concentrations.

## SECTION 3: Composition/information on ingredients

### 3.1. Substances

Name	Product identifier	Composition [V-%]:	Classification according to Regulation (EC) No. 1272/2008 [CLP]
Nitrogen	(CAS-No.) 7727-37-9 (EC-No.) 231-783-9 (EC Index-No.) --- (Registration-No.) *1	100	Press. Gas (Comp.), H280

Contains no other components or impurities which will influence the classification of the product.

\*1: Listed in Annex IV / V REACH, exempted from registration.

\*2: Registration deadline not expired.

\*3: Registration not required: Substance manufactured or imported < 1t/y.

### 3.2. Mixtures


: Not established.

## SECTION 4: First aid measures

### 4.1. Description of first aid measures

- Inhalation : Remove victim to uncontaminated area wearing self contained breathing apparatus. Keep victim warm and rested. Call a doctor. Apply artificial respiration if breathing stopped.
- Skin contact : Adverse effects not expected from this product.
- Eye contact : Adverse effects not expected from this product.
- Ingestion : Ingestion is not considered a potential route of exposure.



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**4.2. Most important symptoms and effects, both acute and delayed**

: In high concentrations may cause asphyxiation. Symptoms may include loss of mobility/consciousness. Victim may not be aware of asphyxiation.  
Refer to section 11.

**4.3. Indication of any immediate medical attention and special treatment needed**

: None.

**SECTION 5: Firefighting measures**

**5.1. Extinguishing media**

- Suitable extinguishing media : Water spray or fog.  
- Unsuitable extinguishing media : Do not use water jet to extinguish.

**5.2. Special hazards arising from the substance or mixture**

Specific hazards : Exposure to fire may cause containers to rupture/explode.  
Hazardous combustion products : None.

**5.3. Advice for firefighters**

Specific methods : Use fire control measures appropriate for the surrounding fire. Exposure to fire and heat radiation may cause gas receptacles to rupture. Cool endangered receptacles with water spray jet from a protected position. Prevent water used in emergency cases from entering sewers and drainage systems.  
If possible, stop flow of product.  
Use water spray or fog to knock down fire fumes if possible.  
Move containers away from the fire area if this can be done without risk.


Special protective equipment for fire fighters : In confined space use self-contained breathing apparatus.  
Standard protective clothing and equipment (Self Contained Breathing Apparatus) for fire fighters.  
Standard EN 137 - Self-contained open-circuit compressed air breathing apparatus with full face mask.  
Standard EN 469 - Protective clothing for firefighters. Standard - EN 659: Protective gloves for firefighters.

**SECTION 6: Accidental release measures**

**6.1. Personal precautions, protective equipment and emergency procedures**

: Try to stop release.  
Evacuate area.  
Wear self-contained breathing apparatus when entering area unless atmosphere is proved to be safe.  
Ensure adequate air ventilation.  
Act in accordance with local emergency plan.  
Stay upwind.  
Oxygen detectors should be used when asphyxiating gases may be released.

**6.2. Environmental precautions**

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: Try to stop release.

### **6.3. Methods and material for containment and cleaning up**

: Ventilate area.

### **6.4. Reference to other sections**

: See also sections 8 and 13.

## **SECTION 7: Handling and storage**

### **7.1. Precautions for safe handling**

Safe use of the product


- : The product must be handled in accordance with good industrial hygiene and safety procedures.
- Only experienced and properly instructed persons should handle gases under pressure.
- Consider pressure relief device(s) in gas installations.
- Ensure the complete gas system was (or is regularly) checked for leaks before use.
- Do not smoke while handling product.
- Use only properly specified equipment which is suitable for this product, its supply pressure and temperature. Contact your gas supplier if in doubt.
- Avoid suck back of water, acid and alkalis.
- Do not breathe gas.
- Avoid release of product into atmosphere.

Safe handling of the gas receptacle

- : Refer to supplier's container handling instructions.
- Do not allow backfeed into the container.
- Protect cylinders from physical damage; do not drag, roll, slide or drop.
- When moving cylinders, even for short distances, use a cart (trolley, hand truck, etc.) designed to transport cylinders.
- Leave valve protection caps in place until the container has been secured against either a wall or bench or placed in a container stand and is ready for use.
- If user experiences any difficulty operating cylinder valve discontinue use and contact supplier.
- Never attempt to repair or modify container valves or safety relief devices.
- Damaged valves should be reported immediately to the supplier.
- Keep container valve outlets clean and free from contaminants particularly oil and water.
- Replace valve outlet caps or plugs and container caps where supplied as soon as container is disconnected from equipment.
- Close container valve after each use and when empty, even if still connected to equipment.
- Never attempt to transfer gases from one cylinder/container to another.
- Never use direct flame or electrical heating devices to raise the pressure of a container.
- Do not remove or deface labels provided by the supplier for the identification of the cylinder contents.
- Suck back of water into the container must be prevented.
- Open valve slowly to avoid pressure shock.

### **7.2. Conditions for safe storage, including any incompatibilities**

- : Observe all regulations and local requirements regarding storage of containers.
- Containers should not be stored in conditions likely to encourage corrosion.
- Container valve guards or caps should be in place.
- Containers should be stored in the vertical position and properly secured to prevent them from falling over.

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Stored containers should be periodically checked for general condition and leakage.

Keep container below 50°C in a well ventilated place.

Store containers in location free from fire risk and away from sources of heat and ignition.

Keep away from combustible materials.

### 7.3. Specific end use(s)

: None.

## SECTION 8: Exposure controls/personal protection

### 8.1. Control parameters

OEL (Occupational Exposure Limits) : No data available.

DNEL (Derived-No Effect Level) : No data available.

PNEC (Predicted No-Effect Concentration) : No data available.

### 8.2. Exposure controls

#### 8.2.1. Appropriate engineering controls

- : Provide adequate general and local exhaust ventilation.
- Systems under pressure should be regularly checked for leakages.
- Oxygen detectors should be used when asphyxiating gases may be released.
- Consider the use of a work permit system e.g. for maintenance activities.

#### 8.2.2. Individual protection measures, e.g. personal protective equipment

- : A risk assessment should be conducted and documented in each work area to assess the risks related to the use of the product and to select the PPE that matches the relevant risk. The following recommendations should be considered:  
PPE compliant to the recommended EN/ISO standards should be selected.

- Eye/face protection : Wear safety glasses with side shields.  
Standard EN 166 - Personal eye-protection - specifications.
- Skin protection
  - Hand protection : Wear working gloves when handling gas containers.  
Standard EN 388 - Protective gloves against mechanical risk.
  - Other : Wear safety shoes while handling containers.  
Standard EN ISO 20345 - Personal protective equipment - Safety footwear.
- Respiratory protection : Self contained breathing apparatus (SCBA) or positive pressure airline with mask are to be used in oxygen-deficient atmospheres.  
Standard EN 137 - Self-contained open-circuit compressed air breathing apparatus with full face mask.
- Thermal hazards : None in addition to the above sections.


#### 8.2.3. Environmental exposure controls

- : None necessary.

## SECTION 9: Physical and chemical properties

### 9.1. Information on basic physical and chemical properties

Appearance

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• Physical state at 20°C / 101.3kPa	: Gas.
• Colour	: Colourless.
Odour	: No odour warning properties.
Odour threshold	: Odour threshold is subjective and inadequate to warn of overexposure.
pH value	: Not applicable for gases and gas mixtures.
Molar mass	: 28 g/mol
Melting point	: -210 °C
Boiling point	: -196 °C
Flash point	: Not applicable for gases and gas mixtures.
Critical temperature [°C]	: -147 °C
Evaporation rate (ether=1)	: Not applicable for gases and gas mixtures.
Flammability range	: Non flammable.
Vapour pressure [20°C]	: Not applicable.
Vapour pressure [50°C]	: Not applicable.
Relative density, gas (air=1)	: 0.97
Relative density, liquid (water=1)	: Not applicable.
Solubility in water	: 20 mg/l
Partition coefficient n-octanol/water [log Kow]	: Not applicable for inorganic gases.
Auto-ignition temperature	: Non flammable.
Decomposition point [°C]	: Not applicable.
Viscosity [20°C]	: No reliable data available.
Explosive Properties	: Not applicable.
Oxidising Properties	: Not applicable.

## **9.2. Other information**

Other data : No additional information available

## **SECTION 10: Stability and reactivity**

### **10.1. Reactivity**

: No reactivity hazard other than the effects described in sub-sections below.

### **10.2. Chemical stability**

: Stable under normal conditions.

### **10.3. Possibility of hazardous reactions**

: None.

### **10.4. Conditions to avoid**

: Avoid moisture in installation systems.

### **10.5. Incompatible materials**

: None.

For additional information on compatibility refer to ISO 11114.


### **10.6. Hazardous decomposition products**

: None.

## **SECTION 11: Toxicological information**

### **11.1. Information on toxicological effects**

**Acute toxicity** : No known toxicological effects from this product.

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		Country : DK / Language : EN

<b>Skin corrosion/irritation</b>	: No known effects from this product.
<b>Serious eye damage/irritation</b>	: No known effects from this product.
<b>Respiratory or skin sensitisation</b>	: No known effects from this product.
<b>Germ cell mutagenicity</b>	: No known effects from this product.
<b>Carcinogenicity</b>	: No known effects from this product.
<b>Reproductive toxicity</b>	: No known effects from this product. No known effects from this product.
<b>STOT-single exposure</b>	: No known effects from this product.
<b>STOT-repeated exposure</b>	: No known effects from this product.
<b>Aspiration hazard</b>	: Not applicable for gases and gas mixtures.

## SECTION 12: Ecological information

### 12.1. Toxicity

Assessment	: No ecological damage caused by this product.
EC50 48h - Daphnia magna [mg/l]	: No data available.
EC50 72h - Algae [mg/l]	: No data available.
LC50 96 h - Fish [mg/l]	: No data available.

### 12.2. Persistence and degradability

Assessment	: No ecological damage caused by this product.
------------	--

### 12.3. Bioaccumulative potential

Assessment	: No data available.
------------	----------------------

### 12.4. Mobility in soil

Assessment	: Because of its high volatility, the product is unlikely to cause ground or water pollution. Partition into soil is unlikely.
------------	---

### 12.5. Results of PBT and vPvB assessment

Assessment	: No data available.
------------	----------------------


### 12.6. Other adverse effects

Other adverse effects	: No known effects from this product.
Effect on the ozone layer	: None.
Effect on global warming	: None.

## SECTION 13: Disposal considerations

### 13.1. Waste treatment methods

May be vented to atmosphere in a well ventilated place.  
Do not discharge into any place where its accumulation could be dangerous.

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Return unused product in original cylinder to supplier.

List of hazardous waste codes (from Commission Decision 2001/118/EC)

: 16 05 05 : Gases in pressure containers other than those mentioned in 16 05 04.

**13.2. Additional information**

: External treatment and disposal of waste should comply with applicable local and/or national regulations.

**SECTION 14: Transport information**

**14.1. UN number**

UN-No. : 1066

**14.2. UN proper shipping name**

Transport by road/rail (ADR/RID) : NITROGEN, COMPRESSED

Transport by air (ICAO-TI / IATA-DGR) : Nitrogen, compressed

Transport by sea (IMDG) : NITROGEN, COMPRESSED

**14.3. Transport hazard class(es)**

Labelling :



2.2 : Non-flammable, non-toxic gases.

**Transport by road/rail (ADR/RID)**

Class : 2.

Classification code : 1A.

Hazard identification number : 20.

Tunnel Restriction : E - Passage forbidden through tunnels of category E.

**Transport by air (ICAO-TI / IATA-DGR)**

Class / Div. (Sub. risk(s)) : 2.2

**Transport by sea (IMDG)**

Class / Div. (Sub. risk(s)) : 2.2

Emergency Schedule (EmS) - Fire : F-C.

Emergency Schedule (EmS) - Spillage : S-V.

**14.4. Packing group**

Transport by road/rail (ADR/RID) : Not established.

Transport by air (ICAO-TI / IATA-DGR) : Not established.


Transport by sea (IMDG) : Not established.

**14.5. Environmental hazards**

Transport by road/rail (ADR/RID) : None.

Transport by air (ICAO-TI / IATA-DGR) : None.

Transport by sea (IMDG) : None.

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		Country : DK / Language : EN

#### **14.6. Special precautions for user**

##### **Packing Instruction(s)**

Transport by road/rail (ADR/RID) : P200.

Transport by air (ICAO-TI / IATA-DGR)

Passenger and Cargo Aircraft : 200.

Cargo Aircraft only : 200.

Transport by sea (IMDG) : P200.

Special transport precautions : Avoid transport on vehicles where the load space is not separated from the driver's compartment.  
 Ensure vehicle driver is aware of the potential hazards of the load and knows what to do in the event of an accident or an emergency.  
 Before transporting product containers:  
 - Ensure there is adequate ventilation.  
 - Ensure that containers are firmly secured.  
 - Ensure cylinder valve is closed and not leaking.  
 - Ensure valve outlet cap nut or plug (where provided) is correctly fitted.  
 - Ensure valve protection device (where provided) is correctly fitted.

#### **14.7. Transport in bulk according to Annex II of Marpol and the IBC Code**

: Not applicable.

### **SECTION 15: Regulatory information**

#### **15.1. Safety, health and environmental regulations/legislation specific for the substance or mixture**

##### **EU-Regulations**

Restrictions on use : None.

Seveso Directive : 2012/18/EU (Seveso III) : Not covered.

##### **National regulations**

National legislation : Ensure all national/local regulations are observed.


#### **15.2. Chemical safety assessment**

A CSA does not need to be carried out for this product.

### **SECTION 16: Other information**

Indication of changes : Revised safety data sheet in accordance with commission regulation (EU) No 453/2010.

Abbreviations and acronyms : ATE - Acute Toxicity Estimate  
 CLP - Classification Labelling Packaging Regulation; Regulation (EC) No 1272/2008  
 REACH - Registration, Evaluation, Authorisation and Restriction of Chemicals Regulation (EC) No 1907/2006  
 EINECS - European Inventory of Existing Commercial Chemical Substances  
 CAS# - Chemical Abstract Service number

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PPE - Personal Protection Equipment  
 LC50 - Lethal Concentration to 50 % of a test population  
 RMM - Risk Management Measures  
 PBT - Persistent, Bioaccumulative and Toxic  
 vPvB - Very Persistent and Very Bioaccumulative  
 STOT- SE : Specific Target Organ Toxicity - Single Exposure  
 CSA - Chemical Safety Assessment  
 EN - European Standard  
 UN - United Nations  
 ADR - European Agreement concerning the International Carriage of Dangerous Goods by Road  
 IATA - International Air Transport Association  
 IMDG code - International Maritime Dangerous Goods  
 RID - Regulations concerning the International Carriage of Dangerous Goods by Rail  
 WGK - Water Hazard Class

Training advice : The hazard of asphyxiation is often overlooked and must be stressed during operator training.

Full text of H- and EUH-statements

Press. Gas (Comp.)	Gases under pressure : Compressed gas
H280	Contains gas under pressure; may explode if heated.

DISCLAIMER OF LIABILITY : Before using this product in any new process or experiment, a thorough material compatibility and safety study should be carried out.

Details given in this document are believed to be correct at the time of going to press.

Whilst proper care has been taken in the preparation of this document, no liability for injury or damage resulting from its use can be accepted.



# C.1.4: Oxygen

## Safety Data Sheet

according to Regulation (EU) 2015/830

### Oxygen



Date of issue: 28/12/2010

Supersedes: 17/12/2015

Revision date: 10/07/2019

Version: 1.2

SDS reference: 2010479

**Danger**



### SECTION 1: Identification of the substance/mixture and of the company/undertaking

#### 1.1. Product identifier

Trade name : Oxygen, Alphahaz™ Oxygen, Purified/ Compressed Oxygen, Medical Oxygen, PRESENCE™, TAKEO™, Breathing Oxygen.  
SDS no : 2010479  
Chemical description : Oxygen  
CAS-No. : 7782-44-7  
EC-No. : 231-956-9  
EC Index-No. : 008-001-00-8  
Registration-No. : Listed in Annex IV / V REACH, exempted from registration.  
Chemical formula : O<sub>2</sub>

#### 1.2. Relevant identified uses of the substance or mixture and uses advised against

Relevant identified uses : Industrial and professional. Perform risk assessment prior to use.  
Test gas/Calibration gas.  
Welding, cutting, heating and brazing.  
Shield gas for welding processes.  
Use for manufacture of electronic/photovoltaic components.  
Water treatment.  
Laser gas.  
Laboratory use.  
Food applications.  
Contact supplier for more information on uses.

Uses advised against : Consumer use.

#### 1.3. Details of the supplier of the safety data sheet

Company identification : AIR LIQUIDE SINGAPORE PTE LTD  
HEAD OFFICE : 2 VENTURE DRIVE, VISION EXCHANGE, #22-28, SINGAPORE 608526  
SPECIALGASES OFFICE, NO 24 JALAN BUROH SINGAPORE 619480  
T +65 6 265 3788  
<https://industry.airliquide.sg/resources/safety-data-sheets-sds>  
Sg-info@airliquide.com

#### 1.4. Emergency telephone number

Emergency telephone number : +65 6265 3788, +65 9619 9229 (After Office Hour)

### SECTION 2: Hazards identification

#### 2.1. Classification of the substance or mixture

AIR LIQUIDE SINGAPORE PTE LTD  
HEAD OFFICE : 2 VENTURE DRIVE,  
VISION EXCHANGE, #22-28,  
SINGAPORE 608526 SPECIALGASES  
OFFICE, NO 24 JALAN BUROH  
SINGAPORE 619480  
+65 6 265 3788

EN (English)

SDS Ref.: 2010479

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- Inhalation : Remove victim to uncontaminated area wearing self contained breathing apparatus. Keep victim warm and rested. Call a doctor. Perform cardiopulmonary resuscitation if breathing stopped.  
Remove victim to uncontaminated area.
- Skin contact : Adverse effects not expected from this product.
- Eye contact : Adverse effects not expected from this product.
- Ingestion : Ingestion is not considered a potential route of exposure.

**4.2. Most important symptoms and effects, both acute and delayed**

- : Continuous inhalation of concentrations higher than 75% may cause nausea, dizziness, respiratory difficulty and convulsion.  
Refer to section 11.

**4.3. Indication of any immediate medical attention and special treatment needed**

- : None.

**SECTION 5: Firefighting measures****5.1. Extinguishing media**

- Suitable extinguishing media : Water spray or fog.
- Unsuitable extinguishing media : Do not use water jet to extinguish.

**5.2. Special hazards arising from the substance or mixture**

- Specific hazards : Supports combustion.  
Exposure to fire may cause containers to rupture/explode.
- Hazardous combustion products : None.

**5.3. Advice for firefighters**

- Specific methods : Use fire control measures appropriate for the surrounding fire. Exposure to fire and heat radiation may cause gas receptacles to rupture. Cool endangered receptacles with water spray jet from a protected position. Prevent water used in emergency cases from entering sewers and drainage systems.  
If possible, stop flow of product.  
Use water spray or fog to knock down fire fumes if possible.  
Move containers away from the fire area if this can be done without risk.
- Special protective equipment for fire fighters : Standard protective clothing and equipment (Self Contained Breathing Apparatus) for fire fighters.  
Standard EN 469 - Protective clothing for firefighters. Standard - EN 659: Protective gloves for firefighters.

**SECTION 6: Accidental release measures****6.1. Personal precautions, protective equipment and emergency procedures**

- : Try to stop release.  
Evacuate area.  
Monitor concentration of released product.  
Wear self-contained breathing apparatus when entering area unless atmosphere is proved to be safe.  
Eliminate ignition sources.  
Ensure adequate air ventilation.  
Act in accordance with local emergency plan.  
Stay upwind.

**6.2. Environmental precautions**

: Try to stop release.

**6.3. Methods and material for containment and cleaning up**

: Ventilate area.

**6.4. Reference to other sections**

: See also sections 8 and 13.

**SECTION 7: Handling and storage****7.1. Precautions for safe handling**

Safe use of the product

: Do not breathe gas.

The product must be handled in accordance with good industrial hygiene and safety procedures.

Only experienced and properly instructed persons should handle gases under pressure.

Consider pressure relief device(s) in gas installations.

Ensure the complete gas system was (or is regularly) checked for leaks before use.

Do not smoke while handling product.

Keep equipment free from oil and grease. For more guidance, refer to the EIGA Doc. 33 - Cleaning of Equipment for Oxygen Service downloadable at <http://www.eiga.eu>.

Use no oil or grease.

Use only properly specified equipment which is suitable for this product, its supply pressure and temperature. Contact your gas supplier if in doubt.

Use only oxygen approved lubricants and oxygen approved sealings.

Use only with equipment cleaned for oxygen service and rated for cylinder pressure.

Avoid suck back of water, acid and alkalis.

Safe handling of the gas receptacle

: Refer to supplier's container handling instructions.

Do not allow backfeed into the container.

Protect cylinders from physical damage; do not drag, roll, slide or drop.

When moving cylinders, even for short distances, use a cart (trolley, hand truck, etc.) designed to transport cylinders.

Leave valve protection caps in place until the container has been secured against either a wall or bench or placed in a container stand and is ready for use.

If user experiences any difficulty operating cylinder valve discontinue use and contact supplier.

Never attempt to repair or modify container valves or safety relief devices.

Damaged valves should be reported immediately to the supplier.

Keep container valve outlets clean and free from contaminants particularly oil and water.

Replace valve outlet caps or plugs and container caps where supplied as soon as container is disconnected from equipment.

Close container valve after each use and when empty, even if still connected to equipment.

Never attempt to transfer gases from one cylinder/container to another.

Never use direct flame or electrical heating devices to raise the pressure of a container.

Do not remove or deface labels provided by the supplier for the identification of the cylinder contents.

Suck back of water into the container must be prevented.

Open valve slowly to avoid pressure shock.

**7.2. Conditions for safe storage, including any incompatibilities**

- : Observe all regulations and local requirements regarding storage of containers.
- Containers should not be stored in conditions likely to encourage corrosion.
- Container valve guards or caps should be in place.
- Containers should be stored in the vertical position and properly secured to prevent them from falling over.
- Stored containers should be periodically checked for general condition and leakage.
- Keep container below 50°C in a well ventilated place.
- Segregate from flammable gases and other flammable materials in store.
- Store containers in location free from fire risk and away from sources of heat and ignition.
- Keep away from combustible materials.

### **7.3. Specific end use(s)**

- : None.

## **SECTION 8: Exposure controls/personal protection**

### **8.1. Control parameters**

- OEL (Occupational Exposure Limits) : None available.
- DNEL (Derived-No Effect Level) : None available.
- PNEC (Predicted No-Effect Concentration) : None available.

### **8.2. Exposure controls**

#### **8.2.1. Appropriate engineering controls**

- : Provide adequate general and local exhaust ventilation.
- Systems under pressure should be regularly checked for leakages.
- Avoid oxygen rich (>23,5%) atmospheres.
- Gas detectors should be used when oxidising gases may be released.
- Consider the use of a work permit system e.g. for maintenance activities.

#### **8.2.2. Individual protection measures, e.g. personal protective equipment**

- : A risk assessment should be conducted and documented in each work area to assess the risks related to the use of the product and to select the PPE that matches the relevant risk. The following recommendations should be considered:
  - PPE compliant to the recommended EN/ISO standards should be selected.

- Eye/face protection : Wear safety glasses with side shields.  
Standard EN 166 - Personal eye-protection - specifications.
- Skin protection
  - Hand protection : Wear working gloves when handling gas containers.  
Standard EN 388 - Protective gloves against mechanical risk.
  - Other : Consider the use of flame resistant safety clothing.  
Standard EN ISO 14116 - Limited flame spread materials.  
Wear safety shoes while handling containers.  
Standard EN ISO 20345 - Personal protective equipment - Safety footwear.
- Respiratory protection : None necessary.
- Thermal hazards : None in addition to the above sections.

**8.2.3. Environmental exposure controls**

: Refer to local regulations for restriction of emissions to the atmosphere. See section 13 for specific methods for waste gas treatment.

**SECTION 9: Physical and chemical properties****9.1. Information on basic physical and chemical properties**

## Appearance

- Physical state at 20°C / 101.3kPa : Gas
- Colour : Colourless.

Odour : No odour warning properties.

Odour threshold : Odour threshold is subjective and inadequate to warn of overexposure.

pH : Not applicable for gases and gas mixtures.

Melting point / Freezing point : -219 °C

Boiling point : -183 °C

Flash point : Not applicable for gases and gas mixtures.

Evaporation rate : Not applicable for gases and gas mixtures.

Flammability (solid, gas) : Non flammable.

Explosive limits : Non flammable.

Vapour pressure [20°C] : Not applicable.

Vapour pressure [50°C] : Not applicable.

Vapour density : Not applicable.

Relative density, liquid (water=1) : 1.1

Relative density, gas (air=1) : 1.1

Water solubility : 39 mg/l

Partition coefficient n-octanol/water (Log Kow) : Not applicable for inorganic products.

Auto-ignition temperature : Non flammable.

Decomposition temperature : Not applicable.

Viscosity, kinematic : No reliable data available.

Explosive properties : Not applicable.

Oxidising properties : Oxidiser.

**9.2. Other information**

Molar mass : 32 g/mol

Critical temperature [°C] : -118 °C

- Coefficient of oxygen equivalency (Ci) : 1

**SECTION 10: Stability and reactivity****10.1. Reactivity**

: No reactivity hazard other than the effects described in sub-sections below.

**10.2. Chemical stability**

: Stable under normal conditions.

**10.3. Possibility of hazardous reactions**

: Violently oxidises organic material.

**10.4. Conditions to avoid**

: Avoid moisture in installation systems.

**10.5. Incompatible materials**

: May react violently with combustible materials.

May react violently with reducing agents.

Keep equipment free from oil and grease. For more guidance, refer to the EIGA Doc. 33 - Cleaning of Equipment for Oxygen Service downloadable at <http://www.eiga.eu>.

Consider the potential toxicity hazard due to the presence of chlorinated or fluorinated polymers in high pressure (&gt; 30 bar) oxygen lines in case of combustion.

For additional information on compatibility refer to ISO 11114.

**10.6. Hazardous decomposition products**

: None.

**SECTION 11: Toxicological information****11.1. Information on toxicological effects**

<b>Acute toxicity</b>	: No known toxicological effects from this product.
<b>Skin corrosion/irritation</b>	: No known effects from this product.
<b>Serious eye damage/irritation</b>	: No known effects from this product.
<b>Respiratory or skin sensitisation</b>	: No known effects from this product.
<b>Germ cell mutagenicity</b>	: No known effects from this product.
<b>Carcinogenicity</b>	: No known effects from this product.
<b>Toxic for reproduction : Fertility</b>	: No known effects from this product.
<b>Toxic for reproduction : unborn child</b>	: No known effects from this product.
<b>STOT-single exposure</b>	: No known effects from this product.
<b>STOT-repeated exposure</b>	: No known effects from this product.
<b>Aspiration hazard</b>	: Not applicable for gases and gas mixtures.

**SECTION 12: Ecological information****12.1. Toxicity**

Assessment	: No ecological damage caused by this product.
EC50 48h - Daphnia magna [mg/l]	: No data available.
EC50 72h - Algae [mg/l]	: No data available.
LC50 96 h - Fish [mg/l]	: No data available.

**12.2. Persistence and degradability**

Assessment	: No ecological damage caused by this product.
------------	--

**12.3. Bioaccumulative potential**

Assessment	: No data available.
------------	----------------------

**12.4. Mobility in soil**

Assessment	: Because of its high volatility, the product is unlikely to cause ground or water pollution. Partition into soil is unlikely.
------------	---

**12.5. Results of PBT and vPvB assessment**

Assessment : No data available.

**12.6. Other adverse effects**

Other adverse effects : No known effects from this product.  
 Effect on the ozone layer : None.  
 Effect on global warming : None.

**SECTION 13: Disposal considerations**

**13.1. Waste treatment methods**

Contact supplier if guidance is required.  
 May be vented to atmosphere in a well ventilated place.  
 Do not discharge into any place where its accumulation could be dangerous.  
 Ensure that the emission levels from local regulations or operating permits are not exceeded.  
 Refer to the EIGA code of practice Doc.30 "Disposal of Gases", downloadable at <http://www.eiga.eu> for more guidance on suitable disposal methods.  
 Return unused product in original cylinder to supplier.  
 : 16 05 04 \*: Gases in pressure containers (including halons) containing hazardous substances.

List of hazardous waste codes (from Commission Decision 2000/532/EC as amended)

**13.2. Additional information**

: External treatment and disposal of waste should comply with applicable local and/or national regulations.

**SECTION 14: Transport information**

**14.1. UN number**

UN-No. : 1072

**14.2. UN proper shipping name**

Transport by road/rail (ADR/RID) : OXYGEN, COMPRESSED  
 Transport by air (ICAO-TI / IATA-DGR) : Oxygen, compressed  
 Transport by sea (IMDG) : OXYGEN, COMPRESSED

**14.3. Transport hazard class(es)**

Labelling :



2.2 : Non-flammable, non-toxic gases.  
 5.1 : Oxidizing substances.

**Transport by road/rail (ADR/RID)**

Class : 2  
 Classification code : 10  
 Hazard identification number : 25  
 Tunnel Restriction : E - Passage forbidden through tunnels of category E



**Transport by air (ICAO-TI / IATA-DGR)**

Class / Div. (Sub. risk(s)) : 2.2 (5.1)

**Transport by sea (IMDG)**

Class / Div. (Sub. risk(s)) : 2.2 (5.1)

Emergency Schedule (EmS) - Fire : F-C

Emergency Schedule (EmS) - Spillage : S-W

**14.4. Packing group**

Transport by road/rail (ADR/RID) : Not applicable

Transport by air (ICAO-TI / IATA-DGR) : Not applicable

Transport by sea (IMDG) : Not applicable

**14.5. Environmental hazards**

Transport by road/rail (ADR/RID) : None.

Transport by air (ICAO-TI / IATA-DGR) : None.

Transport by sea (IMDG) : None.

**14.6. Special precautions for user****Packing Instruction(s)**

Transport by road/rail (ADR/RID) : P200

Transport by air (ICAO-TI / IATA-DGR)

Passenger and Cargo Aircraft : 200.

Cargo Aircraft only : 200.

Transport by sea (IMDG) : P200

Special transport precautions : Avoid transport on vehicles where the load space is not separated from the driver's compartment.  
Ensure vehicle driver is aware of the potential hazards of the load and knows what to do in the event of an accident or an emergency.  
Before transporting product containers:  
- Ensure there is adequate ventilation.  
- Ensure that containers are firmly secured.  
- Ensure cylinder valve is closed and not leaking.  
- Ensure valve outlet cap nut or plug (where provided) is correctly fitted.  
- Ensure valve protection device (where provided) is correctly fitted.

**14.7. Transport in bulk according to Annex II of Marpol and the IBC Code**

: Not applicable.

**SECTION 15: Regulatory information****15.1. Safety, health and environmental regulations/legislation specific for the substance or mixture****EU-Regulations**

Restrictions on use : None.

Seveso Directive : 2012/18/EU (Seveso III) : Listed.

**National regulations**

National legislation : Ensure all national/local regulations are observed.

**15.2. Chemical safety assessment**

: A CSA does not need to be carried out for this product.

**SECTION 16: Other information**

Indication of changes	: Revised safety data sheet in accordance with commission regulation (EU) No 2015/830.
Abbreviations and acronyms	: ATE - Acute Toxicity Estimate CLP - Classification Labelling Packaging Regulation; Regulation (EC) No 1272/2008 REACH - Registration, Evaluation, Authorisation and Restriction of Chemicals Regulation (EC) No 1907/2006 EINECS - European Inventory of Existing Commercial Chemical Substances CAS# - Chemical Abstract Service number PPE - Personal Protection Equipment LC50 - Lethal Concentration to 50 % of a test population RMM - Risk Management Measures PBT - Persistent, Bioaccumulative and Toxic vPvB - Very Persistent and Very Bioaccumulative STOT- SE : Specific Target Organ Toxicity - Single Exposure CSA - Chemical Safety Assessment EN - European Standard UN - United Nations ADR - European Agreement concerning the International Carriage of Dangerous Goods by Road IATA - International Air Transport Association IMDG code - International Maritime Dangerous Goods RID - Regulations concerning the International Carriage of Dangerous Goods by Rail WGK - Water Hazard Class STOT - RE : Specific Target Organ Toxicity - Repeated Exposure
Training advice	: Ensure operators understand the hazard of oxygen enrichment.
DISCLAIMER OF LIABILITY	: Before using this product in any new process or experiment, a thorough material compatibility and safety study should be carried out. Details given in this document are believed to be correct at the time of going to press. Whilst proper care has been taken in the preparation of this document, no liability for injury or damage resulting from its use can be accepted.

**End of document**

**C.1.5: Argon****Argon****2010483**

2.2 : Non-flammable, non-toxic gases

**Warning****SECTION 1. Identification of the substance/mixture and of the company/undertaking****1.1. Product identifier**

**Trade name** : Argon, ALPHAGAZ™ Argon, SMARTOP™ Argon, Purified /Compressed Argon, Blueshield™ Argon, ARCAL™ 1, ARCAL™ Prime

**SDS Nr** : 2010483

**Chemical description** : Argon  
CAS No :7440-37-1  
EC No :231-147-0  
Index No :---

**Chemical formula** : Ar

**1.2. Relevant identified uses of the substance or mixture and uses advised against**

**Relevant identified uses** : Industrial and professional. Perform risk assessment prior to use.  
Test gas/Calibration gas. Laboratory use.  
Shield gas for welding processes. Contact supplier for more information on uses.

**1.3. Details of the supplier of the safety data sheet**

**Company identification** : AIR LIQUIDE SINGAPORE PTE LTD  
HEAD OFFICE : 438B ALEXANDRA ROAD,  
BLOCK B, ALEXANDRA TECHNOPARK #07-01  
119968 SINGAPORE  
SPECIAL GASES OFFICE : NO 24 JALAN BUROH SINGAPORE 619480

**1.4. Emergency telephone number**

**Emergency telephone number** : +65 6265 3788, +65 9619 9229 (After Office Hour)

**SECTION 2. Hazards identification****2.1. Classification of the substance or mixture****Hazard Class and Category Code Regulation EC 1272/2008 (CLP)**

• **Physical hazards** : Gases under pressure - Compressed gas - Warning - (CLP : Press. Gas) - H280

**Classification EC 67/548 or EC 1999/45**

: Not classified as dangerous substance / mixture.  
Not included in Annex VI.  
No EC labelling required.

**2.2. Label elements****AIR LIQUIDE SINGAPORE PTE LTD****In case of emergency : +65 6265 3788, +65 9619 9229 (After Office Hour)**

HEAD OFFICE : 438B ALEXANDRA ROAD, BLOCK B, ALEXANDRA TECHNOPARK #07-01 119968 SINGAPORE

SPECIAL GASES OFFICE : NO 24 JALAN BUROH SINGAPORE 619480

**Argon****2010483****SECTION 2. Hazards identification (continued)**Labelling Regulation EC 1272/2008 (CLP)

## • Hazard pictograms



- Hazard pictograms code : GHS04
- Signal word : Warning
- Hazard statements : H280 - Contains gas under pressure; may explode if heated.
- Precautionary statements
  - Storage : P403 - Store in a well-ventilated place.

**2.3. Other hazards**

: Asphyxiant in high concentrations.

**SECTION 3. Composition/information on ingredients****3.1. Substance / 3.2. Mixture****Substance.**

Substance name	Contents	CAS No EC No Index No Registration no	Classification(DSD)	Classification(CLP)
Argon	: 100 %	7440-37-1 231-147-0 ----- * 1	Not classified (DSD)	Press. Gas Compressed (H280)

Contains no other components or impurities which will influence the classification of the product.

\* 1: Listed in Annex IV / V REACH, exempted from registration.

\* 2: Registration deadline not expired.

\* 3: Registration not required: Substance manufactured or imported &lt; 1t/y.

Full text of R-phrases see section 16. Full text of H-statements see section 16.

**SECTION 4. First aid measures****4.1. Description of first aid measures****First aid measures**

- Inhalation : Remove victim to uncontaminated area wearing self contained breathing apparatus. Keep victim warm and rested. Call a doctor. Apply artificial respiration if breathing stopped.
- Skin contact : Adverse effects not expected from this product.
- Eye contact : Adverse effects not expected from this product.
- Ingestion : Ingestion is not considered a potential route of exposure.

**4.2. Most important symptoms and effects, both acute and delayed**

: In high concentrations may cause asphyxiation. Symptoms may include loss of mobility/ consciousness. Victim may not be aware of asphyxiation. Refer to section 11.

**4.3. Indication of any immediate medical attention and special treatment needed**

: None.

**Argon****2010483****SECTION 4. First aid measures (continued)****SECTION 5. Firefighting measures****5.1. Extinguishing media****Extinguishing media**

- Suitable extinguishing media : Water spray or fog.
- Unsuitable extinguishing media : Do not use water jet to extinguish.

**5.2. Special hazards arising from the substance or mixture**

- Specific hazards : Exposure to fire may cause containers to rupture/explode.
- Hazardous combustion products : None.

**5.3. Advice for fire-fighters**

- Specific methods : If possible, stop flow of product.  
Use fire control measures appropriate for the surrounding fire. Exposure to fire and heat radiation may cause gas receptacles to rupture. Cool endangered receptacles with water spray jet from a protected position.  
Move away from the container and cool with water from a protected position.  
Use water spray or fog to knock down fire fumes if possible.
- Special protective equipment for fire fighters : Use self-contained breathing apparatus.  
Standard EN 137 - Self-contained open-circuit compressed air breathing apparatus with full face mask.  
Standard protective clothing and equipment (Self Contained Breathing Apparatus) for fire fighters.  
Standard EN 469 - Protective clothing for firefighters. Standard - EN 659: Protective gloves for firefighters.

**SECTION 6. Accidental release measures****6.1. Personal precautions, protective equipment and emergency procedures**

- : Evacuate area.  
Try to stop release.  
Wear self-contained breathing apparatus when entering area unless atmosphere is proved to be safe.  
Prevent from entering sewers, basements and workpits, or any place where its accumulation can be dangerous.  
Ensure adequate air ventilation.

**6.2. Environmental precautions**

- : Try to stop release.

**6.3. Methods and material for containment and cleaning up**

- : Ventilate area.

**6.4. Reference to other sections**

- : See also sections 8 and 13.

**Argon****2010483****SECTION 7. Handling and storage****7.1. Precautions for safe handling****Safe use of the product**

: Use only properly specified equipment which is suitable for this product, its supply pressure and temperature. Contact your gas supplier if in doubt.  
Only experienced and properly instructed persons should handle gases under pressure. The substance must be handled in accordance with good industrial hygiene and safety procedures.  
Do not smoke while handling product.  
Ensure the complete gas system was (or is regularly) checked for leaks before use.  
Consider pressure relief device(s) in gas installations.

**Safe handling of the gas receptacle**

: Refer to supplier's container handling instructions.  
Suck back of water into the container must be prevented.  
Do not allow backfeed into the container.  
Protect cylinders from physical damage; do not drag, roll, slide or drop.  
When moving cylinders, even for short distances, use a cart (trolley, hand truck, etc.) designed to transport cylinders.  
Leave valve protection caps in place until the container has been secured against either a wall or bench or placed in a container stand and is ready for use.  
If user experiences any difficulty operating cylinder valve discontinue use and contact supplier.  
Never attempt to repair or modify container valves or safety relief devices.  
Damaged valves should be reported immediately to the supplier.  
Keep container valve outlets clean and free from contaminants particularly oil and water.  
Replace valve outlet caps or plugs and container caps where supplied as soon as container is disconnected from equipment.  
Close container valve after each use and when empty, even if still connected to equipment.  
Never attempt to transfer gases from one cylinder/container to another.  
Never use direct flame or electrical heating devices to raise the pressure of a container.  
Do not remove or deface labels provided by the supplier for the identification of the cylinder contents.  
Containers should be stored in the vertical position and properly secured to prevent toppling.

**7.2. Conditions for safe storage, including any incompatibilities**

: Keep container below 50°C in a well ventilated place.  
Observe all regulations and local requirements regarding storage of containers.  
Containers should not be stored in conditions likely to encourage corrosion.  
Containers should be stored in the vertical position and properly secured to prevent toppling.  
Stored containers should be periodically checked for general condition and leakage.  
Container valve guards or caps should be in place.  
Store containers in location free from fire risk and away from sources of heat and ignition.  
Keep away from combustible materials.

**7.3. Specific end use(s)**

: None.

**SECTION 8. Exposure controls/personal protection****8.1. Control parameters****DNEL: Derived no effect level (Workers)**

: No data available.

**DMEL: Derived minimum effect level (Workers)**

: No data available.

**PNEC: Predicted no effect concentration**

**Argon****2010483****SECTION 8. Exposure controls/personal protection (continued)**

: No data available.

**8.2. Exposure controls**

- 8.2.1. Appropriate engineering controls** : Oxygen detectors should be used when asphyxiating gases may be released. Systems under pressure should be regularly checked for leakages. Provide adequate general and local exhaust ventilation. Consider work permit system e.g. for maintenance activities.
- 8.2.2. Individual protection measures, e.g. personal protective equipment** : A risk assessment should be conducted and documented in each work area to assess the risks related to the use of the product and to select the PPE that matches the relevant risk. The following recommendations should be considered: PPE compliant to the recommended EN/ISO standards should be selected.
- **Eye/face protection** : Wear safety glasses with side shields. Standard EN 166 - Personal eye-protection.
  - **Skin protection**
    - **Hand protection** : Wear working gloves when handling gas containers. Standard EN 388 - Protective gloves against mechanical risk.
    - **Other** : Wear safety shoes while handling containers. Standard EN ISO 20345 - Personal protective equipment - Safety footwear.
  - **Respiratory protection** : None necessary.
  - **Thermal hazards** : None necessary.
- 8.2.3. Environmental exposure controls** : Refer to local regulations for restriction of emissions to the atmosphere. See section 13 for specific methods for waste gas treatment.

**SECTION 9. Physical and chemical properties****9.1. Information on basic physical and chemical properties**

- Appearance**
- Physical state at 20°C / 101.3kPa** : Gas.
- Colour** : Colourless.
- Odour** : Odourless.
- Odour threshold** : Odour threshold is subjective and inadequate to warn for overexposure.
- pH value** : Not applicable.
- Molar mass [g/mol]** : 40
- Melting point [°C]** : -189
- Boiling point [°C]** : -186
- Critical temperature [°C]** : -122
- Flash point [°C]** : Not applicable for gases and gas-mixtures.
- Evaporation rate (ether=1)** : Not applicable for gases and gas-mixtures.
- Flammability range [vol% in air]** : Non flammable.
- Vapour pressure [20°C]** : Not applicable.
- Relative density, gas (air=1)** : 1.38
- Relative density, liquid (water=1)** : Not applicable.
- Solubility in water [mg/l]** : Solubility in water of component(s) of the mixture : 67
- Partition coefficient n-octanol/water [log Kow]** : Not applicable for inorganic gases.
- Viscosity at 20°C [mPa.s]** : Not applicable.
- Explosive Properties** : Not applicable.

**Argon****2010483****SECTION 9. Physical and chemical properties (continued)**

Oxidising Properties : None.

**9.2. Other information**

Other data : Gas/vapour heavier than air. May accumulate in confined spaces, particularly at or below ground level.

**SECTION 10. Stability and reactivity****10.1. Reactivity**

: No reactivity hazard other than the effects described in sub-sections below.

**10.2. Chemical stability**

: Stable under normal conditions.

**10.3. Possibility of hazardous reactions**

: None.

**10.4. Conditions to avoid**

: None under recommended storage and handling conditions (see section 7).

**10.5. Incompatible materials**: None.  
For additional information on compatibility refer to ISO 11114.**10.6. Hazardous decomposition products**

: Under normal conditions of storage and use, hazardous decomposition products should not be produced.

**SECTION 11. Toxicological information****11.1. Information on toxicological effects**

Toxicity information : No known toxicological effects from this product.

Acute toxicity : No known toxicological effects from this product.

Rat inhalation LC50 [ppm/4h] : No data available.

Skin corrosion/irritation : No known effects from this product.

Serious eye damage/irritation : No known effects from this product.

Respiratory or skin sensitisation : No known effects from this product.

STOT-single exposure : No known effects from this product.

STOT-repeated exposure : No known effects from this product.

Aspiration hazard : Not applicable for gases and gas-mixtures.



**Argon****2010483****SECTION 12. Ecological information****12.1. Toxicity**

- : No ecological damage caused by this product.
- EC50 48h - Daphnia magna [mg/l] : No data available.
- EC50 72h Algae [mg/l] : No data available.
- LC50-96 h - fish [mg/l] : No data available.

**12.2. Persistence and degradability**

: No ecological damage caused by this product.

**12.3. Bioaccumulative potential**

: No ecological damage caused by this product.

**12.4. Mobility in soil**

: No ecological damage caused by this product.

**12.5. Results of PBT and vPvB assessment**

: Not classified as PBT or vPvB.

**12.6. Other adverse effects**

- Ecological effects information : None.
- Effect on the global warming : None.

**SECTION 13. Disposal considerations****13.1. Waste treatment methods**

: May be vented to atmosphere in a well ventilated place.  
Do not discharge into any place where its accumulation could be dangerous.  
Refer to the EIGA code of practice Doc.30 "Disposal of Gases", downloadable at <http://www.eiga.org> for more guidance on suitable disposal methods.  
Contact supplier if guidance is required.

List of hazardous wastes : 16 05 05: Gases in pressure containers other than those mentioned in 16 05 04.

**13.2. Additional information**

: None.

**SECTION 14. Transport information**

- UN number : 1006
- Labelling ADR, IMDG, IATA



: 2.2 : Non-flammable, non-toxic gases

**Land transport (ADR/RID)**

- H.I. nr : 20
- UN proper shipping name : ARGON, COMPRESSED
- Transport hazard class(es) : 2
- Classification code : 1 A

**Argon****2010483****SECTION 14. Transport information (continued)**

Packing group : P200  
Packing Instruction(s) : P200  
Tunnel Restriction : E : Passage forbidden through tunnels of category E.  
Environmental hazards : None.

**Sea transport (IMDG)**

Proper shipping name : ARGON, COMPRESSED  
Class : 2.2  
Emergency Schedule (EmS) - Fire : F-C  
Emergency Schedule (EmS) - Spillage : S-V  
Packing instruction : P200  
IMDG-Marine pollutant : -

**Air transport (ICAO-TI / IATA-DGR)**

Proper shipping name (IATA) : ARGON, COMPRESSED  
Class : 2.2  
Passenger and Cargo Aircraft : Allowed.  
Packing instruction - Passenger and Cargo Aircraft : 200  
Cargo Aircraft only : Allowed.  
Packing instruction - Cargo Aircraft only : 200

**Special precautions for user**

: Avoid transport on vehicles where the load space is not separated from the driver's compartment.  
Ensure vehicle driver is aware of the potential hazards of the load and knows what to do in the event of an accident or an emergency.  
Before transporting product containers:  
- Ensure there is adequate ventilation.  
- Ensure that containers are firmly secured.  
- Ensure cylinder valve is closed and not leaking.  
- Ensure valve outlet cap nut or plug (where provided) is correctly fitted.  
- Ensure valve protection device (where provided) is correctly fitted.

14.7. Transport in bulk according to Annex II of MARPOL 73/78 and the IBC Code : Not applicable.

**SECTION 15. Regulatory information****15.1. Safety, health and environmental regulations/legislation specific for the substance or mixture****EU legislation**

Restrictions on use : None.  
Seveso directive 96/82/EC : Not covered.

**National legislation**

National legislation : Ensure all national/local regulations are observed.

**15.2. Chemical safety assessment**

: A CSA does not need to be carried out for this product.

**Argon****2010483****SECTION 15. Regulatory information (continued)****SECTION 16. Other information**

- Indication of changes** : Revised safety data sheet in accordance with commission regulation (EU) No 453/2010.
- Training advice** : The hazard of asphyxiation is often overlooked and must be stressed during operator training.
- List of full text of H-statements in section 3.** : H280 - Contains gas under pressure; may explode if heated.
- Further information** : Classification in accordance with calculation methods of regulation (EC) 1272/2008 CLP / (EC) 1999/45 DPD.  
This Safety Data Sheet has been established in accordance with the applicable European Union legislation.
- DISCLAIMER OF LIABILITY** : Before using this product in any new process or experiment, a thorough material compatibility and safety study should be carried out.  
Details given in this document are believed to be correct at the time of going to press. Whilst proper care has been taken in the preparation of this document, no liability for injury or damage resulting from its use can be accepted.

**End of document**

**SECTION 1: Identification****1.1. Identification**

Product form : Substance  
 Substance name : Water  
 CAS-No. : 7732-18-5  
 Product code : LC26750  
 Formula : H<sub>2</sub>O

**1.2. Recommended use and restrictions on use**

Use of the substance/mixture : For laboratory and manufacturing use only.  
 Recommended use : Laboratory chemicals  
 Restrictions on use : Not for food, drug or household use

**1.3. Supplier**

LabChem Inc  
 Jackson's Pointe Commerce Park Building 1000, 1010 Jackson's Pointe Court  
 Zelenople, PA 16063 - USA  
 T 412-826-5230 - F 724-473-0647  
[info@labchem.com](mailto:info@labchem.com) - [www.labchem.com](http://www.labchem.com)

**1.4. Emergency telephone number**

Emergency number : CHEMTREC: 1-800-424-9300 or +1-703-741-5970

**SECTION 2: Hazard(s) identification****2.1. Classification of the substance or mixture****GHS-US classification**

Not classified

**2.2. GHS Label elements, including precautionary statements**

Not classified as a hazardous chemical.

Other hazards not contributing to the classification : None.

**2.4. Unknown acute toxicity (GHS US)**

Not applicable

**SECTION 3: Composition/Information on ingredients****3.1. Substances**

Substance type : Mono-constituent

Name	Product identifier	%	GHS-US classification
Water (Main constituent)	(CAS-No.) 7732-18-5	100	Not classified

Full text of hazard classes and H-statements : see section 16

**3.2. Mixtures**

Not applicable

**SECTION 4: First-aid measures****4.1. Description of first aid measures**

First-aid measures general : If you feel unwell, seek medical advice (show the label where possible).  
 First-aid measures after inhalation : Allow victim to breathe fresh air. Allow the victim to rest. Adverse effects not expected from this product.  
 First-aid measures after skin contact : Adverse effects not expected from this product. Take off contaminated clothing.  
 First-aid measures after eye contact : Adverse effects not expected from this product.  
 First-aid measures after ingestion : Do NOT induce vomiting. Adverse effects not expected from this product.

**4.2. Most important symptoms and effects (acute and delayed)**

Symptoms/effects : Not expected to present a significant hazard under anticipated conditions of normal use.

# Water

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### 4.3. Immediate medical attention and special treatment, if necessary

Treat symptomatically.

## SECTION 5: Fire-fighting measures

### 5.1. Suitable (and unsuitable) extinguishing media

Suitable extinguishing media : Foam. Dry powder. Carbon dioxide. Water spray. Sand.

### 5.2. Specific hazards arising from the chemical

No additional information available

### 5.3. Special protective equipment and precautions for fire-fighters

Firefighting instructions : Use water spray or fog for cooling exposed containers. Exercise caution when fighting any chemical fire.

Protection during firefighting : Do not enter fire area without proper protective equipment, including respiratory protection.

## SECTION 6: Accidental release measures

### 6.1. Personal precautions, protective equipment and emergency procedures

#### 6.1.1. For non-emergency personnel

Emergency procedures : Evacuate unnecessary personnel.

#### 6.1.2. For emergency responders

Protective equipment : Equip cleanup crew with proper protection.

Emergency procedures : Ventilate area.

### 6.2. Environmental precautions

Prevent entry to sewers and public waters. Notify authorities if liquid enters sewers or public waters.

### 6.3. Methods and material for containment and cleaning up

Methods for cleaning up : Soak up spills with inert solids, such as clay or diatomaceous earth as soon as possible.

### 6.4. Reference to other sections

See Heading 8. Exposure controls and personal protection.

## SECTION 7: Handling and storage

### 7.1. Precautions for safe handling

Precautions for safe handling : Wash hands and other exposed areas with mild soap and water before eating, drinking or smoking and when leaving work.

### 7.2. Conditions for safe storage, including any incompatibilities

Storage conditions : Keep container closed when not in use.

Incompatible products : Metallic sodium.

Incompatible materials : Sources of ignition. Direct sunlight.

## SECTION 8: Exposure controls/personal protection

### 8.1. Control parameters

No additional information available

### 8.2. Appropriate engineering controls

Appropriate engineering controls : Provide adequate general and local exhaust ventilation.

### 8.3. Individual protection measures/Personal protective equipment

#### Personal protective equipment:

Gloves. Safety glasses.



#### Hand protection:

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Wear protective gloves.

### Eye protection:

Chemical goggles or safety glasses

### Respiratory protection:

None necessary.

### Other information:

Do not eat, drink or smoke during use.

## SECTION 9: Physical and chemical properties

### 9.1. Information on basic physical and chemical properties

Physical state	: Liquid
Color	: Colorless
Odor	: None.
Odor threshold	: No data available
pH	: 7
Melting point	: 0 °C
Freezing point	: No data available
Boiling point	: 100 °C
Critical temperature	: 374.1 °C
Critical pressure	: 218.3 atm
Flash point	: No data available
Relative evaporation rate (butyl acetate=1)	: No data available
Flammability (solid, gas)	: Non flammable.
Vapor pressure	: 17.535 mm Hg
Vapor pressure at 50 °C	: 92.51 mm Hg
Relative vapor density at 20 °C	: No data available
Relative density	: 1
Specific gravity / density	: 0.99823 g/ml
Molecular mass	: 18 g/mol
Solubility	: Soluble in acetic acid. Soluble in acetone. Soluble in ammonia. Soluble in ammonium chloride. Soluble in ethanol. Soluble in glycerol. Soluble in hydrochloric acid. Soluble in methanol. Soluble in nitric acid. Soluble in sulfuric acid. Soluble in sodium hydroxide solution. Soluble in propylene glycol.
Log Pow	: No data available
Auto-ignition temperature	: No data available
Decomposition temperature	: No data available
Viscosity, kinematic	: 1.004 cSt
Viscosity, dynamic	: 1.002 cP
Explosion limits	: No data available
Explosive properties	: Not applicable.
Oxidizing properties	: None.

### 9.2. Other information

VOC content : 0 %

## SECTION 10: Stability and reactivity

### 10.1. Reactivity

No additional information available

### 10.2. Chemical stability

Stable under normal conditions.

### 10.3. Possibility of hazardous reactions

Not established.

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### 10.4. Conditions to avoid

Extremely high or low temperatures.

### 10.5. Incompatible materials

Metallic sodium.

### 10.6. Hazardous decomposition products

Hydrogen. oxygen.

## SECTION 11: Toxicological information

### 11.1. Information on toxicological effects

Likely routes of exposure : Skin and eye contact

Acute toxicity : Not classified

Water (7732-18-5)	
LD50 oral rat	≥ 90000 mg/kg
ATE US (oral)	90000 mg/kg body weight

Skin corrosion/irritation : Not classified  
pH: 7

Serious eye damage/irritation : Not classified  
pH: 7

Respiratory or skin sensitization : Not classified

Germ cell mutagenicity : Not classified

Carcinogenicity : Not classified

(Based on available data, the classification criteria are not met)

Reproductive toxicity : Not classified

Specific target organ toxicity – single exposure : Not classified

Specific target organ toxicity – repeated exposure : Not classified

Aspiration hazard : Not classified

Potential Adverse human health effects and symptoms : Based on available data, the classification criteria are not met.

## SECTION 12: Ecological information

### 12.1. Toxicity

No additional information available

### 12.2. Persistence and degradability

Water (7732-18-5)	
Persistence and degradability	Not established.

### 12.3. Bioaccumulative potential

Water (7732-18-5)	
Bioaccumulative potential	Not established.

### 12.4. Mobility in soil

No additional information available

### 12.5. Other adverse effects

Other information : No other effects known.

## SECTION 13: Disposal considerations

### 13.1. Disposal methods

Waste disposal recommendations : Dispose in a safe manner in accordance with local/national regulations.

# Water

## Safety Data Sheet

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### SECTION 14: Transport information

#### Department of Transportation (DOT)

In accordance with DOT  
Not regulated

### SECTION 15: Regulatory information

#### 15.1. US Federal regulations

##### Water (7732-18-5)

Listed on the United States TSCA (Toxic Substances Control Act) inventory

All components of this product are listed, or excluded from listing, on the United States Environmental Protection Agency Toxic Substances Control Act (TSCA) inventory

#### 15.2. International regulations

##### CANADA

No additional information available

##### EU-Regulations

No additional information available

##### National regulations

No additional information available

#### 15.3. US State regulations

California Proposition 65 - This product does not contain any substances known to the state of California to cause cancer, developmental and/or reproductive harm

### SECTION 16: Other information

Revision date : 06/12/2018

Other information : None.

NFPA health hazard : 0 - Materials that, under emergency conditions, would offer no hazard beyond that of ordinary combustible materials.

NFPA fire hazard : 0 - Materials that will not burn under typical fire conditions, including intrinsically noncombustible materials such as concrete, stone, and sand.

NFPA reactivity : 0 - Material that in themselves are normally stable, even under fire conditions.

#### Hazard Rating

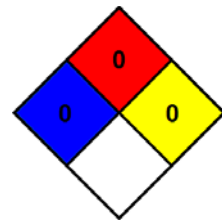
Health : 0 Minimal Hazard - No significant risk to health

Flammability : 0 Minimal Hazard - Materials that will not burn

Physical : 0 Minimal Hazard - Materials that are normally stable, even under fire conditions, and will NOT react with water, polymerize, decompose, condense, or self-react. Non-Explosives.

Personal protection : A  
A - Safety glasses

SDS US LabChem



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# C.1.7: Ammonia

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## SECTION 1: Identification of the substance/mixture and of the company/undertaking

### 1.1. Product identifier

Trade name : Ammonia, Anhydrous ammonia, Ammonia N38, Ammonia HG, Ammonia LGC  
SDS no : NOAL\_0002  
Chemical description : Anhydrous ammonia  
CAS-No. : 7664-41-7  
EC-No. : 231-635-3  
EC Index-No. : 007-001-00-5  
Registration-No. : 01-2119488876-14  
Chemical formula : NH<sub>3</sub>

### 1.2. Relevant identified uses of the substance or mixture and uses advised against

Relevant identified uses : Industrial and professional. Perform risk assessment prior to use.  
See the list of identified uses and exposure scenarios in the annex of the safety data sheet.  
Contact supplier for more information on uses.  
Uses advised against : Consumer use.

### 1.3. Details of the supplier of the safety data sheet

#### Company identification

AIR LIQUIDE GAS AB  
Lundavägen 151  
21209 Malmö - SWEDEN  
T +46 40 38 10 00  
[eunordic-sds@airliquide.com](mailto:eunordic-sds@airliquide.com)

E-Mail address (competent person) : eunordic-sds@airliquide.com

### 1.4. Emergency telephone number


Emergency telephone number : 112  
Availability  
( 24 / 7 )

## SECTION 2: Hazards identification

### 2.1. Classification of the substance or mixture

#### Classification according to Regulation (EC) No. 1272/2008 [CLP]

Physical hazards	Flammable gases, Category 2	H221
	Gases under pressure : Liquefied gas	H280
Health hazards	Acute toxicity (inhalation:gas) Category 3	H331
	Skin corrosion/irritation, Category 1B	H314
	Serious eye damage/eye irritation, Category 1	H318
Environmental hazards	Hazardous to the aquatic environment — Acute Hazard, Category 1	H400

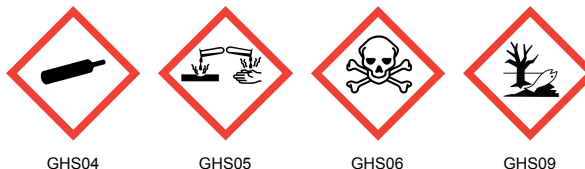
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Hazardous to the aquatic environment — Chronic Hazard, Category 2 H411

## 2.2. Label elements

### Labelling according to Regulation (EC) No. 1272/2008 [CLP]

Hazard pictograms (CLP) :



Signal word (CLP) :

Danger

Hazard statements (CLP) :

H221 - Flammable gas..  
H280 - Contains gas under pressure; may explode if heated..  
H314 - Causes severe skin burns and eye damage..  
H331 - Toxic if inhaled..  
H410 - Very toxic to aquatic life with long lasting effects..  
EUH071 - Corrosive to the respiratory tract..

Precautionary statements (CLP)

- Prevention : P210 - Keep away from heat, hot surfaces, sparks, open flames and other ignition sources. No smoking..  
P260 - Do not breathe gas, vapours..  
P273 - Avoid release to the environment..  
P280 - Wear protective gloves, protective clothing, eye protection, face protection..
- Response : P303+P361+P353+P315 - IF ON SKIN : (or hair) Remove/Take off immediately all contaminated clothing. Rinse skin with water/shower. Get immediate medical advice / attention..  
P304+P340+P315 - IF INHALED : Remove person to fresh air and keep comfortable for breathing. Get immediate medical advice / attention..  
P305+P351+P338+P315 - IF IN EYES : Rinse cautiously with water for several minutes. Remove contact lenses, if present and easy to do. Continue rinsing. Get immediate medical advice / attention..  
P377 - Leaking gas fire: Do not extinguish, unless leak can be stopped safely..  
P381 - In case of leakage, eliminate all ignition sources..
- Storage : P403 - Store in a well-ventilated place..  
P405 - Store locked up..


## 2.3. Other hazards

: None.

## SECTION 3: Composition/information on ingredients

### 3.1. Substances

Name	Product identifier	Composition [V-%]:	Classification according to Regulation (EC) No. 1272/2008 [CLP]
Anhydrous ammonia	(CAS-No.) 7664-41-7 (EC-No.) 231-635-3 (EC Index-No.) 007-001-00-5 (Registration-No.) 01-2119488876-14	100	Flam. Gas 2, H221 Press. Gas (Liq.), H280 Acute Tox. 3 (Inhalation:gas), H331 Skin Corr. 1B, H314 Eye Dam. 1, H318 Aquatic Acute 1, H400 Aquatic Chronic 2, H411

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Contains no other components or impurities which will influence the classification of the product.

### **3.2. Mixtures**

: Not established.

## **SECTION 4: First aid measures**

### **4.1. Description of first aid measures**

- Inhalation : Remove victim to uncontaminated area wearing self contained breathing apparatus. Keep victim warm and rested. Call a doctor. Apply artificial respiration if breathing stopped.
- Skin contact : Remove contaminated clothing. Drench affected area with water for at least 15 minutes. In case of frostbite spray with water for at least 15 minutes. Apply a sterile dressing. Obtain medical assistance.
- Eye contact : Immediately flush eyes thoroughly with water for at least 15 minutes.
- Ingestion : Ingestion is not considered a potential route of exposure.

### **4.2. Most important symptoms and effects, both acute and delayed**

- : May cause severe chemical burns to skin and cornea. Suitable first-aid treatment should be immediately available. Seek medical advice before using product.
- Prolonged exposure to small concentrations may result in pulmonary oedema.
- Material is destructive to tissue of the mucuous membranes and upper respiratory tract. Cough, shortness of breath, headache, nausea.
- Refer to section 11.

### **4.3. Indication of any immediate medical attention and special treatment needed**

- : Obtain medical assistance.
- Treat with corticosteroid spray as soon as possible after inhalation.

## **SECTION 5: Firefighting measures**

### **5.1. Extinguishing media**


- Suitable extinguishing media : Water spray or fog.  
Foam.
- Unsuitable extinguishing media : Carbon dioxide.  
Do not use water jet to extinguish.

### **5.2. Special hazards arising from the substance or mixture**

- Specific hazards : Exposure to fire may cause containers to rupture/explode.
- Hazardous combustion products : Nitric oxide/nitrogen dioxide.

### **5.3. Advice for firefighters**

- Specific methods : Use fire control measures appropriate for the surrounding fire. Exposure to fire and heat radiation may cause gas receptacles to rupture. Cool endangered receptacles with water spray jet from a protected position. Prevent water used in emergency cases from entering sewers and drainage systems.
- If possible, stop flow of product.
- Use water spray or fog to knock down fire fumes if possible.

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Do not extinguish a leaking gas flame unless absolutely necessary. Spontaneous/explosive re-ignition may occur. Extinguish any other fire.

Move containers away from the fire area if this can be done without risk.

Special protective equipment for fire fighters

: Wear gas tight chemically protective clothing in combination with self contained breathing apparatus.

Standard EN 943-2: Protective clothing against liquid and gaseous chemicals, aerosols and solid particles. Gas-tight chemical protective suits for emergency teams.

Standard EN 137 - Self-contained open-circuit compressed air breathing apparatus with full face mask.

## SECTION 6: Accidental release measures

### 6.1. Personal precautions, protective equipment and emergency procedures

: Try to stop release.

Evacuate area.

Monitor concentration of released product.

Consider the risk of potentially explosive atmospheres.

Wear self-contained breathing apparatus when entering area unless atmosphere is proved to be safe.

Eliminate ignition sources.

Use chemically protective clothing.

Ensure adequate air ventilation.

Act in accordance with local emergency plan.

Stay upwind.

### 6.2. Environmental precautions

: Reduce vapour with fog or fine water spray.

Try to stop release.

### 6.3. Methods and material for containment and cleaning up

: Hose down area with water.

Ventilate area.

Keep area evacuated and free from ignition sources until any spilled liquid has evaporated (ground free from frost).

Wash contaminated equipment or sites of leaks with copious quantities of water.

### 6.4. Reference to other sections

: See also sections 8 and 13.

## SECTION 7: Handling and storage

### 7.1. Precautions for safe handling

Safe use of the product


: The product must be handled in accordance with good industrial hygiene and safety procedures.

Only experienced and properly instructed persons should handle gases under pressure.

Consider pressure relief device(s) in gas installations.

Ensure the complete gas system was (or is regularly) checked for leaks before use.

Do not smoke while handling product.

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Avoid exposure, obtain special instructions before use.

Use only properly specified equipment which is suitable for this product, its supply pressure and temperature. Contact your gas supplier if in doubt.

Installation of a cross purge assembly between the cylinder and the regulator is recommended.

Purge system with dry inert gas (e.g. helium or nitrogen) before gas is introduced and when system is placed out of service.

Avoid suck back of water, acid and alkalis.

Assess the risk of potentially explosive atmospheres and the need for explosion-proof equipment.

Purge air from system before introducing gas.

Take precautionary measures against static discharge.

Keep away from ignition sources (including static discharges).

Consider the use of only non-sparking tools.

Do not breathe gas.

Avoid release of product into atmosphere.

Ensure equipment is adequately earthed.

Safe handling of the gas receptacle

: Refer to supplier's container handling instructions.

Do not allow backfeed into the container.

Protect cylinders from physical damage; do not drag, roll, slide or drop.

When moving cylinders, even for short distances, use a cart (trolley, hand truck, etc.) designed to transport cylinders.

Leave valve protection caps in place until the container has been secured against either a wall or bench or placed in a container stand and is ready for use.

If user experiences any difficulty operating cylinder valve discontinue use and contact supplier.

Never attempt to repair or modify container valves or safety relief devices.

Damaged valves should be reported immediately to the supplier.

Keep container valve outlets clean and free from contaminants particularly oil and water.

Replace valve outlet caps or plugs and container caps where supplied as soon as container is disconnected from equipment.

Close container valve after each use and when empty, even if still connected to equipment.

Never attempt to transfer gases from one cylinder/container to another.

Never use direct flame or electrical heating devices to raise the pressure of a container.

Do not remove or deface labels provided by the supplier for the identification of the cylinder contents.

Suck back of water into the container must be prevented.

Open valve slowly to avoid pressure shock.

### **7.2. Conditions for safe storage, including any incompatibilities**

: Observe all regulations and local requirements regarding storage of containers.

Containers should not be stored in conditions likely to encourage corrosion.

Container valve guards or caps should be in place.

Containers should be stored in the vertical position and properly secured to prevent them from falling over.

Stored containers should be periodically checked for general condition and leakage.

Keep container below 50°C in a well ventilated place.


Store containers in location free from fire risk and away from sources of heat and ignition.

Keep away from combustible materials.

Segregate from oxidant gases and other oxidants in store.

All electrical equipment in the storage areas should be compatible with the risk of a potentially explosive atmosphere.

### **7.3. Specific end use(s)**

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: None.

## SECTION 8: Exposure controls/personal protection

### 8.1. Control parameters

Anhydrous ammonia (7664-41-7)		
OEL : Occupational Exposure Limits		
EU	TWA IOELV (EU) 8 h [mg/m <sup>3</sup> ]	14 mg/m <sup>3</sup>
	TWA IOELV (EU) 8 h [ppm]	20 ppm
	STEL IOELV (EU) 15 min [mg/m <sup>3</sup> ]	36 mg/m <sup>3</sup>
	STEL IOELV (EU) 15 min [ppm]	50 ppm
Sweden	TWA (SV) OEL 8h [mg/m <sup>3</sup> ]	14 mg/m <sup>3</sup>
	TWA (SV) OEL 8h [ppm]	20 ppm
	STEL (SV) OEL 15min [mg/m <sup>3</sup> ]	36 mg/m <sup>3</sup>
	STEL (SV) OEL 15min [ppm]	50 ppm
	Anmärkning (SE)	4 (Korttidsgränsvärdet avser en 5-minutersperiod. Detta gäller för ammoniak, diisocyanater, 2,6-diisopropylfenylisocyanat, fenylisocyanat, isocyanosyra och metylisocyanat)

Anhydrous ammonia (7664-41-7)	
DNEL: Derived no effect level (Workers)	
Acute - local effects, inhalation	36 mg/m <sup>3</sup>
Acute - systemic effects, inhalation	47.6 mg/m <sup>3</sup>
Long-term - local effects, inhalation	14 mg/m <sup>3</sup>
Long-term - systemic effects, inhalation	47.6 mg/m <sup>3</sup>
Acute - systemic effects, dermal	6.8 mg/kg bw/day
Long-term - systemic effects, dermal	6.8 mg/kg bw/day

Anhydrous ammonia (7664-41-7)	
PNEC: Predicted no effect concentration	
Aqua (freshwater)	0.0011 mg/l
Aqua (marine water)	0.0011 mg/l

### 8.2. Exposure controls

#### 8.2.1. Appropriate engineering controls

- : Provide adequate general and local exhaust ventilation.
- Product to be handled in a closed system.
- Systems under pressure should be regularly checked for leakages.
- Ensure exposure is below occupational exposure limits (where available).
- Gas detectors should be used when toxic gases may be released.
- Consider the use of a work permit system e.g. for maintenance activities.

#### 8.2.2. Individual protection measures, e.g. personal protective equipment

- : A risk assessment should be conducted and documented in each work area to assess the risks related to the use of the product and to select the PPE that matches the relevant risk. The following recommendations should be considered:  
PPE compliant to the recommended EN/ISO standards should be selected.


#### • Eye/face protection

- : Wear goggles and a face shield when transfilling or breaking transfer connections.  
Standard EN 166 - Personal eye-protection - specifications.  
Provide readily accessible eye wash stations and safety showers.

#### • Skin protection

##### - Hand protection

- : Wear working gloves when handling gas containers.

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Standard EN 388 - Protective gloves against mechanical risk.

Wear cold insulating gloves when transfilling or breaking transfer connections.

Standard EN 511 - Cold insulating gloves.

Wear chemically resistant protective gloves.

Standard EN 374 - Protective gloves against chemicals.

Permeation time: minimum >30min short term exposure: material / thickness Chloroprene rubber (CR) / 0.5 [mm] .

Permeation time: minimum >480min long term exposure : material / thickness Butyl rubber (IIR) / 0.7 [mm].

Consult glove manufacturer's product information on material suitability and material thickness.

The breakthrough time of the selected gloves must be greater than the intended use period.

- Other

: Keep suitable chemically resistant protective clothing readily available for emergency use.  
Standard EN943-1 - Full protective suits against liquid, solid and gaseous chemicals.  
Wear safety shoes while handling containers.  
Standard EN ISO 20345 - Personal protective equipment - Safety footwear.

• Respiratory protection

: Gas filters may be used if all surrounding conditions e.g. type and concentration of the contaminant(s) and duration of use are known.  
Use gas filters with full face mask, where exposure limits may be exceeded for a short-term period, e.g. connecting or disconnecting containers.  
Recommended: Filter K (green).  
Gas filters do not protect against oxygen deficiency.  
Standard EN 14387 - Gas filter(s), combined filter(s) and full face mask - EN 136.  
Keep self contained breathing apparatus readily available for emergency use.  
Self contained breathing apparatus is recommended, where unknown exposure may be expected, e.g. during maintenance activities on installation systems.  
Standard EN 137 - Self-contained open-circuit compressed air breathing apparatus with full face mask.

• Thermal hazards

: None in addition to the above sections.

### 8.2.3. Environmental exposure controls

: Refer to local regulations for restriction of emissions to the atmosphere. See section 13 for specific methods for waste gas treatment.

## SECTION 9: Physical and chemical properties

### 9.1. Information on basic physical and chemical properties

Appearance

- Physical state at 20°C / 101.3kPa : Gas.
- Colour : Colourless.

Odour : Ammoniacal.

Odour threshold : Odour threshold is subjective and inadequate to warn of overexposure.

pH value : If dissolved in water pH-value will be affected.

Molar mass : 17 g/mol

Melting point : -77.7 °C

Boiling point : -33 °C

Flash point : Not applicable for gases and gas mixtures.

Critical temperature [°C] : 132 °C

Evaporation rate (ether=1) : Not applicable for gases and gas mixtures.

Flammability range : 15.4 - 33.6 vol %

Vapour pressure [20°C] : 8.6 bar(a)

Vapour pressure [50°C] : 20 bar(a)

Relative density, gas (air=1) : 0.6

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Relative density, liquid (water=1)	: 0.7
Solubility in water	: 517 g/l
Partition coefficient n-octanol/water [log Kow]	: Not applicable for inorganic gases.
Auto-ignition temperature	: 630 °C
Decomposition point [°C]	: Not applicable.
Viscosity [20°C]	: No reliable data available.
Explosive Properties	: Not applicable.
Oxidising Properties	: Not applicable.

**9.2. Other information**

Other data : No additional information available

**SECTION 10: Stability and reactivity****10.1. Reactivity**

: No reactivity hazard other than the effects described in sub-sections below.

**10.2. Chemical stability**

: Stable under normal conditions.

**10.3. Possibility of hazardous reactions**: Can form explosive mixture with air.  
May react violently with oxidants.**10.4. Conditions to avoid**: Keep away from heat/sparks/open flames/hot surfaces. – No smoking.  
Avoid moisture in installation systems.**10.5. Incompatible materials**: Air, Oxidisers.  
Reacts with water to form corrosive alkalis.  
May react violently with acids.  
For additional information on compatibility refer to ISO 11114.**10.6. Hazardous decomposition products**


: Under normal conditions of storage and use, hazardous decomposition products should not be produced.

**SECTION 11: Toxicological information****11.1. Information on toxicological effects****Acute toxicity**: Toxic if inhaled.  
Inhalation of large amounts leads to bronchospasm, laryngeal oedema and pseudomembrane formation.

LC50 inhalation rat (ppm) 2000 ppm/4h

<b>Skin corrosion/irritation</b>	: Causes severe skin burns and eye damage.
<b>Serious eye damage/irritation</b>	: Causes serious eye damage.
<b>Respiratory or skin sensitisation</b>	: No known effects from this product.
<b>Germ cell mutagenicity</b>	: No known effects from this product.
<b>Carcinogenicity</b>	: No known effects from this product.
<b>Reproductive toxicity</b>	: No known effects from this product. No known effects from this product.
<b>STOT-single exposure</b>	: Severe corrosion to the respiratory tract at high concentrations.



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May cause inflammation of the respiratory system.  
**Target organ(s)** : Respiratory tract.  
**STOT-repeated exposure** : No known effects from this product.  
**Aspiration hazard** : Not applicable for gases and gas mixtures.

## SECTION 12: Ecological information

### 12.1. Toxicity

**Assessment** : Very toxic to aquatic life.  
 Toxic to aquatic life with long lasting effects.  
 EC50 48h - Daphnia magna [mg/l] : 101 mg/l  
 EC50 72h - Algae [mg/l] : No data available.  
 LC50 96 h - Fish [mg/l] : 0.89 mg/l

### 12.2. Persistence and degradability

**Assessment** : The substance is biodegradable. Unlikely to persist.

### 12.3. Bioaccumulative potential

**Assessment** : No data available.

### 12.4. Mobility in soil

**Assessment** : Because of its high volatility, the product is unlikely to cause ground or water pollution.  
 Partition into soil is unlikely.

### 12.5. Results of PBT and vPvB assessment

**Assessment** : Not classified as PBT or vPvB.


### 12.6. Other adverse effects

Other adverse effects : May cause pH changes in aqueous ecological systems.  
 Effect on the ozone layer : None.  
 Effect on global warming : No known effects from this product.

## SECTION 13: Disposal considerations

### 13.1. Waste treatment methods

Contact supplier if guidance is required.  
 Must not be discharged to atmosphere.  
 Toxic and corrosive gases formed during combustion should be scrubbed before discharge to atmosphere.  
 Gas may be scrubbed in sulphuric acid solution.  
 Gas may be scrubbed in water.  
 Ensure that the emission levels from local regulations or operating permits are not exceeded.

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Refer to the EIGA code of practice Doc.30 "Disposal of Gases", downloadable at <http://www.eiga.org> for more guidance on suitable disposal methods.

Return unused product in original cylinder to supplier.

List of hazardous waste codes (from Commission Decision 2001/118/EC)

: 16 05 04 \*: Gases in pressure containers (including halons) containing dangerous substances.

**13.2. Additional information**

: External treatment and disposal of waste should comply with applicable local and/or national regulations.

**SECTION 14: Transport information**

**14.1. UN number**

UN-No. : 1005

**14.2. UN proper shipping name**

Transport by road/rail (ADR/RID) : AMMONIA, ANHYDROUS

Transport by air (ICAO-TI / IATA-DGR) : Ammonia, anhydrous

Transport by sea (IMDG) : AMMONIA, ANHYDROUS

**14.3. Transport hazard class(es)**

Labelling :



2.3 : Toxic gases.

8 : Corrosive substances.

Environmentally hazardous substances

**Transport by road/rail (ADR/RID)**

Class : 2.

Classification code : 2TC.

Hazard identification number : 268.

Tunnel Restriction : C/D - Tank carriage : Passage forbidden through tunnels of category C, D and E. Other carriage : Passage forbidden through tunnels of category D and E.

**Transport by sea (IMDG)**

Class / Div. (Sub. risk(s)) : 2.3 (8)

Emergency Schedule (EmS) - Fire : F-C.

Emergency Schedule (EmS) - Spillage : S-U.

**14.4. Packing group**

Transport by road/rail (ADR/RID) : Not established.


Transport by air (ICAO-TI / IATA-DGR) : Not established.

Transport by sea (IMDG) : Not established.

**14.5. Environmental hazards**

Transport by road/rail (ADR/RID) : Environmentally hazardous substance / mixture.

Transport by air (ICAO-TI / IATA-DGR) : Environmentally hazardous substance / mixture.

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Transport by sea (IMDG) : Marine pollutant

#### **14.6. Special precautions for user**

##### **Packing Instruction(s)**

Transport by road/rail (ADR/RID) : P200.

Transport by air (ICAO-TI / IATA-DGR)

Passenger and Cargo Aircraft : Forbidden.

Cargo Aircraft only : Forbidden.

Transport by sea (IMDG) : P200.

Special transport precautions : Avoid transport on vehicles where the load space is not separated from the driver's compartment.  
 Ensure vehicle driver is aware of the potential hazards of the load and knows what to do in the event of an accident or an emergency.  
 Before transporting product containers:  
 - Ensure there is adequate ventilation.  
 - Ensure that containers are firmly secured.  
 - Ensure cylinder valve is closed and not leaking.  
 - Ensure valve outlet cap nut or plug (where provided) is correctly fitted.  
 - Ensure valve protection device (where provided) is correctly fitted.

#### **14.7. Transport in bulk according to Annex II of Marpol and the IBC Code**

: Not applicable.

### **SECTION 15: Regulatory information**

#### **15.1. Safety, health and environmental regulations/legislation specific for the substance or mixture**

##### **EU-Regulations**

Restrictions on use : None.

Seveso Directive : 2012/18/EU (Seveso III) : Listed.

##### **National regulations**

National legislation : Ensure all national/local regulations are observed.


#### **15.2. Chemical safety assessment**

A CSA has been carried out.

### **SECTION 16: Other information**

Indication of changes : Revised safety data sheet in accordance with commission regulation (EU) No 453/2010.

Abbreviations and acronyms : ATE - Acute Toxicity Estimate  
 CLP - Classification Labelling Packaging Regulation; Regulation (EC) No 1272/2008  
 REACH - Registration, Evaluation, Authorisation and Restriction of Chemicals Regulation (EC) No 1907/2006

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EINECS - European Inventory of Existing Commercial Chemical Substances  
CAS# - Chemical Abstract Service number  
PPE - Personal Protection Equipment  
LC50 - Lethal Concentration to 50 % of a test population  
RMM - Risk Management Measures  
PBT - Persistent, Bioaccumulative and Toxic  
vPvB - Very Persistent and Very Bioaccumulative  
STOT- SE : Specific Target Organ Toxicity - Single Exposure  
CSA - Chemical Safety Assessment  
EN - European Standard  
UN - United Nations  
ADR - European Agreement concerning the International Carriage of Dangerous Goods by Road  
IATA - International Air Transport Association  
IMDG code - International Maritime Dangerous Goods  
RID - Regulations concerning the International Carriage of Dangerous Goods by Rail  
WGK - Water Hazard Class  
STOT - RE : Specific Target Organ Toxicity - Repeated Exposure


Training advice : Users of breathing apparatus must be trained.  
Ensure operators understand the flammability hazard.  
Ensure operators understand the toxicity hazard.

Full text of H- and EUH-statements

Acute Tox. 3 (Inhalation:gas)	Acute toxicity (inhalation:gas) Category 3
Aquatic Acute 1	Hazardous to the aquatic environment — Acute Hazard, Category 1
Aquatic Chronic 2	Hazardous to the aquatic environment — Chronic Hazard, Category 2
Eye Dam. 1	Serious eye damage/eye irritation, Category 1
Flam. Gas 2	Flammable gases, Category 2
Press. Gas (Liq.)	Gases under pressure : Liquefied gas
Skin Corr. 1B	Skin corrosion/irritation, Category 1B
H221	Flammable gas.
H280	Contains gas under pressure; may explode if heated.
H314	Causes severe skin burns and eye damage.
H318	Causes serious eye damage.
H331	Toxic if inhaled.
H400	Very toxic to aquatic life.
H411	Toxic to aquatic life with long lasting effects.
EUH071	Corrosive to the respiratory tract.

DISCLAIMER OF LIABILITY

: Before using this product in any new process or experiment, a thorough material compatibility and safety study should be carried out.  
Details given in this document are believed to be correct at the time of going to press.  
Whilst proper care has been taken in the preparation of this document, no liability for injury or damage resulting from its use can be accepted.

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## 1. Exposure scenario EIGA002-1

### Industrial uses, closed contained conditions

ES Ref.: EIGA002-1  
ES Type: Worker - EIGA  
Revision date: 25/04/2017

Use descriptors	SU3 PROC1, PROC2, PROC3, PROC4, PROC8b, PROC9 ERC1, ERC2, ERC4, ERC6a, ERC6b, ERC7
Processes, tasks, activities covered	Industrial uses, including product transfers and associated laboratory activities within different closed or contained systems
Assessment method	ECETOC TRA 2.0 EUSES

## 2. Operational conditions and risk management measures

### 1.2.1 Contributing scenario controlling environmental exposure (ERC1)

Manufacture of substances	
ERC1	Manufacture of substances
Assessment method	EUSES

#### Product characteristics

Physical form of product	See section 9 of the SDS, No additional information
Concentration of substance in product	<= 100 %

#### Operational conditions

Amounts used	Annual site tonnage:	950000 t/yr
	Regional use tonnage:	6500000 t/yr
Frequency and duration of use	Emission Days (days/year)	330
Environmental factors not influenced by risk management	Flow rate of receiving water at least:	18000 m³/d
	Dilution of STP emissions at least:	10
Other given operational conditions affecting environmental exposure	Closed systems are used in order to prevent unintended emissions	

#### Risk Management Measures

Technical onsite conditions and measures to reduce or limit discharges, air emissions and releases to soil	Use appropriate air emissions abatement systems (e.g. wet or dry scrubber or local STP) to ensure that the emission levels defined by local regulations are not exceeded	
	Soil emission controls are not applicable as there is no direct release to soil	
Organisation measures to prevent/limit release from site	Ensure operatives are trained to minimise releases	
Conditions and measures related to sewage treatment plant	Direct emissions to the municipal STP should not be made.	
Conditions and measures related to external treatment of waste for disposal	See section 13 of the SDS	

### 1.2.2 Contributing scenario controlling environmental exposure (ERC2)

Formulation of preparations	
ERC2	Formulation of preparations
Assessment method	EUSES

#### Product characteristics

Physical form of product	See section 9 of the SDS, No additional information
Concentration of substance in product	<= 100 %

#### Operational conditions

Amounts used	Annual site tonnage:	1000000 t/yr
	Regional use tonnage:	3800000 t/yr

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Frequency and duration of use	Emission Days (days/year)	330
Environmental factors not influenced by risk management	Flow rate of receiving water at least:	18000 m <sup>3</sup> /d
	Dilution of STP emissions at least:	10
Other given operational conditions affecting environmental exposure	Closed systems are used in order to prevent unintended emissions	

#### Risk Management Measures

Technical onsite conditions and measures to reduce or limit discharges, air emissions and releases to soil	Use appropriate air emissions abatement systems (e.g. wet or dry scrubber or local STP) to ensure that the emission levels defined by local regulations are not exceeded	
	Soil emission controls are not applicable as there is no direct release to soil	
Organisation measures to prevent/limit release from site	Ensure operatives are trained to minimise releases	
Conditions and measures related to sewage treatment plant	Direct emissions to the municipal STP should not be made.	
Conditions and measures related to external treatment of waste for disposal	See section 13 of the SDS	

#### 1.2.3 Contributing scenario controlling environmental exposure (ERC4)

Industrial use of processing aids in processes and products, not becoming part of articles	
ERC4	Industrial use of processing aids in processes and products, not becoming part of articles

#### Product characteristics

Physical form of product	See section 9 of the SDS, No additional information
Concentration of substance in product	<= 100 %

#### Operational conditions

Amounts used	Annual site tonnage:	25000 t/yr
	Regional use tonnage:	354000 t/yr
Frequency and duration of use	Emission Days (days/year)	330
Environmental factors not influenced by risk management	Flow rate of receiving water at least:	18000 m <sup>3</sup> /d
	Dilution of STP emissions at least:	10
Other given operational conditions affecting environmental exposure	Closed systems are used in order to prevent unintended emissions	

#### Risk Management Measures

Technical onsite conditions and measures to reduce or limit discharges, air emissions and releases to soil	Use appropriate air emissions abatement systems (e.g. wet or dry scrubber or local STP) to ensure that the emission levels defined by local regulations are not exceeded	
	Soil emission controls are not applicable as there is no direct release to soil	
Organisation measures to prevent/limit release from site	Ensure operatives are trained to minimise releases	
Conditions and measures related to sewage treatment plant	Direct emissions to the municipal STP should not be made.	
Conditions and measures related to external treatment of waste for disposal	See section 13 of the SDS	

#### 1.2.4 Contributing scenario controlling environmental exposure (ERC6a)

Industrial use resulting in manufacture of another substance (use of intermediates)	
ERC6a	Industrial use resulting in manufacture of another substance (use of intermediates)
Assessment method	EUSES

#### Product characteristics

Physical form of product	See section 9 of the SDS, No additional information
Concentration of substance in product	<= 100 %

#### Operational conditions

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Amounts used	Annual site tonnage:	800000 t/yr
	Regional use tonnage:	3800000 t/yr
Frequency and duration of use	Emission Days (days/year)	330
Environmental factors not influenced by risk management	Flow rate of receiving water at least:	18000 m <sup>3</sup> /d
	Dilution of STP emissions at least:	10
Other given operational conditions affecting environmental exposure	Closed systems are used in order to prevent unintended emissions	

#### Risk Management Measures

Technical onsite conditions and measures to reduce or limit discharges, air emissions and releases to soil	Use appropriate air emissions abatement systems (e.g. wet or dry scrubber or local STP) to ensure that the emission levels defined by local regulations are not exceeded	
	Soil emission controls are not applicable as there is no direct release to soil	
Organisation measures to prevent/limit release from site	Ensure operatives are trained to minimise releases	
Conditions and measures related to sewage treatment plant	Direct emissions to the municipal STP should not be made.	
Conditions and measures related to external treatment of waste for disposal	See section 13 of the SDS	

#### 1.2.5 Contributing scenario controlling environmental exposure (ERC6b)

Industrial use of reactive processing aids	
ERC6b	Industrial use of reactive processing aids

#### Product characteristics

Physical form of product	See section 9 of the SDS, No additional information
Concentration of substance in product	<= 100 %

#### Operational conditions

Amounts used	Annual site tonnage:	25000 t/yr
	Regional use tonnage:	354000 t/yr
Frequency and duration of use	Emission Days (days/year)	330
Environmental factors not influenced by risk management	Flow rate of receiving water at least:	18000 m <sup>3</sup> /d
	Dilution of STP emissions at least:	10
Other given operational conditions affecting environmental exposure	Closed systems are used in order to prevent unintended emissions	

#### Risk Management Measures

Technical onsite conditions and measures to reduce or limit discharges, air emissions and releases to soil	Use appropriate air emissions abatement systems (e.g. wet or dry scrubber or local STP) to ensure that the emission levels defined by local regulations are not exceeded	
	Soil emission controls are not applicable as there is no direct release to soil	
Organisation measures to prevent/limit release from site	Ensure operatives are trained to minimise releases	
Conditions and measures related to sewage treatment plant	Direct emissions to the municipal STP should not be made.	
Conditions and measures related to external treatment of waste for disposal	See section 13 of the SDS	

#### 1.2.6 Contributing scenario controlling environmental exposure (ERC7)

Industrial use of substances in closed systems	
ERC7	Industrial use of substances in closed systems

#### Product characteristics

Physical form of product	See section 9 of the SDS, No additional information
Concentration of substance in product	<= 100 %

#### Operational conditions

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Amounts used	Annual site tonnage:	25000 t/yr
	Regional use tonnage:	354000 t/yr
Frequency and duration of use	Emission Days (days/year)	330
Environmental factors not influenced by risk management	Flow rate of receiving water at least:	18000 m <sup>3</sup> /d
	Dilution of STP emissions at least:	10
Other given operational conditions affecting environmental exposure	Closed systems are used in order to prevent unintended emissions	

#### Risk Management Measures

Technical onsite conditions and measures to reduce or limit discharges, air emissions and releases to soil	Use appropriate air emissions abatement systems (e.g. wet or dry scrubber or local STP) to ensure that the emission levels defined by local regulations are not exceeded	
	Soil emission controls are not applicable as there is no direct release to soil	
Organisation measures to prevent/limit release from site	Ensure operatives are trained to minimise releases	
Conditions and measures related to sewage treatment plant	Direct emissions to the municipal STP should not be made.	
Conditions and measures related to external treatment of waste for disposal	See section 13 of the SDS	

#### 1.2.7 Contributing scenario controlling worker exposure (PROC1)

Use in closed process, no likelihood of exposure	
PROC1	Use in closed process, no likelihood of exposure

#### Product characteristics

Physical form of product	See section 9 of the SDS, No additional information
Concentration of substance in product	<= 100 %

#### Operational conditions

Amounts used	The actual tonnage handled per shift is not considered to influence the exposure as such for this scenario. Instead, the combination of the scale of operation (industrial vs. professional) and level of containment/automation (as reflected in the PROCs and technical conditions) is the main determinant of the process-intrinsic emission potential.	
Frequency and duration of use	Exposure duration	<= 8 h/day
	Covers frequency up to:	5 days/week
Other given operational conditions affecting workers exposure	Indoor or outdoor use	

#### Risk Management Measures

Technical conditions and measures at process level (source) to prevent release	Handle product within a closed system	
	Apply a good standard of general or controlled ventilation when maintenance activities are carried out.	
Organisational measures to prevent /limit releases, dispersion and exposure	Ensure operatives are trained to minimise exposure	
	Ensure supervision is in place to check that the RMMs are in place and are being used correctly and that the OCs are being followed	
Conditions and measures related to personal protection, hygiene and health evaluation	See section 8 of the SDS.	


#### 1.2.8 Contributing scenario controlling worker exposure (PROC2)

Use in closed, continuous process with occasional controlled exposure	
PROC2	Use in closed, continuous process with occasional controlled exposure

#### Product characteristics

Physical form of product	See section 9 of the SDS, No additional information
Concentration of substance in product	<= 100 %



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### Operational conditions

Amounts used	The actual tonnage handled per shift is not considered to influence the exposure as such for this scenario. Instead, the combination of the scale of operation (industrial vs. professional) and level of containment/automation (as reflected in the PROCs and technical conditions) is the main determinant of the process-intrinsic emission potential.	
Frequency and duration of use	Exposure duration	<= 8 h/day
	Covers frequency up to:	5 days/week
Other given operational conditions affecting workers exposure	Indoor or outdoor use	

### Risk Management Measures

Technical conditions and measures at process level (source) to prevent release	Handle product within a closed system	
	During indoor processes or in cases where natural ventilation is not sufficient, LEV should be in place at points where emissions could occur. Outdoor, LEV is not generally required.	
	Ensure samples are obtained under containment or extract ventilation.	
	Drain down and flush system prior to equipment break-in or maintenance.	
	Apply a good standard of general or controlled ventilation when maintenance activities are carried out.	
Organisational measures to prevent /limit releases, dispersion and exposure	Ensure operatives are trained to minimise exposure	
	Ensure supervision is in place to check that the RMMs are in place and are being used correctly and that the OCs are being followed	
Conditions and measures related to personal protection, hygiene and health evaluation	Use suitable eye protection. Wear suitable face shield. Wear suitable coveralls to prevent exposure to the skin	Personal protection measures have to be applied in case of potential exposure only.
	Wear gloves providing a minimum efficiency of (%):	90
	Wear a respirator providing a minimum efficiency of (%):	95 Mandatory if activities take place outdoors or indoors with no local exhaust ventilation
	See section 8 of the SDS.	

#### 1.2.9 Contributing scenario controlling worker exposure (PROC3)

Use in closed batch process (synthesis or formulation)	
PROC3	Use in closed batch process (synthesis or formulation)

### Product characteristics

Physical form of product	See section 9 of the SDS, No additional information
Concentration of substance in product	<= 100 %

### Operational conditions

Amounts used	The actual tonnage handled per shift is not considered to influence the exposure as such for this scenario. Instead, the combination of the scale of operation (industrial vs. professional) and level of containment/automation (as reflected in the PROCs and technical conditions) is the main determinant of the process-intrinsic emission potential.	
Frequency and duration of use	Exposure duration	<= 8 h/day
	Covers frequency up to:	5 days/week
Other given operational conditions affecting workers exposure	Indoor or outdoor use	

### Risk Management Measures

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Technical conditions and measures at process level (source) to prevent release	Handle product within a closed system	
	During indoor processes or in cases where natural ventilation is not sufficient, LEV should be in place at points where emissions could occur. Outdoor, LEV is not generally required.	
	Ensure samples are obtained under containment or extract ventilation.	
	Drain down and flush system prior to equipment break-in or maintenance.	
	Apply a good standard of general or controlled ventilation when maintenance activities are carried out.	
Organisational measures to prevent /limit releases, dispersion and exposure	Ensure operatives are trained to minimise exposure	
	Ensure supervision is in place to check that the RMMs are in place and are being used correctly and that the OCs are being followed	
Conditions and measures related to personal protection, hygiene and health evaluation	Use suitable eye protection. Wear suitable face shield. Wear suitable coveralls to prevent exposure to the skin	Personal protection measures have to be applied in case of potential exposure only.
	Wear gloves providing a minimum efficiency of (%):	90
	Wear a respirator providing a minimum efficiency of (%):	95 Mandatory if activities take place outdoors or indoors with no local exhaust ventilation
	See section 8 of the SDS.	

#### 1.2.10 Contributing scenario controlling worker exposure (PROC4)

Use in batch and other process (synthesis) where opportunity for exposure arises	
PROC4	Use in batch and other process (synthesis) where opportunity for exposure arises

#### Product characteristics

Physical form of product	See section 9 of the SDS, No additional information
Concentration of substance in product	<= 100 %

#### Operational conditions

Amounts used	The actual tonnage handled per shift is not considered to influence the exposure as such for this scenario. Instead, the combination of the scale of operation (industrial vs. professional) and level of containment/automation (as reflected in the PROCs and technical conditions) is the main determinant of the process-intrinsic emission potential.	
Frequency and duration of use	Exposure duration	<= 8 h/day
	Covers frequency up to:	5 days/week
Other given operational conditions affecting workers exposure	Indoor or outdoor use	

#### Risk Management Measures

Technical conditions and measures at process level (source) to prevent release	Handle product within a closed system	
	During indoor processes or in cases where natural ventilation is not sufficient, LEV should be in place at points where emissions could occur. Outdoor, LEV is not generally required.	
	Ensure samples are obtained under containment or extract ventilation.	
	Drain down and flush system prior to equipment break-in or maintenance.	
	Apply a good standard of general or controlled ventilation when maintenance activities are carried out.	
Organisational measures to prevent /limit releases, dispersion and exposure	Ensure operatives are trained to minimise exposure	
	Ensure supervision is in place to check that the RMMs are in place and are being used correctly and that the OCs are being followed	

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Conditions and measures related to personal protection, hygiene and health evaluation	Use suitable eye protection. Wear suitable face shield. Wear suitable coveralls to prevent exposure to the skin	Personal protection measures have to be applied in case of potential exposure only.
	Wear gloves providing a minimum efficiency of (%):	90
	Wear a respirator providing a minimum efficiency of (%):	95 Mandatory if activities take place outdoors or indoors with no local exhaust ventilation
	See section 8 of the SDS.	

#### 1.2.11 Contributing scenario controlling worker exposure (PROC8b)

Transfer of substance or preparation (charging/discharging) from/to vessels/large containers at dedicated facilities	
PROC8b	Transfer of substance or preparation (charging/discharging) from/to vessels/large containers at dedicated facilities

#### Product characteristics

Physical form of product	See section 9 of the SDS, No additional information
Concentration of substance in product	<= 100 %

#### Operational conditions

Amounts used	The actual tonnage handled per shift is not considered to influence the exposure as such for this scenario. Instead, the combination of the scale of operation (industrial vs. professional) and level of containment/automation (as reflected in the PROCs and technical conditions) is the main determinant of the process-intrinsic emission potential.	
Frequency and duration of use	Exposure duration	<= 8 h/day
	Covers frequency up to:	5 days/week
Other given operational conditions affecting workers exposure	Indoor or outdoor use	

#### Risk Management Measures


Technical conditions and measures at process level (source) to prevent release	Handle product within a closed system	
	During indoor processes or in cases where natural ventilation is not sufficient, LEV should be in place at points where emissions could occur. Outdoor, LEV is not generally required.	
	Fill containers at dedicated fill points supplied with local extract ventilation.	
	Drain down and flush system prior to equipment break-in or maintenance.	
	Apply a good standard of general or controlled ventilation when maintenance activities are carried out.	
Organisational measures to prevent /limit releases, dispersion and exposure	Ensure operatives are trained to minimise exposure	
	Ensure supervision is in place to check that the RMMs are in place and are being used correctly and that the OCs are being followed	
Conditions and measures related to personal protection, hygiene and health evaluation	Use suitable eye protection. Wear suitable face shield. Wear suitable coveralls to prevent exposure to the skin	Personal protection measures have to be applied in case of potential exposure only.
	Wear gloves providing a minimum efficiency of (%):	90
	Wear a respirator providing a minimum efficiency of (%):	95 Mandatory if activities take place outdoors or indoors with no local exhaust ventilation
	See section 8 of the SDS.	

#### 1.2.12 Contributing scenario controlling worker exposure (PROC9)

Transfer of substance or preparation into small containers (dedicated filling line, including weighing)	
PROC9	Transfer of substance or mixture into small containers (dedicated filling line, including weighing)

#### Product characteristics

Physical form of product	See section 9 of the SDS, No additional information
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Concentration of substance in product	<= 100 %
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#### Operational conditions

Amounts used	The actual tonnage handled per shift is not considered to influence the exposure as such for this scenario. Instead, the combination of the scale of operation (industrial vs. professional) and level of containment/automation (as reflected in the PROCs and technical conditions) is the main determinant of the process-intrinsic emission potential.	
Frequency and duration of use	Exposure duration	<= 8 h/day
	Covers frequency up to:	5 days/week
Other given operational conditions affecting workers exposure	Indoor or outdoor use	

#### Risk Management Measures

Technical conditions and measures at process level (source) to prevent release	Handle product within a closed system	
	During indoor processes or in cases where natural ventilation is not sufficient, LEV should be in place at points where emissions could occur. Outdoor, LEV is not generally required.	
	Fill containers at dedicated fill points supplied with local extract ventilation.	
	Drain down and flush system prior to equipment break-in or maintenance.	
	Apply a good standard of general or controlled ventilation when maintenance activities are carried out.	
Organisational measures to prevent /limit releases, dispersion and exposure	Ensure operatives are trained to minimise exposure	
	Ensure supervision is in place to check that the RMMs are in place and are being used correctly and that the OCs are being followed	
Conditions and measures related to personal protection, hygiene and health evaluation	Use suitable eye protection. Wear suitable face shield. Wear suitable coveralls to prevent exposure to the skin	Personal protection measures have to be applied in case of potential exposure only.
	Wear gloves providing a minimum efficiency of (%):	90
	Wear a respirator providing a minimum efficiency of (%):	95 Mandatory if activities take place outdoors or indoors with no local exhaust ventilation
	See section 8 of the SDS.	

### 3. Exposure estimation and reference to its source

#### 3.1. Health

#### 3.2. Environment


### 4. Guidance to Downstream User to evaluate whether he works inside the boundaries set by the ES

#### 4.1. Health

Guidance - Health	Guidance is based on assumed operating conditions which may not be applicable to all sites; thus, scaling may be necessary to define appropriate site-specific risk management measures. For scaling see : . <a href="http://www.ecetoc.org/tra">http://www.ecetoc.org/tra</a>
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#### 4.2. Environment

Guidance - Environment	Guidance is based on assumed operating conditions which may not be applicable to all sites; thus, scaling may be necessary to define appropriate site-specific risk management measures. For scaling see : . <a href="https://ec.europa.eu/jrc/en/scientific-tool/european-union-system-evaluation-substances">https://ec.europa.eu/jrc/en/scientific-tool/european-union-system-evaluation-substances</a>
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## 1. Exposure scenario EIGA002-2

### Professional uses

ES Ref.: EIGA002-2 ES Type: Worker - EIGA Revision date: 25/04/2017	
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Use descriptors	SU22 PROC4, PROC8a ERC9a, ERC9b
Processes, tasks, activities covered	Professional uses, including transfer of product in non-industrial settings
Assessment method	ECETOC TRA 2.0

## 2. Operational conditions and risk management measures

### 1.2.1 Contributing scenario controlling environmental exposure (ERC9a, ERC9b)

Wide dispersive indoor use of substances in closed systems, Wide dispersive outdoor use of substances in closed systems	
ERC9a	Wide dispersive indoor use of substances in closed systems
ERC9b	Wide dispersive outdoor use of substances in closed systems

#### Product characteristics

Physical form of product	See section 9 of the SDS, No additional information
Concentration of substance in product	<= 100 %

#### Operational conditions

Amounts used	No additional information
Other given operational conditions affecting environmental exposure	Closed systems are used in order to prevent unintended emissions

#### Risk Management Measures

Organisation measures to prevent/limit release from site	Ensure operatives are trained to minimise exposure
Conditions and measures related to sewage treatment plant	No additional information
Conditions and measures related to external treatment of waste for disposal	See section 13 of the SDS

### 1.2.2 Contributing scenario controlling worker exposure (PROC4)

Use in batch and other process (synthesis) where opportunity for exposure arises	
PROC4	Use in batch and other process (synthesis) where opportunity for exposure arises

#### Product characteristics

Physical form of product	See section 9 of the SDS, No additional information
Concentration of substance in product	<= 100 %

#### Operational conditions

Amounts used	The actual tonnage handled per shift is not considered to influence the exposure as such for this scenario. Instead, the combination of the scale of operation (industrial vs. professional) and level of containment/automation (as reflected in the PROCs and technical conditions) is the main determinant of the process-intrinsic emission potential.	
Frequency and duration of use	Exposure duration	<= 8 h/day
	Covers frequency up to:	5 days/week
Other given operational conditions affecting workers exposure	Indoor or outdoor use	

#### Risk Management Measures

Technical conditions and measures at process level (source) to prevent release	Handle product within a closed system
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	During indoor processes or in cases where natural ventilation is not sufficient, LEV should be in place at points where emissions could occur. Outdoor, LEV is not generally required.	
	Drain down and flush system prior to equipment break-in or maintenance.	
	Apply a good standard of general or controlled ventilation when maintenance activities are carried out.	
Organisational measures to prevent /limit releases, dispersion and exposure	Ensure operatives are trained to minimise exposure	
	Ensure supervision is in place to check that the RMMs are in place and are being used correctly and that the OCs are being followed	
Conditions and measures related to personal protection, hygiene and health evaluation	Use suitable eye protection. Wear suitable face shield. Wear suitable coveralls to prevent exposure to the skin	Personal protection measures have to be applied in case of potential exposure only.
	Wear gloves providing a minimum efficiency of (%):	90
	Wear a respirator providing a minimum efficiency of	95 Mandatory if activities take place outdoors or indoors with no local exhaust ventilation
	See section 8 of the SDS.	

### 1.2.3 Contributing scenario controlling worker exposure (PROC8a)

Transfer of substance or preparation (charging/discharging) from/to vessels/large containers at non dedicated facilities

PROC8a

Transfer of substance or preparation (charging/discharging) from/to vessels/large containers at non dedicated facilities

#### Product characteristics


Physical form of product	See section 9 of the SDS, No additional information
Concentration of substance in product	<= 100 %

#### Operational conditions

Amounts used	The actual tonnage handled per shift is not considered to influence the exposure as such for this scenario. Instead, the combination of the scale of operation (industrial vs. professional) and level of containment/automation (as reflected in the PROCs and technical conditions) is the main determinant of the process-intrinsic emission potential.	
Frequency and duration of use	Exposure duration	<= 8 h/day
	Covers frequency up to:	5 days/week
Other given operational conditions affecting workers exposure	Indoor or outdoor use	

#### Risk Management Measures

Technical conditions and measures at process level (source) to prevent release	Handle product within a closed system	
	During indoor processes or in cases where natural ventilation is not sufficient, LEV should be in place at points where emissions could occur. Outdoor, LEV is not generally required.	
	Drain down and flush system prior to equipment break-in or maintenance.	
	Apply a good standard of general or controlled ventilation when maintenance activities are carried out.	
Organisational measures to prevent /limit releases, dispersion and exposure	Ensure operatives are trained to minimise exposure	
	Ensure supervision is in place to check that the RMMs are in place and are being used correctly and that the OCs are being followed	
Conditions and measures related to personal protection, hygiene and health evaluation	Use suitable eye protection. Wear suitable face shield. Wear suitable coveralls to prevent exposure to the skin	Personal protection measures have to be applied in case of potential exposure only.
	Wear gloves providing a minimum efficiency of (%):	90

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	Wear a respirator providing a minimum efficiency of	95
	See section 8 of the SDS.	Mandatory if activities take place outdoors or indoors with no local exhaust ventilation

### 3. Exposure estimation and reference to its source

3.1. Health

3.2. Environment

### 4. Guidance to Downstream User to evaluate whether he works inside the boundaries set by the ES

4.1. Health

Guidance - Health	Guidance is based on assumed operating conditions which may not be applicable to all sites; thus, scaling may be necessary to define appropriate site-specific risk management measures. For scaling see : . <a href="http://www.ecetoc.org/tra">http://www.ecetoc.org/tra</a>
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4.2. Environment

Guidance - Environment	Check that RMMs and OCs are as described above or of equivalent efficiency
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# Appendix D: Extended Financial Information

Process Title: **Green Ammonia**  
 Product: **Ammonia**  
 Plant Site Location: **SW Norway**  
 Site Factor: **1.00**  
 Operating Hours per Year: **8400**  
 Operating Days Per Year: **350**  
 Operating Factor: **0.9589**

## Product Information

This Process will Yield

**2** ton of Ammonia per hour  
**46** ton of Ammonia per day  
**16,178** ton of Ammonia per year

Price **\$550.00 /ton**

## Chronology

<u>Year</u>	<u>Action</u>	<u>Distribution of Permanent Investment</u>	<u>Production Capacity</u>	<u>Depreciation 20 year MACRS</u>	<u>Product Price</u>
2020	Design		0.0%		
2021	Construction	100%	0.0%		
2022	Production	0%	45.0%	3.75%	\$550.00
2023	Production	0%	67.5%	7.22%	\$569.25
2024	Production	0%	90.0%	6.68%	\$589.17
2025	Production		90.0%	6.18%	\$609.79
2026	Production		90.0%	5.71%	\$631.14
2027	Production		90.0%	5.29%	\$653.23
2028	Production		90.0%	4.89%	\$676.09
2029	Production		90.0%	4.52%	\$699.75
2030	Production		90.0%	4.46%	\$724.24
2031	Production		90.0%	4.46%	\$749.59
2032	Production		90.0%	4.46%	\$775.83
2033	Production		90.0%	4.46%	\$802.98
2034	Production		90.0%	4.46%	\$831.09
2035	Production		90.0%	4.46%	\$860.18
2036	Production		90.0%	4.46%	\$890.28



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**Equipment Costs**

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<u>Equipment Description</u>		<u>Bare Module Cost</u>
Haber Bosch Reactor	Process Machinery	\$340,823
Sodium Doped Iron Catalyst	Catalysts	\$20,000
HB-CP-01	Process Machinery	\$30,146
HB-CP-02	Process Machinery	\$3,021,123
HB-HXA-01	Process Machinery	\$127,161
HB-HXA-02	Process Machinery	\$105,901
HB-HXA-03	Process Machinery	\$153,087
HB-HXA-04	Process Machinery	\$120,435
#REF!	#REF!	#REF!
HB-S-01	Process Machinery	\$66,024
HB-S-02	Process Machinery	\$57,136
Storage Tank	Storage	\$940,000
SOEC	Process Machinery	\$15,000,000
UP-EM-01	Process Machinery	\$5,720
UP-PM-01	Process Machinery	\$42,068
#REF!	#REF!	#REF!
#REF!	#REF!	#REF!
UP-CP-01	Process Machinery	\$479,984
UP-CP-02	Process Machinery	\$525,826
UP-CP-03	Process Machinery	\$504,596
UP-CP-04	Process Machinery	\$55,437
UP-HX-01	Process Machinery	\$108,504
UP-HX-02	Process Machinery	\$148,064
UP-CO-01	Process Machinery	\$45,449
UP-CO-02	Process Machinery	\$39,081
UP-CO-03	Process Machinery	\$46,168
UP-CD-01	Process Machinery	\$150,110
M6 Filter	Process Machinery	\$8,000
Ion Exchange Unit	Process Machinery	\$300,000

**Total**

**#REF!**

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**Raw Materials**

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<u>Raw Material:</u>	<u>Unit:</u>	<u>Required Ratio:</u>	<u>Cost of Raw Material:</u>
1 Water	ton	1.5 ton per ton of Ammonia	\$0.000E+00 per ton
2 Air	ton	1 ton per ton of Ammonia	\$0.00 per ton

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Total Weighted Average: \$0.000E+00 per ton of Ammonia

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**Byproducts**

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<u>Byproduct:</u>	<u>Unit:</u>	<u>Ratio to Product</u>	<u>Byproduct Selling Price</u>
1 Oxygen	kg	220 kg per ton of Ammonia	\$0.200 per kg

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Total Weighted Average: \$44.000 per ton of Ammonia

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**Utilities**

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<u>Utility:</u>	<u>Unit:</u>	<u>Required Ratio</u>	<u>Utility Cost</u>
1 High Pressure Steam	MT	0 MT per ton of Ammonia	\$0.000E+00 per MT
2 Low Pressure Steam	MT	0 MT per ton of Ammonia	\$0.000E+00 per MT
3 Process Water	gal	0 gal per ton of Ammonia	\$0.000E+00 per gal
4 Cooling Water	MT	17.340462 MT per ton of Ammonia	\$0.027 per MT
5 Chilled Water	MT	71.023798 MT per ton of Ammonia	\$1.500 per MT

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Total Weighted Average: \$107.004 per ton of Ammonia

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**Variable Costs**

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**General Expenses:**

Selling / Transfer Expenses:	3.00% of Sales
Direct Research:	4.80% of Sales
Allocated Research:	0.50% of Sales
Administrative Expense:	2.00% of Sales
Management Incentive Compensation:	1.25% of Sales

**Working Capital**

---

Accounts Receivable	⇒	30	Days
Cash Reserves (excluding Raw Materials)	⇒	30	Days
Accounts Payable	⇒	30	Days
Ammonia Inventory	⇒	3	Days
Raw Materials	⇒	2	Days

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**Total Permanent Investment**

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Cost of Site Preparations:	5.00% of Total Bare Module Costs
Cost of Service Facilities:	5.00% of Total Bare Module Costs
Allocated Costs for utility plants and related facilities:	\$0
Cost of Contingencies and Contractor Fees:	18.00% of Direct Permanent Investment
Cost of Land:	0.50% of Total Depreciable Capital
Cost of Royalties:	\$0
Cost of Plant Start-Up:	10.00% of Total Depreciable Capital

---

**Fixed Costs**

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**Operations**

Operators per Shift:	5 (assuming 5 shifts)
Direct Wages and Benefits:	\$40 /operator hour
Direct Salaries and Benefits:	15% of Direct Wages and Benefits
Operating Supplies and Services:	6% of Direct Wages and Benefits
Technical Assistance to Manufacturing:	\$7,920.00 per year, for each Operator per Shift
Control Laboratory:	\$11,700.00 per year, for each Operator per Shift

**Maintenance**

Wages and Benefits:	2.00% of Total Depreciable Capital
Salaries and Benefits:	25% of Maintenance Wages and Benefits
Materials and Services:	100% of Maintenance Wages and Benefits
Maintenance Overhead:	5% of Maintenance Wages and Benefits

**Operating Overhead**

General Plant Overhead:	7.10% of Maintenance and Operations Wages and Benefits
Mechanical Department Services:	2.40% of Maintenance and Operations Wages and Benefits
Employee Relations Department:	5.90% of Maintenance and Operations Wages and Benefits
Business Services:	7.40% of Maintenance and Operations Wages and Benefits

**Property Taxes and Insurance**

Property Taxes and Insurance:	2% of Total Depreciable Capital
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**Straight Line Depreciation**

Direct Plant:	8.00% of Total Depreciable Capital, less 1.18 times the Allocated Costs for Utility Plants and Related Facilities
Allocated Plant:	6.00% of 1.18 times the Allocated Costs for Utility Plants and Related Facilities

**Other Annual Expenses**

Rental Fees (Office and Laboratory Space):	\$0
Licensing Fees:	\$0
Miscellaneous:	\$0

**Depletion Allowance**

Annual Depletion Allowance:	\$0
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**Variable Cost Summary**

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**Variable Costs at 100% Capacity:****General Expenses**

Selling / Transfer Expenses:	\$	266,944
Direct Research:	\$	427,110
Allocated Research:	\$	44,491
Administrative Expense:	\$	177,962
Management Incentive Compensation:	\$	111,227

**Total General Expenses** \$ 1,027,733

**Raw Materials** \$0.00 per ton of Ammonia \$0

**Byproducts** \$44.00 per ton of Ammonia (\$711,850)

**Utilities** \$107.00 per ton of Ammonia \$1,731,152

**Total Variable Costs** \$ 2,047,035

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**Fixed Cost Summary**

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**Operations**

Direct Wages and Benefits	\$	2,080,000
Direct Salaries and Benefits	\$	312,000
Operating Supplies and Services	\$	124,800
Technical Assistance to Manufacturing	\$	198,000
Control Laboratory	\$	292,500

**Total Operations** \$ 3,007,300

**Maintenance**

Wages and Benefits	\$	636,072
Salaries and Benefits	\$	159,018
Materials and Services	\$	636,072
Maintenance Overhead	\$	31,804

**Total Maintenance** \$ 1,462,966

**Operating Overhead**

General Plant Overhead:	\$	226,283
Mechanical Department Services:	\$	76,490
Employee Relations Department:	\$	188,038
Business Services:	\$	235,845

**Total Operating Overhead** \$ 726,657

**Property Taxes and Insurance**

Property Taxes and Insurance: \$ 636,072

**Other Annual Expenses**

Rental Fees (Office and Laboratory Space):	\$	-
Licensing Fees:	\$	-
Miscellaneous:	\$	-

**Total Other Annual Expenses** \$ -

**Total Fixed Costs** \$ 5,832,994

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**Investment Summary**

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**Total Bare Module Costs:**

Fabricated Equipment	\$	-	
Process Machinery	\$	23,542,003	
Spares	\$	-	
Storage	\$	940,000	
Other Equipment	\$	-	
Catalysts	\$	20,000	
Computers, Software, Etc.	\$	-	
<b>Total Bare Module Costs:</b>			<b>\$ 24,502,003</b>

**Direct Permanent Investment**

Cost of Site Preparations:	\$	1,225,100	
Cost of Service Facilities:	\$	1,225,100	
Allocated Costs for utility plants and related facilities:	\$	-	
<b>Direct Permanent Investment</b>			<b>\$ 26,952,203</b>

**Total Depreciable Capital**

Cost of Contingencies & Contractor Fees	\$	4,851,397	
<b>Total Depreciable Capital</b>			<b>\$ 31,803,600</b>

**Total Permanent Investment**

Cost of Land:	\$	159,018	
Cost of Royalties:	\$	-	
Cost of Plant Start-Up:	\$	3,180,360	
Total Permanent Investment - Unadjusted			\$ 35,142,978
Site Factor			1.00
<b>Total Permanent Investment</b>			<b>\$ 35,142,978</b>

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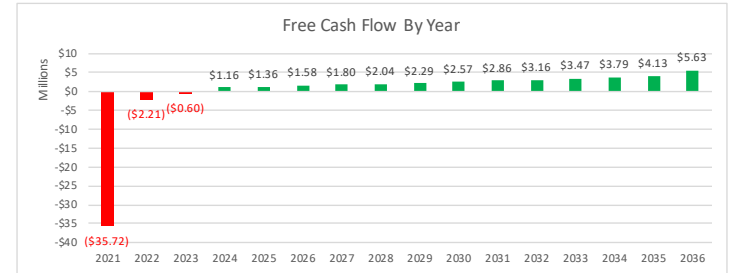
**Working Capital**

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	<u>2021</u>	<u>2022</u>	<u>2023</u>
Accounts Receivable	\$ 329,109	\$ 164,554	\$ 164,554
Cash Reserves	\$ 279,770	\$ 139,885	\$ 139,885
Accounts Payable	\$ (64,029)	\$ (32,014)	\$ (32,014)
Ammonia Inventory	\$ 32,911	\$ 16,455	\$ 16,455
Raw Materials	\$ -	\$ -	\$ -
<b>Total</b>	<b>\$ 577,760</b>	<b>\$ 288,880</b>	<b>\$ 288,880</b>
<i>Present Value at 10%</i>	\$ 525,237	\$ 238,744	\$ 217,040
<b>Total Capital Investment</b>			<b>\$ 36,123,998</b>

### Cash Flow Summary

Year	Percentage of Design Capacity	Product Unit Price	Sales	Capital Costs	Working Capital	Var Costs	Total Costs	20 year MACRS	Fixed Costs	Depreciation	Depletion Allowance	Taxable Income	Taxes	Net Earnings	Cash Flow	Cumulative Net Present Value at 10%
2020	0%	-	-	-	-	-	-	0.00%	-	-	-	-	-	-	-	-
2021	0%	-	-	(35,143,000)	(577,800)	-	-	0.00%	-	-	-	-	-	-	(35,720,700)	(32,473,400)
2022	45%	\$550.00	4,004,200	-	(288,900)	(921,200)	(6,754,160)	3.75%	(5,833,000)	(1,192,600)	-	(3,942,600)	828,000	(3,114,700)	(2,210,900)	(34,300,600)
2023	68%	\$569.25	6,216,400	-	-	(1,381,700)	(7,214,743)	7.22%	(5,833,000)	(2,295,900)	-	(3,294,200)	691,800	(2,602,400)	(595,400)	(34,747,900)
2024	90%	\$589.17	8,578,700	-	-	(1,842,300)	(7,675,326)	6.68%	(5,833,000)	(2,123,500)	-	(1,220,200)	256,200	(963,900)	1,159,600	(33,955,900)
2025	90%	\$609.79	8,879,000	-	-	(1,842,300)	(7,675,326)	6.18%	(5,833,000)	(1,964,500)	-	(760,900)	159,800	(601,100)	1,363,400	(33,109,300)
2026	90%	\$631.14	9,189,700	-	-	(1,842,300)	(7,675,326)	5.71%	(5,833,000)	(1,816,900)	-	(302,500)	63,500	(239,000)	1,577,900	(32,218,600)
2027	90%	\$653.23	9,511,400	-	-	(1,842,300)	(7,675,326)	5.29%	(5,833,000)	(1,680,800)	-	155,200	(32,600)	122,600	1,803,400	(31,293,200)
2028	90%	\$676.09	9,844,300	-	-	(1,842,300)	(7,675,326)	4.89%	(5,833,000)	(1,554,600)	-	614,400	(129,000)	485,400	2,039,900	(30,341,600)
2029	90%	\$699.75	10,188,800	-	-	(1,842,300)	(7,675,326)	4.52%	(5,833,000)	(1,438,200)	-	1,075,300	(225,800)	849,500	2,287,700	(29,371,400)
2030	90%	\$724.24	10,545,400	-	-	(1,842,300)	(7,675,326)	4.46%	(5,833,000)	(1,419,100)	-	1,451,000	(304,700)	1,146,300	2,565,400	(28,382,300)
2031	90%	\$749.59	10,914,500	-	-	(1,842,300)	(7,675,326)	4.46%	(5,833,000)	(1,418,800)	-	1,820,400	(382,300)	1,438,100	2,856,900	(27,381,000)
2032	90%	\$775.83	11,296,500	-	-	(1,842,300)	(7,675,326)	4.46%	(5,833,000)	(1,419,100)	-	2,202,100	(462,400)	1,739,700	3,158,700	(26,374,500)
2033	90%	\$802.98	11,691,900	-	-	(1,842,300)	(7,675,326)	4.46%	(5,833,000)	(1,418,800)	-	2,597,800	(545,500)	2,052,300	3,471,000	(25,369,100)
2034	90%	\$831.09	12,101,100	-	-	(1,842,300)	(7,675,326)	4.46%	(5,833,000)	(1,419,100)	-	3,006,700	(631,400)	2,375,300	3,794,400	(24,369,900)
2035	90%	\$860.18	12,524,600	-	-	(1,842,300)	(7,675,326)	4.46%	(5,833,000)	(1,418,800)	-	3,430,600	(720,400)	2,710,100	4,128,900	(23,381,500)
2036	90%	\$890.28	12,963,000	-	1,155,500	(1,842,300)	(7,675,326)	4.46%	(5,833,000)	(1,419,100)	-	3,868,600	(812,400)	3,056,200	5,630,800	(22,156,100)



## Profitability Measures

The Internal Rate of Return (IRR) for this project is -0.68%

The Net Present Value (NPV) of this project in 2020 is \$ (22,156,100)

### ROI Analysis (Third Production Year)

Annual Sales	8,578,700
Annual Costs	(7,675,326)
Depreciation	(2,811,438)
Income Tax	400,693
Net Earnings	<u>(1,507,371)</u>
Total Capital Investment	<u>36,298,499</u>
ROI	-4.15%

## Sensitivity Analyses

Note: The Sensitivity Analyses section below takes quite a bit of memory to update each time a cell is changed; therefore, automatic calculations are turned off. After making your axis selections, press "F9" to recalculate the IRR values. (These two lines may be deleted before printing.)

		Vary Initial Value by +/-									
		x-axis					y-axis				
		50%					5%				
		Total Permanent Investment									
		\$17,571,489	\$21,085,787	\$24,600,085	\$28,114,382	\$31,628,680	<b>\$35,142,978</b>	\$38,657,276	\$42,171,574	\$45,685,871	\$49,200,169
Product Price	\$523	14.84%	9.92%	6.02%	2.82%	0.10%	-2.27%	-4.36%	-6.24%	-7.95%	-9.52%
	\$528	15.34%	10.35%	6.42%	3.18%	0.44%	-1.94%	-4.04%	-5.92%	-7.64%	-9.21%
	\$534	15.84%	10.78%	6.80%	3.53%	0.77%	-1.62%	-3.73%	-5.62%	-7.33%	-8.91%
	\$539	16.33%	11.21%	7.18%	3.89%	1.10%	-1.30%	-3.42%	-5.32%	-7.04%	-8.62%
	\$545	16.82%	11.63%	7.56%	4.23%	1.43%	-0.99%	-3.12%	-5.02%	-6.75%	-8.33%
	<b>\$550</b>	17.31%	12.05%	7.93%	4.57%	1.75%	-0.68%	-2.82%	-4.73%	-6.46%	-8.05%
	\$556	17.79%	12.46%	8.30%	4.91%	2.07%	-0.38%	-2.53%	-4.45%	-6.18%	-7.77%
	\$561	18.27%	12.87%	8.66%	5.24%	2.38%	-0.09%	-2.25%	-4.17%	-5.91%	-7.50%
	\$567	18.74%	13.27%	9.02%	5.57%	2.68%	0.21%	-1.97%	-3.90%	-5.64%	-7.24%
	\$572	19.21%	13.67%	9.37%	5.90%	2.99%	0.49%	-1.69%	-3.63%	-5.38%	-6.98%
	\$578	19.68%	14.07%	9.73%	6.22%	3.29%	0.78%	-1.42%	-3.37%	-5.12%	-6.72%

Process Title: **Green Ammonia**  
 Product: **Ammonia**  
 Plant Site Location: **SW Norway**

**Timeline:**

Number of Years for Design 1 (must be whole number)  
 Number of Years for Construction 1 (must be whole number)  
 Number of Years for Production 15  
 Total Number of Years for Project 17  
 Start Year 2020  
 Site Factor 1.00

**Continuous Operation:**

Days per Year 350  
 OR  
 Hours per Year 0  
 OR  
 Operating Factor (if multiple entries, "Operating Factor" is used)

**Discrete Operation:**

(cannot use Continuous AND Discrete. If both entered, D)  
 Hours per Day 0  
 AND  
 Days per Year 0  
 Production Capacity 90% of Design Capacity  
 Start production at 50% of Production Capacity  
 Years to achieve full capacity 2  
 Number of Shifts 5  
 Depreciation Schedule 20 year

Income Tax Rate 21%  
 Cost of Capital (for the NPV Calculation) 10% (discount rate)  
 General Inflation Rate 0%  
 Product Inflation Rate 0%  
 Variable Cost Inflation Rate 0%  
 Fixed Cost Inflation Rate 0%

**Product Information:**

Enter Product Units ton  
 (i.e. lb, gram, gal, etc)  
 Price Per Unit \$550.00 /ton

Number of units per: (Specify ONE of the three. If multiple entries, "Year" is used.)

**Year** - ton per Year  
 OR  
**Day** - ton per Day  
 OR  
**Hour** 2 ton per Hour



**Raw Materials**

	<b>Raw Material:</b>	<b>Unit:</b>	<b>Required Ratio:</b>	<b>Cost of Raw Ma</b>
1	Water	ton	1.5 ton per ton of Ammonia	\$0.000E+00
2	Air	ton	1 ton per ton of Ammonia	\$0.000E+00
3				
4				
5				
6				
7				
8				
9				
10				
<hr/> <i>Total Weighted Average:</i>				\$0.000E+00

**Byproducts**

	<b>Byproduct:</b>	<b>Unit:</b>	<b>Ratio to Product</b>	<b>Byproduct Selli</b>
1	Oxygen	kg	220 kg per ton of Ammonia	\$0.200
2				
3				
4				
5				
6				
7				
8				
9				
10				
<hr/> <i>Total Weighted Average:</i>				\$44.000

**Utilities**

	<b>Utility:</b>	<b>Unit:</b>	<b>Required Ratio</b>	<b>Utility Cost</b>
1	High Pressure Steam	MT	0 MT per ton of Ammonia	
2	Low Pressure Steam	MT	0 MT per ton of Ammonia	
3	Process Water	gal	0 gal per ton of Ammonia	
4	Cooling Water	MT	17.34046236 MT per ton of Ammonia	\$0.027
5	Chilled Water	MT	71.02379775 MT per ton of Ammonia	\$1.500
6				
7				
8				
9				
10				
<hr/> <i>Total Weighted Average:</i>				\$107.004

iscrete used by default)

**terial:**

per ton  
per ton

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per ton of Ammonia

**ng Price**  
per kg

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per ton of Ammonia

per MT  
per MT  
per gal  
per MT  
per MT

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per ton of Ammonia

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## Selling Price Worksheet

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This worksheet is optional. It may be used to adjust the product selling prices each year. Your inputs for the product prices, adjusted using the inflation rates, are entered as default values. To change, enter a price into the "Manual Input Price" column.

Year	Calculated Unit Price	Manual Input Price	Price to Be Used
2022	\$550.00	\$550.00	\$550.00
2023	\$550.00	\$569.25	\$569.25
2024	\$550.00	\$589.17	\$589.17
2025	\$550.00	\$609.79	\$609.79
2026	\$550.00	\$631.14	\$631.14
2027	\$550.00	\$653.23	\$653.23
2028	\$550.00	\$676.09	\$676.09
2029	\$550.00	\$699.75	\$699.75
2030	\$550.00	\$724.24	\$724.24
2031	\$550.00	\$749.59	\$749.59
2032	\$550.00	\$775.83	\$775.83
2033	\$550.00	\$802.98	\$802.98
2034	\$550.00	\$831.09	\$831.09
2035	\$550.00	\$860.18	\$860.18
2036	\$550.00	\$890.28	\$890.28

## Other Variable Costs

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### General Expenses

Selling / Transfer Expenses:	3.00% of Sales
Direct Research:	4.80% of Sales
Allocated Research:	0.50% of Sales
Administrative Expense:	2.00% of Sales
Management Incentive Compensation:	1.25% of Sales

## Working Capital

---

Accounts Receivable	⇒	<b>30 Days</b>
Cash Reserves (excluding Raw Materials)	⇒	<b>30 Days</b>
Accounts Payable	⇒	<b>30 Days</b>
Ammonia Inventory	⇒	<b>3 Days</b>
Raw Materials	⇒	<b>2 Days</b>

---

**Total Permanent Investment**

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	% of Total Permanent Investment	
<u>Year:</u> <b>2021</b>	100%	(default is first year of Construction, otherwise)
<b>2022</b>	0%	
<b>2023</b>	0%	
<b>2024</b>	0%	
Cost of Site Preparations:	5.00%	of Total Bare Module Costs
Cost of Service Facilities:	5.00%	of Total Bare Module Costs
Allocated Costs for utility plants and related facilities:	\$0	
Cost of Contingencies and Contractor Fees:	18.00%	of Direct Permanent Investment
Cost of Land:	0.50%	of Total Depreciable Capital
Cost of Royalties:	\$0	
Cost of Plant Start-Up:	10.00%	of Total Depreciable Capital



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**Fixed Costs**

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**Operations**

Operators per Shift:	5 (assuming 5 shifts)
Direct Wages and Benefits:	\$40 /operator hour
Direct Salaries and Benefits:	15% of Direct Wages and Benefits
Operating Supplies and Services:	6% of Direct Wages and Benefits
Technical Assistance to Manufacturing:	\$7,920.00 per year, for each Operator per Shift
Control Laboratory:	\$11,700.00 per year, for each Operator per Shift

**Maintenance**

Wages and Benefits:	2.00% of Total Depreciable Capital
Salaries and Benefits:	25.00% of Maintenance Wages and Benefits
Materials and Services:	100.00% of Maintenance Wages and Benefits
Maintenance Overhead:	5.00% of Maintenance Wages and Benefits

**Operating Overhead**

General Plant Overhead:	7.10% of Maintenance and Operations Wages and Benefits
Mechanical Department Services:	2.40% of Maintenance and Operations Wages and Benefits
Employee Relations Department	5.90% of Maintenance and Operations Wages and Benefits
Business Services	7.40% of Maintenance and Operations Wages and Benefits

**Property Taxes and Insurance**

Property Taxes and Insurance:	2.00% of Total Depreciable Capital
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**Straight Line Depreciation**

Direct Plant:	8.00% of Total Depreciable Capital, less	1.18 times the Allocated Costs for Utility Plants and Related Facilities
Allocated Plant:	6.00% of	1.18 times the Allocated Costs for Utility Plants and Related Facilities

**Other Annual Expenses**

Rental Fees (Office and Laboratory Space):	\$0
Licensing Fees:	\$0
Miscellaneous:	\$0

**Depletion Allowance**

Annual Depletion Allowance:	\$0
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## Appendix E.1: Equipment Costing SOEC

## Bare Module Cost Analysis Worksheet

### Instructions (Read Carefully Before Using!!!)

1. Input the CE cost index below that corresponds to the date when you want the cost estimate (e.g. a 2018 CE will provide 2018 costs for equipment) . The CE index will automatically update each page accordingly.
2. Select the link below for the appropriate unit operation. Links provided at the top of each worksheet will return back to this title page.
3. Enter all data into the yellow boxes ONLY. For a process involving multiple sizes of the same type unit operations, use a different line to input the specs (up to 5 provided)
4. The Bare Module Cost of the Unit Operation is calculated and shown in red.
 

**Bare Module Cost**
5. If you are extrapolating the cost correlations, the spreadsheet will warn you. Consult the textbook for valid ranges of the equations, and use outside those ranges very carefully.
6. Below are the individual unit bare module costs and compiled tables of each type of unit operation, summarizing the different properties.
7. Total Bare Module Cost for all types of all equipment is also displayed below.

### All costing from:

Product and Process Design Principles

4th Edition

© Seider, Lewin, Seader, Widagdo, Gani, Ng, 2017

Worksheet prepared by Prof. Russell Dunn, Department of Chemical and Biomolecular Engineering, Vanderbilt University

Revised by Prof. Bruce Vrana, Department of Chemical and Biomolecular Engineering, University of Pennsylvania

CE Cost Index for this Estimate

600

Equipment	Total Cbm For each Unit Op
Electric Motors	\$ 5,720
Centrifugal Pumps	\$ 42,068
External Gear Pumps	\$ -
Reciprocating Plunger Pumps	\$ -
Fans	\$ -
Centrifugal (turbo) Blower	\$ -
Rotary Straight Lobe Blower	\$ -
Compressors	\$ 1,565,844
Shell and Tube Heat Exchanger	\$ 387,265
Double Pipe Heat Exchanger	\$ -
Fired Heaters	\$ 2,061,159
Pressure Vessel	\$ -
Packed Column	\$ -
Tray Column	\$ -
Storage Tanks	\$ -

Total Bare module Cost= \$ 4,062,057

Warning - extrapolation in cost estimate, refer to textbook for valid range

Warning - extrapolation in cost estimate, refer to textbook for valid range

Warning - extrapolation in cost estimate, refer to textbook for valid range

Electric Motors	Q (gal/min)	H (ft)	FT	Pb (hp)	Cbm
UP-EM-01	40.58	1357.6	1.00	33.52	5720
	0	0	0.00	0.00	0
	0	0	0.00	0.00	0
	0	0	0.00	0.00	0
	0	0	0.00	0.00	0

Centrifugal Pumps	Q (gal/min)	H (ft)	Ft	Fm	Cbm
UP-PM-01	40.58	1357.6	2.7	1	42068
	0	0	0	0	0
	0	0	0	0	0
	0	0	0	0	0
	0	0	0	0	0

External Gear Pumps	Q (gal/min)	Fm	Cbm
	0	0	0
	0	0	0
	0	0	0
	0	0	0
	0	0	0

Reciprocating Plunger Pumps	Q (gal/min)	H (ft)	Fm	Pb (hp)	Cbm
	0	0	0.00	0.00	0
	0	0	0.00	0.00	0
	0	0	0.00	0.00	0
	0	0	0.00	0.00	0
	0	0	0.00	0.00	0

Fans	Type of Fan	Q (ACFM)	CBM
		0	0
		0	0
		0	0
		0	0
		0	0

Centrifugal Blower	Qi (cuft/min)	Pi (lbf/in <sup>2</sup> )	Po (lbf/in <sup>2</sup> )	Pc	Cbm
	0	0	0	0.00	0
	0	0	0	0.00	0
	0	0	0	0.00	0
	0	0	0	0.00	0
	0	0	0	0.00	0

Rotary Straight-Lobe Blowers	Qj (ft <sup>3</sup> /min)	Pi (lbf/in <sup>2</sup> )	Po (lbf/in <sup>2</sup> )	Pc (hp)	Cbm
	0	0	0	0.00	0
	0	0	0	0.00	0
	0	0	0	0.00	0
	0	0	0	0.00	0
	0	0	0	0.00	0

Compressor	Type	Pc (hp)	CBM
UP-CP-01	Centrifugal Compressor	138	479984
UP-CP-02	Centrifugal Compressor	159.5	525826
UP-CP-03	Centrifugal Compressor	149.4	504596
UP-CP-04	Centrifugal Compressor	2.63	55437

Warning - extrapolation in cost estimate, refer to textbook for valid range

Warning - extrapolation in cost estimate, refer to textbook for valid range

Warning - extrapolation in cost estimate, refer to textbook for valid range

Warning - extrapolation in cost estimate, refer to textbook for valid range

	0	0	0
--	---	---	---

Shell and Tube Heat Exchangers	Heat Exchanger Design	Surface Area (ft <sup>2</sup> )	Pressure (psig)	CBM
UP-HX-01	Fixed Head	75.97	561.15	108504
UP-HX-02	Fixed Head	13.9326	555.35	148064
UP-CO-01	Fixed Head	21.6	30.16	45449
UP-CO-02	Fixed Head	40.9	150.22	39081
UP-CO-03	Fixed Head	31.7	549.55	46168

Warning - extrapolation in cost estimate, refer to textbook for valid range  
Warning - extrapolation in cost estimate, refer to textbook for valid range  
Warning - extrapolation in cost estimate, refer to textbook for valid range  
Warning - extrapolation in cost estimate, refer to textbook for valid range  
Warning - extrapolation in cost estimate, refer to textbook for valid range

Double Pipe Heat Exchanger	Surface Area (ft <sup>2</sup> )	Pressure (psig)	CBM
	0	0	0
	0	0	0
	0	0	0
	0	0	0
	0	0	0

Fired Heaters	Q (BTU/hr)	Pressure (psig)	Fm	Cbm
UP-BO-01	2.78E+07	565.5	1.4	1951834
UP-FH-01	7.07E+05	565.5	1.4	109325
	0.00E+00	0	0	0
	0.00E+00	0	0	0
	0.00E+00	0	0	0

Warning - extrapolation in cost estimate, refer to textbook for valid range

Pressure vessel	Type	Di	L	Pressure	Weight	Cbm
		0	0	0	0	0
		0	0	0	0	0
		0	0	0	0	0
		0	0	0	0	0
		0	0	0	0	0

Packed Column	Di (ft)	L (ft)	Pressure (psig)	Vp (ft <sup>3</sup> )	Cbm
	0	0	0	0	0
	0	0	0	0	0
	0	0	0	0	0
	0	0	0	0	0
	0	0	0	0	0

Tray Column	Di (ft)	L(ft)	Pressure (psig)	Nt	Ftt	Cbm
	0	0	0	0	0	0
	0	0	0	0	0	0
	0	0	0	0	0	0
	0	0	0	0	0	0
	0	0	0	0	0	0

Storage Tanks	V (gal)	Cbm
	0	0
	0	0
	0	0
	0	0
	0	0

## Electric Motors

S

FBM 3.3 CE = 600

Given Q, H,  $\rho$

Name	Q (gal/min)	H (ft)	$\rho$ (lb/gal)	$\eta_p$	PB (hp)	$\eta_m$	Pc (hp)
UP-EM-01	40.58	1357.6	8.21	0.41	33.52	0.89	37.68

[Summary page](#)

CB	FT	CP	CP	CBM
$\$ (CE=567)$	Table 22.22	$\$ (CE=567)$	$\$ (Given CE)$	$\$ (Given CE)$
1638	1.00	1638	1733	<b>5720</b>

### Centrifugal Pumps

[Summary page](#)

FBM = 3.3 CE = 600

Name	Q (gal/min)	H (ft)	S (gpm)(ft) <sup>1.5</sup>	CB \$ (CE=567)	FT Table 22.20	FM Table 22.21	CP \$ (CE=567)	CP \$ (Given CE)	CBM \$ (Given CE)
UP-PM-01	40.58	1357.6	1495	4462	2.7	1	12047	12748	42068
			0	0			0	0	0
			0	0			0	0	0
			0	0			0	0	0
			0	0			0	0	0

**Table 16.20** Typical Types of Radial Centrifugal Pumps and  $F_T$  Factors

No. of Stages	Shaft rpm	Case-Split Orientation	Flow Rate Range (gpm)	Pump Head Range(ft)	Maximum Motor Hp	Type Factor [ $F$ Eq. (16.15)]
1	3,600	VSC	50–900	50–400	75	1.00
1	1,800	VSC	50–3,500	50–200	200	1.50
1	3,600	HSC	100–1,500	100–450	150	1.70
1	1,800	HSC	250–5,000	50–500	250	2.00
2	3,600	HSC	50–1,100	300–1,100	250	2.70
2+	3,600	HSC	100–1,500	650–3,200	1,450	8.90

**Table 16.21** Materials of Construction Factors,  $F_M$ , for Centrifugal Pumps

Material of Construction	Material Factor [ $F_M$ , in Eq. (16.15)]
Cast iron	1.00
Ductile iron	1.15
Cast steel	1.35
Bronze	1.90
Stainless steel	2.00
Hastelloy C	2.95
Monel	3.30
Nickel	3.50
Titanium	9.70

**Compressors**

FBM = 2.15 CE = 600

Name	Compressor Type <i>(screw, centrifugal, reciprocating)</i>	Aspen Pc hp	Cb \$(CE=567)	FD <i>see below</i>	FM <i>see below</i>	Cp \$(CE=567)	Cp \$(Given CE)
UP-CP-01	Centrifugal Compressor	138	210970	1	1	210970	223248
UP-CP-02	Centrifugal Compressor	159.5	231119	1	1	231119	244570
UP-CP-03	Centrifugal Compressor	149.4	221788	1	1	221788	234696
UP-CP-04	Centrifugal Compressor	2.63	17405	1	1.4	24367	25785
			0			0	0

Possible FD values

Electric	1
Steam	1.15
Gas	1.25

Possible FM values

Cast iron	1
Carbon Steel	1
Stainless Steel	2.5
Nickel Alloy	5



[Summary page](#)

CBM

\$ (Given CE)

**479984** Warning - extrapolation in cost estimate, refer to textbook for valid range

**525826** Warning - extrapolation in cost estimate, refer to textbook for valid range

**504596** Warning - extrapolation in cost estimate, refer to textbook for valid range

**55437** Warning - extrapolation in cost estimate, refer to textbook for valid range

**0**

## Tube Heat Exchangers

[Summary page](#)

FBM = 3.17 CE = 600

Name	Heat Exchanger Design	Surface Area <i>ft</i> <sup>2</sup>	CB \$ (CE=567)	a <i>Table 22.25</i>	b <i>Table 22.25</i>	FM	Pressure <i>psig</i>	Fp
UP-HX-01	Fixed Head	75.97	10632	1.7	0.07	2.68094566	561.15	1.13483818
UP-HX-02	Fixed Head	13.9326	15866	1.55	0.05	2.45615316	555.35	1.13269332
UP-CO-01	Fixed Head	21.6	13549	0	0	1	30.16	1
UP-CO-02	Fixed Head	40.9	11522	0	0	1	150.22	1.01117583
UP-CO-03	Fixed Head	31.7	12174	0	0	1	549.55	1.13055988

**Table 16.25** Materials of Construction Factors,  $F_M$ , for Shell-and-Tube Heat Exchangers

Materials of Construction Shell/Tube	<i>a</i> in Eq. (16.44)	<i>b</i> in Eq. (16.44)
Carbon steel/carbon steel	0.00	0.00
Carbon steel/brass	1.08	0.05
Carbon steel/stainless steel	1.75	0.13
Carbon steel/Monel	2.1	0.13
Carbon steel/titanium	5.2	0.16
Carbon steel/Cr-Mo steel	1.55	0.05
Cr-Mo steel/Cr-Mo steel	1.70	0.07
Stainless steel/stainless steel	2.70	0.07
Monel/Monel	3.3	0.08
Titanium/titanium	9.6	0.06

**Tube L**

FL <i>See below</i>	Cp \$ (CE=567)	Cp \$(Given CE)	CBM \$ (Given CE)	
1	32346	34228	<b>108504</b>	Warning - extrapolation in cost estimate, refer to textbook for valid range
1	44139	46708	<b>148064</b>	Warning - extrapolation in cost estimate, refer to textbook for valid range
1	13549	14337	<b>45449</b>	Warning - extrapolation in cost estimate, refer to textbook for valid range
1	11650	12328	<b>39081</b>	Warning - extrapolation in cost estimate, refer to textbook for valid range
1	13763	14564	<b>46168</b>	Warning - extrapolation in cost estimate, refer to textbook for valid range

Length (ft)	$F_L$
8	1.25
12	1.12
16	1.05
20	1.00

**Tube Heat Exchangers**

[Summary page](#)

FBM = 3.17 CE = 600

Name	Heat Exchanger Design	Surface Area <i>ft</i> <sup>2</sup>	CB \$ (CE=567)	a <i>Table 22.25</i>	b <i>Table 22.25</i>	FM	Pressure <i>psig</i>	Fp
UP-CD-01	Fixed Head	710	14920	1.55	0.05	2.65296801	549.55	1.13055988
			0			0		1
			0			0		1
			0			0		1
			0			0		1

**Table 16.25** Materials of Construction Factors,  $F_M$ , for Shell-and-Tube Heat Exchangers

**Tube L**

Materials of Construction Shell/Tube	<i>a</i> in Eq. (16.44)	<i>b</i> in Eq. (16.44)
Carbon steel/carbon steel	0.00	0.00
Carbon steel/brass	1.08	0.05
Carbon steel/stainless steel	1.75	0.13
Carbon steel/Monel	2.1	0.13
Carbon steel/titanium	5.2	0.16
Carbon steel/Cr-Mo steel	1.55	0.05
Cr-Mo steel/Cr-Mo steel	1.70	0.07
Stainless steel/stainless steel	2.70	0.07
Monel/Monel	3.3	0.08
Titanium/titanium	9.6	0.06

2

FL <i>See below</i>	Cp \$(CE=567)	Cp \$(Given CE)	CBM \$(Given CE)
1	44749	47353	150110
	0	0	0
	0	0	0
	0	0	0
	0	0	0

Length (ft)	$F_L$
8	1.25
12	1.12
16	1.05
20	1.00

## Fired Heaters

[Summary page](#)

FBM =  
*see below*

2.19

CE = 600

Name	Q <i>BTU/hr</i>	P <i>psig</i>	CB <i>\$ (CE=567)</i>	FM <i>see below</i>	Fp	CP <i>\$ (CE=567)</i>	CP <i>\$ (Given CE)</i>	CBM <i>\$ (Given CE)</i>
UP-BO-01	2.78E+07	565.5	598941	1.4	1.00442682	842230	891249	1951834
UP-FH-01	7.07E+05	565.5	33547	1.4	1.00442682	47174	49920	109325
			0		1	0	0	0
			0		1	0	0	0
			0		1	0	0	0

### Possible FBM Values

2.19 shop fabricated  
1.86 field fabricated

### Possible FM Values

1.4 Cr-Mo alloy steel  
1.7 stainless steel

## Appendix E.2: Equipment Costing Haber Bosch

## Bare Module Cost Analysis Worksheet

### Instructions (Read Carefully Before Using!!!)

1. Input the CE cost index below that corresponds to the date when you want the cost estimate (e.g. a 2018 CE will provide 2018 costs for equipment) . The CE index will automatically update each page accordingly.
2. Select the link below for the appropriate unit operation. Links provided at the top of each worksheet will return back to this title page.
3. Enter all data into the yellow boxes ONLY. For a process involving multiple sizes of the same type unit operations, use a different line to input the specs (up to 5 provided)
4. The Bare Module Cost of the Unit Operation is calculated and shown in red.  
**Bare Module Cost**
5. If you are extrapolating the cost correlations, the spreadsheet will warn you. Consult the textbook for valid ranges of the equations, and use outside those ranges very carefully.
6. Below are the individual unit bare module costs and compiled tables of each type of unit operation, summarizing the different properties.
7. Total Bare Module Cost for all types of all equipment is also displayed below.

### All costing from:

#### Product and Process Design Principles

4th Edition

© Seider, Lewin, Seader, Widagdo, Gani, Ng, 2017

Worksheet prepared by Prof. Russell Dunn, Department of Chemical and Biomolecular Engineering, Vanderbilt University

Revised by Prof. Bruce Vrana, Department of Chemical and Biomolecular Engineering, University of Pennsylvania

CE Cost Index for this Estimate

600

Equipment	Total Cbm For each Unit Op
Electric Motors	\$ -
Centrifugal Pumps	\$ -
External Gear Pumps	\$ -
Reciprocating Plunger Pumps	\$ -
Fans	\$ -
Centrifugal (turbo) Blower	\$ -
Rotary Straight Lobe Blower	\$ -
Compressors	\$ 3,051,269
Shell and Tube Heat Exchanger	\$ 506,584
Double Pipe Heat Exchanger	\$ -
Fired Heaters	\$ -
Pressure Vessel	\$ 463,983
Packed Column	\$ -
Tray Column	\$ -
Storage Tanks	\$ -

Total Bare module Cost= \$ 4,021,836

Warning - extrapolation in cost estimate, refer to textbook for valid range

Warning - extrapolation in cost estimate, refer to textbook for valid range

Warning - extrapolation in cost estimate, refer to textbook for valid range

Electric Motors	Q (gal/min)	H (ft)	FT	Pb (hp)	Cbm
	0	0	0.00	0.00	0
	0	0	0.00	0.00	0
	0	0	0.00	0.00	0
	0	0	0.00	0.00	0
	0	0	0.00	0.00	0

Centrifugal Pumps	Q (gal/min)	H (ft)	Ft	Fm	Cbm
	0	0	0	0	0
	0	0	0	0	0
	0	0	0	0	0
	0	0	0	0	0
	0	0	0	0	0

External Gear Pumps	Q (gal/min)	Fm	Cbm
	0	0	0
	0	0	0
	0	0	0
	0	0	0

Reciprocating Plunger Pumps	Q (gal/min)	H (ft)	Fm	Pb (hp)	Cbm
	0	0	0.00	0.00	0
	0	0	0.00	0.00	0
	0	0	0.00	0.00	0
	0	0	0.00	0.00	0
	0	0	0.00	0.00	0

Fans	Type of Fan	Q (ACFM)	CBM
		0	0
		0	0
		0	0
		0	0
		0	0

Centrifugal Blower	Qi (cuft/min)	Pi (lbf/in <sup>2</sup> )	Po (lbf/in <sup>2</sup> )	Pc	Cbm
	0	0	0	0.00	0
	0	0	0	0.00	0
	0	0	0	0.00	0
	0	0	0	0.00	0
	0	0	0	0.00	0

Rotary Straight-Lobe Blowers	Qi (ft <sup>3</sup> /min)	Pi (lbf/in <sup>2</sup> )	Po (lbf/in <sup>2</sup> )	Pc (hp)	Cbm
	0	0	0	0.00	0
	0	0	0	0.00	0
	0	0	0	0.00	0
	0	0	0	0.00	0
	0	0	0	0.00	0

Compressor	Type	Pc (hp)	CBM
		0	0
HB-CP-01	Centrifugal Compressor	1	30146
HB-CP-02	Centrifugal Compressor	1500	3021123
		0	0

Warning - extrapolation in cost estimate, refer to textbook for valid range



	0	0	0
--	---	---	---

Shell and Tube Heat Exchangers	Heat Exchanger Design	Surface Area (ft <sup>2</sup> )	Pressure (psig)	CBM
HB-HXA-02	Fixed Head	79	490	105901
HB-HXA-01	Fixed Head	24	490	127161
		0	0	0
HB-HXA-04	Fixed Head	25	507.5	120435
HB-HXA-03	Fixed Head	25	1160	153087

Warning - extrapolation in cost estimate, refer to textbook for valid range  
Warning - extrapolation in cost estimate, refer to textbook for valid range

Double Pipe Heat Exchanger	Surface Area (ft <sup>2</sup> )	Pressure (psig)	CBM
	0	0	0
	0	0	0
	0	0	0
	0	0	0
	0	0	0

Fired Heaters	Q (BTU/hr)	Pressure (psig)	Fm	Cbm
	0.00E+00	0	0	0
	0.00E+00	0	0	0
	0.00E+00	0	0	0
	0.00E+00	0	0	0
	0.00E+00	0	0	0

Pressure vessel	Type	Di	L	Pressure	Weight	Cbm
HB-S-01	Vertical	0.87	10.37	565.5	479.7687074	66024
HB-S-02	Vertical	0.78	12.16	145	328.3323075	57136
		0	0	0	0	0
Haber Bosch Reactor	Vertical	2.87	14.35	1160	11269.89793	340823
		0	0	0	0	0

Warning - extrapolation in cost estimate, refer to textbook for valid range  
Warning - extrapolation in cost estimate, refer to textbook for valid range

Packed Column	Di (ft)	L (ft)	Pressure (psig)	Vp (ft <sup>3</sup> )	Cbm
	0	0	0	0	0
	0	0	0	0	0
	0	0	0	0	0
	0	0	0	0	0
	0	0	0	0	0

Tray Column	Di (ft)	L(ft)	Pressure (psig)	Nt	Ftt	Cbm
	0	0	0	0	0	0
	0	0	0	0	0	0
	0	0	0	0	0	0
	0	0	0	0	0	0
	0	0	0	0	0	0

Storage Tanks	V (gal)	Cbm
	0	0
	0	0
	0	0
	0	0
	0	0

**Compressors**

FBM = 2.15 CE = 600

Name	Compressor Type <i>(screw, centrifugal, reciprocating)</i>	Pc hp	Cb \$(CE=567)	FD <i>see below</i>	FM <i>see below</i>	Cp \$(CE=567)	Cp \$(Given CE)
			0	1	1.4	0	0
HB-CP-01	Centrifugal Compressor	1	9464	1	1.4	13250	14021
HB-CP-02	Centrifugal Compressor	1500	948492	1	1.4	1327889	1405174
			0			0	0
			0			0	0

Possible FD values

Electric	1
Steam	1.15
Gas	1.25

Possible FM values

Cast iron	1
Carbon Steel	1
Stainless Steel	2.5
Nickel Alloy	5

[Summary page](#)

CBM  
\$ (Given CE)

0

**30146** Warning - extrapolation in cost estimate, refer to textbook for valid range

**3021123**

0

0

## Tube Heat Exchangers

[Summary page](#)

FBM = 3.17 CE = 600

Name	Heat Exchanger Design	Surface Area <i>ft</i> <sup>2</sup>	CB \$ (CE=567)	a <i>Table 22.25</i>	b <i>Table 22.25</i>	FM	Pressure <i>psig</i>	Fp
HB-HXA-02	Fixed Head	79	10605	1.7	0.07	2.68363483	490	1.109317
HB-HXA-01	Fixed Head	24	13118	1.7	0.07	2.60492959	490	1.109317
			0			0		1
HB-HXA-04	Fixed Head	25	12963	1.55	0.05	2.48303299	507.5	1.11543456
HB-HXA-03	Fixed Head	25	12963	1.55	0.05	2.48303299	1160	1.417852

**Table 16.25** Materials of Construction Factors,  $F_M$ , for Shell-and-Tube Heat Exchangers

Materials of Construction Shell/Tube	$a$ in Eq. (16.44)	$b$ in Eq. (16.44)
Carbon steel/carbon steel	0.00	0.00
Carbon steel/brass	1.08	0.05
Carbon steel/stainless steel	1.75	0.13
Carbon steel/Monel	2.1	0.13
Carbon steel/titanium	5.2	0.16
Carbon steel/Cr-Mo steel	1.55	0.05
Cr-Mo steel/Cr-Mo steel	1.70	0.07
Stainless steel/stainless steel	2.70	0.07
Monel/Monel	3.3	0.08
Titanium/titanium	9.6	0.06

**Tube L**

2

FL <i>See below</i>	Cp \$ (CE=567)	Cp \$(Given CE)	CBM \$ (Given CE)	
1	31570	33407	<b>105901</b>	Warning - extrapolation in cost estimate, refer to textbook for valid range
1	37908	40114	<b>127161</b>	Warning - extrapolation in cost estimate, refer to textbook for valid range
1	0	0	<b>0</b>	
1	35902	37992	<b>120435</b>	Warning - extrapolation in cost estimate, refer to textbook for valid range
1	45636	48292	<b>153087</b>	Warning - extrapolation in cost estimate, refer to textbook for valid range

Length (ft)	$F_L$
8	1.25
12	1.12
16	1.05
20	1.00

**Pressure Vessels**

FBM =

4.16

CE =

600

Name	Type	Di <i>ft</i>	L <i>ft</i>	Pressure <i>psig</i>	Pd <i>psig</i>	E
HB-S-01	Vertical	0.87	10.37	565.5	649	1
HB-S-02	Vertical	0.78	12.16	145	182	1
					0	
Haber Bosch Reactor	Vertical	2.87	14.35	1160	1272	1
					0	

Note: see text for vacuum vessels

Note: if carbon steel, S = 13750

For 304 Stainless, S = 11200

Potential Values for S (low alloy steel):

Temperature (°F)	Maximum Allowable Stress (psi)
-20 to 650	15,000
700	15,000
750	15,000
800	14,750
850	14,200
900	13,100

**Table 16.26** M  
Vessels

Material of Con
Carbon steel
Low-alloy steel
Stainless steel 3
Stainless steel 3
Carpenter 20CE
Nickel-200
Monel-400
Inconel-600
Incoloy-825
Titanium

[Summary page](#)

S <i>psi (see below)</i>	tp <i>ft</i>	Wind/Earthquake? <i>Include=Y</i>	tw <i>ft</i>	taverage <i>ft</i>	Corrosion tc <i>inch</i>	ts <i>inch</i>	tsrounded <i>inch</i>
15000	0.01932	N	0.00000	0.01932	0.125	0.35683	0.37500
15000	0.00477	N	0.00000	0.00477	0.125	0.18222	0.25000
	0.00000		0.00000	0.00000	0.125	0.12500	0.25000
15000	0.12824	N	0.00000	0.12824	0.125	1.66385	1.75000
	0.00000		0.00000	0.00000	0.125	0.12500	0.25000

Materials-of-Construction Factors,  $F_M$ , for Pressure

Instruction	Material Factor [ $F_M$ in Eq. (16.52)]
	1.0
	1.2
104	1.7
116	2.1
3-3	3.2
	5.4
	3.6
	3.9
	3.7
	7.7

tsrounded ft	Density lb/ft <sup>3</sup>	Weight lb	Cv \$(CE=567)	Cpl \$(CE=567)	Fm Table 22.26	Cp \$(CE=567)	CP \$(Given CE)	Cbm \$(Given CE)	
0.0313	490	480	9333	1932	1.4	14998	15871	66024	Warning - extrapolation in
0.0208	490	328	7846	1994	1.4	12979	13735	57136	Warning - extrapolation in
0.0208	490	0	0	0	1.4	0	0	0	
0.1458	490	11270	51105	5875	1.4	77423	81929	340823	
0.0208	490	0	0	0	1	0	0	0	