



1 **Abstract**

2 This paper considers a process through which the wind costs the agricultural industry hundreds of  
3 millions of pounds per year - crop lodging. Lodging is the displacement of crops by wind (and rain)  
4 that can result in either stem breakage or uprooting. In particular this paper builds upon recent work  
5 to develop a generalised model of the lodging process and presents the results of several  
6 experimental campaigns to identify dynamic and aerodynamic parameters that are required as  
7 inputs to the model in order to estimate lodging wind speeds. These experiments were carried out at  
8 various sites in the UK and the Republic of Ireland to determine the natural frequencies, damping  
9 ratios and drag areas of maize, oats and oil seed rape. The experimental methodology, which was  
10 based upon the tracking of plant displacements, was shown to be robust, and consistent values of  
11 the parameters were obtained, albeit with much larger experimental uncertainties than would  
12 normally be expected in wind engineering applications. The values of these parameters were also  
13 consistent with those of earlier measurements for wheat. The generalised model was then used to  
14 determine lodging wind speeds for the three crops, and an assessment was made of the effect of  
15 experimental uncertainties in dynamic, aerodynamic and agronomic variables on the predicted  
16 values. In broad terms the generalised lodging model was shown to well describe the crop behaviour  
17 for isolated crops, and it was shown that it could be used in a simplified form for interlocked crop  
18 canopies. It was also shown that uncertainties in the aerodynamic parameters resulted in  
19 uncertainties of around an order of magnitude in lodging risk, whilst typical variations between  
20 plants in some crop parameters (notably stem strength and radius) could result in lodging risk  
21 uncertainties of two orders of magnitude.

1 **1. Introduction**

2 Lodging is the permanent displacement of crop stems from their (original) vertical position, due to a  
3 combination of high winds and heavy rain, and can result in significant crop yield reductions (Berry  
4 et al., 2000). The phenomenon affects a wide range of crops – wheat, barley, rice, oats, maize,  
5 oilseed rape etc., and is a problem of significant concern in many countries around the world. There  
6 are two basic failure modes – stem lodging (failure at some point of the stem above the ground) and  
7 root lodging (failure at the root/soil interface). These two lodging mechanisms are illustrated in  
8 Figure 1 for the three crops with which this paper is mainly concerned - oats (*Avena sativa*), maize  
9 (*Zea mays*) and oilseed rape (OSR, *Brassica napus*). Whilst the primary loading on the plants that  
10 causes lodging to occur is the wind, heavy rainfall can affect the soil conditions and increase the  
11 likelihood of root lodging.

12 The costs of lodging can be considerable. For example, in the UK it is estimated that as a direct  
13 result of lodging in OSR, yield is reduced by ~46% resulting in losses of ~£120 million per year  
14 (Kendall et al., 2017). Stem lodging of maize accounts for worldwide yield losses of up to 20% (Flint-  
15 Garcia et al., 2003), whilst a further 20% reduction in yield can be attributed to root lodging. The  
16 costs incurred by lodging arise as a direct consequence of yield loss and indirectly from reduced  
17 grain quality, increased drying, increased susceptibility to plant pathogens and pests, and the  
18 increased difficulties associated with harvesting (Crook and Ennos, 1993; Berry et al 2003, Berry et  
19 al., 2004, Berry and Spink 2012, Sterling et al 2018). Furthermore, the effects of crop lodging can  
20 directly and indirectly impact on a number of the United Nations Sustainable Development Goals  
21 (United Nations 2018), in particular: no poverty, zero hunger, good health and well-being, and  
22 responsible consumption and production. Some researchers have suggested that climate change  
23 may exacerbate the issue in certain parts of the world (Challinor et al., 2010; Mohammadi et al,  
24 2020), particularly through heavier rain fall increasing the susceptibility of crops to root lodging.

25 Whilst much of the basic work in this area has been carried out by agronomists and plant scientists,  
26 some experimental work looking at tree behaviour in high winds from an engineering perspective

1 has been carried out both by one of the author and his co-workers (Baker and Bell, 1992;  
2 Roodbaraky et al, 1994) for urban trees, and by Boldes and his colleagues in Argentina (Boldes et al  
3 2001, 2002, 2003) for forest trees and shelterbelts. Computational studies of flows within canopies  
4 are also reported by Hiraoka (1993) and Hiraoka and Ohashi (2000). More recently Rhee and  
5 Lombardo (2018) have begun to consider tree and crop failure as indicators of the strength of  
6 tornadoes.

7 Over the last two decades, research has been carried out by some of the authors to understand the  
8 mechanisms of lodging and, in doing so, to enable the best application of remedial  
9 measures/interventional (management) approaches. As a result of this work, a mechanical model of  
10 the lodging process was developed in which a single plant is represented as a damped harmonic  
11 oscillator (Baker, 1995; Baker et al, 1998; Berry et al, 2006). Applying a representative wind gust, it  
12 was possible in this model to calculate the wind-induced bending moment at the base of the plant,  
13 which was compared with the stem failure moment and the failure moment of the root plate. An  
14 improved model was subsequently developed (Baker et al., 2014) which was generalised for any  
15 plant type and enabled canopy interactions with the environment to be taken into account. The  
16 model allows for consideration of both individual plants and crops with interlocked canopies, such as  
17 OSR. In addition, a more complex, stochastic, representation of the wind was used. For crops that  
18 oscillate as isolated plants (e.g., wheat), the generalised model reduces to that described in Baker  
19 (1995). This model is being used in a number of linked multi-disciplinary investigations to study the  
20 lodging of a variety of crops around the world, based on a range of aerodynamic, climate and  
21 agronomic studies, with a view to incorporating of the results into a GIS framework that can be used  
22 to identify crops at risk of lodging, or, conversely, the development of more risk resistant crops  
23 (Berry et al, 2019).

24 In order to apply the new model, a variety of aerodynamic and plant related parameters are  
25 required. The focus of the current paper is to present a viable methodology for determining these  
26 parameters using *in-situ* measurements of wind over the crop canopy and the corresponding wind-

1 induced displacement of the crop. Section 2 of the paper briefly outlines the generalised lodging  
2 model and how it is parameterised. Section 3 outlines the methodology of the field experiments  
3 undertaken on oats, maize and OSR. Experimental results are set out and discussed in section 4 and  
4 some concluding remarks are made in section 5.

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Figure 1 Images of a) stem lodging in oats (photo credit Teagasc), (b) root lodging in maize (photo credit CIMMYT) and (c) stem lodging in OSR (photo credit ADAS UK)

## 1 2. The Generalized Lodging Model

2 As noted above, the authors have developed a model of the lodging process that can predict, for  
3 specific wind and rain conditions, the probability of root and stem lodging. This will not be described  
4 in detail here, and the reader is referred to Baker et al (2014) for further details. Here it is sufficient  
5 to say that a mechanical analysis of individual plants or an interlocked canopy of multiple plants,  
6 assuming the crop can be represented by point masses at the top of weightless, elastic stems, results  
7 in a model of plant or canopy dynamics that can be represented by a simple two degree of freedom  
8 oscillator. This allows the calculation of the crop displacements and bending moments under the  
9 action of a fluctuating wind load at the canopy top. This is solved using the normal wind engineering  
10 frequency domain approach that allows the displacement and stem bending moment spectra to be  
11 determined. The one-second peak values of this bending moment at different points along the plant  
12 stem are then calculated from these spectra, and compared with the stem failure moment to check  
13 for the occurrence of stem lodging, while the minute averaged values are compared with the root  
14 plate failure moment, to check for the occurrence of root lodging. The output from the model can be  
15 succinctly expressed in the form shown in Figure 2, where the regions of root and stem lodging are  
16 shown in terms of daily rainfall ( $i$ ) and hourly mean wind speed ( $\bar{U}$ ) at the canopy top. The major  
17 boundary between the regions has a simple parabolic form. In Figure 2,  $\bar{U}_S$  is the mean wind velocity  
18 below which no lodging occurs;  $\bar{U}_{LSB}$  is the mean wind velocity where stem breakage occurs at the  
19 base of the stem (note this is a vertical line and thus the value is not dependent on rainfall);  $\bar{U}_{LR}$  is  
20 the mean wind velocity which results in root lodging in all circumstances; and  $i_o$  is the daily rainfall  
21 above which root lodging always occurs, even at very low wind speeds. These parameters are  
22 themselves somewhat complex algebraic functions of a range of measurable parameters. For  
23 example the stem lodging velocity at the base of the stem ( $\bar{U}_{LS} = \bar{U}_{LSB}$ ) is given by

$$24 \bar{U}_{LS} = \left( \frac{n(2\pi f_n)^2(X/g)(\sigma\pi a^3/4)(1-((a-t)/a)^4)}{(1+(2\pi f_n)^2(X/g))(0.5\rho AC_F X) \left(1+6.86I_u \left(1+0.087\left(\frac{\pi}{4\theta}\right)^{0.5}\right)\right)} \right)^{0.5} \quad (1)$$

25 The parameters in this equation are in one of three categories.

- 1 • Crop geometric and material parameters – the number of shoots per plant  $n$ , the centre of  
2 gravity height  $X$ , the stem failure strength at the base  $\sigma$ , the stem radius at the base  $a$ , and  
3 the stem wall thickness at the base  $t$ ;
- 4 • wind turbulence characteristics at the top of the canopy, in particular the along wind  
5 turbulence intensity  $I_u$ ;
- 6 • plant dynamic and aerodynamic characteristics – in particular plant or canopy natural  
7 frequency  $f_n$ , and damping ratio  $\theta$  and drag area  $AC_F$  per plant.

8 Also note that  $\rho$  is the density of air, and  $g$  is the acceleration due to gravity. Similar expressions can  
9 also be developed for stem lodging velocities at an arbitrary point up the stem away from the base,  
10 and for root lodging velocities. The latter will of course also be a function of various root and soil  
11 characteristics. Further details are given in Baker et al (2014).

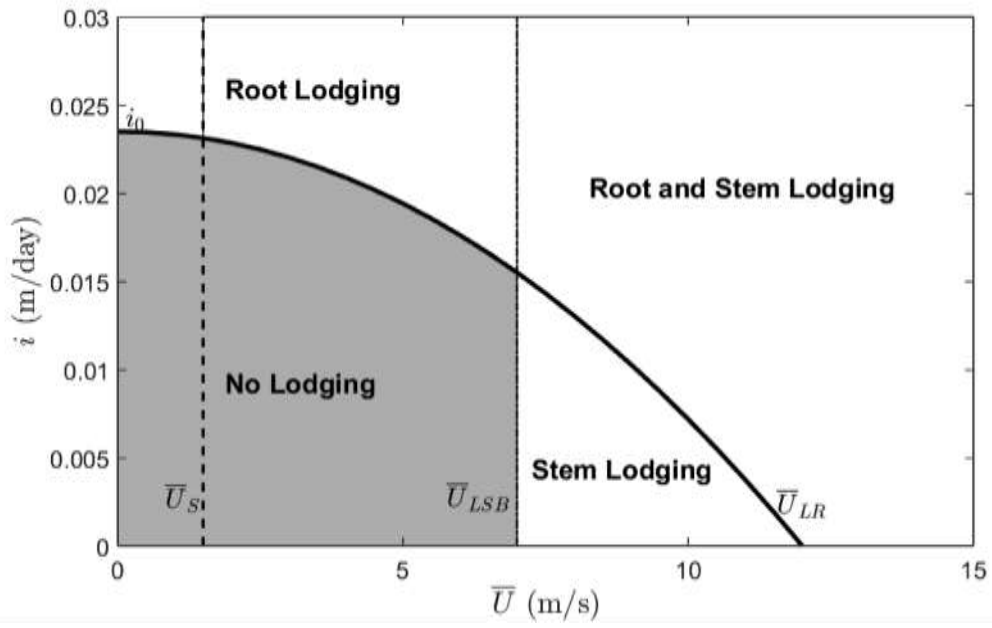
12 The crop geometric and material properties and root characteristics required for the model were  
13 measured by using a range of agronomic methods and are reported elsewhere (Berry et al, 2000).  
14 This paper is concerned with the determination of the wind turbulence characteristics and the plant  
15 dynamic and aerodynamic characteristics for three crop types –maize, oats and OSR. These three  
16 crops represent different degrees of plant interlocking – a maize crop consists of essentially  
17 independent plants; an oat crop in the later growth stages can be regarded as mildly interlocking,  
18 and an OSR crop as very interlocked.

19 The model of course has limitations – the description of the crop dynamic behaviour is very  
20 idealised, and does not allow for major variability in the dynamic parameters during the root lodging  
21 process, where failure is likely to be progressive. It should primarily be regarded as a framework for  
22 considering experimental results, and as a method for identifying the sensitivity of lodging to  
23 different parameters.

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**Figure 2** The parabolic lodging relationship (Baker et al., 2014).

### 1 **3. Aerodynamic Experiments**

#### 2 **3.1 Experimental set-up**

3 The experiments reported below were undertaken at various farm locations in the UK and the  
4 Republic of Ireland (Table 1). The primary objective of these experiments was to observe the effects  
5 of wind and rain on the motion of three specific crops, namely oats, maize and OSR, selected  
6 because of differences in their canopy morphologies which leads to variations in canopy  
7 interlocking. Wind conditions and plant displacement were simultaneously measured. The  
8 experiments were conducted after panicle emergence for oats, at cob maturity for maize and  
9 flowering stage for OSR, which corresponded with the periods when the plants were most  
10 vulnerable to lodging. The equipment used in all three experiments is illustrated in Figure 3 and  
11 consists of two ultrasonic anemometers (Gill Instruments R3-100, 100Hz research  
12 anemometers), two high definition CCTV cameras (Lorex, LW2770 series) operating at a frame  
13 capture rate of 30 frames per second, and a rain gauge (ThiesClima precipitation sensor). The  
14 ultrasonic anemometers measured all three components of velocity. For each dataset the raw values  
15 were transformed to give horizontal velocities in the average flow direction,  $u_x$ : horizontal velocities  
16 normal to the average flow direction  $u_y$ ; and vertical velocities,  $u_z$ . Note that one anemometer was  
17 positioned with a horizontal axis, to be as close as possible to the canopy top. To measure crop  
18 movement, one camera was set up to capture crop displacement in the East-West plane, whilst the  
19 other recorded displacement in the North-South plane. A 12V 65Ah deep cycle lead acid battery was  
20 used to power the sensors and camera. Target plants were selected, based on visual similarity to  
21 average plant properties (e.g. height, morphological characteristics such as number of cobs for  
22 maize). Visible aerial parts of the target plant were painted red, to enable detection and tracking of  
23 plant deflections by a bespoke pixel tracking code written in MATLAB (further details provided in the  
24 Appendix)). This power source and the associated data logging equipment were stored in a  
25 watertight box, to prevent water ingress into components. Figure 3 shows the equipment

- 1 configuration in the field for the three crops and highlights the challenges that exist for some crops,
- 2 most notably maize, where the height of the crop can present practical challenges.

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**Table 1** Locations and dates of the lodging experiments

Crop	Crop height (m)	Farm	Location	Coordinates	Elevation above sea level (m)	Experiment dates
Maize	2.5	ADAS Gleadthorpe	Mansfield, Nottingham, UK	53.22N, 1.11W	49.0	28/09/17–02/10/17
Oats	1.0	Teagasc, Carlow	Carlow, Republic of Ireland	52.86N, 6.94E	54.0	31/05/17–15/06/17 29/05/18 – 30/06/18
OSR	1.6	ADAS Terrington	Terrington, King's Lyn, Norfolk, UK	52.77N, 0.32W	4.0	16/05/18–24/05/18

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(a) Maize



(b) Oats



(c) OSR

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**Figure 3** Equipment set up in the field.

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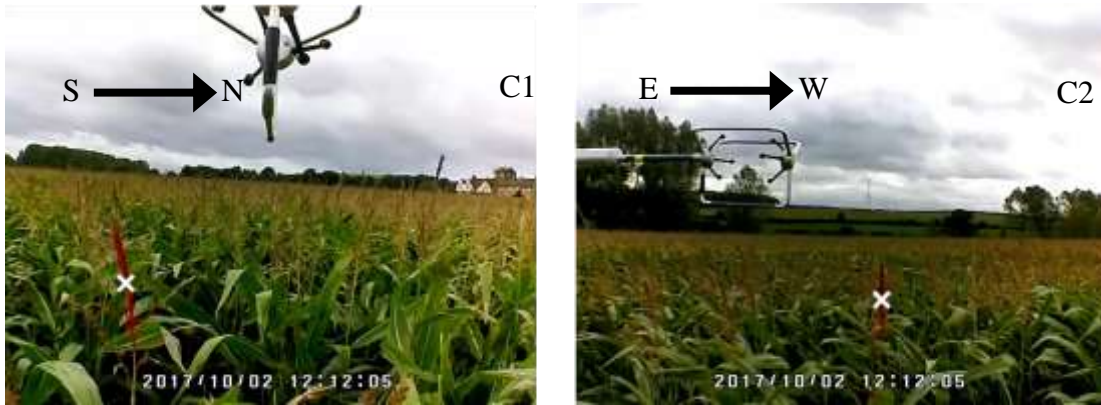
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### 1 **3.2 Tracking crop deflections in MATLAB**

2 Work by Py et al (2006) has demonstrated the utility of video tracking methods to monitor the  
3 oscillatory motions of plants and it was shown that compared to accelerometer based techniques,  
4 video-based methods allowed for precise determination of the zero displacement position of a plant  
5 and since these methods do not require sensors affixed to the plants, they do not add mass and alter  
6 the dynamic response characteristics of the plant. The current work differs somewhat from Py et al  
7 (2006) which used video tracking to study the global motion of the crop canopy in the form of  
8 Honami waves due to the downward transfer of momentum from coherent structures in the canopy  
9 mixing layer. Here, a two-camera configuration allows oscillations of individual marked plants to be  
10 captured in the wider horizontal field of view of each camera. The cameras have been calibrated  
11 using the MATLAB Camera Calibrator application to determine camera intrinsic parameters including  
12 lens distortion. From these observations, the dynamic response spectra of the plants and their  
13 corresponding aerodynamic characteristics were obtained.

14 A bespoke tracking program was developed in MATLAB to read the imported video files and  
15 detect red pixels in the video frames. Figure 4 illustrates a typical video image where the target  
16 plant (painted red) is highlighted by a white cross. As the tracking program progresses through the  
17 individual frames of the video file, a two dimensional array of centroid coordinates is created –  
18 expressed in Figure 5 as a pixel displacement time history. The Appendix gives more detail of the  
19 method that was used.

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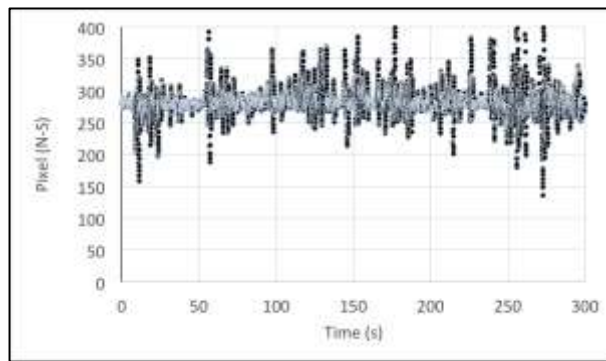
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**Figure 4** Centroid tracking of maize tassel in a single video frame for each camera, C1 and C2.

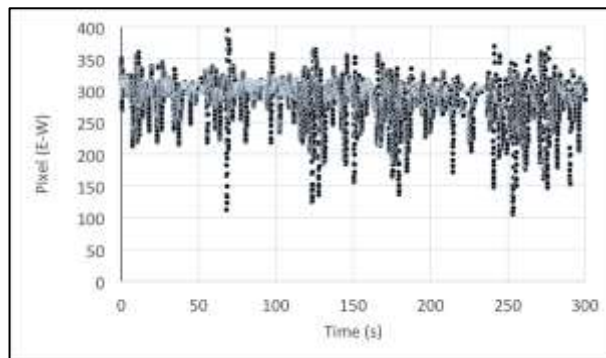
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**Figure 5** Example of oats pixel displacement time histories (a) Camera 1 (b) Camera 2

## 1 4. Results and Discussion

### 2 4.1 Canopy top flow parameters

3 In this section and subsequent sections relevant parameters have been averaged over 20, 10 minute,  
4 datasets for oats, 17 for maize and 18 for OSR. Table 2 shows average values across all the datasets  
5 at crop height of  $\sigma_i/u_*$  where  $\sigma_i$  is the standard deviation of the velocity component  $i$  and  $u_*$  is the  
6 friction velocity given by  $\sqrt{u_x u_z}$ ;  $I_i$ , the turbulence intensity of the velocity component  $i$  ( $\sigma_i/\bar{U}$ ); and  
7  $L_i/h$ , the integral length scales of the velocity component  $i$  normalised by crop height  $h$ . The latter is  
8 obtained by two methods – the integration of the area under the velocity component  
9 autocorrelation curve for all components (to the point of the first zero crossing), and a von Karman  
10 fit to the velocity power spectrum for the  $u$  component only. Standard deviations of  $\sigma_i/u_*$  and  $I_i$  are  
11 also given, which allows the variability between datasets to be appreciated. Ranges of experimental  
12 data from a number of other sources are also given. In general the turbulence parameters were  
13 found to be in good agreement with those in the literature, corresponding to near-neutral  
14 stratification above a wheat canopy (Finnigan, 2000 and Sterling et al., 2003). The turbulence  
15 intensity over the interlocked rape crop is lower than over the other crops, and the longitudinal  
16 length scales are somewhat larger. The high values of the components of turbulence intensity just  
17 above the canopy are worthy of note, being very much higher than over simple flat terrain (which  
18 one would expect to be around 0.2 to 0.3), which again reflects the values found in previous  
19 research. The length scales estimated from a spectral fit are somewhat below the equivalent  
20 autocorrelation values. The autocorrelation method tends to over-predict the length scales due to  
21 the uncertainty associated with the precise position of the zero crossing value.

22 The wind power spectra,  $S_i$ , for each of the three crops, normalized by the variance,  $\sigma_i^2$ , are  
23 illustrated in Figure 6. The slope of the  $u$  and  $v$  spectra are consistent with Kolmogorov's -5/3 power  
24 law in all three crops, implying that the turbulent energy cascade over the crop canopy exists in the  
25 inertial subrange, where the flow can be considered locally isotropic (Katul et al. 1997). These

- 1 spectra above the crops are similar to those measured by other authors in the past such as those
- 2 reported in Finnigan (2000).
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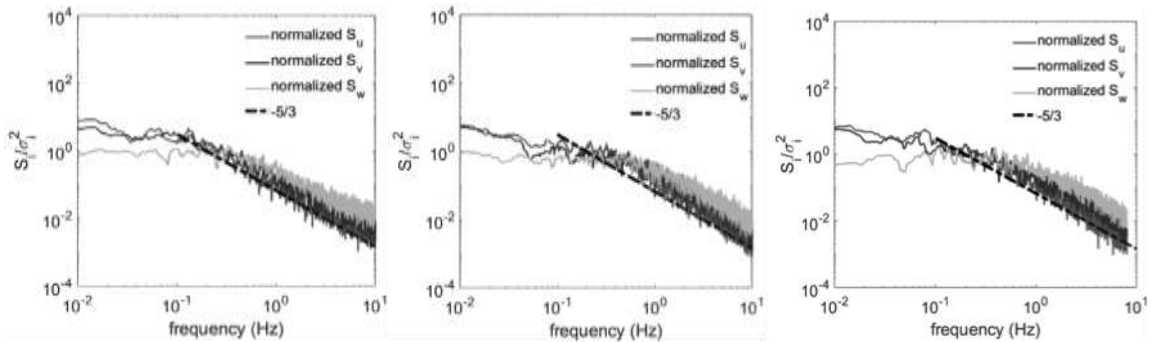
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**Table 2: Values of wind turbulence statistics for oats, maize and OSR**

(standard deviation of values from the range of datasets given in brackets; for the length scales, the normal type are values obtained from velocity autocorrelations, and the italics from a spectral fit using the von Karman form)

	Maize (h=2.5 m)	Oats (h=1.0 m)	OSR (h=1.6 m)	Panofsky and Dutton (1984)	Finnigan (2000) Wheat	Sterling et al (2003) Wheat
$\sigma_u/u_*$	2.04 (0.24)	2.33 (0.50)	2.20 (0.08)	2.39	1.8 – 3.0	2.11– 2.12
$\sigma_v/u_*$	1.85 (0.17)	1.99 (0.36)	1.78 (0.09)	1.92	-	-
$\sigma_w/u_*$	1.19 (0.07)	1.29 (0.12)	1.13 (0.03)	1.25	1.0 – 1.3	1.04 – 1.10
$I_u$	0.59 (0.04)	0.62 (0.02)	0.46 (0.03)	-	0.4 – 0.6	0.48 – 0.74
$I_v$	0.54 (0.08)	0.54 (0.04)	0.37 (0.02)	-	0.4 – 0.6	0.44 – 0.61
$I_w$	0.35 (0.05)	0.34 (0.005)	0.23 (0.01)	-	-	0.25 – 0.36
$L_u/h$	3.83	2.03	5.87	-	-	3.5 – 6.7
	<i>1.20</i>	<i>0.87</i>	<i>1.83</i>	-	-	
$L_v/h$	2.99	2.17	2.58	-	-	1.6-3.7
$L_w/h$	0.25	0.28	0.48	-	-	0.2 – 0.3

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(a) Maize

(b) Oats

(c) OSR

**Figure 6** Wind velocity component power spectra at crop height.

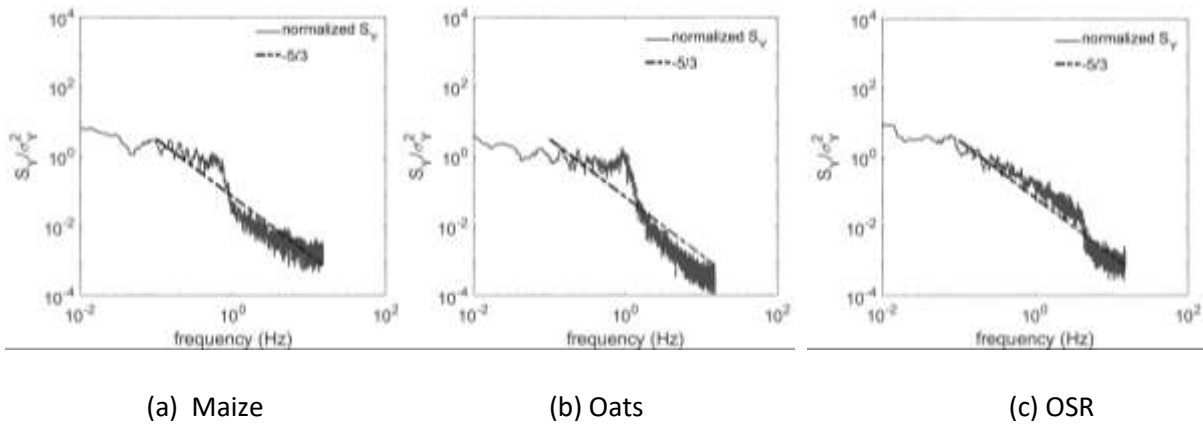
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## 1 **4.2 Natural frequencies**

2 The displacement spectrum describes the dynamic response of a plant in the frequency domain and  
3 identifies the energy associated with plant oscillations at different frequencies. Examples of the  
4 along-wind displacement spectra over a 10-minute interval are shown in Figures 7(a) to 7(c) for  
5 target maize, oats and OSR plants. Similar to the velocity power spectra, the displacement spectra  
6 have been normalized using the variance. The fundamental natural frequency,  $f_n$ , of each species  
7 can be determined from the peak of the corresponding displacement spectra, which represents the  
8 first mode of vibration; average values for oats and maize are 1.1Hz and 0.7Hz respectively. For  
9 these crops, the natural frequency of plant oscillations fall within the inertial subrange,  
10 consequently, it is expected that turbulent eddies in this range dominate the lodging process.  
11 However, for the OSR data (Figure 7c) there is less evidence for a peak, although one can perhaps be  
12 discerned at around 2 to 3Hz. This difference in behaviour for OSR will be discussed below. The  
13 mean and the standard deviations (SDs) of the natural frequency data obtained from the power  
14 spectra are shown in Table 3, together with the value for wheat from Baker et al (2014) and Berry et  
15 al (2003). In wind engineering terms the spread of natural frequencies seems high. However such  
16 variability is a feature of biological systems, and similar spreads of data will be observed in the other  
17 parameters that are considered in this paper.

18 Natural frequency may also be estimated by manually displacing a single shoot during still, dry  
19 weather conditions and timing the corresponding oscillations once released. This method is  
20 described in full by Berry et al. (2000) but essentially requires a plant to be isolated from its  
21 neighbours and the aforementioned process repeated around 80 times and the means and standard  
22 deviations of the frequency calculated. It only of course gives the primary natural frequency. This  
23 method is not ideal for two reasons. Firstly, it can potentially damage an area of crops during the  
24 isolation process and secondly, for an interlocked (or heavily damped) plant, it can be impossible to  
25 perform. Table 3, summarises these results and compares them with those obtained from the  
26 spectral fit. For maize the spectral estimates are less than the agronomic measurements, and the

1 standard deviation bands of the two methods do not overlap. For oats, the measured frequencies  
 2 are similar to those for wheat reported in Sterling et al (2003), and the spectral estimates are  
 3 somewhat higher than the agronomic measurements and again the standard deviations do not  
 4 overlap. For OSR the spectral measurements are significantly higher than the agronomic  
 5 measurements. The authors are of the view that in crops with significant canopy interlocking and  
 6 more pronounced damping, the spectral method is a more appropriate way of determining the  
 7 natural frequency of plants, as canopy damping may lead to rapidly decaying oscillations that are  
 8 difficult to observe.



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11 (a) Maize (b) Oats (c) OSR  
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13 **Figure 7** Typical streamwise displacement spectra

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15 **Table 3** Natural frequencies determined from displacement spectra and oscillating plants

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	Spectral estimate		Oscillating plants	
	Mean Hz	SD Hz	Mean Hz	SD Hz
Maize	0.69	0.12	1.0	0.14
Oats	1.1	0.12	0.8	0.18
OSR	2.56	0.45	1.0	0.12
Wheat (Baker et al 2014)	0.95			

### 1 4.3 Damping ratio

2 The dynamic response of a plant subject to a wind-induced displacement can be expressed in the  
3 frequency domain as (Sterling et al., 2003):

$$4 S_Y = |H(f)|^2 \frac{4\bar{Y}^2}{\bar{U}^2} S_U \quad (2)$$

5 where  $S_Y$  and  $S_U$  are the spectra corresponding to the plant's displacement and the wind  
6 respectively;  $\bar{Y}$  and  $\bar{U}$  are the mean values of displacement and wind velocity respectively and  
7  $|H(f)|^2$  represents the mechanical admittance function. Thus, if  $S_Y$ ,  $S_U$ ,  $\bar{Y}$  and  $\bar{U}$  are known it is  
8 possible to obtain the mechanical admittance function. Sterling et al. (2003) show that the  
9 mechanical admittance function for an isolated plant can itself be represented in the form of a two  
10 degree of freedom oscillator:

$$11 |H(f)|^2 = \frac{1}{\left(1 - \left(\frac{f}{f_n}\right)^2\right)^2 + 4\theta^2 \left(\frac{f}{f_n}\right)^2} \quad (3)$$

12 where  $f_n$  is the natural frequency and  $\theta$  is the plant's damping ratio. Fits of this type are also shown  
13 on Figure 8. Now it is possible to differentiate this equation and show that the mechanical  
14 admittance function has a maximum value when the normalised frequency is  $4\theta^2(1 - \theta^2)$ . Thus it is  
15 in principle possible to determine the damping ratio from experimental results for the mechanical  
16 admittance.

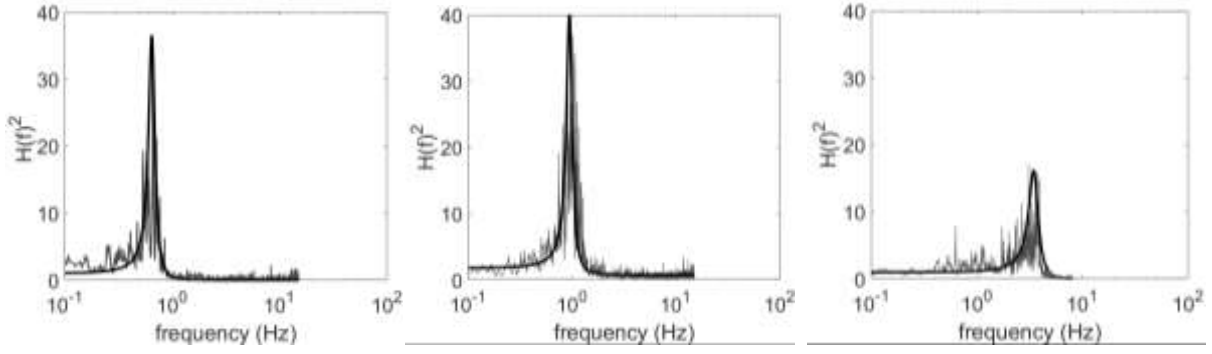
17 For both maize and oats, a clear peak can be identified from which the damping ratio can be  
18 obtained. However, for the case of OSR, the peak of the transfer function is not so clear, possibly  
19 due to the interlocked nature of the canopy, which effectively distributes the damping over a range  
20 of possible values. Results for all datasets are summarised in Table 4.

21 The damping ratio can also be obtained by observing oscillations of individual plants, and finding the  
22 ratio of two successive peaks (Clough and Penzien 1993). The damping ratio and the ratio of the  $n$   
23 and  $(n+1)$  peak are then related by the simple expression

$$24 \frac{2\pi\theta}{\sqrt{1-\theta^2}} = \ln\left(\frac{Y_n}{Y_{n+1}}\right) \quad (4)$$

1 from which a further estimate of damping ratio can be obtained. For oats, maize and for OSR, the  
2 two methods give similar values, with the ranges overlapping. In general, as would be expected the  
3 damping ratios for OSR are somewhat higher than for oats and maize, due to plant interlocking,  
4 although the difficulties in obtaining the OSR values from either method needs to be emphasised.  
5 The values for wheat from Baker et al (2014) are also shown and are similar to the values measured  
6 for oats.  
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(a) Maize

(b) Oats

(c) OSR

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**Figure 8** Mechanical admittance functions

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**Table 4** Values of damping ratio from spectral method and oscillating plants

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	Spectral method		Oscillating plants	
	Mean	SD	Mean	SD
Maize	0.13	0.04	0.15	0.09
Oats	0.11	0.05	0.10	0.04
OSR	0.13	0.05	0.22	0.08
Wheat (Baker et al 2014))	0.10			

#### 1 4.4 Drag Area

2 The drag force is dependent on canopy density, porosity, plant aerodynamic shape and the surface  
3 area of the canopy elements. From the lodging model (Baker et al, 2014), the following formula can  
4 be derived which relates the drag coefficient to the mean displacement

$$5 \bar{Y} = \frac{0.5\rho AC_F \bar{U}^2}{\mu(2\pi f_n)^2} \quad (5)$$

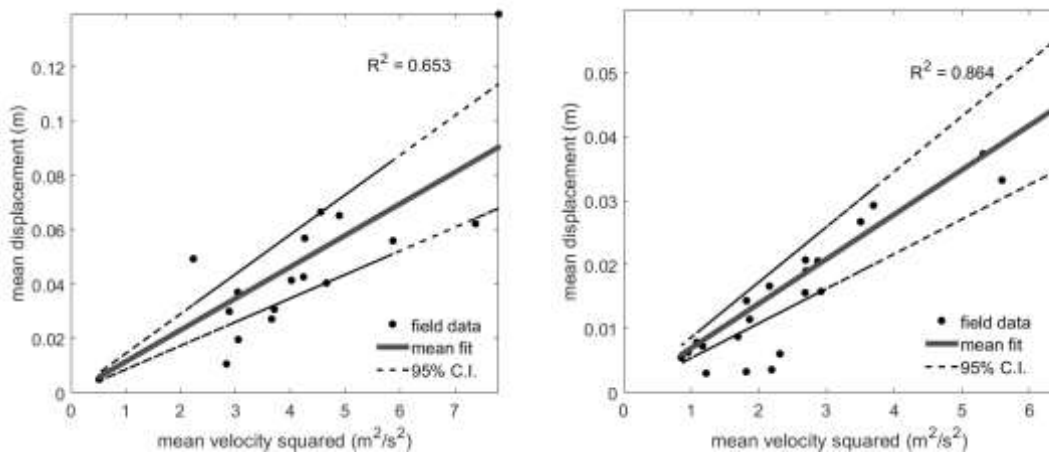
6 where  $\rho$  is the density of air,  $AC_F$  is the drag area per plant and  $\mu$  is the effective weight of a plant.

7 Figure 9 plots the mean displacement against the square of the mean velocity as would be suggested  
8 by the above equation. There is a reasonably good linear relationship, which enables the parameter  
9  $AC_F$  to be determined from the slope of the curve using the above expression. The mean fit and  
10 upper and lower bounds of the 95% confidence interval pass through the origin to satisfy the  
11 premise of equation (5), i.e. that the mean displacement is zero at zero mean wind speed. The  
12 resultant values and the 95% confidence levels are shown in table 6.

13 As might be expected, the smallest value of drag area / plant is for oats and the largest for maize,  
14 simply reflecting the physical size of the crop. The value for wheat (from Baker et al, 2014) is  
15 somewhat lower than that for oats, although it should be noted that the experimental basis for the  
16 determination of this drag area was not the same as that reported in this paper and involved the  
17 measurement of moments on individual stems to give the drag coefficient (which was close to unity)  
18 and a quite crude estimate of the exposed plant area.

19

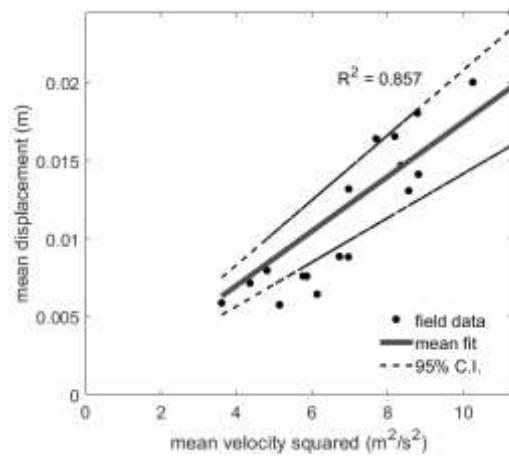
1



(a) Maize

(b) Oats

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(c) OSR

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**Figure 9** Mean displacement of all datasets plotted against mean velocity squared.

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**Table 6** Drag area values from plot of mean displacements against mean velocity squared

	$\mu$ (kg)	Mean	Upper bound	Lower bound
Maize	0.412	0.153	0.191	0.110
Oats	0.040	0.021	0.026	0.017
OSR	0.100	0.073	0.090	0.060
Wheat (Baker et al 2014)	-	0.008		

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#### 1 4.5 Parameter values from displacement time histories

2 An alternative methodology for determining crop dynamic and aerodynamic parameters is to  
3 directly fit the generalised model equation to the measured time histories of crop displacement.  
4 From the generalised model, the following equation relating displacement time history  $Y(t)$  to wind  
5 speed time history  $U(t)$  can be derived

$$6 \frac{1}{(2\pi f_n)^2} \frac{d^2 Y(t)}{dt^2} + \frac{2\theta}{2\pi f_n} \frac{dY(t)}{dt} + Y = \frac{0.5\rho AC_F}{(2\pi f_n)^2 \mu} U(t)^2 \quad (6)$$

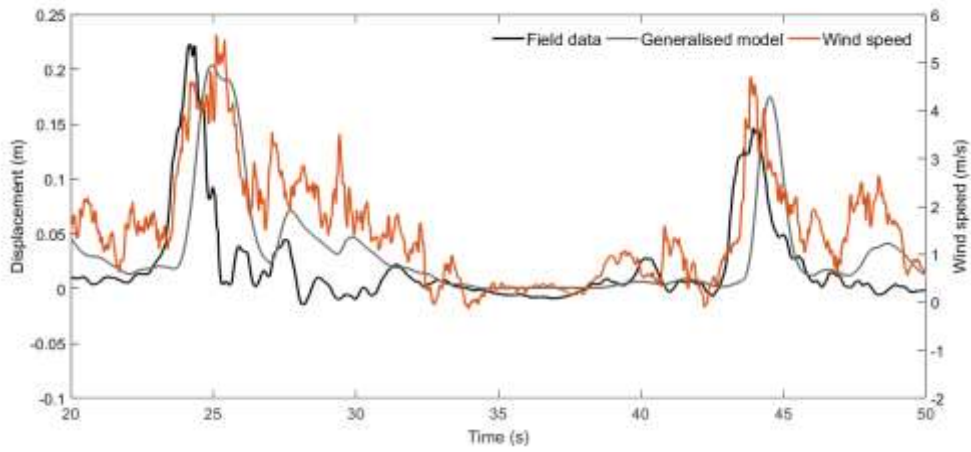
7 where  $t$  is time. Thus for a given wind speed time series it is possible in principle to solve this  
8 equation to predict the time dependent plant displacement, and to determine best fit values of  $f_n$ ,  $\theta$   
9 and  $AC_F$ . Using a fourth order Runge-Kutta approach (Lai et al 2017), the results of such a process  
10 are shown in Figure 10 below for oats, maize and OSR, for three datasets that are independent of  
11 those used in the earlier analysis and are not related to those shown in Figure 5 or used in the  
12 determination of the aerodynamic parameters. The best-fit values of the parameters are shown in  
13 Table 7. In general agreement the fit can be seen to be reasonably good, and the best-fit parameters  
14 fall mostly within the parameter ranges given in Tables 4 to 6, which gives added confidence in the  
15 overall analysis methodology. These figures also allow some more general comments to be made on  
16 the adequacy of the modelling process

- 17 • The predicted peak displacements for maize, oats and OSR agree well with the field data,  
18 although the displacements for OSR are small.
- 19 • The model captures the general oscillatory motion of oats quite well.
- 20 • Although the peak values are in good agreement, the intermediate values of displacement  
21 for maize and oats from the field experiments and the model do not agree terribly well. This  
22 is probably due to a 'friction' within the plant canopies i.e. a certain wind force is required to  
23 make the plants move at all. This could be allowed for in the model, although at the cost of  
24 removing the linearity of the solution, but since the peak values are, in practice, what is  
25 required, this does not seem to be necessary.

- 1       • The displacement for OSR are small, which is due to the fact that the OSR moves as a very  
2       large unit, because of the entanglement of the plants in the canopy, and does not react  
3       rapidly to sudden changes in wind speed. This suggests that such canopies could be  
4       modelled in a much simpler way, assuming the displacements simply follow the wind speed  
5       fluctuations averaged over (say) 5 to 10 seconds in a quasi-steady fashion.

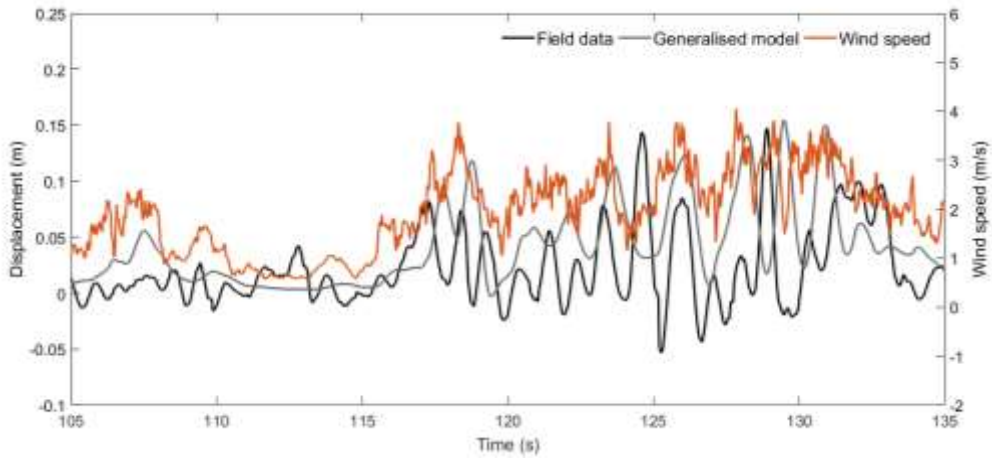
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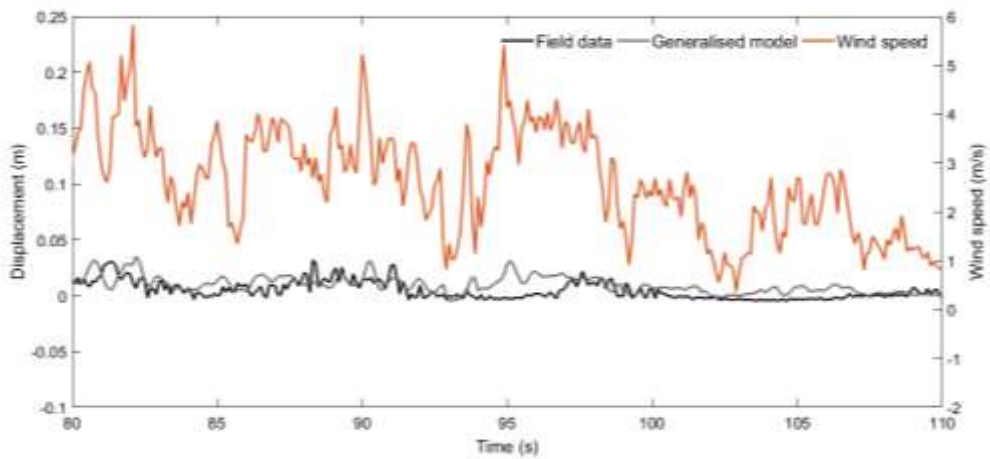
(a) Maize

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(b) Oats

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(c) OSR

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**Figure 10** Predicted and measured displacement data.

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**Table 7 Best fit parameters**

	$f_n$ (Hz)	$\theta$	$AC_F$
Maize	0.7	0.1	0.105
Oats	1.0	0.08	0.023
OSR	3.0	0.3	0.071

4

## 1 **4.6 Stem lodging velocities**

2 Table 8 brings together the various parameters for different crops, including stem parameters, and  
3 gives values of the stem lodging velocity from equation (1). These are between 4.0 and 5.3 m/s,  
4 values that at first sight seems rather low. However, it needs to be remembered that these are  
5 average velocities at crop height. The gust values at crop height that cause lodging will be of the  
6 order of 2 to 2.5 times the values given in the table (due to the high turbulence intensity). The values  
7 in the table can also be extrapolated to the normal meteorological measurement height of 10m  
8 above ground level through the use of the logarithmic velocity profile. To do so we make the  
9 assumption that the roughness length is 0.05m, and that the displacement height is 80% of crop  
10 height (both assumptions being somewhat arbitrary). These calculated mean values at 10m height  
11 are also shown in the table. Now, the normal definition of strong winds is a mean value of 10m/s at  
12 10m height, and it can be seen that the extrapolated values are in the strong wind range between  
13 11.5m/s and 16.5m/s. For context, in the UK, the 99<sup>th</sup> percentile average hourly wind speed at 10m  
14 height is between 11 and 13 m/s (Cook, 1985), and thus these stem lodging velocities would only be  
15 exceeded for a small proportion of the time. This is consistent with the lodging risk of commercial  
16 crops for which severe lodging seasons are experienced once every three to four years, when 10-  
17 20% of the UK crop experiences some lodging (Berry et al, 1998). This is not a proper statistical  
18 measure however and must be regarded as only a qualitative figure. It should be noted however that  
19 these extrapolated 10m velocities are very sensitive to the assumptions of surface roughness and  
20 displacement height, so should only be regarded as indicating a very approximate value  
21 corresponding to the more accurately determined lodging wind speeds at crop height.

22 Finally it is instructive to examine how the considerable uncertainties in the lodging velocities due to  
23 uncertainties in the parameters measured in these experiments relate to the uncertainties due to  
24 variations on plant agronomic parameters. Figure 11 shows a plot of the variation in stem lodging  
25 mean wind speed at 10m above the ground for variations in the dynamic and aerodynamic  
26 parameters and plant characteristics between the mean value minus two standard deviations and

1 the mean value plus two standard deviations for each parameter. For the agronomic parameters,  
 2 the standard deviations that are used are typical of those found in field trials for nominally identical  
 3 plants. It can be seen that in general, the greatest uncertainties in lodging velocities arise because of  
 4 uncertainties in stem strength and stem radius. Of the parameters measured here, the measured  
 5 uncertainties in natural frequency and damping ratio do not result in major variations in lodging  
 6 velocity, whereas variations in the drag area are more significant. Thus, in practical terms, the  
 7 uncertainties in the dynamic parameters measured here are of less significance than uncertainties in  
 8 the various agronomic parameters.

9 To give further context to these calculations, if we assume a wind climate with a Weibull distribution  
 10 of hourly mean velocities, with a shape factor of 2.0 and a scale factor of 5m/s, which is typical of UK  
 11 conditions (Cook, 1985), then the risk of those velocities being exceeded is shown in Figure 12. It can  
 12 be seen that a change of 2m/s results in the risk of the value being exceeded changing by an order of  
 13 magnitude, and a change of 4m/s results in a two order of magnitude change in risk. Thus, from  
 14 Figure 11, very broadly, uncertainties in the aerodynamic parameters results in an uncertainty in risk  
 15 of lodging of an order of magnitude, whilst uncertainties in stem strength and stem diameter results  
 16 in two orders of magnitude uncertainty in risk. The uncertainties are thus large, and in practical  
 17 terms the lodging model is best used to compare the risks of different plant characteristics to  
 18 identify those most associated with lodging, and also to give an indication of regions where lodging  
 19 risk may become excessive.

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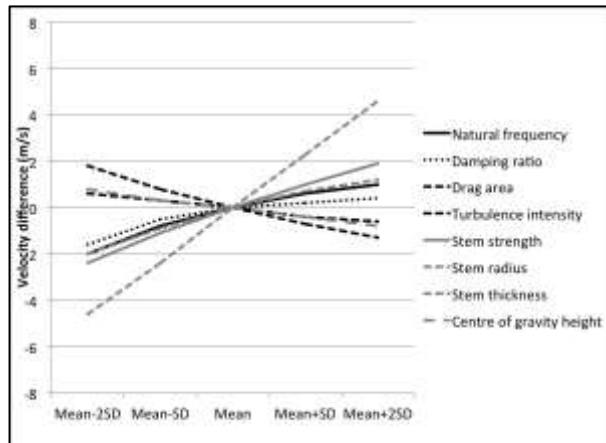
**Table 8** Calculated stem lodging velocities

	Maize	Oats	OSR	Wheat (Baker et al 2014)
$f_n$ (Hz)	0.7	1.1	2.6	0.95
$\theta$	0.11	0.11	0.13	0.10
$AC_F$ (m <sup>2</sup> ) (per plant)	0.153	0.021	0.090	0.008
$I_u$	0.59	0.62	0.46	0.50
$X$ (m)	0.95	0.63	0.46	0.43
$\sigma$ (MPa)	21.9	40.0	23.2	30.0
$a$ (mm)	12.5	2.8	6.2	1.65
$t$ (mm)	2.6	0.9	2.4	0.6

Number of shoots	1	2	1	4
$\bar{U}_{LS}$ (m s <sup>-1</sup> )	5.2	4.0	5.3	4.4
Crop height (m)	2.5	1.0	1.6	1.0
10m wind speed (m/s)	11.5	15.1	14.8	16.5

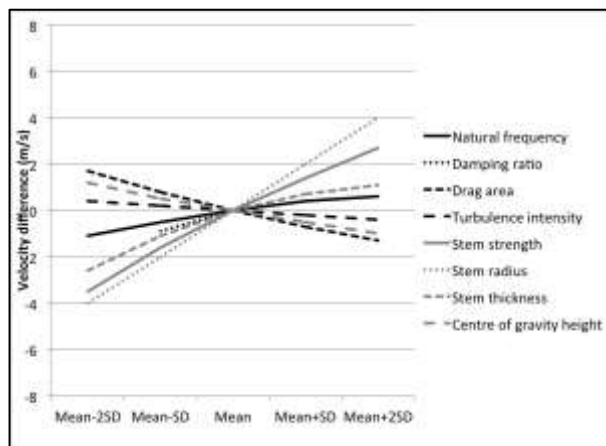
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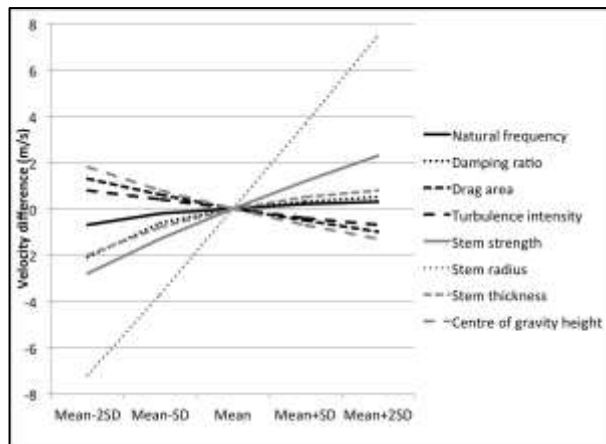
(a) Maize

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(b) Oats

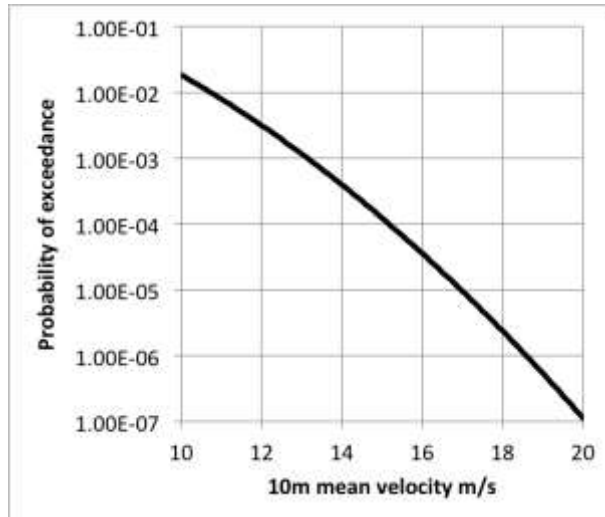
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(c) OSR

**Figure 11** Variations in lodging wind speed caused by dynamic, aerodynamic and agronomic parameters





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**Figure 12** 10m mean velocity probabilities

## 1 5. Conclusions

2 From what has been set out above, the following major conclusions can be drawn.

- 3 • The experimental methodologies adopted have been shown to be robust and consistent  
4 dynamic and aerodynamic parameter values have been derived. The spread of data for the  
5 biological systems studied here is large in comparison to normal wind engineering  
6 expectations.
- 7 • Whilst the measurements for oats and maize show strong peaks in the displacement spectra  
8 at the natural frequency, the experimental data for the interlocked canopies of OSR do not  
9 indicate a much smaller resonant peak.
- 10 • Mean values of the fundamental natural frequency measured from displacement spectra  
11 have been determined as 0.7Hz, 1.1Hz and 2.6Hz for maize, oats and OSR respectively. The  
12 values obtained from measurements of oscillations of plants are somewhat different to  
13 these, due to plant interaction.
- 14 • Mean damping ratios for maize and oats are 0.13 and 0.11 from the spectral measurements  
15 with the manually oscillated plant measurements being similar, whilst the mean damping  
16 ratio for OSR is 0.13 from spectral measurements and 0.22 from the manually oscillate  
17 plants.
- 18 • The results for natural frequency and damping indicate that canopy interlocking in the OSR  
19 crop significantly damps the oscillatory response of a representative plant compared to  
20 maize and oats in which canopy interlocking is not as pronounced.
- 21 • Mean values of drag area / plant are  $0.153\text{m}^2$ ,  $0.021\text{m}^2$  and  $0.09\text{m}^2$  for maize, oats and OSR  
22 respectively. The values for this parameter show considerable scatter between datasets.
- 23 • The parameter values are consistent with those obtained for wheat in earlier investigations.
- 24 • Matching solutions of the differential equation for displacement with independent  
25 measured data requires parameter values that fall within or close to the measured ranges.

- 1 • These calculations also indicate that there may be considerable ‘friction’ within plant  
2 canopies that dampens out plant movement at low wind speeds.
- 3 • Further the calculations suggest that to determine lodging velocities for OSR a much simpler  
4 methodology could be used, where the response can be modelled in a quasi-steady way,  
5 with the canopy moving directly in phase with velocity fluctuations.
- 6 • Using the average values of the dynamic and aerodynamic parameters to calculate stem  
7 lodging velocities shows that these are approximately equivalent to 10m average wind  
8 speeds of 11m/s to 15m/s for the three crops, within the normally defined range for strong  
9 winds.
- 10 • The sensitivity of the lodging velocities to the uncertainties in the measured dynamic and  
11 aerodynamic parameters leads to an uncertainty in lodging risk of the order of one order of  
12 magnitude. By contrast, uncertainties in the measurements of stem strength and radius lead  
13 to risk uncertainties of approximately two orders of magnitude.

14 The work described in this paper is one aspect of a number of linked projects that are investigating  
15 lodging in various crops in various parts of the world. Future papers will describe how the calibrated  
16 lodging model is incorporated into a GIS based model to characterise the spatial distribution of the  
17 risk for both stem and root lodging.

18

1 **Acknowledgements**

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3 Council Global Challenges Research Fund (GCRF BB/P023282), Sustainable Agriculture Research and  
4 Innovation Club (SARIC BB/P004555) fund and Teagasc (Walsh Fellowship) the Agricultural and Food  
5 development Authority of the Republic of Ireland.

6

7 **Dedication**

8 This paper is dedicated to one of the authors, John Finnan, who died in an aircraft accident during  
9 the course of the research. John's expertise and input was instrumental for the agricultural  
10 elements of the research on oats. However, John also had an uncanny knack of delivering a  
11 constructive and well-timed challenge on the wind engineering aspects of the research, thereby  
12 ensuring that those authors who claim to profess such expertise reflected long and hard on how  
13 their message could be delivered more appropriately – something which is key to ensuring  
14 successful trans-disciplinary research. Perhaps this is something that we all might like to reflect on  
15 as subject boundaries become less opaque – he would have liked that.

16

17

18

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## 1 **Appendix**

2 This appendix presents details relating to the framework adopted in the tracking program which was  
3 developed in-house by Dr S Gillmeier using the Image Processing Toolbox' and the 'Statistics and  
4 Machine Learning Toolbox' available in MATLAB (<https://uk.mathworks.com/>). The developed code  
5 uses the MATLAB HSV (Hue Saturation Value) colour model to read the input video file which is in  
6 RGB (red green blue) format and set to detect red pixels in the video frames (Figure A1). A different  
7 colour filter could have been applied but red was chosen since it provided an appropriate contrast  
8 with the plants. Using hue, saturation and value thresholds corresponding to the HSV ranges of the  
9 target red colour in the video file, the colour model masks other colours and outputs a binary image  
10 of the target for each frame. In which the areas of detected targets is marked with ones (indicated in  
11 white in figure A2a) and the rest of the figure is marked with zeros (indicated in black in figure A2a).  
12 A filtering operation is used to isolate the region with the highest concentration of red pixels by  
13 eliminating small pixel clusters below a specified size tolerance (Figure A2b); these may arise from  
14 objects in the background and would otherwise skew the centre of mass of the target region. The  
15 code then calculates the centroid of these isolated pixels relative to the image space in each frame  
16 of the video object (indicated with a red cross in figure A2c, corresponding to the red cross in figure  
17 A1). As the video reader steps through the frames of a video file, a two-dimensional array of  
18 centroid coordinates is created. If the target is not detected, the tracking code records a NaN value.  
19 Correction steps have been implemented in the code to account for strong wind conditions when  
20 the target is deflected out of the field of view of the cameras; these steps replace NaN values with  
21 centroid coordinates determined using the target's trajectory from its last recorded centroid  
22 position. In cases where the number of such values exceeded 2% of the record, the entire record is  
23 rejected.

24 The raw output of the tracking code is in the form of pixel displacement time histories in the along-  
25 wind and crosswind directions, Figure 5. Using the focal length of the camera lens, the image space

1 occupied by one pixel, the distance of the target to each camera lens aperture and the pixel  
2 coordinates of the target at zero stem displacement (i.e. when the target plant is still), the pixel  
3 displacement can be converted to displacements in length units.

4 The MATLAB Camera Calibration App ([https://uk.mathworks.com/help/vision/ug/single-camera-](https://uk.mathworks.com/help/vision/ug/single-camera-calibrator-app.html)  
5 [calibrator-app.html](https://uk.mathworks.com/help/vision/ug/single-camera-calibrator-app.html)) was used in order to calibrate each of the cameras, i.e., a checkerboard of known  
6 dimensions and two contrasting colours was created, positioned at various distances and angles  
7 from both cameras and multiple images from each of the cameras were created. This calibration  
8 was also supplemented by a rather simple experiment which involved placing a number of different  
9 colour dots (of various sizes) on a target and moving the target at a given rate in a known direction  
10 with a known velocity, and also by measuring the static deflections of marked crops in wind tunnel  
11 conditions.

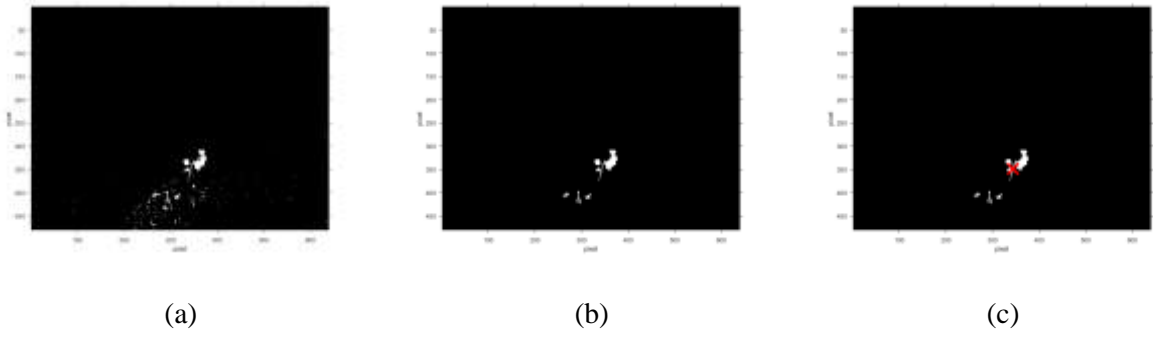


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13 **Figure A1:** Image of red pixel centroid tracking in a single video frame (OSR flowering)

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Figure A2 Steps in the video analysis procedure