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1	Direct 3D printing of monolithic ion exchange adsorbers
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7	
8	Abstract
9	Monolithic adsorbers with anion exchange (AEX) properties have been 3D printed in an easy
10	one-step process, i.e. not requiring post-functionalization to introduce the AEX ligands. The
11	adsorber, 3D printed using a commercial digital light processing (DLP) printer, was obtained
12	by copolymerisation of a bifunctional monomer bearing a positively charged quaternary
13	amine as well as an acrylate group, with the biocompatible crosslinker polyethylene glycol
14	diacrylate (PEGDA). To increase the surface area, polyethylene glycol was introduced into
15	the material formulation as pore forming agent. The influence of photoinitiator (Omnirad
16	819) and photoabsorber (Reactive Orange 16, RO16) concentration was investigated in
17	order to optimize printing resolution, allowing to reliably 3D print features as small as 200
18	μm and of highly complex Schoen gyroids. Protein binding was measured on AEX adsorbers
19	with a range of ligand densities (0.00, 2.03, 2.60 and 3.18 mmol/mL) using bovine serum
20	albumin (BSA) and c-phycocyanin (CPC) as model proteins. The highest equilibrium binding
21	capacity was found for the material presenting the lowest ligand density analysed
22	(2.03 mmol/mL), adsorbing 73.7 \pm 5.9 mg/mL and 38.0 \pm 2.2 mg/mL of BSA and CPC,
23	respectively. This novel 3D printed material displayed binding capacities in par or even
24	higher than commercially available chromatographic resins. We expect that the herein
25	presented approach of using bifunctional monomers, bearing commonly used
26	chromatography ligands, will help overcome the material limitations currently refraining 3D
27	printing applications in separation sciences.
28	
29	Keywords: Additive manufacturing; Digital light processing; 3D print materials;
30	Anion exchange chromatography; Protein adsorption
31	

32 **1. Introduction**

33 3D printing, also known as additive manufacturing (AM), encompasses a range of techniques

to fabricate three dimensional objects from computer aided design (CAD) models through

35 layer by layer addition of material. Several 3D printing methods have been developed and

36 optimised over the last couple of decades, each with its own specifications in terms of costs,

- resolution, build size, speed and materials [1]. AM techniques are developing at a fast pace,
- 38 and today it is possible to print complex structures with high fidelity at micron scale
- resolution in a rapid and robust process [1]. In addition, the cost of 3D printers is dropping
- 40 significantly with time, triggering the adoption of AM methods in a range of scientific fields

such as chemistry [2], drug delivery [3], microfluidic [4,5] and tissue engineering [6].

42 Interestingly, 3D printing is not widely employed in the separation sciences yet, especially in

43 chromatographic separations [7]. A range of serious barriers has so far limited the use of 3D

44 printing methods in chromatography, e.g. the lack of materials compatible with both 3D

45 printing processing and chromatographic operations, as well as the relatively poor

46 resolution of current 3D printers to generate features in the micron scale [8].

47 The performance of chromatographic separations depends on a number of factors,

48 including the flow of the mobile phase within the column and the related axial dispersion

49 and band broadening effects. Traditional stationary phases consist either of random beds of

50 spherical particles or random monolithic networks. Accordingly, each column has a slightly

51 different internal morphology and porous structure, their chromatographic behaviour is

52 impossible to be predicted *a priori*, and they require careful testing and validation of the

53 packing quality prior to use. Computer simulations demonstrated that ordered beds provide

significantly improved chromatographic performance over randomly organised stationary

phases [9,10]. In an attempt to experimentally prove the simulated results, Fee *et al.* [11] 3D

56 printed chromatography beds with precisely controlled and highly ordered morphology.

57 These were printed with high fidelity and reproducibility to the original CAD designs. 3D

58 printing also opened the opportunity to explore alternative bed configurations and particle

- 59 shapes, allowing experimental demonstration that spherical particles are not necessarily the
- 60 best shape for chromatographic operations, and that new bed morphologies can improve
- 61 pressure drop and plate height characteristics [12]. Yet, only commercially available
- 62 urethane-based materials for 3D polyjet printing could be tested, and flow performance of

the columns was determined by residence time distribution experiments with non-retained
 tracers. No separation could be carried out as the material did not present suitable

functional groups, while its proprietary composition limited opportunity for targeted

66 activation chemistry and functionalization with chromatographic ligands.

67 Lack of suitable materials for chromatographic separations that can be processed by 3D

68 printers represents the current biggest hurdle for the 3D printing of separation devices.

Although, there is a large range of 3D printable materials available on the market (metals,

ceramics, polymers), none of it was developed to bear specific functional groups for

- separations. Additionally, most material formulations are proprietary, and include a range of
- components such as plasticizers, fillers and additives to enable their 3D printing. This greatly

- 73 limits any attempt in their functionalization and renders impossible the prediction of their
- 74 potential separation behaviour.
- To overcome this issue, three main approaches have been applied to 3D print separation
- 76 devices. The simplest approach employs commercial materials which show some degree of
- separation properties. For example, MacDonald et al. exploited the overall negative surface
- charge of the Veroclear material (from Stratasys) to fabricate thin layer chromatography
- 79 (TLC) platforms for protein separations [13]. Su *et al.* employed another polyacrylate based
- 80 material (BV-001, Rays Optics Inc.) with electron donor groups on its surface for the
- fabrication of a device able to selectively extract trace elements from seawater [14].
- 82 Although this method is relatively straightforward, the lack of knowledge of the material
- chemistry heavily limits its extension to other separation methods e.g. relying on
- 84 hydrophobic, multimodal or affinity interactions.
- A second approach involves the printing of materials with known composition and
- 86 chemistry, which are functionalised with appropriate chromatographic ligands post printing.
- 87 This strategy was employed by Fee *et al.* to produce agarose and cellulose based stationary
- phase which were later functionalized with a range of chromatographic ligands [15]. Seo *et*
- *al.* printed micropatterned AEX membranes by printing the desired membrane shape with
- non-functionalised material which was then followed by a quaternisation procedure [16].
- 91 Such approach is at all similar to current production of chromatographic resins. Albeit it is
- 92 well established and robust, it requires additional manufacturing steps and adds complexity
- 93 in the processing line. Functionality can also be achieved by coating 3D printed structures
- 94 using, for example, initiated chemical vapour deposition [17] or porous metal frameworks
- 95 [18].
- 96 The third approach aims at custom design and 3D print the column casing only, which is
- 97 later packed with commercial adsorber particles [19] or monolithic structures [20]. This
- 98 approach is particularly original and can lead to column geometries with improved
- 99 performance [21], but cannot be considered 3D printing of chromatography stationary
- 100 phases.
- 101 All these approaches require additional steps than just 3D printing, e.g. material
- 102 characterisation, post printing functionalisation or the assembly of different parts. On the
- 103 other hand, direct 3D printing of chromatographic adsorbers, i.e. already containing the
- 104 desired functional groups, would enable a convenient one-step fabrication method for
- 105 printing separation devices.
- 106 3D printing of functional materials has been recently proven in the field of chemical
- 107 catalysis, where catalytically active structures with carboxylic acid, amine and copper
- 108 carboxylate functionality were directly printed using bifunctional monomers as building
- 109 blocks [22]. These bifunctional monomers provided one functional group with the desired
- 110 catalytic chemistry as well as one to take part in the polymerization reaction. Experiments
- showed that the performances of the 3D printed catalytic structures were comparable with
- 112 those of commercial material.

- The use of bifunctional monomers has been explored in IEX monoliths by Milton Lee's 113
- 114 group. Fully functional porous monoliths were prepared in a single step synthesis via UV
- initiated polymerisation by copolymerising the crosslinker PEGDA with bifunctional 115
- monomers containing sulfonic acid [23,24], phosphoric acid [25], carboxylic acid [26] or 116
- amine groups [27]. Porosities were created by the solvents present in the reacting mixture. 117
- 118 All produced monoliths showed good protein uptake comparable to commercial columns.
- 119 In this work, direct 3D printing was employed to fabricate chromatography stationary
- 120 phases. The material developed contained AEX moieties, and its formulation was tuned and
- 121 optimised for their 3D printing in a digital light processing (DLP) 3D printer. Free radical
- polymerisation between a PEGDA crosslinker and a bifunctional monomer bearing 122
- quaternary amine groups was achieved using Omnirad 819 as photoinitiator. Addition of a 123
- light absorber was key to tune and control the resolution of the 3D printed models, enabling 124
- 125 reliable fabrication of complex structures with 200 µm thick features. The developed AEX
- material showed excellent protein adsorption behaviour for two model proteins, bovine 126
- 127 serum albumin (BSA) and C-Phycocyanin (CPC). Optimal ligand density for protein
- 128 adsorption was determined by adjusting the composition of the parent formulation before
- 129 3D printing. To the best of our knowledge, this work is the first proposing the one-step manufacture of functional stationary phases with perfectly ordered internal morphology.
- 130
- 131

2. Experimental 132

2.1. 133 Materials

2-(Acryloyloxy)ethyl trimethylammonium chloride (AETAC, 80 wt. % in water), ethanol 134

- (absolute, for HPLC, ≥99.8%), hexamethyldisilazane (HMDS), Reactive Orange 16 (RO16), 135
- 136 sodium hydroxide and Sudan I were purchased from Sigma-Aldrich (St. Louis, MO, USA).
- Bovine serum albumin (protease free powder), isopropanol (IPA, extra pure), polyethylene 137
- glycol (PEG-200, average MW 200 g/mol), sodium chloride, sodium phosphate mono and 138 139 dibasic were obtained from Fisher Scientific (Hampton, NH, USA). Phenyl bis(2,4,6-
- trimethylbenzoyl)-phosphine oxide (Omnirad 819, former Irgacure 819) was kindly donated 140
- by IGM resins (Waalwijk, The Netherlands). Polyethylene glycol diacrylate (PEGDA, SR259, 141
- average MW 200 g/mol) was donated from Arkema-Sartomer (Colombes, France). C-142
- Phycocyanin (CPC) was extracted from Spirulina platensis and gently provided by Dr. Alistair 143
- 144 McCormick (The University of Edinburgh, Institute of Molecular Plant Sciences). All
- chemicals were used as received; all buffers were prepared using deionised water (EuRO10 145
- 146 Reverse Osmosis System, Evoqua Water Technologies, Pittsburgh, PA, USA).
- 147 2.2. Material development
- The photocurable material was composed of 60 wt. % PEG-200 as porogen and 40 wt. % 148
- 149 PEGDA/AETAC mixture as crosslinker and bifunctional monomer, respectively. Printed
- samples were created with different ligand densities by adjusting the relative ratio of PEGDA 150
- and AETAC (Table 1). 151
- A radical photoinitiator (Omnirad 819, at 0.12, 0.25, 0.5, 1.0 and 1.5 wt. % based on 100 g of 152 porogen-monomers mixture) and a light absorber were added to the mixture. Three dyes 153

154 were considered as light absorbers to help increase the resolution of the 3D printed models,

- namely RO16, Sudan I and Tinuvin 326. A NanoDrop 2000c (Fisher Scientific, Hampton, NH,
- 156 USA) was employed to measure the absorbance spectra of the photoinitiator and
- 157 photoabsorbers to direct selection of the appropriate light absorber. RO16 was chosen for
- all further experiments due to its most suitable absorbance spectrum (see Results and
- 159 Discussion section). Three different concentrations of RO16 (0.063, 0.125, 0.250 wt. %,
- 160 based on 100 g of porogen-monomers mixture) were tested in combination with 0.5 wt. %
- 161 Omnirad 819. A final concentration of 0.125 wt. % RO16 was chosen to fabricate the prints
- 162 (100 μm cure depth at 1.7 s exposure). All material formulations were stored in tubes
- 163 covered in aluminium foil to prevent spontaneous polymerisation prior to 3D printing.

164

[Table 1]

165 2.3. Model creation and 3D printing

Computer-aided design (CAD) models were created on SolidWorks 2015 (Dassault Systèmes
 SOLIDWORKS Corp., Waltham, MA, USA), exported as STL file and sliced into 2D-layers using
 Netfabb 2017 (Autodesk, San Rafael, CA, USA). A unit cell of the Schoen Gyroid was created
 using Mathematica 10.4 (Wolfram Research Inc., Champaign, IL, USA).

- A Solfex 350 (W2P Engineering, Vienna, Austria) digital light processing (DLP) printer (50 μm
- 171 pixel size in x-y plane, UV-LED at 385 nm with light intensity of 16 mW/cm²) was used as 3D
- printing platform. All parts were printed in 100 μm layers (z-direction) as a reasonable
- 173 compromise between printing resolution, column size and overall printing time. Post-
- 174 printing, the parts were washed three times in IPA in an ultrasonic bath (Allendale
- 175 Ultrasonics, Hodesdon, UK) and then fully cured in water with a xenon Otoflash G171 unit
- 176 (NK-Optik, Baierbrunn, Germany). Parts were stored in water until final use.
- 177 To determine the working curve (layer thickness vs exposure time) of the new material
- 178 formulations, 8 mL of the material were transferred into a petri dish (ø 60 mm) and placed
- above the printing area of the DLP. Eleven circles (ø 8 mm) were cured at different locations
- 180 with exposure times from 1 to 60 s. After cleaning with IPA and post-curing, the thickness of
- 181 the polymerised circles was measured using a micrometre (RS Pro Micrometer External, RS
- 182 Components, Corby, UK).

183 **2.4.** Qualitative characterisation of porous network

The internal structure of printed parts was imaged through scanning electron microscopy
(SEM, S-4700, Hitachi, Tokyo, Japan). Cylindrical gyroidal structures (50 % external porosity,
500 µm wall thickness) were printed and then dehydrated in 70 %, 80 %, 90 % and 100 %
ethanol, with each step performed three times for 10 min. The gyroids were then
transferred to HMDS for 2 min, HMDS was then removed and samples were left to dry
[28,29]. Subsequently, the cylinders were immersed in liquid nitrogen and snapped into
halves, gold sputter coated and SEM imaged.

- 191 The interconnectivity of the porous structure was tested by incubating cylindrical gyroid
- 192 structures (50% external porosity, 500 µm wall thickness) with 1 mg/mL blue CPC in
- phosphate buffer (25 mM, pH 7) for 24 h. After incubation, gyroids were cut into halves and 193
- 194 the cross section of the walls was visually investigated in regard of colour.

2.5. **Protein batch adsorption** 195

Hollow cylinders fitting into 96-microplate wells were designed and 3D printed (Figure 1). 196 197 Prior to protein adsorption tests, printed cylinders were equilibrated with phosphate buffer (25 mM, pH 7) for a minimum of 48 h, with buffer exchange every 12 h. Protein adsorption 198 was triggered by addition of 170 µL phosphate buffer (25 mM, pH 7) containing 0-32 mg/mL 199 200 BSA or 0-8 mg/mL CPC to each well. The microplates were agitated at 800 rpm using a Thermomixer C (Eppendorf, Hamburg, Germany). Protein adsorption kinetics onto the 3D 201 202 printed cylinders was calculated by protein uptake in the bulk solution, measuring protein absorbance with a Modulus II Microplate Multimode Reader (Turner BioSystems, Sunnyvale, 203 204 CA, USA) at regular time intervals. The binding capacity, q, was calculated for each time 205 point using equation (1):

$$q = \frac{(c_i - c) \cdot V}{V_{cylinder}}$$

207 where c_i and c are the initial protein concentration and the concentration at time t, respectively, V is the volume of buffer in the wells and V_{cylinder} is the printed cylinder volume 208 209 (19.37 μL).

- The Langmuir model was employed to describe protein loading at equilibrium conditions 210 (q_{eq}) as function of the equilibrium protein concentration in the liquid phase (c_{eq}) : 211
- $q_{eq} = \frac{q_{max} \cdot c_{eq}}{K_D + c_{eq}}$ (2) 212
- The maximum binding capacity, q_{max} , and the Langmuir equilibrium coefficient, K_D , were 213 214 estimated by best fit regression using Origin 2016 (OriginLab, Northampton, MA, USA).

BSA concentration was measured through UV readings at 280 nm, while CPC concentration 215 was calculated from the absorbance at 615 and 652 nm according to the expression 216 reported in [30,31], adapted for NanoDrop measurements by adding a correction factor of 217 218 0.1 to account for the shorter path length: $c_{CPC} = \frac{A_{615} - 0.474 \cdot A_{652}}{5.34 \cdot 0.1}$

3

(1)

- The absorbance ratio of A_{615}/A_{280} is generally used to describe the purity of CPC. The 220
- absorbance at 615 nm corresponds to the maximum absorbance of CPC, whereas the 221
- absorbance at 280 nm correlates to contamination with other proteins. A ratio of 0.7 is 222
- considered as food grade, 3.9 as reactive grade and greater than 4.0 as analytical grade [32]. 223
- 224 The CPC applied in experiments had a purity of $A_{615}/A_{280} = 2.3$. All batch adsorption
- experiments were performed in triplicate. 225
- 226

[Figure 1]

228 **3. Results & Discussion**

229 3.1. Material development

230 The aim of this study was the one-step 3D printing of chromatographic beds with AEX 231 functionality. This was achieved by UV copolymerisation of the crosslinker PEGDA and the 232 bifunctional monomer AETAC bearing positive charged quaternary amine groups (Figure 2). 233 As second functional group, AETAC displays an acrylate group for the incorporation in the 234 polymeric network. PEGDA was chosen as crosslinker due to its known biocompatibility and low non-specific protein binding [33]. This principle of copolymerisation has previously been 235 reported for the fabrication of ion exchange monoliths [23–27]. In this study, 40 wt. % of the 236 crosslinker-monomer blend was mixed with 60 wt. % PEG-200 as pore forming agent. 237

238 239

[Figure 2]

240

241 3.1.1. Optimization of photoinitiator and photoabsorber concentration

The concentration of the photoinitiator in the material formulation determines the thickness of 3D printed layers, commonly known as the cure depth C_D . Different concentrations of the Omnirad 819 photoinitiator were tested and the resulting C_D for an exposure time of 1 and 2 s is summarised in Figure 3a. An exposure time of 1 to 2 s was found to be desirable to ensure an acceptable printing time for monolithic structures in later experiments. At fixed exposure time, the cure depth decreased with increasing

248 photoinitiator concentration. For instance, at 1 s exposure (i.e. a reasonably small exposure 249 time to enable fast printing), C_D was 1456 ± 271 µm when 0.125 wt. % Omnirad 819 was

employed, whereas $408 \pm 12 \,\mu\text{m}$ cured layer was obtained with an eight times higher

251 photoinitiator concentration (1.5 wt. %). At higher photoinitiator concentrations, the

supplied light is entirely absorbed in a thinner layer immediately above the print surface,

hence limiting light penetration into the photocurable material. Yet, the thinnest printed
layer achieved at the highest photoinitiator concentration of 1.5 wt. % (limited by the

solubility of Omnirad 819 in the monomers/porogen mixture) was 408 \pm 12 μ m for an

exposure time of 1 s. Such layer thickness was considered too large for appropriate

resolution in the 3D printed models; in addition, formulations with high initiator

concentrations are extremely sensitive to light, and start polymerizing before the 3D

259 printing process is initiated, thus making its handling particularly delicate. On the other

hand, C_D can be reduced by shortening the exposure time, however, extremely short
exposure times are not reliably delivered by the light engine of the DLP printer. The required
exposure time to cure a 100 µm layer was estimated equal to 64 ms or 344 ms for the

263 materials containing 0.25 wt. % or 1.5 wt. % Omnirad 819, respectively (estimation using

fitting parameters from Table S2). A reasonable compromise of 0.5 wt. % Omnirad 819 wasselected to prepare all material formulations.

266

267

268

[Figure 3]

- 269 Light absorbers (or photoabsorbers, PA) are usually added to the formulation to increase
- control over the polymerization reaction and further decrease the cure depth. These 270
- components absorb part of the supplied light, thus lowering the penetration depth of the 271
- UV light within the material, hence reducing C_D . Figure 3b presents the absorbance spectra 272
- of three light absorbers considered in this work, RO16, Tinuvin 326 and Sudan I. All three 273
- PAs absorb light at 385 nm, i.e. the printer's output. Tinuvin 326 absorbed up to 410 nm, 274
- 275 whereas the photoinitiator (Omnirad 819) absorbed up to 440 nm. Accordingly, Tinuvin 326 276 is unable to protect the formulation from early polymerisation in ambient light. Sudan I and
- 277 RO16 showed similar absorbance spectra, overlapping completely with the Omnirad 819
- 278 spectrum in the UV-vis range, hence ensuring full protection in ambient light. For further
- 279 investigations RO16 was chosen due to its lower health and safety risks.
- Working curves (C_D vs. exposure time) for different RO16 concentrations in combination 280
- 281 with 0.5 wt. % Omnirad 819 are shown in Figure 3c. As expected, use of higher
- concentrations of the PA resulted in thinner polymerised layers. The appropriate 282
- 283 concentration of PA to be used is a compromise between its concentration in the
- formulation and the exposure time required to achieve a certain cure depth, i.e. an 284
- 285 appropriate resolution of the printed part. On one hand, concentration should be as small as
- possible to limit its presence in the cured model part, which in turn could cause secondary 286
- 287 issues such as non-specific protein binding and colour retention. On the other hand, light 288 exposure should enable curing of a layer in a reasonable time and with reasonable
- resolution. As stated earlier, the target in this work was the printing of 100 µm layers in 289
- 1 2 s. At the smallest RO16 concentration tested (0.06 wt. %), an exposure time of 1 s 290
- resulted in a C_D of 286 ± 31 μ m, i.e. a 30 % reduction with respect to the parent formulation 291
- with no PA. At 0.25 wt. % RO16, 1 s exposure did not cure a measurable layer, and 292
- 293 approximately 2.4 s would be required to cure a 100 µm thick layer (according to
- 294 logarithmic fit). An intermediate concentration of 0.125 wt. % RO16 led to a C_D of
- 295 $100 \pm 30 \,\mu$ m in 1 s UV exposure, equivalent to a 75 % reduction with respect to the 296 formulation with no PA. This concentration was employed in all further formulations and
- 297 experiments.

298 3.1.2. Printability and resolution of the new material formulation

- 299 To investigate the printability and resolution of the material formulation here developed, a 300 test cube was designed and 3D printed (Figure 4a and b). The cube contains square channels of 500 µm width separated by walls with thickness ranging from 200 to 1000 µm. The design 301 of the test cube is symmetrical and such that resolution over all three printing directions (x, 302 303 y and z) can be investigated at the same time, regardless of the orientation of the cube. As
- can be observed in Figure 4b, all walls were neatly printed, demonstrating the ability to 304 reliably print up to 200 μ m thin features, i.e. two 100 μ m printed layers.
- 305
- Conventional IEX adsorber beads for preparative chromatography have diameters ranging 306
- 307 from 15 to 200 μ m, with average diameter of 90 μ m [34]. The structures 3D printed with the
- 308 new IEX material have feature size comparable with those of commercial chromatographic
- resins. Yet, this study aims at presenting the proof the concept of direct printing of 309

functional materials for IEX. Further increase of the print resolution (50 to 100 μ m range) is currently being investigated and will be the focus of future reports.

312 The capability of 3D printing technologies to enable manufacturing of optimized three

dimensional ordered structures has been recently discussed [8,10,12]. In particular, printing

- of complex monolithic structures with defined channel size, geometry and configuration
- 315 tuned for specific separations is particularly attractive. Triply periodic minimal surfaces

316 (TMPS) have been recently reported as geometries for chromatographic beds, with

317 computer simulations demonstrating superior chromatographic performance in terms of

- permeability and axial dispersion (HETP) over random packed beds and monoliths [10]. The
- 319 potential to print these complex TPMS geometries using the novel material formulation was
- demonstrated (Figure 4c-f). The complex Schoen Gyroid structure, designed with 50 %
 external porosity and 500 μm wall thickness, was reliably and accurately printed, with
- interconnected walls for mechanical strength and no occluded channels for fluid flow. These
- 323 printed cylinders can be easily introduced into traditional chromatography columns and
- 324 connected to chromatography systems (e.g. FPLC) for chromatographic separations. As
- 325 printer resolution is addressed, TPMS structures with smaller features will be able to be
- 326 printed and employed.

327 328

[Figure 4]

329

330 3.1.3. Qualitative study of material porosity

331 The formulation of the new material incorporated PEG-200 as pore forming agent. The porous network within the printed material could not be analysed by SEM as the drying 332 operations for sample preparation caused substantial shrinkage and collapse of the porous 333 structure. As an alternative to SEM, the porous structure and its interconnectivity was 334 qualitatively tested by incubation of the gyroid model in CPC (Figure 4f-h), a blue protein 335 pigment complex extracted from the cyanobacterium Spirulina platensis. After 24 h 336 337 incubation, the original orange colour due to the RO16 dye was completely concealed by the 338 blue characteristic of CPC (Figure 4f and g). The cylinder was cut open to demonstrate 339 diffusion of the CPC protein within the bulk of the walls, with strong blue staining of the cut 340 sections (Figure 4h). As a result, it was concluded that the pores within the polymerised network were, on average, larger than the diameter of the CPC protein complex (11 nm) 341 [35] and that the pores were highly interconnected. Typical soluble proteins have a 342 343 diameter of 3 - 6 nm [36], suggesting that the internal porous network is suitable for protein adsorption. Further quantitative work on the porosity characteristics of the 3D printed 344 materials is required, both to improve the current material in terms of protein adsorption, 345 346 but also to enable use of this material towards other separation targets such as DNA and 347 viruses (VLPs, viral vectors, etc.).

348 3.2. Protein batch adsorption

Batch adsorption experiments were performed to analyse the protein adsorption behaviour
of the novel material formulations. The advantage of 3D printing to fabricate three
dimensional shapes from CAD models was employed here to simplify execution of the

experiments. In particular, the adsorbers were designed as hollow cylinders with 5 mm
outer diameter and 3.5 mm height as to fit in a well of a UV transparent 96-well plate
(Figure 1). The walls of the cylinders had a thickness of 500 µm to ensure sufficient
mechanical properties, and presented a number of holes to facilitate mixing of the buffers

356 and protein solutions.

In batch adsorption experiments with traditional chromatographic beads, protein 357 concentration is measured by withdrawal of a small amount of solution followed by 358 359 spectrophotometry. This method requires careful handling or a robotic platform, and 360 inherently introduce experimental errors due to the change of the overall volume of buffer throughout the experiment. This is particularly true in kinetic essays, i.e. where protein 361 concentration has to be monitored frequently. The hollow cylinder design here proposed, 362 363 enabled by 3D printing, allowed to measure protein concentration using a simple plate reader, with no need to either remove the adsorber from the wells or withdrawal of the 364 protein solutions, greatly simplifying execution of the experiments. 365

The effect of ligand density on protein adsorption was preliminary tested using BSA as 366 367 model protein. Four different material compositions, corresponding to ligand densities of quaternary amine functionality of 0.00 (control), 2.03, 2.60 and 3.18 mmol/mL, were 368 prepared and printed in the hollow cylinder format. BSA is considerably smaller than CPC 369 370 [37], thus it is reasonable to assume that the material's internal porous structure is 371 accessible to BSA. Figure 5a presents the BSA binding kinetics onto the AEX material with a 372 ligand density of 2.03 mmol/mL (kinetics for the materials with 2.60 and 3.18 mmol/mL ligand density can be found in Fig. S2). The adsorption kinetics was relatively fast, reaching 373 equilibrium conditions after a few hours only (dependent on initial BSA concentration). In 374 375 particular, at the lowest concentrations tested, equilibrium is reached after 1-3 hours, while 376 equilibrium was reached in less than 24 h at the highest BSA concentration tested. 377 Commercial bead based chromatography resins generally reach equilibrium within a couple 378 of hours [31,38–40], however, their characteristic dimension for diffusion (i.e. bead size) is 379 about 10 times shorter than the 3D printed cylinder walls (500 μ m). The adsorption kinetics observed results from a combination of different mass transport mechanisms, including 380 boundary layer mass transfer, diffusion within the internal pores, and adsorption kinetics. 381 The relatively thick walls of the cylindrical adsorbers (500 µm) suggests that diffusional 382 383 resistance might be the limiting factor for adsorption. This is particularly true at higher 384 protein concentrations, i.e. where diffusion may be hindered by previously adsorbed protein 385 molecules.

Equilibrium adsorption isotherms were measured using the data obtained after 24 h incubation (Figure 5b). The Langmuir model was employed to best-fit the adsorption isotherms, with model parameter summarized in Table 2. The highest binding capacity of 73.7 ± 5.9 mg/mL was achieved with ligand density of 2.03 mmol/mL. Higher ligand densities resulted in significantly lower binding capacities (57.4 ± 2.6 and 23.3 ± 2.5 mg/mL for 2.60 and 3.18 mmol/mL ligand density), indicating lower pore diffusivity and ligand accessibility as the ligand density increases. Similar trends of protein binding capacity with ligand density are relatively common [41,42] and justify the need to determine the optimum ligand density

- 394 when a new material is being developed. It is not excluded that lower ligand densities may
- 395 lead to improved binding characteristics for pre-functionalized 3D printed materials. The
- control adsorber, i.e. 3D printed without functional monomer, showed detectable albeit low
- non-specific protein adsorption (less than 10% with respect to the material with
- 2.03 mmol/mL ligand density) in agreement with other research findings [33]. Low non-
- 399 specific binding is a desirable characteristic for stationary phases, supporting the use of the
- 400 herein developed material as monolithic adsorbent for chromatography.

401 Commercial chromatographic resins with quaternary amine functional groups show equilibrium binding capacities of over 100 mg/mL for BSA. For example, Streamline Q XL 402 403 media from GE Healthcare, a resin for expanded bed adsorption chromatography, has 404 maximum binding capacity of $170 \pm 5 \text{ mg/mL}$ and equilibrium coefficient of $8 \pm 4 \text{ mg/mL}$ for BSA [43]. Q-Sepharose FF, another AEX resin from GE Healthcare, displays a maximum 405 406 binding capacity of 102.4 ± 1.6 mg/mL and an equilibrium coefficient of 0.109 ± 0.011 mg/mL [44]. Both resins bear a tenfold lower ligand density than material developed in this 407 408 work [45,46]. That supports the earlier observation that lower ligand densities may lead to 409 increased binding capacities. Other chromatographic media, such as membranes and 410 monoliths, instead display capacities in the 25-40 mg/ml range. For instance, the Sartorius's 411 Q membrane has a reported maximum capacity of 27.7 mg/mL [47] for a ligand density of 412 0.18 - 0.24 mmol/mL [48], while BIA CIM-QA monoliths are endowed with dynamic binding 413 capacities of 30-40 mg/mL for BSA [49] and ligand densities of about 1.1 mmol/mL [50]. Li et 414 al. prepared an AEX monolith using similar chemistry as described in this work and reported 415 a dynamic binding capacity of 56 mg/mL for a ligand density of 2.63 mmol/mL [27], comparable to the material with intermediate ligand density presented in this work (note Li 416 417 et al. determined binding capacity in dynamic conditions). The novel 3D-printable material 418 here presented displays somewhat lower binding capacity than traditional bead based resins (approx. 0.4 times than Streamline Q XL and 0.7 times than Q-Sepharose), but 419 420 significantly higher than membranes and monoliths. These results are extremely promising, 421 considering this is the first reported attempt to develop a pre-functional 3D printable 422 material for chromatography. Optimisation of the material's composition, ligand density and 423 separation conditions has great potential to improve the adsorption performance of such 3D printable materials. 424

425

[Figure 5]

426

The best performing material with 2.03 mmol/mL ligand density was selected for further adsorption experiments with CPC. Its strong blue colour facilitated visual observation of the adsorption process with time, with apparent colour changes of both the protein solution and the adsorber cylinders. In particular, a noticeable decrease in colour of the supernatant was observed for all CPC concentrations investigated (Figure 6a). At the same time, the adsorber cylinders turned from the initial orange colour to blue (Figure 6b), with stronger 433 blue shade at higher CPC concentrations. This visually proved successful adsorption, with

434 transfer of the protein from the liquid to the solid phase.

435 Protein adsorption was quantitatively confirmed by spectrophotometry, with equilibrium 436 adsorption data of CPC onto the newly developed AEX material summarized in Figure 6c and 437 best-fit Langmuir parameters in Table 2. Data for CPC adsorption onto quaternary amine resins is particularly scarce in the literature, limiting the comparison between different 438 439 chromatographic materials. The only data equilibrium data for CPC adsorption available are 440 for the Streamline Q XL [38] and Q Sepharose FF [31] (extracted from [38] and [31] and 441 reported in Figure 6 c to ease comparison). As opposite to what observed with adsorption of 442 BSA, the novel 3D printed AEX material displayed higher CPC adsorption capacity than the 443 commercial AEX resins, namely 1.4 times and 1.7 higher q_{max} for Streamline Q XL and Q-444 Sepharose, respectively. The affinity towards the CPC protein complex is on the same order of magnitude for the three materials, with the 3D printed adsorber having slightly better 445 446 affinity compared to Streamline Q-XL (halved k_D) and very similar to Q-Sepharose. 447 [Figure 6] 448 449 Interestingly, the adsorption capacity significantly drops from BSA to CPC, irrespective of the 450 material considered. However, while the drop-in binding capacity from BSA to CPC was a 451 452 dramatic 83 % in the Streamline Q XL and 78% in Q-Sepharose material, it only dropped of 453 40 % in the 3D printed AEX material. This difference is not related solely to the different 454 properties of the two proteins such as their difference in size (67 kDA BSA [44] vs. 112 kDa CPC [51]), their isoelectric point (4.9 for BSA [44] vs. 5.8 for CPC [52]) and the distribution of 455 456 charged and hydrophobic patches on the outer protein shell, but also to the material 457 properties e.g. ligand density, size and interconnectivity of internal porous structure. This 458 observation highlights, again, the importance of material optimization towards the specific target protein of interest. Current work is targeting material optimisation in regard of 459 porous structure, ligand density and mechanical properties. Other than optimization of 460 material properties, inherent matter for researchers in the material and separation sciences, 461 3D printing enables the tuning of the geometry for the stationary phase as well as the 462 mobile phase, thus offering an additional factor for further process optimization. 463

464

[Table 2]

465 **4. Conclusions**

This work demonstrates, for the first time, the potential to directly 3D print fully functional
stationary phases for protein separations in one simple manufacturing step. In particular,
anion exchange adsorbers were fabricated from a 3D printable material formulation
comprising i) a bifunctional monomer bearing quaternary amine groups as AEX ligands, ii) a
crosslinker to impart mechanical stability to the polymeric network, iii) a photoinitiator to
trigger the polymerization reaction upon exposure to UV light, iv) a pore forming agent to

- 472 increase the surface area of the resulting stationary phase, and v) a photoabsorber to
- 473 increase the resolution of the 3D printed part. This mixture enabled 3D printing of complex
- 474 structures such as the Schoen gyroid with high fidelity, as well as to fabricate parts with
- 475 200 μm large features. Even though this feature size is on the top range of commercial
- 476 chromatography resins, upcoming developments in 3D printing technologies are expected
- 477 to bring the resolution below the 100 μm threshold.
- 3D printed anion exchange structures were tested for adsorption of BSA and CPC, revealing 478 479 excellent adsorption characteristics, in line or even superior than those of commercially 480 available quaternary amine adsorbers. It is worth noting that such results were obtained after a basic optimization of the material composition and 3D printing settings. Additional 481 optimization efforts, e.g. on the porous structure of the cured material, print resolution, and 482 483 material formulation, has the potential to further improve the adsorption characteristics of such 3D printable AEX chromatographic materials. Also, use of other bifunctional monomers 484 485 enables extension of this approach to fabricate columns that could operate in other chromatographic modes. For example, 2-carboxyethyl acrylate [26] and sulfopropyl 486 487 methacrylate [23] could produce cation exchange materials, while butyl methacrylate and 2-488 hydroxyethyl methacrylate could be part of the formulation to fabricate hydrophobic
- 489 interaction columns [53].
- 490 The capability of 3D printing to create complex three-dimensional models directly from CAD
- 491 designs was exemplified in this work. Adsorbers were designed and 3D printed as hollow
- 492 cylinders, significantly simplifying execution of batch adsorption experiments in 96 well
- 493 plate format. This concept can be extrapolated in the future, with columns designed and
- 494 fabricated with new internal geometries, with improved chromatographic characteristics to
- 495 suit specific separation and purification applications.
- 496 We believe the results presented here enable the first steps to overcome the current
- 497 limitation in terms of materials compatible with 3D printing operations and at the same
- 498 time suitable for chromatographic separations. This has the potential to revolutionise the
- 499 chromatography arena, with fine-tuned and robust columns locally 3D printed, on demand
- and over a short period of time (e.g. overnight) as opposed to the current paradigm of "one-
- 501 column-fits-all-applications" produced in centralized manufacturing facilities.
- 502

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509 6. References

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7. Tables

Table 1: Composition of the different resin formulations.

Ligand density	AETAC	PEGDA	PEG-200
[mmol/mL]	[wt. %]	[wt. %]	[wt. %]
0	0	40	60
2.03	14	26	60
2.60	18	22	60
3.18	22	18	60

Table 2: Langmuir parameters for BSA and CPC adsorption onto the novel 3D printed material in comparison to commercial chromatography

679 resins. Displayed errors correspond to standard error.

	3D printed material		Streamline Q XL	Q Sepharose FF	Sartorius Q membrane		
		2.03 mmol/mL	2.60 mmol/mL	3.18 mmol/mL	0.23 - 0.33 mmol/mL [45] ¹	0.18- 0.24 mmol/mL [46] ¹	0.07 – 0.18 mmol/mL [48] ²
	<i>q_{max}</i> [mg/mL]	73.7 ± 5.9	57.4 ± 2.6	23.3 ± 2.5	170 ± 5	102.4 ± 1.6^3	27.2
DCA	k_D [mg/mL]	0.381 ± 0.108	0.274 ± 0.048	0.128 ± 0.075	8 ± 4	0.109 ± 0.011^3	0.054
DJA	R ²	0.92	0.98	0.75	-	-	0.99
	Data source	This work	This work	This work	[43]	[44]	[47]
	q _{max}	38.0 ± 2.2			28.1 ± 0.1	22.7	
CDC	k _D	0.041 ± 0.010			0.082 ± 0.001	0.031	
CPC	R ²	0.97			0.96	0.98	
	Data source	This work			[38]	[31]	
¹ Data g	¹ Data given in mmol Cl ⁻ /mL, assumed same molar concentration between Cl ⁻ and Q-ligand						
² Data g	² Data given in μeq/cm ² , assumed normal concentration equals to molar concentration, converted to mmol/mL using membrane thickness of 275 μm [47]						
³ Data g	³ Data given in mmoL/L, converted to mg/mL using molecular weight of BSA (67 kDa).						

681 Figure captions



682

Figure 1: Printed adsorber in form of a hollow cylinder. a) CAD model, b) photograph of printed cylinder, c) cylinders in 96-microplate wells. The hollow cylinder format allows convenient measurement of the protein concentrations using a plate reader.

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687

688 **Figure 2**: Chemical structures of a) PEGDA and b) AETAC.



Figure 3: AEX material development. a) cure depth, C_D, as function of Omnirad 819 691 (photoinitiator) concentration for exposure times of 1 and 2 s. Monomer to crosslinker ratio 692 of 14:26 (2.03 mmol/mL ligand density). b) Absorbance spectrum of Omnirad 819 (50 ppm by 693 weight in IPA) and the analysed dyes RO16, Sudan I and Tinuvin 326 (12.5 ppm in IPA/H₂O). 694 Printer's output wavelength was 385 nm (black dotted line). c) Working curves at different 695 concentrations of RO16 as photoabsorber. Other components are 0.5 wt. % Omnirad 819 and 696 697 monomer to crosslinker ratio of 14:26 (2.03 mmol/mL ligand density). Error bars in a) and c) 698 correspond to standard deviation. Green dotted lines correspond to the target layer thickness 699 of 100 µm. Fitting parameters in supplementary Table S1.



Figure 4: Testing printability, printing resolution and porous structure of the new material
formulation (ligand density 2.03 mmol/mL). a) CAD model and b) photograph of test cube
with 500 µm channels, separated by 200 to 1000 µm thick walls. c) CAD model and d,e) SEM
images of a Schoen gyroid with a designed external porosity of 50 % and wall thickness of
500 µm. Some degree of shrinkage can be noticed as a result of drying for sample preparation.
f) Photograph of printed cylindrical Schoen gyroid before and g) after 24h incubation with 1
mg/mL CPC. h) Model cut open after 24 h of incubation with 1 mg/mL CPC.



Figure 5: BSA batch adsorption experiments. a) Adsorption kinetics onto novel material
 formulation with ligand density of 2.03 mmol/mL. Initial BSA concentration of 0.5 – 6 mg/mL.
 b) Equilibrium adsorption data for the four materials tested (ligand densities of 0.00, 1.81,

712 2.32 and 2.84 mg/g). Continuous lines are best-fit according to Langmuir model. Fitting

parameters are listed in Table 2. Error bars correspond to standard deviation.



CPC concentration

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Figure 6: CPC batch adsorption onto novel 3D printed AEX material with ligand density of 2.03 mmol/mL. CPC concentration at beginning of experiment of 0.000, 0.125, 0.250, 0.500, 1.000, 2.000, 4.00 and 6.00 mg/ml. a) 3D printed cylinders in multiwell plate soaked in CPC solutions of different concentration at 0, 3 and 24 h following incubation. b) Adsorber cylinders after 24 h incubation with CPC solutions at increasing concentration. c) Comparison of equilibrium adsorption data of the AEX printed material (this work), Streamline Q XL (from

721 722	[40]) and Q-Sepharose (from [31]). Continuous lines are best-fit according to Langmuir model. Fitting parameters are listed in Table 2. Error bars correspond to standard deviation.
723	
724	Supplementary material
725	Direct 3D printing of monolithic ion exchange adsorbers
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731	

Table S1: Fitting parameter for working curves in Figure 3c. Curves are fitted with y=a*ln(x)+b.
Displayed error corresponds to standard error.

RO16 concentration [wt. %]	a [µm]	b [μm]	R ²
0.000	400 + 25	715 + 42	0.07
0.000	406 ± 25	715±43	0.97
0.063	318± 16	130 ± 43	0.98
0.125	188 ± 2	33 ± 3	0.99
0.250	97 ± 6	14 ± 17	0.98



Figure S1: Working curves for different Omnirad 819 concentrations from 0.25 to 1.5 wt. %. The green dotted line displays the target layer thickness of 100 μ m. The higher the initiator concentration the lower the C_D. Error bars correspond to standard deviation.

Table S2: Fitting parameter for working curves in Figure S1. Curves are fitted with y=a*ln(x)+b.

747	Displayed	error r	epresents	the stand	lard err	or.

Omnirad 819 concentration [wt. %]	a [µm]	b [μm]	R ²
0.25	384 ± 18	1157 ± 33	0.98
0.5	406 ± 25	715 ± 43	0.97
1.0	351 ± 12	315 ± 24	0.99
1.5	239 ± 15	355 ± 21	0.97



751 Figure S2: BSA binding kinetics for the initial protein concentrations from 0.5 to 4 mg/mL BSA.

752 Displayed errors represent standard deviation. (a) Material presenting a ligand densities of

- 753 2.60 mmol/mL. (b) Material with ligand density of 3.18 mmol/mL.