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Electromechanical Active Filter as a Novel Custom Power Device (CP)

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1. Introduction

One of the serious problems in electrical power systems is the increase of electronic devices which are used by the industry as well as residences. These devices, which need high-quality energy to work properly, at the same time, are the most responsible ones for decreasing of power quality by themselves.

In the last decade, Distributed Generation systems (DGs) which use Clean Energy Sources (CESs) such as wind power, photo voltaic, fuel cells, and acid batteries have integrated at distribution networks increasingly. They can affect in stability, voltage regulation and power quality of the network as an electric device connected to the power system.

One of the most efficient systems to solve power quality problems is Unified Power Quality Conditioner (UPQC). It consists of a Parallel-Active Filter (PAF) and a Series-Active Filter (SAF) together with a common dc link [1-3]. This combination allows a simultaneous compensation for source side currents and delivered voltage to the load. In this way, operation of the UPQC isolates the utility from current quality problems of load and at the same time isolates the load from the voltage quality problems of utility. Nowadays, small synchronous generators, as DG source, which are installed near the load can be used for increase reliability and decrease losses.

Scope of this research is integration of UPQC and mentioned synchronous generators for power quality compensation and reliability increase. In this research small synchronous generator, which will be treated as an electromechanical active filter, not only can be used as another power source for load supply but also, can be used for the power quality compensation. Algorithm and mathematical relations for the control of small synchronous generator as an electromechanical active filter have been presented, too. Power quality compensation in sag, swell, unbalance, and harmonized conditions have been done by use

of introduced active filter with integration of Unified Power Quality Conditioner (UPQC). In this research, voltage problems are compensated by the Series Active Filter (SAF) of the UPQC. On the other hand, issues related to the compensation of current problems are done by the electromechanical active filter and PAF of UPQC. For validation of the proposed theory in power quality compensation, a simulation has been done in MATLAB/SIMULINK and a number of selected simulation results have been shown.

A T-type active power filter for power factor correction is proposed in [4]. In [5], neutral current in three phase four wire systems is compensated by using a four leg PAF for the UPQC. In [6], UPQC is controlled by H_∞ approach which needs high calculation demand. In [7], UPQC can be controlled based on phase angle control for share load reactive power between SAF and PAF. In [8] minimum active power injection has been used for SAF in a UPQC-Q, based on its voltage magnitude and phase angle ratings in sag conditions. In [9], UPQC control has been done in parallel and islanding modes in dqo frame use of a high pass filter. In [10-12] two new combinations of SAF and PAF for two independent distribution feeders power quality compensation have been proposed. Section 2 generally introduces UPQC. Section 3 explains connection of the proposed active filter. Section 4 introduces electromechanical active filter. Section 5 explains used algorithm for reference generation of the electromechanical filter in detail. Section 6 simulates the paper. Finally, section 7 concludes the results.

2. Unified Power Quality Conditioner (UPQC)

UPQC has composed of two inverters that are connected back to back [2]. One of them is connected to the grid via a parallel transformer and can compensate the current problems (PAF). Another one is connected to the grid via a series transformer and can compensate the voltage problems (SAF). These inverters are controlled for the compensation of the power quality problems instantaneously. Figure 1 shows the general schematic of a UPQC.

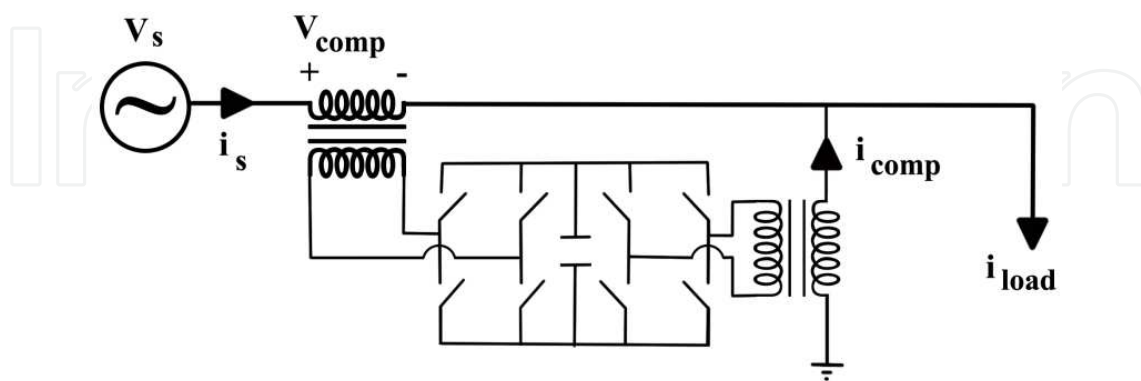


Figure 1. General schematic of a UPQC

A simple circuit model of the UPQC is shown in Figure 2. Series active filter has been modeled as the voltage source and parallel active filter has been modeled as the current source.

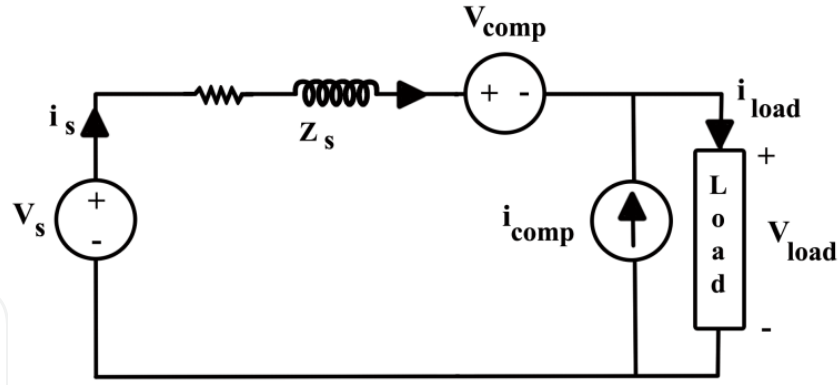


Figure 2. Circuit model of UPQC

3. Connection of Electromechanical Filter

Figure 3, shows schematic of the proposed compensator system. In this research load current harmonics with higher order than 7, has been determined as PAF of UPQC compensator signal. But, load current harmonics with lower order than 7 and reactive power have been compensated by the proposed electromechanical filter.

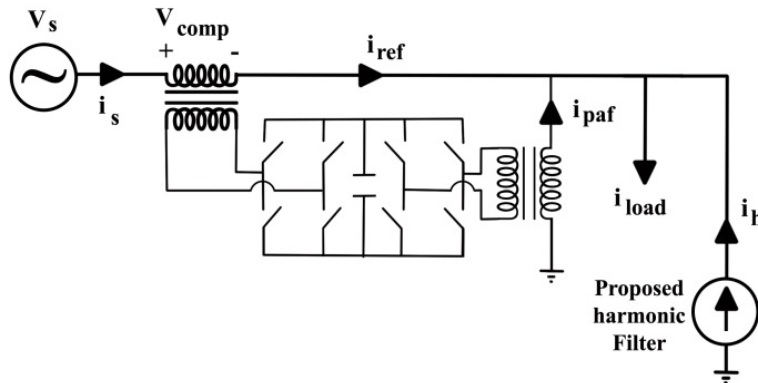


Figure 3. Proposed compensator system

4. Electromechanical Parallel Active Filter

Figure 4, shows the simple structure of a synchronous generator. Based on equation (1), a DC field current of i_f produces a constant magnitude flux.

$$F_f = N_f i_f, \quad \phi_f = \frac{N_f i_f}{R}, \quad \psi_f = \frac{N_f N_s i_f}{R} = M i_f \quad (1)$$

As in [13] N_f and N_s are effective turns of the field windings and the stator windings, respectively; F_f is the magnetomotive force; R is the reluctance of the flux line direction and M is the mutual induction between rotor and stator windings. Speed of rotor is equal to the synchronous speed ($n_s = \frac{120f}{p}$). Thus, the flux rotates with the angular speed of

$\omega_s = \frac{2\pi n_s}{60}$. So, stator windings passing flux has been changed as equation (2). It is assumed that in $t=0$, direct axis of field and stator first phase windings conform each other.

$$\psi_s = i_f M \cos(\omega t) \tag{2}$$

The scope of this section is theoretical investigation of a synchronous machine as a rotating active filter. This theory will be investigated in the static state for a circular rotor type synchronous generator that its equivalent circuit has been shown in Figure 5.

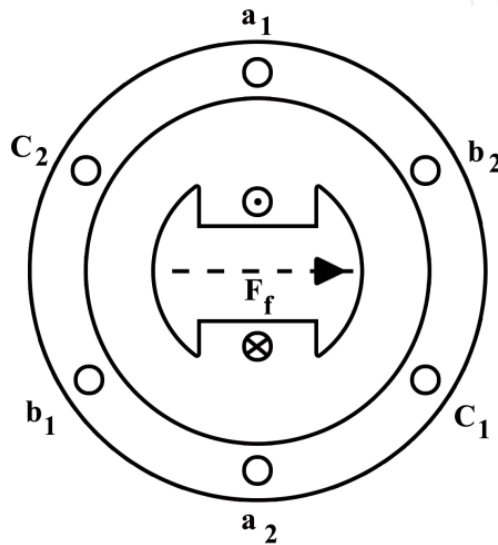


Figure 4. Simple structure of synchronous generator

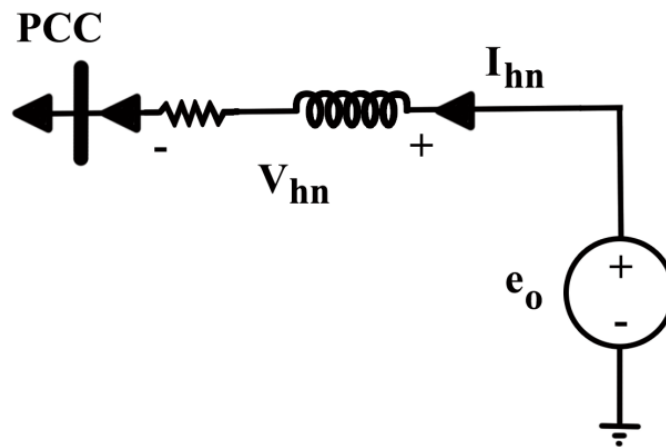


Figure 5. Equivalent circuit of synchronous generator

Equation (3) shows the relation between magnetic flux and voltage behind synchronous reactance of the generator.

$$e = - \frac{d\psi_s(t)}{dt} = - \frac{d(i_f M \cos(\omega t))}{dt} = -M \frac{d(i_f \cos(\omega t))}{dt} \tag{3}$$

Based on equation (3), if the field current be a DC current, the stator induction voltage will be a sinusoidal voltage by the amplitude of $M\omega i_f$. But, if the field current be harmonized as equation (4) then, the flux and internal induction voltage will be as equations (5) and (6), respectively.

$$i_f = I_{dc} + \sum_n I_{fn} \sin(n\omega t - \phi_{fn}) \quad (4)$$

$$\begin{aligned} \psi_f &= i_f M \cos(\omega t) = [I_{dc} + \sum_n I_{fn} \sin(n\omega t - \phi_{fn})] M \cos(\omega t) = \\ &MI_{dc} \cos(\omega t) + \frac{1}{2} M \sum I_{fn} [\sin((n+1)\omega t - \phi_{fn}) + \sin((n-1)\omega t - \phi_{fn})] \end{aligned} \quad (5)$$

$$\begin{aligned} e_o^* &= [-MI_{dc}\omega \sin(\omega t) + \frac{1}{2} MI_{f2}\omega \cos(\omega t - \phi_{f2})] + \\ &\sum_{n=2} [\frac{1}{2} MI_{f(n-1)} n\omega \cos(n\omega t - \phi_{f(n-1)}) + \frac{1}{2} MI_{f(n+1)} n\omega \cos(n\omega t - \phi_{f(n+1)})] \end{aligned} \quad (6)$$

Equation (6) shows that each component of the generator output voltage has composed of two components of the field current. This problem has been shown in Figure 6.

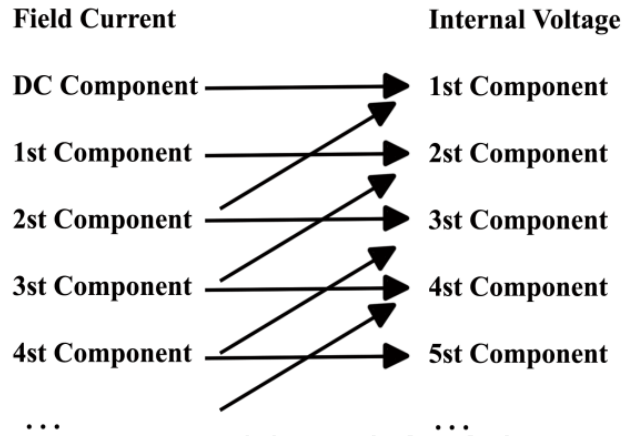


Figure 6. Relation of the field current components by the stator voltage components

It seems that a synchronous generator can be assumed as the Current Controlled System (CCS). Thus it can be used for the current harmonic compensation of a nonlinear load (I_{hn}) as parallel active filter.

5. Algorithm and method

From Figure 5, relation between terminal voltage of the generator and I_{hn} can be derived as equation (7).

$$e_o = V_{pcc} + Z_n I_{hn} = \sum_n V_n \sin(n\omega t + \theta_n) \quad (7)$$

Where, n is the harmonic order; $Z_n = R + jnX$ is the harmonic impedance of the synchronous generator and connector transformer which are known, V_{PCC} is the point of common coupling voltage and I_{hm} is the compensator current that has been extracted from the control circuit.

If similar frequency components of voltage signal e_o^* in equation (6) and e_o in equation (7) set equal, the magnitude and phase angle of the related field current components will be extracted as:

For $n=1$:

$$-MI_{dc}\omega \sin(\omega t) + \frac{1}{2}MI_{f2}\omega \cos(\omega t - \varphi_{f2}) = V_1 \sin(\omega t + \theta_1) \quad (8)$$

$$\sqrt{[-MI_{dc}\omega + \frac{1}{2}MI_{f2}\omega \sin \varphi_{f2}]^2 + [\frac{1}{2}MI_{f2}\omega \cos \varphi_{f2}]^2} = V_1 \quad (9)$$

$$\tan^{-1}\left[\frac{\frac{1}{2}MI_{f2}\omega \cos \varphi_{f2}}{-MI_{dc}\omega + \frac{1}{2}MI_{f2}\omega \sin \varphi_{f2}}\right] = \theta_1 \quad (10)$$

For simplicity equations (9) and (10) can be rewritten as follows:

$$X = -MI_{dc}\omega + \frac{1}{2}MI_{f2}\omega \sin \varphi_{f2} \quad (11)$$

$$Y = \frac{1}{2}MI_{f2}\omega \cos \varphi_{f2} \quad (12)$$

$$X^2 + Y^2 = V_1^2 \quad (13)$$

$$\frac{X}{Y} = \theta_1 \quad (14)$$

From the above equations, magnitude and phase of the second component of field current can result in:

$$X = \frac{V_1}{\sqrt{1 + \tan^2 \theta_1}} \quad (15)$$

$$\tan \varphi_{f2} = \frac{X + MI_{dc}\omega}{X \tan \theta_1} \quad (16)$$

$$I_{f2} = \frac{2(X + MI_{dc}\omega)}{M\omega \sin \phi_{f2}} \tag{17}$$

For $n \geq 2$:

$$X = \frac{1}{2}MI_{f(n-1)}n\omega \sin \phi_{f(n-1)} + \frac{1}{2}MI_{f(n+1)}n\omega \sin \phi_{f(n+1)} \tag{18}$$

$$Y = \frac{1}{2}MI_{f(n-1)}n\omega \cos \phi_{f(n-1)} + \frac{1}{2}MI_{f(n+1)}n\omega \cos \phi_{f(n+1)} \tag{19}$$

$$X = \frac{V_n}{\sqrt{1 + \tan^2 \theta_n}} \tag{20}$$

$$\tan \phi_{f(n+1)} = \frac{X - 0.5Mn\omega I_{f(n-1)} \sin \phi_{f(n-1)}}{X \tan \theta_n - 0.5Mn\omega I_{f(n-1)} \cos \phi_{f(n-1)}} \tag{21}$$

$$I_{f(n+1)} = \frac{2(X - 0.5Mn\omega I_{f(n-1)} \sin \phi_{f(n-1)})}{Mn\omega \sin \phi_{f(n-1)}} \tag{22}$$

Where, M and ω are the mutual inductance and angular frequency, respectively. Obviously for the extraction of required components of field current from the above equations, first suggestion for DC and first order component of the field current are need. Resulted field current can be injected via a PWM and current inverter to the field windings of the synchronous generator. Figure 7, shows the control circuit of the electromechanical

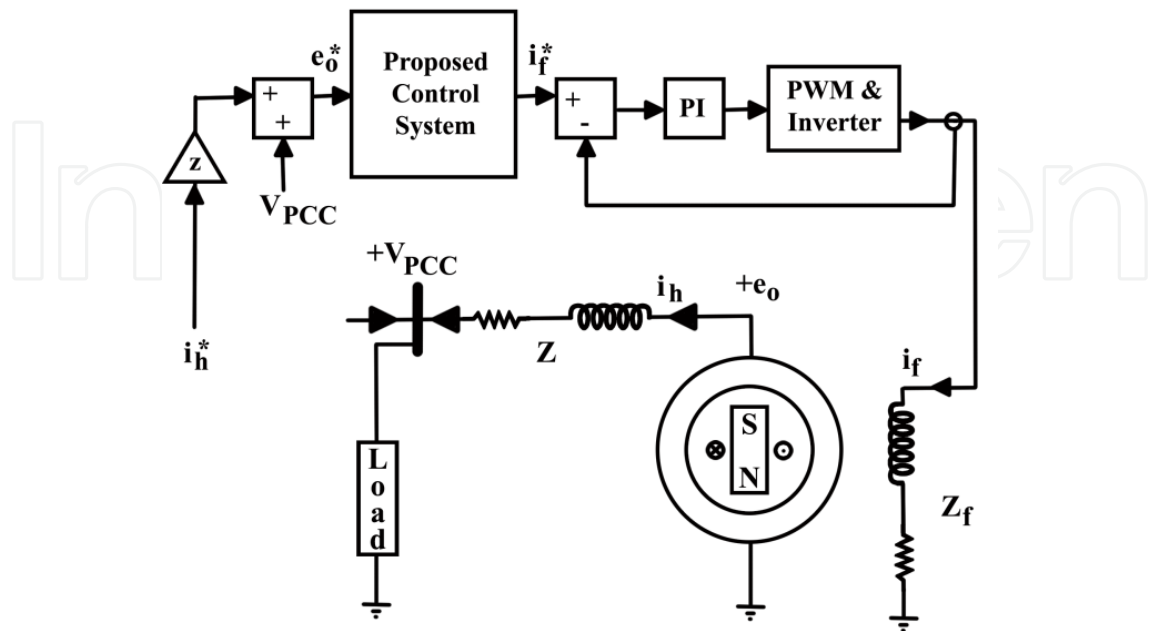


Figure 7. Block diagram of the proposed active filter control

voltage harmonic condition, utility voltages have harmonic and negative sequence components between 0.05 s and 0.2 s. Also, for the investigation of the proposed control strategy in unbalance condition, magnitude of the first phase voltage is increased to the 1.25 pu between 0.05 s and 0.1 s and decreased to the 0.75 pu between 0.15 s to 0.2 s. Table 1, shows the utility voltage harmonic and sequence parameters data and Table 2, shows the load power and voltage parameters. A number of selected simulation results will be showed further.

Voltage Order	Sequence	Magnitude (pu)	Phase Angle (deg)
5	1	0.12	-45
3	2	0.1	0

Table 1. Utility voltage harmonic and sequence parameters data

Load	Nominal Power (kVA)	Nominal Voltage (RMS, L-L)
Linear	10	380V
Non linear	5	380V

Table 2. Load power and voltage parameters data

Figure 9, shows the source side voltage of phase 1. Figure 10, shows the compensator voltage of phase 1. Figure 11, shows load side voltage of phase 1. Figure 12, shows the load side current of phase 1. Figure 13, shows the CCS current of phase 1 that has been supplied by the proposed active filter. Figure 14, shows the PAF of UPQC current of phase 1. Figure 15, shows the source side current of phase 1. Figure 16, shows the field current of the proposed harmonic filter. Figure 17 and 18 show source voltage and load voltage frequency spectrum, respectively. Figure 19 and 20 show load current and source current frequency spectrum, respectively. Figure 21 and 22 show CCS and PAF frequency spectrum, respectively. Table 3 shows THDs of source and load voltages and currents. Load voltage and source current harmonics have been compensated satisfactory.

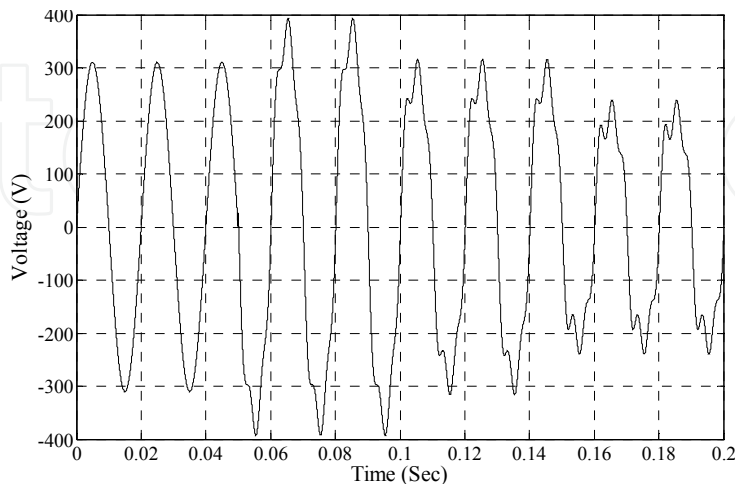


Figure 9. Source side voltage of phase 1 (swell has been occurred between 0.05 and 0.1 sec and sag has been occurred between 0.15 and 0.2 sec. Also, harmonics of positive and negative sequences have been concluded between 0.05 to 0.2 sec)

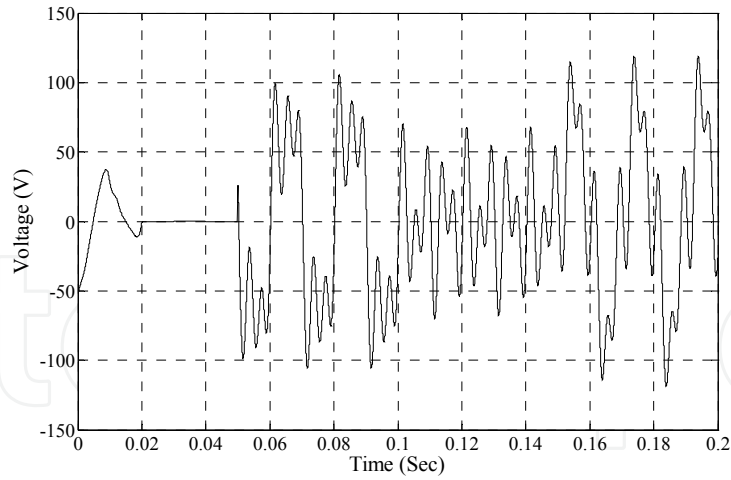


Figure 10. Compensator voltage of phase 1 (compensator voltage has been determined for the sag, swell, negative sequence and harmonics improvement)

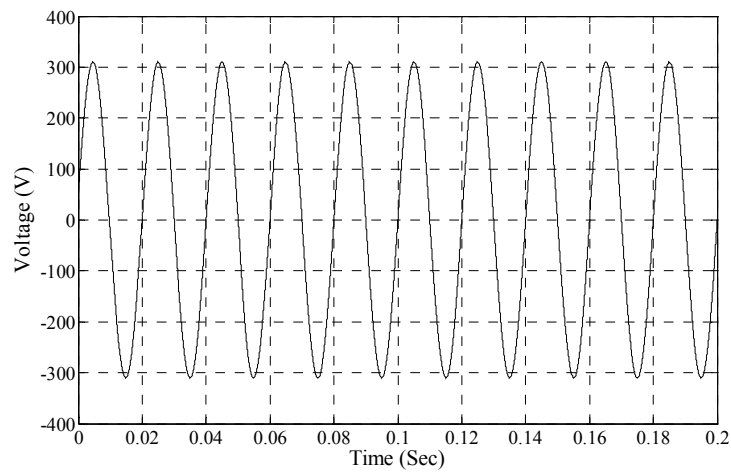


Figure 11. Load side voltage of phase 1 (sag, swell, harmonics, positive and negative sequences have been canceled)

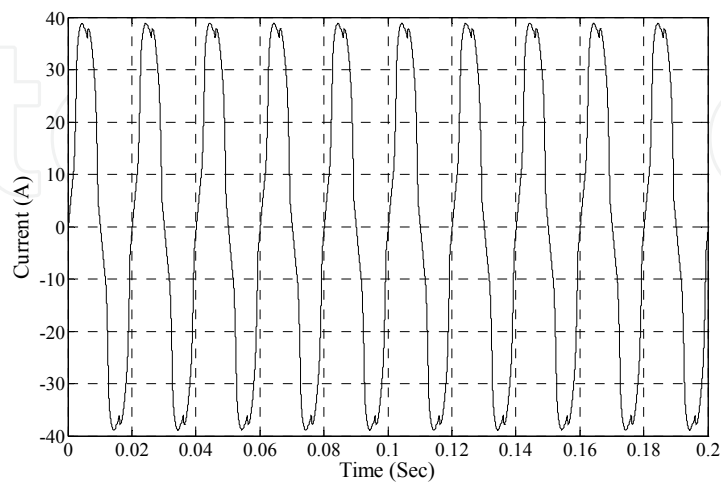


Figure 12. Load side current of phase 1 (it is harmonized. It should be noticed that this current has been calculated after the voltage compensation and thus voltage unbalance has not been transmitted to the current)

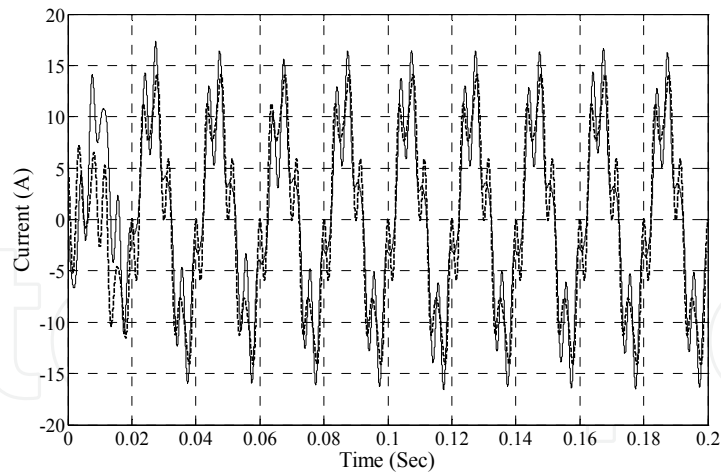


Figure 13. Proposed CCS current of phase 1 (this current has been injected to the grid by the electromechanical active filter. The solid line shows output current of filter and dotted line shows desired current of filter)

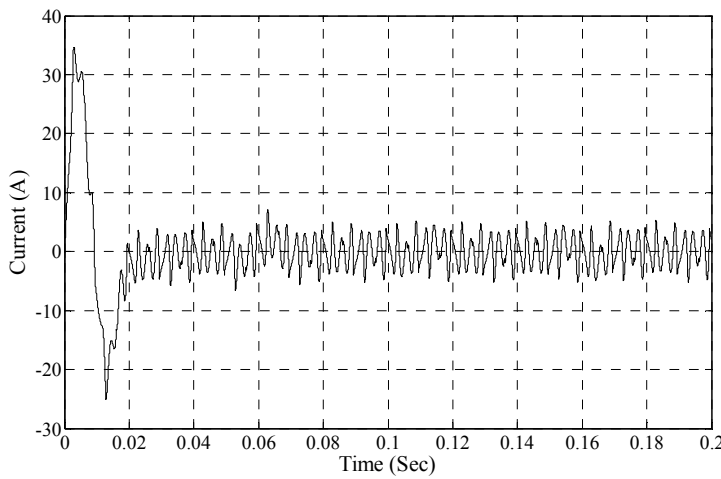


Figure 14. PAF of UPQC current of phase 1 (this current has been injected to the grid by the parallel active filter of UPQC)

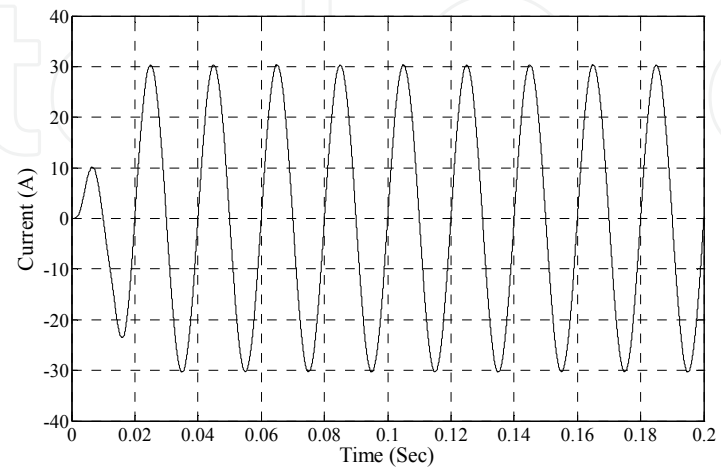


Figure 15. Source side current of phase 1 (harmonics and reactive components of load current have been canceled)

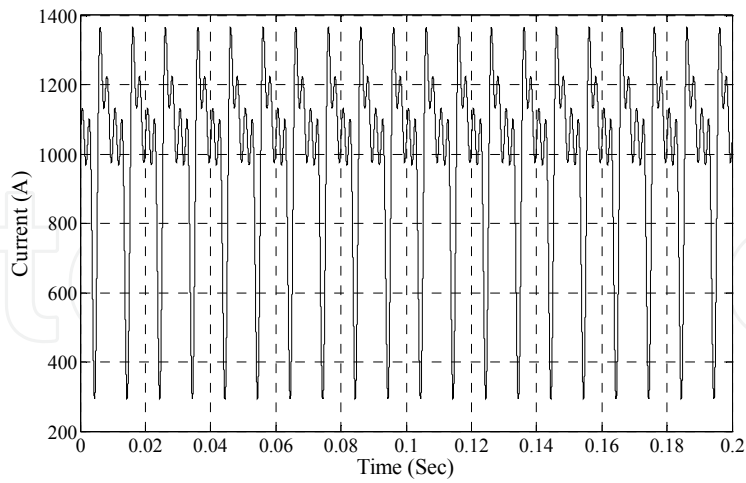


Figure 16. Field current of proposed harmonic filter (field current is controlled for the load active, reactive and harmonic current compensation)

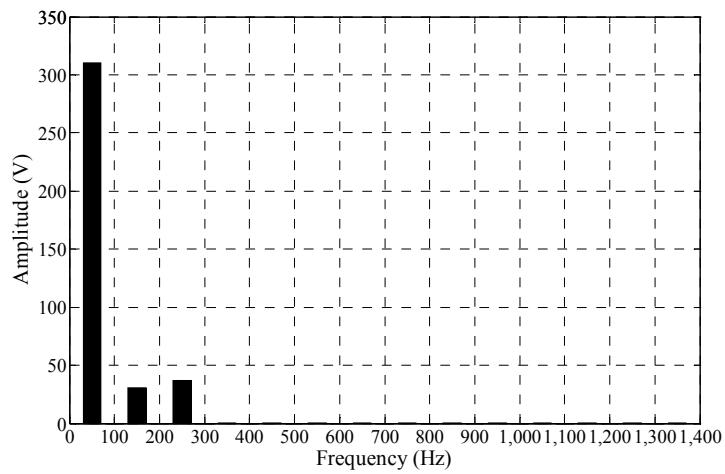


Figure 17. Source side voltage frequency spectrum

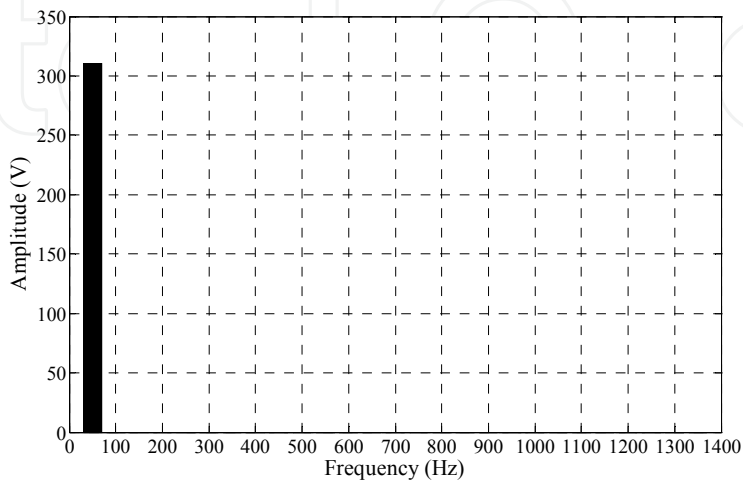


Figure 18. Load side voltage frequency spectrum

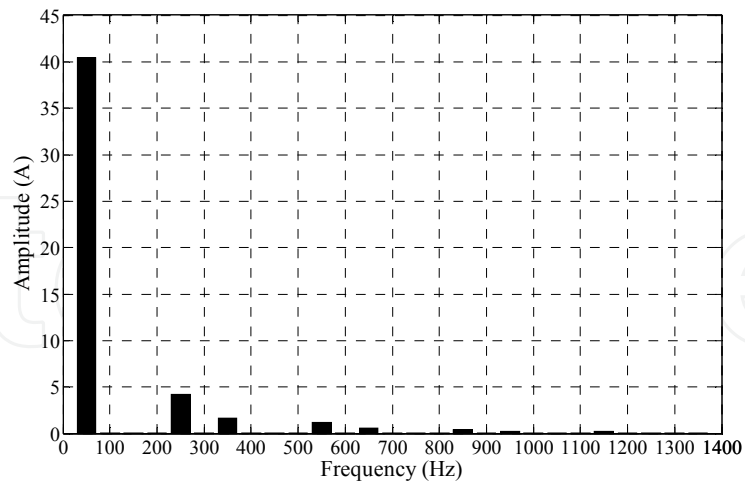


Figure 19. Load side current frequency spectrum

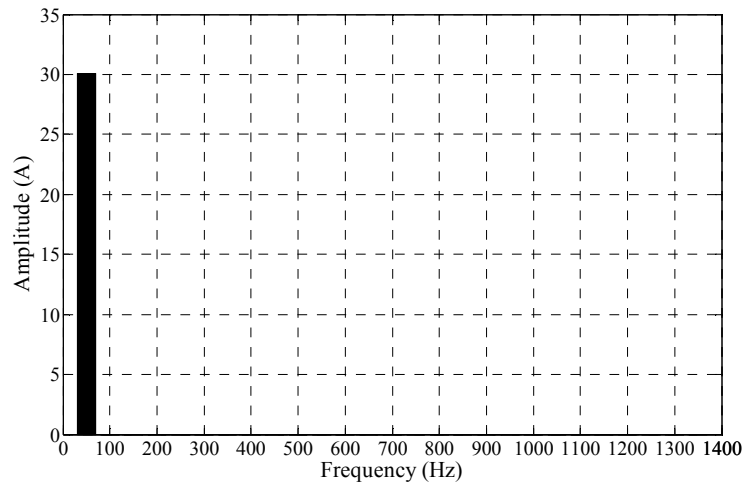


Figure 20. Source side current frequency spectrum

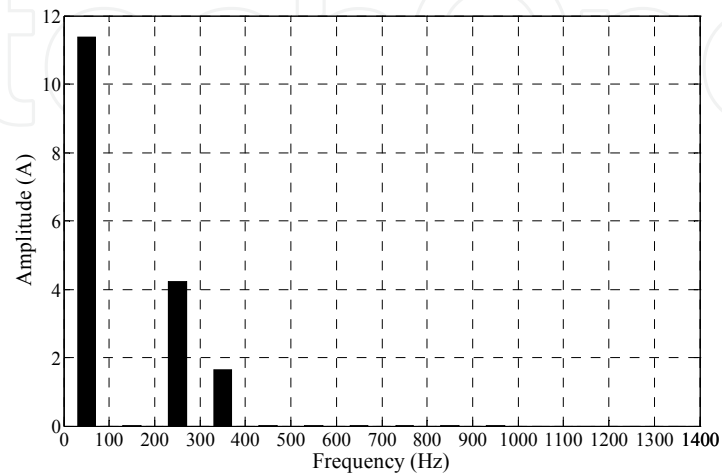


Figure 21. Proposed current controlled system frequency spectrum

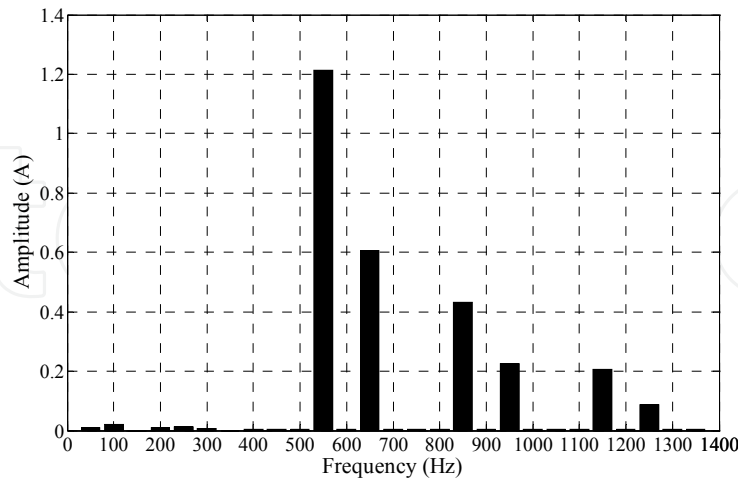


Figure 22. Parallel active filter frequency spectrum

V_s THD	I_L THD	V_L THD	I_s THD
0.1561	0.1179	.001	.0012

Table 3. Total Harmonic Distortion (THD)

7. Conclusions

It is known that use of small synchronous generators in distributed generated networks can reduce transmitted active and reactive powers from the main source and consequently line losses. In this research power quality compensation was done by composition of UPQC and synchronous generators as electromechanical active filter. In other word, by proper determination and control of synchronous generator field current it could be used as controlled current source for power quality compensation. This was for reduction of UPQC power rating in the distributed generated networks. Also, an algorithm was investigated for the determination of the reference field current. Proposed CCS modeling was implemented based on the mentioned related algorithm in MATLAB software. Control strategy had three instantaneously stages. Voltage harmonics were compensated by SAF of the UPQC. Current harmonics with higher order than 7 were compensated by PAF of the UPQC. Lower order current harmonics, load reactive power and a part of load active power were compensated by the proposed controlled current source. Total harmonic distortion of load voltage before compensation was 0.15 which was reduced to almost zero after compensation. Also, total harmonic distortion of the source current before compensation was 0.12 which was reduced to almost zero after compensation.

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