

The Effect of Distribution Network on the Annual Energy Yield and Economic Performance of Residential PV Systems under High Penetration

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Abstract

1 Technological advances, environmental awareness and, in several countries (including the
2 UK), financial incentives lead to the adoption of PV (photovoltaic) systems. Economic
3 viability, an important consideration for investment in residential PV, is dependent on the
4 annual energy yield which is affected by distribution network based factors such as point of
5 connection to network, network hosting capacity, load profiles etc. in addition to the climate
6 of the location. A computational algorithm easy on resources is developed in this work to
7 evaluate the effects of distribution network on the annual energy yield of residential PV
8 systems under scenarios of increasing PV penetration. A case study was conducted for
9 residential PV systems in Newcastle upon Tyne with a generic UK distribution network
10 model. Results identified penetration levels at which PV generation curtailment would occur
11 as a consequence of network voltage rise beyond grid limits and the variation in the
12 percentage of annual energy yield curtailed among the systems connected to the network.
13 The volatility of economic performance of the systems depending on its location within the
14 network is also analysed. The study also looked at the impact of the resolution of PV
15 generation profiles on energy yield estimates and consequently economic performance.

Keywords

PV systems; curtailment; generation profile; energy yield; grid-connected; load profile

1. Introduction

16 Governments across the world are ambitiously focussing on solar energy exploitation. This is
17 mainly due to climate change, CO₂ emission reduction targets and consequent renewable
18 energy obligations such as the European 20/20/20 targets. To drive installation of PV
19 systems, governments provide financial incentives to PV system owners as the adoption of

20 the technology still requires some market support. In the UK, the government Feed-in-Tariff
21 (FIT) has supported the development of grid-connected distributed (micro) PV generation,
22 with the majority of such installations being residential [1]. For every unit of electricity
23 generated by a PV system the FIT scheme provides the system owners a price which is
24 between 1 and 2 times the per unit price of electricity. In the case of a residential owner
25 installing a PV system, the system meets all or part of their energy demand and exports any
26 surplus energy available to the grid subject to the customer's contractual agreement with the
27 distribution system operator. For residential PV system owners, the economic performance
28 of the system with respect to their electricity costs is an important factor which influences the
29 adoption of PV systems.

1.1 Significance of annual energy yield estimates in economic analysis of PV systems

30 Levelised cost of energy (LCOE) is a common parameter used for financial comparison of
31 renewable energy systems and evaluation of their economic viability. It is defined as the ratio
32 of annualised life time revenue (less costs) from PV generation to the annualised life time
33 energy yield from the PV system [2, 3]. The annual revenue from the system is dependent
34 on the energy generated. Net present value (NPV) is another parameter commonly used to
35 assess the long-term viability of renewable energy systems [3]. It is defined as the net
36 discounted cash flow over the system lifetime. It is numerically the same as the numerator of
37 LCOE. Both LCOE and NPV consider the financial returns over the system lifetime i.e. the
38 long term benefits. They look at PV generation alone without consideration of demand. As
39 such these parameters are particularly useful for large commercial systems, such as solar
40 farms, where profitability is expected in the long-term (PV system ownership is similar to that
41 of a conventional generating plant) and local demand profile is not relevant.

42 *Prosumer (Producer and consumer)* is a term that can be used to describe a residential
43 consumer installing a grid-connected PV system [4]. For residential prosumers, near-term
44 economic benefits from meeting all or some of their demand through their on-site PV
45 generation is as important as the long-term benefits. For countries where the feed-in-tariff is
46 implemented near-term economic benefits can be assessed by Prosumer Electricity Unit
47 Cost (PEUC), a parameter previously introduced by the authors [4], which is defined as:

$$48 \quad PEUC = \frac{TAC+GP-FITR1-FITR2}{TEC} \quad (1)$$

49 Where TAC is the total annual cost of the system which is composed of annualised
50 investment and operation and maintenance costs; GP is the annual cost of electricity
51 purchased from the grid by the prosumer; FITR1 and FITR2 are the FIT incomes that the
52 prosumer receives for PV generation and export of surplus generation to the grid,

53 respectively; TEC is the total energy consumed by the prosumer annually. In the PEUC
54 definition near-term is defined as the first year of operation. Evidently, both the near-term
55 and the long-term financial returns from a PV system, assessed in terms of PEUC and NPV
56 or LCOE respectively, depend on the energy yield from the system. A variation in the energy
57 yield will alter the economic performance of the system and consequently the investment
58 attractiveness of PV systems to possible prosumers.

1.2 Impact of grid integration on annual energy yield

59 Grid integration of residential PV systems is a multifaceted problem involving the electricity
60 distribution network operator (DNO), PV system, the prosumer and the policy regulator. The
61 primary technical objective of the DNO is to deliver high-quality, safe, and reliable electric
62 power to its customers (residential, industrial, commercial, etc.). Distribution networks were
63 originally developed on the assumption that electricity flows in one direction, from the
64 generation side (usually large power plants) to the load side. Distributed Generation (DG)
65 technologies like PV systems are connected to the distribution side of the power network
66 and this may result in a reverse power flow (i.e. in a direction opposite to that of the
67 conventional power flow). The impacts of integrating PV to the grid can be twofold: the first is
68 the impact of PV systems on the grid performance and the second is the impact of the grid
69 events (including those caused by PV systems) on the performance of PV systems. Many
70 researchers have looked at the impact of PV systems on the grid in terms of voltage
71 regulation, losses, harmonics and resonance, fault levels and protection, stability etc. [5].
72 However, the effects of grid events on PV system performance (and hence energy yield) are
73 often underestimated [6].

74 The energy yield from a grid connected PV system depends on the distribution network
75 capacity, the demand profiles and the penetration level of PV or other renewables in the
76 network in addition to the meteorological conditions [7]. As the level of PV penetration
77 increases, at times of high generation and low demand network voltage may rise beyond the
78 statutory limit due to reverse power flow [8]. In the UK, Engineering Recommendation G83/1
79 requires that PV systems connected to the low voltage (LV) distribution networks are
80 disconnected from the grid when the voltage at the point of their connection to the LV
81 network exceeds 1.1 p.u. [9]. The disconnection requirements vary amongst different
82 countries, for example in Germany conventional generation currently has to yield in favour of
83 renewable energy. A voltage rise will therefore result in curtailing of PV generation and in so
84 doing reduce the PV energy yield.

85 A summary of the factors that affect PV energy curtailment is given in Fig. 1. The energy
86 capture from a grid connected PV system and consequently curtailment depends on the

87 inverter and the network capacities. PV inverters in westerly climates like that of the UK are
 88 often de-rated to reduce costs and improve efficiency as the modules generate their peak
 89 kW output only for a short time during the entire year [10]. The reliability of the inverter
 90 technology also influences the energy yield. At any instant the original network installed
 91 capacity may not be fully available to host PV generation. The capacity will depend on the
 92 topology of the network and the demand, the presence of other DGs and their generation
 93 and the presence of active network control elements such as on load tap changing
 94 transformers and their operation.

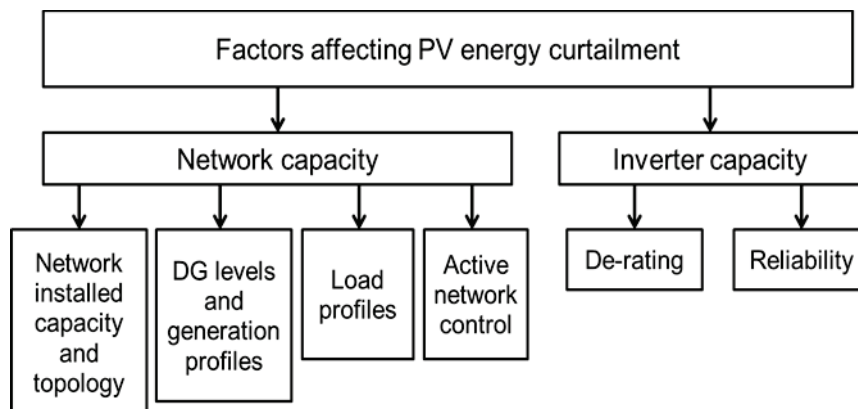


Fig. 1 Factors affecting PV energy curtailment

95 Previous studies have considered the impact of meteorological conditions on the energy
 96 yield of PV systems [11] and the impact of PV systems on the grid operation. However, an
 97 assessment of the impact of grid events on the PV system in the context of energy yield has
 98 not previously been undertaken.

1. 3. Development of an algorithm to estimate PV energy yield under grid-connected operation

99 The problem of estimating renewable energy curtailment under a high level of penetration is
 100 an important one and has been discussed in [12] which looked at the wind energy
 101 curtailment in Ireland. As the PV penetration in the UK has grown at a fast rate since the
 102 introduction of feed-in tariffs in 2010, there is a need for development of methodologies to
 103 investigate the impact of the distribution network on the annual energy yield from PV
 104 systems. There needs to be an algorithm which takes into account PV generation and
 105 prosumer load profiles. For the benefit of potential PV prosumers and decision makers
 106 (possible end users) the algorithm should be (1) efficient in terms of computational
 107 resources, (2) easy to implement, (3) able to consider a range of PV penetration scenarios

108 and (4) able to deal with PV generation and prosumer load profiles having different
109 resolutions.

110 Fig. 2 shows a block diagram of the algorithm proposed to meet these targets. For the same
111 network, different scenarios can be simulated by varying the PV penetration level, demand
112 profile and PV generation profiles. PV generation profiles, network configuration and
113 demand profiles are the inputs to the algorithm. Voltage profiles for all nodes of the network,
114 for the PV penetration level considered, are calculated by the algorithm based on load flow.
115 PV systems are required to shutdown at nodes where voltage limits are violated, which
116 results in curtailment of PV energy. In the next step of the algorithm, nodes with voltage limit
117 violations are identified and PV energy curtailment is quantified. The energy yield estimates
118 are then determined, for PV systems at all nodes, by subtracting their respective curtailment
119 from the energy yield.

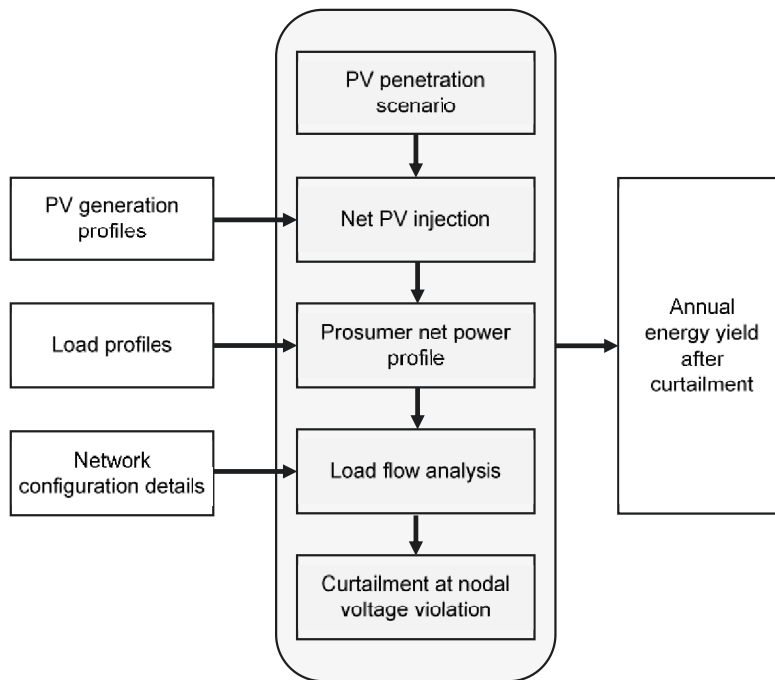


Fig. 2 Proposed energy yield estimation algorithm

1.4 Aims

120 This study aims to evaluate the effect of distribution network on the annual energy yield and
121 economic performance of residential PV systems under increasing PV penetration levels; a
122 case study was created for Newcastle upon Tyne with a generic UK distribution network
123 model. With the aid of the proposed energy yield estimation algorithm this study aims to: (1)
124 identify penetration levels at which PV generation curtailment as a consequence of network

125 voltage rise beyond grid limits occurred, (2) analyse the variation in the percentage of annual
126 energy yield curtailed among the systems connected to the network, (3) investigate the
127 volatility of economic performance of the systems depending on their location within the
128 network (nodal sensitivity), and (4) evaluate the impact of the resolution of PV generation
129 profiles (in techno-economical terms, a statistical analysis is not intended) on energy yield
130 estimates and consequently economic performance for the case study created for Newcastle
131 upon Tyne.

2. Research Methodology

2.1 PV system design and simulation

132 The UK government promotes the adoption of PV systems by means of the Feed-in Tariff
133 (FIT) scheme for systems below 50 kW. FIT is a two-part incentive payment for energy
134 generated by PV systems. A generation tariff is paid for the entire PV energy generated
135 while an export tariff is paid only for energy exported to the grid. The average installed
136 capacity of residential PV systems under the highest FIT category is about 3 kW [13] and
137 therefore, this size was chosen in this study for ease of simulation. This assumption does not
138 affect the direction of this study and the conclusions. The module technology chosen is
139 crystalline silicon since it is the most mature PV technology and has a market share of 80-
140 90% [14]. The system configuration chosen is twelve 250 W poly-crystalline modules (3 kW
141 in total) connected in series to a 2.5 kVA inverter.

142 Typical PV systems were modelled in PVSyst [15], for simulating hourly PV energy outputs
143 for a typical year and thus determining the annual PV generation. As it is the most up-to-date
144 public domain database for Europe, PVGIS climate-SAF was selected as the reference solar
145 database for the UK [16]. The simulation studies were based on the following assumptions:
146 (1) all systems are of the same size and technology, (2) all systems have optimum design for
147 the location i.e. the system has optimum tilt, south facing array and optimum inverter to array
148 de-rating, (3) the effect of shadowing is not considered and (4) storage is not considered.

2.2 Prosumer's demand

149 The electricity demand of a residential consumer depends on a number of factors, such as
150 the number of occupants at the residence, age, lifestyle habits and the quantity and nature of
151 electrical devices [17]. A smart meter electricity trial was undertaken in the North-East of UK
152 (2012-14) as part the Customer Led Network Revolution (CLNR) project [18]. Hi-resolution
153 metering was conducted at selected customer premises. The resulting load profile data sets
154 are free to download from the project website [18]. Since the residential type load profile

155 data from CLNR project is representative of different residential house types, family sizes
156 and occupancy patterns, they were used as the prosumer load profile data for this study.
157 The authors trust the data to be of sufficient accuracy. As it is not the focus of this work an
158 uncertainty analysis on the data was not considered. However, the impact data uncertainty
159 could have on the results will be discussed in section 3.2.

2.3. Network Modelling

160 The typical UK distribution network model [19] used is shown in Fig. 3. A 33/11 kV
161 substation with two 15 MVA transformers supplies six 11 kV outgoing feeders and each 11
162 kV feeder in turn supplies eight 11/0.4 kV substations. To simplify the analysis, only one 400
163 V feeder from an 11/0.4 kV substation, supplying 384 houses through four 400 V outgoing
164 radial feeders, was modelled in detail. The other feeders together with their connected loads
165 were represented as individual lumped loads connected to the respective 11/0.4 kV
166 substations. Therefore, the total load connected to an 11 kV feeder is equivalent to that of
167 3072 ($= 8 \times 384$) houses and the total load supplied by the 33/11 kV substation is equivalent
168 to that of 18432 ($= 6 \times 3072$) houses.

2.4. Load flow

169 A voltage rise beyond grid limits results in the curtailment of PV generation at a node. In
170 order to calculate the voltages at all nodes of the distribution network model considered for a
171 particular load/ generation condition it is essential to incorporate a suitable load flow method
172 in the energy yield estimation algorithm. Considering daily PV generation / load profiles at a
173 resolution of 30 minutes, there would be 48 load/ generation states which translates to
174 running the load flow 48 times. For 365 days (i.e. for the annual energy estimate), at a daily
175 resolution of 30 minutes load flow has to be run 17520 ($= 365 \times 48$) times. In practice, the
176 available resolution of PV generation and load profile may not be as high. However, the
177 number of load flow runs required may still might be in thousands. For this reason, it is
178 necessary to have a simple and computationally efficient load flow method. Because of its
179 flexibility and ease of use MATLAB/Simulink was chosen for modelling. Analysis of the
180 dynamic variation of PV penetration at select nodes was not considered in this work as it is a
181 much larger topic and most literature [20] in this research area point to the need of intelligent
182 mechanisms for the choosing which PV system should be curtailed.

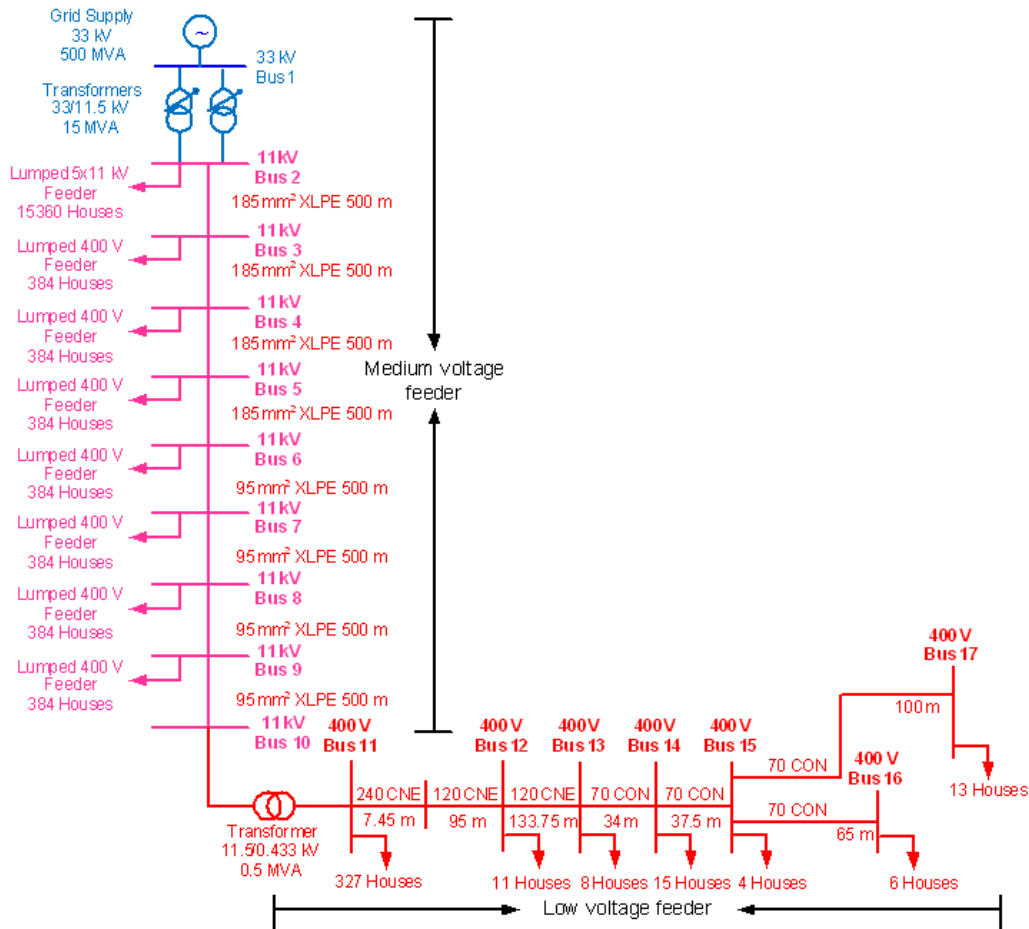


Fig. 3 Typical UK distribution network with one LV feeder shown in detail [19]

2.4.1 Simulink model

183 Initially the model of the distribution network as described in section 2.3 was built in
 184 Simulink. Load profile and PV generation profile for a single summer day from [21] having a
 185 resolution of 1 hour was used to observe the computation time taken. Given the resolution,
 186 assuming every house in the network has a PV system, 24 simulation runs were required.
 187 For an Intel core i7 2.2 GHz computer with 8GB of RAM running MATLAB/Simulink 2015,
 188 simulations took between 1 and 3 minutes depending on prosumer's net power injection for
 189 that run. It took 28 minutes to simulate the entire day. Assuming the same daily duration it
 190 was estimated that it will take 170 hours and 20 minutes to simulate a complete year so that
 191 annual energy yield post any curtailment can be calculated.

2.4.2 MATLAB distribution load flow

192 In order to reduce the computation time, and to able to consider a range of PV penetration
 193 scenarios in parallel a program was written in MATLAB. The Distflow distribution load flow
 194 algorithm for radial networks [22, 23] was chosen. As the mitigation of unbalance is a key

195 step dealt with in the power distribution planning process, a balanced system is assumed, so
 196 a “Per Phase” analysis was used. However the magnitude of unbalance and its propagation
 197 will be For a radial distribution network comprising of n buses as shown in Fig. 4, Distflow
 198 involves the following recursive formula to find the active power, reactive power and voltage
 199 at each branch on the feeder [22]:

$$200 \quad P_{i+1} = P_i - r_{i+1} \frac{P_i^2 + Q_i^2}{V_i^2} - P_{Li+1} \quad (2)$$

$$201 \quad Q_{i+1} = Q_i - x_{i+1} \frac{P_i^2 + Q_i^2}{V_i^2} - Q_{Li+1} \quad (3)$$

$$202 \quad V_{i+1}^2 = V_i^2 - 2(r_{i+1}P_i + x_{i+1}Q_i) + \frac{(r_{i+1}^2 + x_{i+1}^2)(P_i^2 + Q_i^2)}{V_i^2} \quad (4)$$

203 Where P_i , Q_i are the active and reactive power flows at the sending end of bus $i+1$, V_i the
 204 magnitude of the bus voltage at node i . Lines are represented by series resistance r and
 205 reactance x . P_L and Q_L are the active and reactive power consumed by the load at the bus. It
 206 is assumed that the substation bus voltage V_0 is always constant.

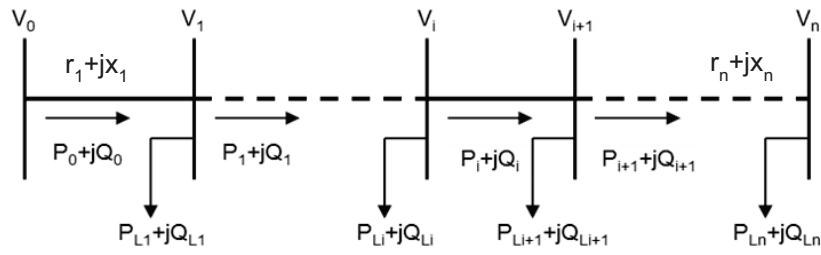


Fig 4. Representative diagram of radial distribution network parameters

207 The MATLAB program developed was run on the same computer for the single summer
 208 day’s load and PV generation conditions described (for observing the computation time) in
 209 section 2.4.1. The simulation run took less than 5 seconds. Fig. 5 shows the correlation
 210 between the Simulink model and the MATLAB algorithm for the 24 hourly voltages at the
 211 most sensitive node (bus 17). The value of R^2 coefficient was 0.83 indicating a very good
 212 agreement.

2. 5. Post-Curtailment Energy Yield Estimation (PCEYE) algorithm

213 The computational sequence for scenario based post-curtailment annual energy yield
 214 estimation is as depicted in Fig. 6. Distribution network parameters, load profiles and PV
 215 generation profiles are the inputs to the algorithm.

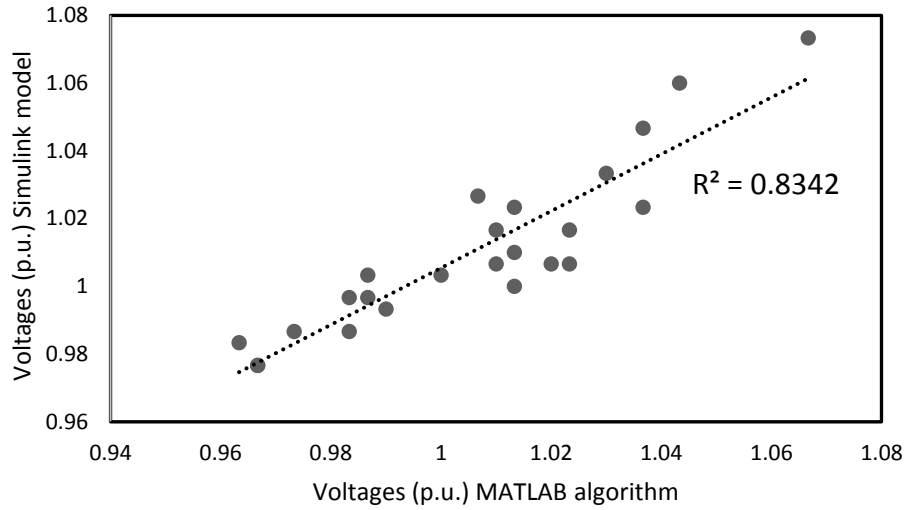


Fig. 5 Correlation between the distribution network voltages obtained using the Simulink model and the MATLAB algorithm

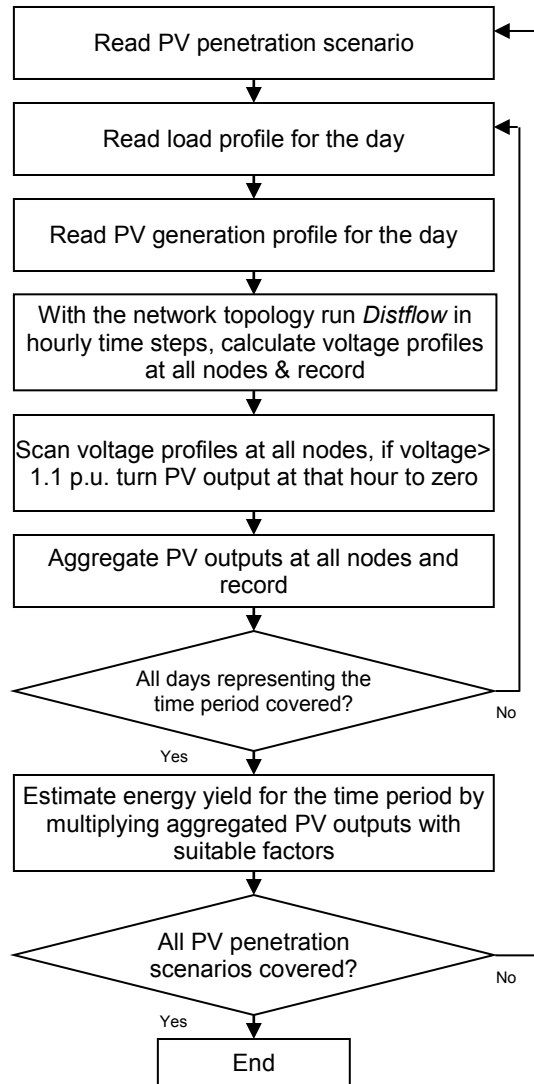


Fig. 6 A flowchart of the post-curtailment energy yield estimation algorithm

216 Load profiles are assigned to buses based on the number of customers at the bus. PV
 217 generation is assigned according to the PV penetration scenario. Voltages at different nodes
 218 of the distribution network corresponding to the PV penetration scenarios are then
 219 calculated. A PV power curtailment event was considered when the voltage rose beyond the
 220 statutory limit (1.1 p.u.). The calculation is performed for all representative days of the time
 221 period, which can be in multiples of a day e.g. a day, a week, a year etc. Losses in PV
 222 system energy yield during the time period considered, due to power curtailment in response
 223 to voltage rise under the operating scenario, is estimated by applying suitable multiplication
 224 factors. There are two multiplication factors: The first one is the number of days of the time
 225 period with the specified load profile and second is the number of days of the time period
 226 with the specified PV generation profile.

227 At the end of the *Distflow* (for every hour), the results of voltages at all nodes are checked, if
 228 any of them is found to exceed 1.1 p. u., the PV generation at that node for that hour is
 229 counted as zero while calculating the daily energy yield of a PV system at that node. To
 230 produce an estimate of the annual energy yield post-curtailment, the daily energy yields are
 231 summed and multiplied by suitable factors to form the monthly energy yield. The monthly
 232 energy yields are then summed up to give the annual energy yield. The network's PV
 233 generation hosting capacity, i.e. the penetration level beyond which voltage rise and PV
 234 power curtailment occurs in the studied network, can be estimated by varying the PV
 235 penetration levels at the MV and LV network.

2.6 Economic performance analysis

236 PEUC described in section 1.1 was used in this study to analyse the sensitivity in economic
 237 performance of prosumers' PV systems, depending on their point of connection within the
 238 network. For any scenario considered, the prosumers annual cost of electricity is the product
 239 of their annual electricity demand and PEUC for that scenario. The data used in this work for
 240 economic performance analysis based on sources described in [24] is shown in Table 1.

Table 1. Data for economic performance analysis

Description	Value
System cost (£)	7000
Project term (years)	20
Interest rate (%)	4
Grid electricity price (£/kWh)	0.18
Generation tariff, FIT1 (£/kWh)	0.0432
Export tariff, FIT2 (£/kWh)	0.0491
Prosumer annual energy demand (kWh)	3600

2.7 Scenarios

241 In this study, the level of PV penetration is defined as the ratio of the number of houses with
 242 a PV system to the total number of houses in that section of the distribution network, with
 243 each PV system assumed to be 3 kW in capacity. In order to identify penetration, the levels
 244 at which PV generation curtailment as a consequence of network voltage rise beyond grid
 245 limits occurred and analyse the variation in annual energy yield curtailed among the
 246 systems, the following incremental PV penetration scenarios were considered for the case
 247 study of Newcastle upon Tyne:

- 248 ➤ None of the houses have a PV system; i.e. 0% PV penetration in the network.
- 249 ➤ PV penetration in the 11 kV network and the detailed 400 V feeder increased in
 250 steps of 10% from 10 to 100% as shown in Table 2.

Table 2. PV profile classification for analysis based on temporal resolution

		% PV penetration level in 11kV network									
		10	20	30	40	50	60	70	80	90	100
% PV pnetration level in the detailed 400V feeder	10	S(10,10)	S(10,20)	S(10,30)	S(10,40)	S(10,50)	S(10,60)	S(10,70)	S(10,80)	S(10,90)	S(10,100)
	20	S(20,10)	S(20,20)	S(20,30)	S(20,40)	S(20,50)	S(20,60)	S(20,70)	S(20,80)	S(20,90)	S(20,100)
	30	S(30,10)	S(30,20)	S(30,30)	S(30,40)	S(30,50)	S(30,60)	S(30,70)	S(30,80)	S(30,90)	S(30,100)
	40	S(40,10)	S(40,20)	S(40,30)	S(40,40)	S(40,50)	S(40,60)	S(40,70)	S(40,80)	S(40,90)	S(40,100)
	50	S(50,10)	S(50,20)	S(50,30)	S(50,40)	S(50,50)	S(50,60)	S(50,70)	S(50,80)	S(50,90)	S(50,100)
	60	S(60,10)	S(60,20)	S(60,30)	S(60,40)	S(60,50)	S(60,60)	S(60,70)	S(60,80)	S(60,90)	S(60,100)
	70	S(70,10)	S(70,20)	S(70,30)	S(70,40)	S(70,50)	S(70,60)	S(70,70)	S(70,80)	S(70,90)	S(70,100)
	80	S(80,10)	S(80,20)	S(80,30)	S(80,40)	S(80,50)	S(80,60)	S(80,70)	S(80,80)	S(80,90)	S(80,100)
	90	S(90,10)	S(90,20)	S(90,30)	S(90,40)	S(90,50)	S(90,60)	S(90,70)	S(90,80)	S(90,90)	S(90,100)
	100	S(100,10)	S(100,20)	S(100,30)	S(100,40)	S(100,50)	S(100,60)	S(100,70)	S(100,80)	S(100,90)	S(100,100)

2.7 Data resolution

251 Most common weather databases used for PV system simulations, such as US Department
 252 of Energy [25], provide one data set per month at an hourly resolution for a typical year. For
 253 load profiles, it is usual to have one data set per season (spring, summer etc.) at an hourly
 254 resolution [4]. However, with the advent of the smart grids movement and consequently
 255 smart metering, the load profile data resolution has started to increase. Monthly data sets
 256 (instead of seasonal) have become available [26]. For CLNR residential customer data sets
 257 there were 7 load profiles with half hourly resolution representing the days of a week for

258 every month of the year. This was the best temporal resolution available for load profiles of
 259 north-east England.

260 Usually, solar data from common weather databases are used as input to PV system
 261 simulation software to generate PV generation profiles (which are representative of the
 262 monthly average). However, for this study the climate-SAF database provided daily solar
 263 data for a typical year. For an optimally designed 3 kW residential grid-connected PV system
 264 in Newcastle upon Tyne, PVSyst [27] simulations resulted in 365 realistic daily PV
 265 generation profiles at an hourly resolution. To represent the temporal resolution of common
 266 available PV generation profiles monthly averaged PV generation profiles were created by
 267 averaging PVSyst hourly outputs. Thus, to investigate the impact of temporal resolution of
 268 PV generation profiles on post-curtailment energy yield estimates, PV generation profiles
 269 were classified into two types as shown in Table 3. A number of research studies have been
 270 published on the impact of temporal resolution of input data on renewable energy
 271 simulations [28]. However, they were all statistical analyses and the focus was not on energy
 272 yield and the impact of the grid on this.

Table 3. PV profile classification and data resolution

Description	PV data title	No. of PV Generation Profiles	No. of Load Profiles	No. of data points per profile
Base case	Monthly averaged	12	12 x 7 = 84	24
High-res	Daily	365	12 x 7 = 84	24

3. Results and Discussion

273 The use of monthly averaged PV generation profiles was considered as the base case. For
 274 the high-resolution case, i.e. with daily PV generation profiles, simulation and analysis was
 275 conducted based on the insights drawn from the base case.

3.1 Scenarios of PV generation curtailment

276 For the distribution network described in section 2.3, the voltage at each node is calculated
 277 for the base case (with resolution indicated in first row of Table 3). The amount of prosumer
 278 PV energy to be curtailed as consequence of voltage rise above the statutory limit at any
 279 node is then estimated for different PV penetration scenarios based on which post
 280 curtailment annual energy yield estimates were generated. Buses at the far end of the LV
 281 feeder are the most sensitive ones where voltage rise events occurred. Results showed that
 282 voltage rise occurred in the sensitive buses only at very high PV penetration levels of 90% or
 283 greater in both MV (11 kV) and LV network sections. Table 4 shows the PV penetration
 284 scenarios (from Table 1) where a reduction in energy yield occurred due to curtailment. With

285 100% penetration in the MV network, voltage rise was observed in the LV network even
 286 when it had only 30% PV penetration level. This sensitivity arises because of the upstream
 287 PV production and the LV feeder being at the far end of the network. The buses at the end
 288 of the LV feeder numbered 16 and 17 (see Fig. 3) were the most sensitive to changes in PV
 289 penetration levels. This is in agreement with previously published research [29].

Table 4. Base case PV penetration scenarios where curtailment occurred

Sl. No.	Scenario	% PV penetration in MV network	% PV Penetration in LV network
1	S(90,90)	90	90
2	S(90,100)	90	100
3	S(100,30)	100	30
4	S(100,40)	100	40
5	S(100,50)	100	50
6	S(100,60)	100	60
7	S(100,70)	100	70
8	S(100,80)	100	80
9	S(100,90)	100	90
10	S(100,100)	100	100

290 For the year considered in this work, the month of May had the highest average monthly PV
 291 generation for Newcastle. Fig. 7 shows the generation profile of the peak PV generation day
 292 which also occurs in May. High grid voltages occur under low demand conditions. The load
 293 profile for Wednesday in May (when the average demand is lowest) and the monthly
 294 averaged PV generation profile for May is also shown in this figure.

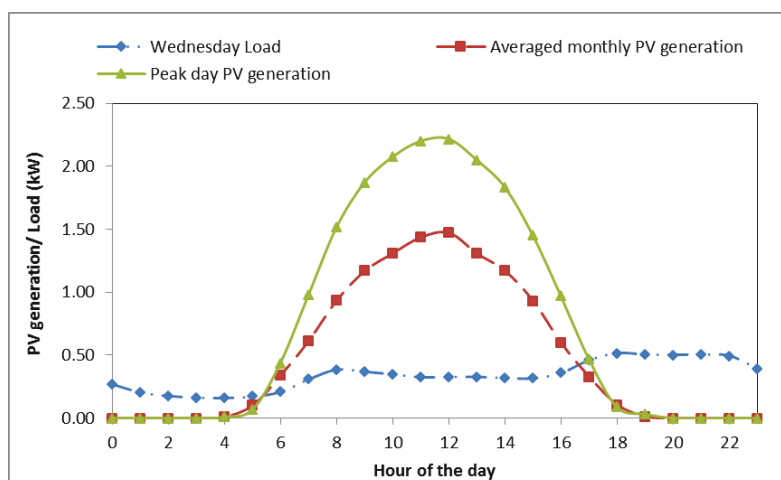


Fig. 7 Profiles of maximum PV generation and minimum demand profiles in the month of May for Newcastle upon Tyne

295 Figs. 8 shows the base case voltage profiles at each node along the LV feeder with 100%
 296 PV penetration in both MV and detailed LV feeders (scenario S(100,100)) for the monthly
 297 averaged PV generation profile and load profile shown in Fig. 7. As mentioned earlier, buses
 298 16 and 17 are the most sensitive buses. Since their simulation results are identical, only bus
 299 17 is mentioned from this point onward. Fig. 9 shows the voltage profile for bus 17 for the
 300 daily PV generation and load profiles shown in Fig.7 for the scenario S(100,100). A variant of
 301 the scenario simulated with the PV penetration at bus 17 set to zero also resulted in the
 302 same voltage profile due to the relatively small number of houses at the bus.

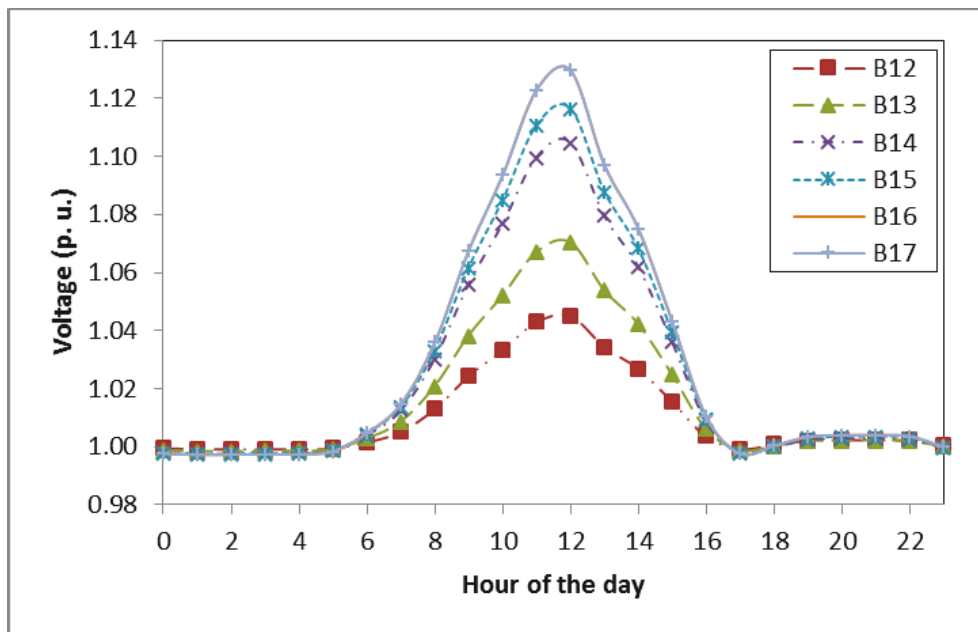


Fig. 8 Voltage profile along the 400 V feeder for an average Wednesday in May for PV penetration scenario S(100,100)¹

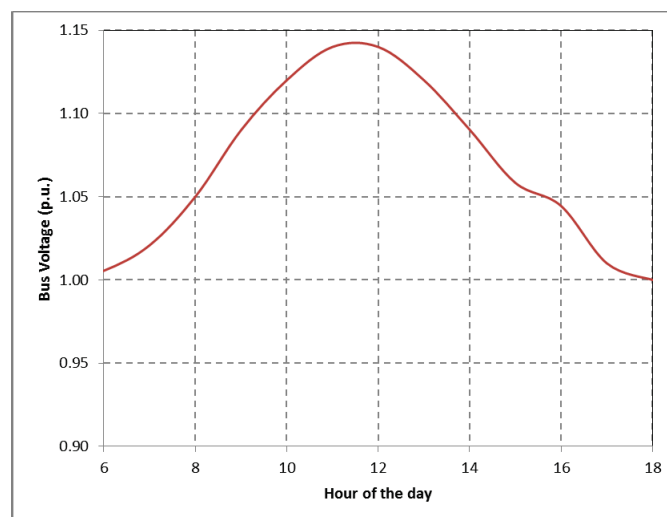


Fig. 9 Voltage profile at the bus 17 with daily PV generation profile

¹ In the legends of Fig 8 'B' is an abbreviation for 'Bus', e.g. B12 stands for Bus12. The voltage profiles of B16 and B17 are coincident.

303 It can be noticed that in both cases the voltage rises above the 1.1 p.u. limit for the scenario
 304 shown. The rise in voltage and the duration of voltage rise is greater with the daily PV
 305 generation profile as can be seen from Fig. 9. It was observed from CLNR load dataset that,
 306 the demand is minimum between 10:00 and 15:00 for most part of the year. Thus, it can be
 307 concluded that, even under lower levels of PV penetration, during peak PV generation days
 308 the chances of voltage rise above statutory limits and consequent PV energy curtailment is
 309 high. Therefore, as for the base case, PCEYE was run to estimate prosumer energy yields
 310 for all scenarios of Table 1 with high-res case PV data. Unlike for the base case, there were
 311 49 PV penetration scenarios (from Table 1) where a reduction in energy yield occurred due
 312 to curtailment as listed in Table 5. For convenience, 7 out of the 49 scenarios, highlighted in
 313 grey in Table 5 were chosen for detailed analysis. These scenarios had the same
 314 penetration level in both the MV and the LV networks. Fig. 10 shows the voltage profiles at
 315 the most sensitive bus (Bus17) for the peak PV generation and low demand day (in May) for
 316 these chosen scenarios. It was noted that voltage rise due to PV generation stays within 1.1
 317 p.u. until the 40% PV penetration level. Beyond 50%, the voltage rises beyond limits and PV
 318 energy curtailment results.

319 It can be noted that the voltage exceeds 1.1 p.u. between 9:00 and 16:00. Without any
 320 control measures like Demand Side Management (DSM), the default setting for PV inverters
 321 is to turn off when node voltage exceeds 1.1 p.u. which will lead to a large PV energy loss
 322 for all PV systems connected at Bus 17 and possibly others. In this case, PV systems at
 323 buses 12-17 were affected by curtailment (unlike buses 14-17 for the base case), with bus
 324 17 being the most severely affected.

Table 5. High-res case PV penetration scenarios where curtailment occurred

		% PV penetration level in 11kV network						
		40	50	60	70	80	90	100
% PV penetration level in the detailed 400V feeder	40	S(40,40)	S(40,50)	S(40,60)	S(40,70)	S(40,80)	S(40,90)	S(40,100)
	50	S(50,40)	S(50,50)	S(50,60)	S(50,70)	S(50,80)	S(50,90)	S(50,100)
	60	S(60,40)	S(60,50)	S(60,60)	S(60,70)	S(60,80)	S(60,90)	S(60,100)
	70	S(70,40)	S(70,50)	S(70,60)	S(70,70)	S(70,80)	S(70,90)	S(70,100)
	80	S(80,40)	S(80,50)	S(80,60)	S(80,70)	S(80,80)	S(80,90)	S(80,100)
	90	S(90,40)	S(90,50)	S(90,60)	S(90,70)	S(90,80)	S(90,90)	S(90,100)
	100	S(100,40)	S(100,50)	S(100,60)	S(100,70)	S(100,80)	S(100,90)	S(100,100)

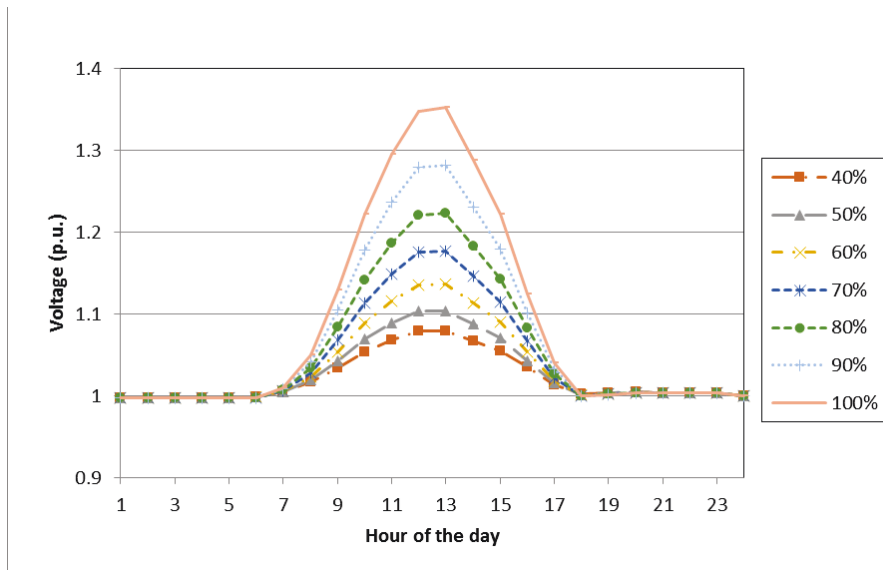


Fig. 10 Voltage profiles at bus 17 for the peak PV generation-low demand day

325 Fig. 11 shows the monthly variation in aggregate PV energy curtailment in the detailed LV
 326 feeder for the 7 PV penetration scenarios chosen for the high-res case. It can be seen that
 327 summer months have higher curtailment, with May having the highest curtailment, while
 328 winter months have generally lower curtailment, with December having the lowest amount of
 329 curtailment.

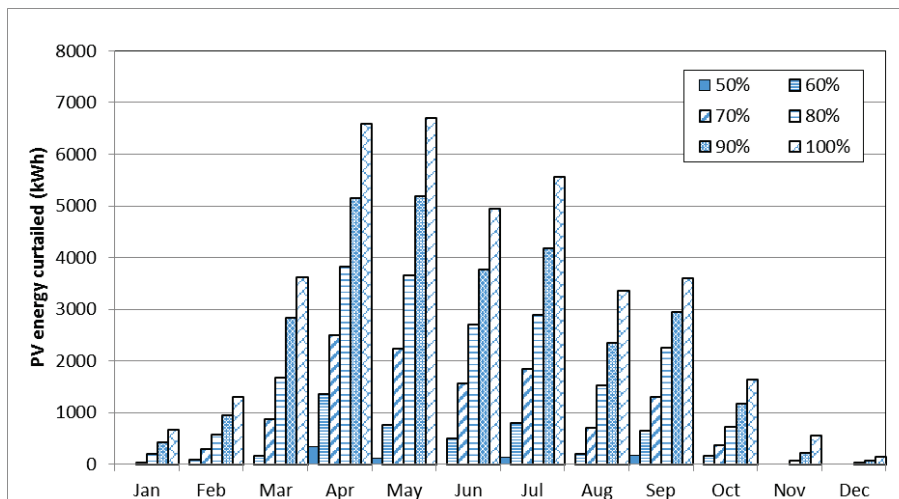


Fig. 11 Monthly variation in aggregate PV energy curtailment in detailed LV feeder

330 3.2 Impact of temporal resolution on curtailment

331 For prosumers located at different nodes on the LV network a curtailment ratio (CR) can be
 332 defined as the ratio of the PCEYE annual energy yield estimates to the un-curtailed energy
 333 yield. The maximum value possible for CR is 1, indicating no curtailment. The PVsyst annual
 334 energy yield for a typical PV system in Newcastle is 2651.3 kWh. Table 6 shows the CRs for

335 the buses where curtailment was observed for the base case. It is observed that for the base
 336 case with monthly averaged PV generation profiles, the annual energy yield estimates would
 337 depict a loss only from Bus 14 towards the end of the LV feeder. The highest loss was
 338 incurred by PV systems at the end of the LV feeder (Bus 16 and Bus 17). PV systems closer
 339 to the MV source in terms of their point of connection in the network had lower losses in
 340 energy yield. This is under the assumption that the On Load Tap Changer (OLTC) operates
 341 to keep the MV substation at constant voltage.

Table 6. Curtailment ratios for the buses with curtailment under different scenarios for the base case

Bus No.\ Scenario	14	15	16	17
S(90,90)	1	1	0.9972	0.9972
S(90,100)	1	1	0.9845	0.9845
S(100,30)	1	1	0.9944	0.9944
S(100,40)	1	1	0.9845	0.9485
S(100,50)	1	1	0.9769	0.9769
S(100,60)	1	0.9944	0.9747	0.9747
S(100,70)	1	0.9845	0.9747	0.9747
S(100,80)	1	0.9769	0.9747	0.9747
S(100,90)	0.9972	0.9747	0.9747	0.9747
S(100,100)	0.9894	0.9747	0.9655	0.9655

342 Since averaging reduces the peaks in the PV generation profiles, using average values
 343 results in lower curtailment and gives smaller values for reduction in energy yield. Therefore,
 344 average PV generation profiles provide the most optimistic energy yield estimates. To
 345 comprehend the impact of averaging, results with averaged PV generation profiles have to
 346 be compared with those with daily PV generation profiles. Table 7 shows the CRs for the
 347 buses where curtailment was observed for the base case. It can be observed that there
 348 is a large difference in CR for 100 % penetration level (scenario S(100,100)). The use of
 349 monthly averaged PV data was showing a loss of energy yield of less than 4% much lesser
 350 than the 39% reduction obtained with daily PV data. Since it is closer to actual operation, the
 351 results with daily high-res data are closer to reality. The high-res CR values with 50% PV
 352 penetration S(50,50) are lower than that for the 90% PV penetration scenario S(90,90)
 353 obtained with base-case (monthly averaged) PV data.

354 The results of the high-res study identify that, with increasing PV penetration levels, the grid
 355 has a significant impact on the energy yield from the PV systems. The annual energy yield
 356 values for the prosumer could be far different from what was provided by the PV system
 357 designer (or installer) at the time of installation despite similar weather conditions. This is an
 358 additional financial risk, one that most prosumers do not consider at the time of investing in

359 PV. The results also point to the impact of temporal resolution of PV data in estimating grid
 360 impacts and consequently investment decisions and policies.

Table 7. Curtailment ratios for the buses with curtailment under different scenarios for the high-res case

Bus No.\ Penetration level	12	13	14	15	16	17
50	1	1	0.9991	0.9973	0.9854	0.9854
60	1	1	0.9764	0.9519	0.9300	0.9300
70	1	0.9973	0.9185	0.8833	0.8434	0.8434
80	1	0.9683	0.8406	0.7982	0.7610	0.7610
90	0.9973	0.9147	0.7564	0.7181	0.6830	0.6830
100	0.9763	0.8362	0.6841	0.6485	0.6107	0.6107

361 Fig. 12 and 13 show the variation in annual aggregate PV energy curtailment in the detailed
 362 LV feeder with increase in PV penetration levels for the base case and the high-res case. It
 363 can be seen that for the case with PV generation profiles having daily temporal resolution,
 364 the network considered was able to host a PV penetration level of up to 40%, beyond which
 365 it needs to resort to curtailing the output from PV systems. The use of monthly averaged PV
 366 generation profiles (base case) was suggestive of a very high network hosting capacity. The
 367 results showed that the network could host PV generation without curtailment even at very
 368 high penetration levels (over 80%). Thus it can be observed that network hosting capacity
 369 estimates using distributed generation data with low temporal resolution (as in the base
 370 case) could be misleading. For the load profiles, the temporal resolution used for this study
 371 was restricted to what was available from the CLNR dataset (84 daily profiles for a year).
 372 However, by using synthetic load profile generation methodologies [30] it is possible to
 373 extend the resolution to 365 days if essential input data required for the methodology are
 374 available. The conclusions drawn from this analysis will not be much different with an
 375 improvement in the accuracy of CLNR data, considering the magnitudes of load profiles,
 376 voltage limits and other network parameters.

3.3 Analysis of economic performance

377 In order to investigate the volatility of economic performance of the systems depending on its
 378 location within the network, PEUC was calculated for prosumers at each bus with CR less
 379 than 1 (i.e. curtailment occurred) for the base case and high-res scenarios previously
 380 discussed. For comparison of the impact of temporal resolution, PEUC and annual cost of
 381 electricity for prosumers at the most sensitive bus (Bus 17) are shown in Table 8 and 9. It
 382 can be observed from Table 9 that there is a significant increase in PEUC with higher
 383 penetration. The use of low resolution data (base case) only shows a slight increase in
 384 PEUC, giving an increase of £15.56 in the prosumer's annual electricity cost even with 100%

385 PV penetration in the network. This is not a significant investment risk and most prosumers
 386 would not be worried. However, an increase of £156.74 (at 100% penetration high-res case)
 387 is a significant investment risk and worry to most prosumers.

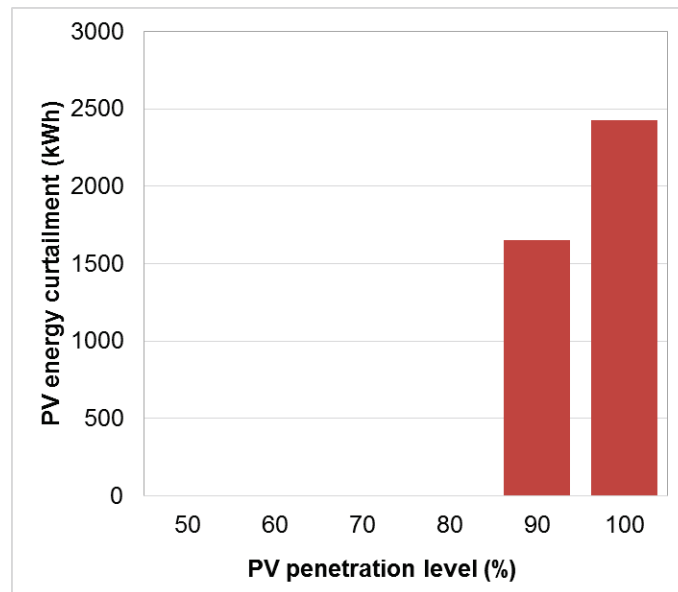


Fig. 12 Annual aggregate PV energy curtailment in detailed LV feeder for the base case

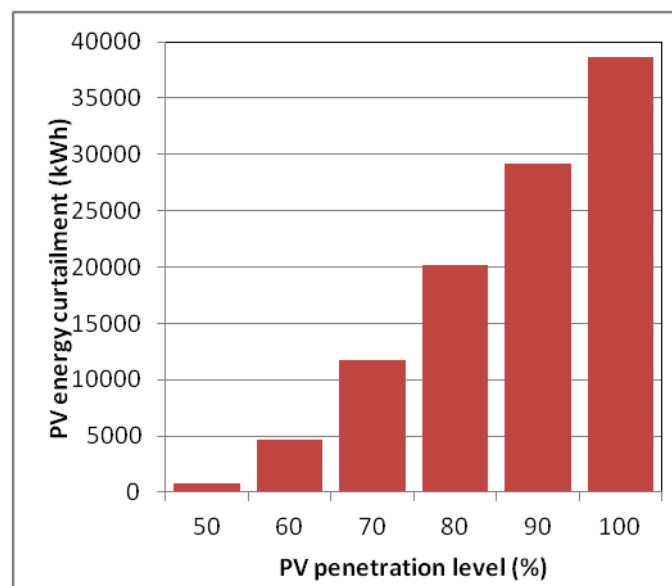


Fig. 13 Annual aggregate PV energy curtailment in detailed LV feeder for the high-res case

Table 8. Base case PEUC and annual electricity cost for prosumers at the most sensitive bus

Sl. No.	Case	Scenario	PEUC (£)	Annual electricity cost (£)
1	No curtailment		0.2055	739.76
2	Lowest curtailment	S(90,90)	0.2058	740.93
3	Highest curtailment	S(100,100)	0.2098	755.32

Table 9. High-res case PEUC and annual electricity cost for prosumers at the most sensitive bus

Sl. No.	Penetration level	PEUC (£)	Annual electricity cost (£)
1	50	0.2072	745.84
2	60	0.2136	769.03
3	70	0.2237	805.24
4	80	0.2333	839.73
5	90	0.2423	872.35
6	100	0.2507	902.58

388 With high PV penetration levels, there is not only an increase in investment risk due to lower
389 income from PV generation but also a disparity in income distribution. Some PV system
390 owners are more susceptible to low return on investment than others. As can be seen from
391 Table 10, the annual electricity cost of prosumers at Bus 16/17 is increased by £156.74
392 whereas for prosumers at Bus 12 the increase is only £3.83. Thus prosumers at the buses
393 farthest from the main substation are the ones most prone to a reduction in income from PV
394 and consequently have higher investment risk. These prosumers have no say in the
395 installation of PV or other DGs upstream. DNOs and policy makers should make policy
396 decisions taking this possible income disparity into account. If data on the impact of the grid
397 on their potential PV outputs are available, prosumers would be able to make a sound
398 decision as to whether or not to invest in a PV system for their home.

Table 10. High-res case PEUC and prosumers annual electricity cost between buses for 100% PV penetration

Bus	PEUC (£)	Annual electricity cost (£)
12	0.2082	749.67
13	0.2245	808.27
14	0.2422	871.88
15	0.2463	886.77
16	0.2507	902.58
17	0.2507	902.58

399 Since FIT income is not received for the energy lost by curtailment, both the long-term and
400 near-term economic viability of the prosumers is affected. This points to the necessity for
401 adequate measures like the use of storage, active voltage control (AVC) [31, 32] and DSM to
402 be put in place to enable the capture of maximum PV energy.

4. Conclusions

403 A computational algorithm easy on resources is developed in this work to evaluate the
404 effects of distribution network on the annual energy yield of residential PV systems under
405 scenarios of increasing PV penetration. Results with high-res PVGIS solar data for the case
406 study of Newcastle, UK showed that, even for low PV penetration levels (50%), during peak

407 PV generation days, the chances of voltage rise above statutory limits and consequent PV
408 energy curtailment is high. This is much different from the curtailment penetration level
409 (90%) predicted with the monthly solar data. The monthly data was also misrepresenting the
410 number of prosumers who would be affected and was suggestive of a very high network
411 hosting capacity.

412 The results of the high-res study also identified that, with increasing PV penetration levels,
413 the prosumers' annual energy yield and annual electricity costs could be far different from
414 what they would have expected for the weather conditions. This is an additional financial
415 risk, one that most prosumers do not consider at the time of investing in PV. There is also a
416 disparity in income distribution, some PV system owners are more susceptible to low return
417 on investment than other. DNOs and policy makers should include this possible income
418 disparity into their policy considerations and should make potential prosumers aware of this
419 disparity before they make investment decisions. In order to improve the economic viability
420 of prosumers affected by curtailment adequate measures like the use of storage, active
421 voltage control and demand side management could be put in place. The PCEYE algorithm
422 can be a valuable tool to investigate the effectiveness of these control measures.

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