

# **Towards the investigation of unsteady control surface aerodynamics**

Dipl.-Ing. Sven Geisbauer

DLR Institute of Aerodynamics and Flow Technology

Transport Aircraft Department

Braunschweig



Knowledge for Tomorrow

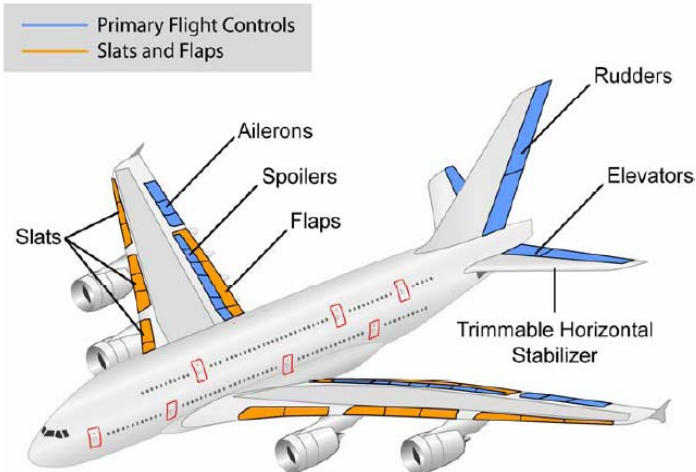
# Outline

- Motivation, objectives and funding
- Spoiler aerodynamics
- Development of a wind tunnel model
- Outlook



# Why focus on control surfaces?

- Long-term vision at DLR: **digital aircraft**, i.e. numerically simulate the aircraft within its entire flight envelope, including manoeuvres
  - Today CFD still mostly applied on cruise and high-lift configurations in steady conditions
  - Manoeuvre simulation requires geometrical representation of (all) control surfaces



# Why focus on control surfaces?

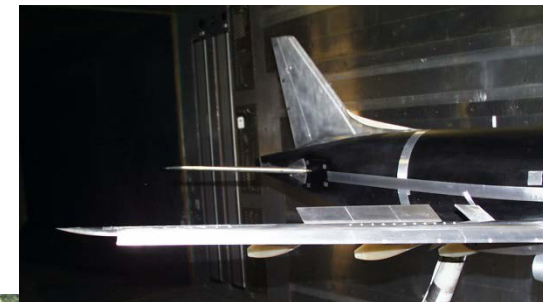
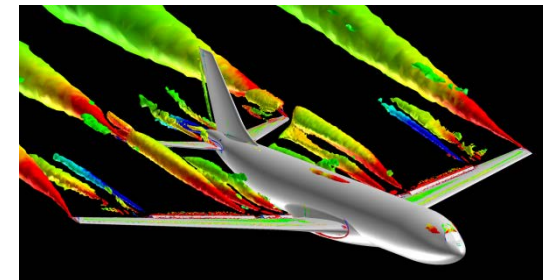
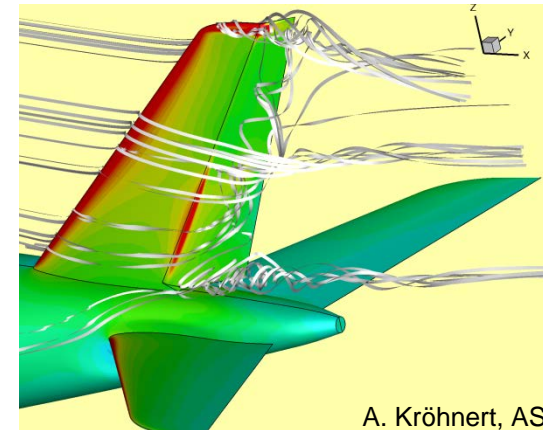
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  - Today CFD still mostly applied on cruise and high-lift configurations in steady conditions
  - Manoeuvre simulation requires geometrical representation of (all) control surfaces
  - Accurate simulation of the time-dependent impact of control surface deflection on the overall aerodynamics of the aircraft required

Deeper insight into control surface aerodynamics and reliable validation data is of high priority!



# Where are we today?

- Growing interest in configurations with deflected control surfaces, both numerically and experimentally
- Examples:
  - High-lift
  - One engine inoperative
  - Emergency descent
  - Loads (re-)distribution
  - Control surface efficiency
- Predominantly static deflections, i.e. dynamic effects not considered yet
- Some control surfaces exhibit a non-linear behaviour, associated with time lags and adverse effects

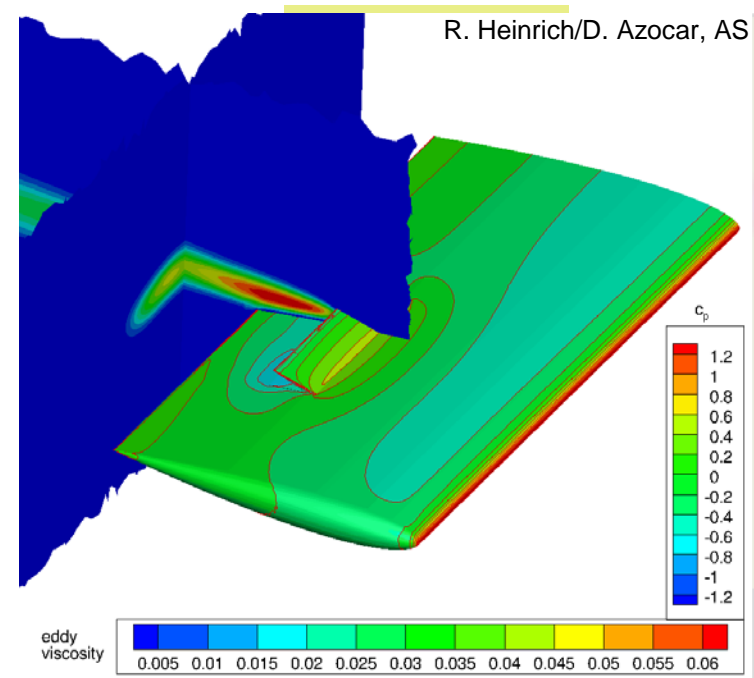
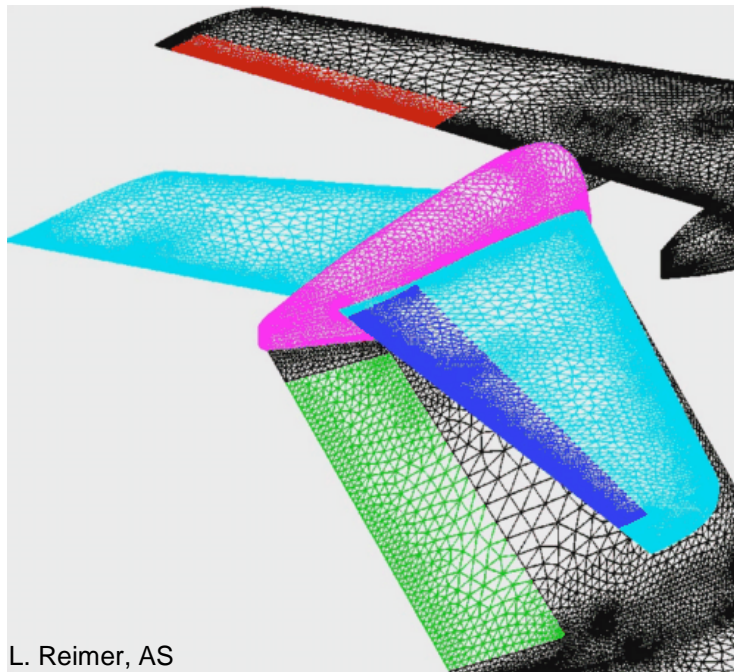


Capture these effects and their impact on the aerodynamic behaviour of the configuration

# Where are we today?

## Dynamic control surface modelling

- Mostly based on **mesh deformation**

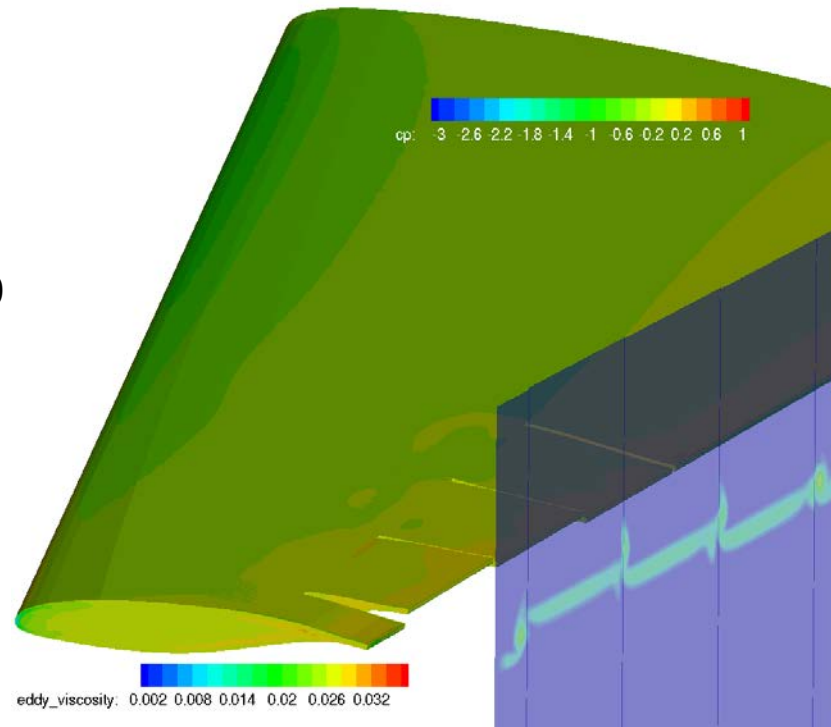


# Where are we today?

## Dynamic control surface modelling

- Mostly based on **mesh deformation** in combination with **patched grids**

Demonstration of A380  
„aileron waltz“



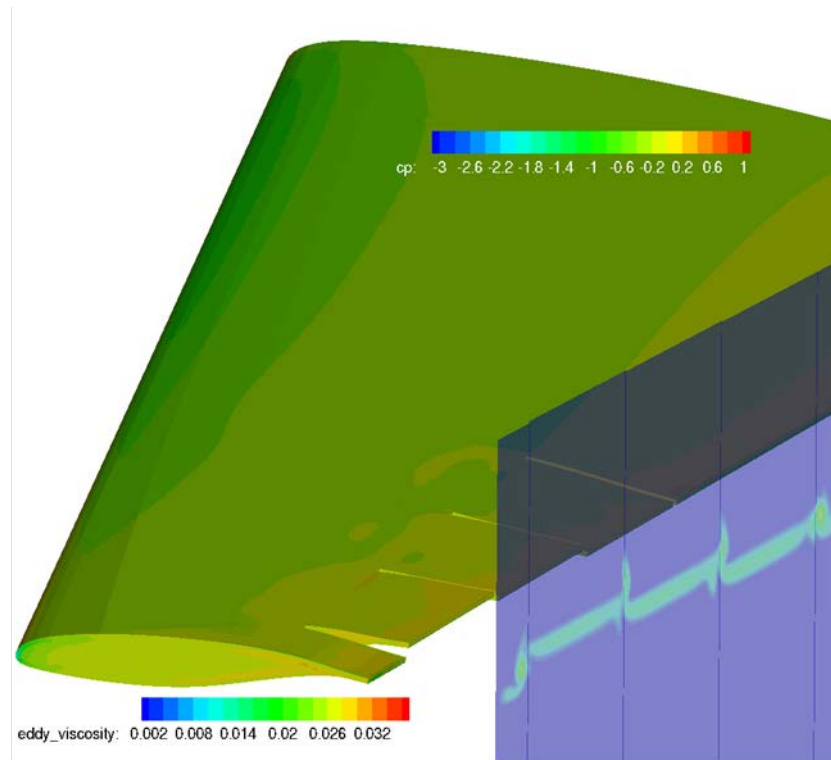
R. Heinrich/D. Azocar, AS



# Where are we today?

## Dynamic control surface modelling

- Mostly based on **mesh deformation** in combination with **patched grids**
- Satisfying representation for most control surfaces...



R. Heinrich/D. Azocar, AS





# Where are we today?

## Dynamic control surface modelling

- Mostly based on **mesh deformation** in combination with **patched grids**
- Satisfying representation for most control surfaces...  
...**apart from spoilers**



# Objectives of this work

- (1) Develop a wind tunnel setup to investigate the transient behaviour of a dynamic spoiler**
- (2) Assess the impact of the relevant motion parameters such as deflection rate, deflection angle and type of deflection**
- (3) Verify and validate the DLR TAU code for configurations with a dynamic spoiler**



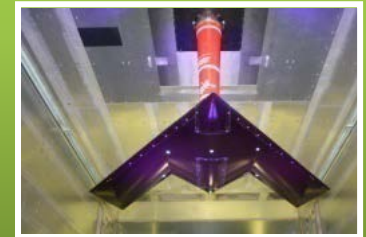
*Further benefits  
for a given control  
surface layout?*

# Funding of this work



DLR project ***Mephisto***  
2014 – 2018

***Improving design capabilities of unmanned vehicles***  
*including aerodynamics, aeroelastics, structures, propulsion,  
flight mechanics, radar/thermal/acoustic signature*



## Work package „Simulation“

- Determination of critical aero loads for wind tunnel model with deflected spoiler
- Verification and validation of the DLR TAU code
- CFD investigation of the unsteady aerodynamic behaviour during spoiler deployment



## Work package „Experiments“

- Concept finding, construction and manufacturing of the new wind tunnel model
- 2 wind tunnel campaigns in 2016
- Provide validation data for the simulation

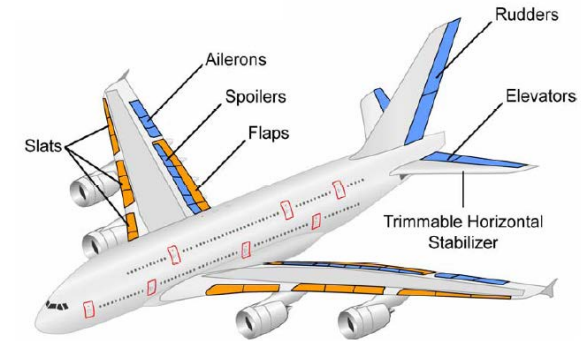


# Outline

- Motivation, objectives and funding
- **Spoiler aerodynamics**
- Development of a wind tunnel model
- Outlook



# Why focus on spoilers?



- Truly multifunctional control surface
- High aerodynamic efficiency over the entire flight envelope (unlike ailerons)
- Induce favourable yawing moment (unlike ailerons)
- Use of spoilers allows for smaller aileron size, hence more space for the high-lift system
- Highly unsteady wake
- Significant time lag between spoiler deflection and aircraft response
- Hardly predictable by low-fidelity methods
- Very demanding to investigate with high-fidelity methods (grid generation, time scales)



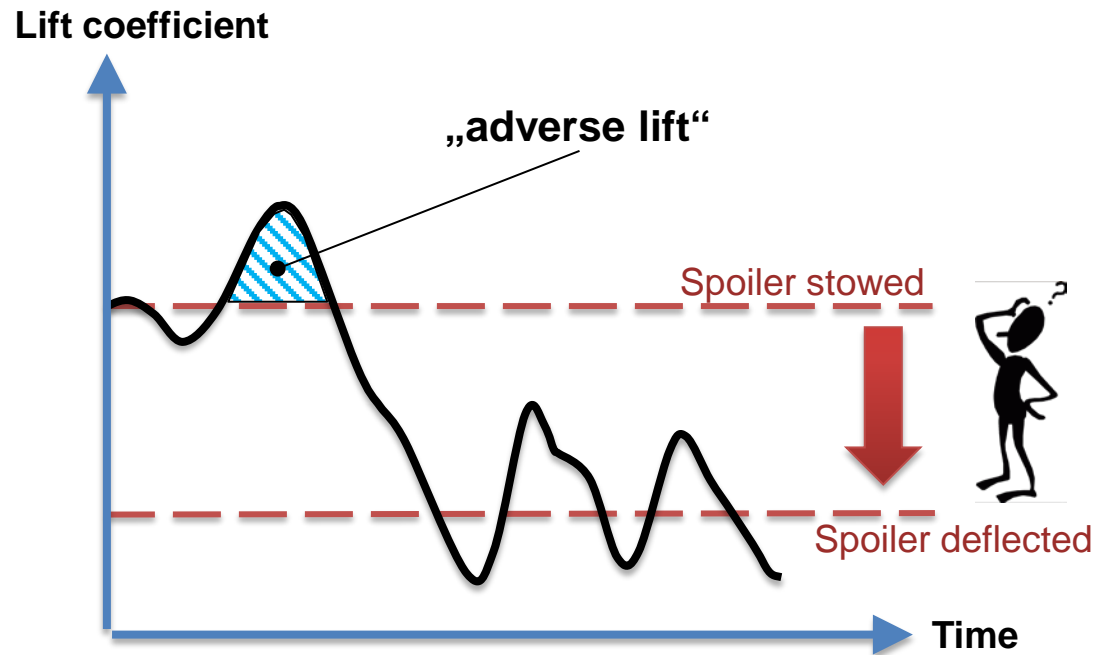
Quotation of Mack et al. (Boeing, 1979)

***„...the characteristics of spoilers are the most difficult to predict of any control surface due to strong non-linearities.“***



# Spoiler aerodynamics

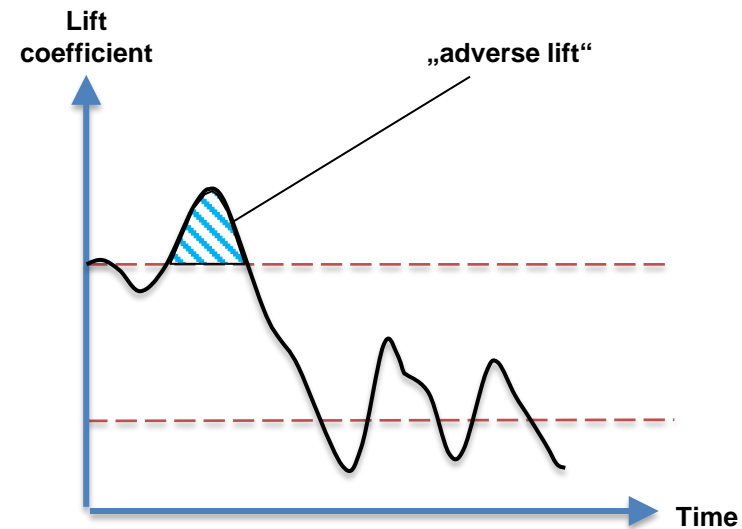
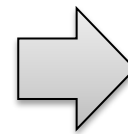
## Non-linearities and adverse effects



# Spoiler aerodynamics

- Adverse lift is a function of the deflection rate
- **Rapid spoiler** deflection leads to adverse lift
- Different definitions of what „rapid“ means

- Mabey, 1983:  $\delta \geq 400 \text{ deg/s}$  (full scale)  
 $t_{rise} = 5 * c/U_{\infty}$



Onflow velocity	Rise time
10 m/s	300 ms
90 m/s	33 ms

- To comply with this definition at wind tunnel scale and at 90 m/s, a rapid spoiler deflection from  $0^\circ \rightarrow 30^\circ$  requires a mean deflection rate of **910 deg/s**
- The chosen actuator is capable of 1250 deg/s



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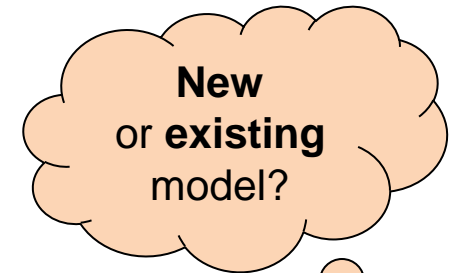




# Requirements for the wind tunnel model

## The new wind tunnel model should...

- (1) ...be 2D and yield a simple and well understood flow field
- (2) ...offer enough space to integrate the kinematics
- (3) ...include a moving spoiler, limited in spanwise direction, with deflection angles of up to  $60^\circ$  and ...
- (4) ...have a spoiler drive allowing for variable deflection rates and different motion types
- (5) ...allow for investigating sweep effects at a later stage



**The DLR-F15 model with spoiler**



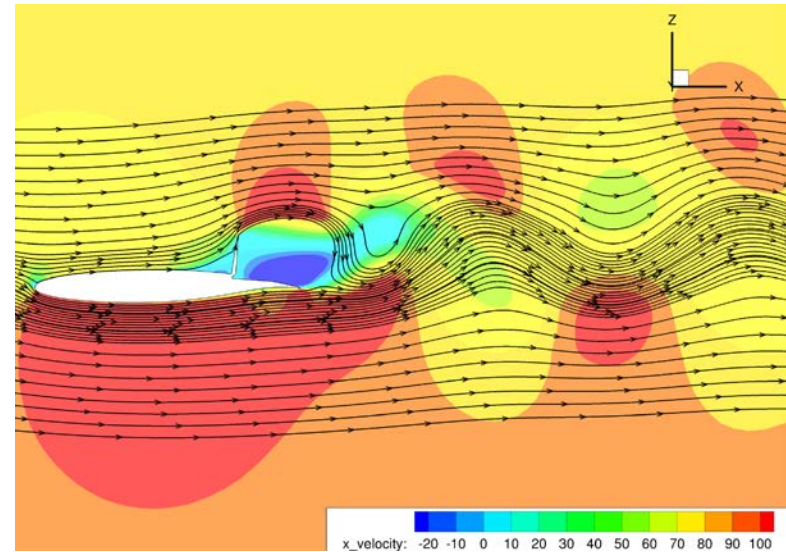
# Determination of critical aerodynamic loads

## Worst case conditions

- Spoiler chord length  $c_s$ : 0,09 m (15 % \* c)
- Deployment angle: 90°
- Onflow velocity: 90 m/s
- Onflow Mach number: 0.265
- Reynolds number: 3,700,000 based on  $c_{ref}$
- Angles of attack: -10° to + 10°

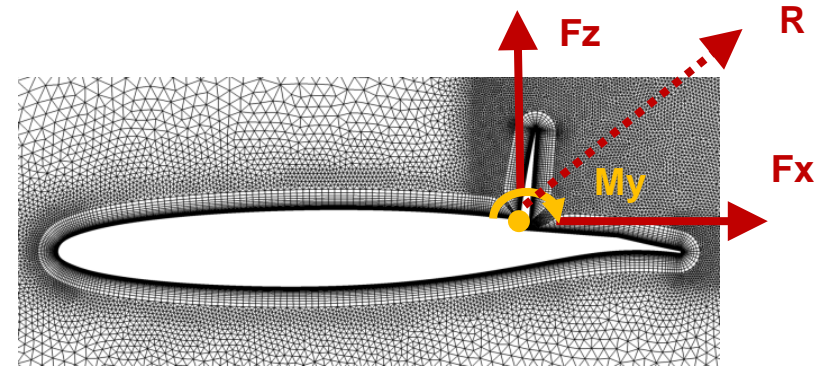
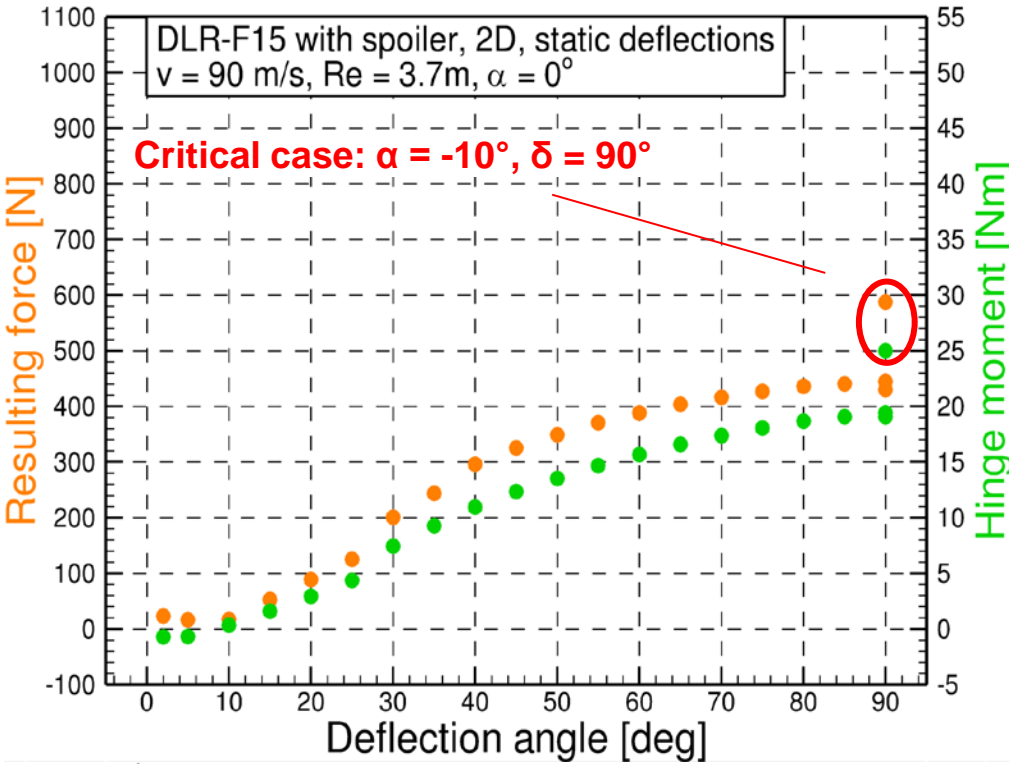
## Grid generation and computation

- Unstructured 2D Centaur grids
- Unsteady TAU computations with  $\Delta t = 0.16 \text{ ms}$



# Determination of critical aerodynamic loads

## Maximum hinge moment

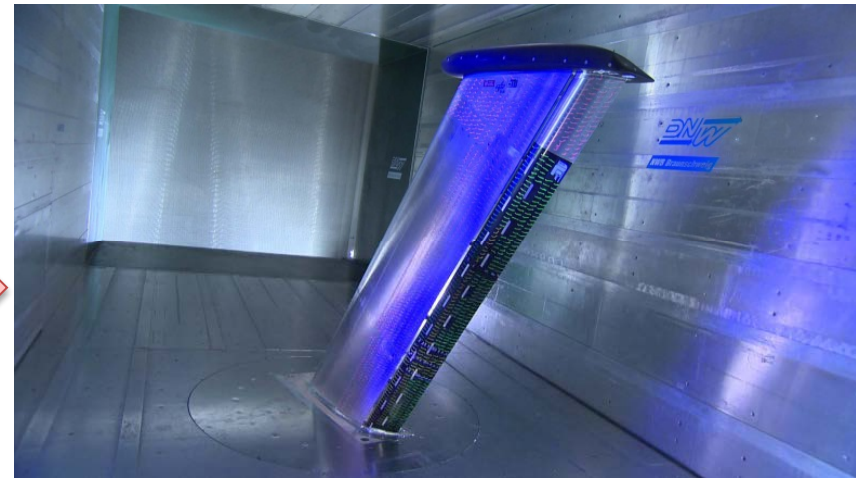


		$\alpha = 0^\circ$ $\delta = 90^\circ$	$\alpha = -10^\circ$ $\delta = 90^\circ$
<b>Spoiler</b>	R	445 N	<b>587 N</b>
	My	20 Nm	<b>25 Nm</b>



# Spoiler kinematics

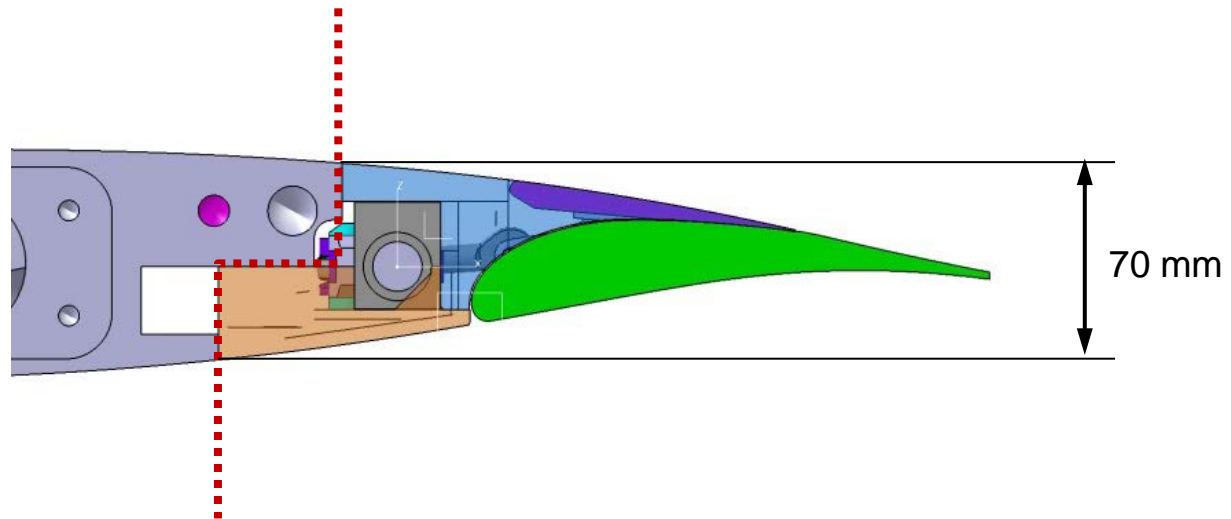
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- Spoiler will be driven from one side only, i.e. through the floor of the test section to maintain the ability to vary the leading edge angle



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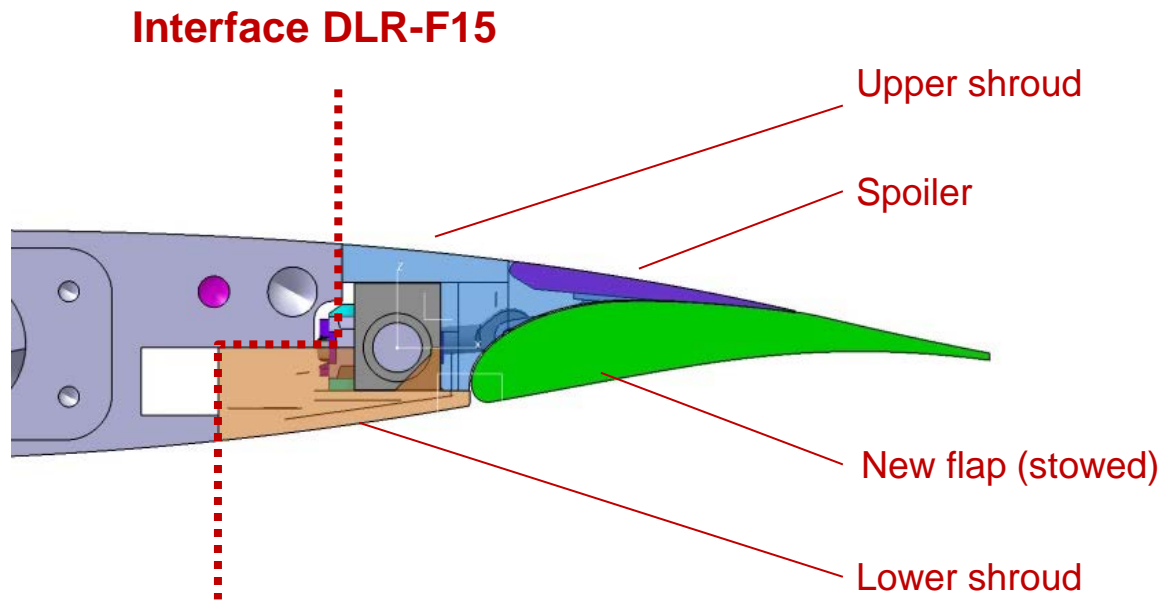
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- Spoiler torque drive not feasible due insufficient torsional stiffness → push rod drive and lever kinematics instead

## Interface DLR-F15



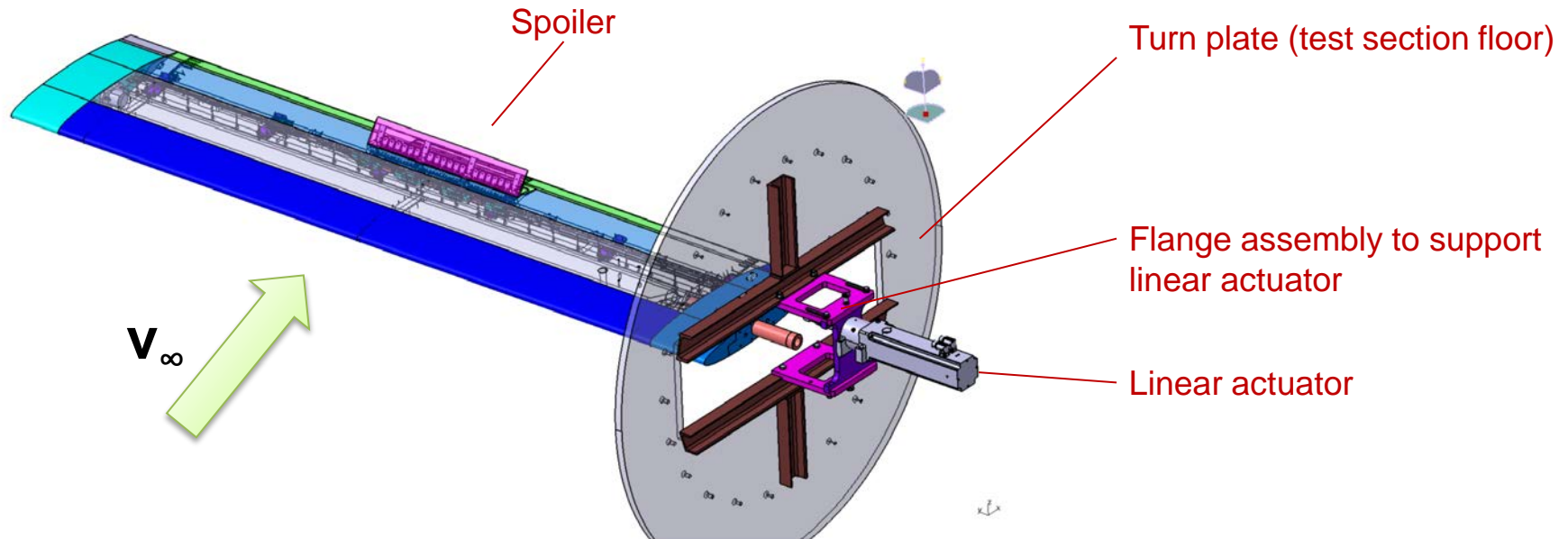
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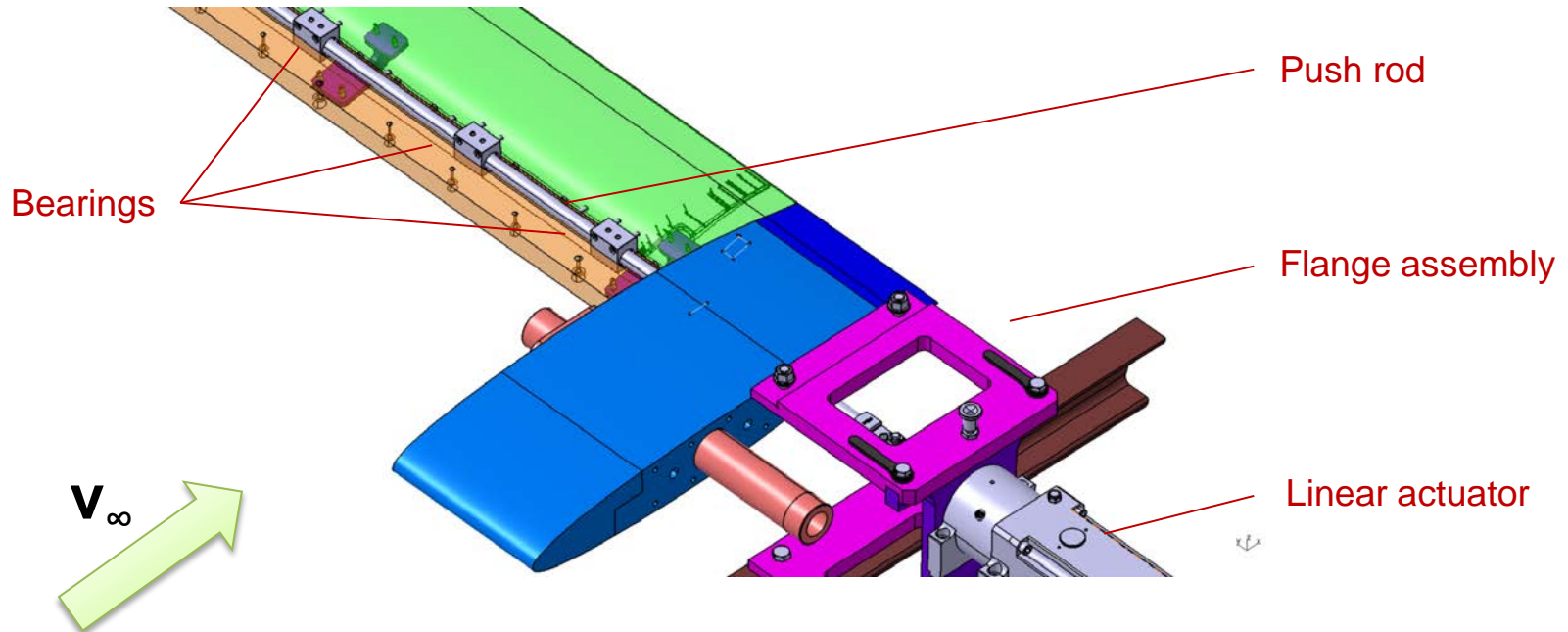
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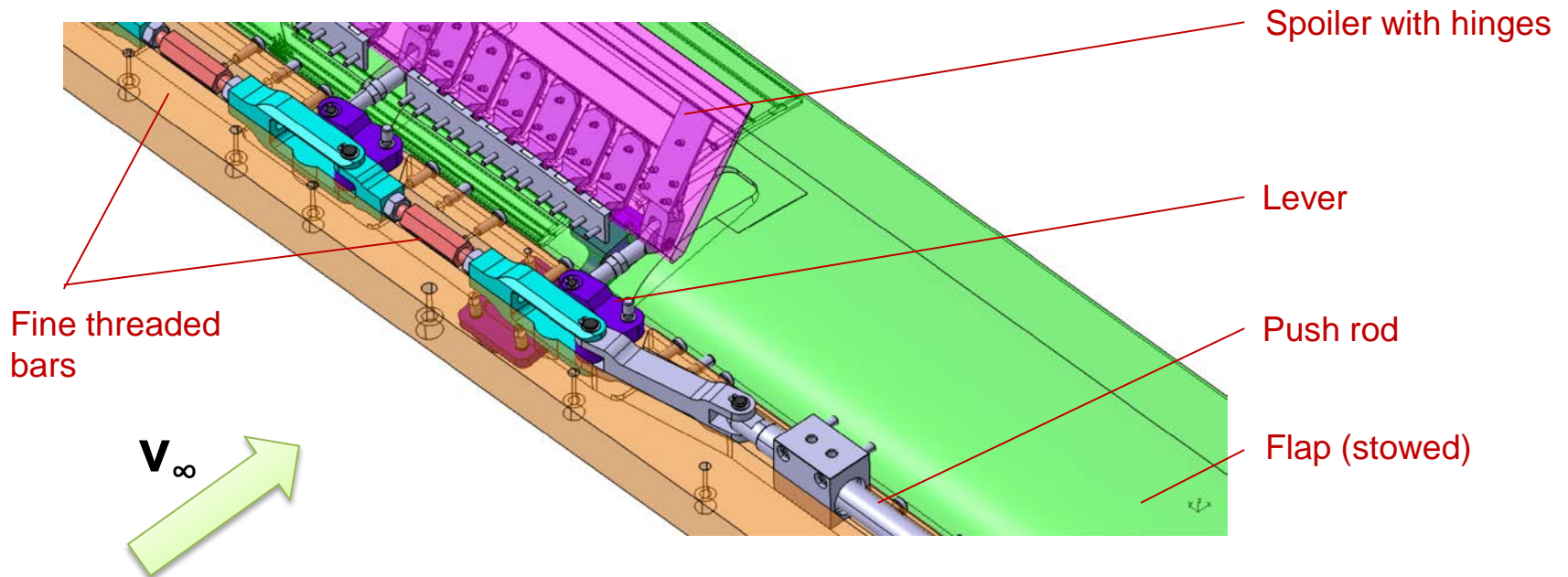
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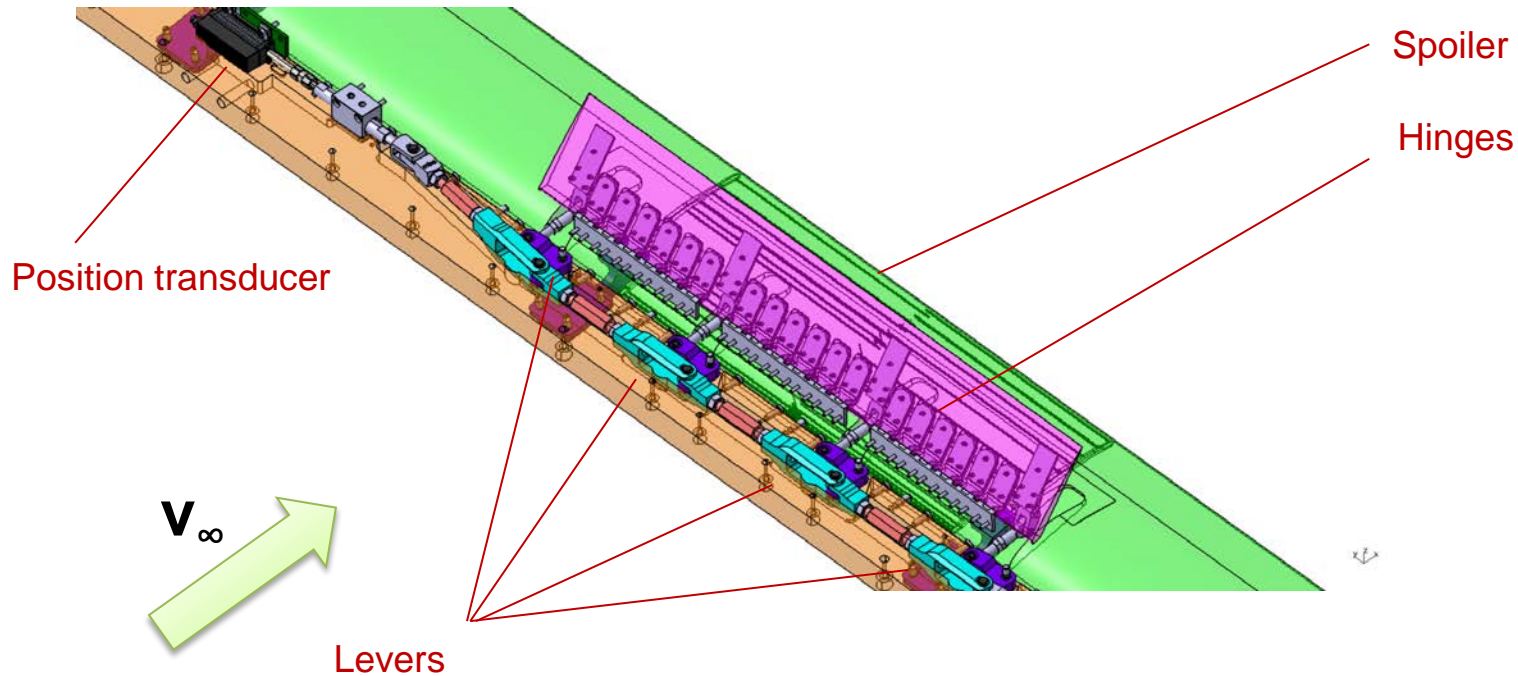
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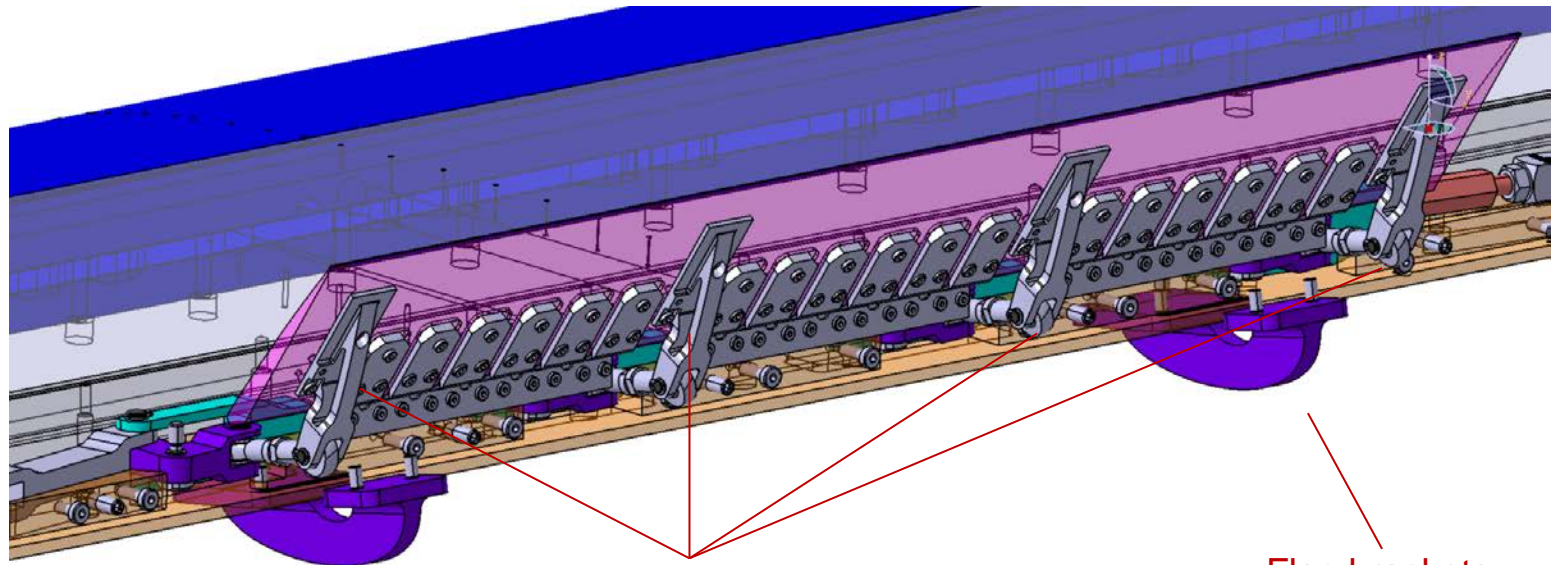
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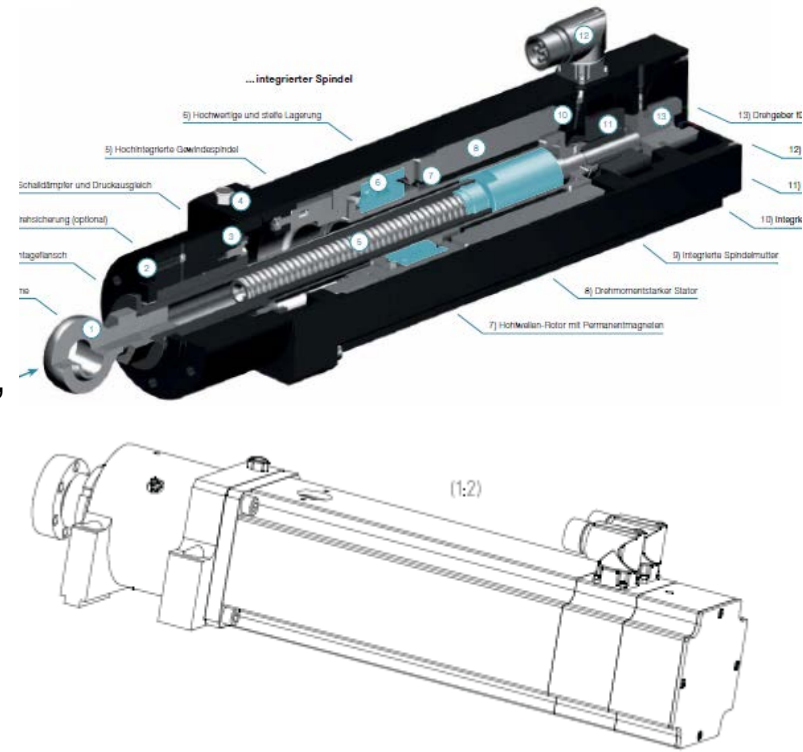
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# Spoiler actuator

- Electrically driven ball screw drive
- Fully integrated unit consisting of motor, ball screw, encoder and brake
- High forces and movement speed
- Challenge: very small travelling distances  
→ deflection from 0° → 90° equals ~ 22 mm only
- Dimensions:  
Length                    471 mm  
Diameter                100 mm x 100 mm



Stroke length	200 mm
Ball screw pitch	5 mm
Max. brake force	4000 N
Max. continuous force	6000 N
Max. force (temporary)	20000 N
Max. movement speed	300 mm/s



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# Outlook

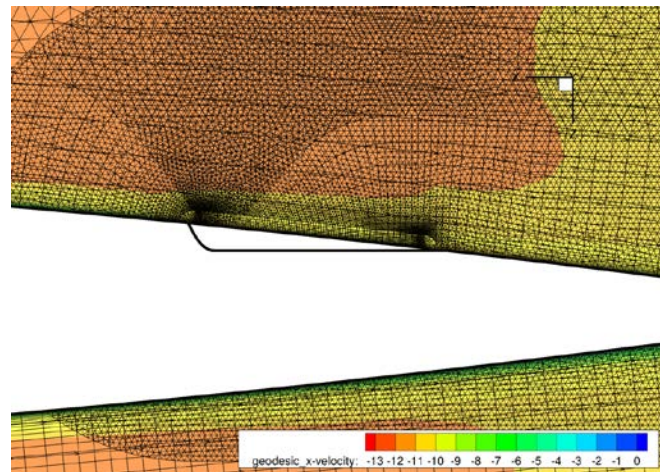
## Experiments

- Manufacturing has started in 11/2015
- The DLR-F15 model with spoiler will be capable to sustain cryogenic conditions
- Two wind tunnel campaigns in 2016 in the DNW-NWB facility in Braunschweig
  - Apr/May 2016: 10 days
    - Focus on steady and unsteady surface pressure information while investigating static and dynamic spoiler deflections
    - 2D setup
    - Optical monitoring of the spoiler position
  - Nov 2016: 10 days
    - Additional PIV measurements
    - 2D or 2.5D?
    - Additional flap deflections?



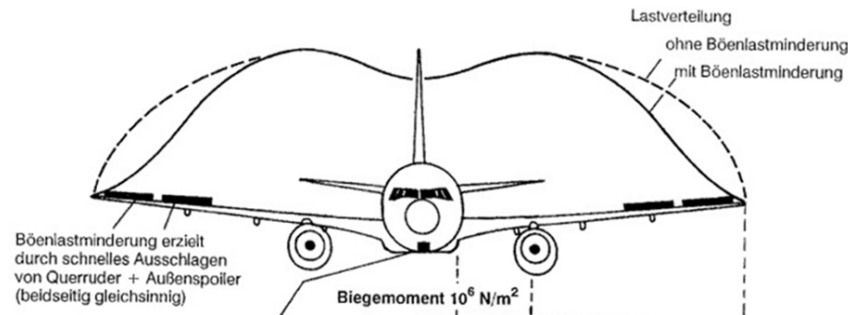
# Outlook Simulation

- Determination of critical loads completed
- Successfully verified and validated the DLR TAU code for a similar configuration
- Main work on dynamic simulations is beginning in mid 2016
- First attempts to simulate a deploying spoiler using a new, automatic hole cutting functionality of the DLR TAU code have already begun



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- Digital-X successor project VitAM (2016 – 2019) in which the modelling of a dynamic spoiler will also be addressed to virtually assess load alleviation systems





# Thank you!

## Any questions?

