

Sidecut radius and the mechanics of turning equipment designed to reduce risk of severe traumatic knee injuries in alpine giant slalom ski racing

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ABSTRACT

Background There is limited empirical knowledge about the effect of ski geometry, particularly in the context of injury prevention in alpine ski racing. We investigated the effect of sidecut radius on biomechanical variables related to the mechanics of turning.

Methods During a field experiment, six European Cup level athletes skied on three different pairs of giant slalom (GS) skis varying in sidecut radii (30 m, 35 m and 40 m). Using a video-based three-dimensional (3D) kinematic system, a 22-point body segment model of the athletes was reconstructed in 3D, and the variables ground reaction force, centre of mass (COM) speed, COM turn radius, ski turn radius, edge angle, fore/aft position and skid angle were calculated.

Results While steering out of the fall line after gate passage, ground reaction force significantly differed between the 30 m and 40 m skis and between the 35 m and 40 m skis. These differences were mainly explainable by larger COM turn radii when skiing on the 40 m ski. During the same turn phase, significant differences in ski turn radius also were found, but there were no differences in edge angle, fore/aft position and skid angle.

Summary The sidecut-induced reduction in ground reaction force and the sidecut-induced increase in centre of mass and ski turn radius observed in this study provides indirect evidence of reduced self-steering of the ski. Self-steering plays a central role in the mechanism of anterior cruciate ligament rupture in alpine ski racing.

INTRODUCTION

In alpine ski racing, the risk of sustaining a severe knee injury is known to be high.¹⁻⁴ The absolute rate of knee injuries in World Cup (WC) alpine skiers has been reported to be 13.8 injuries/100 athletes/season.³ Recent studies have provided a deeper understanding of the underlying injury mechanisms.⁵ ⁶ Most anterior cruciate ligament (ACL) injuries occur while skiing without the athlete crashing.⁵ More than half of all ACL injuries were ascribed to the so called 'slip-catch' mechanism while turning.⁵ A common characteristic of this injury mechanism is that, initially, the skier loses balance backward and inward while steering out of the fall line and loses the pressure on the outer ski.⁵ Then, while trying to regain grip on the outer ski, the inside edge of the outer ski abruptly catches the snow surface, suddenly increasing of knee joint compression, knee valgus and internal

rotation and, as a result, a rupture of the ACL.⁶ These adverse loading patterns are related to the ski's self-steering effect.^{5–7}

The ski's self-steering effect (ie, the ski turns itself if it is edged and loaded) is theoretically expected to depend on its sidecut radius and its longitudinal and torsional stiffness.⁸ Basically, a ski with a small sidecut radius enables the skier to carve tight turns with a minimum of skidding, as long as the ski is loaded and under control.^{9–11} However, in an uncontrolled skiing situation (eg, a sudden catch of the edge while recovering from an out-of-balance situation), the skier's centre of mass (COM) cannot follow the path of the ski anymore; because of the small sidecut radius, the ski will carve inward sharply and force the knee into excessive valgus and internal rotation.⁶

While the influence of the ski's sidecut radius during the injury mechanism itself is readily apparent,5its effect on the general mechanics of turning is still not well understood. Theoretical models and parameter studies have provided valuable insights into the basic mechanics of turning, and revealed important general knowledge about the effect of equipment properties.¹²⁻²² However, as all of these approaches neglect some of the skiers' adaption mechanisms (eg, adjustments of the amount of skidding), it is not clear how sidecut radius influences the relation between turn speed and turn radius, and the resultant ground reaction force under realistic in-field conditions. This knowledge is essential to clarify the role of sidecut radius as a cause of ACL injuries in alpine ski racing, particularly as more than half of these injuries occur while turning.5

Therefore, we: (1) investigated the effect of skis with different sidecut radii on variables related to the mechanics of turning in giant slalom (GS); and (2) discuss the findings in the context of injury prevention in alpine ski racing.

METHODS

Measurement protocol and data collection

During a biomechanical field experiment, six European Cup level athletes skied GS runs on three different pairs of skis with varying sidecut radii (30 m, 35 m and 40 m). All other geometrical specifications of the skis were in accordance with the current equipment rules of the International Ski Federation (FIS).²³ In order to become accustomed to the different skis, in the months prior the experiment, the athletes skied them during



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their regular training sessions. The GS course was set on a 26° inclined, water-injected slope with an average gate distance of 27 m and an offset of 8 m (figure 1). In the mid-section of the course, the athletes were simultaneously filmed over one turn cycle by six panned, tilted and zoomed HDV-cameras (Sony PMW-EX3, 50 Hz, gen-locked). A total of 142 reference points were positioned around the analysed turn and were geodetically measured by a tachymeter (Leica Total station 1200). For each of the analysed turns, a 22-point body segment model and subject ambient reference points were manually digitised in each frame of each camera. Finally, a direct linear transformation (DLT)-based panning algorithm by Drenk²⁴ and the position information of the geodetic measured reference points were used to reconstruct a segment model of each skier in three-dimensional (3D). Manual digitising and model reconstruction were performed using a custom-made software (Volker Drenk, Germany). Owing to reasons of processing time manageability, for each of the six athletes and three pairs of skis, only the fastest run out of three (ie, the run with shortest section time between gates 1 and 5 as illustrated in figure 1) was considered for the data analysis, resulting in a total of 18 analysed turns. The measurement method used has been shown to be reliable for collecting kinematic data under in-field conditions in an earlier study with comparable setup and circumstances.25

Postprocessing and calculations

Figure 1 Schematic on-hill setup (CAM 1–6: positions of the panned, tilted and zoomed video-cameras).

Postprocessing and calculations were performed in *MATLAB*, *R2012b*. The reconstructed 3D position data of each landmark was low-pass filtered using a second-order Butterworth filter with a cut-off frequency between 2 and 5 Hz determined using the Jackson-Knee method.²⁶ In addition, using a technique suggested by Smith,²⁷ the reconstructed body segments were normalised based on anthropometrical data that was measured following the protocol of de Leva.²⁸ COM position was calculated based on the model of Clauser *et al*,²⁹ adapted with the skiing equipment as carried out in earlier studies.^{30 31} The beginning and end of the turn were defined as the crossing points of the ski trajectory (=path travelled by the midpoint

between the outer and the inner ankle) and the COM-trajectory orthogonally projected to the slope plane, as suggested by Supej et al.32 The four functional turn phases Initiation, COM Direction Change I, COM Direction Change II and Completion were defined in accordance to Spörri et al.³⁰ Ground reaction force ($F_{calcGRF}$) was defined in accordance with Mössner *et al*¹¹ as the root of squared total radial force plus squared normal force, and was calculated based on the measured kinematic data, skier's mass and slope inclination angle. Furthermore, the plausibility of the aforementioned method to calculate F_{calcGRF} was double checked by the use of an alternative kinematic-based computation method introduced by Gilgien et al,³³ which additionally considers an estimation of air drag and ski snow friction force. COM speed (v_{COM}), COM turn radius (R_{COM}), fore/ aft position (d_{Fore/Aft}) and skid angle (γ_{Ski}) were determined as described in earlier studies.^{30 31} Ski turn radius (R_{Ski}) was calculated in analogy to R_{COM} based on the ankle joint trajectory of the outer leg. For the calculation of the edge angle (θ_{Edge}), a local coordinate system (x'y'z') at the ankle joint of the outside ski was used (figure 2). x' was defined by the joint ankle and the direction of the longitudinal axis of the ski. z' was defined to be perpendicular to the slope plane and y' was defined as forming a right-handed triad with x' and z'. θ_{Edge} was then calculated as the angle between the z-axis and the ankle-knee vector projected to the y'-z' plane.

Statistical analysis

The statistical analysis included the following steps: (1) based on the data of one turn cycle per athlete, the group mean curves (ie, the ensemble averaged individual curves) of $F_{calcGRB}$ v_{COM} , R_{COM} , R_{Ski} , θ_{Edge} , $d_{Fore/Aft}$, γ_{Ski} were calculated for each pair of skis. Thereafter, for each variable the differences between the three different pairs of skis (30 m, 35 m and 40 m sidecut radius) were visualised by plotting the areas of uncertainty around the estimate of the mean (±SE boundaries). (2) Ski differences in average $F_{calcGRF}$ over the entire turn cycle and within the specific turn phases were tested for significance using one-way repeated measures analysis of variance (ANOVA), including post hoc testing with Bonferroni



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Figure 2 Edge angle (θ_{Edge}) definition using a local coordinate system at the ankle joint of the outside ski.

correction for pairwise comparison. Provided that the average $F_{calcGRF}$ differences were significant within a specific turn phase, this phase was further subdivided into a first and a second half and again was analysed by one-way repeated measures ANOVAs. (3) For the turn phases in which significant average $F_{calcGRF}$ differences were observed, the importance of the differences in R_{COM} and v_{COM} to explain the differences in $F_{calcGRF}$ was assessed by comparing the β weights of a multiple regression analysis. (4) For the turn phase with the lowest amount of skidding (ie, the smallest interference of the ski's self-steering effect), a repeated measures multivariate analysis of variance (dependent: R_{Ski} , θ_{Edge} , $d_{Fore/Aft}$, γ_{Ski} ; independent: 30 m ski, 35 m ski, 40 m ski) was calculated. In case of global significance, one-way repeated measures ANOVAs (including post hoc testing with Bonferroni correction) were performed.

RESULTS

Variables' turn cycle progression

The group mean curves of $F_{calcGRF}$ v_{COM} and R_{COM} for the three different pairs of skis are illustrated in figure 3. Those of R_{Ski}, θ_{Edge} , d_{Fore/Aft}, γ_{Ski} are presented in figure 4.

Differences in ground reaction force

The descriptive and inferential statistics of average $F_{calcGRF}$ are presented in table 1. While there were no significant differences in $F_{calcGRF}$ overall turn cycle averages between the different pairs of skis, significant differences in $F_{calcGRF}$ were found for *COM Direction Change II*. When skiing on the 40 m skis, the pairwise comparison between the 30 m and 40 m skis showed a $F_{calcGRF}$ reduction of 7%, and the pairwise comparison between the 35 m and 40 m skis showed a $F_{calcGRF}$ reduction of 5.9%. Considering only the second half of *COM Direction Change II*, these differences were even larger (30 m/40 m: -10.9%; 35 m/40 m: -7.2%).



Figure 3 Areas of uncertainty around the estimate of the mean (±SE) illustrating calculated ground reaction force ($F_{calcGRF}$) and the $F_{calcGRF}$ predicting variables COM speed (v_{COM}) and COM turn radius (R_{COM}) over one turn cycle; black: 30 m ski; dark grey (transparent): 35 m ski; light grey: 40 m ski. COM, centre of mass.

Contribution of COM turn radius and COM speed to ground reaction force

The results of the multiple regression analysis assessing the importance of the differences in R_{COM} and v_{COM} to explain the differences in $F_{calcGRF}$ during the second half of the *COM Direction Change II* are presented in table 2. For both the 30 m/ 40 m ski comparison and the 35 m/40 m ski comparison, the R_{COM} differences were of greater importance for explaining the $F_{calcGRF}$ differences than the v_{COM} differences. Additional analysis revealed that R_{COM} significantly differed between the 30 m and the 40 m skis, as well as between the 35 m and 40 m skis (p<0.05).

Differences in ski turn radius and skiers' actions

The descriptive and inferential statistics of average R_{Ski} , θ_{Edge} , $d_{Fore/Aft}$ and γ_{Ski} during COM Direction Change II are presented in table 3. While there were no significant differences in the variables related to the skiers actions (θ_{Edge} , $d_{Fore/Aft}$ and γ_{Ski}) between the different pairs of skis, significant differences in R_{Ski} COM Direction Change II phase averages were found. The

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Figure 4 Areas of uncertainty around the estimate of the mean (±SE) illustrating the variables ski turn radius (R_{Ski}), edge angle (θ_{Edge}), fore/ aft position ($d_{Fore/Aft}$) and skid angle (γ_{Ski}) over one turn cycle; black: 30 m ski; dark grey (transparent): 35 m ski; light grey: 40 m ski.

pairwise comparison between the 30 m and 40 m skis showed a R_{Ski} increase of 14.3%, and the pairwise comparison between the 35 m and 40 m skis showed a R_{Ski} increase of 11.9% when skiing on the 40 m skis.

DISCUSSION

The main findings of this study were: (1) between the 30 m and 35 m ski, no significant differences in $F_{calcGRF}$ were found; (2)

during COM Direction Change II, and particularly during the second half of this turn phase, the 30 m/40 m and 35 m/40 m pairwise comparisons indicated significantly lower $F_{calcGRF}$ averages when skiing on the 40 m ski (30 m/40 m: -10.9%; 35 m/40m: -7.2%); (3) R_{COM} differences were of greater importance for providing an explanation for these $F_{calcGRF}$ differences than the differences in v_{COM} ; (4) During the turn phase with the lowest amount of skidding (ie, the smallest interference of the ski's self-steering effect), significant differences were found in R_{Ski} (30 m/40m: +14.3%; 35 m/40 m: +11.9%), but no differences in θ_{Edge} , $d_{Fore/Aft}$ and γ_{Ski} were observed.

Methodological considerations

Prior to interpreting the study's findings, it has to be pointed out that the current study design only allows for the derivation of first clues about the effect of sidecut radius on injury risk. Although these clues must be verified by epidemiological studies before the effectiveness of the investigated prevention measures can be judged as conclusive, they are, nevertheless, at this early stage of gathering knowledge, an important means of developing strategies to protect the athletes' health.

At a first glance, a limitation of the current study might be the fact that only six participants and only one representative turn for each ski intervention were considered for the statistical analysis. This choice has cons and pros: On the one hand, it will result in a certain loss of variability information which limits the unrestricted generalisability of the study findings. On the other hand, only a limited number of trials can guarantee a high validity of the outcome measures, because the span of time with constant environmental conditions in field is limited (eg, changing snow conditions as a result of performing repetitive runs on the same course). Furthermore, to provide sufficient accuracy for measuring the underlying COM kinematics in field, the 'videobased 3D kinematics' method was an indispensable choice. Despite major advantages in measurement accuracy, this method has substantial limitations with regard to the capture volume and the 3D reconstruction efforts (manual digitising). Thus, based on these considerations, the measurement protocol of the current study can be argued to be appropriate.

The effect of sidecut radius on the mechanics of turning

Based on the most common theoretical models, greater sidecut radius is expected to increase the resulting ski turn radius,¹² ¹³ and, therefore, also is expected to decrease the acting ground acting reaction forces,¹⁰ ¹¹ provided that the performed edge angle is the same. This was only partially observed in the current study.

Despite almost identical edge angles, $F_{calcGRF}$ and R_{Ski} did not differ between the skis varying in sidecut radius over a wide range of the turn (*Initiation*, COM Direction Change I and Completion phase). This might be explained by the fact that the aforementioned theoretical models assume the occurrence of a purely carved turn without any skidding. However, in a real skiing situation, athletes adjust the amount of skidding, particularly during the aforementioned turn phases (figure 4).

After gate passage (during *COM Direction Change II*), the theoretical expectation that a greater sidecut radius increases the resulting ski turn radius coincided with the experimental findings. This might be explained by the generally higher amount of carving (ie, lower amount of skidding) during this phase (figure 4), which is a major assumption underlying the aforementioned theoretical models. Furthermore, based on the current study findings, it seems plausible that after gate passage, R_{Ski} differed mainly because of the changed sidecut radius of

Descriptive and inferential statistics of average of calculated ground reaction force (F_{calcGRF}) between the tested skis (30 m, 35 m, 40 m Table 1 sidecut radius) for: ^(Turm) turn average; ^(Initiation) average of the *Initiation* phase; ^(COM DC I) average of the *COM Direction Change I* phase; ^(COM DC II) average of the *COM Direction Change I* phase; ^(COM DC II) average of the *COM Direction Change II* phase; ^(Completion) average of the *Completion* phase; ^(first) and ^(second) indicate the first and the second half of a specific turn phase, respectively

		Mean±SD			ANOVA		Pairwise comparisons		
Parameter	Subparameter	30 m	35 m	40 m	p Value	eta _p ²	30 m/35 m	30 m/40 m	35 m/40 m
Turn cycle									
F _{calcGRF} ^(Turn) (N/BW)		1.56±0.07	1.55±0.06	1.52±0.07	0.227	0.232			
Turn phase									
F _{calcGRF} ^(Initiation) (N/BW)		0.97±0.03	0.96±0.02	0.98 ± 0.04	0.454	0.140			
F _{calcGRF} (COM DC I) (N/BW)		1.75±0.11	1.74±0.19	1.75±0.18	0.996	0.001			
F _{calcGRF} (COM DC II) (N/BW)		2.05±0.12	2.02±0.10	1.91±0.15	0.005**	0.698		-7%*	-5.9%*
	F _{calcGRF} (COM DC II, first) (N/BW)	2.09±0.14	2.11±0.09	2.01±0.19	0.259	0.240			
	F _{calcGRF} (COM DC II, second) (N/BW)	1.97±0.17	1.89±0.13	1.75±0.11	0.015*	0.651		-10.9%*	-7.2%*
F _{calcGRF} (Completion) (N/BW)		1.15±0.03	1.13±0.02	1.12±0.02	0.123	0.350			

Repeated measure ANOVA results are based on the Greenhouse-Geisser correction. Post hoc method with Bonferroni correction for pairwise comparison.

Level of significance: *p<0.05, **p<0.01, ***p<0.001. ANOVA, analysis of variance; BW, body weight; COM, centre of mass.

the ski and not due to altered skiers' actions (no differences in θ_{Edge} , $d_{Fore/Aft}$ and γ_{Ski} were observed).

As found in this study, R_{COM} and v_{COM} explained more than 97% of the variance in the reported $F_{calcGRF}$ differences between the tested pairs of skis. This is in line with previous findings by Gilgien et al,³⁴ who demonstrated that, in contrast to other disciplines, in GS centripetal acceleration (v_{COM}^2/R_{COM})

 Table 2
 Results of the multiple regression analysis assessing the
 importance of the 30 m/40 m ski difference and 35 m/40 m ski difference in COM speed (v_{COM}) and COM turn radius (R_{COM}) to explain the corresponding difference in the dependent variable calculated ground reaction force ($F_{calcGRF}$) during the second half of the COM Direction Change II phase (COM DC II, second)

Predictors of FcalcGRF differences	β-weight	p Value
30 m/40 m ski difference (Model*)		
R _{COM} (COM DC II, second) (30 m/40 m)	-0.865	0.002
V _{COM} (COM DC II, second) (30 m/40 m)	0.371	0.018
35 m/40 m ski difference (Model†)		
R _{COM} (COM DC II, second) (35 m/40 m)	-0.687	0.002
V _{COM} ^(COM DC II, second) (35 m/40 m)	0.581	0.003
*Adjusted R^2 =0.970; p=0.002. †Adjusted R^2 =0.981; p=0.001. COM, centre of mass.		

is the main contributor to the ground reaction force. Despite the fact that by physical laws v_{COM} contributes in square to centripetal force (radial component of F_{calcGRF}), its importance for providing an explanation for the differences in F_{calcGRF} is lower than that of the R_{COM} differences.

The role of sidecut radius in the context of injury prevention

Based on the results of the current study, one preventative benefit of skis with greater sidecut radius might be found in the sidecut-induced (ie, not skiers' action-induced) reduction of F_{calcGRF} and increase of R_{Ski}. This can be considered to be an indirect indication for a reduced self-steering effect of the skis, which is known to play a central role within ACL injury mechanisms in alpine ski racing.⁵⁶ In other words: in the case of an uncontrolled skiing situation (eg, a sudden catch of the edge while recovering from an out-of-balance situation), skis with greater sidecut are expected to be less likely to carve sharply inward and to force the knee into excessive adverse valgus and internal rotation.

Another preventative gain of increasing the sidecut radius of the skis might be found in the assertion that within the competition discipline GS, injury risk is most likely associated with high loads while turning,³⁴ and that the skier's balance might be challenged by a combined occurrence of small turn radii and high loads.³⁰ In this context, the current study found that greater sidecut radius significantly reduces F_{calcGRF} by up to 7%

Table 3 Descriptive and inferential statistics of average ski turn radius (R_{Ski}), edge angle (θ_{Edge}), fore/aft position ($d_{Fore/Aft}$) and skid angle (γ_{Ski}) during *COM Direction Change II* phase ^(COM DC II) for the tested skis (30 m, 35 m, 40 m sidecut radius)

-									
	Mean±SD			ANOVA†		Pairwise comp	Pairwise comparisons		
	30 m	35 m	40 m	p Value	eta _p ²	30 m/35 m	30 m/40 m	35 m/40 m	
R _{ski} (COM DC II) (m)	16.70±1.43	17.06±1.60	19.08±1.23	0.012*	0.715		+14.3%*	+11.9%***	
θ_{Edge} (COM DC II) (degree)	68.6±2.3	68.8±3.1	67.2±1.6	0.201	0.290				
$d_{Fore/Aft} \stackrel{(COM DC II)}{\longrightarrow} (m)$	0.06±0.05	0.05±0.06	0.08±0.03	0.471	0.133				
γ _{ski} ^(COM DC II) (degree)	3.0±0.7	2.0±0.4	3.7±3.6	0.390	0.153				

Repeated measure ANOVA results are based on the Greenhouse-Geisser correction. Post hoc method with Bonferroni correction for pairwise comparison.

Level of significance: *p<0.05, **p<0.01, ***p<0.001.

+Prior the ANOVA test a global significance was identified (MANOVA: p<0.008, eta_p^2 =0.712).

ANOVA, analysis of variance; COM, centre of mass; MANOVA, multivariate analysis of variance.

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and significantly increases R_{Ski} by up to 14.3% during COM Direction Change II. This turn phase is of particular interest, because more than half of the ACL injuries occur while turning, mainly during the steering phase out of the fall line after gate passage,⁵ which corresponds to the COM Direction Change II phase in the current study. During this phase, R_{Ski} reaches its minimum, and $F_{calcGRF}$ is already at a very high magnitude, close to the athlete's physical limit (up to 2.3 N/body weight, figure 2), which might conceivably increase the risk for out-of-balance situations.

On a final note, however, it has to be pointed out that based on the results of this study, only a substantial increase in sidecut radius might lead to this preventative gain and that the effectiveness of the investigated prevention measures must be verified by epidemiological studies before the aforementioned interpretations can be judged as conclusive.

CONCLUSION

This biomechanical field study demonstrated that within the competition discipline GS, substantially greater sidecut radius decreases ground reaction force and increases ski turn radius while steering out of the fall line after gate passage. Since no corresponding differences in the skiers' actions (edging, fore/aft leaning and skidding) were found, the aforementioned differences are most likely attributable to altered sidecut radii only. This can be considered to be an indirect indication for a reduced self-steering effect, which is known to play a central role within ACL injury mechanisms in alpine ski racing. Thus, skis with substantially greater sidecut might help to improve the athletes' safety in alpine ski racing.

What are the findings?

- Within the competition discipline giant slalom, greater sidecut radius leads to a substantial decrease in ground reaction force while steering out of the fall line after gate passage.
- This significant decrease in ground reaction force can be principally explained by a significant increase in centre of mass turn radius, and only partially explained by altered centre of mass speed.

How might it impact on clinical practice in the future?

- ➤ Greater sidecut radius of giant slalom skis might prevent anterior cruciate ligament (ACL) injuries in alpine ski racing: the sidecut-induced increase in ski turn radius observed in the current study provides indirect evidence of a less self-steering of the ski. Self-steering plays a central role in the mechanisms of ACL injuries.
- However, this preliminary evidence to protect the athletes' health must be verified by epidemiological studies before their effectiveness can be judged.

Contributors JS, JK and EM conceptualised the study design. JS organised and coordinated the biomechanical field study. JS, JK, MG contributed to the data collection. JS conducted the data processing and analysis. All authors contributed to the intellectual content of the study, manuscript writing and approved the final version of this article.

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Competing interests None declared.

Ethics approval This study was approved by the Ethics Committee of the Department of Sport Science and Kinesiology at the University of Salzburg.

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Sidecut radius and the mechanics of turning —equipment designed to reduce risk of severe traumatic knee injuries in alpine giant slalom ski racing

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