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Haptic-enabled virtual planning and assessment of product assembly

Abstract

Purpose – To present a new haptic-enabled virtual assembly system for the automatic generation and objective assessment of assembly plans. The system is intended to be used as an assembly planning tool along the product development process.

Design/methodology – The generation of product assembly plans is based on the analysis of the assembly movements and operations performed by the user during the virtual assembly execution, and the objective assessment of product assembly is based on the definition and computation of new proposed assembly metrics.

Finding – To evaluate the system, a case study corresponding to the assembly of a mechanical component is presented and analysed. The results demonstrate that the proposed system is an effective tool to plan and evaluate different product assembly strategies in a more practical and objective approach than existing assembly planning methods.

Research limitations – Although the virtual assembly execution time is larger than the real assembly execution time, the assembly planning and evaluation results provided by the system are valid. However, the development of higher performance collision detection algorithms is needed to reduce the simulation time.

Originality – The proposed virtual assembly system is able not only to simulate and automatically generate assembly plans, but also to objectively assess them from the virtual assembly task execution. The introduction and use of several assembly performance metrics to objectively evaluate assembly strategies in virtual assembly, also represents a novel contribution.

Keywords – Virtual assembly (VA); haptics; virtual assembly planning; product assembly; assembly metrics.

Article classification: Research paper

1. Introduction

Assembly process planning plays a vital role in a new or remanufactured product because it affects its quality, manufacturing cost, production time and service life. In addition, the demand for service products, re-manufacturing and recycling has forced companies to consider the ease of product assembly and disassembly at the design stage. A good assembly plan can increase the efficiency of the manufacturing process and the quality of the product. According to the literature, the assembly process takes up to 50% of the total production time, and more than 20% of the total product manufacturing cost (De Fazio *et al.*, 1991; Boothroyd and Alting, 1992). Because of this great impact on the manufacturing cost, a large number of research works have focused on enhancing the assembly planning process.

Traditional methods for assembly planning and evaluation, although effective, they are time consuming and costly because they depend on the specialist's experience, the physical prototypes and the measurement equipment (Liu *et al.*, 2015). To accelerate the assembly planning process, Computer Aided Process Planning (CAPP) systems and mathematical algorithms have been developed; however, their results have not been successful (Thornton, 2009). One of the main reasons for this lack of success is that assembly planning depends on a high level of expertise, which has proved to be difficult to capture and formalise (Fletcher *et al.*, 2012). Other disadvantages of these assembly planning methods include the lack of the usability required by industry; they are not intuitive and require significant training due to complex user interfaces and system's inflexibility, and the results are not always feasible and optimal (Thornton, 2009).

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Recently, Virtual Assembly (VA) technologies have emerged as a tool for planning and evaluating product assembly (Li *et al.*, 2016; Garbaya *et al.*, 2019). VA systems are based on the simulation of real assembly operations in an intuitive and interactive virtual environment that supports the human's assembly cognition, intuitiveness and ergonomic capabilities (Yusof and Latif, 2013). In addition, VA systems have been enhanced with haptic technologies to allow the natural manipulation and dynamic perception of virtual objects (Garbaya and Zaldivar, 2007; Gonzalez-Badillo *et al.*, 2014).

Although VA systems and haptic technologies have advanced computational tools for assembly planning, they have failed in providing a practical solution to generate and evaluate assembly strategies. Most VA systems have focused on evaluating the feasibility of performing assembly tasks in a virtual environment, and little research effort has been made to generate practical and useful assembly information to assist the decision-making process along the product life cycle.

In this paper a novel haptic-enabled virtual assembly system for the automatic generation and objective assessment of assembly plans is proposed. The system is able to automatically generate assembly plans based on the automatic logging and analysis of the VA task execution. Assembly performance metrics are defined and computed to objectively evaluate the assembly strategies and to generate valuable assembly information.

2. Related work

Assembly planning is an important activity that comprises the analysis and simulation of the assembly operations and strategies required to produce a component. The aim of assembly planning is to feedback the product design process, and to identify the assembly strategy that leads to a more efficient and profitable product fabrication process. According to Homem de Mello and Sanderson (1991), the most important technical issues addressed in automated assembly planning are: assembly sequence representation, generation and evaluation; planning process accuracy and efficiency; CAD program integration; and task and motion planner integration.

Traditional methods for representing assembly plans have been summarized in the literature (Medellin *et al.*, 2010; Wang *et al.*, 2013) and they compromise: list of tasks, graph of connections, AND/OR graphs, directed graphs, non-directional blocking graph (NDBG), assembly trees, precedence graphs, Petri nets, and Liasion diagrams. On the other hand, assembly plan generation has primarily focused on algorithms for the fast and efficient generation of feasible assembly plans. However, as the number of parts in a product increases, the number of assembly plans increases exponentially, and therefore the generation and detection of a feasible and optimal assembly plan becomes a challenging task. Assembly plan generation methods can be classified into the following categories (Medellin *et al.*, 2010): feasibility decomposition, forming subassemblies, precedence knowledge, graphical approach, genetic search, random approach, assembly state codification, grouping components, motion based, and virtual approaches.

Several methods for assembly planning have been proposed in the literature, such as genetic algorithms (Bonneville *et al.*, 1995; Marian *et al.*, 2006), simulated annealing (Hui *et al.*, 2006), ant colony algorithms (Akpinar *et al.*, 2013), particle swarm optimization (Lv *et al.*, 2010), neural networks (Sinanoglu *et al.*, 2005), petri net methods (Ben-Arieh *et al.*, 2004; Hu and Liu, 2015; Chen and Hu, 2018, Yang and Hu, 2018), among others. Although all these soft computing methods are capable of obtaining an optimal feasible assembly sequence, they have several limitations such as high computational time and local search space. Moreover, these algorithms do not consider all output parameters and hence the solution obtained is near the optimal. For these

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reasons, and despite all the research efforts, industrial assembly planning still relies on CAD software and the experience and knowledge of an expert.

Assembly evaluation aims to assess assembly plans in order to select the best feasible plan. Assembly feasibility involves manipulability, accessibility, stability, visibility, and geometrical, mechanical and material constraints evaluation. Traditional assembly evaluation relies on the fabrication of physical prototypes that are built and assembled by the specialist to identify any issues regarding the product design and assembly. However, as the assembly task gets more complex, such method tends to be time consuming, costly and prone to errors (Seth *et al.*, 2011). In addition, assembly evaluation requires the definition of criteria to analyse and compare the different assembly plans (Goldwasser *et al.*, 1999). The evaluation criteria should consider performance parameters such as tool changes, part orientation changes, assembly complexity, assembly time, similar assembly operations, cost, ergonomics, energy consumption and parallelism.

In recent years, virtual assembly (VA) has become a popular assembly tool that can be defined as (Xia *et al.*, 2013): The use of virtual reality, computer graphics, artificial intelligence technologies to construct a virtual model and environment of a product assembly in order to interactively analyse and simulate the product design and the assembly process. Several VA platforms have been proposed in the literature, but they have mainly focused on evaluating their functionality as a simulation tool rather than an engineering assisting tool. To address this problem, several authors have developed VA systems using different methodologies and features (Gonzalez-Badillo *et al.*, 2014; Li *et al.*, 2016; Garbaya *et al.*, 2019). Table 1 summarizes the VA systems that have considered the analysis of the assembly process beyond simply bringing the parts together. In this table the systems have been dived into two main categories: haptic-enabled and haptic-unabled systems. In addition, four main characteristics are identified: system evaluation,

which refers to the evaluation of the system's functionality; sequence generation, which represents the ability of the system to generate assembly sequences; assembly metrics, which denotes the metrics or parameters used by the system; and assembly planning, which refers to the system's ability to generate, represent and evaluate assembly plans.

				As	sembly	y metr	ics	Assen	nbly pla	anning
	VA system	System evaluation	Sequence generation	TCT	DOF	Stability	Accessibility	Generation	Representation	Assessment
	Xia et al., 2011	Х		х			х			
	Thing et al., 2010	Х		х			х			
	Bordegoni et al., 2009	Х		х			х			
	Vo et al., 2009	Х		х			х			
oled	Garbaya et al., 2007	Х		х			х			
enat	Adams et al., 2001	Х		х			х			
tic-é	Yoo, 2011	Х		х	х		х			\mathbf{x}^1
Iapi	Seth et al., 2006	Х		х			х			x ²
	Jia <i>et al.</i> , 2009	Х		х			х			
	Ladeveze et al., 2010	Х		х			х			
	Hassan <i>et al.</i> , 2010	Х					х			x ³
	Gonzalez et al., 2014	Х	Х	х		х	х	Х	х	
	Boud et al., 2000	Х		х			х			
	Brough et al., 2007	Х		х						
eq	Jayaram <i>et al.</i> , 2007	Х	х							
labl	Aleotti et al., 2011	Х		х		х	х			
-ur	Gao et al., 2014	Х		х	х	х	х			
apti	Li et al., 2016	Х	Х				х			
Ï	Garbaya <i>et al.</i> , 2019	Х	х					х		
	Jayasekera & Xu, 2019	X			х		x			

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¹ 2-D Virtual environment, ² Only mentioned, ³ In collaboration with Ant colony algorithm, TCT Assembly Task Completion Time, DOF Degrees of Freedom

From Table 1 it is observed that the VA planning systems reported in the literature have been evaluated in terms of its functionality and ability to simulate assembly tasks, but only two are able to generate the assembly sequence from the virtual assembly execution.

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The assembly task completion time (*TCT*) and the accessibility are the assembly metrics used in most of the systems. Only two systems are able to analyse the assembly stability. Regarding the assembly planning, only one system can generate and represent assembly plans, and very few systems perform limited evaluations of virtual assembly strategies. Thus, it can be said that although there have been several VA systems reported in the literature, most of them have focused on evaluating the feasibility of performing assembly tasks rather than on the generation of practical and optimal assembly plans. Consequently, existing VA systems can simulate product assembly tasks but they cannot perform analyses and assessments to generate useful assembly data to support the decision-making process.

3. System description

The proposed haptic-enabled VA planning and assessment approach incorporates the physical-based behaviour and collision detection into the virtual environment to generate only feasible assembly plans, similar as in the real world. Moreover, human expertise and knowledge is incorporated into the VA planning process. Therefore, feasible assembly sequences near to the optimal solution are generated as shown in Figure 1. In this way, the computational cost and time are reduced, and the planning process becomes more efficient and practical than when using existing algorithms.



Figure 1. Haptic-enabled VA planning vs. other assembly planning methods.

The new proposed haptic-enabled VA approach has been implemented in the Haptic Assembly and Manufacturing System (HAMS) (Gallegos *et al.*, 2017). The extended architecture of HAMS is shown in Figure 2 and comprises five modules:

- 1. *Input module*. Enables the importing and uploading of virtual models into the system (*.stl, *.obj, *.vtk), and the definition of the model properties.
- 2. *Graphics module*. Responsible of the graphics rendering, which includes the virtual scene and 3D models; the visualization of assembly paths, messages and assembly information; and the creation of buttons and widgets to configure the simulation parameters.
- 3. *Physics module*. Enables the physical-based behaviour of virtual objects in order to have realistic dynamic and collision responses.
- 4. *Haptic module*. Provides force feedback to the user to enable the sense of touch and kinesthesia.

 5. *Planning module*. Responsible of the assembly data logging, the analysis of the assembly movements, the generation of assembly plans and assembly metrics, and the assessment of assembly plans.



Figure 2. HAMS architecture.

The HAMS system has been implemented in Visual studio C++ using the Microsoft Foundation Class (MFC); the Visualization Tool Kit libraries (VTK 5.10) for the graphic rendering of the virtual environment; the physics simulation engines Bullet, PhysX v2.8 and PhysX v3.1; and the Open Haptics v3.0 to enable the haptic feedback by means of the Phantom Omni device from Sensable®.

The main functionalities of HAMS are haptic-enabled free manipulation of virtual objects, dynamic behaviour and collision detection of virtual objects, automatic assembly data logging (position, movements, time, etc.), automatic computation of assembly metrics, automatic generation of assembly plans from virtual assembly execution, and objective assessment of assembly plans.

4. Assembly planning

Figure 3 presents the overall procedure of the assembly planning module, which comprises two main tasks: assembly plan generation and assembly plan assessment.



Figure 3. Assembly planning procedure.

4.1 Assembly plan generation

4.1.1 Assembly parameters

Before starting the VA execution, it is necessary to define the following parameters for the calculation of the assembly metrics:

- Friction factors (f_x, f_y, f_z) , to estimate the friction work required to move a part along the X, Y, or Z directions, respectively.
- Resolution (r), to define the resolution of the VA trajectories.
- Time-scale (n_t), to estimate the real assembly times from the corresponding VA times:

$$n_t = TCT_{virtual} / TCT_{real} \tag{1}$$

From previous studies in HAMS, n_t has an average value of 17.7 ± 2 (Gallegos *et al.*, 2017).

- Sound, to enable or disable a real-life industry audio during the VA execution.

4.1.2 Virtual assembly task execution

After an assembly task has been uploaded into the system, the user can freely interact with the virtual objects by means of the haptic device, and perform the product assembly. During the VA execution, the system provides the user with the sense of touch to explore and manipulate virtual objects. The user can feel dynamic forces such as weight, inertia and collision among the virtual objects. The system tracks and logs all the information regarding the assembly sequence, trajectories and movements (positions, timestamps, speeds, etc.) made by the user during the VA execution.

4.1.3 Assembly metrics

To objectively assess assembly plans, several assembly metrics are proposed and automatically computed by the system. The proposed metrics are subdivided into part metrics and product metrics. Part metrics refer to the assembly values corresponding to each individual part, whereas product metrics refer to the assembly values corresponding to the complete product assembly task. The proposed metrics are defined as follows:

- Part handling (PH). Refers to the number of times a part is handled by the user.
- Effective handling time (*EHT*). Time duration from the grasping to the release of a part. If a part is manipulated more than once, the time is accumulated.
- Non-productive handling time (*NPHT*). Time duration from the release of the previous part to the grasping of the next part.
- Effective handling distance (*EHD*). Travelled distance from the grasping to the release of a part. If a part is manipulated more than once, the distance is accumulated.
- Non-productive handling distance (*NPHD*). Travelled distance from the release of previous part to the grasping of the next part.
- Start point (*SP*). Initial position (*x*, *y*, *z*) of the part.
- Final point (*FP*). Final position (*x*, *y*, *z*) of the part.
- Final orientation (FO). Final orientation $(\theta x, \theta y, \theta z)$ of the part.

Figure 4 illustrates the concepts of *EHD* and *NPHD*, whereas Figure 5 illustrates the concepts of *SP*, *FP* and *FO*.



Figure 4. Distance concepts involved in the VA.



Figure 5. Initial and final configuration of a part.

• **Potential energy** (*PE*). Potential energy required to manipulate a part along the assembly trajectory:

$$PE = mg(y_{max} - y_{min}) \tag{2}$$

where *m* is the mass of the part, *g* is the gravity, and y_{max} and y_{min} are the maximum and minimum elevations along the assembly trajectory.

• Effective potential energy (*EPE*). Potential energy change between the initial and the final position of a part:

$$EPE = mg(y_{final} - y_{initial})$$
(3)

where $y_{initial}$ and and y_{final} are the initial and final elevations of the part.

• Potential energy efficiency (PEE). It is defined as:

$$PEE = EPE/PE \tag{4}$$

• Total energy (*TE*). Total work or energy required to move a part along its assembly trajectory. The total energy is estimated based on the principle of virtual work as follows:

$$TE = mg\sum[\Delta_x f_x + \Delta_y f_y + \Delta_z f_z + (\Delta_y if \Delta_y > 0)]$$
(5)

where Δ_x , Δ_y , and Δ_z are the small displacements and f_x , f_y , f_z are the friction factors of the part along the X, Y and Z directions, respectively.

• Total energy efficiency (TEE). It is defined as:

$$TEE = EPE/TE \tag{6}$$

Figure 6 shows the assembly trajectory of a part, which comprises all the small displacements (Δ_x , Δ_y , Δ_z) corresponding to each simulation cycle. On the other hand, Figure 7 illustrates the *PE*, *EPE* and *TE* concepts.



Figure 6. Displacements comprising a virtual assembly path.



Figure 7. Energy concepts when moving a part.

• Effective task completion time (*ETCT*). Sum of all the *EHT* values corresponding to the *n* parts of a product:

$$ETCT = \sum_{i=1}^{n} EHT \tag{7}$$

• Non-productive task completion time (*NPTCT*). Sum of all the *NPHT* values corresponding to the *n* parts of a product:

$$NPTCT = \sum_{i=1}^{n} NPHT \tag{8}$$

• Task completion time (*TCT*). Total time to complete the product assembly:

$$TCT = ETCT + NPTCT \tag{9}$$

• Effective assembly distance (*EAD*). Total distance travelled when moving parts during the VA execution:

$$EAD = \sum_{i=1}^{n} EHD \tag{10}$$

• Non-productive assembly distance (*NPAD*). Total travelled distance when no parts are moved during the VA execution:

$$NPAD = \sum_{i=1}^{n} NPHD \tag{11}$$

• **Total assembly distance** (*TAD*). Total travelled distance during the execution of the product assembly:

$$TAD = EAD + NPAD \tag{12}$$

• Total assembly energy (*TAE*). Total work or energy required to complete the product assembly:

$$TAE = \sum_{i=1}^{n} TE \tag{13}$$

• **Total assembly energy efficiency** (*TAEE*). Energy efficiency of the entire assembly process:

$$TAEE = \sum_{i=1}^{n} EPE / \sum_{i=1}^{n} TE$$
(14)

• Assembly potential energy efficiency (*APEE*). Efficiency of the assembly process in terms of the potential energy:

$$APEE = \sum_{i=1}^{n} EPE / \sum_{i=1}^{n} PE$$
(15)

• Workspace (*WS*). Size of the workspace required to carry out the product assembly. The workspace is represented by a rectangular prism with dimensions (*dx, dy, dz*) that bounds all the assembly trajectories, as shown in Figure 8.



Figure 8. Representation of the virtual workspace.

Assembly manipulability (*AM*). It is defined as the degree of angular dexterity or manipulability required to carry out the assembly task. It is quantified as the maximum required angular amplitude of rotation around each axis ($d\theta x$, $d\theta y$, $d\theta z$) during the VA execution (yaw, pitch and roll rotations), as shown in Figure 9.



Figure 9. Representation of the assembly manipulability concept.

- Degrees of freedom (DOF). Degrees of freedom used to perform the virtual assembly.
- Total assembly handling (*TAH*). Total number of times that all parts were manipulated (grasped) during the product assembly execution:

$$TAH = \sum_{i=1}^{n} PH \tag{16}$$

• Handling efficiency (*HE*). Efficiency of the manipulation or grasping operation. It is defined as the ratio between the number of parts (*n*) and the *TAH*, as follows:

$$HE = n/TAH \tag{17}$$

4.1.4 Assembly plan

An assembly plan is automatically generated by the system after the user concludes the product assembly. This plan is saved automatically as an *.cvs file and comprises the job information, the model information, the part assembly metrics and the task assembly metrics.

4.2 Assembly plan assessment

After several assembly plans have been generated, they are analysed and evaluated to identify the best assembly plan. The GUI of the assessment analysis comprises six sections, as shown in Figure 10:

- 1. Name. Analyst's name.
- 2. *Evaluation criteria*. Shows the assembly metrics for the user to select one or more as evaluation criteria, and to define priorities.
- 3. Select the plans. Allows the selection of the assembly plans to be evaluated.
- 4. *Summary*. Presents the results of the assembly assessment, ordered from the best to the worst plan according to the selected criteria and priorities.
- 5. *Chart*. Compares the assembly plans at a glance by means of a bar chart.
- 6. Additional information. Allows saving the assessment results.



Figure 10. Assembly plan assessment GUI.

5. Case study

5.1 Description

To evaluate the functionality of the proposed approach a case study corresponding to a linear actuator was selected as shown in Figure 11. According to the number of parts, this device has 40,320 different assembly sequences (feasible and non-feasible). However, because of the dynamic behaviour and collision detection of virtual objects in HAMS, all non-feasible assembly sequences stay automatically out of the analysis. As an example, Figure 12 shows two non-feasible assembly sequences due to accessibility and stability problems.

	Part No.	Name
3	1	Plunger
	2	Rear cap
	3	Front cap
2	4	Cylinder
4	5	Screw_1
	6	Screw_2
5 7	7	Screw_3
	8	Screw_4

Figure 11. Linear actuator virtual assembly task loaded into HAMS.



Figure 12. Non-feasible assembly sequences: a) accessibility problem and b) stability

problem.

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After some preliminary tests in HAMS, the following two feasible assembly sequences were selected by the assembly specialist:

- Assembly sequence 1 (AS1): $\{2-4-1-3-5-6-7-8\}$
- Assembly sequence 2 (AS2): $\{2-1-4-3-5-6-7-8\}$

Although there are more feasible assembly sequences, such as $\{2-4-1-3-6-5-7-8\}$, $\{2-4-1-3-5-8-7-6\}$, etc., the assembly specialist decided that the two selected sequences were closer to the optimal sequence than the others.

5.2 Assembly plans

The product assembly was executed by the specialist using the two selected assembly strategies. Table 2 and Table 3 present the part and the product assembly metrics, respectively. Figure 13 shows the assembly instructions generated automatically by the system, which can be used in the real assembly process.

Table 2. Part assembly metrics.

Part	Name	Н	EHT (s)	NPHT (s)	EHD (mm)	(mm)	$SP(\mathbf{mm})$ (x, y, z)	FP (mm) (x, y, z)	$FO\left(^{\circ} ight) _{x_{y}}^{FO\left(^{\circ} ight) } \left(art art art _{x_{y}}^{\circ}art art art _{z} ight)$	<i>PE</i> (J)	TE (J)	EPE (J)	TEE (%)	PEE (%)
							Assembly	sequence 1						
7	Rear cap	1	7	0	152.7	0	0, 34, 0	6, 11, 52	-90, 0, 0	0.062	0.078	0	0	0
4	Cylinder	1	19	б	527.1	342	114, 27, 0	6, 67, 50	0, -90, -90	0.252	0.283	0.134	47.4	53.2
1	Plunger	3	18	28	470.3	2182.6	-76, 16, 42	6, 89, 50	0, -90, -90	0.662	0.674	0.256	37.9	38.6
3	Front cap	3	39	29	416.2	1665.1	0, 34, -60	6, 125, 50	90, 0, 0	0.797	0.888	0.432	48.6	54.1
5	Screw_1	ю	16	37	452.4	386.3	140, 5, 4	32, 70, 75	0, -90, -90	0.112	0.114	0.036	31.4	31.9
9	Screw_2	ю	20	28	734.2	264.5	155, 5, 4	32, 70, 25	0, -90, -90	0.115	0.200	0.035	17.3	29.9
7	Screw_3	1	5	17	637.2	373.2	170, 5, 4	-18, 70, 75	0, -90, -90	0.120	0.126	0.036	28.5	29.7
8	Screw_4	-	13	12	484.9	1920.8	185, 5, 4	-18, 70, 25	0, 90, 90	0.117	0.122	0.034	27.8	29.3
							Assembly	sequence 2						
7	Rear cap	1	8	0	120.1	0	0, 34, 0	4, 13, 44	-90, 0, 0	0.068	0.080	0	0	0
1	Plunger	1	16	б	303.3	402.3	-76, 16, 42	3, 90, 48	0, -90, -90	0.360	0.382	0.256	67.1	71.1
4	Cylinder	٢	47	26	634.9	1923.3	114, 27, 0	5, 76, 47	0, -90, -90	0.720	0.775	0.161	20.8	22.4
Э	Front cap	ю	41	56	695.0	1615.3	0, 34, -60	4, 130, 50	90, 0, 0	0.839	1.854	0.481	25.9	57.3
5	Screw_1	1	14	21	549.1	532.1	140, 5, 4	30, 78, 22	0, -90, -90	0.126	0.135	0.041	30.5	32.6
9	Screw_2	ю	11	19	503.2	451.3	155, 5, 4	30, 75, 75	0, -90, -90	0.120	0.130	0.041	31.7	34.3
٢	Screw_3	1	11	22	538.2	323.2	170, 5, 4	-22, 75, 74	0, -90, -90	0.115	0.124	0.041	32.8	35.5
8	Screw_4	Э	32	17	623.1	2006.7	185, 5, 4	-21, 78, 22	0, 90, 90	0.117	0.214	0.041	19.05	34.6

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Assembly metric	Assembly sequence 1	Assembly sequence 2
ETCT	137 s	180 s
NPTCT	154 s	164 s
TCT	291 s	344 s
EAD	3875 mm	3966 mm
NPAD	7134 mm	7254 mm
TAD	11009 mm	11220 mm
TAE	2.485 J	3.694 J
TAEE	38.75 %	28.8 %
APEE	43.04 %	43.08 %
WS	(277.6, 224.5, 206.5) mm	(263.2, 221.5, 189.2) mm
AM	$\theta_x = 180^\circ, \theta_y = 180^\circ, \theta_z = 180^\circ$	$\theta_x = 180^\circ, \theta_y = 180^\circ, \theta_z = 180^\circ$
DOF	6	6
TAH	16	20
HE	50 %	40 %

Table 3. Task assembly metrics.

	Ass	embly instru	ction of: Actuator		
	Part No.	Name		Part No.	Name
Assembly operation: 10	2	Rear cap	Assembly operation: 50	5	Screw 1
200 Om					
Assembly operation: 20			Assembly operation: 60		
M.	4	Cylinder	*	6	Screw_2
Assembly operation: 30			Assembly operation: 70	_	~ •
	1	Plunger		7	Screw_3
Assembly operation: 40			Assembly operation: 80		
* ////	3	Front cap		8	Screw_4

Figure 13. Assembly instructions corresponding to AS1.

5.3 Assembly assessment

In general, AS1 is the best assembly strategy because in most of the assembly metrics (> 70%) it obtained better values than AS2. However, the selection of the best assembly plan may depend on the particular criterion defined by the specialist.

Regarding the assembly time performance, AS1 is the best because its *TCT* value is 15% smaller than AS2. Moreover, in all time related assembly metrics (*TCT*, *ETCT* and *NPTCT*) AS1 leads to smaller values than AS2. In terms of time efficiency (*ETCT/TCT*), both assembly sequences have an efficiency of 50%, but AS1 is faster than AS2. Considering a time scale factor of 17.7 (Gallegos *et al.*, 2017), the expected *TCT* values in the real assembly process are 16.4 and 19.4 seconds for AS1 and AS2, respectively. Concerning the assembly travelled distance; the results show that AS1 requires a smaller travelled distance than AS2. The assembly distance efficiency (*EAD/TAD*) is 36% for both sequences. Figure 14 shows some of the assembly trajectories corresponding to AS1.



Figure 14. Visualization of the AS1 trajectories: a) cylinder assembly and b) complete

assembly.

The results evidence that AS1 needs only 67% of the energy (*TAE*) required by AS2. This performance is also observed in the *TAEE* metric, where the energy efficiencies of AS1 and AS2 are 38.8% and 28.8%, respectively. These results are because in the AS2 the plunger is assembled before the cylinder, leading to eccentricity problems that cause interferences and require more manipulation movements during the cylinder assembly, as shown in Figure 15. In addition, the *PH* and *EHT* metrics for the cylinder are 1 and 19s for AS1, respectively, and 7 and 47s for AS2, confirming that AS2 requires more grasping and manipulation operations than AS1.



Figure 15. Cylinder assembly differences: a) AS2 and b) AS1.

Regarding part grasping (*TAH*), AS1 is better than AS2 since it requires only 16 grasping operations while AS2 requires 20 operations. This performance is also observed in the *HE* values, being 50% for AS1 and 40% for AS2.

The results also shows that AS2 requires a smaller workspace (WS) volume (11 030.1 cm³) than AS1 (12 869.3 cm³); being the main difference in the elevation. This WS information is relevant for the assembly cell design and its integration into a production

line (factory planning). In the case of robotic assembly, the information is useful to define the robot workspace.

Lastly, AS1 and AS2 are equally complex because both require an angular manipulability of 180° around each coordinate axis (*AM*) and 6 degrees of freedom (*DOF*).

6. Discussion

The case study results have shown that the proposed haptic-enabled virtual approach is an effective tool to plan and objectively assess product assembly. The system is able to generate assembly plans from the VA execution. Moreover, by incorporating the experience of the specialist in the virtual assembly environment, the number of assembly plans to be generated and evaluated are reduced, and therefore the efficiency of the assembly planning process increases. The objective assessment of a product assembly is based on the quantification and comparison of new proposed assembly metrics, which are related to the assembly performance. These assembly metrics are automatically calculated from the information logged during the VA execution, and quantify the assembly performance in terms of time, distance, energy and efficiency.

Note that the values of the assembly metrics calculated from the virtual assembly information may differ from the values corresponding to the real assembly process; however, the behaviour and tendencies of the virtual and the real assembly tasks are the same (Gonzalez-Badillo *et al.*, 2014; Gallegos-Nieto *et al.*, 2017). Therefore, the VA evaluation is valid and useful, and the metrics can be adjusted to reproduce the real assembly values. Finally, it can be said that the proposed VA planning approach generates a large amount of technical data that can be used to support the decision-making process along the entire product life cycle, leading to time and cost reductions.

7. Conclusions

A new method for the generation and objective evaluation of product assembly using virtual reality and haptics has been presented. The proposed method is based on the execution and data recording of the product assembly in a haptic-enabled virtual environment. For each completed assembly task, the system automatically generates the assembly plan and computes a set of assembly metrics, *which are used to objectively evaluate the* assembly strategies. The results have shown that the proposed approach is feasible, effective, and able to generate more useful and practical information than existing methods and systems. Moreover, the integration of haptics, physical-based behaviour, assembly logging, assembly metrics, and the experience and knowledge of the specialist, has led to a more intuitive, practical, objective and efficient assembly planning system.

Acknowledgments

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Figure 2. HAMS architecture.

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Figure 3. Assembly planning procedure.



Figure 4. Distance concepts involved in the VA.



Figure 5. Initial and final configuration of a part.



Figure 6. Displacements comprising a virtual assembly path.



Figure 7. Energy concepts when moving a part.



Figure 8. Representation of the virtual workspace.



Figure 9. Representation of the assembly manipulability concept.

	TDAC Total dead assembly difficent TAE Total assembly efficient AE Assembly efficiency V/S Work space AM Angular manipulability DOP Degrees of freedom Heading efficiency Heading efficiency	stance Slow Inc.	hart ruction Ideo	Assembly name Cylinder Best value the shortest time: Location of the bes C:\Users\UASLP\D	206 s assembly plan esktop \Pruebas_Pla	ineacion (Secuen	icia_11/EGN_		Bar 1 Bar Assemb	2 Bar 3 Bar 4 D lies evalua	#F 5	
6 M	Name file Sequence	TAT (min:seg) TEAT (n	n:seg) TDAT (mir	n:seg) TEAD (mm)	TDAD (mm)	TAE	AE	WS (XYZ)	AM (AxAyAz)	DOF	HE	
	EGN_4.Csv 37-31-30-36 EGN_2.csv 37-31-30-36	3:26 1:53 4:38 2:4	1:33 2:34	3665.13 4581.65	11348.84 11646.53	9285	286	280.40; 226 262.48; 243	180.00; 96.5 180.00; 173	6	15	
	EGN_1.csv 37-31-30-36	4:54 2:35	2:19	4974.09	19498.46	3031	589	277.62; 224	180.00; 182	6	28	
	EGN_3.csv 37-31-30-36	5:36 2:45	2:51	9554.58	33849.68	3448	183	310.96; 223	180.00; 180	6	20	

Figure 10. Assembly plan assessment GUI.



Figure 11. Linear actuator virtual assembly task loaded into HAMS.



Figure 12. Non-feasible assembly sequences: a) accessibility problem and b) stability problem.





Figure 13. Assembly instructions corresponding to AS1.



Figure 14. Visualization of the AS1 trajectories: a) cylinder assembly and b) complete assembly.



(b) Figure 15. Cylinder assembly differences: a) AS2 and b) AS1.



				Assembly metrics				Assen	nbly pla	anning
	VA system	System evaluation	Sequence generation	TCT	DOF	Stability	Accessibility	Generation	Representation	Assessment
	Xia et al., 2011	Х		Х			X			
	Thing et al., 2010	Х		х			x			
	Bordegoni et al., 2009	Х		Х			х			
_	Vo et al., 2009	Х		Х			х			
bleć	Garbaya <i>et al.</i> , 2007	Х		Х			х			
ena	Adams et al., 2001	Х		Х			х			
tic-	Yoo, 2011	Х		Х	Х		х			\mathbf{X}^1
Hap	Seth et al., 2006	Х		х			х			\mathbf{x}^2
, ,	Jia <i>et al.</i> , 2009	Х		Х			х			
	Ladeveze et al., 2010	Х		Х			х			
	Hassan <i>et al.</i> , 2010	Х					х			x ³
	Gonzalez et al., 2014	Х	Х	х		х	х	х	х	
	Boud et al., 2000	Х		Х			х			
	Brough <i>et al.</i> , 2007	Х		х						
led	Jayaram <i>et al.</i> , 2007	Х	Х							
nab	Aleotti et al., 2011	Х		х		х	х			
ic-u	Gao et al., 2014	Х		х	х	х	х			
apti	Li et al., 2016	Х	Х				x			
Η	Garbaya <i>et al.</i> , 2019	Х	Х					х		
	Jayasekera & Xu, 2019	Х			х		x			

Table 1	VA sy	vstems	for	assembl	v n	lannino
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¹ 2-D Virtual environment, ² Only mentioned, ³ In collaboration with Ant colony algorithm, TCT Assembly Task Completion Time, DOF Degrees of Freedom

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Table 2. Part assembly metrics.

Part	Name	Hd	EHT (s)	NPHT (s)	EHD (mm)	(um)	SP(mm) (x, y, z)	FP (mm) (x, y, z)	$FO \stackrel{(0)}{_{x_{y}}} \stackrel{(0)}{_{y_{y}}} \stackrel{(0)}{_{y_{y}}} \stackrel{(0)}{_{y_{y}}}$	<i>PE</i> (J)	TE (J)	EPE (J)	TEE (%)	PEE (%)
							Assembly :	sequence 1						
7	Rear cap	1	٢	0	152.7	0	0, 34, 0	6, 11, 52	-90, 0, 0	0.062	0.078	0	0	0
4	Cylinder	1	19	б	527.1	342	114, 27, 0	6, 67, 50	0, -90, -90	0.252	0.283	0.134	47.4	53.2
1	Plunger	ŝ	18	28	470.3	2182.6	-76, 16, 42	6, 89, 50	0, -90, -90	0.662	0.674	0.256	37.9	38.6
3	Front cap	3	39	29	416.2	1665.1	0, 34, -60	6, 125, 50	90, 0, 0	0.797	0.888	0.432	48.6	54.1
5	Screw_1	3	16	37	452.4	386.3	140, 5, 4	32, 70, 75	0, -90, -90	0.112	0.114	0.036	31.4	31.9
9	Screw_2	ŝ	20	28	734.2	264.5	155, 5, 4	32, 70, 25	0, -90, -90	0.115	0.200	0.035	17.3	29.9
٢	Screw_3	1	5	17	637.2	373.2	170, 5, 4	-18, 70, 75	0, -90, -90	0.120	0.126	0.036	28.5	29.7
8	Screw_4	1	13	12	484.9	1920.8	185, 5, 4	-18, 70, 25	0, 90, 90	0.117	0.122	0.034	27.8	29.3
							Assembly	sequence 2						
7	Rear cap	1	8	0	120.1	0	0, 34, 0	4, 13, 44	-90, 0, 0	0.068	0.080	0	0	0
1	Plunger	1	16	б	303.3	402.3	-76, 16, 42	3, 90, 48	0, -90, -90	0.360	0.382	0.256	67.1	71.1
4	Cylinder	٢	47	26	634.9	1923.3	114, 27, 0	5, 76, 47	0, -90, -90	0.720	0.775	0.161	20.8	22.4
ю	Front cap	б	41	56	695.0	1615.3	0, 34, -60	4, 130, 50	90, 0, 0	0.839	1.854	0.481	25.9	57.3
S	Screw_1	1	14	21	549.1	532.1	140, 5, 4	30, 78, 22	0, -90, -90	0.126	0.135	0.041	30.5	32.6
9	Screw_2	б	11	19	503.2	451.3	155, 5, 4	30, 75, 75	0, -90, -90	0.120	0.130	0.041	31.7	34.3
٢	Screw_3	1	11	22	538.2	323.2	170, 5, 4	-22, 75, 74	0, -90, -90	0.115	0.124	0.041	32.8	35.5
8	Screw_4	3	32	17	623.1	2006.7	185, 5, 4	-21, 78, 22	0, 90, 90	0.117	0.214	0.041	19.05	34.6

Assembly Automation

Assembly metric	Assembly sequence 1	Assembly sequence 2
ETCT	137 s	180 s
NPTCT	154 s	164 s
TCT	291 s	344 s
EAD	3875 mm	3966 mm
NPAD	7134 mm	7254 mm
TAD	11009 mm	11220 mm
TAE	2.485 J	3.694 J
TAEE	38.75 %	28.8 %
APEE	43.04 %	43.08 %
WS	(277.6, 224.5, 206.5) mm	(263.2, 221.5, 189.2) mm
AM	$\theta_x = 180^\circ, \theta_y = 180^\circ, \theta_z = 180^\circ$	$\theta_x = 180^\circ, \theta_y = 180^\circ, \theta_z = 180^\circ$
DOF	6	6
TAH	16	20
HE	50 %	40 %

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The authors would like to thank the editor for the work and comments provided in order to improve the quality of the manuscript before its publication. The manuscript has been revised and the following changes have been made. Major changes have been highlighted as red text in the document.

Response to Editor's comments

- 1. Before we proceed to publication I would like to invite you to read the attached draft guidelines for authors 'How to publish in Assembly Automation'. Our aim is to help you maximise the impact of your manuscript so that it is as widely downloaded and cited as possible.
- *R*: The guidelines "How to publish in Assembly Automation" were carefully reviewed and the manuscript was modified according to them.
- 2. At this stage the most appropriate section of the attached guide is 'Pre-accept' and under this heading I would like you to improve/correct the following aspects:

-
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- L Z R: The entire paper has been formatted according to the provided guide. The English grammar has been also carefully revised. All references have been formatted according to the Harvard style and checked for completeness, accuracy and consistency. Figures have been also revised and none of them requires copyright since the authors created all figures.
- 3. Please also consider the comments under 'How to submit a Manuscript' that relate to the title and structured abstract. I am not suggesting that you should change them - just that you consider if they could be further optimised.
- *R*: *The title of the paper has been revised and modified to eight words. The structured abstract* was also revised and modified to remove the use of personal pronouns within the structured abstract and body of the paper.

Once again, the authors greatly appreciate the valuable comments provide by the editor. We believe that the quality of the revised manuscript has been largely improved.