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ABSTRACT

We demonstrate a thin-film flip-chip (TFFC) light-emitting diode (LED) emitting in the ultraviolet B (UVB) at 311 nm, where substrate removal has been achieved by electrochemical etching of a sacrificial $\text{Al}_{0.37}\text{Ga}_{0.63}\text{N}$ layer. The electroluminescence spectrum of the TFFC LED corresponds well to the as-grown LED structure, showing no sign of degradation of structural and optical properties by electrochemical etching. This is achieved by a proper epitaxial design of the sacrificial layer and the etch stop layers in relation to the LED structure and the electrochemical etch conditions. Enabling a TFFC UV LED is an important step toward improving the light extraction efficiency that limits the power conversion efficiency in AlGaIn-based LEDs.

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Ultraviolet (UV) light sources are used in a number of applications such as water disinfection, UV curing, and phototherapy.¹ UV light-emitting diodes (LEDs) are expected to replace conventional UV light sources like mercury gas discharge lamps due to their small form factor, robustness, environmentally friendly materials, and selectable emission wavelength.² However, the poor power conversion efficiency of UV LEDs below 10% for wavelengths shorter than 350 nm, see Ref. 2, strongly limits their widespread use.

One of the major factors limiting the power conversion efficiency is the light extraction efficiency (LEE),² which can be improved by a thin-film flip-chip (TFFC) design. Aoshima *et al.*³ have fabricated TFFC LEDs emitting in the ultraviolet A (UVA) and achieved an improvement in the LEE of $1.7\times$ compared to a flip-chip (FC) design. Sung *et al.*⁴ demonstrated an improvement in the LEE for ultraviolet C (UVC) LEDs of $1.31\times$ for a TFFC design compared to a FC design. In both the cases, a major factor for the improvement was the surface roughening to reduce total internal reflection, which was made possible by removing the substrate. The influence of the surface roughening on the LEE for TFFC LEDs emitting in the UVA and UVC has also been reported by other groups.^{5–8}

Despite these demonstrations using laser lift-off (LLO) for the fabrication of UV TFFC LEDs,^{3–5,7,8} substrate removal remains challenging. LLO is a standard process for GaN-based LEDs emitting in

the blue,⁹ but for AlGaIn-based LEDs, the thermal decomposition of AlGaIn yields aluminum residues that are more rigid than Ga residues as in the case of GaN.¹⁰ In addition, the substrate removal by LLO can lead to cracking of the strained epitaxial layers due to the thermal shock that is enhanced since AlGaIn requires higher temperature to decompose.^{10,11} To circumvent these issues, a GaN interlayer has been used for LLO, which was completely removed afterwards using dry etching to avoid optical absorption of the UV emission from the LED.¹² The integration of such a non-lattice matched layer can lead to dislocation generation, relaxation, and roughness of the layers grown on top,^{13,14} which strongly limits the aluminum contents and layer thicknesses that can be used for the LED structure grown on top.

An alternative to thermal decomposition of AlGaIn for the substrate removal is doping-selective electrochemical etching. This has been used to laterally etch GaN and low Al composition AlGaIn layers for the fabrication of thin-film LEDs emitting in the blue regime,^{15–17} transfer of III-nitride membranes,^{18–21} and fabrication of photonic crystal structures.²² Electrochemical etching has low requirements on the processing equipment and can be accomplished using standard electroplating tools. This is in contrast to photoelectrochemical etching that is based on bandgap-selective absorption.^{23,24} Therefore, photoelectrochemical etching requires a more complex setup with a wavelength-specific homogeneous illumination. Thus, for photoelectrochemical etching, the

sacrificial layer and device layers have to be designed with respect not only to selective current flows as in electrochemical etching but also to selective optical absorption, which, in most cases, involves the use of non-lattice matched sacrificial layers.

Recently, we have demonstrated that electrochemical etching can be applied to etch AlGaN with an Al content up to 50%.²⁵ This opens up the possibility to incorporate a lattice matched sacrificial AlGaN layer that can be selectively removed to realize TFCC UV LEDs of high quality. In this work, we demonstrate a TFCC ultraviolet B (UVB) LED using this method.

The epitaxial layer structure of the UVB LED including the layers required for the electrochemical etching is shown in Fig. 1. The structure was grown in a $3 \times 2''$ close-coupled showerhead reactor using the standard precursors trimethylaluminum (TMAl), trimethylgallium (TMGa), trimethylindium (TMIn), and ammonia (NH_3) with hydrogen or nitrogen as the carrier gas. Silane (SiH_4) was used as a n-dopant source and cyclopentadienyilmagnesium (Cp_2Mg) as a p-dopant. First, an AlN/AlGaN-superlattice for strain management was grown on an AlN/sapphire substrate¹³ provided by the Ferdinand-Braun-Institut. This was followed by a $4 \mu\text{m}$ thick relaxed silicon doped $\text{Al}_{0.5}\text{Ga}_{0.5}\text{N}$ -layer with a Si concentration of $2 \times 10^{18} \text{ cm}^{-3}$ to complete the quasi-substrate.^{14,26} After that, a 130 nm thick $\text{Al}_{0.37}\text{Ga}_{0.63}\text{N}:\text{Si}$ sacrificial layer with a Si-concentration of $2 \times 10^{19} \text{ cm}^{-3}$ was sandwiched between two 240 nm thick $\text{Al}_{0.5}\text{Ga}_{0.5}\text{N}:\text{Si}$ etch-stop layers with a reduced Si-concentration of $0.5 \times 10^{18} \text{ cm}^{-3}$. On top of that, the $\text{Al}_{0.5}\text{Ga}_{0.5}\text{N}:\text{Si}$ current spreading layer for the LED was grown. This was followed by a threefold InAlGaN MQW active region emitting at 311 nm, an $\text{Al}_{0.75}\text{Ga}_{0.25}\text{N}$ electron blocking layer, and a Mg-doped AlGaN/AlGaN superlattice with an average Al concentration of 50% and a Mg concentration of $7 \times 10^{19} \text{ cm}^{-3}$. Finally, the structure was capped by a 20 nm thick GaN:Mg contact layer. The threading dislocation density of the epitaxial layers is around $3 \times 10^9 \text{ cm}^{-2}$.

The process flow for the TFCC LEDs is summarized in Figs. 2(a)–2(d), 3(a), and 3(b). The fabrication started with the definition of the LED's emission area. A circular mesa with a diameter of $80 \mu\text{m}$ was defined by standard photolithography and chlorine-based reactive ion etching into the n-doped $\text{Al}_{0.5}\text{Ga}_{0.5}\text{N}$ current spreading layer of the LED. An additional dry etching step into the bottom n-doped $\text{Al}_{0.5}\text{Ga}_{0.5}\text{N}$ -layer, used as the etch stop layer, was performed to expose the n-doped $\text{Al}_{0.37}\text{Ga}_{0.63}\text{N}$ sacrificial layer. This etch also

20 nm	p-GaN		
200 nm	p-AlGaN SL		
	InAlGaN/AlGaN MQWs	EBL	LED structure
730 nm	n- $\text{Al}_{0.5}\text{Ga}_{0.5}\text{N}$		
240 nm	n- $\text{Al}_{0.5}\text{Ga}_{0.5}\text{N}$	Etch block	
130 nm	n ⁺ - $\text{Al}_{0.37}\text{Ga}_{0.63}\text{N}$	Sacrificial layer	Release structure
240 nm	n- $\text{Al}_{0.5}\text{Ga}_{0.5}\text{N}$	Etch block	
4.25 μm	n- $\text{Al}_{0.5}\text{Ga}_{0.5}\text{N}$	Current spreader	
	Buffer layer		
	AlN/Sapphire template		

FIG. 1. Epitaxial structure of the UVB LED and the layers required for substrate removal by electrochemical etching.

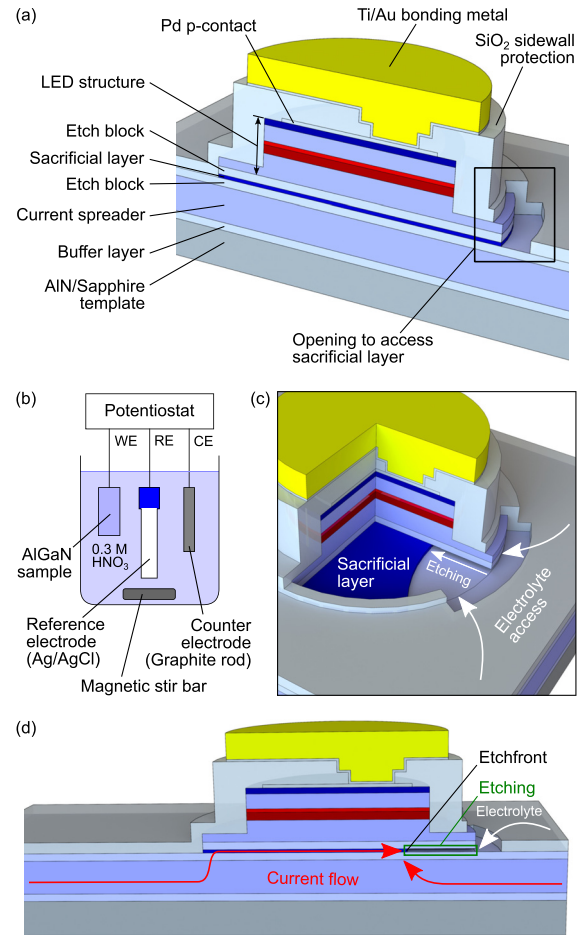


FIG. 2. (a) Sample structure after the p-side processing, (b) three-electrode setup for electrochemical etching, (c) sacrificial layer removal, and (d) current flow during electrochemical etching.

defined the area to be lifted-off. The contact pad for the electrochemical etching consisting of Ti/Al/Ti/Au (20/80/40/100 nm) was deposited on one end of the sample using electron-beam evaporation and annealed for 1 min at 900°C in a N_2 atmosphere. A 50 nm Pd p-contact was then evaporated on top of the double mesa and annealed for 1 min at 550°C in the N_2 atmosphere. To protect the doped epitaxial LED layers from parasitic etching during the electrochemical process, a SiO_2 layer was deposited on the sample using sputtering. In a first dry etching step, the SiO_2 layer was etched down beside the mesa to 300 nm to obtain a thinner tether layer, while its full thickness of $1 \mu\text{m}$ was kept on top of the mesa to create a larger distance between the mesa top and the sample surface to facilitate bonding. In a second dry etching step, the SiO_2 layer was opened up at three different locations: on top of the mesas to access the p-contact layer, at one point at the mesa edge to expose the sacrificial layer, and on the n-contact pad used for electrochemical etching. Subsequently, a Ti/Au pad for bonding and contacting was deposited on top of the mesa by tilted e-beam evaporation. The device structure after the p-side processing is shown in Fig. 2(a).

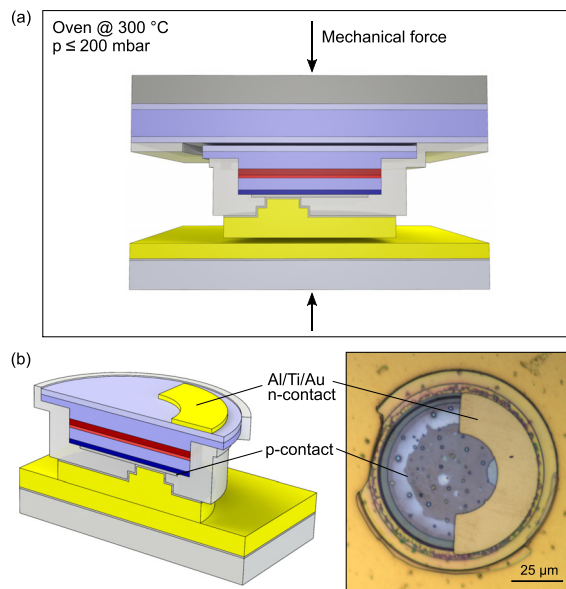


FIG. 3. (a) Flip-chip bonding in the vacuum oven and (b) schematic and optical microscope image of the thin-film flip-chip LED before the n-contact annealing.

To release the LEDs from the substrate, the sacrificial layer was laterally removed using electrochemical etching. In this step, the sample was immersed in 0.3 M nitric acid and electrically connected to a Biologic potentiostat in a three-electrode setup, see Fig. 2(b). To prevent parasitic etching, the electrical connection to the sample was protected from the electrolyte. A graphite rod was used as the counter electrode to drive the required current through the sample in order to achieve the set potential on the sample relative to the Ag/AgCl reference electrode. The electrolyte was stirred with a magnetic stir bar, and etching was conducted at room temperature with no intentional illumination. An etching voltage of 25 V vs the Ag/AgCl reference electrode was chosen to achieve complete removal of the n-doped $\text{Al}_{0.37}\text{Ga}_{0.63}\text{N}$ sacrificial layer, as shown in Ref. 25, and still to prevent etching of the etch stop and doped device layers. The lower Al composition and higher doping of the sacrificial layer relative to the etch block layers on both the sides confine the etching to only the sacrificial layer. Because the sacrificial layer is only exposed to the electrolyte at one side of the mesa, the etching proceeds across the mesa from one direction in one step, see Fig. 2(c). The SiO_2 sidewall protection further ensures a good current flow throughout the full electrochemical etch process and constant etching conditions, see Figs. 2(c) and 2(d). After the etching process, the sample was immersed in de-ionized water for 1 min to dissolve acid residues and then immersed in isopropanol to reduce any force on the membrane when allowed to dry in air. The underetched LEDs were held in place by the SiO_2 tethers. To flip-chip bond the underetched thin-film LEDs, thermocompression bonding was used. Prior to the bonding, the bonding metal surfaces on both the LED devices and the Si carrier chip with a Ti/Au (10/300 nm) bonding layer were cleaned by UV-ozone. Subsequently, the chips were pressed together using an in-house designed stainless-steel compression fixture that was placed in an oven at 300 °C for 2 h, see Fig. 3(a). The bonding pressure on

the bond pad area was set to 50 MPa. To reduce air pockets, the oven was evacuated to a pressure ≤ 200 mbar. During the bonding process, the SiO_2 tethers break and the thin-film LEDs are transferred to the Si carrier.

The device process was completed by the formation of an Al/Ti/Au (100/20/30 nm) n-contact on top of the mesa as shown in the optical microscope image in Fig. 3(b). An annealing temperature of 550 °C for the n-contact was chosen to minimize the degradation of the p-contact. The cross-sectional SEM image of the final TFFC LED achieved by a focused-ion-beam-cut shows well-defined device layers and indicates a smoothly etched surface as seen in Fig. 4. Moreover, the device layers show no indication of being porosified by the electrochemical etch process. An improper combination of doping levels, thicknesses, and Al compositions of the LED layers and etch stop layer in relation to the sacrificial layer and etch voltage would result in undesired porosification with pore diameters of 50 nm–100 nm,²⁷ which would clearly be visible in the cross-sectional SEM image. In addition, time-resolved photoluminescence (PL) measurements yielded similar PL decay times of 340 ± 30 ps at room temperature for the quantum wells in the as-grown LEDs and in the TFFC LEDs, indicating no degradation of the active region.²⁵

Figure 5 shows the electroluminescence spectrum at room temperature of the TFFC LED at a current density of 0.8 A/cm^2 with a single emission peak at 311 nm. This corresponds well to the electroluminescence peak wavelength of 312 nm of the as-grown LED structure that was contacted using an In-dot, for which the emission was collected through the sapphire substrate. The full width at half maximum for the TFFC LED is 9 nm and 11 nm for the as-grown LED structure.

Figure 6 shows the voltage and optical output power as a function of current density for a TFFC LED with a p-contact diameter of $68 \mu\text{m}$. The electroluminescence was measured using a broad-area UV-enhanced Si photodiode S2281 from Hamamatsu. The graph shows a linear output power vs current density, as expected for an LED. This proof-of-principle device is not optimized for high light extraction efficiency, and therefore, the optical output power that is in the low μW regime is stated in arbitrary units. A homogeneous current injection across the p-contact area is assumed when calculating the current density. However, near-field imaging of the spontaneous emission at a current of 0.2 mA [see Fig. 7(b)] shows that this is an underestimation of the current density due to a non-homogeneous

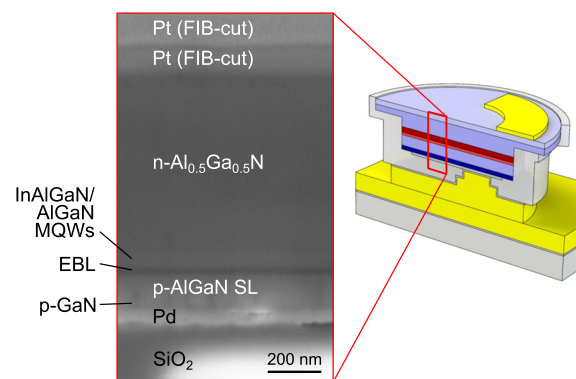


FIG. 4. Cross-sectional SEM image of the transferred LED structure.

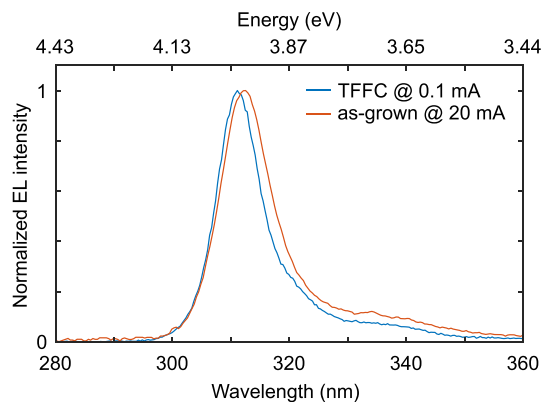


FIG. 5. Normalized electroluminescence spectrum of the as-grown epitaxy and the TFCC LED at room temperature.

current injection caused by a degraded p-contact. The voltage vs current density reveals a high differential resistance of the LED of about $63 \text{ k}\Omega$ at $3 \text{ A}/\text{cm}^2$. This is attributed to a highly resistive n-contact as the fabrication process was not optimized for the N-polar backside with low n-type doping, additionally hindered by the limited annealing temperature to avoid damaging of the LED and possible degradation of the p-contact. A different process flow, where the n-contact can be annealed before the p-contact, could solve these issues.

In conclusion, we have demonstrated a thin-film flip-chip UVB LED where the substrate removal was achieved by lateral electrochemical etching of an AlGaN sacrificial layer. The LED structure was not structurally or optically affected by the substrate removal technique, through a proper design of the sacrificial layer (doping level, thickness, and Al composition) in relation to the etch stop layer and the device layers, and choice of the etch voltage. The electroluminescence spectrum shows a single peak emission at 311 nm for the thin-film flip-chip LED, which corresponds to the emission wavelength of the as-grown LED structure, indicating no significant strain being introduced or released in the thin-film flip-chip process. The high series resistance of the LED was attributed to high contact resistance caused by a non-optimized annealing temperature and n-contacts on low-doped, N-polar AlGaN. An alternative process flow, where the n-contact is

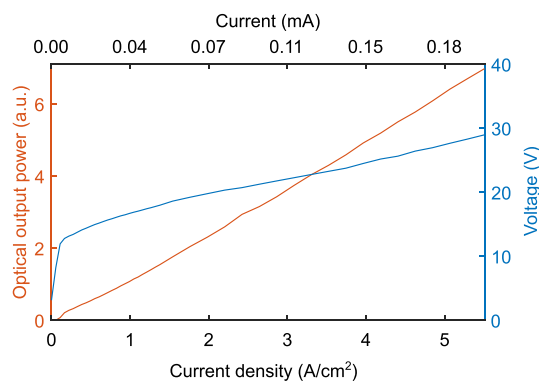


FIG. 6. P-I-V characteristics of the TFCC LED.

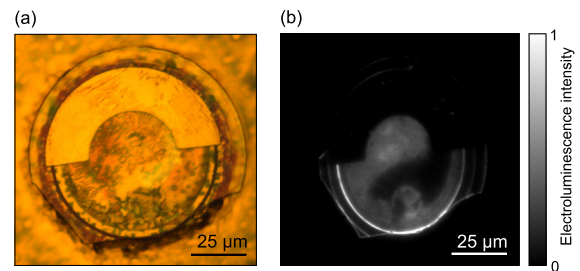


FIG. 7. (a) Optical microscope image of the TFCC LED and (b) spatially resolved near-field emission at a current of 0.2 mA . Electroluminescence intensity is on a linear scale.

annealed before the p-contact, should solve this issue. The developed thin-film process is not limited to UVB LEDs but can also be applied to deep-UV LEDs and other devices such as UV vertical-cavity surface-emitting lasers that benefit from the integration of high-quality III-nitride device layers with other structures such as dielectric distributed Bragg reflectors.

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