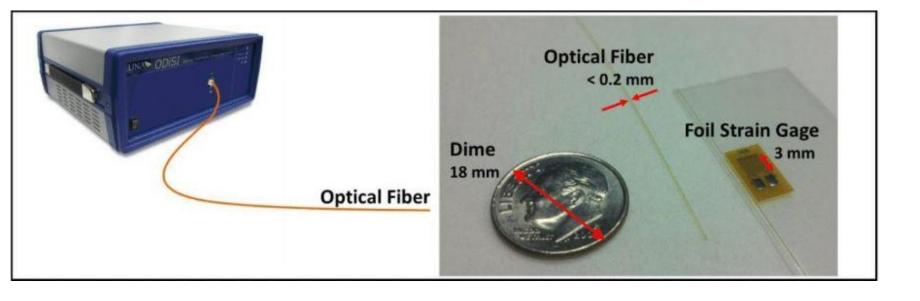


#### Introduction

The goal of this project is to optimize the existing optical dynamic monitoring conditions, OFDR can be implemented in frequency-domain reflectometry (OFDR) method to facilitate virtually any SHM application. To date, only preliminary studies dynamic structural health monitoring using Distributed Optical have been performed under laboratory conditions to evaluate Fiber Sensors (DOFS) under field conditions. These sensors offer dynamic measurements using OFDR. Thus, this study aims at developing an optimized OFDR for dynamic monitoring using a cost-effective solution that reveals temperature, strain, and DOFS under field conditions. A laboratory experimental program vibration information from any point along the entire length of an optical fiber. However, one of the biggest challenges that hinder and field monitoring program has been developed to validate static the wide implementation of DOFS is the dynamic monitoring and dynamic measurements with conventional sensors, capability under field conditions. Although several efforts have respectively. The research team has established collaboration with been made to improve the dynamic monitoring capability of the Florida Department of Transportation and other industrial DOFS using polarization-optical time-domain reflectometry partners/agencies. The research related to distributed optical fiber (OTDR), OTDR is limited to a spatial resolution of  $\sim 1$ m. sensing is still in the early stages of development. Successful execution of this project will give ERAU a great advantage in our signature SHM field.

The cost to improve the spatial resolution of OTDR is very high and limits its suitability. On the other hand, optical frequency-domain reflectometry (OFDR) technique offer high spatial resolution. If similar performance can be achieved under

# Structural Health Analysis Data Collection Equipment



Luna DOFS System

Fiber Optic Sensor



# Development of Spectral Analysis Algorithm

Because Rayleigh scattering is independent of temperature and strain, the Rayleigh backscatter profile of an optical fiber depends on its heterogeneous permittivity, which varies randomly along the length of the fiber. Thus, when the external stimulus causes a shift of permittivity, it consequently causes a spectral shift. Considering a singlemode optical fiber in which the permittivity of the core varies along the axis, based on equation, the steady-state Maxwell propagation can be described as

$$\frac{\partial^2 E}{\partial z^2} + \beta^2 \left[ 1 + \frac{\Delta \varepsilon(z)}{\varepsilon} \right] E = 0$$

Domain

$$\frac{\partial^2 \Psi}{\partial z^2} - 2i f$$

is the constant amplitude of the forwarding traveling wave;  $E_0$  $\Psi(z,\beta)$  is the spatially varying amplitude of the backward-traveling wave.

#### Development of New De-noising Method

- The interference of sinusoidal waveforms with random amplitudes generates fading noise. Fading noise presents a fantastic debacle for dynamic monitoring using Rayleigh-based OFDR.
- The result of fading noise is that the total amplitude fluctuates, which strongly restricts the possibility of detecting small reflections in the fiber.
- A new de-noising method is proposed to remove fading noise and optimize the signal strength. Singular-spectrum analysis (SSA) has been proven in many previous studies to be an efficient method to address the noise level of the sample.
- □ In this study, a Monte-Carlo based SSA method will be developed to minimize the noise effects. Compared to ordinary SSA, Monte-Carlo SSA (MC-SSA) takes the statistical significance of the signal into consideration.

**Optimization of Optical Frequency-domain Reflectometry for Dynamic Structural Health Monitoring using Distributed Optical Fiber Sensors** PI: Dan Su, Co-PI: Jeff Brown, Daewon Kim Vishal Verma, Parker Brooks, Ricardo Robalino

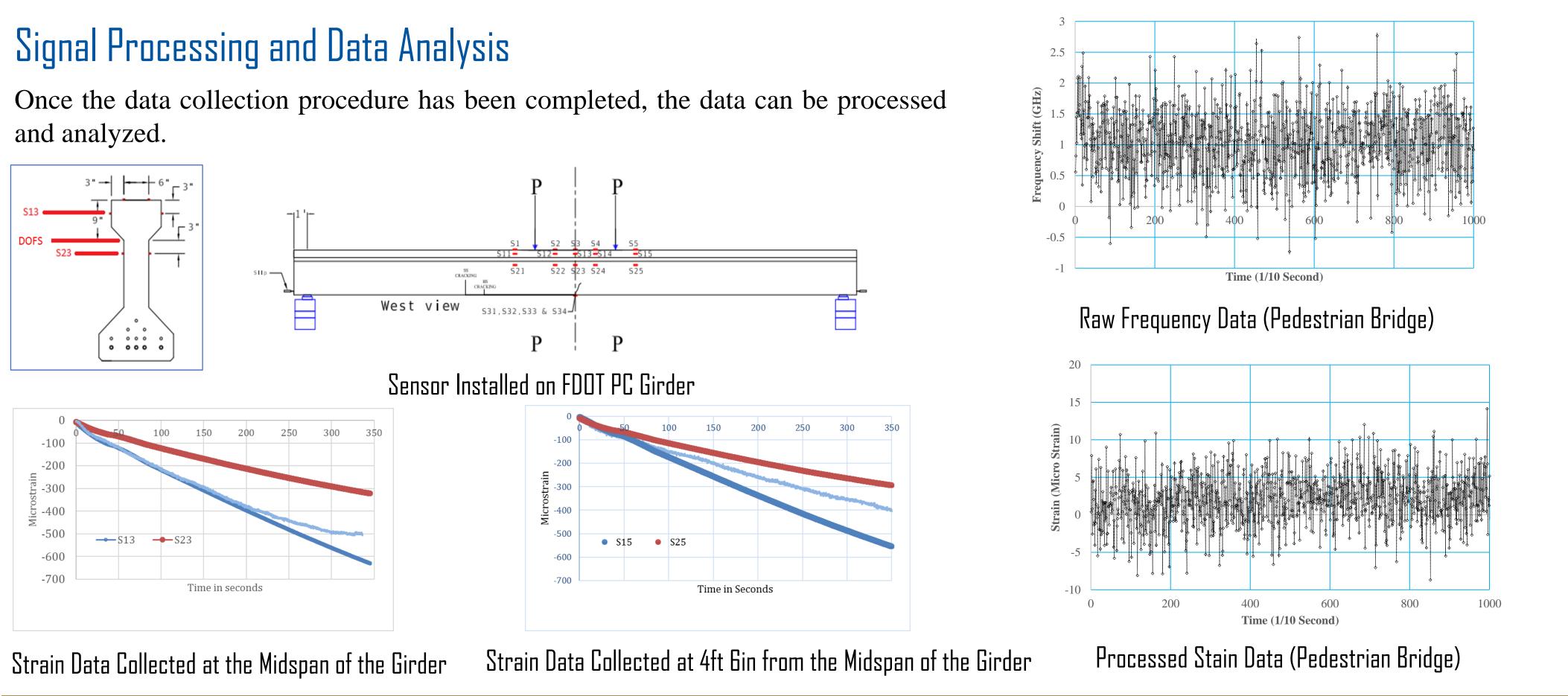


The field experimental study was performed on Student Village Pedestrian Bridge. Strain data was collected at peak traffic hours using both DOFS and STS strain transducer system. The data collected from DOFS was compared and validated with STS data. The data collected also used to develop spectral analysis algorithm.

The experimental test conducted at FDOT structure laboratory was first time applying OFDR-based distributed optical fiber sensor (DOFS) to a full size prestressed concrete girder flexural test

FDOT Structural Research Center Reinforced Girder Test



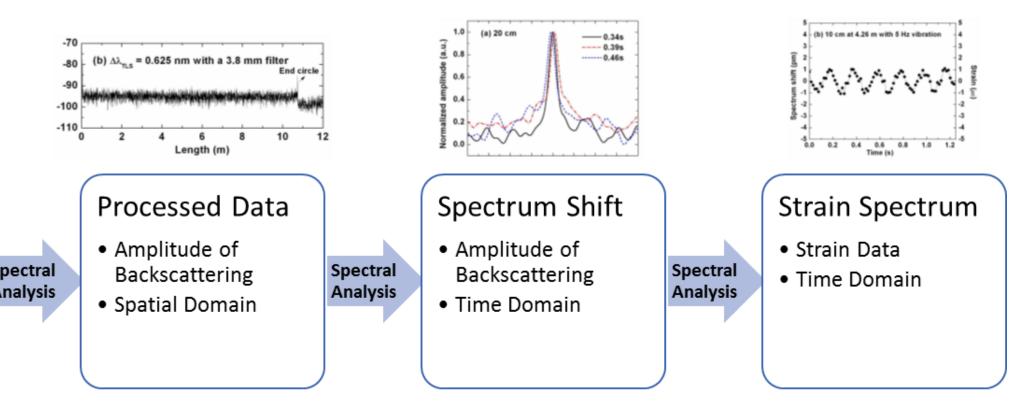


Strain Data Collected at the Midspan of the Girder

Luna Fiber Optic Sensor along with BDI STS Data Acquisition system to verify results



FDOT Structural Research Center Reinforced Girder Test



Flowchart of Spectral Analysis Processes

 $E = E_0 \exp(i\beta z) + \Psi(z,\beta) \exp(-i\beta z)$ 

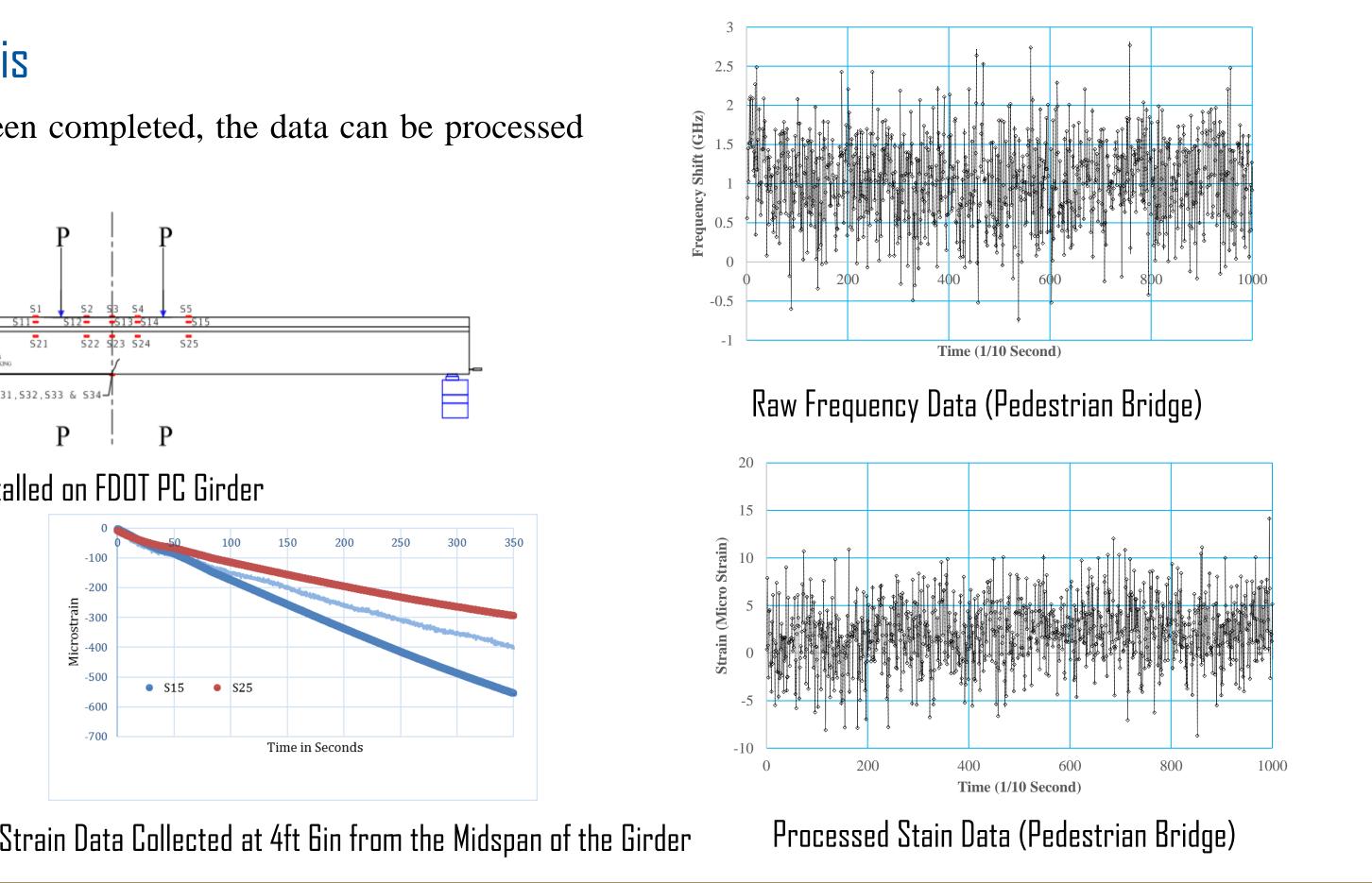
 $\beta \frac{d\Psi}{dz} + \beta^2 \frac{\Delta \varepsilon(z)}{2} E_0 \exp(2i\beta z) + \beta^2 \frac{\Delta \varepsilon(z)}{2} \Psi = 0$ 

A new MC-SSA method will not only minimize the noise effects but will also enhance the quality of spectrum reconstruction.

### Field Data Collection

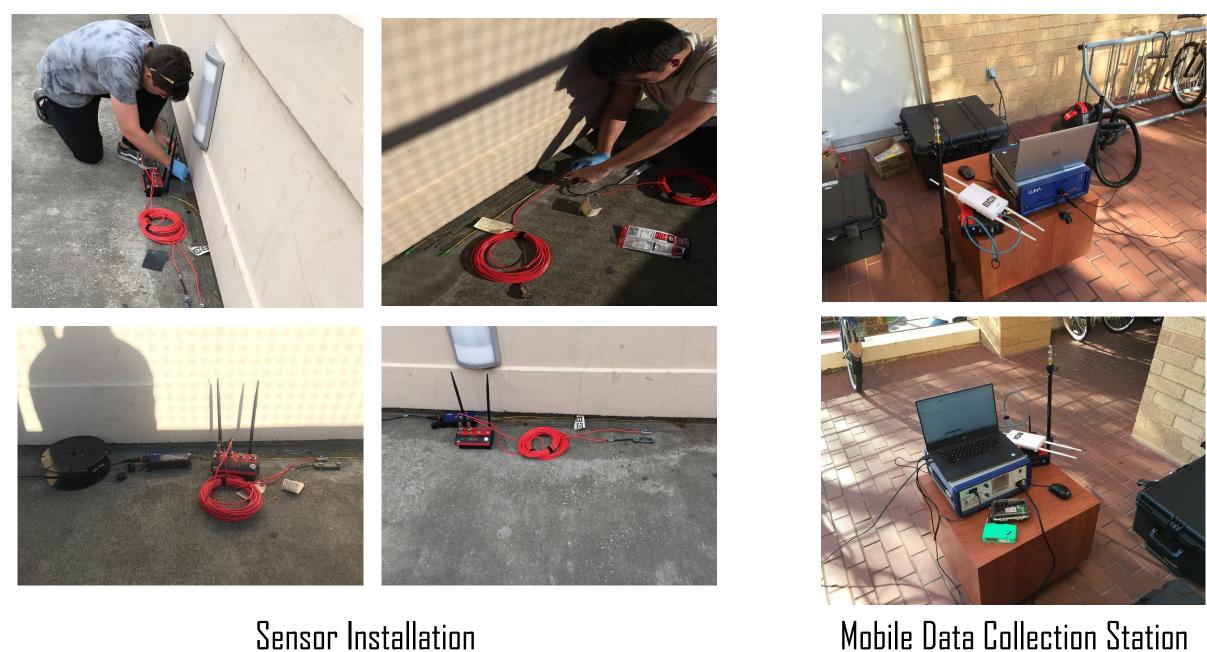
## Laboratory Data Collection

Quality Threshold 0.38 Vibration Correction 🔢 0.000



## Summary and Conclusions

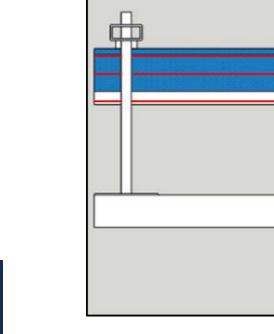
- The research related to OFDR-based dynamic monitoring is still in the early stages of development. Successful execution of this project will give ERAU a great advantage in our signature SHM field.
- □ The contribution of this project will significantly elevate the applicability and dynamic monitoring capability of Rayleigh-based OFDR. The new optimized OFDR-based DOFS will be the first to achieve dynamic monitoring under field condition.
- □ The research group is currently expanding this research effort into several new scopes: (1) Self-sensing Carbon Fiber Reinforced Polymer (CFRP) composite with distributed sensing capability, and (2) Design and Development of Prestressed Concrete Girder with Embedded Distributed Sensing System



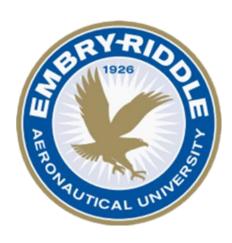


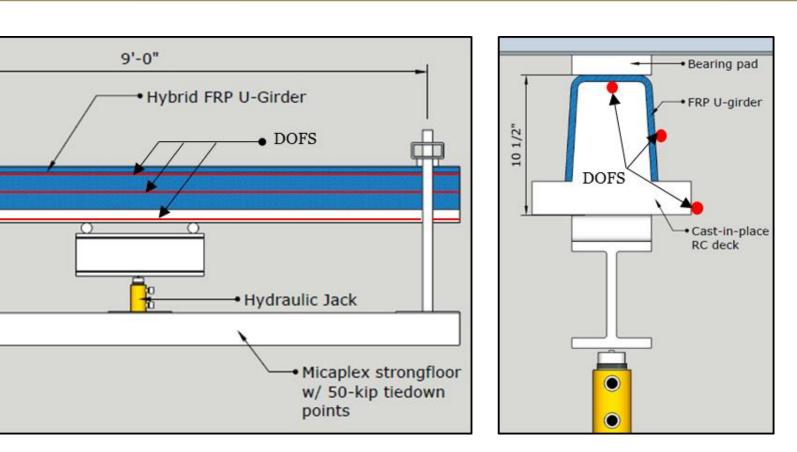


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the research team proposes to instrument a series of DOFS on two quarter-scale FRP U-girders with span lengths of 8 ft. Strain gauges will also be installed to collect strain data at midspan location at the same heights as the DOFS.





Measurement concept for distributed/continuous strain measurements