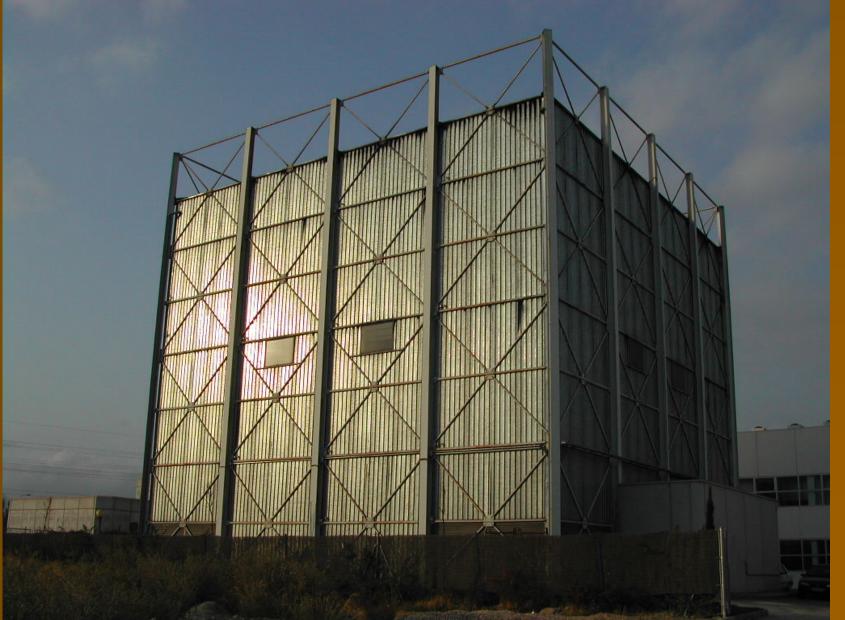




NUMERICAL AND EXPERIMENTAL STUDY OF ATRIUM ENCLOSURE FIRES IN A FULL SCALE FIRE TEST FACILITY

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Work Description

For the present work, a 3-D numerical model has been implemented to simulate the thermal and fluid fields induced by an enclosure fire in an atrium and for smoke exhaust system assessment. This study is focused on the 'Fire Atrium', a new full-scale fire test facility of the Technological Metal Centre in Murcia, Spain. It is an aluminium prismatic squared base building of 19.5 m x 19.5 m x 20 m with several vents arranged in its walls and four exhaust fans at the roof.

Many experimental tests have been carried out using several heptane normalized pool-fires placed at the centre of the atrium, being registered the inside air, wall and ceiling temperatures, the air through the vents inlet velocities and the exhaust fan pressure differences. The data obtained from these experiments have been used for the model validation.

Some numerical simulations have been performed. The results show good agreement with experimental data. For a fire test of 1.6 MW of average heat release power, the exhaust and ventilation system is not enough to extract the hot combustion products. There is an excessive and dangerous accumulation of hot gases at the upper part of the atrium and the exhaust capacity of the roof fan must be increased. Three different smoke exhaust systems have been compared showing that the CFD model can give the answer to that question. Also, for a 1.8 MW fire it has been predicted the smoke layer interface height showing good agreement with some other expressions from technical bibliography.

"Fire Atrium" in Murcia, Spain.

Numerical model

Mesh \rightarrow 3D quasi-structured non-uniform mesh (of the entire domain and a quarter of the domain) Frame material \rightarrow Walls and roof: Aluminium Ground: Concrete **Discretization schemes: SIMPLE** PRESTO QUICK \ UPWIND Radiation model \rightarrow P1 Model Turbulence model \rightarrow k– ϵ Standard

Ways for simulating the fire

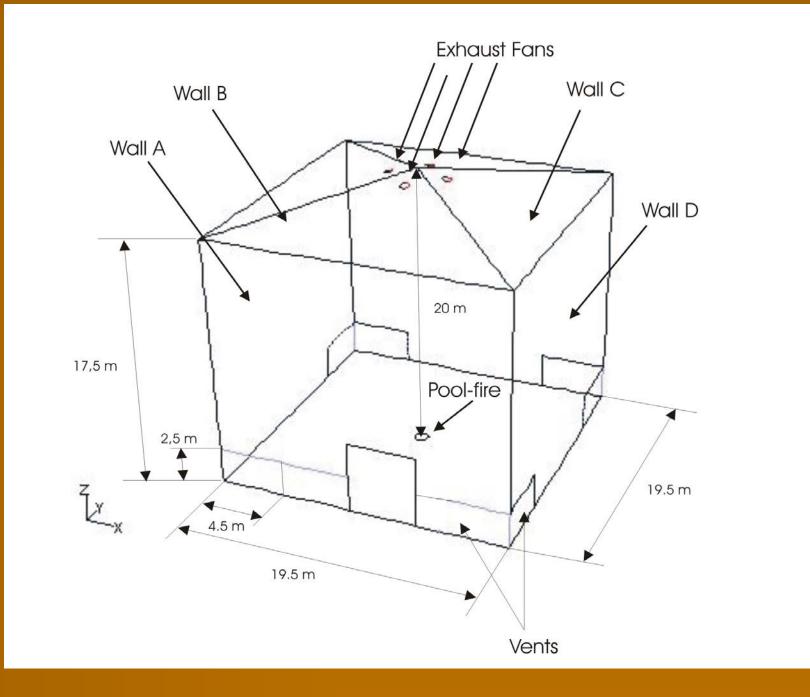
Finally, many different ways of simulating the pool-fire are being studied in order to get an accurate and relative low computational cost fire model.

kg/s

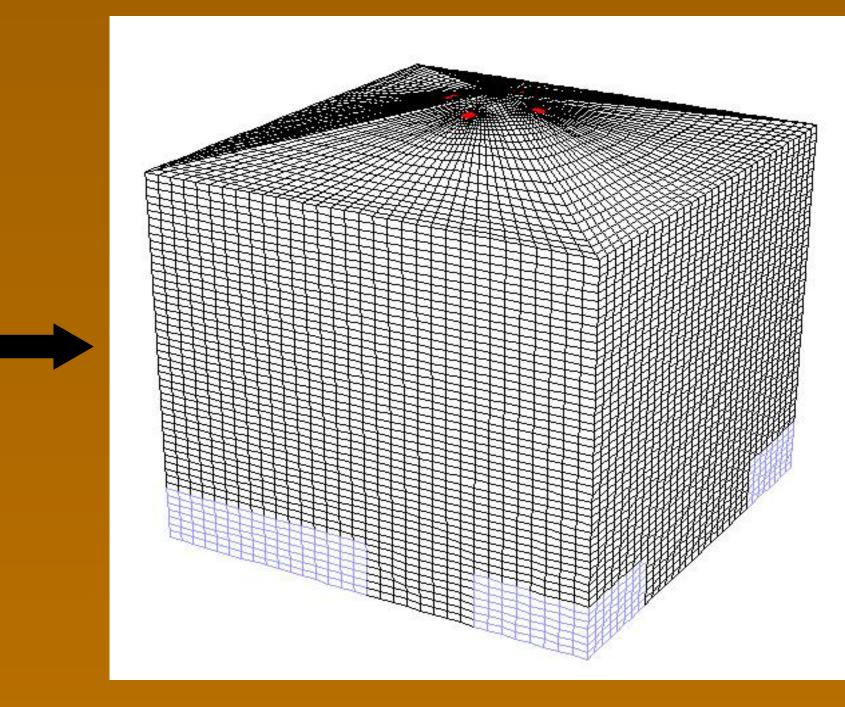
 $v_{inj} = f(r,t)? \longrightarrow$

3.72e+02 3.639e+02 3.65e+02 3.65e+02 3.65e+02 3.55e+02 3.56e+02 3.56e+02 3.56e+02 3.56e+02 3.56e+02 3.50e+02 3.48e+02 3.48e+02 3.48e+02 3.48e+02 3.48e+02 3.48e+02 3.48e+02 3.38e+02 3.27e+02 3.27e+02 3.27e+02 3.27e+02 3.27e+02 3.27e+02 3.27e+02 3.17e+02 3.15e+02 3.15e+02 3.15e+02 3.15e+02 3.06e+02 3.06e+02 3.06e+02 3.06e+02

kg/s



Fire Atrium scheme



Computation domain

Without combustion:

Less computational cost

Complete combustion products injection (sources), oxygen suction (sink) and heat power source

 $O_2 + CO_2 + H_2O + Heat release rate$

kg/s

 $C_7H_{16}(kg/s) \rightarrow CO_2 + H_2O$

 $C_7H_{16}(kg/s))+O_2\rightarrow CO_2+CO+C+...$

Num

0.5

 $... + H_2O + H + H_2 + O_2 + O + OH$

Exp

1.5

Less accuracy near the fire

With combustion:

(heptane injection) More computational cost

Higher accuracy near the fire

State:

Unsteady State

Steady State

Complete non-premixed combustion model (species transport eddy dissipation model)

Incomplete non-premixed combustion model (mixture fraction / PDF model)

Average mass burning rate injection

Constant average mass burning rate injection

Variable mass burning rate injection as a function of *r* and *t*

Fire tests simulations (Pool-fire D=0.92 m)

1.6 MW

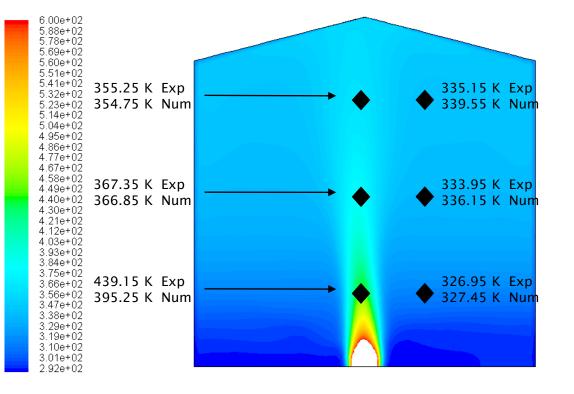
Model validation:

1.8 MW

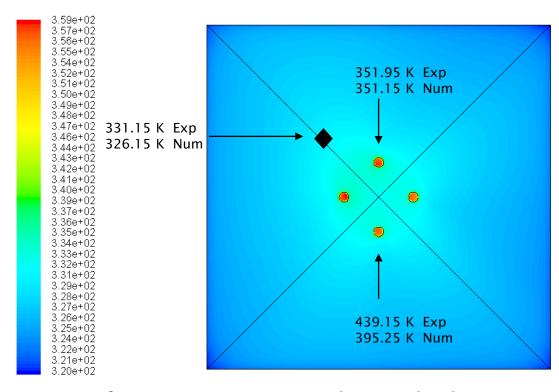
CFD application for fire safety

2.5





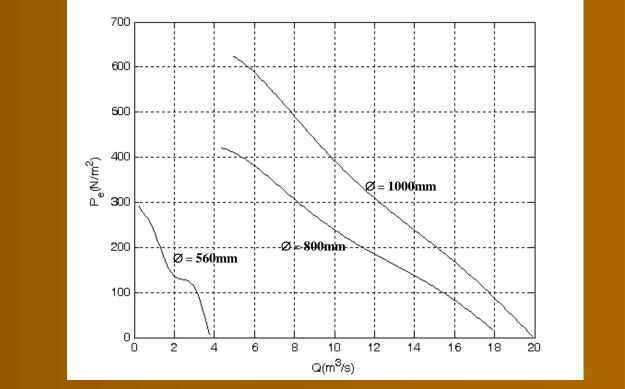
Flow temperature at a central section



Flow temperature through the exhaust fans and roof temperature

CFD application for fire safety

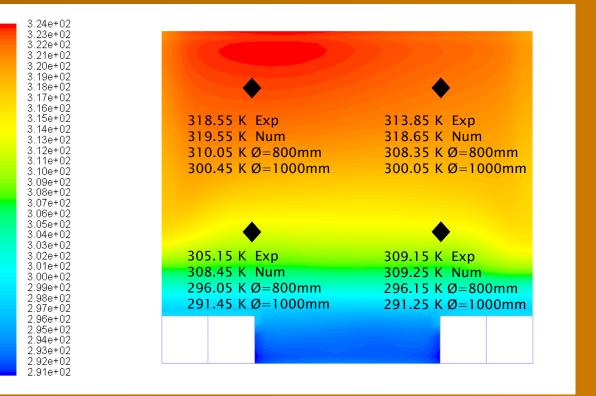
design: alternative smoke exhaust system study



Effects	over	smoke	exhaust	mass	flow

	Experimental	Numerical		
	Ø = 560mm	Ø = 560mm	Ø = 800mm	Ø = 1000mm
Exhaust fan 1	3.7	3.2	7.8	14
Exhaust fan 2	-	3.2	7.8	14
Exhaust fan 3	3.8	3.3	7.8	14
Exhaust fan 4	-	3.2	7.8	14

Effects over wall temperature



Model validation: 3.39e+02 3.38e+02 3.37e+02 3.36e+02 3.35e+02 3.35e+02 3.32e+02 3.32e+02 3.32e+02 3.29e+02 3.28e+02 3.27e+02 3.26e+02 3.25e+02 3.22e+02 3.22e+02 3.22e+02 3.22e+02 3.22e+02 3.12e+02 3.18e+02 3.15e+02 3.15e+02 3.15e+02 3.12e+02 3.02e+02 335.35 K Exp 336.12 K Num

 $\rightarrow \blacklozenge$

320.15 K Exp 313.89 K Num

358.85 K Exp

368.79 K Num

352.25 K Exp 354.79 K Num

325.55 K Exp

328.48 K Num

308.55 K Exp

302.43 K Num

Air next to wall temperature

Wall temperature

design: Smoke layer interface height prediction at two vertical lines

MW

