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WORKSHOP EM-ISAE 2018

TEST CASE 4: Dual band Transmit-array

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I. Introduction

In this report a numerical solution for the dual band transmit-array challenge proposed for the WORKSHOP EM-ISAE 2018 (test case n° 4) is presented. The numerical results are compared with the measurements of the corresponding prototype (see Figure 1). More details about the design and fabrication processes of the dual band TA can be found in [1]. To perform the corresponding full-wave simulations was quite challenging, mainly due to the large volume occupied by the antenna (comprising the feed and lens) and the fine subwavelength details of the unit cells that populate the TA. In fact, we did not had at that time sufficient memory to perform the full-wave simulation of the complete antenna (feed+lens). In this workshop we detailed the developed approach used to conduct the full-wave analysis of the TA within our available computational resources.

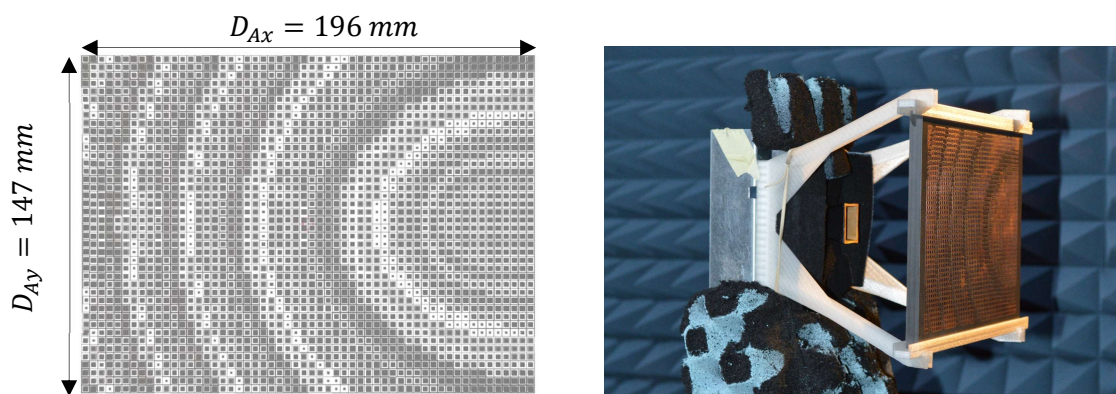


Figure 1 – Fabricated prototype of the dual band lens in Instituto de Telecomunicações, Lisbon, Portugal.

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II. Computational method

We use CST Microwave Studio ® Finite-difference time-domain (FDTD) for evaluating the Transmit-array (TA) performance. A high volume mesh density is required to capture the subwavelength details of the unit cells that compose the TA. This problem is computationally difficult even with high end PC workstations. To circumvent this problem a hybrid approach was developed that consist in separating the analysis of the feed from the analysis of the TA. This is a reasonable approximation as the coupling between the feed and the transmit-array is neglectable. The method involves the definition of an equivalent near-field source as a closed parallelepiped region near the transmit-array, as schematized in Figure 2. This near-field source is defined through equivalent electric and magnetic currents at the surface, according to the surface equivalence theorem. The goal is to achieve a near-field distribution that mimics the radiated field distribution of the original feed close to the lens bottom surface. The general procedure of finding the equivalent illumination is describe in Figure 3. Another advantage of this approach, besides the memory reduction, is that with a single simulation is possible to evaluate the transmit-array in both bands, whereas in the real problem two separate simulations would be required, one for each horn.

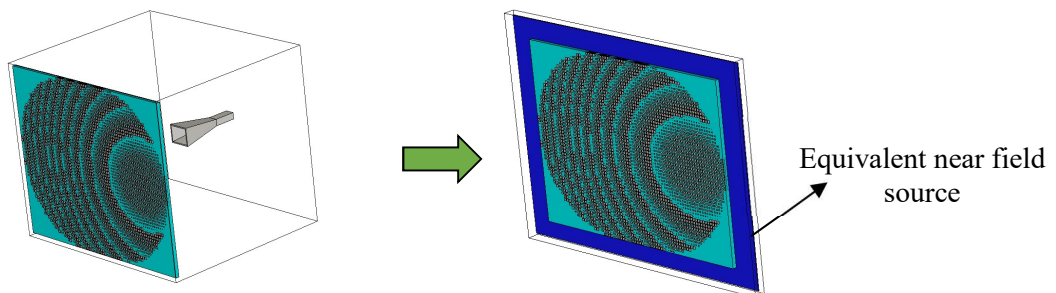


Figure 2 – Schematics of the hybrid approach used to simplify the analysis of TAs.

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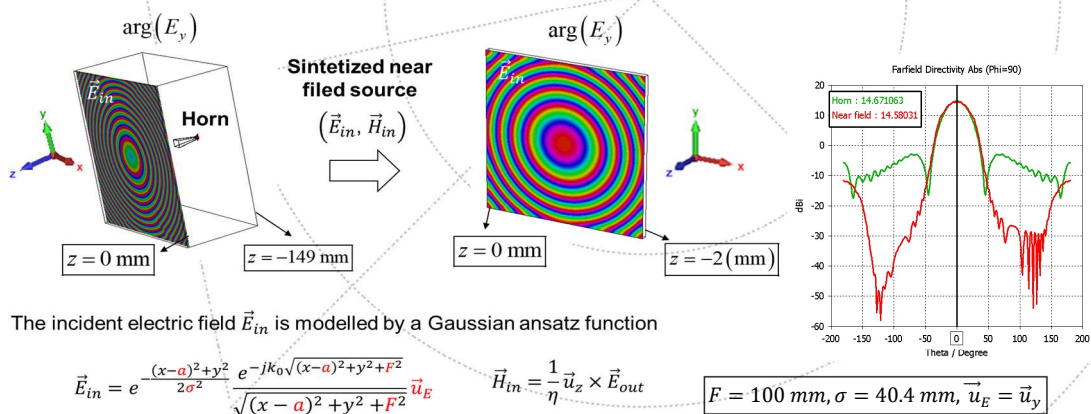


Figure 3 – Definition of the equivalent near field source

A previous single band TA design for Tx Ka-band (30 GHz) [2] is used to validate the accuracy of this method when compared with the complete antenna simulation. The presented results in Figure 4 validate the propose method for the analysis of the dual band TA.

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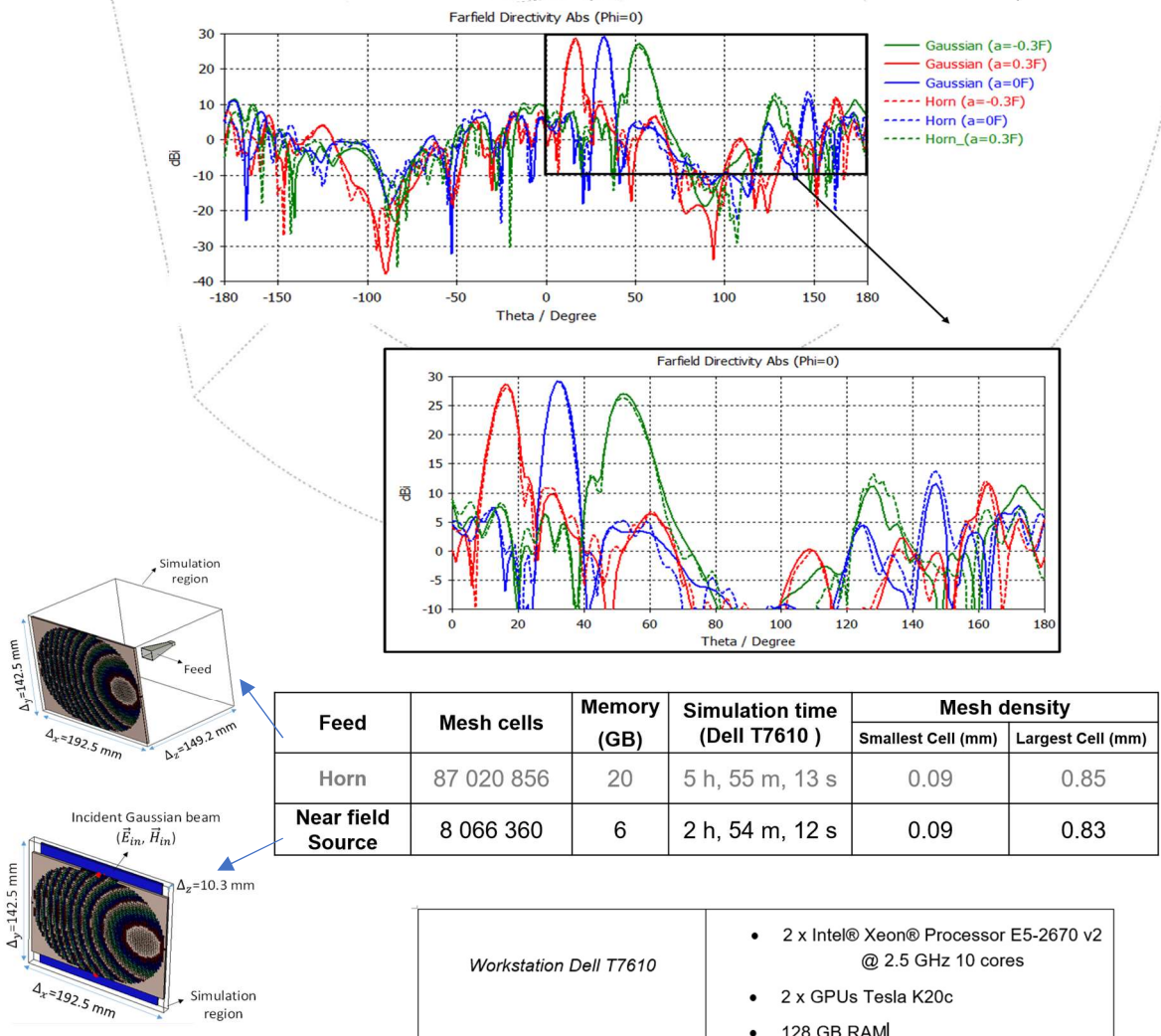


Figure 4 – Comparison between the equivalent near field source method and the full-wave simulation of the complete antenna. These simulations were performed using 2 GPUs K20c.

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III. Dual band Transmit-array – test case results

In Figure 5 and Figure 6 the comparison between the simulations and measurements is shown for each band, respectively. We should stress that manufacturing process of this TA is also quite challenging. The most demanding elements are the unit cells other rings that can be as small as 0.05 mm, which is in the limit of our manufacturing precision. These elements affect more the unit cell response at 20 GHz than 30 GHz, which may explain why we get a better agreement at 30 GHz.

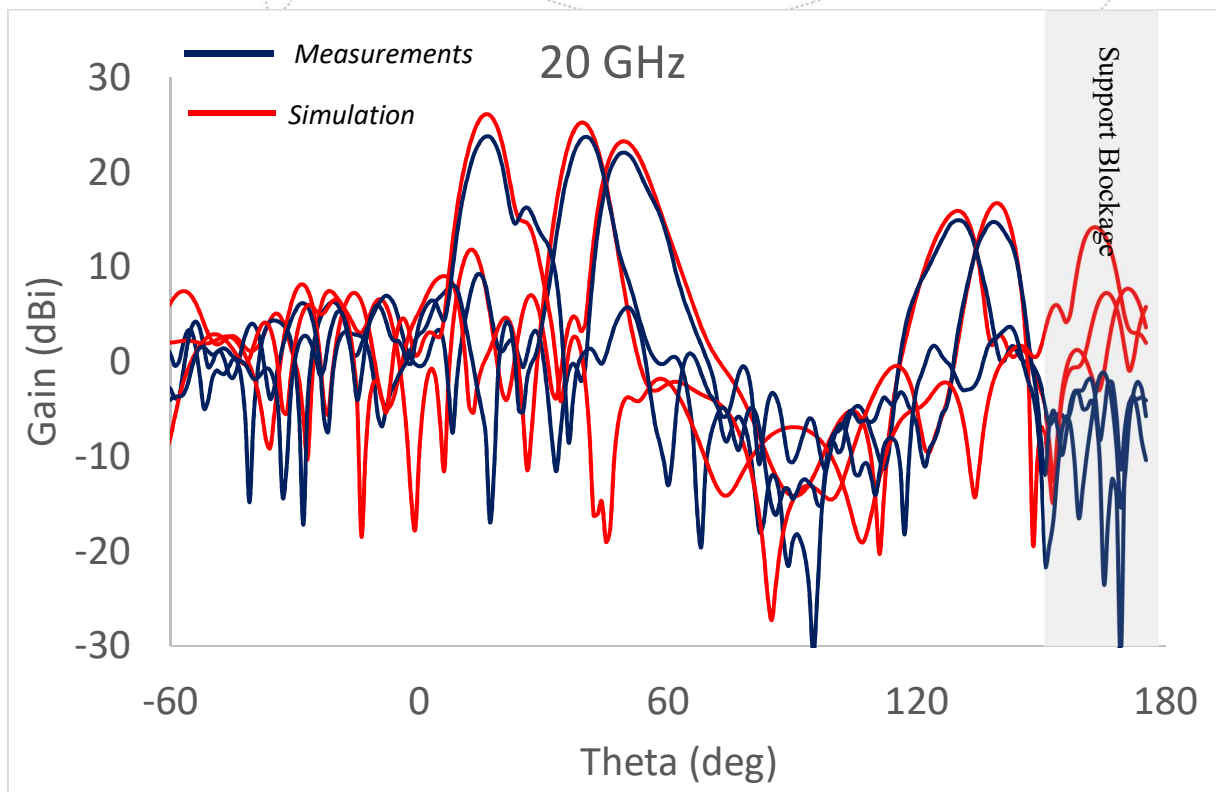


Figure 5 – Comparison between the simulations and measurements for 20 GHz.

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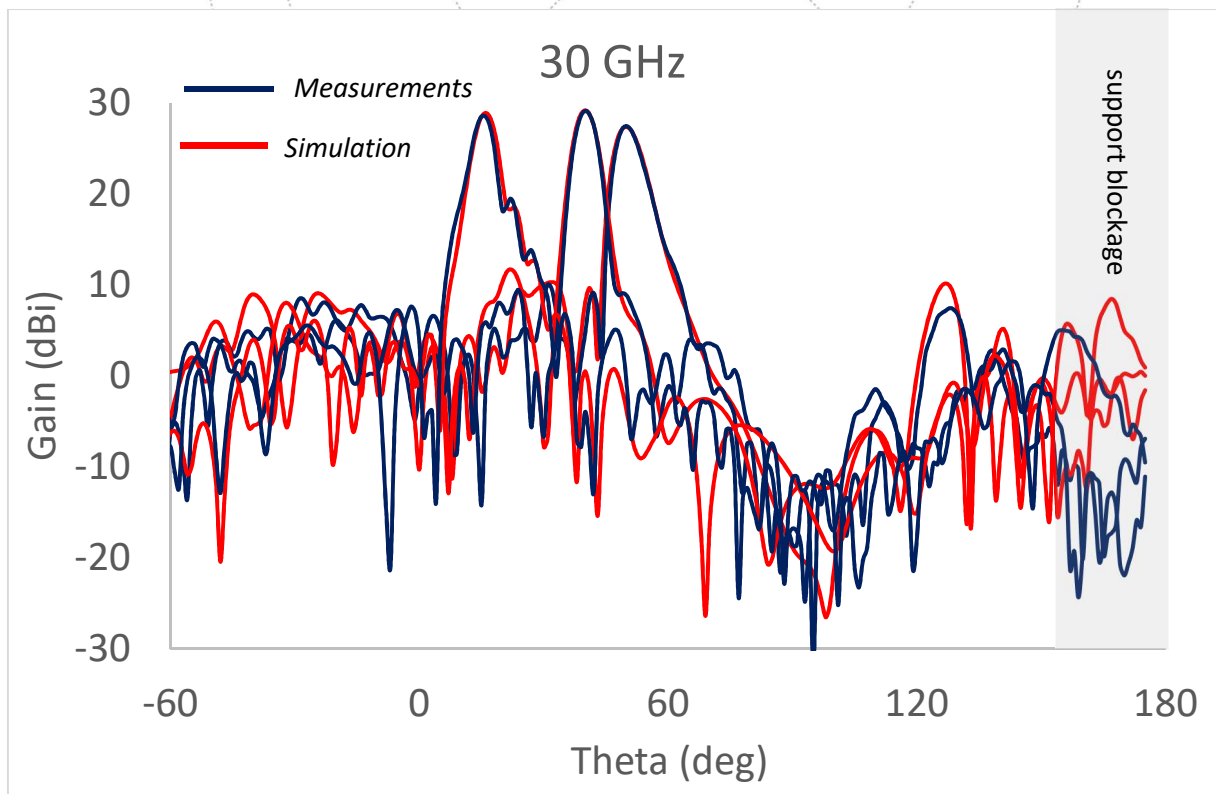


Figure 6 – Comparison between the simulations and measurements for 30 GHz.

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Table 1 – Simulation parameters

| | |
|----------------------------------|---|
| <i>Workstation Dell T7610</i> | 2 x Intel® Xeon® Processor E5-2670 v2 @ 2.5 GHz 10 cores 128 GB RAM |
| Number of time steps | 28 840 |
| Steady state accuracy limit (dB) | -18.6 |
| Smallest cell (mm) | 0.0975 |
| Largest cell (mm) | 1.29881 |
| Number of Mesh cells | 87 357 816 |
| Memory used (GBytes) | 24 |
| Elapsed time/ feed position | 50h52m54s |

IV. References

- [1] S. A. Matos, E. B. Lima, J. S. Silva, J. R. Costa, C. A. Fernandes, N. J. G. Fonseca, and J. R. Mosig, "High gain dual-band beam-steering transmit array for satcom terminals at Ka-Band," *IEEE Trans. Antennas Propagat.*, vol. 65, no. 7, pp. 3528-3539, Jul. 2017.
- [2] E. B. Lima, S. A. Matos, J. R. Costa, C. A. Fernandes and N. Fonsenca, "Circular Polarization Wide-angle Beam Steering at Ka-band by In-plane Translation of a Plate Lens Antenna," *IEEE Trans. Antennas and Propag.*, Vol. 63, No. 12, pp. 5443-5455, Dec. 2015.

V. Acknowledgments

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