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# A new continuous planar fit method for calculating fluxes in complex, forested terrain

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## Abstract

The planar fit method is often recommended for long-term eddy covariance flux measurements since it offers a number of advantages over rotating into streamwise coordinates. For sites over complex, forested terrain a single planar fit may not account for complex variations in slope and canopy cover with wind direction. An alternative to the planar fit method is presented where the tilt angle is fitted as a continuous function of the wind direction. This retains many of the benefits of the planar fit method, while at the same time better representing local variations in tilt with wind direction.

**Keywords:** Complex terrain; Sonic anemometer coordinate transformation; Eddy covariance; Planar fit

## 1 Introduction

When calculating fluxes using the eddy covariance method it is necessary to choose a suitable frame of reference for the measurements so that the vertical velocity component  $w$ , and hence the vertical fluxes, are not strongly affected by the large mean flow  $u$ . There are two types of methods commonly used to achieve this: rotating into a streamwise coordinate system using either double rotations (DR) or triple rotations (TR) (McMillen, 1988) and rotating into a planar fit coordinate system (Wilczak et al., 2001; Paw U et al., 2000). Lee et al. (2004) provides a nice practical summary and comparison of these methods, along with a discussion of some of the advantages and disadvantages of each approach. A more theoretical analysis of the different coordinate systems and their suitability for use over complex terrain is given by Finnigan (2004).

The planar fit (PF) method works well for relatively flat, uniform sites. By choosing a coordinate system averaged over the whole data set it avoids problems with unphysically large tilt angles in light wind conditions which can be seen with streamwise coordinate rotations (Wilczak et al., 2001). A further benefit of the planar fit method is that it provides an estimate of the instrument vertical velocity offset.

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In complex terrain with heterogeneous forest cover it is not clear that a single plane is the correct coordinate system to choose. Turnipseed et al. (2003) performed a detailed comparison of the streamwise coordinate method (both DR and TR) and the PF method at a forested site in mountainous terrain. Although they noted a large variability in rotation angle in low wind speeds, and also in  $\overline{v'w'}$ , they did not see significant differences in other fluxes between the three methods. The angle of tilt may be very different for different wind directions depending on the upwind canopy cover and terrain. One approach to handling this is to split the dataset into sectors based on wind direction and perform a different planar fit in each sector to account for upstream differences (e.g. Mammarella et al., 2007; Yuan et al., 2011). This sector planar fit (SPF) can help account for the variability in the coordinate plane with wind direction, but it involves a somewhat arbitrary splitting of the data into sectors and leads to discontinuities in the coordinate planes at the edge of the sectors which may impact on the calculated fluxes. Over a gently sloping site Mammarella et al. (2007) saw little difference in momentum, heat and CO<sub>2</sub> fluxes calculated using the DR and SPF methods. The SPF method is essentially what Lee (1998) used to correct the vertical velocities for the effects of tilt, zero offset in the electronics and flow distortion due to the instrument structure or tower. Paw U et al. (2000) discussed both the standard planar fit method, and also the potential for having the tilt angle as an arbitrary function of the wind direction to account for the effects of complex terrain or vegetation. So far as we know this more complex method has not been tested however.

Long term flux measurement sites tend to avoid complex terrain in order to minimise the impact of the terrain and of advection on the flux measurements. Correctly calculating fluxes of momentum, heat and other scalars over complex terrain with heterogeneous canopy cover is however important in order to understand the impact of this complexity on the canopy flow and canopy - atmosphere exchange. It is often desirable to correctly partition fluxes into flow parallel and flow normal components. In complex terrain or near canopy edges these may differ significantly from the horizontal / vertical. Finally accurate fluxes are necessary in order to compare field observations with the results from numerical models which are now being used to investigate these phenomena.

Here we develop the ideas of Paw U et al. (2000) to extend the planar fit method and include arbitrary changes in tilt angle with wind direction. Section 2 describes the method. Results from the different methods are presented in section 3 using data from an experiment on a forested ridge described in Grant (2011); Grant et al. (2015). Section 4 discusses the results, and section 5 draws some conclusions.

## 2 Methodology

### 2.1 The continuous planar fit method

The rationale for the continuous planar fit (CPF) method is to preserve the benefits of a planar fit to the data over a large dataset, while accounting for the variations in tilt with wind direction. It also avoids the arbitrary discontinuous behaviour of the SPF method. Assume that the tilt angle,  $\phi$  is a continuous function of the wind direction  $\theta$  (in an instrument coordinate system). Having determined the function  $\phi(\theta)$ , the  $\hat{\mathbf{i}}$  unit vector aligned with the mean wind in the sonic frame of reference is given by

$$\hat{\mathbf{i}} = (\cos \theta \cos \phi, \sin \theta \cos \phi, \sin \phi). \quad (1)$$

For a given wind direction  $\theta$  the  $\hat{i} - \hat{j}$  plane used in the planar fit is assumed to be tangential to the surface mapped out by  $\theta(\phi)$ , so the  $\hat{j}$  unit vector is parallel to  $d\hat{i}/d\theta$ , hence

$$\hat{j} = \frac{1}{(\cos^2 \phi + (d\phi/d\theta)^2)^{1/2}} \left( -\sin \theta \cos \phi - \cos \theta \sin \phi \frac{d\phi}{d\theta}, \right. \\ \left. \cos \theta \cos \phi - \sin \theta \sin \phi \frac{d\phi}{d\theta}, \cos \phi \frac{d\phi}{d\theta} \right). \quad (2)$$

Finally the unit vector normal to the plane,  $\hat{k}$ , is determined as

$$\hat{k} = \hat{i} \times \hat{j}. \quad (3)$$

The function  $\phi(\theta)$  needs to be determined from the data. Values of  $\theta$  and  $\phi$  are obtained as in the DR method. To produce a continuous function  $\phi(\theta)$  requires the fitting of some function curve to the smoothed data. Given the intrinsic periodicity of the function  $\phi$  with  $\phi(\theta) = \phi(\theta + 2\pi)$  then it is natural to choose a Fourier approximation so

$$\phi(\theta) = a_0 + \sum_{n=1}^N [a_n \cos(n\theta) + b_n \sin(n\theta)], \quad (4)$$

where  $N$  is the number of terms to include in the approximation and the  $a_n$  and  $b_n$  are constant coefficients to be determined. Setting  $N = 1$  essential reduces this method to the standard planar fit. The coefficients are determined by solving a nonlinear least squares problem. The derivative  $d\phi/d\theta$  is determined by differentiating the series approximation so

$$\frac{d\phi}{d\theta} = \sum_{n=1}^N [-na_n \sin(n\theta) + nb_n \cos(n\theta)]. \quad (5)$$

Having determined the basis vectors  $(\hat{i}, \hat{j}, \hat{k})$  as a function of  $\theta$ , the velocities and fluxes in the rotated coordinate system can be determined based on the vector velocities and fluxes in the sonic coordinate system (see e.g. Lee et al., 2004, for details).

## 2.2 Observational data

The method is applied to a dataset from an experiment to study canopy-boundary layer interactions over complex terrain which took place during March - May 2007 on the Isle of Arran, Scotland (Grant, 2011; Grant et al., 2015). The field site is located on a small ridge (approx 1 km in width, 160 m height, NW-SE aligned). At the measurement sites the ridge is primarily covered by a mature spruce plantation with an average tree height of 12 m. Tower 1 is located on the west side of the ridge on a small outcrop with dense trees approximately 10m to the east, but a more open aspect to the west. Tower 2 is situated in a small clearing on top of the ridge, with trees in most directions, although it is slightly more open to the south. Tower 3 is situated in a clearing on the steep eastern slope. There are small trees and shrubs close by, with the denser forest approximately 20 – 30 m away. These three sites are all characterised by a mixture of complex terrain and heterogeneous canopy cover and therefore provide a challenging test for any tilt correction scheme. Each tower was instrumented with 4 sonic anemometers at different levels. The height of the top sonic was 15.5 m for towers 1 and 2 and 23 m for tower 3. The instruments were mostly Metek USA-1 apart from two Gill HS-50 sonic anemometers on tower 2. All instruments were sampling at 10 Hz. A 15-minute averaging period was used for calculating mean winds and fluxes. A sidewind temperature correction is applied to the sonic temperatures (Liu et al., 2001), and this corrected

sonic temperature was used to calculate the heat fluxes. Flow distortion by the terrain and canopy may potentially depend on leaf cover (Dellwik et al., 2014). To minimise these effects, as in Grant et al. (2015), we restrict the data to the period 1 April - 15 May which is after leaf bud. Flow distortion may also depend on stability (Turnipseed et al., 2003) and so we filter the data to only include cases of near-neutral and transition-to-stable as in Dupont and Patton (2012), based upon the Obukhov lengthscale at the top of tower 1. Details of the method are given in Grant et al. (2015). The stationarity test of Foken and Wichura (1996) was used to check the quality of the flux data (see also Lee et al., 2004). Time periods where the difference between the covariances was greater than 30% for any of the fluxes were excluded from all analysis. For this study two further checks were included. Firstly, cases where the 15-minute mean wind speed was less than  $0.5 \text{ m s}^{-1}$  were excluded as low winds tended to be associated with very variable winds. Secondly the data was despiked to remove cases where the tilt angle was unrealistic. This was achieved by sorting the data by wind direction, then calculating a running median with a 21-point window. Points which deviated by more than 10 degrees from the median were marked as spikes and filtered out. The stationarity, wind speed and despiking tests resulted in up to 50% of the data being excluded at sites low down in the canopy at tower 3, but only about 15% at exposed sites above the canopy at tower 1. Limiting the stability regimes further reduced the data to 23-48% of the total data depending on the instrument location. Exclusion of this data reduced the scatter in the data, but did not have a significant impact on the overall results. The number of 15-minute averaged data points varies between towers and instruments depending on data availability and post-processing for quality control. In total there were about 1100-1400 data points for instruments on tower 1, 500-900 for tower 2 and 400-600 for tower 3 used in the analysis.

### 3 Results and discussion

Figure 1 shows the angle of tilt,  $\phi$ , from the DR method and the various planar fit methods as a function of the wind direction. Results are presented for the standard planar fit (PF) method, for the sector planar fit (SPF) method with 8 equal sectors and for the continuous planar fit (CPF) method. In fitting the function  $\theta$  for the continuous planar fit  $N = 4$  was chosen for the number of Fourier terms. In practice the first few terms dominated. Tests with  $N = 8$  did not show any improvement in the quality of the fit, and in some cases introduced spurious wiggles, particularly where there were directions with a sparsity of data. The optimal number of terms required will obviously depend on the complexities of each particular site.

Figures 2-4 show a comparison of the fluxes calculated using the three planar fit methods (PF, SPF, CPF) against the equivalent fluxes using the DR method. Also plotted on the figures is a 1:1 line, and for each method the best fit equation and  $R^2$  value. Figure 2 shows the streamwise momentum fluxes,  $\overline{u'w'}$ . For the planar fit methods the direction of the streamwise velocities,  $u$ , are calculated as the 15-minute mean velocity projected onto the relevant planar surface. The effect of the different methods on calculating a scalar flux is demonstrated in figure 3 using the temperature flux  $\overline{w'T'}$  as an example. Figure 4 shows results for the cross-wind momentum flux  $\overline{v'w'}$ , as previous studies have shown this to be a quantity which is particularly sensitive to the coordinate transformation used.

Figure 1 clearly demonstrates the issues with flux measurements over complex forested terrain. Tower 1 is more exposed than the other two towers, with higher av-

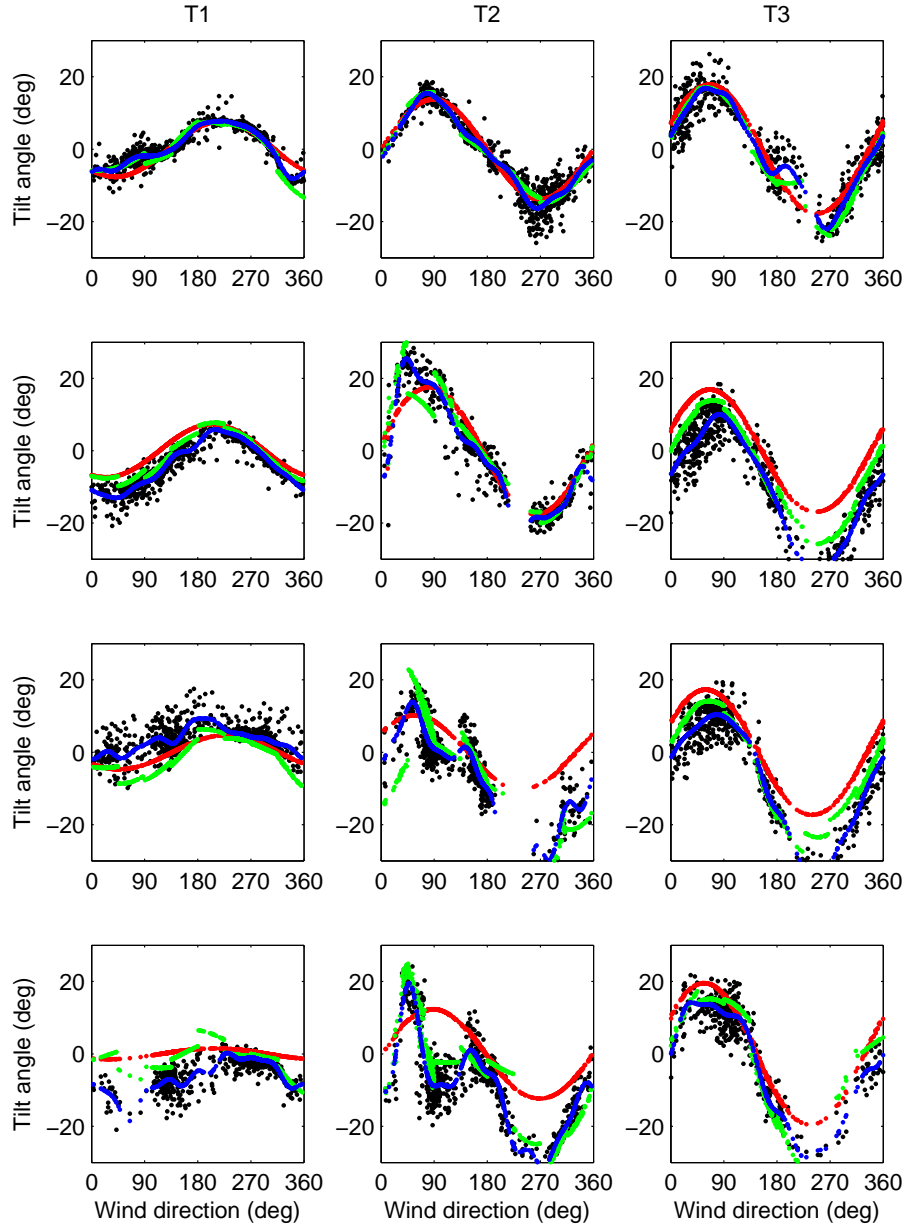


Figure 1: Tilt angle,  $\phi$  as a function of the wind direction. Results are plotted for towers 1, 2 and 3 (left, middle, right respectively). The highest sonic anemometers are in the top row, down to the lowest sonic anemometers in the bottom row. Black dots show the 15-minute averaged tilt calculated using the DR method. The red, green and blue dots represent the tilt angle for each 15-minute measurement using the PF, SPF and CPF methods.

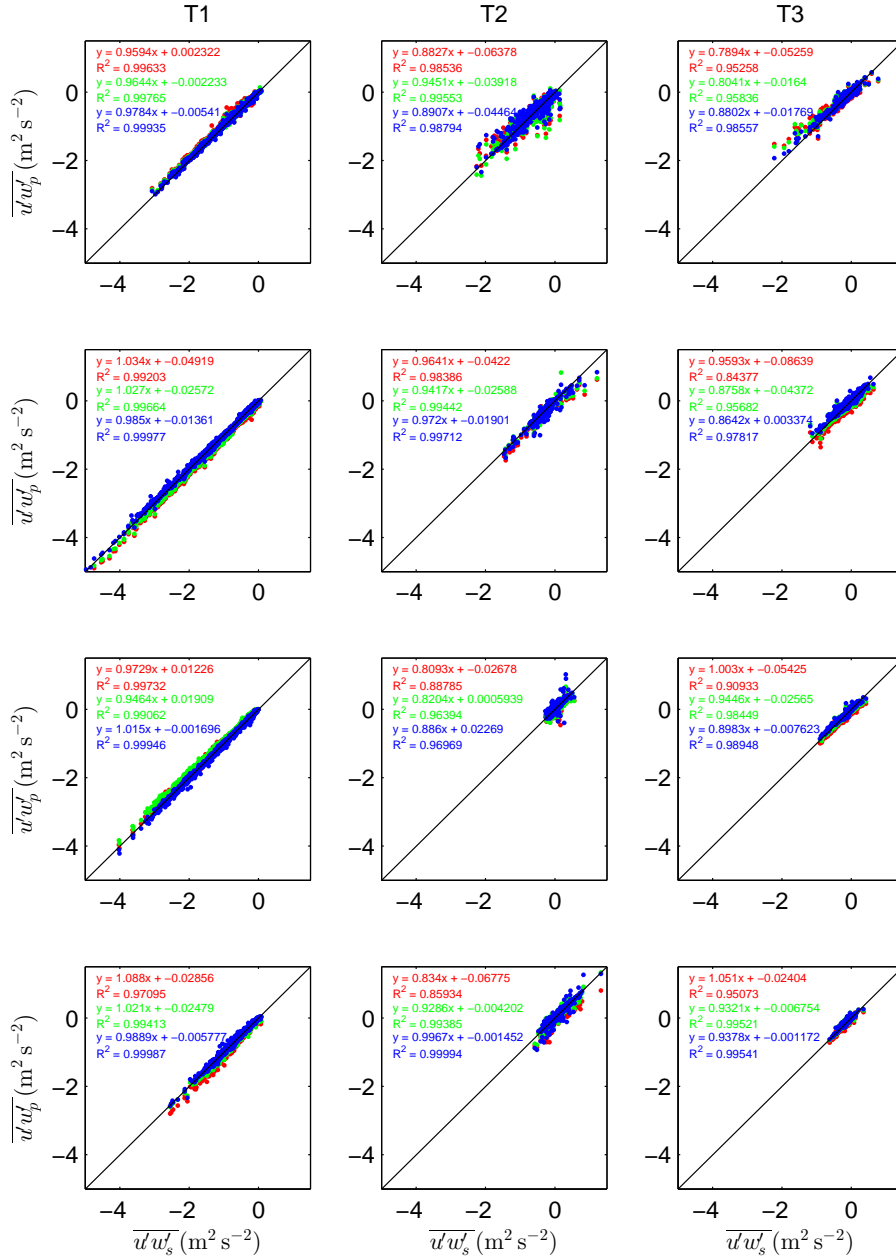


Figure 2: Momentum flux,  $\overline{u'w'_p}$  calculated using the various planar fit coordinate systems as a function of the flux in the streamwise coordinate system,  $\overline{u'w'_s}$ . The different fits are marked with different coloured dots: PF (red), SPF (green), CPF (blue). Results are plotted for towers 1, 2 and 3 (left, middle, right respectively). The black line shows the 1:1 line. Each figure shows the best fit equation and  $R^2$  value for each of the 3 methods. The highest sonic anemometers are in the top row, down to the lowest sonic anemometers in the bottom row.

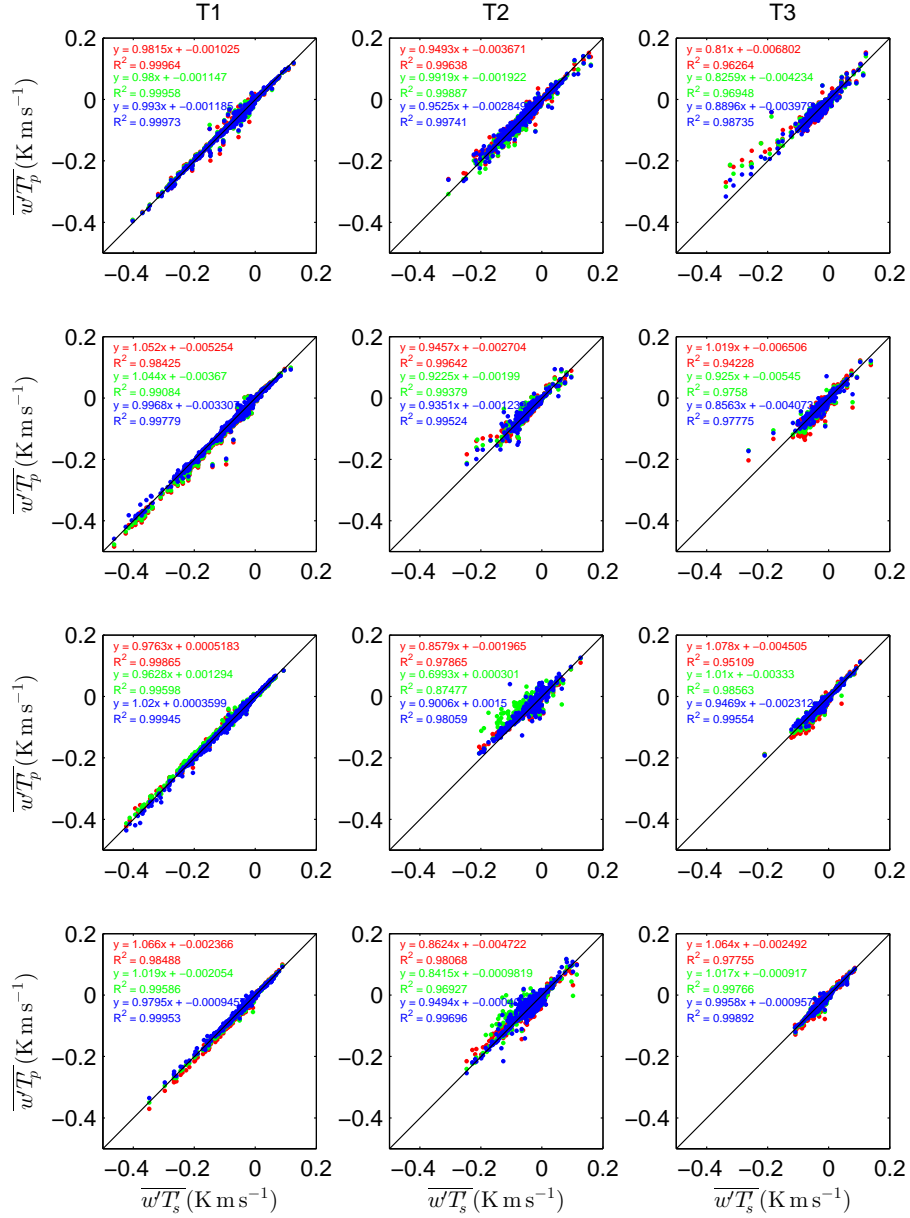


Figure 3: As for figure 2, but showing temperature flux,  $\overline{w'T^l}$ .



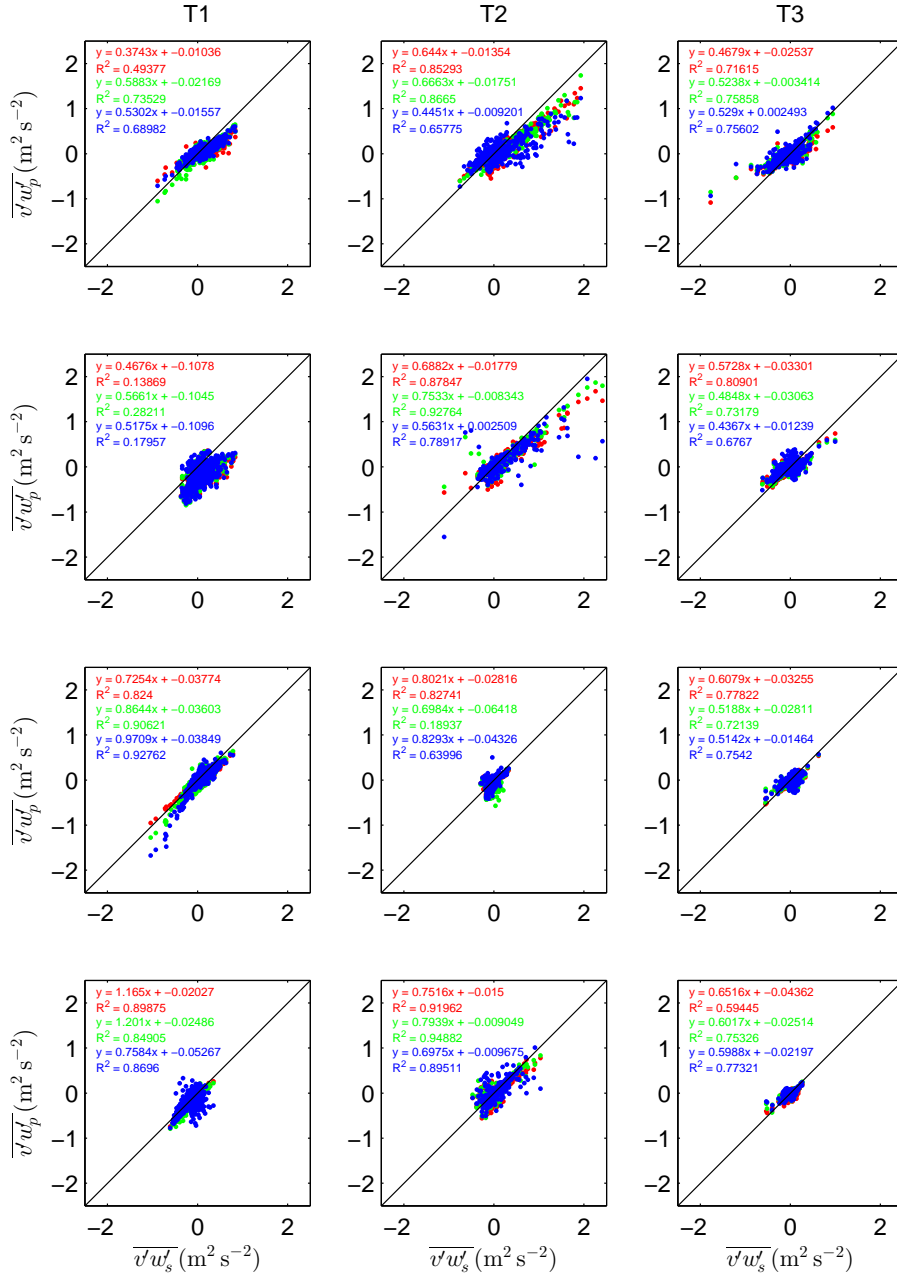


Figure 4: As for figure 2, but showing cross-wind momentum flux,  $\overline{v'w'}$ .

erage wind speeds and this explains the lower scatter in the tilt angle from the double rotation (DR) method, particularly at the top of the tower. Even at the top of the tower there is evidence that the sinusoidal variation of  $\phi$  with  $\theta$  assumed in the standard planar fit (PF) method is not necessarily accurate. Both the SPF and CPF methods show a kink in  $\phi$  at a wind direction of around  $90^\circ$  which corresponds to flow coming directly off the nearby dense canopy. The big difference between the two methods is that the CPF deals with this smoothly while the SPF approach shows very different planar fits for the two adjacent sectors which suggests that the fit (and hence the fluxes) will depend in a somewhat arbitrary way on the choice of sectors. Similar large discontinuities in the SPF are observed in a number of the other plots.

Lower on tower 1 the scatter in the data increases as the wind speeds decrease and the observations become more influenced by the canopy. There is also some evidence of a bias in the scatter with the outliers being generally mostly higher or mostly lower than the average for a particular instrument. This seems unlikely physically and is possibly due to interference of the tower on the air flow. The towers are round with a diameter of about 10 cm and the sonic anemometers are mounted on a long boom approximately 1 m from the tower. The sonic anemometers have a symmetrical design with a central column so there are no preferred wind directions. These factors, together with a lack of evidence of any variation in these outliers with wind direction, suggests that it is not direct distortion of the wind flow by the tower that is the cause of this. A similar effect is observed on the other towers.

Closer to the ground, below canopy top, the impact of wind direction on the tilt becomes more pronounced. In particular the lower instruments on tower 1 show the clear benefits of the CPF approach in better representing local variations in tilt angle with wind direction. Note that both the planar fit and sector planar fit methods apply an offset correction to the vertical velocity, which in turn alters the slope of the fitted plane. This explains the offset in Fig. 1 between these methods and the tilt angle calculated from the raw data, but not the failure to capture the shape of the curve.

Towers 2 and 3 exhibit similar results, although both show a larger scatter in the data due to their more sheltered positions and lower mean wind speeds (mean wind speeds of  $1 - 2 \text{ m s}^{-1}$  compared to  $5 \text{ m s}^{-1}$  at the top of tower 1). The third sonic anemometer down on tower 2 demonstrates one potential issue with the SPF method. There is very little data for wind directions of  $200^\circ$  to  $260^\circ$ . This means that the fitted plane is not very strongly constrained in this range. The CPF deals with this data sparsity more smoothly, particularly since we only include a small number of terms in the Fourier series here. While more intelligent choices of sectors for the SPF might also help, this introduces additional complexity and subjectivity to the method.

The scatter plots of the momentum flux in Figure 2 show that for tower 1, with relatively higher wind speeds, the three planar fit methods and the double rotation into streamwise coordinates all produce very similar values for  $\overline{u'w'}$ , although the agreement between the fluxes from planar fit methods and the streamwise coordinate method improves moving from the PF to the SPF then CPF methods. All three planar fit methods significantly reduce the unrealistic positive fluxes observed in the streamwise coordinates to close to zero in most cases, particularly at the top of tower 3. These results are similar to those presented by Lee et al. (2004) for a single instrument located well above the canopy top at a site with a relatively uniform canopy and rolling terrain. The remaining plots for towers 2 and 3 exhibit a much larger scatter in the fluxes between methods which is to be expected given the greater scatter in Figure 1. There is often flow separation and reversal at these two sites and negative wind shear with height, and so positive momentum fluxes may be reasonable (Grant, 2011; Grant et al., 2015).

In these cases the positive fluxes are similar between the planar fit and streamwise coordinate methods.

The scatter in temperature fluxes at all three towers (Figure 3) is smaller than in the momentum fluxes, particularly within the canopy. Agreement between all four methods is generally good, with the largest differences observed at the extremes. At tower 1 there is more scatter for unstable conditions ( $\overline{w'T'} > 0$ ) at all heights. In the canopy it tends to be stable conditions ( $\overline{w'T'} < 0$ ) which leads to greater scatter. This may be partly because stable conditions are often associated with low, variable winds and decoupled flow. In such conditions it is unsurprising that there is more variability in the 15-minute flow direction compared to the planar fit. As with the momentum flux, the scatter is reduced for the CPF method compared to the PF and SPF methods.

The greatest differences between the methods are seen with the cross-wind momentum fluxes (Figure 4). The low  $R^2$  values show that the 1:1 line is not a good fit to the data. There is a systematic bias at most instrument locations with all the planar fit methods showing lower fluxes than the corresponding value calculated using the streamwise coordinate rotation. The cross-wind momentum fluxes at towers 2 and 3 are larger than those at tower 1, which reflects the stronger direction wind shear with height observed in the flow separation regions at these towers (Grant et al., 2015).

The results of Lee et al. (2004) show a strong periodic directional dependence to the  $\overline{v'w'}$  values which they attribute to disruption of the flow by the tower. Directional dependence is also seen in these results (not shown), although in this case it appears to be a real effect due to differences in the surrounding terrain and canopy rather than an artifact of the tower setup. There are a couple of factors supporting this conclusion. As described above, the tower and the instrument mounts were designed to minimise flow disruption. More significantly, the instruments were mounted alternately on opposite sides of the tower. For each tower all four instruments show similar variations in  $\overline{v'w'}$  with direction, despite being mounted on different sides of the tower. If the effect was due to flow disruption by the tower it would be expected that instruments mounted on opposite sides would exhibit a different directional dependence. The evidence of physically realistic  $\overline{v'w'}$  terms suggests that applying a triple rotation to the data so  $\overline{v'w'} = 0$  would not be wise for sites with complex terrain and/or heterogeneous canopy cover.

In common with other planar fit methods, the optimal fit for the CPF method may depend on other environmental factors including the stability, wind speed and whether the trees are in leaf. Here we have tried to minimise these effects by filtering the data, although the method could in theory be used to investigate these effects further.

All planar fit methods need a sufficiently long dataset to accurately carry out the planar fit. Both the SPF and CPF methods have more degrees of freedom than the PF method and potentially require larger data sets to obtain an accurate fit. A sensitivity experiment was done by recalculating the planar fits using only half the dataset. There was very little difference in the PF results suggesting this amount of data was more than sufficient. The SPF method showed noticeable differences in the fitted planes. In particular one sector with little data in was not well constrained, and depending on which half of the dataset was used the fitting of the plane in that sector did not even converge. The CPF method also showed some variations in the fit, but less than for the SPF. Despite having the same degrees of freedom as the SPF method it did not exhibit the same problems with convergence. The reason seems to be that the method handles wind directions with sparse data more gracefully than the SPF method since all the data is used to fit each coefficient in the model. The use of different sized sectors in the SPF method to ensure that each sector has a similar amount of data in may partially

alleviate this problem, but at the expense of having some larger sectors.

## 4 Conclusions

This paper presents an alternative to the widely used planar fit method for calculating fluxes using the eddy covariance method. The new continuously variable planar fit (CPF) method extends the ideas of the sector planar fit (SPF) to account for the effects of forest canopy and terrain variations with wind direction which lead to deviations from a simple planar fit (PF). The new method has the advantage that it does not depend on an arbitrary division of the data into different sectors, with a corresponding discontinuity in how the fluxes are handled at the edges of the sectors. The CPF method produces fluxes closer to those obtained with the DR method in most cases (reflecting the fact it better represents the variation in the mean streamwise deflection with wind direction), while at the same time preventing the unrealistic rotation angles and positive streamwise momentum fluxes seen with the DR method. This improved agreement with the DP method comes despite the fact that the CPF method has fewer degrees of freedom than the SPF method in this case.

One potential disadvantage of this method is that, unlike the PF method, it does not offer an estimate of the instrument offset in vertical velocity. The error estimate of the PF method assumes that the data is well represented by a planar fit and so any offset is a result of instrument error. This assumption almost certainly fails for cases with complex terrain and variable canopy cover where the CPF method is likely to be applied. This paper successfully tests the new method with data from a number of sites over complex terrain, both within and above the heterogeneous forest canopy. The comparisons are limited to momentum and heat fluxes. Further tests are required to see how the method performs for other scalar fluxes of interest, including latent heat and carbon dioxide fluxes, and the impact it has on long term cumulative fluxes.

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