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# Enabling Technologies for the Rapid Dechlorination of Polychloroarenes and PCBs

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### 37 Abstract

38 39 Dielectric heating and acoustic cavitation (ultrasound or highperformance disperser) may all dramatically enhance conversion 40 41 rates and yields in heterogeneous metal-assisted organic 42 reactions even when low reagent excesses are used. These so 43 called "enabling technologies" bring with them process 44 intensification, safer protocols, cost reduction and energy 45 savings. We herein describe a series of rapid polychlorinated 46 aromatic and PCBs dechlorinations (15 min) carried out in a 47 moderate excess of metallic sodium and using non-conventional 48 techniques. We compared the results with those obtained for 49 reactions carried out under conventional heating and with those 50 performed with less reactive metals such as magnesium and 51 zinc. In this comparison, high-intensity ultrasound stands out as 52 the technique of choice.

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54 KEYWORDS. Polychloroarenes, PCBs, Dechlorination, Ultrasound,
55 Microwaves, High-performance disperser.

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#### 59 **1. Introduction**

Reductive dechlorination has become one of the most attractive 60 61 topics in chemistry since the Stockholm Convention on Persistent 62 Organic Pollutants (POPs) imposed the elimination of 63 polychlorinated biphenyls (PCBs) use by 2025 and their disposal via environmentally sound waste management by 2028. Besides 64 65 incineration or high temperature pyrolysis, which are powerful but 66 elimination methods, there are several controversial noncombustion alternatives to be considered. These are reported in 67 68 Table 1. Of the several dechlorination methods available, the metal based process has been singled out as the most cost effective and 69 70 efficient because no toxic by-products (i.e. biphenyl, 71 phenylcyclohexadiene, and phenylcyclohexene) are formed. 72 Nevertheless, safety concerns have been voiced over the huge 73 metal excess that is usually required. Alkaline-earth metals (Ca, 74 Mg) and transition metals (Ni, Pd, Fe, Ti and Zn) (Mitoma et al., 75 2004; Upendra and Suresh, 2008; Azzena et al., 2010; Liu et al., 76 2009; Zhang et al., 2011; Zhang, 2003; Fuku et al., 2010; Feng 77 and Lim, 2005) have been investigated as alternatives to the 78 alkaline metals (mainly Na) that are normally used. The reaction times of PCB dechlorination are in the region of several hours or 79 80 even days. The use of alternative energy sources, such as 81 microwaves (MW) (Kappe, 2004), ultrasound (US) (Cravotto and 82 Cintas, 2006) or mechanochemistry (Nasir and Varma, 2012; Stolle

- 83 et al., 2011) has been proven to strongly accelerate the reductive
- 84 process and limit gaseous emissions (Tajik et al., 2012; Liu et al.,
- 85 2011; Zhang and Hua, 2000; Sáez, 2011).
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**Table 1.** Non-combustion technologies for PCBs degradation.

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METHOD	CHARACTERISTICS	Ref.
Reduction with alkali-metals	<ul> <li>Metal stability is a crucial factor (i.e. Ca vs Na)</li> <li>Mild conditions (r.t., N<sub>2</sub> atmosphere)</li> <li>Improved by catalysts (i.e. Pd/C, TiCl<sub>4</sub>, CoCl<sub>2</sub>, Ni(OAc)<sub>2</sub>)</li> </ul>	Chiu, <i>et al.</i> , 2012; Noma, <i>et al.</i> , 2003.
Base-catalyzed decomposition	<ul> <li>Cost-effective and safe dechlorination occurs with alkali hydroxides</li> </ul>	Takada, <i>et al.</i> , 1997; Sun, <i>et al.</i> , 2007; Ye, <i>et al.</i> , 2011.
Catalytic hydro- dechlorination	<ul> <li>Heterogeneous catalysts (i.e. Fe, Ni, or Pd) and H<sub>2</sub> pressure</li> <li>Aqueous or organic solvents</li> <li>Generation of biphenyls, HCl</li> </ul>	Schüth and Reinhard, 1998.
Photochemical - electrochemical processes	<ul> <li>Closed systems, mild and eco-friendly conditions</li> <li>Safe additives (i.e. 2- propanol)</li> </ul>	Hawarl, <i>et al.</i> , 1992; Noma, <i>et al.</i> , 2002; Ghosh, <i>et al.</i> , 2012.
Plasma arc	<ul> <li>High efficiency</li> <li>Environmentally friendly</li> <li>Generation of H<sub>2</sub>O<sub>2</sub>, H<sub>2</sub>, O<sub>2</sub>, O<sub>3</sub> (also radicals)</li> <li>Shock waves and UV light may occur simultaneously</li> <li>Mandatory energy control</li> </ul>	Du, <i>et al.</i> , 2005.
Microbial reductive transformation	<ul> <li>Temperature, pH, substrate composition monitoring for microorganisms growth</li> <li>Slow process</li> </ul>	Borja, <i>et al.</i> , 2005; Field and Sierra- Alvarez, 2008.

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90 The use of metal particles in a MW oven can result in arcing and 91 generate fire or explosion if a flammable solvent is present. It is, 92 however, possible to perform organic reactions using well-dispersed

93 fine metal particles in a high-boiling-point polar solvent. Whittaker 94 and Mingos described all the safety operations needed to minimize 95 the risk of arcing which include moderating the power rating, using low metal loads and ensuring efficient stirring (Whittaker and 96 97 Mingos, 2000). Kappe showed, for the first time, how the electric field strength could influence the outcome of a chemical reaction. In 98 99 low field density conditions, the metal undergoes a cleaning effect 100 and becomes more reactive, whereas under a more intense 101 electrostatic discharge the high temperature reached generates a 102 carbonaceous material that covers the metal, thus reducing its 103 effect (Gutmann et al., 2011). Besides the close control of electric 104 field strength, another method that can influence this type of 105 reaction is the use of an inert atmosphere ( $N_2$  or  $Ar_2$  pressure). This 106 provides a totally safe environment in which to carry out the 107 procedure as it avoids the risk of combustion and explosion in all 108 MW reactions that use metals in a pivotal role (Cintas et al., 2012). US has found several applications in metal-assisted reactions 109 110 (Cintas et al., 2011) and in heterogeneous conditions (Cravotto et 111 al., 2003; Palmisano et al. 2011).

High-intensity US induces strong acoustic cavitation and streaming which enable efficient mixing, metal surface activation and particle dispersion to occur (Cravotto and Cintas, 2006). In the present study we intend to show how US, MW and high-performance 116 disperser favor the rapid metal-assisted dechlorination of117 polychloroarenes and PCBs.

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#### 119 **2. Materials and methods**

#### 120 2.1. Materials

121 All the chemicals were used as received. 1,3,5-trichlorobenzene 122 (<99%) and hexachlorobenzene were purchased from Fluka 123 Chemika, 2,4-dichlorophenol (99%) and a sodium dispersion 30 124 wt% in toluene (<0.1mm particles size) were purchased from Acros 125 Organics. Sodium cubes (99.95%), magnesium chips (98%) and Zn 126 powder were purchased from Sigma-Aldrich. PCBs oil: (Askarel by 127 Monsanto) a mixture of Aroclor 1260 70% and trichlorobenzene 30%. The US probe system (21.1 kHz, max power 250 W,  $\emptyset$  = 2.92 128 129 cm) with a titanium horn is commercially available from 130 Danacamerini s.a.s. (Turin, Italy). MW-assisted reactions were 131 carried out under pressure in a SynthWAVE by Milestone (Bergamo, 132 Italy). An Ultra Turrax<sup>®</sup> T 25 Basic by IKA was used as the high-

133 performance disperser.

134 2.2. Gaschromatography Analysis

a) Polychloroarenes; gaschromatography-mass spectrometry (GCMS) analyses were performed in a Agilent 6890 gaschromatograph
(Agilent Technologies - USA) fitted with a Agilent Network 5973
mass detector using a 30 m long capillary column, an i.d. of 0.25
mm and a film thickness of 0.25 µm.

GC conditions were; injection split 1:20, injector temperature
250°C, detector temperature 280°C. Gas carrier: helium (1.2
mL/min), temperature program; from 70°C (2 min) to 300°C at
5°C/min.

144 b) PCBs; Gaschromatography-electron capture detector (GC-ECD) 145 analyses were performed in a Agilent 6890 gaschromatograph 146 (Agilent Technologies - USA) fitted with an ECD, using a 50 m long 147 5% phenylpolysiloxane capillary column, i.d of 0.20 mm and film 148 thickness 0.33 µm. Gas carrier; helium (1 mL/min), make-up gas 149 for ECD; argon-methane (5%). ECD temp. 340°C. Splitless injection 150 1 µL. Temperature program: from 120°C (1 min), then 50°C/min up to 200°C (1 min); 5C°/min up to a 270°C; 20C°/min up to 315°C. 151

152 *2.3. MW under pressure* 

Aryl halide (0.1 mmol, 1 eq), metallic reagent (15 eq of metal for each Cl atom) and toluene (10 mL) were placed in the reaction vessel. The mixture was irradiated with MW (average power 300 W) at 130°C for the optimized time of 15 min under N<sub>2</sub> pressure (5 bar). The solution was filtered on a Celite<sup>®</sup> pad, soaked in ethanol to remove any un-reacted sodium and analyzed by GC-MS.

159 *2.4. US and the high-performance disperser* 

Aryl halide (0.1 mmol, 1 eq), the metallic reagent (15 eq of metal for each Cl atom) and hexadecane (10 mL) were placed in a threenecked-round-bottomed flask. The mixture, pre-heated in an oil bath at 130°C until the sodium melted, was then sonicated with an immersion horn (21.1 kHz, 60W) for 15 min. In an alternative procedure, a high-performance disperser probe was inserted into the flask and switched on/off intermittently every minute for a total time of 30 min (15 min high speed mixing and 15 min pause) to avoid super-heating and damage to the Ultra Turrax<sup>®</sup>. The solution was filtered on a Celite<sup>®</sup> pad, soaked in ethanol to remove any unreacted sodium and analyzed by GC-MS.

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#### 172 **3. Results and discussion**

173 In this paper, enabling technologies have been applied to the 174 dechlorination process with the aim of designing a safe, fast and 175 efficient protocol in the presence of a low alkali-metal excess ( $\leq 15$ 176 eq.). Four different techniques have been applied; MW, US, high-177 performance disperser (Ultra Turrax<sup>®</sup>) and simple conductive 178 heating in an oil bath (OB) was used as a conventional method 179 reference. The three main parameters that affect the dechlorination 180 rate were; temperature, mixing efficiency and metal/chlorine atom 181 ratio (scheme 1).

182

183 **Scheme 1.** Reductive dechlorination with non-conventional 184 techniques.



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In this work, dechlorination reactions were carried out by
suspending the reducing metal (mainly Na, 15 eq. for each Cl atom)
in toluene or a hexadecane solution containing a polychloroarene.
The first set of experiments was conducted with trichlorobenzene,
2,4-dichlorophenol and hexachlorobenzene.

191 MW-assisted dechlorination reactions were performed in a closed 192 MW reactor (SynthWAVE - Milestone) under nitrogen pressure (5 193 bar) thus avoiding any possible risk of fire and explosion. The high 194 power density (1.5 kW per 1.5 l) and the efficient cooling system 195 enabled fast volumetric heating and rapid cooling with very sharp 196 temperature ramps.

197 Table 2 reports the results achieved for MW-assisted reactions 198 according to the varying conditions and sodium source (sodium 199 cubes or a dispersion 30 wt% in toluene). In the light of the results 200 obtained in a few preliminary experiments with 10 eq. (entry 5), we 201 decided to proceed with a metal excess of 15 eq. for each Cl atom. 202 Although the reactions proceed well in 30 minutes at 150°C (entries 203 1, 10 and 17), we also investigated milder conditions at the same 204 reaction time. Complete dechlorination was also achieved (entries 2, 205 11 and 18) when the reaction was carried out at 130°C, whilst no reaction occurred within the 30 min period at temperatures below 206 207 the metal melting point (entries 9, 16 and 23). However, the 208 sodium dispersion showed much higher reactivity than the sodium 209 cubes when the temperature was close to the metal melting point

because of its higher particle dispersion (entries 8, 15 and 22). A temperature of 130°C together with a sodium/chlorine atom ratio of 15 eq. and an average reaction time of 15 min was the best compromise in the case of MW-promoted reactions. Lower dechlorination yields were detected working under reflux in an OB (entry 3, 12 and 19).

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217 **Table 2.** Residual polychloroarenes after MW-promoted 218 dechlorination with Na (15 eq.) in toluene (5 bar  $N_2$  pressure). 219

Entry	Substrate <sup>#</sup>	Time (min)	Temperature (°C)	Na cubes (residual %)	Na dispersion (residual %)
1		30	150	0	0
2		30	130	0	0
3	ÇI	30	OB reflux	67	60
5		30	130	$14^{*}$	10*
6		15	130	0	0
7	CICI	7	130	55	54
8		30	100	80	0
9		30	80	100	100
10		30	150	0	0
11	он	30	130	0	0
12	CI	30	OB reflux	52	44
13		15	130	0	0
14		7	130	13	17
15	ĊI	30	100	33	0
16		30	80	100	100
17		30	150	0	0
18		30	130	0	0
19		30	OB reflux	100	96
20		15	130	0	0
21		7	130	85	56
22		30	100	100	78
23		30	80	100	100

# In the cases of incomplete conversion, GC-MS analysis did not detect partially
 dechlorinated compounds; results are the mean of at least 2-3 trials

222 \* Na 10 eq.

224 The optimization of the MW-assisted procedure caused a decrease 225 in reaction time to 15 (entries 6, 13 and 20) and 7 min (entries 7, 226 14 and 21), where the former is the preferred choice. This study 227 has provided us with the following order of reactivity; 2,4-228 dichlorophenol >> 1,3,5-trichlorobenzene > hexachlorobenzene. 229 The last in the list was the most refractory towards dechlorination. 230 The MW-assisted procedure was employed in experiments carried 231 out with US (average power of 80 W) and with high-performance 232 dispersers (Ultra Turrax<sup>®</sup> at 10,000 rpm). Both methods generate 233 cavitation phenomena and cause the reactive metal to be very finely 234 dispersed. Moreover they played a pivotal role in the set up of this 235 protocol ensuring the process was strongly accelerated. Since the 236 experiments were carried out at atmospheric pressure and at 237 130°C, toluene was replaced with hexadecane. A constant 238 hexadecane solution reaction temperature was guaranteed by a 239 thermostatted bath (130°C). At this temperature, the metallic 240 sodium (cubes) melted (97.7°C) and therefore easily dispersed into 241 the medium, however, particle size was a crucial point for the other 242 metals (zinc and magnesium). Melting proceeded even more quickly when a commercially available sodium dispersion was used (30 wt%) 243 244 in toluene, < 0.1mm particles size). Table 3 shows the results 245 achieved with the sodium dispersion, zinc and magnesium. The sodium dispersion gave excellent yields, confirming the results 246

obtained with the MW protocol. The yields were significantly lower in

the presence of magnesium and zinc as they act in the solid phase.

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**Table 3**. Residual polychloroarenes after treatment with US or a
high-performance disperser with various metals (15 eq.) in
hexadecane for 15 min at 130°C.

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Entro	Mathad#	Substrate	Residual %		
Entry	Method	Substrate	Na dispersion Mg		Zn
24		trichlorobenzene	0	91	92
25	US	2,4-dichlorophenol	0	83	76
26		hexachlorobenzene	0	100	100
27	*1.11+	trichlorobenzene	0	92	95
28	UITIA Turray®	2,4-dichlorophenol	4	90	88
29	Turrax	hexachlorobenzene	10	100	100

254 # Results are the mean of 2-3 trials

<sup>\*</sup> Alternatively on/off 1 min (15 min high speed mixing and 15 min pause).

256

257 The optimized procedures; MW carried out in a pressurized reactor, 258 high-intensity US with an immersion horn and the high-performance 259 disperser (Ultra Turrax<sup>®</sup> at 10,000 rpm) were also tested in the 260 dechlorination of PCBs. A mineral oil containing 271 ppm of PCBs was used to this aim and was treated with a sodium dispersion at 261 262 130°C for 15 min with all techniques. After a few preliminary 263 experiments we defined a sodium excess value of 40 mole eq. as 264 being optimal. Table 4 summarizes the results achieved; 7 ppm with 265 MW, <2 ppm with US, 28 ppm with Ultra Turrax<sup>®</sup>, whilst the reference reaction in an oil bath gave a 120 ppm residue. All the 266 267 reactions were monitored via GC-ECD.

268

Table 4. Residual PCBs in mineral oil (271 ppm) under OB, Ultra
 Turrax<sup>®</sup>, MW and US.

Entry	Method	Time (min)	PCBs residual (ppm) Na (15 mole eq)	PCBs residual (ppm) Na (40 mole eq)
30	oil bath	60	270	120
31	*Ultra Turrax®	15	79	28
32	MW	15	56	7
33	US	15	48	<2

\*alternatively on/off 1 min (15 min high speed mixing and 15 min pause).

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#### 274 **4. Conclusion**

275 In conclusion, we have herein reported a dechlorination protocol 276 performed under non-conventional techniques that enables a 277 moderate excess of metallic sodium to be used rather than the 278 much higher excesses that are currently commonplace. On the basis 279 of the three main parameters studied, temperature, metal/chlorine 280 ratio and physical activation, we can conclude that the crucial issues 281 in the effectiveness of the procedure are the use of melted metal, a 282 sodium reasonable excess and efficient physical metal 283 activation/dispersion. Rapid reactions in low metal excesses (15 284 mole eq and 40 eq. for PCBs) are possible thanks to the enabling 285 technologies we have outlined above and would be impossible under 286 conventional heating.

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