

Up-milling and down-milling wood with different grain orientations – theoretical background and general appearance of the chips

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Abstract Peripheral milling with up-milling and down-milling techniques is very well known from a geometrical point of view. However, in processing anisotropic materials such as wood these geometrical aspects imply relevant differences when machining. In fact milling anisotropic materials leads to different cutting geometries when up-milling or down-milling and when changing the depth of cut. This results in a relative orientation of the grain depending on the process adopted. In this paper the geometrical interactions between tool and wood grain have been analysed theoretically and supported by experimental evidence. To achieve this result, Douglas fir has been processed with different depths of cut and grain orientations, the resulting chips have been collected and analysed. The experiments show how a shift of the cutting phenomenon and the chip type can be observed to support the theoretical background.

Gleichlauf- und Gegenlauffräsen von Holz bei unterschiedlichem Faserverlauf – theoretischer Hintergrund und erzeugte Spänegeometrien

Zusammenfassung Die geometrischen Aspekte beim Umfangfräsen mittels Gleichlauf- und Gegenlauffräse sind sehr bekannt. Allerdings treten bei der Zerspanung von

anisotropen Materialien wie z. B. Holz erhebliche Unterschiede auf. Tatsächlich führt das Fräsen von anisotropen Materialien beim Gleichlauf- und Gegenlauffräsen sowie bei einer Änderung der Frästiefe zu unterschiedlichen Schneidgeometrien. Die Ursache ist die jeweilige Orientierung des Faserverlaufs in Abhängigkeit des angewandten Verfahrens. In dieser Studie wurden die geometrischen Interaktionen zwischen Werkzeug und Faserverlauf theoretisch analysiert und mittels experimenteller Ergebnisse bestätigt. Dazu wurde Douglasienholz bei unterschiedlichem Faserverlauf und mit unterschiedlichen Frästiefen bearbeitet und die erzeugten Späne wurden analysiert. Die bei den jeweiligen Fräsverfahren experimentell ermittelten Spanformen bestätigen die theoretischen Annahmen.

1 Introduction

When milling wood it is universally known that the material can be cut using up-milling or down-milling techniques according to the directions of the cutting velocity vector and the feeding velocity vector. When the two vectors (applied to the tool) have the same direction, the cutting is up-milling (herein after referred to as UM), when the vectors have an opposite direction, the cutting is down-milling (herein after referred to as DM). UM and DM techniques have a different influence on the cutting resulting in differences in the cutting geometry. The cutting geometry is a well known factor, as it is the same as the one found in metal cutting, which is well documented in cutting technology books. In general, the following is assumed for UM and DM: different shape of the chip, different cutting velocity (albeit often negligible), different wave depth of the surface marks, the beginning of the cut from the thickest (DM) or from the thinnest (UM) part of the chip, different

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vibro-acoustic behaviour and different relative angle in the cutting path between the grain and the rake face. This has many consequences on other factors such as: magnitude and direction of cutting force, tool wear, evolution of force along the cutting path. The grain orientation is a fundamental factor in order to understand the cutting of wood. Given that wood is an anisotropic material, it is well known that when stressed in different directions, it behaves differently. The result, when machining with different grain orientations, is a wide range of mechanisms of chip formation that require specific analysis in order to be understood. Essential work has already been carried out regarding cutting geometries and is well documented in text books (Zompì and Levi 2003, Juan 2000, Santochi and Giusti 2000), as well as on the fundamentals of wood cutting processes (Kivimaa 1950, Franz 1958, McKenzie 1961, McKenzie and Franz 1964, McKenzie and Cowling 1971a, 1971b, Woodson and Koch 1970, Mori 1969, 1970, 1971a, 1971b, Piao and Fukui 1984), the basic properties of wood when stressed with different grain orientations (Yoshihara and Ohta 2000), and the surface quality after cutting. Some work has already been completed in the field of surface quality and grain orientation (Stewart 1969, 1971, Negri and Goli 2000, Goli et al. 2002, 2003, 2004a, 2004b), and certain scholarly articles analyse some of the above mentioned factors together (Cyra and Tanaka 2000). This paper is aimed at presenting a geometrical explanation of the general processes during milling of wood and in particular to understand the relations between the blade and the grain. First, a geometrical introduction is presented which is then supported by experimental evidence from the chip type. Douglas fir was machined with different grain orientations using a three axis CNC router and the resulting chips were collected and analysed after cutting.

2 Material and method

After some preliminary tests with different grain orientations, depths of cut (*doc*), feeding speeds and tool revolution per minute; samples such as shown in Table 1 were prepared and a machine set-up such as in Table 2 was chosen. The parameters are noted with their abbreviations and are thus reported in the text.

During machining, the chip suction system was disabled in order to collect the chips after cutting. The sample was fixed on a dynamometric platform in order to measure the cutting forces, which will be discussed elsewhere. The sample was fixed directly on the dynamometric platform by a compression plate, and the platform was firmly mounted on a steel plate which was surface ground on both sides to ensure a perfectly flat contact surface. The assembly was then fixed to the machine table by a conventional vacuum

Table 1 Description of the specimens used in the tests and relative abbreviations

Tabelle 1 Beschreibung der Versuchsparameter und jeweilige Abkürzungen

Species:	Douglas fir (<i>Pseudotsuga Menziesii</i> Fr. Var. <i>Menziesii</i>)
Moisture content (mc):	13% ~
Average specific gravity (ρ_{12}):	0.43 g/cm ³
Depth of cut (doc):	0.5–1.5 mm
Cutting length (l):	80 mm
Cutting height (h):	30 mm

Table 2 Experimental set-up and relative abbreviations

Tabelle 2 Versuchsbedingungen und jeweilige Abkürzungen

Milling machine type:	3 axes CNC router
Milling machine model:	SCM Record 1
Rake angle (γ):	20°
Clearance angle (α):	15°
Inserts on the cutting head (z):	2
Inserts material:	tungsten carbide screwed inserts (WC)
Cutting technology:	up-milling (UM) and down milling (DM)
Feeding speed (F):	5 m/min
Cutting speed (Vc):	29 m/s
Tool revolutions: (S):	13 867 rev/min
Cutting head diameter (D):	40 mm

system (see Fig. 1). The specimens were routed by peripheral milling using a straight blade and the sample was prepared in order to achieve only a peripheral contact with the cutting tool. The machine was tested for repeatability of the positioning which was measured within ± 0.05 mm. The reference surface was obtained by cutting 10 times with a depth of cut of 0.05 mm. Although very near the repeata-

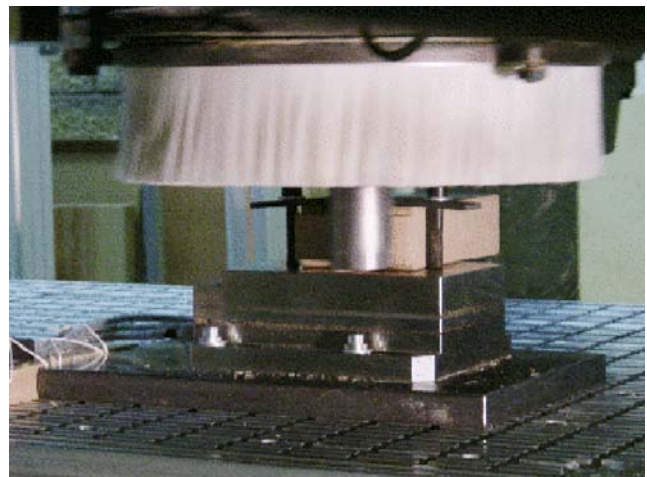
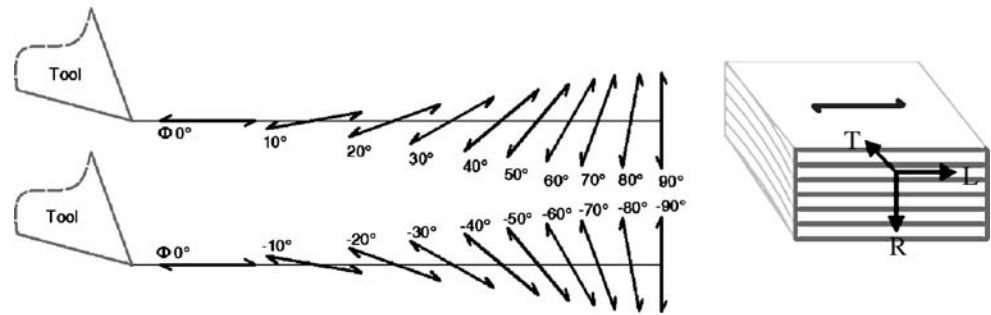


Fig. 1 The specimen hanging on the dynamometric platform during a cut

Abb. 1 Prüfkörper im eingebauten Zustand während des Fräsens

Fig. 2 Grain orientation and tangential specimens, the darker face is the face that has been machined
Abb. 2 Faserverlauf und tangentielle Proben. Die dunklere Fläche ist die bearbeitete Fläche



bility of the machine after 10 cuts of 0.05 mm, the absolute error can still be considered equal to 0.05 mm. This leads to very thin chips and a process very close to sanding instead of routing, and consequently a very clear reference surface. In fact, processing at 0.1 mm cut depth already results in surface defects, that when processing against the grain, propagate under the surface resulting in a bad reference surface. The final cut (0.5 mm or 1.5 mm) was made in the same working cycle in order to reduce positioning errors as much as possible and minimise the play of the machine.

The specimen was machined along and across the grain, and with and against the grain, varying the grain orientation in steps of 10° to 10°. To describe the grain orientation with respect to the blade, a system proposed by McKenzie ($\Omega-\Phi$) was used where Ω is the angle between the grain and the cutting edge and Φ the angle between the grain and the cutting velocity vector. The angle Ω was kept constant at 90° while Φ was varied. When $\Phi = 0^\circ$ processing is along the grain, tilting the grain leads to processing with ($0 < \Phi < 90$) or against ($0 > \Phi > -90$) the grain (see Fig. 2). Finally, because the cutting geometry at 90° is the same at -90°, these values of Φ lead to processing across the grain. Tangential specimens were processed on their radial face in order to minimise the effects of the interactions between early- and late-wood (see Fig. 2). Specimens were cut as close to each other as possible in order to minimise the wood variability, and from a straight grain oriented board.

3 Theoretical background

Solid wood is usually machined with the UM technique because of:

- the progressive increase of the chip thickness that leads to a lesser impact between tool and wood at the contact time,
- the limited wear of the tool when compared to down-milling,
- lesser safety concerns,

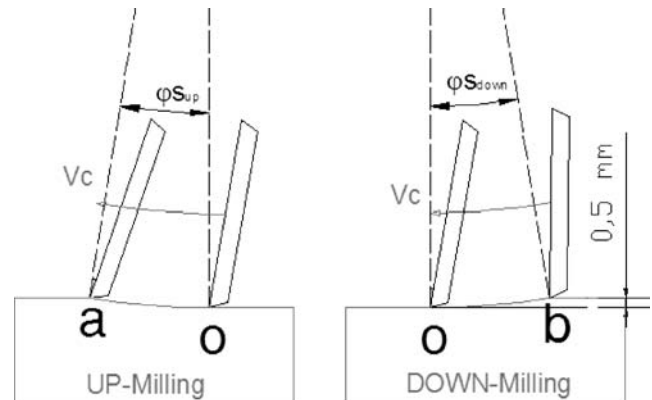


Fig. 3 Different impact point and coming out of the tool when up-milling or down-milling. Work angle $\phi_{s_{up}}$ for the up-milling technique and $\phi_{s_{down}}$ for the down-milling technique
Abb. 3 Verschiedene Auftreff- und Austrittstellen des Werkzeugs beim Gleichlauf- und Gegenlauffräsen. Fräswinkel $\phi_{s_{up}}$ beim Gleichlauffräsen und $\phi_{s_{down}}$ beim Gegenlauffräsen

- very similar final surface status to the one achieved with the DM technique (the situation could be very different for wood derivatives or for some specific processes).

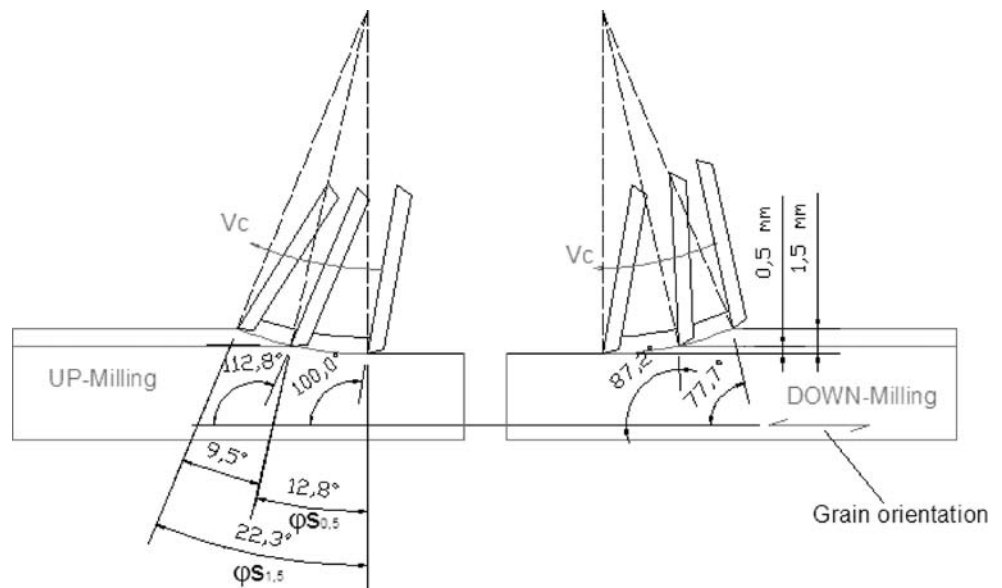
When UM, although the chip is longer, the resulting lesser tool wear is due to the last part of the chip usually being torn away instead of being cut, and because of the progressive rather than abrupt beginning of the cut.

These differences between the two techniques are mainly ascribed to the different cutting geometries. When UM, the cut begins at the thinnest part of the chip (point *o* in Fig. 3), while DM begins at the thickest part (point *b* in Fig. 3). Moreover, in UM and DM, the relative orientation of the blade, in relation to the grain, changes. In fact in UM the tool cutting path is along the arc *oa* while in DM it is along the arc *bo* (see Fig. 3). In UM the maximum chip thickness is obtained very close to point (*a*), whereas it is close to point (*b*) when DM. Given that the rotation of the tool during cutting is the *work angle* (ϕ_s) it can be said that (see Fig. 4):

- during a cut, either in UM or DM, between the minimal chip thickness and the maximum chip thickness the tool has a rotation of ϕ_s ,

Fig. 4 Relative angles between the rake face and the grain at the maximum chip thickness level when up-milling or down-milling with 0.5 mm and 1.5 mm of depth of cut and a tool diameter of 40 mm

Abb. 4 Winkel zwischen Fräs Werkzeug und Faserverlauf bei maximaler Spandicke beim Gleichlauf- und Gegenlauf fräsen mit einer Frästiefe von 0,5 mm und 1,5 mm und einem Werkzeugdurchmesser von 40 mm



- this rotation, referred as to the grain orientation, corresponds to $+\phi_s$ (*oa* arc) when UM and $-\phi_s$ (*ob* arc) when DM,
- between the maximum chip thicknesses UM and the maximum chip thickness DM, the tool undergoes a rotation of $2\phi_s$ (*ab* arc).

These are very important factors because the cutting forces and the cutting mechanisms are largely influenced by the chip thickness, and it is then expected that the magnitude and direction of the cutting forces will be mainly dependent on the processes acting at the maximum chip thickness levels. Given that the grain orientation (Φ) changes continuously with the cutting velocity vector direction, it is necessary to introduce two other factors in order to describe the processes: the *absolute grain orientation* (Φ_a), that is the grain orientation taking the new formed surface in machining as reference, and the *relative grain orientation* (Φ_r), that is the grain orientation value at the maximum chip thickness. Thus a specified *work angle*, that can be computed using Eq. 1,

$$\phi_s = \arccos((R - p)/R) \tag{1}$$

from any Φ_a the relative grain orientation can be easily determined for the UM and DM processes using Eqs. 2 and 3.

$$\Phi_{r_{up}} = \Phi_a - \phi_s \tag{2}$$

$$\Phi_{r_{down}} = \Phi_a + \phi_s \tag{3}$$

Moreover, since between UM and DM with the same absolute grain orientation results in a shift of $2\phi_s$, it means that to obtain the same relative grain orientation at the maximum chip thickness point (the same Φ_r) when UM or DM, differ-

ent Φ_a must be chosen. Table 3 shows for a given value of Φ_a the resulting value of Φ_r when UM or DM with 0.5 or 1.5 mm of *doc*. For example processing with 0° of Φ_a with 0.5 mm of *doc*, UM will give a Φ_r of $12,8^\circ$ while DM will give a Φ_r of $-12,8^\circ$. At the same time it is clear that UM with Φ_r $12,8^\circ$ and DM with Φ_r $-12,8^\circ$ will result in the same Φ_a of 0° .

From a geometrical point of view the greater the depth of cut, the greater ϕ_s and the greater the effect of the rela-

Table 3 Absolute grain orientations (Φ_a) and the corresponding relative grain orientations (Φ_r) for different depths of cut when up-milling and down-milling

Tabelle 3 Absoluter Faserverlauf (Φ_a) und entsprechender relativer Faserverlauf (Φ_r) für unterschiedliche Frästiefen beim Gleichlauf- und Gegenlauf fräsen

Φ_a	$\Phi_{r_{0,5\text{ up}}}$	$\Phi_{r_{0,5\text{ down}}}$	$\Phi_{r_{1,5\text{ up}}}$	$\Phi_{r_{1,5\text{ down}}}$
-90	-77.2	77.2	-67.7	67.7
-80	-67.2	87.2	-57.7	77.7
-70	-57.2	-82.8	-47.7	87.7
-60	-47.2	-72.8	-37.7	-82.3
-50	-37.2	-62.8	-27.7	-72.3
-40	-27.2	-52.8	-17.7	-62.3
-30	-17.2	-42.8	-7.7	-52.3
-20	-7.2	-32.8	2.3	-42.3
-10	2.8	-22.8	12.3	-32.3
0	12.8	-12.8	22.3	-22.3
10	22.8	-2.8	32.3	-12.3
20	32.8	7.2	42.3	-2.3
30	42.8	17.2	52.3	7.7
40	52.8	27.2	62.3	17.7
50	62.8	37.2	72.3	27.7
60	72.8	47.2	82.3	37.7
70	82.8	57.2	-87.7	47.7
80	-87.2	67.2	-77.7	57.7
90	-77.2	77.2	-67.7	67.7

Table 4 Similar chips to be obtained when UM or DM processing with and against the grain with 0.5 mm depth of cut

Tabelle 4 Bedingungen zur Erzeugung ähnlicher Späne beim Gleichlauf- und Gegenlauffräsen in und gegen Faserrichtung mit einer Frästiefe von 0,5 mm

Against the grain										
$\Phi_{a_{0,5}} \text{ up}$	-90	-80	-70	-60	-50	-40	-30	-20	-10	00
$\Phi_{a_{0,5}} \text{ down}$	70	80	90	-80	-70	-60	-50	-40	-30	-20
With the grain										
$\Phi_{a_{0,5}} \text{ up}$	00	10	20	30	40	50	60	70	80	90
$\Phi_{a_{0,5}} \text{ down}$	-20	-10	00	10	20	30	40	50	60	70

Table 5 Similar chips to be obtained when UM or DM processing with and against the grain with 1.5 mm depth of cut

Tabelle 5 Bedingungen zur Erzeugung ähnlicher Späne beim Gleichlauf- und Gegenlauffräsen in und gegen Faserrichtung mit einer Frästiefe von 1,5 mm

Against the grain										
$\Phi_{a_{1,5}} \text{ up}$	-90	-80	-70	-60	-50	-40	-30	-20	-10	00
$\Phi_{a_{1,5}} \text{ down}$	50	60	70	80	90	-80	-70	-60	-50	-40
With the grain										
$\Phi_{a_{1,5}} \text{ up}$	00	10	20	30	40	50	60	70	80	90
$\Phi_{a_{1,5}} \text{ down}$	-40	-30	-20	-10	00	10	20	30	40	50

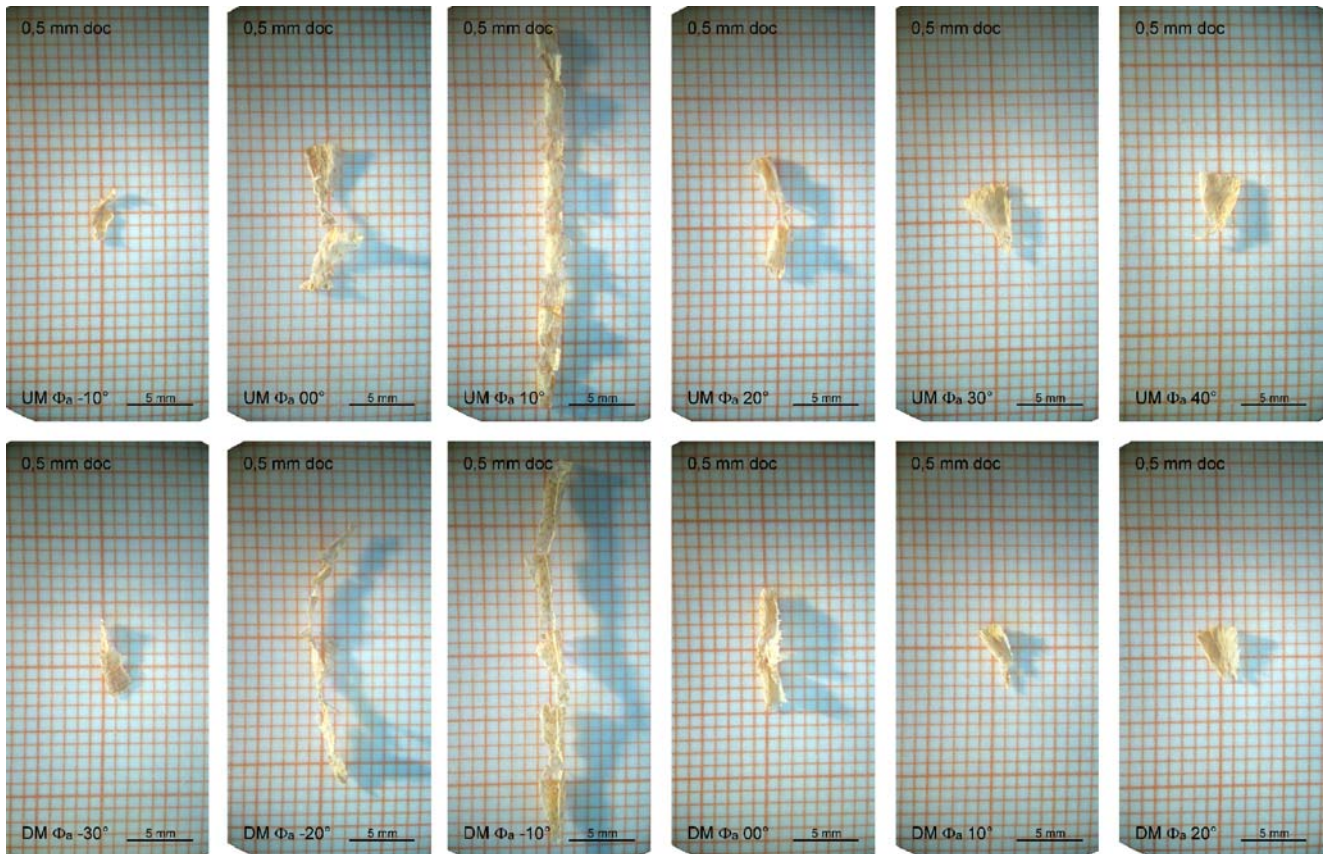


Fig. 5 Douglas fir chips obtained when up-milling and down-milling with different grain orientations with a 0.5 mm depth of cut
Abb. 5 Beim Gleichlauf- und Gegenlauffräsen und unterschiedlichem Faserverlauf mit einer Frästiefe von 0,5 mm erzeugte Douglasienspäne

tive grain orientation. In any case, relevant *work angles* do not necessarily result in a poor final surface status because the final surface quality mainly depends on mechanisms acting in a limited area near the surface (Koch 1972, Goli et al. 2004a, 2004b). Since the rotation of the tool inside this area does not usually lead to relevant shifts in the grain orientation, no relevant differences between the final quality within UM and DM processes were observed (Goli et al. 2002). The movement of the tool that, in UM, comes out from the surface tearing out the fibres, and in DM goes towards the surface, pressing fibres, appears to be a more significant influence on the final surface when UM and DM.

The result of these conditions is that rather than leading to relevant changes in the surface status, UM or DM lead to relevant changes in the cutting forces and chip types, and in particular the following is clear:

- the final quality will be strictly dependent on the *absolute grain orientation* (Φ_a) that determines the grain orientation near the forming surface,
- the chip types and the cutting forces will mainly depend on the *relative grain orientation* (Φ_r) because that will be the grain orientation at the maximum chip thickness level.

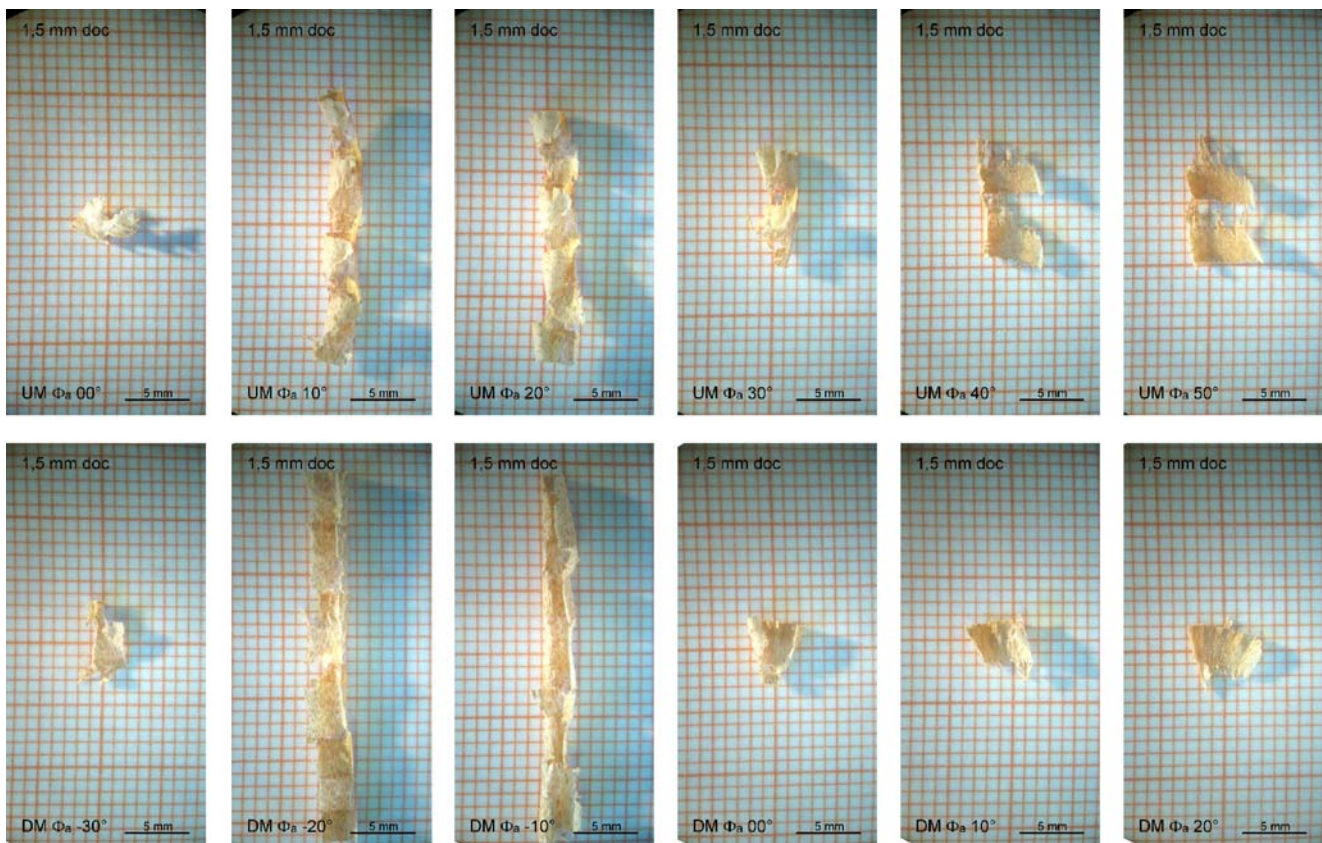


Fig. 6 Douglas fir chips obtained when up-milling and down milling with different grain orientations with a 1.5 mm depth of cut
Abb. 6 Beim Gleichlauf- und Gegenlauf Fräsen und unterschiedlichem Faserverlauf mit einer Frästiefe von 1,5 mm erzeugte Douglasienspäne

The practical effect of these considerations when UM and DM with the same Φ_a and the same doc will thus be:

- a shift of approximately $2\phi_s$ in the Φ_a of the same chip type in the collected chips when ordered according to the absolute grain orientation,
- a shift of approximately $2\phi_s$ in the Φ_a of the cutting forces when plotted vs. the absolute grain orientation.

4 Experimental results

Since in the experiments the samples are processed with increments of 10° of grain, the work angles computed in the theoretical part will need to be rounded off to the nearest 10° step. As ϕ_s processing with a 0.5 mm depth of cut is about 12.8° , it can reasonably be rounded off to 10° . And as ϕ_s is 22.3° when processing with a 1.5 mm depth of cut it can be reasonably rounded off to 20° . The practical effect of the theoretical background discussed previously should be that processing along the grain with $\Phi_a = 0^\circ$ results in similar chips when UM with $\Phi_a = 10^\circ$ or DM with $\Phi_a = -10^\circ$. This is because at their thickest parts, the chips have a very close relative grain orientation. The

values reported in Tables 4 and 5 should help to compare similar chips and to interpret Figs. 5 and 6. The case previously discussed for a doc of 1.5 mm should result in the same type of chips when UM with $\Phi_a = 20^\circ$ and DM with $\Phi_a = -20^\circ$.

In a photographic comparison of the chips obtained when processing with 0.5 mm doc (see Fig. 5) this behaviour can be clearly observed and a shift is visible in the chip type of about 20° as discussed before. The chip obtained when UM with a Φ_a of 00° is similar to those obtained when DM with $\Phi_a -20^\circ$, and the same for the other orientations investigated. Even when processing with 1.5 mm doc a shift can be clearly observed. In this case the shift is bigger than for 0.5 mm doc but not as big as expected. In fact for 0.5 mm doc the expected shift is 20° , the same value observed in the chip type, for 1.5 mm doc the expected shift is 40° while the real shift was found to be 30° (see Fig. 6). This is probably because when increasing the doc the chip in the last part is not cut but torn away. Because of this the cut happens at an angle $\phi_i < \phi_s$ that results in a lower value than the one computed theoretically. The theoretical background previously discussed is then completely supported by this experimental part concerning the chip examination.

5 Conclusion

Cutting wood with different grain orientation offers a wide range of phenomenon. The geometric basics have been discussed in this paper and some relevant connections have been found between grain orientation and depth of cut. Absolute and relative grain orientations have been defined and discussed. The experimental part presents evidence totally supporting the theoretical assumptions advanced. The differences in the relative grain orientation analysed in the theoretical part have been shown to have significant consequences on the chip type when up-milling and down-milling with different grain orientations and depths of cut. For chip types the resulting processes shifted according to the rotation of the tool during the process. In particular, the resultant chip type was found to be identical when processing with the same relative grain orientation.

References

- Cyra G, Tanaka C (2000) The effects of wood fiber directions on acoustic emission in routing. *Wood Sci Technol* 34:237–252
- Franz NC (1958) An analysis of the wood cutting process. PhD Thesis, University Michigan, Ann Arbor
- Goli G, Bleron L, Marchal R, Uzielli L, Negri M (2002) Formation and quality of wood surfaces processed at various grain angles – Douglas fir and oak. *Wood Struct Prop* 02:91–98
- Goli G, Marchal R, Uzielli L, Negri M (2003) Measuring cutting forces in routing wood at various grain angles. Study and comparison between up and down-milling techniques, processing Douglas fir and oak. Proceedings of the 16th International Wood Machining Seminar, Matsue, August 24–30, pp 127–137
- Goli G, Marchal R, Uzielli L (2004a) Classification of wood surface defects according to their mechanical formation during machining. Proceedings of the 2nd International Symposium on Wood Machining, Vienna, July 5–7, pp 315–324
- Goli G, Uzielli L (2004b) Mechanisms of wood surface formation and resulting final condition after planing. Proceedings of the 2nd International Symposium on Wood Machining, Vienna, July 5–7, pp 451–457
- Goli G, Fioravanti M, Sodini N, Jiangang Z, Uzielli L (2005) Wood Processing: a contribute to the interpretation of surface origin according to grain orientation. Proceedings of the 17th International Wood Machining Seminar, Rosenheim, September 26–28, pp 44–54
- Kivimaa E (1950) Cutting force in woodworking. State institute for Technical Research, VTT Publication No. 18
- Koch P (1972) Utilization of the southern pines Vol. II, U.S. Department of Agriculture-Forest Service
- Juan J (2000) Wood machining technology. CTBA (in French)
- McKenzie WM (1960) Fundamental aspects of the wood cutting process. *For Prod J* 10:447–456
- McKenzie WM (1961) Fundamental aspects of the wood cutting process. PhD Thesis, University Michigan, Ann Arbor
- McKenzie WM, Franz NC (1964) Inclined or oblique wood cutting. *For Prod J* 14:555–566
- McKenzie WM, Cowling RL (1971a) A factorial experiment in transverse plane cutting of wood – Part I. Cutting force and edge wear. *Wood Sci* 3(4):204–213
- McKenzie WM, Cowling RL (1971b) A factorial experiment in transverse plane (90/90) cutting of wood – Part II. Chip formation. *Wood Sci* 4(1):55–61
- Mori M (1969) An analysis of cutting work in peripheral milling of wood. I On the work done by a knife in up-milling parallel to wood grain. *Mokuzai Gakkaishi* 15:93–98
- Mori M (1970) An analysis of cutting work in peripheral milling of wood. II The cutting force, power and energy requirements in up-milling parallel to wood grain. *Mokuzai Gakkaishi* 16:1–9
- Mori M (1971a) An analysis of cutting work in peripheral milling of wood. III Variation of cutting force in inside cutting of wood with router-bit. *Mokuzai Gakkaishi* 17:437–442
- Mori M (1971b) An analysis of cutting work in peripheral milling of wood. IV The power requirements in inside cutting of wood with router-bit. *Mokuzai Gakkaishi* 17:443–448
- Negri M, Goli G (2000) Quality of machined surfaces of Norway spruce and Douglas fir assessed by visual grading. *Legno Carta* 6(1):10–21 (in Italian)
- Piao SY, Fukui H (1984) Specific cutting-force in the machining of wood I. Dependence on rake and clearance angles and effect of chip thickness. *Mokuzai Gakkaishi* 30:359–367
- Santochi M, Giusti F (2000) Manufacturing technology and engineering. Casa Editrice Ambrosiana, Milano (in Italian)
- Stewart HA (1971) Chip formation when orthogonally cutting wood against the grain. *Wood Sci Technol* 3(4):193–203
- Stewart HA (1969) Effect of cutting direction with respect to grain angle on the quality of machined surface, tool force components, and cutting friction coefficient. *For Prod J* 19(3):43–46
- Woodson GE, Koch P (1970) Tool forces and chip formation in orthogonal cutting of loblolly pine. Department of Agriculture-Forest Service research paper SO-52
- Yoshihara H, Ohta M (2000) Estimation of the shear strength of wood by uniaxial-tension tests of off-axis specimens. *J Wood Sci* 46:159–163
- Zompi A, Levi R (2003) Manufacturing technology. Chip removal processing. UTET Libreria, Torino (in Italian)