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Second Gradient Viscoelastic Fluids: Dissipation Principle and Free Energies

G. Amendola
Universita Dini

M. Fabrizio
Universita Bologna

Murrough Golden
Dublin Institute of Technology, murrough.golden@dit.ie

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Author	Family name	Amendola
	Particle	
	Given Name	G.
	Suffix	
	Division	
	Organization	Dipartimento di Matematica Applicata "U. Dini"
	Address	via F. Buonarroti 1c, 56127, Pisa, Italy
	E-mail	amendola@dma.unipi.it

Author	Family name	Fabrizio
	Particle	
	Given Name	M.
	Suffix	
	Division	
	Organization	Dipartimento di Matematica
	Address	Piazza di Porta S. Donato 5, 40127, Bologna, Italy
	E-mail	fabrizio@dm.unibo.it

Corresponding Author	Family name	Golden
	Particle	
	Given Name	J.
	Given Name	M.
	Suffix	
	Division	School of Mathematical Sciences
	Organization	Dublin Institute of Technology
	Address	Kevin Street, Dublin, 8, Ireland
	E-mail	murrough.golden@dit.ie

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Keywords

Non-simple fluid – Viscoelasticity – Free energy – Thermodynamic constraints – Mechanical power

Footnotes

Second gradient viscoelastic fluids: dissipation principle and free energies

G. Amendola · M. Fabrizio · J.M. Golden

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Abstract We consider a generalization of the constitutive equation for an incompressible second order fluid, by including thermal and viscoelastic effects in the expression for the stress tensor. The presence of the histories of the strain rate tensor and its gradient yields a non-simple material, for which the laws of thermodynamics assume a modified form. These laws are expressed in terms of the internal mechanical power which is evaluated, using the dynamical equation for the fluid. Generalized thermodynamic constraints on the constitutive equation are presented. The required properties of free energy functionals are discussed. In particular, it is shown that they differ from the standard Graffi conditions. Various free energy functionals, which are well-known in relation to simple materials, are generalized so that they apply to this fluid. In particular, expressions for the minimum free energy and a more recently introduced explicit functional of

the minimal state are proposed. Derivations of various formulae are abbreviated if closely analogous proofs already exist in the literature.

Keywords Non-simple fluid · Viscoelasticity · Free energy · Thermodynamic constraints · Mechanical power

1 Introduction

In this work we consider new constitutive equations for incompressible second order fluids, which include memory effects. These are materials for which the stress tensor is a function of the history of \mathbf{D} and $\nabla \cdot \nabla \mathbf{D}$, where $\mathbf{D} = \frac{\nabla \mathbf{v} + (\nabla \mathbf{v})^T}{2}$ is the strain rate tensor and \mathbf{v} the velocity. It is the presence of the quantity $\nabla \cdot \nabla \mathbf{D}$ ($= \Delta \mathbf{D}$, where Δ is the Laplacian) which renders the material non-local or non-simple. The classical laws of thermodynamics must be modified for such materials either by introducing suitable extra fluxes, or directly, by expressing these laws in terms of internal powers, characteristic of the material under consideration [13]. For the first method, there is the problem that the vector fluxes are introduced *a posteriori*, in order that compatibility with the laws of thermodynamics is maintained. The second formulation, in terms of internal powers, is more general than the first, since it is defined *a priori* by means of the constitutive equations, taking into account the power balance laws. In this article we use the second method.

G. Amendola
Dipartimento di Matematica Applicata "U. Dini",
via F. Buonarroti 1c, 56127 Pisa, Italy
e-mail: amendola@dma.unipi.it

M. Fabrizio
Dipartimento di Matematica, Piazza di Porta S. Donato 5,
40127 Bologna, Italy
e-mail: fabrizio@dm.unibo.it

J.M. Golden (✉)
School of Mathematical Sciences, Dublin Institute of
Technology, Kevin Street, Dublin 8, Ireland
e-mail: murrough.golden@dit.ie

The assumed constitutive equation includes thermal and viscoelastic effects in the expression for the stress tensor. We firstly discuss the laws of thermodynamics and use the equations of motion of the fluid to determine an expression for the internal mechanical power. Also, thermodynamic constraints on the constitutive equation are derived. Then, some free energy functionals are generalized to apply to this new material. This includes a functional of the minimal state introduced in [7, 10] and an explicit formula for the minimum free energy.

The layout of the paper is as follows. In Sect. 2, the constitutive equation with memory effects is presented and an expression for the internal mechanical power is derived. Moreover, the concepts of a free energy and of the corresponding internal dissipation rate are introduced. Thermodynamic constraints on the constitutive equation are also given. In Sect. 3, some free energies, already introduced for simple viscoelastic materials, are adapted to our non-simple fluid and their related internal dissipation rates are also deduced. The required properties of free energies in this new context are discussed.

Various steps in the derivations are omitted or abbreviated when they are closely analogous to developments in [3] (also [4]) for non-simple heat conductors.

2 Basic equations

For an incompressible second order fluid without memory, the stress tensor \mathbf{T} is given by [14]

$$\mathbf{T} = -p\mathbf{I} + 2\mu\mathbf{D} - \varkappa\nabla \cdot \nabla\mathbf{D} \quad (2.1)$$

where p is the scalar function known as the reaction pressure, μ and \varkappa are two positive constants, while \mathbf{I} is the identity second order tensor.

In this work we generalize (2.1), by assuming that the incompressible fluid, which is isotropic and homogeneous, exhibits both viscoelastic and thermal effects. The following constitutive equation is adopted:

$$\begin{aligned} \mathbf{T}(t) = & -p(t)\mathbf{I} + 2 \int_0^{+\infty} \mu(s)\mathbf{D}^t(s) ds \\ & - \int_0^{+\infty} \varkappa(s)[\nabla \cdot \nabla\mathbf{D}^t(s)] ds \\ & + \alpha[\vartheta(t) - \vartheta_0]\mathbf{I}, \end{aligned} \quad (2.2)$$

where ϑ denotes the absolute temperature and ϑ_0 is a fixed ambient absolute temperature, while μ and \varkappa are

smooth functions which belong to $L^1(\mathbf{R}^+) \cap H^1(\mathbf{R}^+)$. It is assumed that the motions are infinitesimal so that second order terms in \mathbf{v} or \mathbf{D} are neglected.

We consider this relation at a specific point $\mathbf{x} \in \Omega$, which is the domain occupied by the fluid. For brevity, however, the space dependence of the fields is henceforth generally omitted.

Let

$$\mathbf{E}(t) = \frac{\nabla\mathbf{u}(t) + [\nabla\mathbf{u}(t)]^\top}{2} \quad (2.3)$$

be the infinitesimal strain tensor at time t , where \mathbf{u} is the displacement vector. Then

$$\mathbf{D}(t) = \frac{d}{dt}\mathbf{E}(t) = \dot{\mathbf{E}}(t). \quad (2.4)$$

Also, let $\mathbf{E}^t(s) = \frac{\nabla\mathbf{u}^t(s) + [\nabla\mathbf{u}^t(s)]^\top}{2}$ be the infinitesimal strain history where

$$\frac{d}{dt}\mathbf{E}^t(s) = \dot{\mathbf{E}}^t(s) = \mathbf{D}^t(s), \quad (2.5)$$

$$\frac{d}{ds}\mathbf{E}^t(s) = -\frac{d}{dt}\mathbf{E}^t(s) = -\mathbf{D}^t(s).$$

We define the relative history as

$$\mathbf{E}_r^t(s) = \mathbf{E}^t(s) - \mathbf{E}(t). \quad (2.6)$$

The dependence of the stress tensor on \mathbf{D}^t and $\nabla \cdot \nabla\mathbf{D}^t$ in (2.2) can be expressed in terms of $\mathbf{E}_r^t(s)$ and $\nabla \cdot \nabla\mathbf{E}_r^t(s)$, since we have

$$\begin{aligned} \int_0^{+\infty} \mu(s)\mathbf{D}^t(s) ds &= - \int_0^{+\infty} \mu(s) \frac{d}{ds}\mathbf{E}^t(s) ds \\ &= - \int_0^{+\infty} \mu(s) \frac{d}{ds}\mathbf{E}_r^t(s) ds \\ &= \int_0^{+\infty} \mu'(s)\mathbf{E}_r^t(s) ds \end{aligned} \quad (2.7)$$

and, analogously,

$$\begin{aligned} \int_0^{+\infty} \varkappa(s)\nabla \cdot \nabla\mathbf{D}^t(s) ds \\ = \int_0^{+\infty} \varkappa'(s)\nabla \cdot \nabla\mathbf{E}_r^t(s) ds. \end{aligned} \quad (2.8)$$

Thus, we can write (2.2) as follows:

$$\begin{aligned} \mathbf{T}(t) = & \{-p(t) + \alpha[\vartheta(t) - \vartheta_0]\}\mathbf{I} \\ & + 2 \int_0^{+\infty} \mu'(s)\mathbf{E}_r^t(s) ds \\ & - \int_0^{+\infty} \varkappa'(s)\nabla \cdot \nabla\mathbf{E}_r^t(s) ds. \end{aligned} \quad (2.9)$$

201 The extra stress tensor has the form

$$202 \tilde{\mathbf{T}}(t) = 2 \int_0^{+\infty} \mu'(s) \mathbf{E}_r^t(s) ds$$

$$203 - \int_0^{+\infty} \varkappa'(s) \nabla \cdot \nabla \mathbf{E}_r^t(s) ds. \quad (2.10)$$

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208 **2.1 Thermodynamics**

209 For a mechanical system, we have in general that

$$210 \frac{d}{dt} T(t) + \mathcal{P}_m^i(t) = \mathcal{P}_m^e(t), \quad (2.11)$$

211 where $T(t)$ is the kinetic energy, while $\mathcal{P}_m^i(t)$ and
212 $\mathcal{P}_m^e(t)$ denote the internal and external mechanical
213 power per unit volume of the system, respectively. In
214 the case of a simple fluid, $\mathcal{P}_m^i(t) = \mathbf{T}(t) \cdot \mathbf{D}(t)$. Equa-
215 tion (2.11) is an expression of the balance of power.

216 For non-simple materials the first law assumes the
217 form

$$218 \rho \dot{e}(t) = \rho h(t) + \mathcal{P}_m^i(t), \quad (2.12)$$

219 where e is the internal energy and h is the specific in-
220 ternal heat power, defined as the rate at which heat is
221 absorbed per unit mass. *The heat balance law*

$$222 \rho h = -\nabla \cdot \mathbf{q} + \rho r, \quad (2.13)$$

223 relates h to the heat supply r and the heat flux \mathbf{q} . The
224 Fourier relation,

$$225 \mathbf{q} = -k_0 \nabla \vartheta, \quad k_0 > 0, \quad (2.14)$$

226 will be adopted. The second law yields the existence
227 of the entropy function η with the property that

$$228 \rho \dot{\eta} \geq -\nabla \cdot \left(\frac{\mathbf{q}}{\vartheta} \right) + \rho \frac{r}{\vartheta}, \quad (2.15)$$

229 whence it follows that

$$230 \rho \dot{\eta} \geq \rho \frac{h}{\vartheta} - \frac{k_0}{\vartheta^2} |\nabla \vartheta|^2. \quad (2.16)$$

231 Introducing the free energy $\psi = e - \vartheta \eta$, we can write
232 this as

$$233 \dot{\psi} \leq -\eta \dot{\vartheta} + \frac{1}{\rho} \mathcal{P}_m^i + \frac{k_0}{\rho \vartheta} |\nabla \vartheta|^2, \quad (2.17)$$

234 where (2.12) has been used.

235 The *equation of motion* for the material has the
236 form

$$237 \rho \dot{\mathbf{v}} = \nabla \cdot \mathbf{T} + \rho \mathbf{f}, \quad (2.18)$$

238 where \mathbf{f} denotes the body forces. In order to derive an
239 expression for \mathcal{P}_m^i , we multiply this relation by \mathbf{v} to
240 obtain

$$241 \rho \frac{d}{dt} \left(\frac{1}{2} \mathbf{v}^2 \right) = (\nabla \cdot \mathbf{T}) \cdot \mathbf{v} + \rho \mathbf{f} \cdot \mathbf{v}, \quad (2.19)$$

242 where, taking into account (2.9) and the incompress-
243 ibility condition $\nabla \cdot \mathbf{v} = 0$,

$$244 (\nabla \cdot \mathbf{T}) \cdot \mathbf{v} = -\mathbf{T} \cdot \nabla \mathbf{v} + \nabla \cdot (\mathbf{T} \mathbf{v})$$

$$245 = -2 \int_0^{+\infty} \mu'(s) \mathbf{E}_r^t(s) \cdot \nabla \mathbf{v}(t) ds$$

$$246 - \int_0^{+\infty} \varkappa'(s) \nabla \mathbf{E}_r^t(s) \cdot \nabla \nabla \mathbf{v}(t) ds$$

$$247 + \nabla \cdot \left(\left\{ [-p + \alpha(\vartheta(t) - \vartheta_0)] \mathbf{I} \right. \right.$$

$$248 \left. \left. + 2 \int_0^{+\infty} \mu'(s) \mathbf{E}_r^t(s) ds \right. \right.$$

$$249 \left. \left. - \int_0^{+\infty} \varkappa'(s) \nabla \cdot \nabla \mathbf{E}_r^t(s) ds \right\} \mathbf{v} \right.$$

$$250 \left. + \int_0^{+\infty} \varkappa'(s) \nabla \mathbf{E}_r^t(s) ds \nabla \mathbf{v}(t) \right).$$

251 Therefore, the equation of power balance is given by

$$252 \rho \frac{d}{dt} \left(\frac{1}{2} \mathbf{v}^2 \right) + 2 \int_0^{+\infty} \mu'(s) \mathbf{E}_r^t(s) \cdot \nabla \mathbf{v}(t) ds$$

$$253 + \int_0^{+\infty} \varkappa'(s) \nabla \mathbf{E}_r^t(s) \cdot \nabla \nabla \mathbf{v}(t) ds$$

$$254 = \nabla \cdot \left(\left\{ [-p + \alpha(\vartheta(t) - \vartheta_0)] \mathbf{I} \right. \right.$$

$$255 \left. \left. + 2 \int_0^{+\infty} \mu'(s) \mathbf{E}_r^t(s) ds \right. \right.$$

$$256 \left. \left. - \int_0^{+\infty} \varkappa'(s) \nabla \cdot \nabla \mathbf{E}_r^t(s) ds \right\} \mathbf{v}(t) \right.$$

$$257 \left. + \int_0^{+\infty} \varkappa'(s) \nabla \mathbf{E}_r^t(s) ds \nabla \mathbf{v}(t) \right) + \rho \mathbf{f} \cdot \mathbf{v}. \quad (2.20)$$

258 We deduce from (2.11) that the internal power is ex-
259 pressed by

$$260 \mathcal{P}_m^i(t) = 2 \int_0^{+\infty} \mu'(s) \mathbf{E}_r^t(s) \cdot \nabla \mathbf{v}(t) ds$$

$$261 + \int_0^{+\infty} \varkappa'(s) \nabla \mathbf{E}_r^t(s) \cdot \nabla \nabla \mathbf{v}(t) ds$$

$$262 = 2 \int_0^{+\infty} \mu(s) \dot{\mathbf{E}}^t(s) \cdot \dot{\mathbf{E}}(t) ds$$

$$263 + \int_0^{+\infty} \varkappa(s) \nabla \dot{\mathbf{E}}^t(s) \cdot \nabla \dot{\mathbf{E}}(t) ds. \quad (2.21)$$

The last form follows from (2.4), (2.5)₁, (2.7) and (2.8). The external power is given by the quantity at the right-hand side of (2.20), since the divergence term can be expressed as a surface contribution and the body force is clearly external.

To characterize the behaviour of our fluid, we introduce the state

$$\sigma^T(t) = (\vartheta, \sigma(t)) = (\vartheta, \mathbf{E}_r^t(s), \nabla \mathbf{E}_r^t(s)), \quad (2.22)$$

and the process P^T given by a piecewise continuous map defined as

$$P^T(\tau) = (\dot{\vartheta}_P, P) = (\dot{\vartheta}_P, \dot{\mathbf{E}}_P(\tau), \nabla \dot{\mathbf{E}}_P(\tau)) \quad \forall \tau \in [0, d], \quad (2.23)$$

where d , which generally has a finite value, denotes the duration of the process.

More details on this abstract terminology, which is used below to a limited extent, may be found in [13], for example.

Now, we seek a free energy ψ having the form

$$\psi(\sigma^T(t)) = \psi_1(\vartheta) + \psi_2(\mathbf{E}_r^t(s), \nabla \mathbf{E}_r^t(s)), \quad (2.24)$$

expressed as the sum of $\psi_1(\vartheta)$, a temperature dependent function, and $\psi_2(\mathbf{E}_r^t(s), \nabla \mathbf{E}_r^t(s))$, a functional of $(\mathbf{E}_r^t(s), \nabla \mathbf{E}_r^t(s))$.

Substituting into (2.17), we obtain

$$\left[\frac{\partial \psi_1(\vartheta)}{\partial \vartheta} + \eta \right] \dot{\vartheta} + \dot{\psi}_2(\mathbf{E}_r^t(s), \nabla \mathbf{E}_r^t(s)) \leq \frac{1}{\rho} \mathcal{P}_m^i + \frac{k_0}{\rho \vartheta} |\nabla \vartheta|^2. \quad (2.25)$$

The final term on the right is non-negative. This inequality, taking account of (2.21), is satisfied if

$$\eta = - \frac{\partial \psi_1(\vartheta)}{\partial \vartheta},$$

$$\dot{\psi}_2(\mathbf{E}_r^t(s), \nabla \mathbf{E}_r^t(s)) \leq \frac{1}{\rho} \left[2 \int_0^{+\infty} \mu'(s) \mathbf{E}_r^t(s) \cdot \dot{\mathbf{E}}(t) ds + \int_0^{+\infty} \varkappa'(s) \nabla \mathbf{E}_r^t(s) \cdot \nabla \dot{\mathbf{E}}(t) ds \right]. \quad (2.26)$$

The inequality (2.26)₂ is an expression of the second law for the mechanical aspect of the problem. Taking account of the incompressibility of the fluid, we can absorb the density into the kernels and write this relation as

$$\dot{\psi}_2(\mathbf{E}_r^t(s), \nabla \mathbf{E}_r^t(s)) \leq \mathcal{A}(\sigma, P), \quad (2.27)$$

where

$$\begin{aligned} \mathcal{A}(t) &= \mathcal{A}(\sigma, P) = \frac{1}{\rho} \mathcal{P}_m^i(t) \\ &= 2 \int_0^{+\infty} \mu'(s) \mathbf{E}_r^t(s) ds \cdot \dot{\mathbf{E}}(t) \\ &\quad + \int_0^{+\infty} \varkappa'(s) \nabla \mathbf{E}_r^t(s) ds \cdot \nabla \dot{\mathbf{E}}(t) \\ &= 2 \int_0^{+\infty} \mu(s) \dot{\mathbf{E}}^t(s) \cdot \dot{\mathbf{E}}(t) ds \\ &\quad + \int_0^{+\infty} \varkappa(s) \nabla \dot{\mathbf{E}}^t(s) \cdot \nabla \dot{\mathbf{E}}(t) ds \\ &= 2 \int_{-\infty}^t \mu(t-u) \dot{\mathbf{E}}(u) du \cdot \dot{\mathbf{E}}(t) \\ &\quad + \int_{-\infty}^t \varkappa(t-u) \nabla \dot{\mathbf{E}}(u) du \cdot \nabla \dot{\mathbf{E}}(t), \quad (2.28) \end{aligned}$$

with the aid of (2.5)–(2.8) and a change of integration variables. This quantity, which is the internal mechanical power per unit mass, is analogous to what was termed the entropy action in [3] and generalizes the work function which is central to the discussion of simple materials.

By introducing $D_2(\mathbf{x}, t)$, a non-negative function referred to as the internal dissipation rate, we can transform the inequality (2.27) into an equality

$$\dot{\psi}_2(t) + D_2(t) = \mathcal{A}(t). \quad (2.29)$$

The non-negativity of D_2 in (2.29) is in effect a statement of the second law for the mechanical aspect of the problem.

Recalling (2.6), we see that $\mathbf{E}_r^t(s)$ and $\nabla \mathbf{E}_r^t(s)$ depend on the histories $\mathbf{E}^t(s)$, $\nabla \mathbf{E}^t(s)$ and current values $\mathbf{E}(t)$ and $\nabla \mathbf{E}(t)$. Thus,

$$\psi_2(t) = \tilde{\psi}(\mathbf{E}^t(s), \nabla \mathbf{E}^t(s), \mathbf{E}(t), \nabla \mathbf{E}(t)) \quad (2.30)$$

which is a functional of the histories and a function of the current values.

The quantity $\mathcal{A}(t)$ allows us to derive the total mechanical work per unit mass $\mathcal{B}(\sigma, P)$ done on the material during the application of a process P of duration d ,

$$\mathcal{B}(\sigma, P) = \int_t^{t+d} \mathcal{A}(\xi) d\xi. \quad (2.31)$$

A consequence of the second law is expressed by the following principle.

Referring to (2.22), we define the state $\sigma(t)$ for the mechanical aspect as

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$$\sigma(t) = (\mathbf{E}_r^t(s), \nabla \mathbf{E}_r^t(s)), \quad (2.32)$$

while $P(\tau) = (\dot{\mathbf{E}}_P(\tau), \nabla \dot{\mathbf{E}}_P(\tau))$. Let us denote by Σ and Π the sets of states and processes, which are admissible for the body. For any initial state $\sigma_i \in \Sigma$ and any process $P \in \Pi$, the state transition function $\hat{\rho}$ provides the final state $\sigma_f = \hat{\rho}(\sigma_i, P) \in \Sigma$. Moreover, let $P_\tau \in \Pi$ be any restriction of P to a subset $[0, \tau) \subset [0, d)$, with duration $\tau < d$. So, we have $\sigma(t) = \hat{\rho}(\sigma_0, P_t)$. A cycle is defined as any pair (σ, P) for which $\hat{\rho}(\sigma, P) = \sigma$.

Dissipation principle. On any cycle (σ, P) we have

$$\mathcal{B}(\sigma, P) \geq 0, \quad (2.33)$$

in which the equality sign occurs if and only if the cycle is reversible.

We define the total mechanical work per unit mass done on the material up to time t as

$$\mathcal{B}(t) = \int_{-\infty}^t \mathcal{A}(u) du, \quad (2.34)$$

where it is assumed that the infinite integral exists. Substituting the last form of \mathcal{A} , given by (2.28), into (2.34), we obtain, after integrations by parts, change of variables and other standard manipulations,

$$\begin{aligned} \mathcal{B}(t) = & \int_0^{+\infty} \int_0^{+\infty} \mu_{12}(|u-s|) \mathbf{E}_r^t(s) \cdot \mathbf{E}_r^t(u) ds du \\ & + \frac{1}{2} \int_0^{+\infty} \int_0^{+\infty} \varkappa_{12}(|u-s|) \nabla \mathbf{E}_r^t(s) \\ & \cdot \nabla \mathbf{E}_r^t(u) ds du, \end{aligned} \quad (2.35)$$

where

$$\begin{aligned} \mu_{12}(|u-s|) &= \frac{\partial^2}{\partial u \partial s} \mu(|u-s|), \\ \varkappa_{12}(|u-s|) &= \frac{\partial^2}{\partial u \partial s} \varkappa(|u-s|). \end{aligned} \quad (2.36)$$

2.2 Thermodynamic restrictions

The dissipation principle imposes thermodynamic restrictions on the constitutive equation (2.2). This can be demonstrated by combining (2.28)₃ and (2.31) with periodic histories of period $d = 2\pi/|\omega|$, for $\dot{\mathbf{E}}$ and $\nabla \dot{\mathbf{E}}$ given by

$$\begin{aligned} \dot{\mathbf{E}}(s) &= \cos \omega s \mathbf{c}_1 + \sin \omega s \mathbf{c}_2, \\ \nabla \dot{\mathbf{E}}(s) &= \cos \omega s \mathbf{C}_1 + \sin \omega s \mathbf{C}_2 \end{aligned} \quad (2.37)$$

where $\omega \in \mathbf{R} \setminus \{0\}$ and $\mathbf{c}_i, \mathbf{C}_i$ ($i = 1, 2$) are arbitrary non-zero second and third order tensors, respectively, depending only of \mathbf{x} . Following the steps outlined in [3], we deduce that

$$\mu_c(\omega) > 0, \quad \varkappa_c(\omega) > 0 \quad \forall \omega \in \mathbf{R}. \quad (2.38)$$

These in fact require the extra assumptions

$$\begin{aligned} \mu_c(0) &= \int_0^{+\infty} \mu(s) ds \neq 0, \\ \varkappa_c(0) &= \int_0^{+\infty} \varkappa(s) ds \neq 0. \end{aligned} \quad (2.39)$$

Let

$$\mathbf{D}^t(s) = \dot{\mathbf{E}} \quad \forall s \in \mathbf{R}^+,$$

be a constant (in time) history. Then (2.2) yields

$$\begin{aligned} \tilde{\mathbf{T}}(t) &= \mathbf{T}(t) + \{p - \alpha[\vartheta(t) - \vartheta_0]\} \mathbf{I} \\ &= 2\mu_\infty^{(1)} \dot{\mathbf{E}} - \varkappa_\infty^{(1)} \nabla \cdot \nabla \dot{\mathbf{E}}, \end{aligned}$$

where $\tilde{\mathbf{T}}$ is the extra stress tensor for constant histories and

$$\mu_\infty^{(1)} = \mu_c(0) > 0, \quad \varkappa_\infty^{(1)} = \varkappa_c(0) > 0 \quad (2.40)$$

by virtue of (2.38) and (2.39).

3 Free energies

We now consider some possible expressions for the part of the free energy $\psi_2(t) = \psi_2(\mathbf{E}_r^t, \nabla \mathbf{E}_r^t)$ introduced in (2.24). Our aim here is to adapt to non-simple fluids several classical functionals already introduced for simple linear viscoelastic solids and later modified to apply to simple fluids [1, 2].

For a simple fluid, any free energy has the well-known property that

$$\frac{\partial}{\partial \mathbf{E}(t)} \psi_2(t) = \tilde{\mathbf{T}}(t) \quad (3.1)$$

where $\tilde{\mathbf{T}}(t)$ is the extra stress defined by the first term on the right of (2.10). We will see that this does not hold for non-simple materials. Instead, a generalized version of this relation holds, which will be determined below.

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3.1 The Graffi–Volterra free energy

We firstly consider the important functional, frequently used in applications, known as the Graffi–Volterra free energy [19, 20, 22]. A generalization of this functional to our non-simple fluid is given by

$$\begin{aligned} \psi_{\mathcal{G}}(t) = & - \int_0^{+\infty} \mu'(s) \mathbf{E}_r^t(s) \cdot \mathbf{E}_r^t(s) ds \\ & - \frac{1}{2} \int_0^{+\infty} \varkappa'(s) \nabla \mathbf{E}_r^t(s) \cdot \nabla \mathbf{E}_r^t(s) ds. \end{aligned} \quad (3.2)$$

This is a free energy if the conditions

$$\begin{aligned} \mu'(s) < 0, \quad \varkappa'(s) < 0, \\ \mu''(s) \geq 0, \quad \varkappa''(s) \geq 0 \quad \forall s \in \mathbf{R}^+, \end{aligned} \quad (3.3)$$

are satisfied. The first two relations yield that $\psi_{\mathcal{G}}$ is positive, while the remaining relations are required to ensure a non-negative rate of dissipation related to this quantity. Indeed, differentiating $\psi_{\mathcal{G}}$ and integrating by parts, we can show, with the aid of (2.28)₂ and (2.29) that

$$\begin{aligned} D_{\mathcal{G}}(t) = & \int_0^{+\infty} \mu''(s) [\mathbf{E}_r^t(s)]^2 ds \\ & + \frac{1}{2} \int_0^{+\infty} \varkappa''(s) [\nabla \mathbf{E}_r^t(s)]^2 ds \geq 0 \end{aligned} \quad (3.4)$$

can be identified as the internal dissipation rate.

Note that, by virtue of (2.6),

$$\frac{\partial}{\partial \mathbf{E}(t)} \psi_{\mathcal{G}}(t) = 2 \int_0^{+\infty} \mu'(s) \mathbf{E}_r^t(s) ds \quad (3.5)$$

and (3.1) does not hold. Instead, we have

$$\frac{\partial}{\partial \nabla \mathbf{E}(t)} \psi_{\mathcal{G}}(t) = \int_0^{+\infty} \varkappa'(s) \nabla \mathbf{E}_r^t(s) ds \quad (3.6)$$

and the extra stress tensor (2.10) obeys the relation

$$\begin{aligned} \tilde{\mathbf{T}}(t) = & \frac{\partial}{\partial \mathbf{E}(t)} \psi_{\mathcal{G}}(t) - \nabla \cdot \frac{\partial}{\partial \nabla \mathbf{E}(t)} \psi_{\mathcal{G}}(t) \\ = & \frac{\delta}{\delta \mathbf{E}(t)} \psi_{\mathcal{G}}(t), \end{aligned} \quad (3.7)$$

which is a variational derivative, in the sense of the Calculus of Variations, for a function of $(\mathbf{E}(t), \nabla \mathbf{E}(t))$.

A relation exactly analogous to this form applies to all the free energy functionals considered in this work, and indeed to any free energy for any second order material.

3.2 Conditions for a free energy

We can generalize the Graffi conditions [11, 19, 20] for a free energy in the light of (3.7). The properties listed below will apply to all free energies for all second gradient materials, not just those discussed here.

P1 The first condition will be taken to be (3.7), replacing (3.1), or for a general free energy,

$$\begin{aligned} \tilde{\mathbf{T}}(t) = & \frac{\partial}{\partial \mathbf{E}(t)} \psi(t) - \nabla \cdot \frac{\partial}{\partial \nabla \mathbf{E}(t)} \psi(t) \\ = & \frac{\delta}{\delta \mathbf{E}(t)} \psi(t), \end{aligned} \quad (3.8)$$

which is a variational derivative with respect to the dependence of ψ on the fields $(\mathbf{E}(t), \nabla \mathbf{E}(t))$ at the current time. For linear constitutive relations such as (2.10), conditions analogous to (3.5) and (3.6) hold, which yield (3.8).

P2 Let \mathbf{E}^\dagger be a static history equal to $\mathbf{E}(t)$ at the current and all past times. Then

$$\psi(\mathbf{E}^\dagger, \nabla \mathbf{E}^\dagger, \mathbf{E}(t), \nabla \mathbf{E}(t)) = \phi(\mathbf{E}(t), \nabla \mathbf{E}(t)), \quad (3.9)$$

where $\phi(\mathbf{E}(t), \nabla \mathbf{E}(t))$ is the equilibrium free energy. This is in fact a definition of ϕ , included here for completeness. It vanishes for the free energies relating to the material under discussion.

P3 For any history and current value $(\mathbf{E}^\dagger, \nabla \mathbf{E}^\dagger, \mathbf{E}(t), \nabla \mathbf{E}(t))$,

$$\psi(\mathbf{E}^\dagger, \nabla \mathbf{E}^\dagger, \mathbf{E}(t), \nabla \mathbf{E}(t)) \geq \phi(\mathbf{E}(t), \nabla \mathbf{E}(t)). \quad (3.10)$$

P4 Condition (2.29) holds or, omitting subscripts,

$$\dot{\psi}(t) + D(t) = \mathcal{A}(t), \quad D(t) \geq 0, \quad (3.11)$$

where $D(t)$ is the rate of internal dissipation. The form of $\mathcal{A}(t)$ will depend on the material. The first relation is a statement of the first law, while the non-negativity of $D(t)$ is in effect the second law.

3.3 Dill's free energy

The Dill functional [9] can be generalized to the form

$$\begin{aligned} \psi_{Dill}(t) = & \int_0^{+\infty} \int_0^{+\infty} \mu''(\xi_1 + \xi_2) \mathbf{E}_r^t(\xi_1) \\ & \cdot \mathbf{E}_r^t(\xi_2) d\xi_1 d\xi_2 \\ & + \frac{1}{2} \int_0^{+\infty} \int_0^{+\infty} \varkappa''(\xi_1 + \xi_2) \nabla \mathbf{E}_r^t(\xi_1) \\ & \cdot \nabla \mathbf{E}_r^t(\xi_2) d\xi_1 d\xi_2. \end{aligned} \quad (3.12)$$

Differentiating this with respect to time, as for the Graffi-Volterra case, we find, after standard manipulations ([3], for example) and using (3.11), that the associated rate of dissipation is given by

$$D_{Dill}(t) = - \int_0^{+\infty} \int_0^{+\infty} \mu'(\xi_1 + \xi_2) \dot{\mathbf{E}}^t(\xi_1) \cdot \dot{\mathbf{E}}^t(\xi_2) d\xi_1 d\xi_2 - \int_0^{+\infty} \int_0^{+\infty} \varkappa'(\xi_1 + \xi_2) \nabla \dot{\mathbf{E}}^t(\xi_1) \cdot \nabla \dot{\mathbf{E}}^t(\xi_2) d\xi_1 d\xi_2. \quad (3.13)$$

Both of these functionals are non-negative for all histories if μ' and \varkappa' are strictly monotonic, as defined in [6].

One can show that the equivalent of (3.5) and (3.6) are true for ψ_{Dill} , from which it follows that relation (3.8) holds.

3.4 A free energy in terms of the minimal state

A free energy $\psi_{\mathcal{F}}$, recently introduced and considered, in particular, in [10] and [7] for viscoelastic solids, can be adapted to our fluid.

Two different histories $(\mathbf{E}_{1r}^0, \nabla \mathbf{E}_{1r}^0)$ and $(\mathbf{E}_{2r}^0, \nabla \mathbf{E}_{2r}^0)$ up to time $t = 0$, which coincide after this time, are in the same minimal state if they produce the same stress function for $t \geq 0$. This terminology was introduced in [11] where references to the earlier development of the underlying ideas are given. The categories of materials for which non-trivial examples of such states can arise are discussed in [7]. A simple generalization of arguments in these and other references (e.g. [1, 2]) yields that the quantities

$$\mathbf{I}^t(\tau, \mathbf{E}_r^t) = 2 \int_0^{+\infty} \mu'(\tau + \eta) \mathbf{E}_r^t(\eta) d\eta, \quad (3.14)$$

$$\mathfrak{J}^t(\tau, \nabla \mathbf{E}_r^t) = \int_0^{+\infty} \varkappa'(\tau + \eta) \nabla \mathbf{E}_r^t(\eta) d\eta,$$

have the same values for different histories in the same minimal state, in other words are functionals of the minimal state. Consider the following functional

$$\psi_{\mathcal{F}}(t) = - \frac{1}{4} \int_0^{+\infty} \frac{1}{\mu'(\tau)} |\mathbf{I}_{(1)}^t(\tau, \mathbf{E}_r^t)|^2 d\tau - \frac{1}{2} \int_0^{+\infty} \frac{1}{\varkappa'(\tau)} |\mathfrak{J}_{(1)}^t(\tau, \nabla \mathbf{E}_r^t)|^2 d\tau, \quad (3.15)$$

where $\mathbf{I}_{(1)}^t$ and $\mathfrak{J}_{(1)}^t$ are the derivatives with respect to τ of \mathbf{I}^t and \mathfrak{J}^t , giving

$$\mathbf{I}_{(1)}^t(\tau, \mathbf{E}_r^t) = \frac{d}{d\tau} \mathbf{I}^t(\tau, \mathbf{E}_r^t) = 2 \int_0^{+\infty} \mu''(\tau + \eta) \mathbf{E}_r^t(\eta) d\eta, \quad (3.16)$$

$$\mathfrak{J}_{(1)}^t(\tau, \nabla \mathbf{E}_r^t) = \frac{d}{d\tau} \mathfrak{J}^t(\tau, \nabla \mathbf{E}_r^t) = \int_0^{+\infty} \varkappa''(\tau + \eta) \nabla \mathbf{E}_r^t(\eta) d\eta.$$

The absolute value squared notation in (3.15) indicates scalar products of $\mathbf{I}_{(1)}^t$ and $\mathfrak{J}_{(1)}^t$ with themselves in the appropriate vector spaces. Under the hypotheses (3.3), this functional is a free energy. Note that

$$\mathbf{I}^t(0, \mathbf{E}_r^t) = 2 \int_0^{+\infty} \mu'(\eta) \mathbf{E}_r^t(\eta) d\eta, \quad (3.17)$$

$$\mathfrak{J}^t(0, \nabla \mathbf{E}_r^t) = \int_0^{+\infty} \varkappa'(\eta) \nabla \mathbf{E}_r^t(\eta) d\eta$$

and

$$\mathbf{I}_{(1)}^t(0, \mathbf{E}_r^t) = 2 \int_0^{+\infty} \mu''(\eta) \mathbf{E}_r^t(\eta) d\eta, \quad (3.18)$$

$$\mathfrak{J}_{(1)}^t(0, \nabla \mathbf{E}_r^t) = \int_0^{+\infty} \varkappa''(\eta) \nabla \mathbf{E}_r^t(\eta) d\eta.$$

Use of (3.17) and (2.28)₂ gives that $\psi_{\mathcal{F}}(t)$ obeys (3.11) where the associated rate of dissipation has the form

$$D_{\mathcal{F}}(t) = \frac{1}{4} \int_0^{+\infty} \frac{\mu''(\tau)}{[\mu'(\tau)]^2} |\mathbf{I}_{(1)}^t(\tau, \mathbf{E}_r^t)|^2 d\tau - \frac{1}{4\mu'(0)} |\mathbf{I}_{(1)}^t(0, \mathbf{E}_r^t)|^2 + \frac{1}{2} \int_0^{+\infty} \frac{\varkappa''(\tau)}{[\varkappa'(\tau)]^2} |\mathfrak{J}_{(1)}^t(\tau, \nabla \mathbf{E}_r^t)|^2 d\tau - \frac{1}{2\varkappa'(0)} |\mathfrak{J}_{(1)}^t(0, \nabla \mathbf{E}_r^t)|^2 \geq 0, \quad (3.19)$$

because of the hypotheses (3.3).

The functional $\psi_{\mathcal{F}}$ is manifestly a functional of the minimal state. This is not a necessary requirement for a free energy (and in particular is not true for $\psi_{\mathcal{G}}$ given by (3.2)) though it is an attractive property from a theoretical viewpoint. The Dill free energy and the minimum free energy, derived in the next section, both have this property.

The equivalent of (3.5) and (3.6) for $\psi_{\mathcal{F}}$ can be obtained within the manipulations leading to (3.19). These then imply that relation (3.8) holds.

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701 3.5 The minimum free energy

702
 703 The form of the minimum free energy for second gra-
 704 dient incompressible viscoelastic fluids of the kind un-
 705 der discussion can be derived by generalizing one of
 706 the direct methods outlined in [8, 11, 16] or [1, 2, 15],
 707 which was done in [3]. However, we shall adopt a sim-
 708 pler approach here, namely by using a precise analogy
 709 between the present theory and that for a simple mate-
 710 rial.

711 The core observation is that an explicit formula for
 712 the minimum free energy can be derived by exactly
 713 the same formalism for materials described on differ-
 714 ent vector spaces, provided that the work function has
 715 the same general structure in each case. Thus, we have
 716 the theory developed in [8] for a simple material with
 717 independent and dependent field variables in Sym and
 718 relaxation tensors in $Lin(Sym)$, while in [12, 18], non-
 719 isothermal theories were developed on more general
 720 vector spaces. However, the procedures and results are
 721 precisely analogous for these materials. In particular
 722 they all depend on the factorization of a positive defi-
 723 nite tensor which arises in the work function. The level
 724 of practical difficulty associated with carrying out this
 725 factorization will of course depend on the details of
 726 the material.

727 For a second gradient incompressible viscoelas-
 728 tic fluid, the underlying vector space is $\Gamma = Sym \times$
 729 $(Sym \times \mathbf{R})$ associated with states $\sigma(t) = (\mathbf{E}_r^t, \nabla \mathbf{E}_r^t)$.
 730 Referring to (2.6), we introduce the compact notation

731 $\mathbb{C}(t) = (\mathbf{E}(t), \nabla \mathbf{E}(t)) \in \Gamma,$
 732 $\mathbb{C}_r^t(s) = (\mathbf{E}_r^t(s), \nabla \mathbf{E}_r^t(s)) = \mathbb{C}^t(s) - \mathbb{C}(t) \in \Gamma.$ (3.20)

733 The quantity $\mathcal{B}(t)$, given by (2.35), can be written in
 734 the form

735
$$\mathcal{B}(t) = \frac{1}{2} \int_0^\infty \int_0^\infty \mathbb{L}_{12}(|u-s|) \mathbb{C}_r^t(s) \cdot \mathbb{C}_r^t(u) du ds,$$
 (3.21)

736 where $\mathbb{L} \in Lin(\Gamma)$ is the diagonal tensor

737
$$\mathbb{L}(s) = 2\mu(s)\mathbb{P}_S + \varkappa(s)\mathbb{P}_{SR},$$
 (3.22)

738 where the quantities $\mathbb{P}_S, \mathbb{P}_{SR} \in Lin(\Gamma)$ are real orthog-
 739 onal projectors on Sym and $Sym \times \mathbf{R}$, respectively.
 740 The quantity $\mathcal{B}(t)$ corresponds to the work function
 741 for simple materials and crucially for our purposes,
 742 has exactly the same general form. Using the convolu-
 743 tion theorem and Parseval's formula, we can write it in
 744 terms of the frequency domain quantities, as follows:

751
$$\mathcal{B}(t) = \frac{1}{2\pi} \int_{-\infty}^\infty \mathbb{H}(\omega) \mathbb{C}_{r+}^t(\omega) \cdot \overline{\mathbb{C}_{r+}^t(\omega)} d\omega,$$
 (3.23)

752 where $\mathbb{C}_{r+}^t(\omega)$ is the Fourier transform of $\mathbb{C}_r^t(s)$, de-
 753 fined by (4.2)₂, while $\overline{\mathbb{C}_{r+}^t(\omega)}$ is its complex conju-
 754 gate. The tensor $\mathbb{H} \in Lin(\Gamma)$ is given by

755
$$\mathbb{H}(\omega) = -\omega \mathbb{L}'_s(\omega) = 2\omega^2 \mu_c(\omega) \mathbb{P}_S + \omega^2 \varkappa_c(\omega) \mathbb{P}_{SR} \geq 0,$$
 (3.24)

756 where (4.4) has been used.

757 Therefore, for purposes of deriving the form of the
 758 minimum free energy, the only difference relating to
 759 non-simple materials is that they are described on a
 760 larger vector space. Indeed, the same is true for any
 761 other free energy. Such a formulation is being de-
 762 veloped in the context of a general theory of non-
 763 simple materials and the free energies associated with
 764 them [5]. It emerges from this work that the free en-
 765 ergies discussed here are special (diagonal) cases of
 766 more general formulae.

767 Because of the thermodynamic constraints (2.38),
 768 the scalar functions $\mu_c(\omega)$ and $\varkappa_c(\omega)$ in (3.24) can be
 769 factorized [16] to give

770
$$\mu_c(\omega) = \mu_+(\omega)\mu_-(\omega),$$

 771
$$\varkappa_c(\omega) = \varkappa_+(\omega)\varkappa_-(\omega),$$
 (3.25)

772 where $\mu_+(\omega)$ and $\varkappa_+(\omega)$ are analytic in \mathbf{C}^- while
 773 $\mu_-(\omega)$ and $\varkappa_-(\omega)$ are analytic in \mathbf{C}^+ . Therefore

774
$$\mathbb{H}(\omega) = \mathbb{H}_+(\omega)\mathbb{H}_-(\omega) = [H_{\mu_+}(\omega)\mathbb{P}_S + H_{\varkappa_+}(\omega)\mathbb{P}_{SR}] \times [(H_{\mu_-}(\omega)\mathbb{P}_S + H_{\varkappa_-}(\omega)\mathbb{P}_{SR})],$$
 (3.26)

775
$$H_{\mu_\pm}(\omega) = \sqrt{2}\omega\mu_\pm(\omega), \quad H_{\varkappa_\pm}(\omega) = \omega\varkappa_\pm(\omega),$$

776 which gives the required factorization of \mathbb{H} for the
 777 present diagonal case. The general non-diagonal case
 778 is discussed in [5].

779 The derivation of the form of the minimum free en-
 780 ergy proceeds exactly as described in earlier papers,
 781 for example [8, 11, 16]. We simply present the results
 782 here. The Plemelj formulae [21] give that

783
$$\mathbb{H}_-(\omega)\mathbb{C}_{r+}^t(\omega) = \mathbf{p}_-^t(\omega) - \mathbf{p}_+^t(\omega),$$

 784
$$\mathbf{p}_\pm^t(\omega) = \frac{1}{2\pi i} \int_{-\infty}^\infty \frac{\mathbb{H}_-(\omega')\mathbb{C}_{r+}^t(\omega')}{\omega' - \omega^\mp} d\omega',$$
 (3.27)

785 where $\omega^\mp = \lim_{\alpha \rightarrow 0^+} (\omega + i\alpha)$ and the limit is under-
 786 stood to take place after the integration has been car-
 787 ried out. The form of the minimum free energy is

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$$\begin{aligned} \psi_m(t) &= \frac{1}{2\pi} \int_{-\infty}^{\infty} |\mathbf{p}'_{\mu-}(\omega)|^2 d\omega \\ &= \frac{1}{2\pi} \int_{-\infty}^{\infty} |p'_{\mu-}(\omega)|^2 d\omega \\ &\quad + \frac{1}{2\pi} \int_{-\infty}^{\infty} |p'_{\varkappa-}(\omega)|^2 d\omega, \end{aligned} \quad (3.28)$$

$$\begin{aligned} p'_{\mu-}(\omega) &= \frac{1}{2\pi i} \int_{-\infty}^{\infty} \frac{H_{\mu-}(\omega') \mathbf{E}'_{r+}(\omega')}{\omega' - \omega^+} d\omega', \\ p'_{\varkappa-}(\omega) &= \frac{1}{2\pi i} \int_{-\infty}^{\infty} \frac{H_{\varkappa-}(\omega') \nabla \mathbf{E}'_{r+}(\omega')}{\omega' - \omega^+} d\omega'. \end{aligned}$$

The second form of $\psi_m(t)$ follows from the properties of the projectors. Using the method outlined in [17] for example, one can show that results corresponding to (3.5), (3.6) and (3.8) hold. These may be written in the compact notation

$$\begin{aligned} \frac{\partial}{\partial \mathbb{C}(t)} \psi_m(t) &= \mathbb{D}(t) = (\mathbb{D}_1(t), \mathbb{D}_2(t)) \in \Gamma, \\ \mathbb{D}_1(t) &= 2 \int_0^{+\infty} \mu'(s) \mathbf{E}'_r(s) ds \in \text{Sym}, \\ \mathbb{D}_2(t) &= \int_0^{+\infty} \varkappa'(s) \nabla \mathbf{E}'_r(s) ds \in \text{Sym} \times \mathbf{R}, \end{aligned} \quad (3.29)$$

$$\tilde{\mathbf{T}}(t) = \mathbb{D}_1(t) - \nabla \cdot \mathbb{D}_2(t) = \frac{\delta \psi_m(t)}{\delta \mathbf{E}(t)}.$$

From (2.28)₂, we have the relation $\mathcal{A}(t) = \mathbb{D}(t) \cdot \dot{\mathbf{C}}(t)$, and (3.11) can be written as

$$\dot{\psi}_m(t) + D_m(t) = \mathbb{D}(t) \cdot \dot{\mathbf{C}}(t), \quad (3.30)$$

where D_m is the rate of dissipation corresponding to the minimum free energy and must be non-negative by the second law. Referring to the formulae developed in [8, 11, 16] for example, we see that it is given by

$$\begin{aligned} D_m(t) &= |\mathbf{K}_{\mu}(t)|^2 + |\mathbf{K}_{\varkappa}(t)|^2, \\ \mathbf{K}_{\mu}(t) &= \frac{1}{2\pi} \int_{-\infty}^{\infty} H_{\mu-}(\omega) \mathbf{E}'_{r+}(\omega) d\omega, \\ \mathbf{K}_{\varkappa}(t) &= \frac{1}{2\pi} \int_{-\infty}^{\infty} H_{\varkappa-}(\omega) \nabla \mathbf{E}'_{r+}(\omega) d\omega, \end{aligned} \quad (3.31)$$

again with the use of the properties of projectors.

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Appendix

Various notations used in the main paper are defined here.

The real axis is denoted by \mathbf{R} , while $\mathbf{R}^+ = [0, +\infty)$ and $\mathbf{R}^- = (-\infty, 0]$. Also, $\mathbf{R}^{--} = (-\infty, 0)$ and $\mathbf{R}^{++} = (0, +\infty)$.

The Fourier transform of any function $f : \mathbf{R} \rightarrow \mathbf{R}^n$ is defined by

$$\begin{aligned} f_F(\omega) &= \int_{-\infty}^{+\infty} f(s) e^{-i\omega s} ds \\ &= f_-(\omega) + f_+(\omega) \quad \forall \omega \in \mathbf{R}, \end{aligned} \quad (4.1)$$

where

$$\begin{aligned} f_-(\omega) &= \int_{-\infty}^0 f(s) e^{-i\omega s} ds, \\ f_+(\omega) &= \int_0^{+\infty} f(s) e^{-i\omega s} ds. \end{aligned} \quad (4.2)$$

The half-range Fourier cosine and sine transforms are given by

$$\begin{aligned} f_c(\omega) &= \int_0^{+\infty} f(s) \cos \omega s ds, \\ f_s(\omega) &= \int_0^{+\infty} f(s) \sin \omega s ds. \end{aligned} \quad (4.3)$$

If $f(u)$ vanishes as $u \rightarrow +\infty$, we have

$$f'_s(\omega) = -\omega f_c(\omega). \quad (4.4)$$

If $f'(0)$ is non-zero, then

$$\begin{aligned} \lim_{\omega \rightarrow \infty} i\omega f'_+(\omega) &= f'(0) = \lim_{\omega \rightarrow \infty} \omega f'_s(\omega) \\ &= - \lim_{\omega \rightarrow \infty} \omega^2 f_c(\omega), \end{aligned} \quad (4.5)$$

by virtue of (4.4).

Finally, we define the following subsets of the complex z -plane \mathbf{C} :

$$\begin{aligned} \mathbf{C}^{(-)} &= \{z \in \mathbf{C}; \text{Im } z \in \mathbf{R}^{--}\}, \\ \mathbf{C}^{(+)} &= \{z \in \mathbf{C}; \text{Im } z \in \mathbf{R}^{++}\}, \\ \mathbf{C}^- &= \{z \in \mathbf{C}; \text{Im } z \in \mathbf{R}^-\}, \\ \mathbf{C}^+ &= \{z \in \mathbf{C}; \text{Im } z \in \mathbf{R}^+\}. \end{aligned} \quad (4.6)$$

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