

# The Effect of Co and Zn Addition on Densification and Electrical Properties of Ceria-Based Nanopowders

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In this work, cobalt and zinc-doped  $\text{Ce}_{0.8}\text{Gd}_{0.2}\text{O}_{1.9}$  samples were prepared starting from a commercial nanopowder and compared to the undoped material. The powder samples were pressed and afterwards sintered by a two-step procedure, before characterization by X-Ray Diffraction (XRD), X-ray photoelectron spectroscopy (XPS), Scanning Electron Microscopy (SEM), Transmission Electron Microscopy (TEM) and Impedance Spectroscopy (IS) in air. Cobalt or zinc additions are effective as sintering aid, allowing peak sintering temperatures around 1000 °C to reach densifications above of 93% of theoretical density, showing no evidence for the presence of secondary phases. The total conductivity at 800 °C of pressed Zn-doped samples ( $6.7 \times 10^{-2}$  S/cm) and Co-doped samples ( $7.5 \times 10^{-2}$  S/cm) is similar for undoped samples ( $7.2 \times 10^{-2}$  S/cm) showing that Zn and Co has a positive effect on densification without compromising the electrical conductivity.

**Keywords:** gadolinium-doped ceria, cobalt addition, zinc addition, XPS, SOFC

## 1. Introduction

Solid oxide fuel cell (SOFC) has attracted considerable interest in the last few decades as a promising clean and efficient energy conversion device<sup>1-3</sup>. Classical designs employ yttria-stabilized zirconia (YSZ) as electrolyte, but it exhibits adequate ionic conductivity only at high temperatures (900-1000 °C). Such high temperatures limit the viability of fuel cells due to long-term stability and require expensive materials for sealing, insulation, and interconnects. Efforts to find new electrolyte materials with high electrical conductivity at lower SOFC operation temperatures have identified ceria based electrolytes as a substitute for YSZ<sup>2,3</sup>, and gadolinium-doped ceria (GDC) has shown to be amongst the most promising electrolytes<sup>4</sup>.

Ceria based electrolytes have been investigated over the past 20 years due to their high conductivity which makes them good candidates to be used at intermediate temperature (500-700 °C)<sup>3,5</sup>. A major difficulty in using ceria as electrolyte is related to the reduction of  $\text{Ce}^{+4}$  to  $\text{Ce}^{+3}$ , which is significant at low oxygen partial pressure ( $p(\text{O}_2) < 10^{-15}$  atm) and high temperature ( $T > 800$  °C)<sup>6</sup>. Another drawback regarding ceria solid solutions is their poor sinterability, which requires high temperatures (1400-1600 °C) to achieve high densification (> 95%)<sup>5</sup>.

Adequate methods have been developed to prepare dense ceria-based electrolytes at lower temperature, allowing for

the electrolyte-electrode co-sintering, which simplifies the fabrication process and reduces the cost. Three methods are the most used to achieve high densifications at low temperatures. One is based on decreasing the particle size of the powder to the nanoscale, hence increasing the driving force, i.e. specific surface area, for densification, thus the sintering temperatures are drastically reduced<sup>7</sup>. Conventional powders sinter at  $0.5-0.8 T_m$  (melting temperature), while nanopowders conveniently deagglomerated might sinter at temperatures as low as  $0.2-0.3 T_m$  for similar high density<sup>8</sup>. A second method consists on the use of sintering aids to promote densification through liquid phase sintering or assisted ionic flow along the grain boundaries<sup>9</sup>. Small amounts of sintering aids, e.g. CoO, MnO,  $\text{Fe}_2\text{O}_3$ , and CuO are very effective with respect to densification, but some of them exhibit a detrimental influence on grain boundary conductivity<sup>9-12</sup>. Recent work has showed the effectiveness of ZnO as sintering aid for yttrium-doped ceria (YDC), samarium-doped ceria (SDC), and GDC<sup>13</sup>. A third method involves the optimization of the sintering temperature profile, using the so-called two-step sintering route, with a peak temperature to activate the densification diffusion process, followed by a lower temperature dwell to proceed with densification with minimum grain growth<sup>14</sup>.

While the role of Co additions has been widely studied in recent years, the effect of Zn as sintering aid is less known. Furthermore, there is no systematic comparison between additives following a similar processing route, and starting from identical powders. In this work, the concomitant use

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of nanopowders and cobalt and zinc as sintering aids has been investigated together with the two-step sintering route. The sinterability, microstructure, and electrical conductivity of Co- and Zn-doped  $\text{Ce}_{0.8}\text{Gd}_{0.2}\text{O}_{1.9}$  samples were evaluated against the performance of undoped powders.

## 2. Experimental

$\text{Ce}_{0.8}\text{Gd}_{0.2}\text{O}_{1.9}$  (CGd), 2 mol% CoO-doped  $\text{Ce}_{0.8}\text{Gd}_{0.2}\text{O}_{1.9}$  (CGd-Co), and 0.2, 0.4 and 1 mol% ZnO-doped  $\text{Ce}_{0.8}\text{Gd}_{0.2}\text{O}_{1.9}$  (CGd-0.2Zn, CGd-0.4Zn and CGd-1Zn, respectively), were studied in this work. The starting materials were CGd (Fuel Cell Materials) with  $32.6 \text{ m}^2/\text{g}$  specific surface area,  $\text{Co}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  (Synth, 98% purity), and  $\text{Zn}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  (Synth, 99.98% purity). Appropriate amounts of these powders were mixed in isopropanol containing 1 wt% of poly-vinylbutyral (B-98, Solutia), in a vibratory mill with zirconia milling media. Before uniaxial pressing at 40 MPa, the suspensions were dried in air and granulated through a nylon sieve. The resulting pellets were isostatically pressed at 200 MPa and afterwards sintered following a two-step profile.

Information on early stages of sintering was obtained by dilatometry (Linseis L75, vertical) under a constant heating rate of  $5 \text{ }^\circ\text{C}/\text{min}$ . The peak sintering temperatures were thus adjusted to 1200 and  $1000 \text{ }^\circ\text{C}$ , while the dwell temperatures were 1000 and  $900 \text{ }^\circ\text{C}$  for 5 and 10 h, respectively, at fixed heating/cooling rates of  $5 \text{ }^\circ\text{C}/\text{min}$ . A short designation of the sintering conditions hereby adopted includes sequentially the peak and dwell temperatures, the latter followed by the dwell time (e.g., 1200-1000  $^\circ\text{C}/10\text{h}$ ).

The structure of the sintered samples was characterized by a Siemens D5000 X-ray diffractometer using  $\text{Cu K}\alpha$  source. Samples densities were measured using the Archimedes method. The microstructure of the polished and thermally etched surfaces was analyzed by scanning electron microscopy (SEM, Philips XL 30 FEG). The average grain size was measured by the mean lineal intercept method. Sintered samples were also analyzed by transmission electron microscopy (TEM, Hitachi H-9000).

X-ray photoelectron spectroscopy (XPS) results were obtained by a VSW HA-100 spherical analyzer using non-monochromated  $\text{Al K}\alpha$  radiation ( $h\nu = 1486.6 \text{ eV}$ ). The high resolution spectra were acquired using constant analyzer pass energy of 44 eV. The pressure inside the analysis chamber was kept below than  $2 \times 10^{-8} \text{ mbar}$ . The powdered samples were pressed into pellets and fixed to a stainless steel sample holder with double-faced conducting tape and analyzed without further preparation. Curve fitting was performed using Gaussian line shapes, and a Shirley background was subtracted from the data.

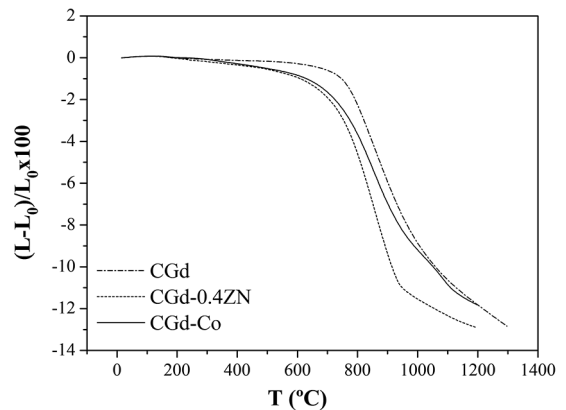
The electrical conductivity of the specimens was measured in air over the temperature range 200-800  $^\circ\text{C}$  using (two-probe) impedance spectroscopy (HP 4192 A) over the frequency range 5 Hz to 13 MHz, with a test signal amplitude

of 500 mV. Platinum paste electrodes were applied on both sides of the pellets.

## 3. Results and Discussion

### 3.1 Sintering Characterization

In order to analyze the effects of cobalt and zinc additions on the ceria-based solid solutions sintering process, a dilatometric analysis was performed (Figure 1). Pure CGd starts to shrink at approximately  $800 \text{ }^\circ\text{C}$ , while CGd-0.4Zn and CGd-Co show early signs of densification already at  $400 \text{ }^\circ\text{C}$ . Once densification starts it proceeds at a much higher rate in the Zn and Co doped samples than in pure CGd.



**Figure 1:** Shrinkage profiles obtained for undoped, zinc, and cobalt-doped samples.

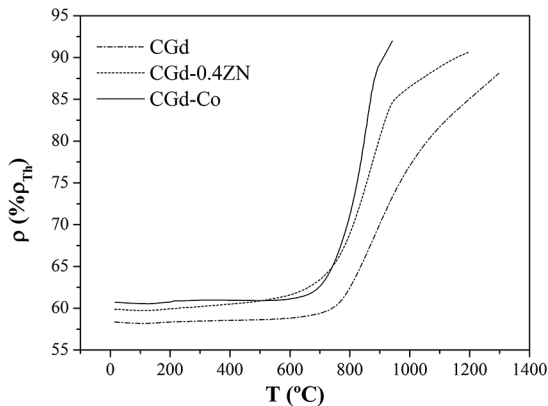
The densification curve (Figure 2) was calculated from the dilatometry data using equation 1<sup>15</sup>:

$$\% \rho_{th} = 100 \left( \frac{L_f}{L_t} \right)^3 \frac{\rho_f}{\rho_t} \quad (1)$$

where  $\% \rho_{th}$  is the percentage of theoretical density,  $L_f$  is the final sample length,  $L_t$  is the time length dependent and is equal to  $L_0 - \Delta L_0$  ( $L_0$  is the initial sample length and  $\Delta L_0$  is the sample displacement during time,  $t$ ),  $\rho_t$  is the theoretical sample density and  $\rho_f$  is the final sample density.

For Zn and Co-doped samples a considerable improvement of the sintering kinetics is observed (Figure 2). It can also be seen that the densification is completed within a narrow temperature interval for CGd-Co, indicating a faster densification and the temperature to achieve 90% of densification is  $\sim 900 \text{ }^\circ\text{C}$ . However, for CGd and CGd-0.4Zn samples, the temperature to attain the same densification is 1300 and  $1220 \text{ }^\circ\text{C}$ , respectively.

Zn and Co-additions (up to 1 mol%) have a major impact on densification, as shown by the relative densities of the



**Figure 2:** Percentage of theoretical density ( $\rho/\rho_{th}$ ) as function of temperature for CGd, CGd-0.4Zn and CGd-Co.

sintered samples in Table 1. Co or Zn additions favored the densification, with peak sintering temperatures as low as 1000 °C achieving densifications higher than 93%. These results agree with previously reported ones<sup>9,11-13</sup>.

### 3.2 Structural and Microstructural Characterization

Figure 3 presents the XRD diffractograms of the sintered samples. The diffraction peaks are indexed to the expected cubic fluorite structure, with no evidence for the presence of secondary phases. The additions of Co and Zn caused minimal changes in the lattice parameter, with a slight increase for the Zn-doped samples. Other authors did not detect either a secondary phase for the additions of 2 at.% of cobalt<sup>12</sup> and 1 at.%Zn<sup>13</sup> to CGd. If secondary phases are formed, they are below the XRD detection limit.

Figure 4 displays SEM micrographs of the sintered samples. (a) CGd-1200-1000 °C/10h fracture sintered sample, (b) CGd-0.4Zn-1000-900 °C/5h fracture sintered sample, (c) and (d) polished and thermally etched surfaces of CGd-0.4Zn and CGd-Co samples, respectively, sintered at 1200-1000 °C/10h. It can be observed the beneficial effect of the sintering aids. The Co addition caused the grains grow more steeply than the Zn additions (Table 1).

Figure 5 displays dark field TEM micrographs of (a) CGd and (b) CGd-1Zn samples sintered at 1200-1000 °C/10h. The micrographs show a homogeneous microstructure for the undoped and Zn-doped samples. An energy dispersive spectroscopy (EDS) analysis detected only Ce (79.2 at.%)

and Gd (20.8 at.%). It was not possible to detect the presence of Zn due to the low amount used, probably below the detection limit.

### 3.3 XPS Analysis

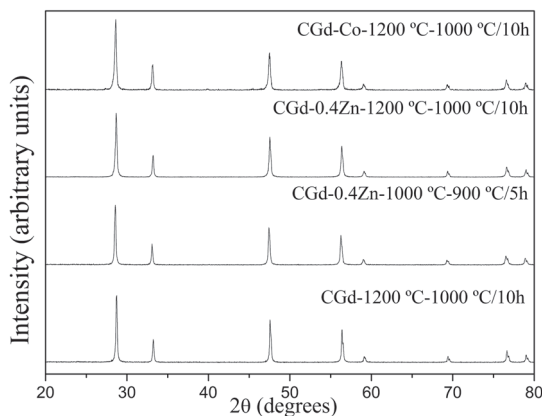
The chemical states of the constituent ions were analyzed by XPS. The Ce 3d spectrum is characterized by a complex line shape that reflects the final state occupation of the Ce 4f level. CeO<sub>2</sub> presents three pairs of spin-orbit doubles, while Ce<sub>2</sub>O<sub>3</sub> presents only two pairs<sup>16,17</sup>. The spin-orbit doublets are commonly denoted *v* and *u* and represent the 3d<sub>5/2</sub> and 3d<sub>3/2</sub> states, respectively. The *v* and *v'* peaks are attributed to a mixture of 3d<sup>9</sup>4f<sup>2</sup>(O 2p<sup>4</sup>) and 3d<sup>9</sup>4f<sup>1</sup>(O 2p<sup>5</sup>) Ce<sup>4+</sup> final states, and *v'''* peak, to 3d<sup>9</sup>4f<sup>0</sup>(O 2p<sup>6</sup>) Ce<sup>4+</sup> final state<sup>17</sup>. The series of *u* structures from the 3d<sub>3/2</sub> level can be explained in the same way. The *v*<sup>0</sup> and *v'* peaks correspond to the 3d<sup>9</sup>4f<sup>2</sup>(O 2s) and 3d<sup>9</sup>4f<sup>1</sup>(O 2p<sup>6</sup>) Ce<sup>3+</sup> final states, respectively<sup>18</sup>. The peak at approximately 916.5 eV is used to identify the existence of Ce<sup>4+</sup>, since it is assigned to 4f<sup>0</sup> transitions, which do not occur for Ce<sup>3+</sup><sup>16,17</sup>.

Figure 6 displays the Ce 3d XP-spectra for the following samples: (a) CGd, (b) CGd-0.2Zn, (c) CGd-0.4Zn, (d) CGd-1Zn, and (e) CGd-Co. The addition of 0.2 mol % Zn (Figure 6(b)) caused a small change in the spectrum, noticeable by the appearance of a small contribution at lower binding energy, related to the *v*<sup>0</sup> peak. The additions of higher amounts of Zn provoked an enhancement of this *v*<sup>0</sup> peak (Figures 6(c) and 6(d)). The addition of Co caused even a more noticeable change (Figure 6(e)). These changes in the Ce 3d spectra are attributed to a partial reduction of Ce<sup>4+</sup> to Ce<sup>3+</sup>. It seems that the *v*<sup>0</sup> peak intensity increases with the increase in the amount of Zn. It should be mentioned that a substantial degree of reduction of Ce<sup>4+</sup> to Ce<sup>3+</sup> during XPS measurements can occur when the measurement time is extended to several hours<sup>19</sup>.

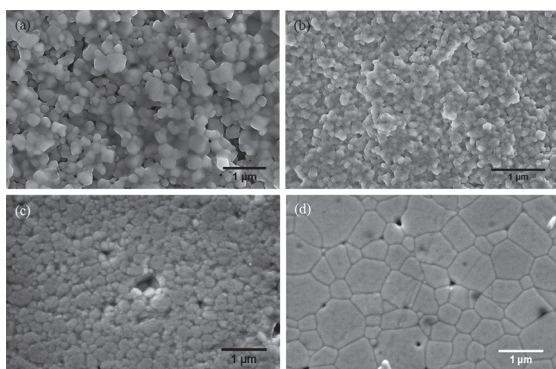
From XPS analyzes, it was possible to identify the chemical changes in cerium ion valence state that occur in CGd samples. The major problem in using doped ceria as electrolyte is the relatively easy reduction of Ce<sup>4+</sup> to Ce<sup>3+</sup> at low oxygen partial pressure and high temperature (typical SOFC anode conditions), which creates an undesirable electronic conduction and leads to a chemical expansion of the lattice parameters. The electronic conduction decreases the fuel conversion efficiency due to partial internal short circuit and the chemical expansion influences the mechanical

**Table 1:** Green, final relative density and average grain size of samples sintered by a two-step method.

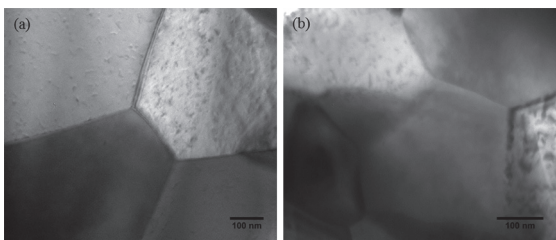
Composition - Peak-Dwell temperature/Time	Green density (%)	Sintered density (%)	Average grain size (nm)
CGd - 1200-1000 °C/10h	57.5	91.8	201±28
CGd-0.4Zn - 1000-900 °C/5h	62.1	93.3	137±13
CGd-0.4Zn - 1200-1000 °C/10h	62.1	96.0	230±12
CGd-Co - 1200-1000 °C/10h	61.1	99.6	450±23



**Figure 3:** XRD diffractograms of the sintered samples.



**Figure 4:** SEM micrographs of the sintered samples: (a) CGd-1200-1000 °C/10h fracture sintered sample, (b) CGd-0.4Zn-1000-900 °C/5h fracture sintered sample, (c) and (d) polished and thermally etched surfaces of CGd-0.4Zn and CGd-Co samples, respectively, sintered at 1200-1000 °C/10h.



**Figure 5:** Dark field TEM micrographs of (a) CGd and (b) CGd-1Zn samples sintered at 1200-1000 °C/10h.

integrity of cells<sup>6</sup>. The addition of either Zn or Co caused a small change in the Ce 3d spectra, indicating only a partial reduction of cerium, however, the impact of these additions on the n-type conductivity of CGd is minimal.

The Gd 4d spectra (not shown here) appear as a broad structure containing two main contributions, Gd 4d<sub>5/2</sub> and Gd 4d<sub>3/2</sub><sup>20</sup>, and are very similar to the one obtained by Cheng *et al.*<sup>21</sup> for a Gd<sub>2</sub>O<sub>3</sub> film deposited on silicon. For all analyzed samples, the binding energy of the Gd 4d<sub>5/2</sub> peak is around 140.7 eV, which is very close to the value (140.9 eV) reported by Kossoy *et al.*<sup>22</sup> for Ce<sub>0.8</sub>Gd<sub>0.2</sub>O<sub>1.9</sub> thin films.

### 3.4 Electrical Conductivity

Figure 7 shows the impedance spectra, measured at 250 °C, of the samples sintered at 1200-1000 °C/10h, corrected for their thickness and electrode area. Impedance spectra of samples containing sintering aids showed the usual characteristics commonly reported for polycrystalline solid electrolytes, with one high frequency arc (ascribed to the bulk contribution), one intermediate frequency arc (related to the grain boundary contribution), besides the lower frequency electrode response often resembling a tail. However, with increasing temperature, the relaxation frequency of the high frequency arc exceeds the upper limit of the equipment, and this arc disappears gradually. The intermediate frequency semicircle displays the same tendency so that at temperatures higher than 500 °C, the impedance spectra showed only the electrode response.

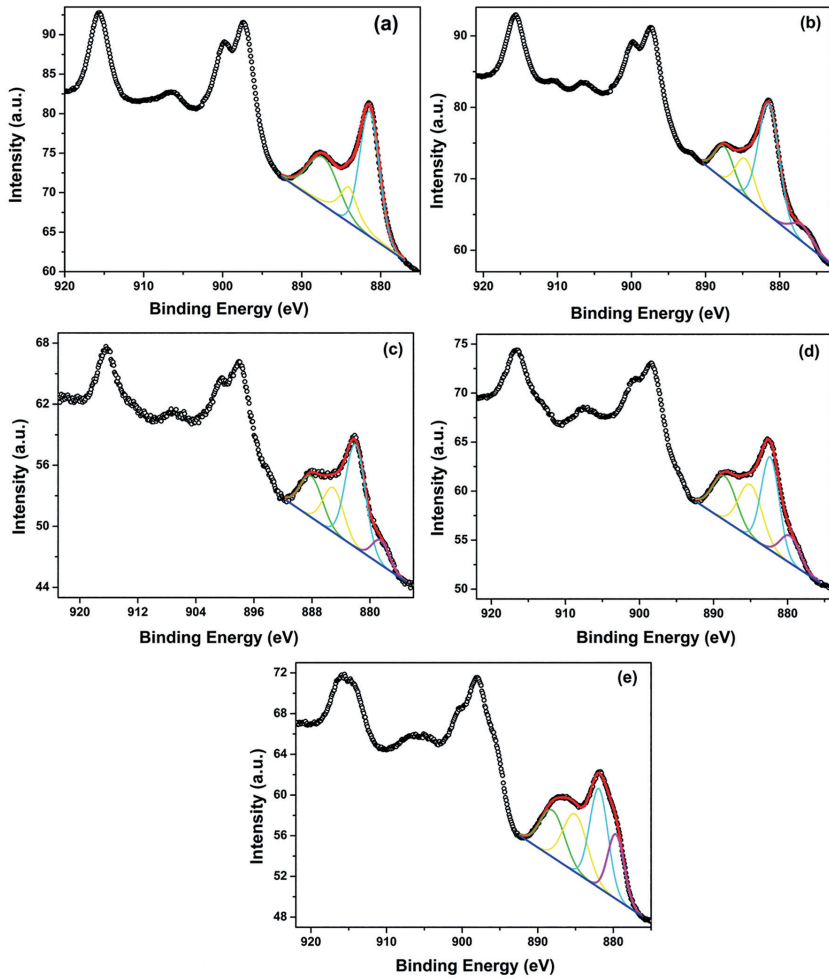
The impedance spectra of samples free of sintering aid sometimes show a higher degree of overlapping of the semi-circles for grain and grain boundary (e.g., see Figure 7) than in the spectra of the doped samples. Instead of well resolved contributions, the result is a depressed impedance arc which can be deconvoluted into specific contributions with the typical relaxation frequencies of grain and grain boundary.

The impedance spectra were fitted by means of the ZView program. Different elementary equivalent circuits arranged in series, each consisting of one resistance (R) and one constant phase element (CPE) in parallel, were adopted as base model. The CPE elements are often used instead of simple capacitors when the impedance data deviates from perfect semicircles, appearing instead as depressed arcs<sup>23</sup>. Each specific contribution (grain, grain boundary, and electrode) was ascribed to one of these elementary circuits, except in the higher temperature range where the arcs related to ionic transport were not well defined. In such cases only the cell total resistance (bulk+grain boundary) was considered.

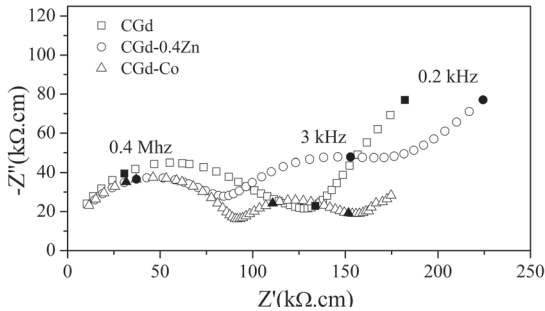
The data shown in Figure 7 suggest that the sintering aids influenced slightly the low temperature performance, but there was no clear trend. Anyhow, even small differences at low temperature quickly vanished with increasing temperature, as it is shown in the following discussion. The bulk ( $\sigma_b$ ) and total ( $\sigma_t$ ) electrical conductivities were calculated from the corresponding (bulk and total=bulk+grain boundary) R values taking into account the sample geometry. The grain boundary conductivity was calculated assuming estimates for the grain boundary thickness and grain size, to calculate the microscopic grain boundary conductivity ( $\sigma_{gb}^{micro}$ ). The  $\sigma_{gb}^{micro}$  can be calculated as usual<sup>24</sup>.

Figure 8 depicts Arrhenius plots of the bulk and microscopic grain boundary electrical conductivities measured in air for specimens sintered 1200-1000 °C/10h. Both bulk and grain boundary conductivities of Zn and Co-doped samples were a little higher than undoped samples, which may be explained by preferential segregation of Zn and Co at grain boundary





**Figure 6:** Ce 3d XPS-spectra for the following samples: (a) CGd, (b) CGd-0.2Zn, (c) CGd-0.4Zn, (d) CGd-1Zn, and (e) CGd-Co.



**Figure 7:** Impedance spectra, measured at 250 °C, of the samples sintered at 1200-1000 °C/10h.

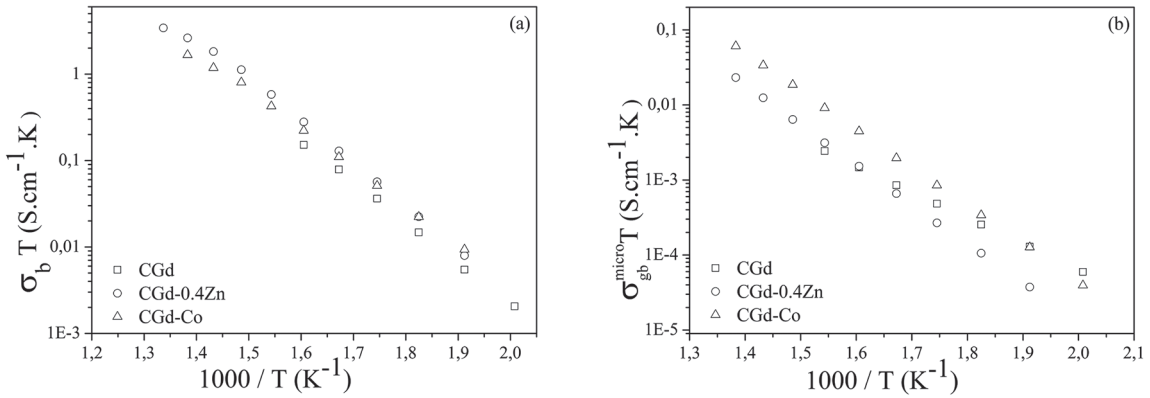
rather than Gd. This behavior affects both bulk and grain boundary electrical properties. In the bulk, the conductivity is higher probably due to the augment of oxygen vacancies with the formation of solid solution among  $Gd_2O_3$  and  $CeO_2$ . The grain boundary is less resistive with sintering aids due to space charge effects, since dopant segregation at

grain boundaries might damage the ionic conductivity. The behavior observed here can be attributed to the influence of sintering aid on the grain boundary thickness ( $\delta_{gb}$ ), as it has been exhaustively discussed for doped-ceria and yttria-stabilized zirconia<sup>23</sup>. The  $\delta_{gb}$  values for Co and Zn-doped and nondoped samples analyzed at 300 °C in air were calculated using equation 2 and are shown in Table 2:

$$\delta_{gb} = \frac{\epsilon_{gb}}{\epsilon_g} \frac{C_g}{C_{gb}} d_g \sim \frac{C_g}{C_{gb}} d_g \quad (2)$$

Where  $\epsilon_{gb}$  and  $\epsilon_g$  are the grain boundary and grain permittivity that were considered equal,  $C_g$  and  $C_{gb}$  are, respectively, the capacitances for grain and grain boundary, and  $d_g$  is the average grain size. The terms  $\epsilon_{gb}$  and  $\epsilon_g$  can be approximately equal since the dielectric constant of  $CeO_2$  is insensitive to the concentration<sup>23</sup>.

The  $\delta_{gb}$  is lower for Co addition than Zn addition, independently of shape, probably indicating that Co and Zn



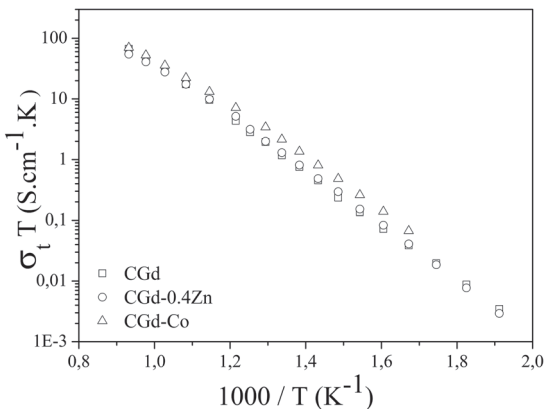
**Figure 8:** Arrhenius plots of (a) bulk and (b) microscopy grain boundary electrical conductivities measured in air of the samples sintered at 1200-1000 °C/10h.

**Table 2:** Activation energies for the bulk ( $E_{ab}$ ) and microscopic grain boundary ( $E_{agb}$ ) conductivities, grain boundary thickness ( $\delta_{gb}$ ) at 300 °C, measured in air, of samples sintered at 1200-1000 °C/10h.

Composition	$E_{ab}$ (eV)		$E_{agb}$ (eV)	$\delta_{gb}$ at 300 °C (nm)
	T < 400 °C	T > 400 °C		
CGd	0.93		0.70	2.79
CGd-0.4Zn	1.00	0.58	1.05	2.17
CGd-Co	0.91	0.67	1.01	1.73

segregate more at the grain boundary than Gd, and this may be correlated to a preferential segregation of the sintering aids rather than the addition of rare earth, and the enhancement of the conductivity may due to change in the space charge layer structure. It is noteworthy that the relative low Co-O bond dissociation and low solubility of cobalt in ceria corroborate with the higher segregation of Co at the grain boundary<sup>12</sup>.

Figure 9 presents the Arrhenius plots of total electrical conductivity ( $\sigma_t$ ) measured in air of the samples sintered at 1200-1000 °C/10h. The differences are relatively small, suggesting that the additions of Co and Zn have little influence on the electrical properties of ceria-based solid solutions. At temperatures higher than 500 °C ( $1000/T \approx 1.3 \text{ K}^{-1}$ ), all lines almost overlap.



**Figure 9:** Arrhenius plots of total electrical conductivity measured in air of the samples sintered at 1200-1000 °C/10h.

The sets of total conductivity data at 800 °C and activation energies are listed in Table 3. The overall conductivity results, including low temperature activation energies in the range 0.8 to 1.0 eV, match the corresponding values for Zn- and Co-free samples. This result suggests that Zn additions have a positive role on the sintering without the formation of ion-blocking grain boundaries, thus resembling Co-doped CGd rather than other ceria-based ceramic materials doped with different sintering aids such as Mn and Fe<sup>9</sup>. The results observed in this work agree well with results reported by Pérez-Coll *et al.*<sup>12</sup> and Ge *et al.*<sup>13</sup>.

## 4. Conclusions

Two-step sintering combined with zinc additions, starting from a nanopowder, successfully produced high density  $\text{Ce}_{0.8}\text{Gd}_{0.2}\text{O}_{1.9}$  samples (>93%) at low peak/dwell temperature ( $T_{\text{peak}} = 1000 \text{ °C}$  and  $T_{\text{dwell}} = 900 \text{ °C}/5\text{h}$ ) without the presence of secondary phases. However, Co additions increased the grain size, while zinc had only a marginal effect on grain growth. Zn and Co additions have a considerable effect on sintering kinetics by improving the densification in comparison with pure CGd samples.

In particular, the chemical states of the constituents were analyzed by XPS and the addition of either Zn or Co caused a change in the Ce 3d spectra, indicating a partial reduction of  $\text{Ce}^{4+}$ . The total conductivity of ceria electrolytes with additives was similar to undoped samples. Zn- and Co-additions had a positive role on sintering without the formation of ion-blocking grain boundaries, since the total conductivities were similar to that of undoped samples.

**Table 3:** Total conductivity ( $\sigma_t$ ) at 800 °C and activation energies for total conductivity ( $E_{at}$ ) in air of sample sintered at 1200-1000 °C/10h.

Composition	$E_{at}$ (eV)		$\sigma_t$ at 800 °C (S/cm) x10 <sup>-2</sup>
	T<600 °C	T>600 °C	
CGd	0.88	0.77	7.2
CGd-0.4Zn	0.91	0.65	6.7
CGd-Co	0.90	0.66	7.5

## 5. Acknowledgements

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