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PAPER

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O P de Sá Neto^{1,2}, M C deOliveira² and G J Milburn³¹ Coordenação de Ciência da Computação, Universidade Estadual do Piauí, CEP: 64202220, Parnaíba, Piauí, Brazil² Instituto de Física 'Gleb Wataghin', Universidade Estadual de Campinas, 13083-970, Campinas, São Paulo, Brazil³ Centre for Engineered Quantum Systems, School of Mathematics and Physics., University of Queensland, QLD 4072, Brisbane, AustraliaE-mail: olimpioqdc@gmail.com

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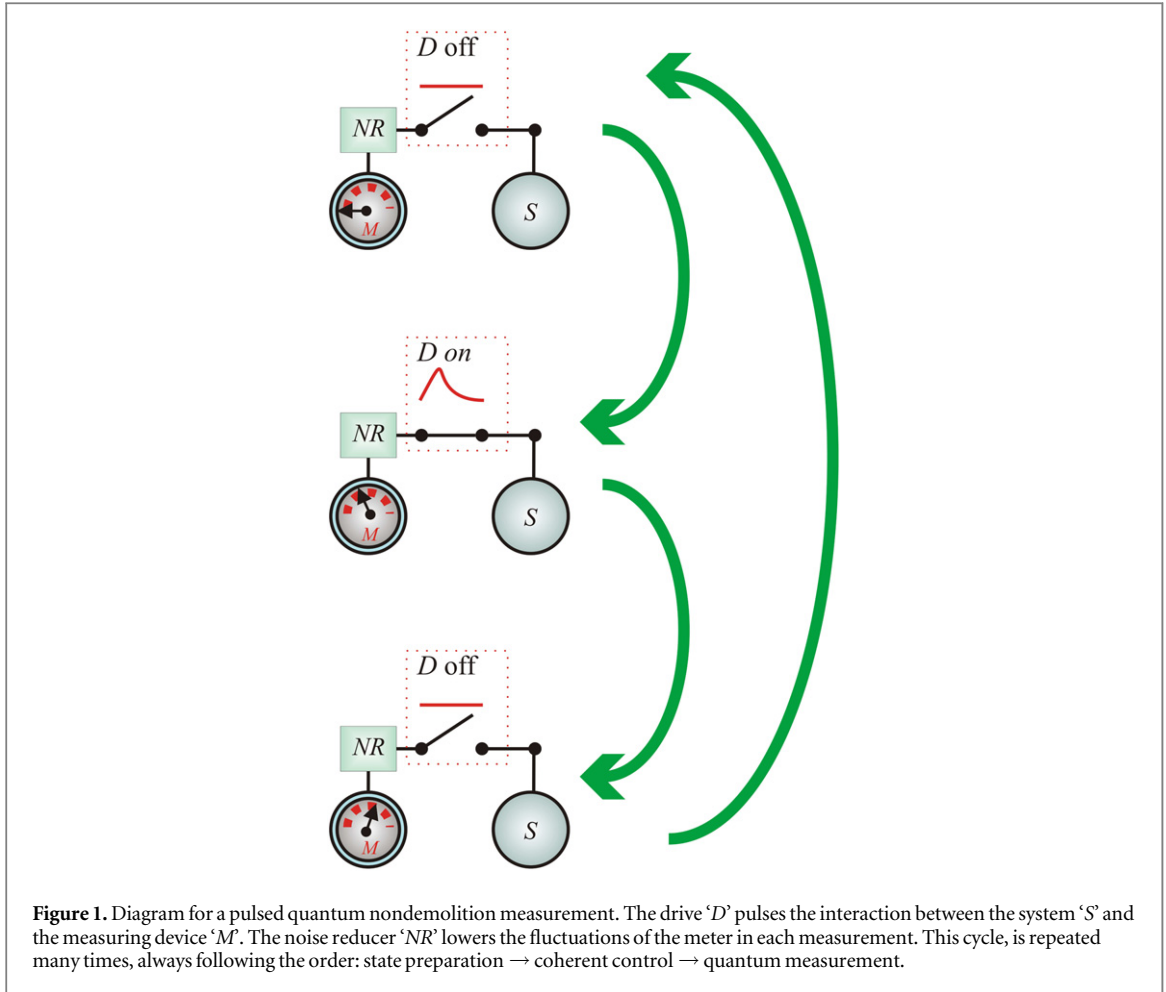
Abstract

Measuring thermodynamic quantities can be easy or not, depending on the system that is being studied. For a macroscopic object, measuring temperatures can be as simple as measuring how much a column of mercury rises when in contact with the object. At the small scale of quantum electromechanical systems, such simple methods are not available and invariably detection processes disturb the system state. Here we propose a method for measuring the temperature on a suspended semiconductor membrane clamped at both ends. In this method, the membrane is mediating a capacitive coupling between two transmission line resonators (TLR). The first TLR has a strong dispersion, that is, its decaying rate is larger than its drive, and its role is to pump in a pulsed way the interaction between the membrane and the second TLR. By averaging the pulsed measurements of the quadrature of the second TLR we show how the temperature of the membrane can be determined. Moreover the statistical description of the state of the membrane, which is directly accessed in this approach is significantly improved by the addition of a Josephson junction coupled to the second TLR.

1. Introduction

Electromechanical systems are devices which couple mechanical displacement and electrostatic interactions. Measuring physical properties of such a device at macroscopic scales is relatively easy—Coulomb in his famous torsion balance attached charged metal spheres to rods and threads and visually measured the torsion produced by the electrostatic interaction between the spheres. The measurement of the torsion allowed him to determine the force acting on the spheres [1, 2]. At the nanoscale however [3], the movement of a nanoelectromechanical system (NEMS) cannot be observed directly. A further complication is that at those scales a quantum description of the system is invariably necessary.

The specific NEMS we are interested in is a suspended semiconductor membrane clamped at both ends, which will be oscillating due to coupling to the thermal modes of the clamps. The smaller is the mechanical element of the NEMS, the stronger is the coupling to the thermal modes of the reservoirs that clamp them at the extremities, and usually some engineered structures must be employed in order to decrease its effects [4]. This oscillator can be coupled electrostatically to other devices, allowing the transduction of the movement as electric signals (see [5] for a general review). Previously schemes to measure the quadrature phase amplitude [6] and to observe the quantum of thermal conductance [7] have been proposed. It is particularly relevant that the detection of the NEMS movement can give direct access to its temperature, a fundamental physical quantity [8, 9]. For the NEMS temperature measurement, usually the area under the noise power spectrum of the displacement amplitude transduced signal is used as it gives directly the mean phonon number in the steady state (see [4, 10] for example). However, one could ask on how to access the temperature of the mechanical resonator by means of a non-demolition detection scheme. Indeed, some previous discussion on non-demolition detection in the assessment of temperature has been given [11, 12]. Also a discussion on back-action-evading



detection and squeezing generation in mechanical resonators through coupling to radiation field were given in [13] as well as the outstanding implementation for movement detection given in [14].

In this work we describe a circuit in which we can perform repeated quantum nondemolition measurement of the expected value of the number of phonons of the NEMS, and show an analysis of the statistics of the number of phonons in this circuit. Through this analysis we show how the temperature of the semiconductor membrane can be directly accessed. Finally, we show that by discretizing the measurement of the expected value we can increase its accuracy in a pulsed linear radiation detection process [15, 16].

In order to perform a measurement on a small oscillator, in a quantum regime [1, 2, 14, 17], a quantum nondemolition measurement is necessary. In this type of measurement, the coupling with the meter is such that it does not disturb the non-demolition observable of interest. Also, because these measurements are probabilistic by nature, it is also important to improve the precision of the meter so that at the end of many measurements there is a significant accuracy in the calculated average. This cyclic sequence of non continuous measurements in time is shown on the diagram of figure 1.

2. Results

We consider the coupling of two transmission line resonators (TLRs) mediated by a mechanical resonator as considered in [18] and represented in figure 2. By assuming the regime of rapid mechanical oscillations at the GHz scale, and that the TLR-1, being in a undepleted regime, is treated classically, the interaction Hamiltonian between the NEMS and the field in the TLR-2 is given by

$$H_I = -\hbar\alpha(t)b^\dagger b(a + a^\dagger), \quad (1)$$

where $\alpha(t)$ is proportional to the microwave amplitude in the TLR-1 [18] and $a(a^\dagger)$ is the annihilation (creation) operator of the normal mode in the TLR-2. $b(b^\dagger)$ is the mechanical resonator annihilation (creation) operator. As one can see in this interaction Hamiltonian the phonon number operator $b^\dagger b$ is a nondemolition variable. In addition the field in this remaining TLR is affected by the presence of a Josephson junction (see figure 2), whose effect (as demonstrated in the appendix) is to induce quadrature

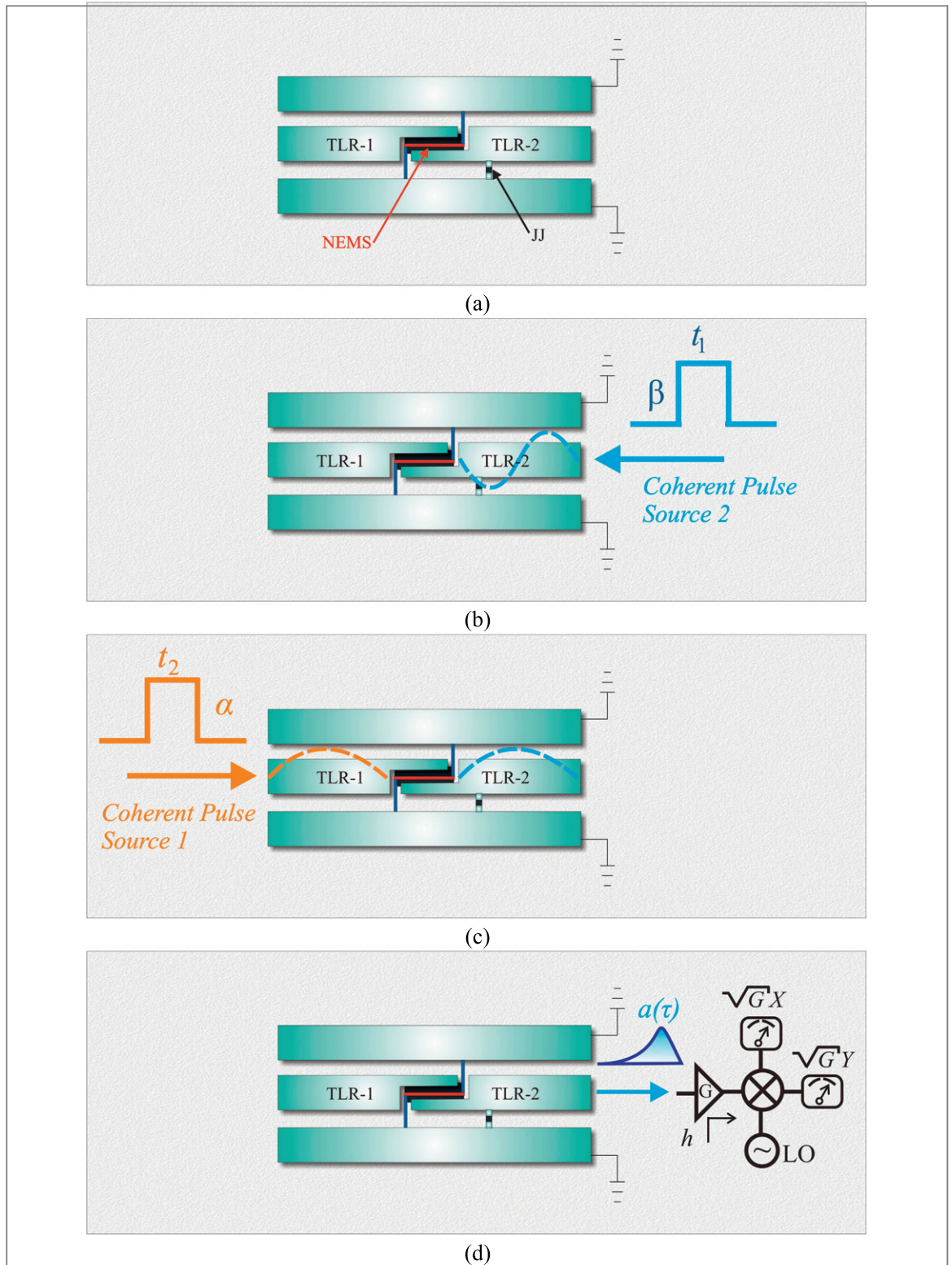


Figure 2. In the proposed experiment, the capacitive coupling between two TLRs is mediated by the vibration of a NEMS. The TLR-2, on the right is directly coupled with a Josephson junction (JJ) for noise reduction. The pulsed measurement sequence is given as follows: (a) *step one*. Initial state preparation $\rho(0)$; (b) *step two*. Application of a pulse in TLR-2 by a coherent pulse source of generating $\rho(t_1)$; (c) *step three*. Application of a pulse in TLR-1 by another coherent pulse source generating $\rho(\tau)$; (d) *step four*. The output of the TLR-2 is directed to a microwave beam splitter (a hybrid). The two outputs are then amplified and run through separate IQ mixers. The four output currents from two IQ mixers can be correlated in various ways. The particular correlation employed here gives access directly to all the normally ordered moments of the cavity field at the start of the measurement. The cross correlations are computed after all the field has been detected and the TLR-2 returned to the vacuum state ready for the next pulse. (Note: the pulse applied in step 3 does not interact with the JJ, for not producing sufficiently large charging energy.)

squeezing [19–25] through a parametric term

$$H_p = -i\hbar \frac{\gamma}{2} (a^2 - a^{\dagger 2}). \quad (2)$$

Without loss of generality we take $\gamma = \beta\chi^{(2)}/2$ as being real and positive, where $\chi^{(2)}$ is the nonlinear susceptibility and β is the amplitude the coherent pulse source in the TLR-2. We shall consider a pulsed measurement scenario [15, 16] where the interaction in H_I is turned on and off rapidly. Note that the unconditional phonon number operator is a quantum non-demolition variable. Moreover given that $[b^\dagger b, H_p + H_I] = 0$, back-action evading is guaranteed and therefore $b^\dagger b$ can be repeatedly measured without the back-action noise [26]. Therefore the phonon number statistics is not changed from pulse to pulse. The detailed process of this pulsed measurement is described in what follows. For a detailed description of the elements involved for linear detection please see [15, 16].

The experiment is carried out according to figure 2. The Josephson junction acts as a source of coherent pulses, with time interval t_1 , on the TLR-2. In sequence, a coherent pulse is applied to TLR-1, with amplitude α_1 and time interval t_2 . The radiation field there is treated classically, as a result of the undepleted regime [18]. After these pulses, the density operator is given by

$$\rho(\tau = t_1 + t_2) = e^{-iH_I t_2/\hbar} e^{-iH_p t_1/\hbar} \rho(0) e^{iH_p t_1/\hbar} e^{iH_I t_2/\hbar}. \quad (3)$$

Initially, the TLR-2 is prepared in a vacuum state, while the NEMS, which oscillates due to thermal excitation, in equilibrium is in a thermal state with mean phonon number N ,

$$\rho(0) = \sum_{n=0}^{\infty} P(n) |n\rangle \langle n|_b \otimes |0\rangle \langle 0|_a, \quad (4)$$

where $P(n) = N^n/(N+1)^{n+1}$ is the thermal phonon number distribution in the NEMS, being $N = (\exp(\hbar\nu/k_B T) - 1)^{-1}$ its thermal number. Given the very short pulses with time intervals $\tau = t_1 + t_2$, the evolution can be approximated as above to give

$$\rho(\tau) = \sum_{n=0}^{\infty} P(n) |n\rangle \langle n|_b \otimes |\alpha_n, \gamma\rangle \langle \alpha_n, \gamma|_a, \quad (5)$$

with $\alpha_n(\tau) = i n \int_0^{t_2} \alpha(t) dt \equiv i n A$, where A is the area of the interaction pulse, and $|\alpha_n, \gamma\rangle_a$ is a coherent squeezed state given by $|\alpha_n, \gamma\rangle_a = \mathcal{D}(\alpha_n) \mathcal{S}(\gamma) |n, 0\rangle$, where $\mathcal{D}(\alpha_n) = \exp[inA(a + a^\dagger)]$ is the displacement operator conditioned on the mechanical resonator phonon excitation number and $\mathcal{S}(\gamma) = \exp[(\gamma t_1/2)(a^{\dagger 2} - a^2)]$ is the squeezing operator.

At the end of a pulse the reduced cavity field state is described by a mixture of squeezed coherent states, which are distributed according to the mechanical resonator thermal phonon number distribution $P(n)$. The field in TLR-2 is dumped out through the dual IQ mixer measurement scheme of [15, 16], detailed in figure 2. In this scheme, the TLR-2 output is directed to a microwave beam splitter (a hybrid coupler). The two outputs are then amplified and run through separate IQ mixers. The four output currents from the IQ mixers can be correlated in various ways after proceeding to linear detectors [15]. One particular cross correlation gives access directly to all the normally ordered moments of the TLR-2 field at the initial time of the measurement. At the end of each pulse a measurement is performed on the output of the second TLR through complex envelopes $S_c = -a(\tau)$ and $S_d = ia(\tau)$. It is important to remark that the criterion for back-action-evasion for $b^\dagger b$, mainly $[b^\dagger b, H_p + H_I] = 0$, is obeyed in every detection step.

These pulsed measurements allow that the cross-correlations be computed after all the field has been detected and the TLR-2 returned to the vacuum state ready for the next pulse. For each individual pulsed measurement the NEMS is to be found on a specific phonon number excitation m according to the thermal distribution $P(m)$. The post-selected state of the TLR-2 field conditioned on this instantaneous (at the time of measurement τ) NEMS excitation m is given by

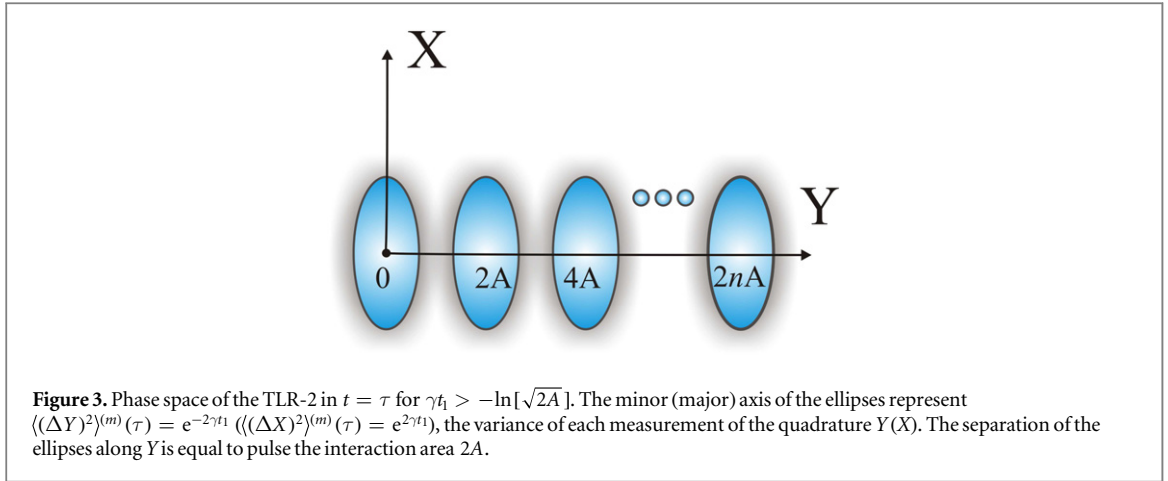
$$\rho_a^{(m)}(\tau) = \frac{\text{Tr}_b \{ \Pi_m \rho(\tau) \Pi_m \}}{\text{Tr}_{ab} \{ \Pi_m \rho(\tau) \Pi_m \}}, \quad (6)$$

where $\Pi_m = |m\rangle \langle m|_b$, $\rho(\tau)$ is given by equation (5), and $\text{Tr}_{ab} \{ \Pi_m \rho(\tau) \Pi_m \} = P(m)$ is the probability to obtain m . Therefore the expected value of the phase quadrature in each measurement

$$\langle Y \rangle_{(m)}(\tau) = \langle \alpha_m, \gamma | Y | \alpha_m, \gamma \rangle, \quad (7)$$

has a variance

$$\langle (\Delta Y)^2 \rangle_{(m)}(\tau) = e^{-2\gamma t_1}. \quad (8)$$



The TLR-2 field pre-selected state $\rho_a(\tau) = \sum_m P(m)\rho_a^{(m)}(\tau)$ average over all the quadrature measurements as $\langle Y \rangle(\tau) = \sum_m P(m)\langle Y \rangle_{(m)}(\tau)$ providing the phonon number (and consequently the temperature) measurement.

The computation of the total variance on Y depends on the variance of the thermal NEMS by adding the variance of each individual measurement, and is dependent on the distinguishability of each individual detection. The squeezing enables the disjunction of the individual conditioned TLR-2 field detections, allowing to attribute the correct excitation m influencing $\rho_a^{(m)}(\tau)$, as depicted in the phase space in figure 3. Therefore the squeezing improves the statistical resolution, being necessary that $\gamma_{t_1} > -\ln[\sqrt{2A}]$ for that to be ensured. The ellipses are centered at $n2A$, $n = 0, 1, 2, \dots$, and their minor and major axes represent the fluctuation of the measurement of each quadrature. Without the squeezing an incorrect attribution could be given to m through the fluctuation $\langle(\Delta Y)^2\rangle_{(m)}(\tau) = e^{-2\gamma_{t_1}}$.

The resulting average over many pulsed measurements is given by the quadratures

$$\langle Y \rangle(\tau) = \text{Tr} \left\{ i(a^\dagger - a)\rho(\tau) \right\} = 2AN \quad (9)$$

and

$$\langle X \rangle(\tau) = \text{Tr} \left\{ (a + a^\dagger)\rho(\tau) \right\} = 0. \quad (10)$$

Therefore, by averaging over many identical pulses we can reconstruct the mean phonon number of the NEMS, N , and thus deduce its temperature, $T = \hbar\nu/[k_B \ln(N^{-1} + 1)]$. In a similar fashion we could also measure two-time correlation functions for the mechanical resonator. Instead here we focus on the quadratures variance and the increasing of accuracy in determining the phonon statistics of the mechanical resonator due to the presence of the squeezing term in equation (2).

Through the pulsed measurement the variance of the quadrature Y is given by

$$\langle(\Delta Y)^2\rangle = 4A^2N(N+1) + \langle(\Delta Y)^2\rangle_{(m)}(\tau), \quad (11)$$

being $\langle(\Delta Y)^2\rangle_{(m)}(\tau)$, the variance of each individual measurement given by equation (8). $N(N+1)$ appearing in equation (11) is the variance of the thermal distribution of the NEMS. The squeezing induced by the Josephson junction allows a reduction of the noise on each measurement, in contrast with the situation without the Josephson junction, for which $\langle(\Delta Y)^2\rangle_{(m)}(\tau) = 1$. In the limit of large squeezing the relative uncertainty $\widetilde{\Delta Y} \equiv \sqrt{\langle(\Delta Y)^2\rangle}/\langle Y \rangle$ is approximately given by

$$\widetilde{\Delta Y} \approx \sqrt{1 + N^{-1}}, \quad (12)$$

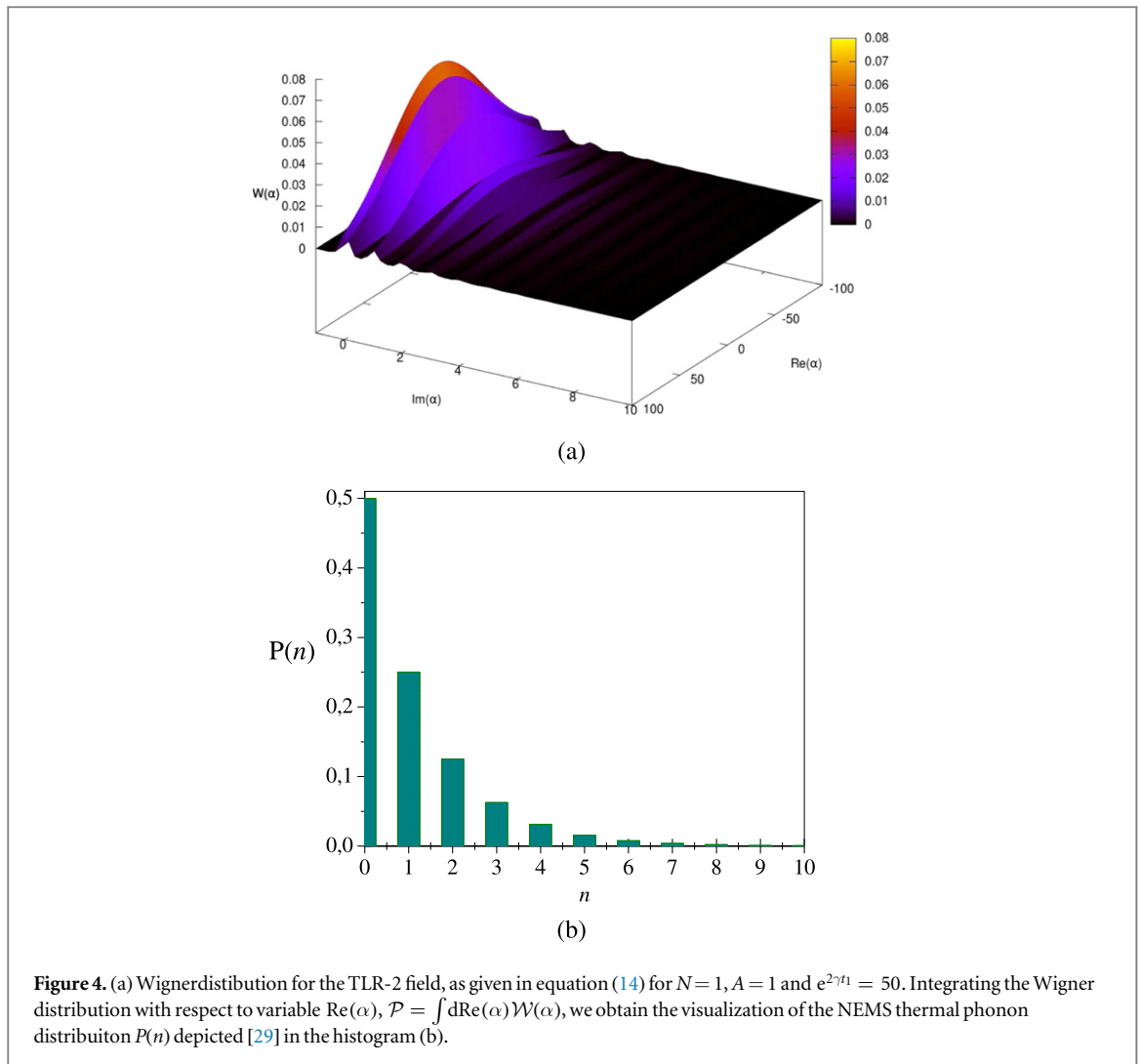
being independent on the pulse area and rapidly reaching the threshold 1 with increasing N .

Extending the previous procedure for measurement of the TLR-2 field ordered moments we can reconstruct the Wigner quasiprobability distribution [27, 28]

$$\mathcal{W}(\alpha) = \sum_{m,n} \int d^2\lambda \frac{\langle (a^\dagger)^n a^m \rangle (-\lambda^*)^m \lambda^n}{\pi^2 n! m!} e^{-\frac{1}{2}|\lambda|^2 + \alpha\lambda^* - \alpha^*\lambda}, \quad (13)$$

for the field state, giving

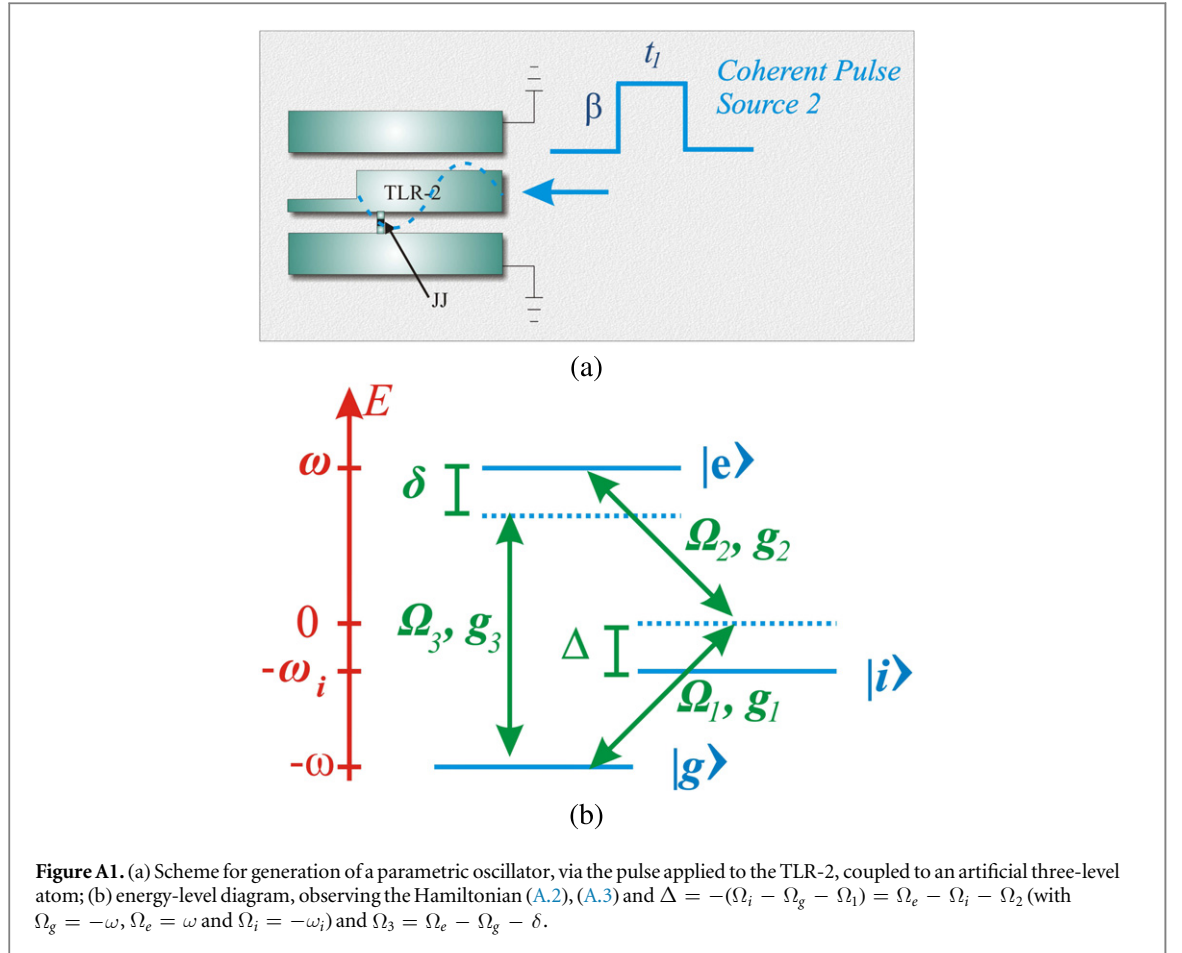
$$\mathcal{W}(\alpha) = \sum_n \frac{P(n)}{2\pi} e^{-\frac{1}{2}\text{Re}^2(\alpha)e^{-2\gamma_{t_1}} - \frac{1}{2}[\text{Im}(\alpha) - \alpha_n]^2 e^{2\gamma_{t_1}}}. \quad (14)$$



The signature of the NEMS phonon distribution $P(n)$ is clearly imprinted in the Wigner distribution profile in figure 4 and can be accessed through the marginal distribution $\mathcal{P} = \int d\text{Re}(\alpha) \mathcal{W}(\alpha)$.

3. Discussion

Detection of thermodynamical quantities associated to nanoscopic movement is important in many aspects. Particularly, the detection of the corresponding temperature of such tiny devices is relevant for physical characterization [8, 9] and latter usage in further applications. Here we have proposed a mechanism to measure the average number of phonons of a NEMS through a pulsed non-demolition detection scheme. Since here the NEMS phonons are due to thermal excitation, a direct way to characterize the temperature of the device as well as its statistical properties in a non-demolition way is derived. The proposed scheme to measure the temperature of the NEMS is experimentally feasible with nowadays technology. The interaction between semiconducting NEMS [1, 2, 7, 17, 30, 31] and superconducting TLR [32–34] has already been carried out [6, 35–38]. Experiments with the IQ mixer measuring method were also performed [16]. Therefore we expect that the presented scheme be readily implemented. The mechanical resonator is assumed to be at thermal equilibrium at the measurement stage, and therefore dissipative effects, which are strong for those devices play a key role for reaching this equilibrium. That is to be reached prior the sequence of pulses of the detection scheme, otherwise it would be expected a continuous decrease of the phonon number, which would be typical in a transient regime. The more relevant dissipative effect comes in fact from the superconducting charge qubit decay time [39] (see [5] for a comprehensive review of some recent experimental numbers). At the frequencies of GHz necessary for the present proposal the charge qubit decay will affect the squeezing of the TLR 2 field, and therefore will affect the accuracy of the detection process. However given the ability to perform short and fast pulses in those devices [15] we do not expect it to be detrimental for the present proposal. A more detailed investigation on that is required.



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Appendix. Derivation of Hamiltonian (2)

We consider the model in figure A1, where the three lowest Josephson junction charge states form a three-level artificial atom is in a configuration where the ground ($|g\rangle$) and excited ($|e\rangle$) states are separated by an intermediary atomic level ($|i\rangle$). The modes with frequency Ω_1 , Ω_2 and Ω_3 are coupled to the transitions $|g\rangle \leftrightarrow |i\rangle$, $|i\rangle \leftrightarrow |e\rangle$ and $|g\rangle \leftrightarrow |e\rangle$ with coupling constants g_1 , g_2 and g_3 , respectively.

The Hamiltonian in the rotating wave approximation is

$$H = H_0 + V, \quad (\text{A.1})$$

being

$$H_0 = \hbar \sum_{j=1}^3 \Omega_j a_j^\dagger a_j + \hbar \Omega_e \sigma_{ee} + \hbar \Omega_i \sigma_{ii} + \hbar \Omega_g \sigma_{gg} \quad (\text{A.2})$$

and

$$V = \hbar \left(g_1 a_1^\dagger \sigma_{ig} + g_2 a_2^\dagger \sigma_{ei} + g_3 a_3^\dagger \sigma_{eg} + \text{h. c.} \right), \quad (\text{A.3})$$

where $\sigma_{jk} = |j\rangle \langle k|$ is the atomic transition for $j, k = g, i, e$. Writing H in the interaction picture, by applying $U_0(t) = e^{-iH_0 t/\hbar}$, and transforming it through $U_1 = e^{-i\Delta t(\sigma_{ee} + \sigma_{gg})}$, we obtain

$$\begin{aligned} \frac{\tilde{H}}{\hbar} = & -\Delta(\sigma_{ee} + \sigma_{gg}) \\ & + g_1 a_1 \sigma_{gi} + g_2 a_2 \sigma_{ie} + g_3 a_3 \sigma_{ge} \\ & + g_1^* a_1^\dagger \sigma_{ig} + g_2^* a_2^\dagger \sigma_{ei} + g_3^* a_3^\dagger \sigma_{eg}. \end{aligned} \quad (\text{A.4})$$

Therefore, the Heisenberg equations of motion for the coherences σ_{gi} and σ_{ie} are

$$i\dot{\sigma}_{ig} = -\Delta\sigma_{ig} + g_1 a_1 (\sigma_{ii} - \sigma_{gg}) + g_3 a_3 \sigma_{ie} - g_2^* a_2^\dagger \sigma_{eg} \quad (\text{A.5})$$

and

$$i\dot{\sigma}_{ie} = -\Delta\sigma_{ie} + g_2^* a_2^\dagger (\sigma_{ii} - \sigma_{ee}) + g_3^* a_3^\dagger \sigma_{ig} - g_1 a_1 \sigma_{ge}. \quad (\text{A.6})$$

Assuming that initially the artificial atom is prepared in the state $|i\rangle$ and that both Δ and δ are large enough so that the states $|e\rangle$ and $|g\rangle$ are not significantly populated so that $\sigma_{ii} = 1$, in the limit where $\Delta \gg |g_1|, |g_2|, |g_3|, \delta$, we have the adiabatic solution with $\dot{\sigma}_{ig} = \dot{\sigma}_{ie} = 0$. Next, the expression of σ_{gi} and σ_{ie} , we can consider $\Delta^2 - g_3^2 a_3^\dagger a_3 \cong \Delta^2$, the terms with $\sigma_{gg}, \sigma_{ee}, \sigma_{ge}$ and σ_{eg} can be neglected, resulting in the solution

$$\sigma_{ig} \cong \frac{g_1}{\Delta} a_1 + \frac{g_2^* g_3}{\Delta^2} a_2^\dagger a_3 \quad (\text{A.7})$$

and

$$\sigma_{ie} \cong \frac{g_2^*}{\Delta} a_2^\dagger + \frac{g_1 g_3^*}{\Delta^2} a_1 a_3^\dagger. \quad (\text{A.8})$$

In this way, preparing the artificial atom in intermediate state $|i\rangle$, and replacing (A.7) and (A.8) expressions in Hamiltonian (A.4), we obtain the effective Hamiltonian of the form

$$\frac{\tilde{H}_{\text{eff}}}{2\hbar} = \frac{g_1^2}{\Delta} a_1^\dagger a_1 + \frac{g_2^2}{\Delta} a_2^\dagger a_2 + \frac{g_1 g_2 g_3^*}{\Delta^2} a_1 a_2 a_3^\dagger + \frac{g_1 g_2 g_3}{\Delta^2} a_1^\dagger a_2^\dagger a_3, \quad (\text{A.9})$$

being g_1 and g_2 real. Now, applying the transformation $U_2 = e^{-it(g_1^2 a_1^\dagger a_1 + g_2^2 a_2^\dagger a_2)}/\Delta$, $a_3 = i\beta$ being a coherent pulse source of amplitude β , and $g_3 \rightarrow \mathcal{G}_3 e^{-i\delta t}$ so that its frequency is adjusted to $\delta = (g_1^2 + g_2^2)/\Delta$, we obtain

$$H_p = -i\hbar \frac{\gamma}{2} (a^2 - a^{\dagger 2}), \quad (\text{A.10})$$

with $a_1 = a_2 = a$, $\Omega_1 = \Omega_2 = \omega$, $\gamma = 4g_1 g_2 \mathcal{G}_3 \beta / \Delta^2$. Note that in this case, the effective frequency is satisfied for $\Omega_3 = 2\omega - (g_1^2 + g_2^2)/\Delta$.

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