

# Spontaneous decay rates in active waveguides

Andrés Anibal Rieznik

*Optics and Photonics Research Center, Instituto de Física Gleb Wataghin, Universidade Estadual de Campinas, cep 13083-970, Campinas, São Paulo, Brazil, and PADTEC, Rodovia Campinas-Mogi-Mirim (SP 340) Km 118.5, cep 13086-902, Campinas, São Paulo, Brazil*

Gustavo Rigolin

*Departamento de Raios Cósmicos e Cronologia, Instituto de Física Gleb Wataghin, Universidade Estadual de Campinas, C.P. 6165, cep 13084-971, Campinas, São Paulo, Brazil*

Received October 4, 2004

We present a new method of measuring the guided, radiated, and total decay rates in uniform waveguides. It is also shown theoretically that large modifications of the total decay rate can be achieved in realistic erbium-doped fiber amplifiers and erbium-doped waveguide amplifiers with effective mode area radii smaller than  $\approx 1 \mu\text{m}$ . © 2005 Optical Society of America

OCIS codes: 060.2410, 230.7370, 250.5300.

It is well known that the spontaneous decay rates (SDRs) of emitting sources such as atoms or quantum wells can be greatly modified in optical microcavities.<sup>1,2</sup> Controlled spontaneous emission plays a key role in a new generation of micro-optic and nano-optic devices. High-performance microcavity lasers, for instance, have been experimentally demonstrated.<sup>3,4</sup> SDR modifications are also expected to affect the performance of optical waveguide amplifiers as the guided mode area radii of these devices become smaller than  $\approx 1 \mu\text{m}$ .<sup>5,6</sup> To characterize one-dimensional nano- and micro-optic devices, a key decomposition of the total decay rate ( $\tau_0^{-1}$ ) into two components was introduced in Refs. 7 and 8. The decay rate was divided into guided modes ( $\tau_g^{-1}$ ) and radiated modes ( $\tau_r^{-1}$ ), where the total decay rate is  $\tau_0^{-1} = \tau_g^{-1} + \tau_r^{-1}$ . Unlike with large devices, where just the total decay rate must be considered for their characterization, the modeling of nano- and micro-optic devices requires the measurement of both components of the decay rate. The usual way to determine the SDR of an emitting source embedded in a uniform waveguide is to measure the exponential decay rate of the amplified spontaneous emission output power when the pump source is switched off.<sup>9</sup> The SDR is given by the exponential decay coefficient of the ASE output power.

Two natural questions arise here: (1) How can  $\tau_g$  and  $\tau_r$  be measured? (2) What is actually measured when one is using the classical method to determine the SDR? In this Letter we answer these two questions. We show that the classical method of measuring  $\tau_0$  in uniform waveguides gives  $\tau_r$  if it is used with long waveguides and actually gives  $\tau_0$  in short waveguides (assuming no reflections at the waveguide ends). We also show how these measures are modified in lossy media, i.e., when a background loss coefficient is incorporated into the rate and propagation equations. Then we show how these ideas are useful for devices of practical interest. Three cases are considered: erbium-doped waveguide amplifiers

(EDWAs), erbium-doped fiber amplifiers (EDFAs), and semiconductor optical amplifiers (SOAs).

We employ an analytical solution for the longitudinal  $z$  dependence of the rate equations presented in Ref. 6 to investigate measurement of the SDR in uniform waveguides. The analytical solution presented there is valid only for waveguides in which the excited-state population of the emitting source,  $N_2(z)$ , is constant along the fiber. Since the decay rate is measured when  $N_2 \rightarrow 0$  along  $z$ , this approximation is valid when one is measuring  $\tau_0$ . The rate equation is<sup>5</sup>

$$\frac{\partial N_2(z,t)}{\partial t} = -\frac{N_2(z,t)}{\tau_0} - \frac{1}{\rho S} \sum_{n=1}^M \{[(\alpha_n + \gamma_n) \times N_2(z,t) - \alpha_n] P_n(z,t)\}, \quad (1)$$

where  $N_1 + N_2 = 1$  are the normalized population of the upper and lower levels of the emitting source,  $\tau_0$  is the spontaneous lifetime of the upper level,  $\rho$  is the number density of active ions,  $S$  is the doped region area, and  $\alpha_n$  and  $\gamma_n$  are the absorption and gain constants. The propagation equation is

$$\frac{\partial P_n(z,t)}{\partial z} = u_n \{[(\alpha_n + \gamma_n) N_2(z,t) - \alpha_n - \alpha_{\text{loss}}] \times P_n(z,t) + 2\gamma_n \Delta\nu N_2(z,t)\}, \quad (2)$$

where  $P_n(z,t)$  is the optical power (in photons per unit time) at location  $z$  of the  $n$ th beam with the wavelength centered at  $\lambda_n$  ( $n \leq M$ ),  $u_n = 1$  for forward-traveling beams and  $u_n = -1$  for backward-traveling beams,  $\alpha_{\text{loss}}$  is the attenuation coefficient given by the background loss of the fiber glass host,  $\Delta\nu$  is the frequency interval between two successive wavelengths considered in the model, and the factor 2 in the last term stands for two possible polarizations. Solving Eqs. (1) and (2) for  $N_2(z,t) = N_2(t)$ , i.e.,  $N_2$  constant along  $z$ , the output power is<sup>6</sup>

$$P_n^{\text{out}}(t) = P_n^{\text{in}}(t)G_n(t) + 2\mathcal{N}_n^{\text{sp}}\Delta\nu[G_n(t) - 1], \quad (3)$$

where

$$G_n(t) = \exp[(\alpha_n + \gamma_n)\mathcal{N}_2(t)L - (\alpha_n - \alpha_{\text{loss}})L], \quad (4)$$

$$\mathcal{N}_n^{\text{sp}} = \frac{\gamma_n\mathcal{N}_2(t)}{(\alpha_n + \gamma_n)\mathcal{N}_2(t) - \alpha_n - \alpha_{\text{loss}}}. \quad (5)$$

The rate equation is

$$\begin{aligned} \frac{d\mathcal{N}_2(t)}{dt} = & -\frac{\mathcal{N}_2(t)}{\tau_0} - \frac{1}{\rho SL} \sum_{n=1}^M [P_n^{\text{out}}(t) - P_n^{\text{in}}(t) \\ & - 2\gamma_n\Delta\nu\mathcal{N}_2(t)L + \alpha_{\text{loss}}H_n(t)L], \end{aligned} \quad (6)$$

where

$$\begin{aligned} H_n(t) = & \frac{P_n^{\text{in}}(t)}{\ln[G_n(t)]} [G_n(t) - 1] + 2\mathcal{N}_n^{\text{sp}}\Delta\nu \\ & \times \left\{ \frac{G_n(t) - 1}{\ln[G_n(t)]} - 1 \right\}. \end{aligned} \quad (7)$$

Here  $P_n^{\text{out}}(t) = P_n(L, t)$  and  $P_n^{\text{in}}(t) = P_n(0, t)$  are the output and input powers of the  $n$ th beam, respectively;  $G_n(t)$  is the linear gain;  $\mathcal{N}_n^{\text{sp}}$  is the spontaneous-emission factor for the  $n$ th mode; and  $L$  is the doped fiber length.

In the classical method<sup>7</sup> of determining the SDR, the input power is turned off [ $P_n^{\text{in}}(t) = 0$ ] and the useful data are collected when the concentration of excited ions is low ( $\mathcal{N}_2 \ll 1$ ). With these two conditions Eqs. (3) and (7) become

$$P_n^{\text{out}}(t) = \frac{2\gamma_n\Delta\nu\mathcal{N}_2(t)}{\alpha_n + \alpha_{\text{loss}}} \{1 - \exp[-(\alpha_n + \alpha_{\text{loss}})L]\}, \quad (8)$$

$$H_n(t) = -\frac{P_n^{\text{out}}(t)}{L(\alpha_n + \alpha_{\text{loss}})} + \frac{2\gamma_n\Delta\nu\mathcal{N}_2(t)}{\alpha_n + \alpha_{\text{loss}}}. \quad (9)$$

Using Eq. (9), we can rewrite Eq. (6) as

$$\begin{aligned} \frac{d\mathcal{N}_2(t)}{dt} = & -\frac{\mathcal{N}_2(t)}{\tau_0} - \sum_{n=1}^M \left\{ \frac{P_n^{\text{out}}(t)}{\rho SL} - \frac{2\gamma_n\Delta\nu\mathcal{N}_2(t)}{\rho S} \right. \\ & \left. - \beta_n \left[ \frac{P_n^{\text{out}}(t)}{\rho SL} - \frac{2\gamma_n\Delta\nu\mathcal{N}_2(t)}{\rho S} \right] \right\}, \end{aligned} \quad (10)$$

where we introduce the effective background loss coefficient for the  $n$ th mode  $\beta_n = \alpha_{\text{loss}}/(\alpha_n + \alpha_{\text{loss}})$ . Looking at Eq. (8), which is linear in  $\mathcal{N}_2(t)$ , we see that the right-hand side of Eq. (10) is also linear in  $\mathcal{N}_2(t)$ . Therefore it can be rewritten as  $d\mathcal{N}_2(t)/dt = -\mathcal{N}_2(t)/\tau_m$ , where  $\tau_m$  is what is actually measured by the classical method and not  $\tau_0$ . Since  $\tau_m$  is quite cumbersome, we do not explicitly write it here. But two limiting cases deserve detailed study. Case 1 is short waveguides. In this case  $(\alpha_n + \alpha_{\text{loss}})L \ll 1$ . With this approximation Eq. (10) reduces to

$$\frac{d\mathcal{N}_2(t)}{dt} = -\frac{\mathcal{N}_2(t)}{\tau_0}. \quad (11)$$

This result shows that only for short waveguides does the classical method<sup>7</sup> furnish the total SDR of the ion. It is interesting to note that Eq. (11) is valid whether or not we have background loss ( $\alpha_{\text{loss}} \neq 0$ ). Case 2 is long waveguides. Here  $(\alpha_n + \alpha_{\text{loss}})L \gg 1$ . Now Eq. (10) becomes

$$\frac{d\mathcal{N}_2(t)}{dt} = -\frac{\mathcal{N}_2(t)}{\tau_r} - \sum_{n=1}^M \beta_n \frac{\mathcal{N}_2(t)}{\tau_{g_n}}, \quad (12)$$

where we use the decomposition<sup>7,8</sup> of  $\tau_0^{-1}$  in guided and radiated modes ( $\tau_0^{-1} = \tau_g^{-1} + \tau_r^{-1}$ ) and the fact that  $\tau_g^{-1} = \sum_{i=1}^M \tau_{g_n}^{-1}$ , where  $\tau_{g_n}^{-1} = 2\gamma_n\Delta\nu/\rho S$  is the guided decay rate into the  $n$ th mode. For sufficiently low background loss  $\beta_n \approx 0$ , which implies that the classical method now furnishes  $\tau_r^{-1}$ .

The fact that  $\tau_g^{-1}$  in a given mode can be written as  $\tau_{g_n}^{-1} = 2\gamma_n\Delta\nu/\rho S$  is pointed out here for what is to our knowledge the first time. It arises naturally from the interpretation given in Ref. 6 for this term as being the photons captured by the guided modes per unit time. Unlike in Refs. 7 and 8, in which  $\tau_g^{-1}$  was given as a function of the dipole moment matrix element between the emitting source's excited and ground states, here we use the easily measurable gain constant  $\gamma_n$ .

Therefore the total ( $\tau_0^{-1}$ ) and the radiated ( $\tau_r^{-1}$ ) decay rates in a given uniform waveguide can, in principle, be measured separately by employing two different waveguide lengths.  $\tau_g^{-1}$  can also be determined by simply subtracting the latter from the former ( $\tau_g^{-1} = \tau_0^{-1} - \tau_r^{-1}$ ). In any case,  $\tau_g^{-1}$  is also easily obtained from the waveguide's intrinsic parameters, as discussed in the previous paragraph. We observe that in Subsection 2.B.3 of Ref. 5 the results presented above were outlined for  $\alpha_{\text{loss}} = 0$ . But here we explicitly perform the calculations and reinterpret these results in light of the decomposition of the decay rate into guided and radiated modes.

We end by studying the range of waveguide lengths at which  $\tau_0^{-1}$  and  $\tau_r^{-1}$  can be measured. We use three sets of parameters of practical interest. They represent typical EDFAs, EDWAs, and SOAs. It is worth mentioning that the term proportional to  $\mathcal{N}_2^2$ , which is usually included in modeling EDWAs and SOAs, can be neglected since  $\mathcal{N}_2 \ll 1$ .

In usual EDFAs and EDWAs, with optical mode areas larger than  $\approx 1 \mu\text{m}^2$ ,  $\tau_g^{-1}$  is negligible and the total lifetime is equal to the radiated lifetime ( $\tau_0 \approx \tau_r \approx 10$  ms). However, when the optical mode area becomes smaller,  $\tau_g^{-1}$  starts to have a nonnegligible and measurable value. For instance, using the parameters shown in Table 1, a  $1\text{-}\mu\text{m}$  optical mode radius, and Eq. (10), we determine the measured lifetime as a function of the waveguide length for typical EDFAs and EDWAs (assuming perfect detection). Without loss of generality, we use an effective gain and ab-

sorption constant along the total transition bandwidth of  $\approx 15$  THz centered at  $1.55 \mu\text{m}$ . We can observe from Fig. 1 that a  $1\text{-}\mu\text{m}$  optical mode radius is small enough to cause a variation of  $\approx 5\%$  between the total and the radiated lifetimes, measured at small and large waveguide lengths, respectively. Although small, an optical mode radius of  $\approx 1 \mu\text{m}$  is already commercially available in photonic crystal fibers. Moreover, it has been shown that waveguides with a high index contrast (and, consequently, small mode areas) have several advantages,<sup>12</sup> which envisages future construction of very small mode area devices. To study how the total and radiated decay rates can be measured in such devices, we perform simulations assuming the values shown in Table 1 for an EDWA but with an optical mode area of  $0.02 \mu\text{m}^2$ , which was obtained, for instance, in Ref. 3. The results are shown in Fig. 2. Of course, such highly confined EDWAs would use materials that would not necessarily have the parameters shown in Table 1. But Fig. 2 illustrates the effects that would always occur at smaller mode areas: the difference between the total and the radiated lifetimes increases (as a consequence of larger  $\tau_g^{-1}$ ), the difference between the decay rates in lossy and nonlossy waveguides increases, and, at last, the waveguide lengths that are

**Table 1. Parameters Used in the Simulations**

Parameter	$\gamma_{\text{eff}}$ ( $\text{m}^{-1}$ )	$\alpha_{\text{eff}}$ ( $\text{m}^{-1}$ )	$\tau_r$ (ms)	$\rho$ ( $\text{m}^{-3}$ )
EDFA <sup>6</sup>	0.2	0.2	10	$1.0 \times 10^{24}$
EDWA <sup>10</sup>	20	49	22	$1.4 \times 10^{26}$

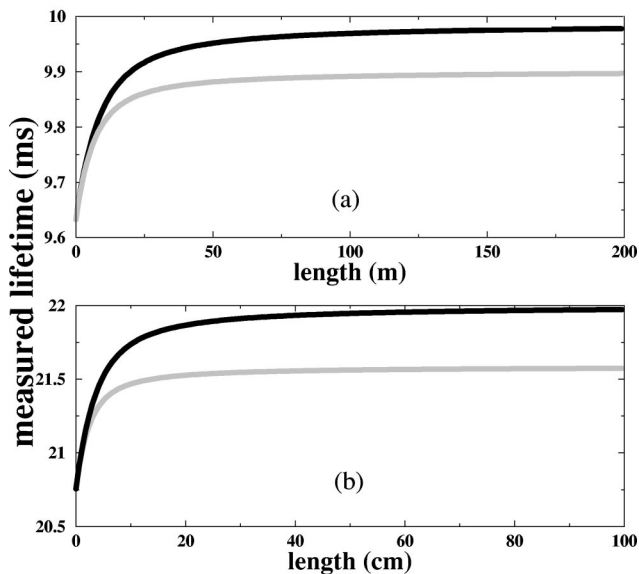


Fig. 1. Simulations of the measured lifetimes as a function of the waveguide length for typical (a) EDFAs and (b) EDWAs. Black curves, nonlossy waveguides; gray curves,  $\alpha_{\text{loss}} = 0.3$  dB/m (EDFAs) (Ref. 11) and  $1$  dB/cm (EDWAs),<sup>10</sup> values typical of fluorozirconate EDFAs and silica-based EDWAs, respectively.

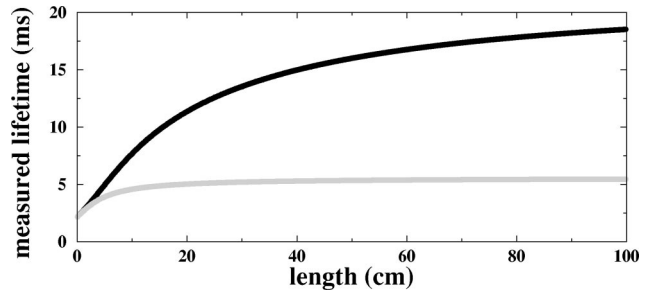


Fig. 2. Theoretical lifetimes as a function of the waveguide length for an EDWA with a  $0.02\text{-}\mu\text{m}^2$  optical mode area. Other parameters are given in Table 1.

necessary to obtain the radiated lifetime with a given accuracy also increase.

In SOAs the condition  $\mathcal{N}_2 + \mathcal{N}_1 = 1$  does not hold, but it is easy to show that the method of measuring the radiated and the total lifetime presented here also works. We observe that  $\gamma_n$  can be written as  $\sigma_n^e \Gamma \rho / S$ , where  $\sigma_n^e$  is the emission cross section at wavelength  $\lambda_n$  and  $\Gamma$  is the overlap factor between the optical mode and the doped region area.<sup>13</sup> Then,  $\tau_g^{-1}$  is given by  $\tau_g^{-1} = 2\sigma_n^e \Gamma / S$ . Using  $\sigma_n^e \Gamma = 2.0 \times 10^{-16} \text{cm}^2$  for a typical SOA,<sup>14</sup> we found that  $\tau_g^{-1}$  becomes comparable with  $\tau_r^{-1}$  of  $\approx (200 \text{ ps})^{-1}$  only at an optical mode radius smaller than  $\approx 1 \text{ nm}$ , which is far from possible with present technologies.

G. Rigolin thanks the Fundação de Amparo à Pesquisa do Estado de São Paulo for funding this research. A. A. Rieznik's e-mail address is anibal@ifi.unicamp.br.

## References

1. D. Kleppner, *Phys. Rev. Lett.* **47**, 233 (1981).
2. S. D. Brorson, H. Yokoyama, and E. P. Ippen, *IEEE J. Quantum Electron.* **26**, 1492 (1990).
3. H. Yokoyama, *Science* **256**, 5053 (1992).
4. J. P. Zhang, D. Y. Chu, S. L. Wu, S. T. Ho, W. G. Bi, C. W. Tu, and R. C. Tiberio, *Phys. Rev. Lett.* **75**, 2678 (1995).
5. T. Sondergaard and B. Tromborg, *Phys. Rev. A* **64**, 033812 (2001).
6. A. A. Rieznik and H. L. Fragnito, *J. Opt. Soc. Am. B* **21**, 1732 (2004).
7. D. Y. Chu and S.-T. Ho, *J. Opt. Soc. Am. B* **10**, 381 (1993).
8. H. Yokoyama and S. D. Brorson, *J. Appl. Phys.* **66**, 4801 (1989).
9. E. Desurvire, *Device and System Applications* (Wiley, New York, 1994), Sect. 4.6.
10. E. Snoeks, G. N. van den Hoven, and A. Polman, *IEEE J. Quantum Electron.* **32**, 1680 (1996).
11. T. Georges and E. Delevaque, *Opt. Lett.* **17**, 1113 (1992).
12. S. Saini, J. Michel, and L. C. Kimerling, *J. Lightwave Technol.* **21**, 2368 (2003).
13. C. R. Giles and E. Desurvire, *J. Lightwave Technol.* **9**, 271 (1991).
14. G. P. Agrawal, *Fiber-Optics Communication Systems* (Wiley, New York, 1992), p. 95.