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# A study of the aftereffect of the magnetic permeability in Co-rich amorphous ferromagnetic alloys

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Room-temperature measurements of saturation magnetization, saturation magnetostriction, and aftereffect of the magnetic permeability have been performed on a set of Co-based amorphous ferromagnetic alloys with magnetostriction values in the range  $-4 \times 10^{-6} \leq \lambda_s \leq +1 \times 10^{-6}$ . The theoretical relation between aftereffect and  $\lambda_s$  has been verified to hold also in Co-rich amorphous alloys. The fraction of atoms participating in the ordering processes giving rise to the aftereffect is calculated to be of the order  $10^{-4}$ . The aftereffect is shown to be related, even in these alloys, to a damping of  $180^\circ$  Bloch walls, whose thickness increases with decreasing  $\lambda_s$ . The influence of the alloy's stability on the permeability aftereffect is discussed in detail.

## I. INTRODUCTION

The aftereffect of the initial magnetic permeability of Fe-rich amorphous ferromagnetic alloys is proportional at room temperature to the square of the saturation magnetostriction of the material.<sup>1</sup> This result has been explained by invoking the directional ordering of structural defects, interacting with the direction of the magnetization  $I_s$  through a magnetoelastic coupling.

A first version of the theory<sup>1</sup> predicts that the permeability aftereffect  $\Delta\mu/\mu$  is directly proportional to  $\lambda_s^2$ , in full agreement with the experimental results for Fe-based alloys. Rather strong magnetic aftereffects were, however, also observed in near zero-magnetostriction, Co-rich amorphous alloys.<sup>2,3</sup> The apparent contradiction between these findings and the predictions of the magnetostrictive theory has been solved by analyzing the problem from two different viewpoints. A deeper analysis of the effect of structural distortions on the local magnetoelastic energy leads one to predict a functional dependence of the type  $\Delta\mu/\mu = A + B\lambda_s^2$  for the permeability aftereffect,<sup>4</sup> consequently accounting in a natural way for the effects observed in zero  $\lambda_s$  alloys. On the other hand, additional contributions to the coupling energy between defects and magnetization have been investigated by Kronmüller *et al.*,<sup>3,5</sup> who pointed out that both the spin orbit and the exchange energy may be considered as possible sources of the aftereffect. A law of the type  $\Delta\mu/\mu = A + B\lambda_s^2$  is derived also in this second case. Obviously, the parameters  $A$  and  $B$  are defined differently in each model. Quite unfortunately, they depend on various factors, which are sometimes not directly measurable, e.g., the number of defects responsible for the aftereffect at a given temperature. As a consequence, no quantitative comparison between the predictions of these competing models has been attempted so far.

Although the aftereffect of the magnetic permeability

has been investigated in several Fe-based alloys, relatively few data for magnetostrictive, Co-rich alloys are available, since most of the measurements were specifically concerned with zero-magnetostriction ribbons.<sup>2,3,6</sup> In this paper a complete set of Co-based alloys (with  $\lambda_s$  continuously ranging from negative to positive values) is studied for the first time, in order to check experimentally the validity of the expression  $\Delta\mu/\mu = A + B\lambda_s^2$  in these materials. The analysis of the behavior of the magnetic aftereffect with  $\lambda_s$  is helpful in determining the values of some physical parameters appearing in the theoretical expressions for  $\Delta\mu/\mu$ . A better knowledge of these factors could, in turn, allow one to verify if the existing approaches to the problem are based on reasonable assumptions.

## II. MEASUREMENTS AND RESULTS

Room-temperature measurements of saturation magnetization, saturation magnetostriction, and low-field permeability aftereffect were performed on as-cast ribbons of composition  $\text{Co}_{75}\text{Si}_5\text{B}_{20}$ ,  $\text{Co}_{75-x}\text{Fe}_x\text{Si}_{15}\text{B}_{10}$  ( $0 < x < 6$ ),  $\text{Co}_{72}\text{Mn}_8\text{B}_{20}$ ,  $\text{Co}_{73}\text{B}_{27}$ , and  $\text{Co}_{61}\text{Fe}_8\text{Ni}_{18}\text{Cr}_{3.2}\text{Cu}_2\text{B}_3\text{Si}_{4.8}$ . The ribbons of the  $\text{Co}_{75-x}\text{Fe}_x\text{Si}_{15}\text{B}_{10}$  alloy series were prepared at USP, São Paulo, Brazil.<sup>7</sup>

The saturation magnetization was measured by means of a vibrating sample magnetometer. The saturation magnetostriction was determined by using a small-angle rotation technique.<sup>8</sup> Both measurements were performed at UNICAMP, Campinas, Brazil. The aftereffect of the magnetic permeability was measured on similar samples at IENGF, Turin, Italy, by making use of an impulsive technique suitable to analyze the permeability decay from about  $10^{-2}$  s after a sudden change of the domain structure of the sample.<sup>9</sup>  $\Delta\mu/\mu \equiv \Delta B/B$  was measured at  $B_M$  at which  $\Delta B$  shows a maximum in the  $\Delta B$  vs  $B$  curve.<sup>1</sup> Examples of such a curve, for selected materials, are shown in Fig. 1.

The crystallization temperature of three samples

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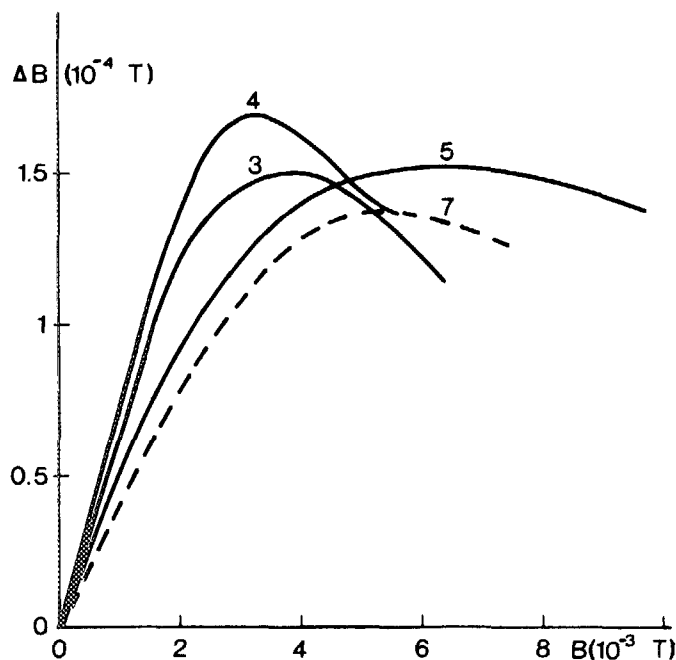


FIG. 1. Behavior of the magnetic aftereffect ( $\Delta B$ ) as a function of induction  $B$  in selected Co-rich amorphous alloys. Numbers refer to Table I. Full lines: negative magnetostriction; dashed line: positive magnetostriction.

( $\text{Co}_{73}\text{B}_{27}$ ,  $\text{Co}_{75}\text{Si}_5\text{B}_{20}$ ,  $\text{Co}_{75}\text{Si}_{15}\text{B}_{10}$ ) was determined by a conventional DSC technique with a heating rate of 30 K/min.

The values of the saturation magnetization and of the permeability aftereffect of the considered alloys are reported in Table I, where the aftereffect is expressed, as usual,<sup>4,10</sup> in the more convenient form  $\Delta\mu/\mu \times H_e \times I_s$ ,  $H_e$  being the value of the external field. The behavior of the aftereffect as a function of  $\lambda_s$  is shown in Fig. 2 (dots). Although some scattering is present, the experimental data are well repre-

sented by the quadratic law  $\Delta\mu/\mu \times H_e \times I_s = a + b \times \lambda_s^2$ , with  $a = 5.67 \times 10^{-2}$  and  $b = 1.05 \times 10^{10} \text{ J/m}^3$  (dashed line in Fig. 2). This result confirms the validity of the theoretical predictions also for these Co-based alloys, as far as the functional dependence of  $\Delta\mu/\mu$  on  $\lambda_s$  is concerned. The position of the maximum of the  $\Delta B$  vs  $B$  curve ( $B_M$ ) for the  $\text{Co}_{75-x}\text{Fe}_x\text{Si}_{15}\text{B}_{10}$  alloy series is reported in Fig. 3 as a function of  $\lambda_s$ .  $B_M$  is found to increase with decreasing magnetostriction (in absolute value).

### III. DISCUSSION

#### A. Dependence of the aftereffect on the alloy's magnetostriction

The expression of the magnetic aftereffect of magnetostrictive nature is, in the light of the more recent calculations,<sup>4</sup>

$$\frac{\Delta\mu}{\mu} H_e I_s = 2.55 \frac{3}{32} \frac{N_T}{kT} [G(t_1) - G(t_2)] \lambda_{\text{eff}}^2 \langle \tau^2 \rangle, \quad (1)$$

where  $N_T$  is the total number (per cubic meter) of atoms present in structural defects ordering at the temperature  $T$ ,  $G(t)$  is a monotonically decreasing function time,<sup>1</sup>  $t_1$  and  $t_2$  are the fixed limits of the time interval chosen to measure the aftereffect, and  $\langle \tau^2 \rangle$  is the second moment of the shear-stress fluctuations according to the definition proposed by Egami *et al.*<sup>11</sup> The "effective" magnetostriction  $\lambda_{\text{eff}}$  is defined as

$$\lambda_{\text{eff}}^2 = (1/25) [8\pi\lambda_s^2 + (1/2\pi)\langle m \rangle \lambda_g^2], \quad (2)$$

where  $\lambda_s$  is the saturation magnetostriction, and the constant  $\lambda_g$ , related to  $\lambda_s$ , is expressed in terms of a particular combination of the local anisotropy energy and its space derivative, as discussed elsewhere.<sup>4</sup> Finally,  $\langle m \rangle$  is the average value of a bond-orientational order parameter describing the degree of distortion of elementary cells in a metallic glass.<sup>12</sup>

The measurable parameters appearing in the right-hand side of Eq. (1) are  $T$ ,  $G(t_{1,2})$ , and  $\lambda_s$ . Both  $\langle \tau^2 \rangle$  and  $\langle m \rangle$

TABLE I. Saturation magnetostriction and permeability aftereffect values for the studied Co-rich alloys (Nos. 1–9). Representative data for Fe-based alloys (Nos. 10–15) are reported for comparison.

No.	Material (nominal composition)	$\lambda_s$ ( $10^{-6}$ )	$(\Delta\mu/\mu)H_e \times I_s$ ( $10^{-1} \text{ J/m}^3$ )
1	$\text{Co}_{73}\text{B}_{27}$	-3.7	2.96
2	$\text{Co}_{75}\text{Si}_5\text{B}_{20}$	-3.9	2.15
3	$\text{Co}_{75}\text{Si}_{15}\text{B}_{10}$	-3.7	1.05
4	$\text{Co}_{73}\text{Fe}_2\text{Si}_{15}\text{B}_{10}$	-2.7	1.08
5	$\text{Co}_{71}\text{Fe}_4\text{Si}_{15}\text{B}_{10}$	-0.6	0.49
6	$\text{Co}_{70.4}\text{Fe}_{4.6}\text{Si}_{15}\text{B}_{10}$	+0.2	0.27
7	$\text{Co}_{69}\text{Fe}_6\text{Si}_{15}\text{B}_{10}$	+1.0	0.67
8	$\text{Co}_{72}\text{Mn}_8\text{B}_{20}$	-2.5	1.60
9	$\text{Fe}_{7.9}\text{Co}_{61.1}\text{Ni}_{18.1}\text{Cr}_{3.2}\text{Cu}_2\text{B}_{3.1}\text{Si}_{4.6}$	+0.4	0.97
10	$\text{Fe}_{29}\text{Ni}_{49}\text{P}_{14}\text{B}_6\text{Si}_2^a$	4.3	0.09
11	$\text{Fe}_{40}\text{Ni}_{40}\text{P}_{14}\text{B}_6^a$	8.7	0.41
12	$\text{Fe}_{80.8}\text{Cr}_5\text{B}_{14.2}^a$	14.4	1.34
13	$\text{Fe}_{75}\text{Cr}_{4.8}\text{B}_{20.2}^a$	14.8	2.00
14	$\text{Fe}_{80}\text{W}_3\text{B}_{17}^a$	15.9	2.17
15	$\text{Fe}_{40}\text{Ni}_{38}\text{Mo}_4\text{B}_{18}^a$	16.1	1.66

<sup>a</sup>P. Allia and F. Vinai, Phys. Rev. B 26, 422 (1986).

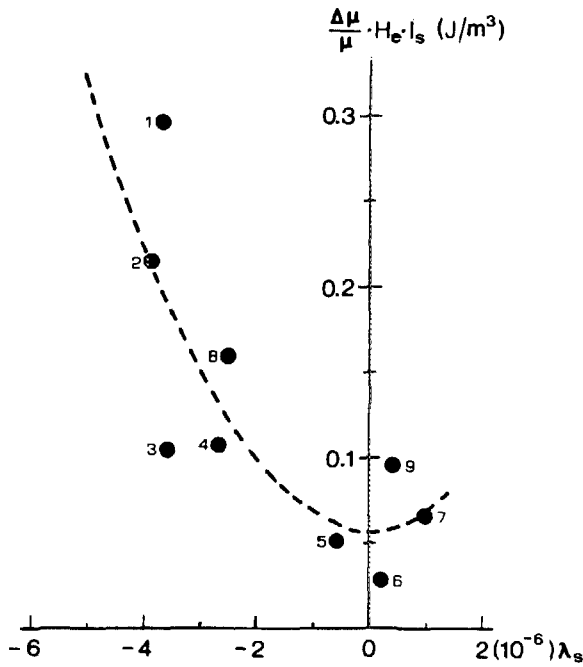


FIG. 2. Plot of the permeability aftereffect  $(\Delta\mu/\mu)H_e \times I_s$ , as a function of magnetostriction of Co-rich alloys. Alloys identified as in Table I. Full lines: best-fit curve,  $(\Delta\mu/\mu)H_e \times I_s = 5.67 \times 10^{-2} + 1.05 \times 10^{10} \lambda_s^2$ .

may be estimated from a simulation of the structure of an amorphous metal. For instance,  $\langle \tau^2 \rangle^{1/2} = 3.29 \text{ eV/\AA}^3 = 5.26 \times 10^{-18} \text{ J/atom}$ , and  $\langle m \rangle = 0.013$  in the realistic model proposed by Egami and Srolovitz.<sup>13</sup> In our opinion, such values are representative of both quantities for the set of amorphous alloys considered here. The parameters  $\lambda_g$  and  $N_T$  may be obtained from the analysis of the present experimental data. Since we need just an order-of-magnitude estimate of these quantities, we make here the simplifying assumption that  $N_T$  is the same in each alloy, and that  $\lambda_g$  remains substantially a constant for small changes of  $\lambda_s$  near

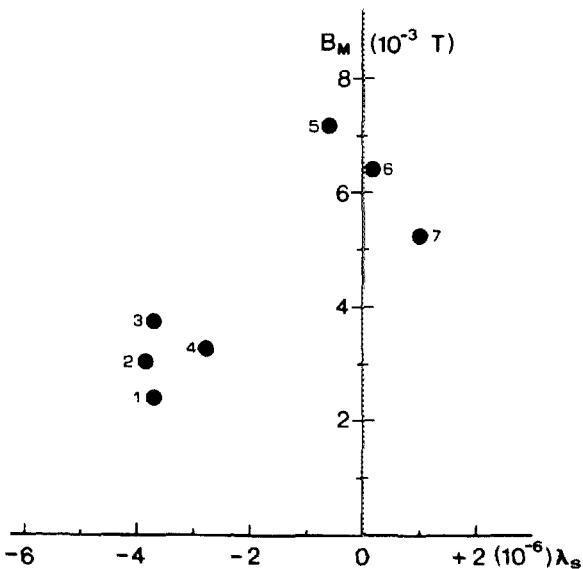


FIG. 3. Position of the maximum of the  $\Delta B(B)$  curves as a function of  $\lambda_s$  in the Co-Fe-Si-B alloy series. Alloys identified as in Table I.

$\lambda_s = 0$ . It is known, in fact, that  $\lambda_g$  retains a positive value even when  $\lambda_s \rightarrow 0$ .<sup>4</sup> Further considerations about  $N_T$  are made in Sec. III B. From Eqs. (1) and (2), and from the experimental data, we have:

$$\begin{aligned}
 (\Delta\mu/\mu)H_e I_s &= a + b\lambda_s^2, \\
 a &= 2.55 \frac{3}{32} \frac{N_T}{kT} [G(t_1) - G(t_2)] \frac{1}{25} \frac{1}{2\pi} \langle m \rangle \lambda_g^2 \langle \tau^2 \rangle \\
 &= 5.67 \times 10^{-2} \text{ J/m}^3, \\
 b &= 2.55 \frac{3}{32} \frac{N_T}{kT} [G(t_1) - G(t_2)] \frac{1}{25} 8\pi \langle \tau^2 \rangle \\
 &= 1.05 \times 10^{10} \text{ J/m}^3. \quad (3)
 \end{aligned}$$

As a consequence,

$$\begin{aligned}
 \lambda_g &= (4\pi\sqrt{a/b}/\sqrt{\langle m \rangle}) = 2.56 \times 10^{-4}, \quad (4) \\
 N_T &= 13.9(kT/\langle \tau^2 \rangle)b \approx 2.2 \times 10^{25}
 \end{aligned}$$

atoms/m<sup>3</sup> (at room temperature).

In other words, the atoms participating in the ordering processes which give rise to the aftereffect are a fraction  $\sim 10^{-4}$  of the total number ( $\approx 10^{29}$  atoms/m<sup>3</sup>).

This result is quite reasonable. Together with the hypothesis that each structural defect involves—on the average, a small number of atoms (10–50)<sup>1,11</sup>—this value of  $N_T$  supports the usual picture of localized ordering events, randomly distributed in the material and weakly correlated.

The value of  $\lambda_g$  is rather large, if compared with the magnetostriction of these alloys, not exceeding  $5 \times 10^{-6}$  in absolute value. This result is again reasonable, since  $\lambda_g$  is expected to be much greater than  $\lambda_s$ .<sup>4</sup>

It may be interesting to make a comparison between the present aftereffect data, and the ones obtained on as-cast Fe-

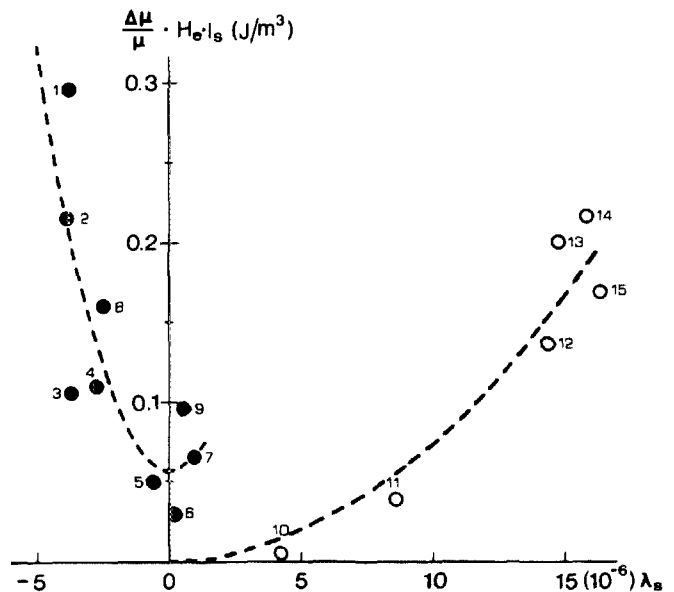


FIG. 4. Behavior of the permeability aftereffect with magnetostriction in the Co-rich alloy series (full dots) and in some representative Fe-rich alloys (open dots), in the magnetostriction interval  $-5 \times 10^{-6} \leq \lambda_s \leq +15 \times 10^{-6}$ . Alloys identified as in Table I. Lines: best-fit curves,  $(\Delta\mu/\mu) \times H_e \times I_s = 5.67 \times 10^{-2} + 1.05 \times 10^{10} \lambda_s^2$  and  $(\Delta\mu/\mu) \times H_e \times I_s = 7.3 \times 10^8 \lambda_s^2$ , respectively.

based alloys with low (positive) magnetostriction, taken from Ref. 4. The measuring technique was exactly the same for both series. The  $\Delta\mu/\mu H_e \times I_s$  vs  $\lambda_s$  curves of Co- and Fe-rich alloys are shown in Fig. 4 in the range  $-5 \times 10^{-6} \leq \lambda_s \leq +15 \times 10^{-6}$ . The full line is the best-fit curve determined from the whole Fe-based alloy series  $\Delta\mu/\mu \times H_e \times I_s = 7.3 \times 10^8 \lambda_s^2$ .<sup>4</sup> The possibility of grouping Fe- and Co-rich alloys in two distinct families is strikingly confirmed by these data. Notice that the slope of the best-fit quadratic law is over one order of magnitude larger in Co-based alloys than in Fe-based ones. The origin of such a discrepancy is presently not clear. In light of the magnetostrictive model, it could be attributed to a difference of some structural parameters ( $N_T, \langle m \rangle, \langle \tau^2 \rangle$ ) between the two alloy families.

### B. Dependence of the aftereffect on the alloy's stability

Although the reported aftereffect data are well represented by the quadratic law discussed in Sec. III A, some scattering is still present. The reasons for this scattering are investigated here. As a matter of fact, the intensity of  $\Delta\mu/\mu \times H_e \times I_s$  at a given temperature turns out to be related not only to the alloy's magnetostriction but also to  $N_T$ , the number of atoms participating in the ordering processes which give rise to the aftereffect [see Eq. (1)]. This number, of the order  $\approx 10^{25}$  atoms/m<sup>3</sup>, may vary as a consequence of changes of the structural state of the amorphous alloy. This effect is particularly evident after structural relaxation, as discussed elsewhere.<sup>4,10</sup>

Generally speaking,  $N_T$  is significantly affected by the stability of the alloy. This fact is not surprising, since the ordering processes responsible for the aftereffect take place easier in less stable structures. A convincing proof of this statement may be given by analyzing the behavior of  $\Delta\mu/\mu \times H_e \times I_s$  in materials having the same  $\lambda_s$  and different thermal stability. This condition occurs in three of the considered alloys, precisely  $\text{Co}_{73}\text{B}_{27}$ ,  $\text{Co}_{75}\text{Si}_5\text{B}_{20}$ , and  $\text{Co}_{75}\text{Si}_{15}\text{B}_{10}$ , characterized by close magnetostriction values and different crystallization temperature  $T_x$ . In these alloys,  $T_x$  is increased and  $\Delta\mu/\mu \times H_e \times I_s$  is reduced by addition of Si, as shown in Table II.

These considerations allow one to conclude that the intensity of the aftereffect may be influenced almost independently by  $\lambda_s$  and  $N_T$ . When both parameters are allowed to vary from one alloy to another, the aftereffect data appear to be rather scattered when plotted versus  $\lambda_s$  (see Fig. 2). When  $\lambda_s$  is kept fixed, the effect of pure variations of the

stability (and  $N_T$ ) is enhanced (alloys 1–3 in Fig. 2). On the other hand, when the thermal stability of a set of alloys is kept as constant as possible (e.g., by varying the transition metal content without changing the metalloid ratio, as in the  $\text{Co}_{75-x}\text{Fe}_x\text{Si}_{15}\text{B}_{10}$  series<sup>7</sup>), the influence of the magnetostriction on the aftereffect intensity is dominant, and the scattering is reduced (alloys 3–7 in Fig. 2). Finally, it should be mentioned that  $N_T$  may also be changed by varying the quenching rate at which the ribbons are produced. As a matter of fact,  $\Delta\mu/\mu \times H_e \times I_s$  increases with increasing the quenching rate. This effect has been discussed in different papers.<sup>14,15</sup>

### C. Dependence of Bloch wall thickness on magnetostriction

According to Néel's theory,<sup>16</sup> the behavior of the magnetic aftereffect ( $\Delta B$ ) as a function of induction  $B$  gives information about the type and the thickness of the Bloch walls, whose motion is progressively hindered by the magnetic viscosity. No direct Kerr-effect observation of the magnetic domain structures was possible on the narrow ribbons under consideration. The presence of a maximum in the  $\Delta B$  vs  $B$  curve (see Fig. 1) suggests, however, that in these alloys the measured aftereffect is substantially related to a damping of the motion of  $180^\circ$  walls.<sup>16</sup> This result is not surprising, at least in ribbons with  $\lambda_s > 0$ , where the magnetic domain pattern is primarily composed of domains separated by  $180^\circ$  walls. In ribbons with  $\lambda_s \leq 0$ , the actual domain structure may be very different, owing to the presence of a transverse anisotropy and complicated secondary domain structures.<sup>17</sup> However, the shape of the  $\Delta B$  vs  $B$  curves (Fig. 1, full lines) is similar to the one observed in ribbons with positive magnetostriction (dashed line in Fig. 1), indicating that even in this case the aftereffect is mainly related to  $180^\circ$  wall motion. The position of the maximum of the  $\Delta B$  vs  $B$  curve  $B_M$  is proportional to the wall thickness  $\delta$ , corresponding to a wall displacement of about  $0.45 \times \delta/2$ .<sup>18</sup> Without a direct knowledge of the average distance between walls, it is not possible to convert the measured  $B_M$  values into actual wall displacements. However, it is clear from Fig. 3 that in the whole  $\text{Co}_{75-x}\text{Fe}_x\text{Si}_{15}\text{B}_{10}$  series  $B_M$  increases with decreasing  $\lambda_s$ . This result is most probably related to a decrease of the anisotropy energy of magnetostrictive type, and to the consequent increase of the wall thickness parameter  $\delta = \pi(A/K_{\text{eff}})^{1/2}$ ,<sup>19</sup> where  $A$  is the exchange energy coefficient, and  $K_{\text{eff}}$  the (total) residual anisotropy energy. A variation of  $\delta$  could also be attributed, in principle, to changes of  $A$ ; however, the Curie temperatures of this alloy series<sup>7</sup> indicate that the variations of  $A$  with varying Fe content do not justify, by themselves, the systematic variation of  $\delta$  with  $\lambda_s$ .

The present aftereffect measurements suggest that the wall thickness increases by a factor of 3 with a reduction of  $\lambda_s$  from  $3.7 \times 10^{-6}$  to  $6 \times 10^{-7}$ . More precise information about the wall thickness in these alloys could be obtained through aftereffect measurements performed on larger ribbons, where the simultaneous observation of the domain structure should be easier.

TABLE II. Permeability aftereffect and crystallization temperatures of three Co-based alloys having similar magnetostriction values.

No.	Material (nominal composition)	$(\Delta\mu/\mu)H_e I_s$ ( $10^{-1}$ J/m <sup>3</sup> )	$T_x$ (K)
1	$\text{Co}_{73}\text{B}_{27}$	2.96	718
2	$\text{Co}_{75}\text{Si}_5\text{B}_{20}$	2.15	765
3	$\text{Co}_{75}\text{Si}_{15}\text{B}_{10}$	1.05	777

#### IV. CONCLUSIONS

A quadratic relation between the magnetic permeability aftereffect and the saturation magnetostriction has been observed also in Co-rich amorphous alloys. The results are in good agreement with the theoretical predictions. The experimental data allow one to obtain a reasonable value for  $N_T$ , the number of atoms involved in ordering processes responsible for magnetic aftereffects in amorphous materials. The room-temperature intensity of the aftereffect has been shown to depend critically on both the alloy's magnetostriction and  $N_T$ . This circumstance explains the scattering typically observed in the plots of the aftereffect as a function of  $\lambda_s$ .

The pure effect of magnetostriction on  $\Delta\mu/\mu$  may be completely disentangled from the one of  $N_T$  only in measurements performed on amorphous ribbons having comparable thermal stability, and produced with similar quenching rates.

Additional information on the functional dependence of the aftereffect on the magnetostriction could be obtained by preparing, with such prescriptions, new ribbons on the  $\text{Co}_{75-x}\text{Fe}_x\text{Si}_{15}\text{B}_{10}$  family, having higher Fe content. In this way, the functional relation between aftereffect and magnetostriction could also be checked in the positive magnetostriction side of this alloy series.

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