

An integrated view on monitoring and compensation for dynamic optical networks: from management to physical layer



A. Teixeira · L. Costa · G. Franzl · S. Azodolmolky ·
I. Tomkos · K. Vlachos · S. Zsigmond · T. Cinkler ·
G. Tosi-Beleffi · P. Gravey · T. Loukina ·
J. A. Lázaro · C. Vazquez · J. Montalvo · E. Le Rouzic

Abstract A vertical perspective, ranging from management and routing to physical layer options, concerning dynamic network monitoring and compensation of impairments (M&C), is given. Feasibility, reliability, and performance improvements on reconfigurable transparent networks are expected to arise from the consolidated assessment of network management and control specifications as a more accurate evaluation of available M&C techniques. In the network layer, physical parameters aware algorithms are foreseen to pursue reliable network performance. In the physical layer, some new M&C methods were developed and rating of the

state-of-the-art reported in literature is given. Optical monitoring implementation and viability is discussed.

Keywords Dynamic networks · Optical performance monitoring · Impairment compensation · Network management and routing

1 Introduction

Reliability in dynamic, wavelength division multiplexed (WDM), photonic communication networks is becoming an

A. Teixeira (✉) · L. Costa
Instituto de Telecomunicações, 3810-193 Aveiro, Portugal
e-mail: teixeira@ua.pt

L. Costa
e-mail: lcosta@av.it.pt

G. Franzl
Institute of Broadband Communications, Vienna University
of Technology, Favoritenstr. 9/388, 1040 Vienna, Austria
e-mail: Gerald.Franzl@tuwien.ac.at

S. Azodolmolky · I. Tomkos
Athens Information Technology, 19002 Peania, Athens, Greece
e-mail: azods@cmu.edu

I. Tomkos
e-mail: itom@ait.edu.gr

K. Vlachos
University of Patras, 26500 Rio, Greece
e-mail: kvlachos@ceid.upatras.gr

S. Zsigmond · T. Cinkler
Budapest University of Technology and Economics,
1117 Budapest, Hungary
e-mail: Zsigmond@tmit.bme.hu

T. Cinkler
e-mail: cinkler@tmit.bme.hu

G. Tosi-Beleffi
Istituto Superiore della Comunicazioni e delle
Tecnologie dell'Informazione, 00144 Rome, Italy
e-mail:Giorgio.tosibeleffi@comunicazioni.it

P. Gravey · T. Loukina
Institut TELECOM, TELECOM Bretagne, Technopôle Brest-Iroise
CS, 83818 - 29238 Brest Cedex 3, France
e-mail: Philippe.gravey@telecom-bretagne.eu

J. A. Lázaro
Universitat Politècnica de Catalunya, 08034 Barcelona, Spain
e-mail: jose.lazaro@tsc.upc.edu

C. Vazquez · J. Montalvo
Universidad Carlos III de Madrid, 28911 Leganés, Madrid, Spain
e-mail: cvazquez@ing.uc3m.es

J. Montalvo
e-mail: Julio.montalvo@uc3m.es

E. Le Rouzic
France Telecom, 2 av. P. Marzin, 22307 Lannion Cedex, France
e-mail: esther.lerouzic@orange-ftgroup.com

increasingly significant research topic. The combination of the ever-increasing demand for capacity, the generalization towards meshed network topologies, and widespread availability of dynamic optical switching, leads to severe constraints on quality of service (QoS) provisioning. These result from the difficulty in maintaining a uniform and acceptable quality for any optical path across a transparent optical network comprising multiple fiber types, signal formats and data rates [1]. Furthermore, the quality of each optical path is often correlated with that of other optical paths due to optical impairments such as crosstalk, limited amplifier output power, or transients in optical amplifiers among others. In this scenario, newly emerging unforeseen demands often cannot be satisfied without modifying the network design, which is costly and time consuming.

A solution for the interoperability issues among network layers based on the introduction of dynamic M&C capabilities must cope with the escalating complexity inherent to the deployment of more reliable transparent networks. The need to achieve higher performance levels and to enhance the network reconfiguration capability & autonomy is also spreading from core to metro and access networks [2].

In communication networks, routing generally performs the identification of a path (route), per connection request, between a source and a destination node, across the network. In optical networks, the particular wavelength(s) along the path should also be determined. The resulting problem is often designated as routing and wavelength assignment (RWA) problem in literature [3]. The existing RWA proposals can be classified into two main categories: (a) considering the effects of impairments on network performance and (b) network design with impairment consideration. Although this is a widespread research topic, for transparent networks the incorporation of physical impairments in the RWA problem is still to be explored in full width. As such, a broader perspective over this problem, which surveys both, physical layer and management and control plane issues, is presented in this paper. The paper is organized as follows. Section 2 discusses impairment-aware RWA (IA-RWA) schemes as well as traffic grooming. An attempt to promote network performance optimization via impact analysis of physical impairments on quality of transmission (QoT) is made and a specific proposal for dynamic monitoring and compensation in terms of per-link and end-to-end control-loop characteristics given. Section 3 describes general requirements for successful implementation of monitoring methods in the physical layer, in order to establish a comprehensive comparison among existing M&C techniques from literature and some new developed described herein. The operator point of view of actual optical performance monitoring (OPM) requirements in current core networks is presented in Sect. 4. Section 5 concludes this paper.

2 Network layer

The reconfigurable optical network offers the possibility to grow services between sites without advanced engineering or planning, and without disrupting services. The real innovation lies in the system engineering related to the reconfigurable functions, addressing per-channel metrics and management, and fault isolation. The evolution of optical networks seems to tend towards a fully reconfigurable network, where the control plane (CP) and management plane (MP) have new functions, intimately correlated with M&C, such as determining the signal quality, tuning the wavelength frequency, setting dispersion compensation units and controlling channel powers.

2.1 Management and routing

2.1.1 Introduction

The RWA problem is an NP-complete problem with computational effort increasing exponentially with the problem size. Thus, a wide range of optimum approximation methods and heuristics have been proposed to solve various network optimization problems. Integer linear programming could be employed [4], but it requires heavy computational efforts. Other heuristic algorithms such as Tabu-search [5], simulated annealing [6], and genetic algorithms [7] with to some extent scalable computation effort have also been proposed. The latter, for instance, have been used to solve the plain single objective RWA problem [8], to optimize amplifier placement [9], as well as to optimize multicasting sessions [5].

Most IA-RWA approaches recently proposed still consider the QoT problem separately from the RWA problem [10, 11]. A common strategy employed is to incorporate impairments into the cost function. However, a cost function for both linear and nonlinear impairments is still an open question. Different analytical models have been developed to describe reference links with or without compensation of fiber impairments [11, 12]. Only few studies, however, consider the simultaneous impact of chromatic dispersion (CD), polarization mode dispersion (PMD), amplifier spontaneous emission (ASE), and nonlinear phase shift [13]. Therefore, other more universal metrics have been used, including the average measured Q [14] or noise variance [12]. In any case, accurate Q_{path} estimation is a heavy computational task, even in the static RWA problem, demanding offline calculation.

For an IA-RWA strategy to be actually implemented, one needs to consider also fundamental aspects like enabling Optical Impairment Monitoring (OIM) for indirect evaluation of signal quality, or enabling direct Optical Performance Monitoring (OPM) [15]. In 2004, ITU-T define a list of OPM parameters that might be used for impairment-aware

RWA [16]. We consider the most important performance parameters to be: (a) residual chromatic dispersion (CD), (b) total EDFA input and output powers, (c) a channel’s optical power budget, (d) optical signal-to-noise ratio (OSNR), and (e) Q-factor as an estimator of the overall optical performance. An effective OIM/OPM strategy shall also support the CP in performing lightpath establishment or re-routing functions, and can be accomplished through (a) a centralized approach, if all paths to be established within a domain are computed by a single and centralized network element (NE), e.g., a network management system (NMS), or path computation element (PCE) [17], or (b) a distributed approach, if a distributed and intelligent CP, embedded in each NE, is responsible for both route computation and lightpath establishment.

2.1.2 Multi-constraint distributed RWA applying service dependent vector-of-constraints and lattice algebra

An RWA algorithm to consider any number and type of parameter individually has been presented in [18]. The presented scheme, entitled ‘Distributed Wavelength-path Provisioning’ (DWP), is proposed to maximally spread the computing effort, to improve accuracy of locally monitored parameters, and to avoid continuous distribution of all per link/node possibly relevant parameters. The basic idea is to sum-up parameters along potential paths on demand, distribute path messages selectively, and thereby exclude paths where service related end-to-end communication constraints are not met in the first place (Step 2). The scheme consists of the 4 steps shown in Fig. 1.

As said before, any number and type of constraint can be considered in parallel, like QoS/BER & delay & reliability, as typically found in service level agreements (SLAs). As such, the fulfillment of constraints is guaranteed as long as the parameters applied during path evaluation do not change. To cope with parameter changes the selection strategy (Step 3)

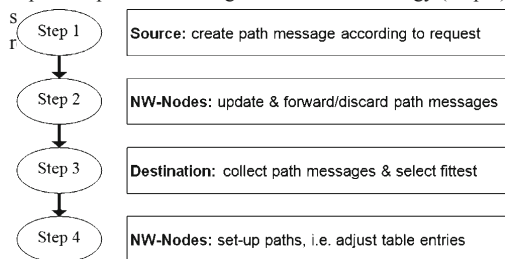


Fig. 1 CB-RWA using DWP algorithm to find feasible all-optical end-to-end paths

parameters (e.g., OSNR, QoS). Monitoring of a path’s end-to-end performance can finally contribute to the control of SLA fulfillment and trigger autonomous re-routing whenever the headroom diminishes below a constraint specific threshold.

DWP’s inherent strength is its individual per constraint operation that allows on-demand adoption to new constraints. However, it is not applicable for packet switching due to the effort introduced by the circulation of a great amount of path messages to find candidate paths. Yet, some experts have recently proposed to control the network dynamics by limiting routing freedom. For instance, MPLS exactly performs that per-flow (per ingress/egress pair). The routing underlying a label-switched path (LSP) typically does not change, and thus the effective effort introduced by finding feasible paths to transport a certain flow type with the demanded QoS inversely depends on the LSP life-time. Complex set-up procedures for long living LSPs thus actually introduce less effort if thereby frequent re-routing can be evaded.

2.1.3 Cross layer impact of physical effects and traffic grooming in multilayer networks

In general, for statically routed networks of practical size, the number of available wavelengths is lower by a few orders of magnitude than the number of connections to be established. The only solution here is to join some of the connections to fit into the available wavelength-paths. This is referred to as traffic grooming, which is possible to perform in the electric domain. It is assumed that there is no signal regeneration, and noise and signal distortion accumulate along lightpaths. Actually, 3R regeneration (re-amplification re-shaping, and re-timing) would be necessary to overcome these impairments. Although it has been demonstrated in laboratories, we consider that only electrical 3R regeneration is economically viable in current networks. To evade the physical limitations in the optical domain, optical/electrical/optical (O/E/O) conversion needs to be (selectively) included to ensure the quality requirements. An algorithm has been proposed in [19] to investigate the effects of these O/E/O conversions on the RWA process. The algorithm can be split in two main parts: the routing part and the physical layer monitoring system (PLMS). The communication between these two parts is as follows. The routing algorithm chooses an optimal route between the source and destination node and, if the PLMS is switched on, it sends the description of the route to PLMS. The PLMS determines the signal quality and, if it is adequate, it sends a connection confirmation message back to the routing part. If the signal quality is not adequate, the PLMS determines the most distant reachable node (MRN) along the path and sends this information back to the routing module. This establishes the connection between the source and the MRN and then chooses a route between the MRN

and the destination node repeating the scheme. If MRN and source node coincide no possible connection exists and the connection is blocked.

In the proposed algorithm the impact of physical impairments on routing the demands in a grooming capable two-layer network is implicitly considered. The emphasis is on the mutual impact of grooming and physical impairments, i.e., application of the electronic time- and space-switching layer for signal regeneration and better joint resource utilization.

2.2 Network performance optimization

To achieve the per connection demanded maximum BER, bit errors caused by temporarily insufficient QoT, caused by the inertia of adjustments to changing traffic assignments, need to be considered. In case of M&C at destination nodes this can be effectively done. However, any thereby forced adjustment must comply with all demands from other traffic flows sharing a resource along the path. For instance, adjusting the gain of all-optical amplifier being part of links carrying many flows based on all the individual per lightpath (end-to-end) monitored parameters is very complex. Instead, for such, per-link (fiber section) monitored parameters that influence all carried flows similarly should be used.

The exact calculation of parameters for M&C to achieve optimal performance poses a fundamental mathematical problem. This is illustrated in Fig. 2 where an abstract impairment is considered. Demand on received QoT is -10 to -3 , degradation per link is -5 , input QoT is $+3$, and the compensation can be adjusted between -3 and $+3$, i.e., degradation cannot be completely compensated but deliberately worsened $a_{ij} = [-8..-2]$, as typical for physical impairments.

To solve the simple dimensioning problem depicted in Fig. 2, we can set up the according equation system:

$$P(\text{Dest}_1) = 3 - a_{12} - a_{23} - a_{34}$$

$$P(\text{Dest}_2) = 3 - a_{51} - a_{12}$$

$$P(\text{Dest}_3) = 3 - a_{34} - a_{45} - a_{51}$$

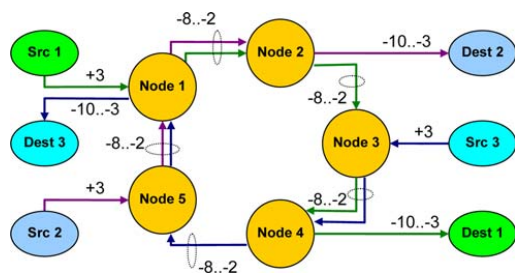


Fig. 2 NP hard problem of interdependent adjustments

We have three equations for five variables, a multi-dimensional continuum of feasible solutions, and thus might assume that an optimum solution providing fair connection quality distribution among all three connections could be found. However, there is a cyclic dependence and parameters are bound to certain intervals adding additional equations. Solving the equation system for feasible real numbers yields not the best solution, i.e., degradation of -8 while in one by one mode we get far better results $[-3..-5]$. We can state that a solution providing equal quality per connection, if it exists, for the example scenario does not yield an optimum. Further, as cycles alike the discussed likely exist in every meshed topology, we derive that, in general, solutions that grant equal quality per connection are suboptimal if impairments cannot be compensated 100% in the first place.

A global optimization approach based on complex and time consuming calculations (e.g., integer linear programming), which relies on a network-wide knowledge of every single flow and resource parameter, appears inadequate for dynamic environments and is unsuited for real-time control-loops. Non-real-time operation allowing off-line calculations would demand synchronized, and, more restrictive, considerably delayed changes in traffic assignments, which is a clear contradiction to dynamic traffic management as featured in optical packet switched (OPS) and optical burst switched (OBS) architectures. We should consequently drop the optimum performance requirement and demand stable performance with least effort, i.e., minimal added cost. Therefore, parameters which can be efficiently stabilized per link shall be managed by per link control-loops, all other per lightpath. This clearly does not grant global optimization. Nonetheless, stable and reliable impairment management is likely more important than squeezing out the least quantum of optical span potentially possible.

2.3 Specification for dynamic monitoring and compensation

2.3.1 Introduction

The heavy dependence of the feasibility of optical spans on the dynamic performance of the physical components and the quality demands of special lucrative services justify the use of performance monitoring for dynamic lightpath management purposes. Performance stability of several components is to some extent dependent on the traffic load and that demands efficient control to be deployed in dynamic environments.

Traditionally the stability is gained by controlling the environment, e.g., adding dummy channels to keep optical power constant when not all wavelengths are in use. Today more dynamic approaches are demanded, since traditional ones are designed and optimized for the entirely opaque, O/E/O-based network architectures. In dynamically switched all-optical

networks the stabilization of physical parameters should be the prime target. When we look at next generation optical networking paradigms, e.g., OBS and OPS, we must solve the problem of keeping the performance of physical components constant, i.e., independent of dynamically changing traffic assignment, to enable their future deployment.

2.3.2 Impact of physical impairments compensation on QoS respectively SLA fulfillment

Customers demand QoS derived from SLAs, which typically consist of statistical metrics, i.e., average and/or maximum (maximum typically a highly probable bound, not an absolute value), on BER, loss-rate, and latency. If BER is met, loss-rate and latency are not related to physical impairments, i.e., loss or repetitions of content are not caused by insufficient BER. Thus, we need to consider BER as the only service requirement dependent on the control of physical impairments.

BER is directly related to QoT, although, the relation depends on modulation format and receiver technology. We can assume that the average values are met by design, respectively, by the applied RWA scheme. The contribution of the considered physical impairments to QoT degradation is expressed in (1).

$$QoT_{[dB]} = Q_{OSNR} - Q_{GVD} - Q_{DGD} - Q_{FWM} - \dots \quad (1)$$

where $Q_{OSNR} = P_{\text{signal}}/P_{\text{noise}}$ reflect the eye-opening at the receiver after consideration of amplified spontaneous emission (ASE) noise. The other are eye-closures caused by other linear and nonlinear, potentially signal or technology dependent, effects. For stabilization we need to consider the dependence of the contributing components on changes of traffic load (sensitivity), their relative impact on QoT (impact), and how fast they possibly could be compensated (speed), alike the assumptions shown in Table 1.

2.3.3 An attempt to specify control-loop characteristics

The specification for impairment compensation can be stated individually for the per-link and the per-lightpath control-loops (Tables 2 and 3).

To which extent these specification contribute to SLA fulfillment depends on the number of hops n with adjustments originated temporarily increased BER ($BER_{\text{transient}}$):

Table 1 Assumed parameters contributing to QoT

Parameter	Sensitivity	Impact	Speed
Q_{OSNR}	Low	Linear	Moderate
Q_{GVD}	Low	Exponential [20]	Slow
Q_{DGD}	Moderate	Exponential [21]	Fast [22]
Q_{FWM}	High	Nonlinear	N/A

Table 2 Exemplary specification for per-link control loops

Parameter name	Stabilization target	Monitoring speed	Adjustment speed
Inserted light-power (fiber)	$\pm x$ dBm	Fast (ns)	Moderate (ms)
Chromatic dispersion	$\pm x$ ps	Moderate (ms)	Fast (ns)

Table 3 Exemplary specification for per-lightpath control loops

Parameter name	Stabilization target	Monitoring speed	Adjustment speed
OSNR	X dB	Slow (s)	Moderate (ms)
Center wavelength	$\pm x$ nm	Fast (ns)	Slow (s)
PMD	$\pm x$ ps	Moderate (ms)	Moderate (ms)

$$\begin{aligned}
 &BER_{\text{transient}}(\text{link}_i) \\
 &= p_{\text{adj}}(i) E[\text{bit error} | QoT(t) < QoT_{\text{target}}] \\
 &BER_{\text{transient}} < \sum_{i=0}^n BER_{\text{transient}}(\text{link}_i) \\
 &+ p_{\text{adj}}(\text{lp}) E[\text{bit error} | QoT(t) < QoT_{\text{target}}] \quad (2)
 \end{aligned}$$

where $p_{\text{adj}}(i)$ is the probability for adjustments on the i -th link in the path, $p_{\text{adj}}(\text{lp})$ the probability for per lightpath adjustments, and $E[\text{bit error} | QoT(t) < QoT_{\text{target}}]$ is the likelihood for bit-errors in case current QoT is below target QoT, i.e., current BER is above that for stable operation.

To get an upper bound let us assume a worst case: No end-to-end headroom and complete detector malfunction for $QoT(\text{lp}) < QoT_{\text{target}}$, i.e., $E[\text{bit error} | QoT(t) < QoT_{\text{target}}] = 0.5$. If we additionally simplify and assume the probability for adjustments to be equal for all links and lightpaths, Eq. 2 reduces to:

$$BER_{\text{transient}} < \frac{(n+1)}{2} p_{\text{adj}} \quad (3)$$

To minimize the transient impact we need to minimize p_{adj} . As p_{adj} is calculated as required number of adjustments per time-unit multiplied by time-units these adjustments cause $QoT(t) < QoT_{\text{target}}$, only the latter can be addressed by design of compensation mechanisms. The common problem of control-loop design, reaction speed versus stabilization time, then arises along with the acknowledgement of cascaded, potentially interdependent, control-loops as the compensation mechanism performance specification parameters.

A simple approach to solve the problem would be to enforce asymptotic control-loop behavior. However, if there is some headroom for sufficient detection, slight overshoot might be acceptable and faster loop operation and reduced number of bit-errors per adjustment would be possible. To solve that we again need to solve a problem as that depicted

in Fig. 2 to cope with the cascades and interdependencies, which now can be done off-line using the methods mentioned earlier, since control-loop performance characteristics are independent of instantaneous traffic load. Nevertheless, the results will depend heavily on actual traffic statistics and network topology.

We conclude that the control-loop performance targets for the deployment of physical impairments compensation mechanisms in arbitrarily meshed transparent networks with dynamic traffic assignment cannot be specific independent of traffic characteristic (holding time distribution), traffic matrix (likelihood of flows per node pair), and network topology (average and maximum path length). For network architectures comprising restriction to a certain topology and stable traffic distribution the specs need to be individually derived.

Only if stabilization is reached within a fraction of a single optical pulse, or if adjustments have per se no effect on QoT, traffic assignment dynamics independent QoT could be achieved ($BER_{transient} = 0$). Assuming that out of reach, we conclude that the demand on stabilization speed is directly related to traffic assignment dynamics. To achieve the same BER as for today's non-dynamic optical connections, the QoT needs to provide sufficient extra head-room. The slower the stabilization, the more hops, the more dynamic traffic changes cause adjustments, the more QoT head-room is required and that needs to be granted by constraint-based RWA.

A switched layer 0 (the transparent analogous physical layer) lacking transparent 3R regeneration with every hop can in general not grant constant QoT and thus shall not be responsible for electrical-to-electrical BER liability, even if that demands renunciation from common attitudes.

3 Physical layer

There is an increasing interest in transferring some monitoring capabilities, which were exclusively managed by SDH/SONET [23], to the physical layer in order to enable fully reconfigurable and transparent optical networks, with improved reliability and flexibility. Even in the context of access networks, where advanced monitoring capabilities are not implicitly considered at first they eventually become crucial to perform packet synchronization, power equalization [24], or link fault detection and identification in Giga-capable networks, contributing for system resilience, as well as for increased reach and overall end user number served.

OPM started by focusing attention on simple channel parameters, like wavelength and optical power, but rapidly advanced to more complex and sophisticated solutions, such as simultaneous and independent monitoring of different physical impairments [1]. The lack of standardization and low maturity level of monitoring methods and systems is still significant. For these reasons, research work on this

topic appears in literature in a large extent. As such, the choice of more adequate M&C techniques is a complex task. Moreover, there is no perfect method capable of meeting the entire requirements imposed by transparent networks [23]. To cope with this, we have produced a collection of state-of-the-art monitoring methods and developed rating criteria to enable straightforward comparison between them. Investigation, improvement, and validation of some new impairment-specific monitoring techniques are also presented.

3.1 Monitoring techniques evaluation

One would agree that technological evolution and commercial deployment are essentially dependent on one critical lim-

Table 4 OSNR monitoring techniques

Criteria	Orthogonal polarization heterodyne mixing [25]	Nonlinear loop mirror [26]	Hi-birefringent loop mirror [27]
Type ^a	O	O	O
Accuracy/sensitivity	Moderate	*	Moderate
Dynamic range	Low	High	Moderate
Other impairments insensitivity ^b	Moderate	Low	Moderate
Modulation format transparency	Yes	Yes	Yes
Bit rate transparency	Yes	Yes	Yes
Transmitter modification	No	No	No
Multi-channel	No	No	No
Multi-parameter	No	No	Yes
Implementation complexity ^c	Simple	Suitable	Simple
Technological requirements ^d	Good	Suitable	Good
Acquisition time ^e	Fast	Moderate	Fast
Cost ^f	Low	Low	Low

* There is not sufficient information in literature

^a 'O' means optical; 'E' means electrical; 'O/E' means optical/electrical

^b Insensitiveness of the monitored physical quantity to other impairments and robustness to environmental parameters (e.g., temperature)

^c Complex when stabilization via filtering carrier dithering, or phase-locked loops are required, and/or the amount of electronic or optical pre- and post-processing involved is high

^d Low power consumption, compactness, non-intrusiveness, and scalability

^e Considered fast if less than 1 ms

^f A low cost-solution is a comprehensive concept, which includes: (i) multi-channel ability, (ii) multi-parameter ability, (iii) simplicity of implementation, (iv) good agreement with technological requirements, and (v) low overall cost of the electrical/optical components which constitute the device

Table 5 GVD Monitoring techniques

Criteria	RF pilot tones [28]	Polarization scrambling [29]	Asynchronous chirp [30]	TPA with semiconductor micro-cavity [31]
Type ^a	O/E	O/E	O	O
Accuracy/sensitivity	High	High	High	*
Dynamic range	Moderate	Moderate	Moderate	High
Other impairments insensitivity ^b	Moderate	Moderate	Low	Low
Modulation format transparency	Yes	Yes	Yes	Yes
Bit rate transparency	Yes	Yes	Yes	Yes
Transmitter modification	Yes	No	No	No
Multi-channel	No	No	No	Yes
Multi-parameter	No	Yes	No	No
Implementation complexity ^c	Suitable	Simple	Simple	Suitable
Technological requirements ^d	Good	Good	Good	Good
Acquisition time ^e	Moderate	Fast	Fast	Fast
Cost ^f	Moderate	Low	Low	Low

Note: See Table 4 for footnote details

Table 6 PMD Monitoring techniques

Criteria	Polarization-based interferometric filter [32]	Degree of polarization [33]	Partial bit delay MZI [34]
Type ^a	E	O	O
Accuracy/sensitivity	High	*	*
Dynamic range	High	Moderate	High
Other impairments insensitivity ^b	Low	Moderate	Good
Modulation format transparency	Yes	No	Yes
Bit rate transparency	Yes	Yes	No
Transmitter modification	No	No	No
Multi-channel	No	No	No
Multi-parameter	No	No	Yes
Implementation complexity ^c	Complex	Simple	Simple
Technological requirements ^d	Good	Suitable	Suitable
Acquisition time ^e	Moderate	Fast	Moderate
Cost ^f	Expensive	Low	Low

Note: See Table 4 for footnote details

iting factor: cost. However, it would not be a wise decision to choose an OPM technology or method based on just a single criterion. Thus, general criteria were derived from the considered three main factors: cost, robustness, and scalability. To simplify the task the methods were divided according to the actual impairment to be monitored. Here, only OSNR, group velocity dispersion (GVD) and polarization mode dispersion (PMD) monitoring methods are contemplated. Some of the techniques which fit best the designated criteria are shown in Tables 4, 5 and 6.

Some of the information needed to fill the table according to the criteria does not exist in the consulted literature. In that case, we report our own assumptions, at the exception of the quantitative criteria. These comparison criteria can also be used for rating of compensation techniques with minor modifications

3.2 Advanced optical performance monitoring and compensation

3.2.1 Multi-channel OPM based on free-space optics

Free space optics can be applied to conceive optical monitoring devices. The use of only passive optical components in an OPM device enables fast spectrum acquisition times, with lower cost. The optical design of our device, based on a diffraction grating and a photo-detector array, involves a trade-off between the image spot dimension, the array pitch and the multiplex spectral bandwidth. Proper operation with 50 GHz spaced DWDM channels can be enabled by two ways: either by using (a) a very high dispersion diffraction grating and a photodiode array with more than 1000 detectors or by using (b) a moderate resolution optical system associated with sophisticated channel reconstruction protocol [35]. The second option is more cost-effective, although it implies partial superposition of adjacent channels.

An OPM prototype with a low PDL 900mm^{-1} reflective relief grating, and a 512 pixels InGaAs array with $25\mu\text{m}$ pitch integrated in commercial linear camera was experimentally evaluated. Several optical configurations were simulated using ZEMAXTM software in order to find the best, which corresponds to a couple of lenses with 30 and 250 mm focal lengths and an incident angle on the grating of 53° . A specific control software featuring the generation of a table of monitored parameters (power level, wavelength, ITU channel number, OSNR), the definition of alarm generation criteria, and the display of these alarms, was developed.

The channel profile reconstruction routine has to deal with two main problems: (i) the choice of a suitable reference shape for each channel, in order to provide its power and optical carrier frequency accurately, and (ii) the influence of closed channels. With an individual channel reconstruction method the -3 dB transfer function width is about 25 GHz,

high is much wider than a standard (NRZ or RZ) 10 Gbit/s modulated spectrum. Therefore, a simple Gaussian approximation of the spectral shape is valid for 10 Gbit/s. For 40 Gbit/s, this may not be valid, and different reference shapes representative of the various modulation formats may need to be used. The tests reported here were performed under the Gaussian approximation.

We then developed a collective profile reconstruction method which fit data with a sum of Gaussian functions to increase reconstruction accuracy. The width of a sliding window is locally adjusted, in order to optimize the trade-off between reconstruction accuracy and computing time. We then compared the accuracy of the individual and collective reconstruction methods in presence of groups of 50 GHz-spaced non-modulated channels, for which the optical power of all odd-number channels was varied. For the individual profile reconstruction, the accuracy decreases with increas-

ing inter-channel power difference and for low-power channels, the maximum power deviation is more than 0.5 dB. This does not occur for the collective profile reconstruction, where power accuracy remains better than 0.3 dB (see Fig. 3). We also evaluated our prototype in presence of up to 40 multiplexed channels spaced at 100 or 50 GHz, with NRZ format at 40 Gbit/s. Both individual and collective methods yield a correct reconstruction, which is shown in Fig. 4, for a group of four 50 GHz-spaced channels.

Finally, we tested the OPM prototype with forty 100-GHz spaced 40 Gbit/s modulated channels using either CSRZ or RZ33% modulation formats. For these formats, one channel presents two 40 GHz separated equal peaks (CSRZ format) or one central peak with two secondary lobes (RZ 33% format), which are always detected and reconstructed as separated channels by our device. It is clear that for these advanced modulation formats, like CSRZ, a specific non-Gaussian

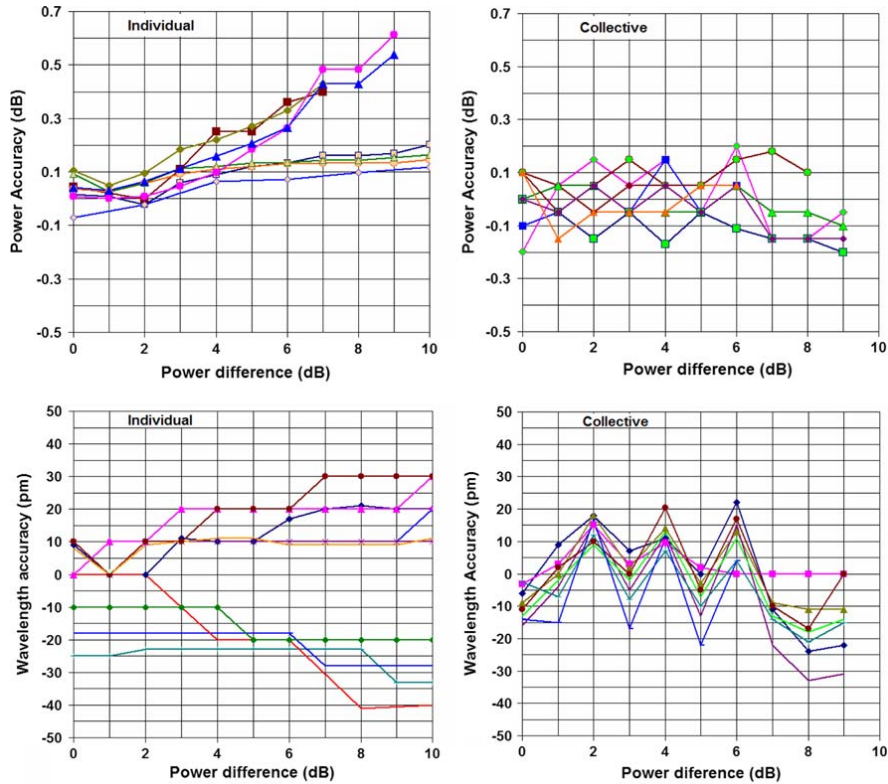


Fig. 3 Power (top) and wavelength (down) accuracy versus power difference between neighboring 50 GHz-spaced channels for individual (left) and collective (right) reconstruction methods

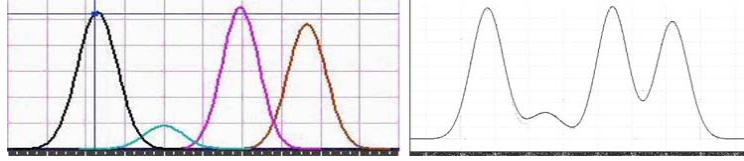


Fig. 4 Individual (left) and collective (right) reconstructions of four 50-GHz spaced NRZ 40 Gbit/s channels with 7 dB power difference between neighboring channels; for collective reconstruction, the red

curve represents the signal generated by the photodiode array, the green one corresponds to the interpolation of rough data, and the white line is the reconstructed channel profil

reconstruction model is required. Work is in progress to test this new feature.

3.2.2 Dynamic and remote OTDR monitoring

Metro and extended Access Networks are showing a tendency towards convergence due to the urge of deploying transparent WDM optical networks. A fully passive and transparent Metro-Access network, SARDANA, has been proposed and investigated [36].

It has shown to be able to provide broadband access up to 10 Gbit/s to more than 100 users covering more than 100 km [37]. Figure 5 shows a possible scenario where several Metro-Access networks are connected to a possible Regional network. In this case, one or more Central Office (CO) are connected to the nodes of the Regional network, where M&C modules can be distributed. We concentrate in this section in describing a method and the developed equipment required for monitoring transparent passive Metro-Access networks.

Since the proposed Metro-Access network is fully passive, electronic equipment has to be concentrated at CO or at Optical Network User equipment (ONU). Remote monitoring is preferred at the CO since it is a more flexible approach for operators, not requiring any kind of ONU equipment upgrade or installation costs.

On one hand, each section of the Metro-Access network with tree topology is working at a fixed wavelength [36]. Thus, it was necessary to implement a tunable OTDR for monitoring the different sections of the network. This was done by using a Grating-Coupled Sampled Reflecto tunable laser (GCSR), as shown in Fig. 6 [38].

Fast tuning of the output signal from the GCSR of only 145 GHz allows generating well formed pulses, with an extinction of >35 dB, as shown in Fig. 7.

On the other hand, the Metro-Access network can be deployed using next generation single fiber reflective ONUs, with the disadvantage of having to deal with Rayleigh Backscattering [39]. In order to minimize this impairment, a double fiber ring is implemented. As such, the experimental OTDR trace shown in Fig. 8 has to be interpreted. After analysis of the experimental data, adequate performance of the diverse elements of the Remote Node (RN) can be remotely

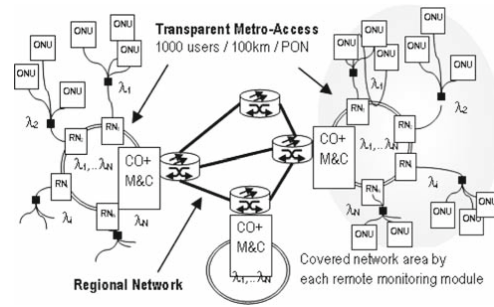


Fig. 5 Scenario for application of remote/distributed Monitoring and Compensation modules to extended transparent Metro-Access networks

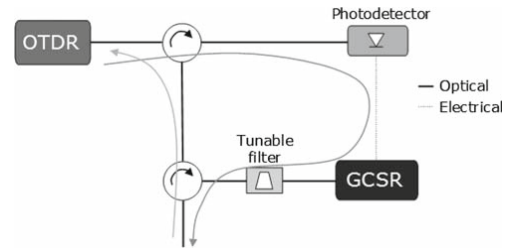


Fig. 6 Implementation of the tunable OTDR using a GCSR laser and an optical filter

checked. They are, for the downstream path: -1.5 dB (filter loss), -3.1 dB (50/50 power splitter), $+25$ dB (EDFA gain), -0.4 dB (circulator), and, for the upstream path: -0.4 dB (circulator), $+18$ dB (EDFA gain), -3.1 dB (power splitter), and -1.8 dB (filter loss), in agreement with independent characterization of each component.

Following the described procedure, each section of the Metro-Access network can be analyzed by tuning the remote OTDR to each one of the λ_1 to λ_N wavelengths and the WDM ring by selecting a non-assigned wavelength. Finally, the Raman amplification gain can be characterized and monitored, as well as the consumption of the remote pumping provided by the CO for feeding the EDFAs at the RNs [36].

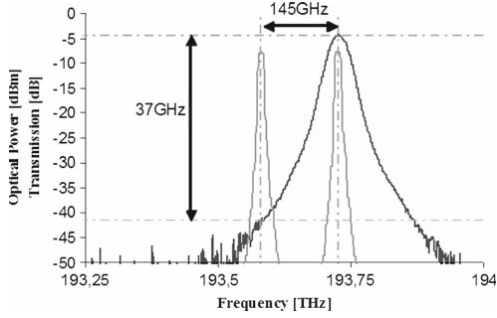


Fig. 7 Spectrum of the laser emission and transmission function of the tunable filter. Center wavelength: 1547.50 nm

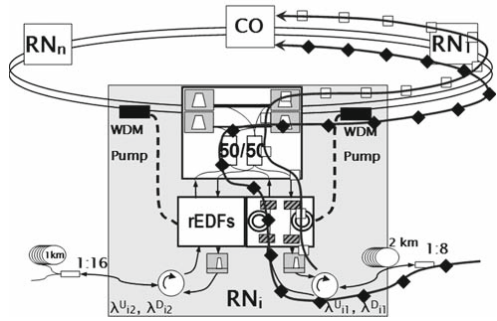
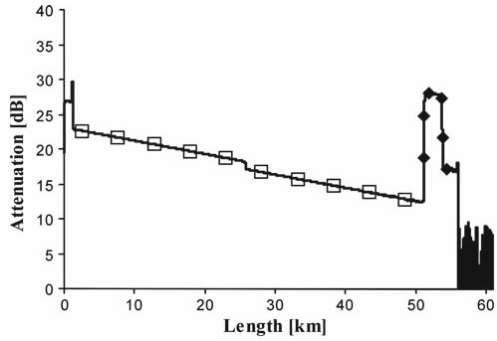


Fig. 8 OTDR measurement and corresponding sections of the network monitored by the proposed technique

The described remote monitoring method provides a powerful tool for the implementation of transparent networks.

3.2.3 Tunable CD compensation with a Sagnac loop in ring resonators

Fiber-optic interferometers, such as the Fabry-Perot (FP) and the ring resonator (RR), have long been considered possible

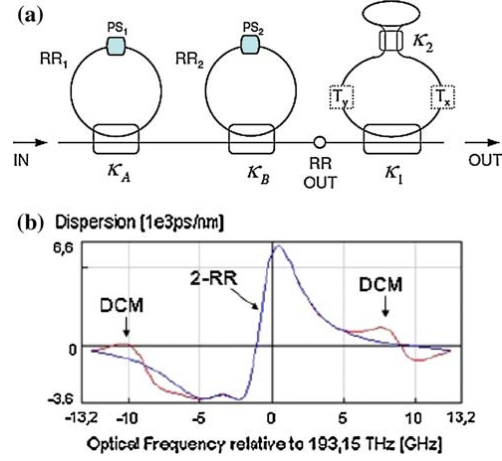


Fig. 9 a Proposed DCM schematic for chromatic dispersion compensation cascading two RR and a RR-SG configuration PS: Phase-shifter. b Quadratic dispersion of a 2-RR + RR-SG filter with FSR = 25 GHz for chromatic dispersion compensation. RR-SG parameters: $k_1 = 0.3, k_2 = 0.8, g_1 = g_2 = 0.925$

CD compensating filter for high bit rate digital transmission systems [40]. To achieve flat-responses in a proper bandwidth, higher order filter should be developed. Recently, a RR with SG loop filter (RR-SG), as the one shown in third block of Fig. 9a, has been reported as a second order tunable optical filter with ultra-narrow-bandwidth for use in DWDM systems [41] or as part of a novel filter design technique [42]. It can also be used for designing tunable dispersion compensation modules (DCMs) by changing the value of the coupling factor k , and to achieve higher order designs in combination with other FIR filters

In Fig. 9a, a specific example of a DCM based on a compound filter made of a 2-RR + RR-SG is presented. The quadratic dispersion of this DCM is shown in Fig. 9b. The dispersion compensating bandwidth of the left sidelobe of this DCM is the double of the DCM based only on the 2-RR filter, for a value of quadratic dispersion around -3100 ps/nm, which is in principle capable of compensating the chromatic dispersion of around 194 km of SMF. Figure 9b also shows that the central frequency of the DCM equals the center of the left-sidelobe with negative dispersion and it emits 0 dBm of average output power.

The performance of RR-SG-based filter in an optical digital transmission system operating at high bit rates was tested. A simplified model of a fiber link has been built using the VPI Photonics™ v. 7.01 software simulation engine.

Figure 10 shows the transmitter, consisting of a 10 MHz linewidth distributed-feedback laser diode (DFB-LD), which

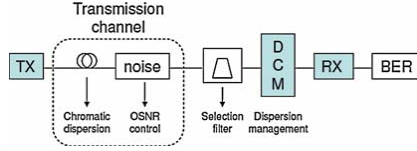


Fig. 10 Simplified model of a digital transmission link with chromatic dispersion and white noise from amplifier

is externally modulated by a pseudo-random NRZ signal at 5 Gbit/s. The second block is a simplified transmission channel, which consists of a CD generator and a white noise generator. The dispersion generator is just a single-mode fiber model without attenuation, with a dispersion of 16 ps/nm+km and a slope of 0.08ps/nm²+km at the central frequency of the simulations. Simulation results demonstrate that, for a fixed OSNR of 13 dB and for a fiber length between 150 km and 300 km, the optical data link is not feasible without dispersion management, which can be solved by using the proposed DCM.

3.3 Signaling in optical networks

Provisioning in a network is controlled through the MP. A similar function to provisioning using automatic configuration refers to signaling, which is a feature of the CP. In a PON, the adoption of EDFAs in the Central Office (CO), where the Optical Line Terminals (OLTs) are placed, can be used for signaling and monitoring purposes.

The experimental setup to evaluate the performance of this signaling technique for PONs is depicted in Fig. 11. An External Cavity Laser (ECL), tuned at 1,537 nm is externally

modulated at 10 Gbit/s rate by a 231-1 PRBS signal. The 980 nm diode pump (SDL0 2596) is directly modulated up to 60 Mb/s by a 215-1 PRBS signal with a modulation depth of around 50%. A T-bias (100 kHz–1 GHz), not shown in figure provides biasing and signaling modulation. The bias current, at the laser working point, is 80 mA for an optical output power of 90 mW. In this condition the EDFA gain is 20 dB and its output power is 14 dBm at ECL wavelength. Both modulated signals are sent to a 2 km single mode fiber coil. This length has been demonstrated to be in Italy the average distance between the CO and the end user. The optical attenuators simulate the power reduction which is mainly caused by the splitter in a PON.

Figure 12b shows the BER curves, for the 10 Gbit/s signal, which have been taken in absence and in presence of the 50 Mb/s pump modulating signal. When the signaling at 50 Mb/s is applied, an increment of less than 0.4 dB is valuable mainly due to a pump current increase.

Figure 12a shows a comparison between BER values of laser pump signal modulation for three different cases (40, 50, and 60 Mb/s). Due to a non-perfect equalization system, tuned for 60 Mb/s data rates, it can be noticed a power penalty of around 3 dB from 40 Mb/s and 60 Mb/s cases. Error-free conditions have been achieved.

4 Implementation viability

In this section, the impact of the implementation of transparency in the MP and CP of core optical networks, from the operator perspective, is discussed.

Fig. 11 Experimental setup for performance evaluation of signaling in PONs

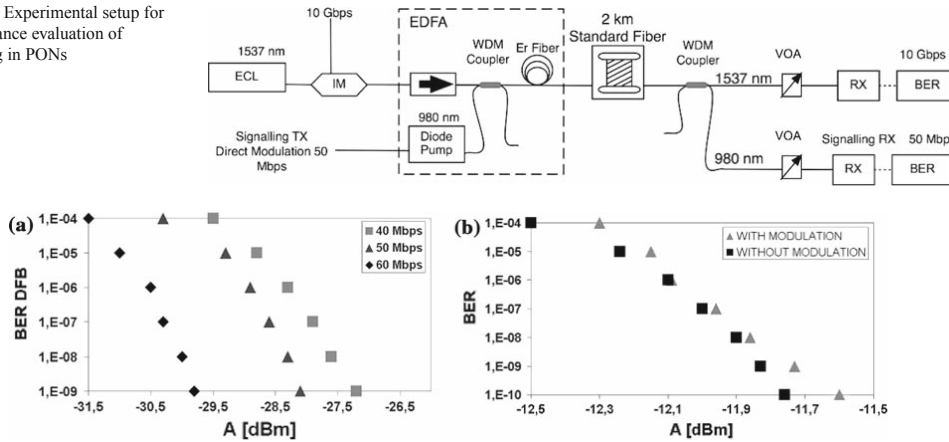


Fig. 12 a BER EDFA diode pump; b BER 10 Gbit/s modulated signal in two cases: EDFA diode pump modulation ON and OFF

4.1 Management from the operator point of view

4.1.1 Performance management

In opaque networks, each NE management system collects information for quality assessment, NE performance, and traffic control, among others. Transparency implies a decrease of the amount of information collected through O/E/O conversion in nodes, which typically concerns QoT, channel identification and channel overhead bytes. Since QoT is measured on an end-to-end basis, it is not clear if the absence of intermediate BER alike measurement at node sites should be complemented by additional OPM functions. Nevertheless, a communication channel is indispensable for proper network operation, whether it is out of channel (e.g., using an OSC channel [43]) or out of band. If intermediate QoT monitoring is required, we expect it to be very closely correlated to classical BER measurement. Since the latter would only work for a specific bit rate, modulation format, and vendor, Q-factor monitoring could be an alternative as long as the equivalence with BER is guaranteed. However, both approaches require CD or power adjustments in order to be accurate. Hence the transparent system design should be adapted accordingly.

4.1.2 Fault management

In transparent networks, performance may only be end-to-end monitored which has an important impact on fault detection (FD), fault localization (FL), and fault management in general. Moreover, the elaboration of large transparency domains causes vulnerability to fault propagation [44]. As such, system vendors will probably adapt transmission systems and node equipments to avoid it. Again, it is not clear if the use of adequate FL algorithms based on alarm correlation [44] may be sufficient. However, convergence time of such algorithms may dramatically increase within transparency domain, and OPM may help to significantly reduce it. In an opaque network, simple parameters commonly measured are the aggregated power in amplification sites, and the channel power at both ends and possibly in equalization sites. In transparent networks the channel power should be monitored in each node crossed, and the other monitoring points should be the same as in opaque networks.

4.1.3 Configuration management

Parameters commonly monitored in current point-to-point transmission systems may not be sufficient for both commissioning and provisioning in transparent systems. They are typically: (i) total input/output power of optical amplifier for pump and gain control; (ii) channel power in gain equaliza-

tion sites or ROADM; (iii) channel power at transmitter output for laser current control; and (iv) transmitter wavelength drift for wavelength locking. OSNR measurement is not a usual feature, but is mandatory for system commissioning.

Commissioning On the physical point of view, transparent transmission systems have additional engineering constraints due to the aggregation of multiple channels with different histories. This feature is already treated in ROADM systems, and during system design and commissioning stages: all possible paths are tested and validated and no additional OPM is required. In the transparent network scenario, the number of possible paths increases exponentially, so their full validation may not be feasible. Instead, systems may rely on automatic procedures with adequate feedback information. Thus, we may suppose that as OSNR measurement is required for traditional system commissioning, then it should also be for installation of new systems. So, OPM with OSNR monitoring would be required in nodes and used punctually to validate lightpaths.

Provisioning A network configuration based on NE database information is required to deliver a transparent network capable of capacity provisioning on demand. This could be difficult to implement, since channel information is reduced to partial analogue information, such as wavelength and OSNR. Configuration also requires using the data communication network. Moreover, the notion of neighbors is not as straightforward as in opaque networks: physical impairments may not allow error-free transmission on a transparent lightpath, although the physical medium exists. Thus, OPM could help to determine physical feasibility of paths, by using a power monitor on each cross-connect ports or perform Q measurement of a test. However, extensive OPM implementation may be expensive and alternative solutions are to rely on Q estimators based on databases or to find new procedures based on successive path testing [45].

4.2 Control plane

Main functions of the CP are neighbor discovery, routing, signaling, and local resource management [46]. We estimate that the first two may be impacted by transparency [47].

Neighbor discovery determines NE connectivity to their neighbors. A link management protocol (LMP) is being standardized by IETF for this purpose. LMP has been designed to accommodate all-optical switches. However, the procedure may not work in service for the case of fully transparent switches. The notion of neighbor may also need to include physical feasibility verification which is not necessary in opaque networks. The short description of LMP in [46] shows that the protocol needs at least power detection at node interfaces, which could be performed by power monitors.

Topology discovery and path computing should only include feasible paths based on (a) the wavelength avail-

ability related to the RWA problem, and (b) the impairment point of view related to the CB-RWA problem. Q-factor estimation based on database stocking of all necessary parameters needed for the computation [48] is proposed as one way of including both approaches. Still, the physical feasibility problem raises issues like the estimation reliability for time-varying parameters which are considered static, and the complex dynamic update of huge databases. In opaque scenarios, the problem is solved during the installation stage of point-to-point systems.

4.3 Operator infrastructure constraints

In the context of dynamic lightpath establishment, the physical feasibility problem can be solved either by relying on estimators and physical parameter databases or on physical tests, as long as the method is reliable. To do so margins are usually set to mask eventual accuracy problems. The resulting trade-off between the amount of margins and the estimation accuracy translates into a cost trade-off between the number of rejected paths due to insufficient quality and the implementation of multiple OPMs. In the following section, we have evaluated this trade-off in the context of France Telecom network, for different scenarios of OPM implementation: (i) test traffic matrices forecasted for 2010, (ii) European size network, (iii) with Table 7, and (iv) with simple estimator.

4.4 Analysis of OPM needs for QoT computation

We analyze the impact of OPM on the feasibility estimation reliability, with focus on the effect of more or less precise measurement points in an operational network, rather than on the exact sources of uncertainties which cause estimation errors. The estimator is assumed to be reliable, i.e., a positive estimation guarantees path feasibility. A negative estimation does not mean the opposite, but depends on the confidence degree of the estimator, which is out of the scope of this paper.

Table 7 Studied network topology

Network size	68 nodes	99 links	
Maximum shortest path	16 hops	5499 km	
	Average	Minimum	Maximum
Link length	321 km	16 km	700 km
	3 spans	1 span	11 spans
Span length	77.1 km	16 km	109 km
Node degree	2.91	2	7

4.4.1 Description of the model and network

We consider an OSNR-based estimator, similar to [49]. In this model, OSNR represents the QoT and some degradations which are translated into penalties on the OSNR value. Penalties are due to nonlinear phase shift (PhiNL) [50], PMD, and CD. Conditions for positive estimation are $OSNR \geq OSNR_{\min} + Penalties$ and $PhiNL \leq PhiNL_{\max}$ [51]. The exact values of $OSNR_{\min}$, $PhiNL_{\max}$, and the maximum allowed amount of penalties depend on the studied transmission equipments. We have restricted the study to classical WDM transmission at 10 Gbit/s with NRZ modulation format, with performances representative of current ultra long haul commercialized transmission systems. Studies are performed on a European backbone type network with 68 nodes and 99 links. All links are equipped with multiple fibers Table 7 summarizes the main characteristics of the topology.

4.4.2 Simulation assumptions

OPM is pointed as a solution to solve parameter estimation inaccuracy and network diversity. To consider the latter we assume that: PMD, CD, and attenuation follow a distribution identical to the existing fiber infrastructure; fiber nonlinear parameters (nonlinear index n_2 , and effective area A_{eff}) follow a bounded uniform distribution with standard deviation corresponding to the one observed in the field for G.652 fibers and amplifier gain and noise parameters are drawn randomly using a Gaussian distribution.

We focus on power and noise uncertainties introduced by amplifiers. Power uncertainty comes mainly from gain ripples of amplifiers. Raman tilt, and PDL. Raman tilt and wavelength dependence of fiber loss are supposed to be perfectly corrected by amplifiers. Noise uncertainty only depends on amplifier noise ripples. PMD, CD, n_2 , A_{eff} , and loss uncertainties are neglected. Usually in order to guarantee performances in spite of uncertainties, QoT estimators include margins, whose amount depends on equipment quality. We first suppose that no margins have been included. Latter, we add margins to the estimator threshold in order to compensate for uncertainties.

To evaluate the impact of power uncertainty on OSNR and PhiNL shift estimations, we simulate an artificial situation, where lightpath performance parameters (OSNR, CD, PMD, and PhiNL) are deduced from off-line measurements, possibly monitored along the path, and used for QoT feasibility estimation. Then we count the number of accepted paths using this estimation. This supposes that the lightpath to monitor exists prior to establishment (e.g., using a test wavelength) or that measurements are collected on neighboring lightpaths having the same route. Situation where no lightpaths are available for monitoring is similar to off-line

measurement. QoT is estimated for a selection of around 1,000 different paths between 500 km and 1,500 km (system reach is around 1,300 km) using two distinct network parameter databases: real represents the network parameters state as if they could be measured exactly, whereas measured represents a mix of measurement, monitoring, and estimation of the first database with accuracy dependent on OPM scenarios. Using the flowchart illustrated on Fig. 13, we calculate the number of accepted or rejected paths with both databases and identify the main sources of discrepancies. Ideally both databases should lead to the same decision for rejecting a path. Simulation results show instead that estimation based on the measured database leads to wrong decision due to over-estimated (measured Q is over the threshold and real Q is under the threshold) or under-estimated real performances. Performance is guaranteed when no path is over-estimated.

The description of the considered OPM scenarios follows. We assume the existence of a database of all required parameters based on measurement and completed with inline OPM data. The reference scenario uses only standard total input/output power monitoring. Power measurement performed by these OPM is also collected for path QoT computation. The expected average channel power in amplification sites is computed through the number of channels crossing the amplifiers. For all scenarios, we consider channel power in gain equalization sites or in ROADMs, and at transmitter output to be measured by embedded OPMS. Channel wavelength drift is not considered.

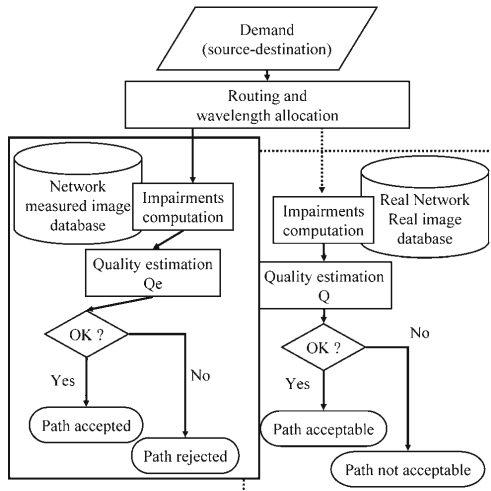


Fig. 13 Simulation set up flowchart

Beside the reference scenario, three optional situations are evaluated: (i) OSNR monitoring at every node input, (ii) channel power monitoring in every amplifier, and (iii) both simultaneously. In all four scenarios we vary measurement accuracy, which is identical for all measurement devices. Averaged values of 40 amplifier configuration were used.

4.4.3 Simulation results

Figure 14 shows that all OPM scenarios perform better when OPM accuracy is below 1 dB. Accuracy on channel power has also less impact on the percentage of badly estimated paths, due to the fact that the error is distributed along the paths for OSNR computation. As a result the error is averaged and as the distribution of power uncertainty is randomly distributed around its mean value, the error on computed OSNR tends to zero for a sufficient high number of measurement points or amplification spans. Reversely, when OSNR monitoring is used, only one measurement at the receiver is used for final QoT estimation and the full inaccuracy is translated on that estimation. Gaussian distribution of amplifier gain ripples is however an optimistic situation. Indeed, operators often select a single equipment type for several links, and then, amplifier on a given link may show similar behavior and gain ripples. Then the error distribution along the path may not be zero in average.

When using both OSNR and channel power monitoring, the percentage of badly estimated paths, when OPM accuracy is ± 0.1 dB is reduced by a factor of 3. Using OSNR monitoring with a bad accuracy may even perform worse than the reference scenario due to the localized error. Even in the best scenario, there is still a non-negligible percentage of paths that are over-estimated, around 1.5%. This percentage should reach zero in order to guarantee performance.

Figure 15 first shows that the increase of the margins results in a higher number of under-estimated lightpaths (from around 1% when no margin is applied to more than

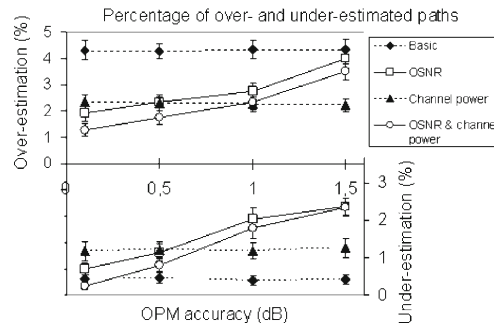


Fig. 14 Percentage of wrong decisions for over- and under-estimations

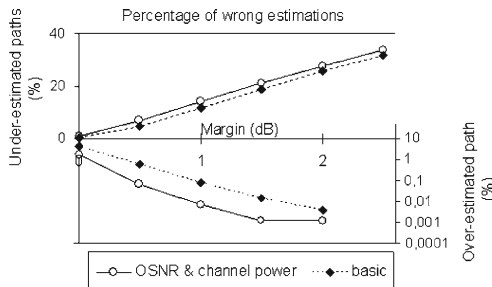


Fig. 15 Percentage of over- and under-estimations as a function of margin

30% with 2.5 dB margin). Figure 15 also shows that the improvement provided by OPM is canceled when margins are used, because bare estimation is slightly optimistic compared to OPM scenarios.

A minimum of 2.5 dB margin is required to guarantee performance at the expense of a huge amount of rejected paths, which means that route should be either changed to an acceptable path, or one regenerator should be at least used. Thus, a 2.5 dB margin represents around 350 additional regenerators as compared to a 0 dB margin.

We conclude that a precise OPM strategy provides better results than bare parameter estimation when power uncertainties are considered. The integration of additional margins for uncertainties allows reducing the percentage of over-estimated lightpaths, but increases the overall number of rejected paths: estimation then performs equally well as monitoring. However, estimation relies on a database, which may not exist due to operational reasons or to a multi-domain configuration. In this case, monitoring would be the only alternative. If other uncertainties are considered (e.g., PMD [52] or CD uncertainty [53]), and especially if errors are not randomly equally distributed around an average value, an increased amount of margins will be needed, which may be reduced thanks to the use of adequate monitoring.

5 Conclusion

The need to explore and identify more suitable M&C methods to incorporate in WDM networks in general can be solved by taking into account the impact of physical impairments in the network performance, ranging from physical to management layer issues, under an integrated perspective [54].

In this paper we came to the conclusion that impairment-free or optimum network performance would be difficult to achieve. Instead, stable performance could be a good compromise when dynamic wavelength assignment and routing is considered. To envisage the exact operation conditions prior

to the occurrence of new network events on time would imply unfeasible allocation of computational resources and time expenditure. A simpler, more reliable, and efficient solution is to monitor the impact of those events and react cautiously, rather than just using complex, sophisticated, and heavy algorithms to predict everything.

The advantages of this complementary approach are also confirmed in Sect. 4. We concluded that intensive use of different monitoring functions throughout the network would probably have undesired consequences on equipment cost, and would essentially rely on used transmission parameters, like bit rate. However, to rely only on margins would greatly reduce the interest for the implementation of transparent domains. As such, a fair combination of margin, estimation, and monitoring can be a better strategy.

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Author Biographies



Aveiro. His research interests include DWDM optical networks, dispersion compensation, fiber Bragg gratings, and radio over fiber technologies. He is member of the Institute of Electrical and Electronics Engineers (IEEE) and of the Optical Society of America (OSA).

A. Teixeira was born in Portugal, on November 17, 1970. He received the Licenciatura degree in Electronics Engineering and Telecommunications, in July of 1994 and the PhD degree in Electrical Engineering, in 1999, all from the University of Aveiro, Portugal. He is currently an Assistant Professor at the Department of Electronics, Telecommunications and Informatics of the University of Aveiro and researcher at the Institute of Telecommunications—



L. Costa was born in Portugal, on August 1, 1984. She received the Licenciatura degree in Electronics Engineering and Telecommunications, in July of 2007. Since then she is working in the Instituto de Telecomunicações in Aveiro, Portugal. Her research interests include semiconductor optical amplifier technologies and applications and optical monitoring techniques. She has been participating in FP6 ePhotonOne+ and FP7 SARDANA and EURO-FOS EU funded projects.



for the professional broadcast industry. Since 2003 he contributes to the Institute of Broadband Communications at the Vienna University of Technology within his PhD program participating in several national and EU funded projects. His current research interests are in the area of optical networks and traffic engineering, focusing on QoS sensitive routing schemes and end-to-end performance evaluation based on queuing models.

G. Franzl received the academic degree Dipl.-Ing. in Electrical Engineering, specialized in Communications Engineering and Information Processing, from the Vienna University of Technology, Austria, in 2002. From February 2004 till June 2007 he was employed first as R&D assistant lately as technical product manager at MEDIORNET GmbH, a startup company in Vienna, closed in June 2007, developing a fiber-based content distribution network (X-Switch)



Atlanta Information Technology as a researcher, while also pursuing a PhD He is a professional member of ACM and a student member of IEEE.

S. Azodolmolky received his computer hardware (B.Eng.) degree from Tehran University in Iran in 1994 and his first master degree (M.Eng.) in computer architecture from Azad University, in 1998. He has worked with the Data Processing Iran (ex-IBM), as a Systems Engineer and Senior R&D Engineer during 1992–2001. He received his second M.Sc. degree with distinction from the Information Networking Institute of the Carnegie Mellon University, in 2006. In August 2007 he joined



I. Tomkos has the rank of Full Professor at Athens Information Technology Center, serves as its Associate Dean (since 2004), and is an Adjunct Faculty at the Information Networking Institute of Carnegie-Mellon University, USA. In the past (1999–2002) he held a senior scientist position at Corning Inc. USA. He joined AIT in 2002 where he founded and serves as the Head of the “High Speed Networks and Optical Communication (NOC)”

Research Group that participates in many EU funded research projects (including 5 running FP7 projects) in which Dr. Tomkos is representing AIT as Principal Investigator and has a consortium-wide leading role (e.g. Project Leader of the EU ICT STREP project DICONET, Technical Manager of the EU IST STREP project TRIUMPH, Chairman of the EU COST 291 project, WP leader). Dr. Tomkos has received the prestigious title of “Distinguished Lecturer” of IEEE Communications Society for the topic of transparent optical networking. Together with his colleagues and students he has authored more than 200 peer-reviewed articles and his work has received over 600 citations. Dr. Tomkos has served as the Chair of the International Optical Networking Technical Committee of IEEE Communications Society and a member of the IEEE ComSoc’s Technical Activities Council. He is currently the Chairman of the OSA Technical Group on Optical Communications and the Chairman of the IFIP working group on “Photonic Networking”. He has been General Chair, Technical Program Chair, and member of the steering/organizing committees for the major conferences (e.g. OFC, ECOC, IEEE GlobeCom, IEEE ICC, etc.) in the area of telecommunications/networking (more than 50 conferences/workshops). In addition he is a member of the Editorial Boards of the IEEE/OSA Journal of Lightwave Technology, the OSA Journal of Optical Networking, the IET Journal on Optoelectronics, and the International Journal on Telecommunications Management.



K. Vlachos received his Dipl.-Ing. degree in electrical and computer engineering from the National University of Athens (NTUA), Greece, in 1998 and his Ph.D. in electrical and computer engineering, also from NTUA, in 2001. From 1997 to 2001 he was a senior research associate in the Photonics Communications Research Laboratory (ICCS/NTUA). In April 2001 he joined Bell Laboratories, Lucent Technologies, working on behalf of the Applied Photonics Group. Prof. Vlachos conducted

research on high-speed optical networks and DWDM transmission techniques. During 2003, he joined the National Regulation Authority of Telecommunication and Postal Service of Greece (EETT), where he served as a scientific advisor for various techno-economic issues for the promotion of broadband technologies. Since 2003, he was also a member of Computer Engineering laboratory of Technical University of Delft and since 2005, a faculty member of Computer Engineering and Informatics Department of Uni-

versity of Patras, Greece. His research interests are in the areas of high-speed protocols and technologies for broadband, high-speed networks, optical packet/burst switching, and grid networks. Prof. Vlachos has participated in various research project funded by the European Commission (IST-STOLAS, IST-PRO3, ESPRIT-DOALL, e-photon/ONe+, IST-PHOSPHROUS, ICT-BONE και ICT-DICONET). Prof. Vlachos is a member of IEEE and the Technical Chamber of Greece and he periodically acts as a scientific reviewer for the General Secretariat for Research and Technology of Greece (GSRT) as well as for the European Commission and the Netherlander Organization for Scientific Research, Technology Foundation. Prof. Vlachos is the (co) author of more than 70 journal and conference publications and holds five patents.



S. Zsigmond has received M.Sc. ('04) degree in physics from the Budapest University of Technology and Economics (BME), Hungary, where he is currently consultant manager at the Department of Telecommunications and Media Informatics. His research interests focus on all optical networks, physical effects of the optical networks, PMD, optical switching architectures, impairments constraint-based routing. He is author of several refereed scientific publications. He has

been involved in numerous related European and Hungarian projects including COST 291, NoE e-Photon/One, and NoE e-Photon/One+; CELTIC PROMISE; NKFP.



T. Cinkler has received M.Sc. ('94) and PhD ('99) degrees from the Budapest University of Technology and Economics (BME), Hungary, where he is currently associate professor at the Department of Telecommunications and Media Informatics. His research interests focus on optimization of routing, traffic engineering, design, configuration dimensioning and resilience of IP, Ethernet, MPLS, ngSDH, OTN, and particularly of heterogeneous GMPLS-controlled WDM-based

multilayer networks. He is author of over 180 refereed scientific publications and of 4 patents. He has been involved in numerous related European and Hungarian projects including ACTS METON and DEMON; COST 266, 291, 293; IP NOBEL I and II and MUSE; NoE e-Photon/One, e-Photon/One+ and BONE; CELTIC PROMISE and Tiger II; NKFP, GVOP, ETIK; and he is member of ONDM, DRCN, BroadNets, AccessNets, IEEE ICC and Globecom, EUNICE, CHINACOM, Networks, WynSys, ICTON, etc. scientific and Program Committees. He has been guest editor of a Feature Topic of the IEEE ComMag and reviewer for many journals and conferences.



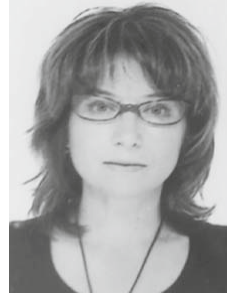
G. Tosi-Beleffi has an experience of 8 years in optical technologies, devices, architectures, systems and subsystems, wired and wireless, for the Metro and Access telecommunication sectors as part of the Next Generation Broadband Network. Dr. Tosi Beleffi has solid skills in scientific research and management activities, in coordination activities at EU level with participation at EU co funded projects and COST actions. Participation to FP5 ATLAS, FP6

ePhotonOne/ePhotonOne+, FP7 BONE, and SARDANA projects. Italian Delegate of COST MP0702 on integrated devices. Didactics performed with courses and seminars at Italian and foreign Universities. Member of IEEE Leos and OSA international societies. TPC member of IEEE ICTON, IEEE ICT, and CONTEL international conferences. Member of Euro-Japan ICT and Euro-SouthKorea communities. Chairman of IEEE ICTON 2007 conference and Chairman of Market in TLC session (IEEE ICTON Conference). Dr. Tosi Beleffi is author of 18 publications on international journals and of more than 40 publications on national and international conferences. Patent on all optical regeneration (WO 2005/109080 A1). Interactions and joint activities/missions performed in foreign countries like Portugal, Japan, Czech Republic, Greece, Spain, UK.



P. Gravey graduated from Ecole Polytechnique (Palaiseau—France) in 1978, from Ecole Nationale Supérieure des Télécommunications (Paris—France) in 1980 and received a Diplôme d'Etudes Approfondies in Optics (Orsay—France), also in 1980. He then joined the Centre National d'Etudes des Télécommunications (now Orange Labs) in Lannion to work on holographic techniques and materials applied to optical interconnections.

Between 1993 and 1997, he was in charge of the "Photonic Switching Processors" department, and then conducted a project on Optical Cross-connects. He was also involved in European Projects on Optical Switching and Optical Packet Switching. In 2000, he joined the Optics Department of TELECOM Bretagne and co-founded the Optogone company in 2001, which developed liquid crystal-based devices for WDM applications. He returned to the Optics department in 2005. His present research interests include access and optical packet networks and monitoring. He authored or co-authored more than 80 publications or communications and 8 patents.



T. Loukina graduated from Kazan State University (Russia) in 1984. During 15 years she worked on diffractive holographic optical components and volume holography: design, fabrication, test benches (PhD on optical holographic elements, 1999, Moscow) in State Institute of Applied Optics (Russia). Since 1999 she works in optical communications domain (Ph.D. on diffractive optics and spectral equalization for DWDM systems in TELECOM Bretagne, 2003, Brest). Between 2002 and 2004 she was

with Optogone SA where she brought a major contribution to the development of a free-space Dynamic Gain Equalizer. Since 2005, she is working on the Perdyn platform, dedicated to advanced WDM functions and access networks and she led a project on a free-space Optical Performance Monitor. Her research interests include holography and optical monitoring. She authored or co-authored more than 25 publications or communications.



J. A. Lázaro received the M.Sc. degree in physics in 1993 and the PhD degree from the University of Zaragoza (Spain) in 1999 for his research work in Erbium Doped Waveguide Amplifier (EDWA). He is currently Ramon y-Cajal Researcher at the Optical Communications Group of the Department of Signal Theory and Communications of the Universitat Politècnica de Catalunya (UPC), teaching at the ETSETB Engineering School of UPC in Barcelona, and the Master in Photonics "PhotonicsBCN".

Prior to this position, he was Senior Researcher at the Optical Transmission and Broadband Technologies Laboratory of the Aragon Institute for Engineering Research (I3A) in Huesca (Spain) and R&D Engineer in ALCATEL in Stuttgart (Germany) at the Department of Passive Optical Components (2000–2002), and at the Department Optical Transmission Systems (2002–2004). He has been participating in several European projects (e-Photon/One, BONE, EURO-FOS, and SARDANA) on optical transmission, monitoring, subsystems, and access networks.



C. Vazquez (M'99–SM'05) was born in Madrid, Spain, on May 1968. She received the M.S. degree in Physics (Electronics) in 1991 from Complutense University of Madrid, and her Ph.D. degree at Telecommunications Engineering School in 1995 from Polytechnic University of Madrid (UPM). In 1991 she enjoys a fellow at TELECOM (Denmark), working in erbium doped fiber amplifiers. From 1992 to October 1995 she worked at Optoelectronics Division of "Telefnica Investigacin y Desarrollo". She was involved in III/V integrated optics devices. In October 1995, she joined Carlos III University of Madrid where she is currently working as an Associate Professor, leader of the Photonics Applications Group, Vice-rector of Quality, Infrastructures and Environment, and has been Head of the Electronics Technology Department for 3 years. Her current work includes optical signal processing, ring resonators, plastic optical fibers broadband access networks, RoF systems, filters switches, fiber sensors design of fiber optics, LC and integrated optic devices and their application to optical communications, instrumentation and sensor networks. She has published more than 140 papers in journals and conferences. She won the extraordinary doctorate prize of UPM in 1995 and biannual prize for young professor at UC3 M in 2004. She participates as leader and researcher in Spanish and European Research Projects in Photonics. She is a member of SPIE, OSA, and SEO.



J. Montalvo was born in Madrid, Spain, on May 1979. He received his M.S. Degree in Telecommunication Engineering in January 2003 from Polytechnic University of Madrid (UPM) and obtained his PhD Degree in Electrical, Electronics and Robotics Engineering in April 2008 from Carlos III University of Madrid (UC3 M). As a member of the Displays and Photonics Applications Group at UC3 M, his research work is involved in optic filter and devices design and characterization for Coarse and Dense Wavelength Division Multiplexed (WDM) networks for sensors and broadband access. Currently he is also working in the Telecommunications Industry on Optical Broadband Networks for Telefnica Research and Development.



E. Le Rouzic received the telecommunications degree from Ecole Nationale Supérieure des Télécommunications de Bretagne, France, the M.Sc. degree from the University College London, U.K., in 1996, and the PhD degree in electronics and communications from Ecole Nationale Supérieure des Télécommunications, France, in 1999. She joined France Telecom R&D in Lannion in 2000, where she has been working on wavelength division multiplexing (WDM) networks, optical functions, optical transmission, and translucent networks. She is involved in national and European projects dealing with optics and authored about 25 national or international papers or communications.