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1 **Reaction kinetics and oxidation product formation in the degradation of**  
2 **acetaminophen by ferrate (VI)**

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21

22 **Abstract**

23 This paper investigates the degradation of acetaminophen (AAP) in aqueous solutions  
24 by ferrate (VI), aiming to propose the kinetics, pathways and the oxidation products'  
25 formation in the AAP degradation. A series of jar tests were undertaken over ferrate  
26 (VI) dosages (molar ratios of ferrate (VI):AAP, 5:1 to 25:1) and pH values (4~11).  
27 The effects of co-existing ions (0.2~5 mM) and humic acid (10~50 mg·l<sup>-1</sup>) on the  
28 AAP removal were investigated. Ferrate (VI) can remove 99.6 % AAP (from 1000  
29 µg·l<sup>-1</sup>) in 60 minutes under study conditions when majority of the AAP reduction  
30 occurred in the first 5 minutes. The treatment performance depended on the  
31 ferrate(VI) dosage, pH and the type and strength of co-existing ions and humic acid.  
32 Raising ferrate (VI) dosage with optimal pH 7 improved the AAP degradation. In the  
33 presence of humic acid, the AAP degradation by ferrate (VI) was promoted in a short  
34 period (< 30 min) but then inhibited with increasing in humic acid contents. The  
35 presence of Al<sup>3+</sup>, CO<sub>3</sub><sup>2-</sup> and PO<sub>4</sub><sup>3-</sup> ions declined but the existence of K<sup>+</sup>, Na<sup>+</sup>, Mg<sup>2+</sup> and  
36 Ca<sup>2+</sup> ions can improve the AAP removal. The catalytic function of Al<sup>3+</sup> on the  
37 decomposition of ferrate (VI) in aqueous solution was found.

38 The kinetics of the reaction between ferrate (VI) and AAP was pseudo first-order  
39 for ferrete (VI) and pseudo second-order for AAP. The pseudo rate constant of ferrate  
40 (VI) with AAP was 1.4x10<sup>-5</sup> L<sup>2</sup>·mg<sup>-2</sup>·min<sup>-1</sup>. Three oxidation products (OPs) were  
41 identified and the AAP degradation pathways were proposed.

42 *Keywords:* Potassium ferrate (VI); Acetaminophen; Reaction mechanism; Influence  
43 factors; Oxidation products

44

## 45 **1. Introduction**

46 In recent years, pharmaceutical and personal care products (PPCPs) have been  
47 detected in numerous water resources (Boyd et al., 2003; Kim et al., 2009; Liu and  
48 Wong, 2013). The potential hazard toward aquatic organisms and public health (Fent  
49 et al., 2006; Crane et al., 2006; Witorsch and Thomas, 2010) resulting from increasing  
50 PPCPs concentrations, and the incomplete removal of PPCPs has been found in  
51 various conventional wastewater treatment plants (Boyd et al., 2003; Khetan and  
52 Collins, 2007). As a typical anti-inflammatory and analgesic medication,  
53 acetaminophen (AAP) is produced and consumed about  $1.45 \times 10^5$  tons per year  
54 worldwide (Kasprzyk-Horderna et al., 2008). AAP has high solubility up to 12.78  
55  $\text{g} \cdot \text{kg}^{-1}$  in aqueous solutions at 20 °C, and has been detected frequently in water courses  
56 (Granberg and Rasmuson, 1999). More than 65  $\mu\text{g}/\text{L}$  of acetaminophen has been  
57 detected in surface water and the concentration of acetaminophen might be much  
58 higher in pharmaceutical industry wastewater (Roberts and Thomas, 2006). Research  
59 has shown that AAP had toxicity on bivalve *Dreissena polymorpha* (Parolini et al.,  
60 2013).

61 Due to the possession of dual functions of oxidation and coagulation, ferrate (VI)  
62 has been studied widely and demonstrated to be a very promising chemical for both  
63 water and waste water treatment (Jiang and Lloyd, 2002; Lee et al., 2004; Jiang et al.,  
64 2006). The elimination of PPCPs by ferrate (VI) has been conducted by many  
65 researchers (e.g., Yang et al., 2012; Jiang et al., 2013; Jiang, 2014; Sharma et al.,  
66 2015). So far, the degradation of AAP has been reported by anodic oxidation with a

67 boron-doped diamond electrode (Brillas et al., 2005), subsurface flow constructed  
68 wetlands (Ranieri et al., 2011), ozonation and H<sub>2</sub>O<sub>2</sub>/UV system (Andreozzi et al.,  
69 2003), Photo-Fenton process (Trovo et al., 2008) and TiO<sub>2</sub> photocatalysis (Yang et al.,  
70 2008). However, to the best of our knowledge, the study on the degradation of AAP  
71 using ferrate (VI) has not been reported so far.

72 And thus, this study focused on the removal of AAP in aqueous solutions by  
73 ferrate (VI). Conditions of the degradation of AAP were investigated with respect to  
74 ferrate (VI) dosage, pH value, and the presence of humic acid and various co-existing  
75 ions (K<sup>+</sup>, Na<sup>+</sup>, Mg<sup>2+</sup>, Ca<sup>2+</sup>, Al<sup>3+</sup>, CO<sub>3</sub><sup>2-</sup>, SO<sub>4</sub><sup>2-</sup>, PO<sub>4</sub><sup>3-</sup>). The study also aimed to reveal  
76 oxidation products (OPs) and kinetics for the degradation of AAP by ferrate (VI).

77

## 78 **2. Experimental section**

### 79 *2.1 Chemicals and reagents*

80 Acetaminophen (AAP) was purchased from aladdin (Shanghai, China); Sodium  
81 hydroxide, methanol (LC) and potassium hydroxide (AR) were purchased from  
82 Hangzhou Xiaoshan Chemical Reagent Factory (Hangzhou, China); Humic acid (HA)  
83 was obtained from Nanjing Chemical Reagent Factory (Nanjing, China). Ferrate (VI)  
84 solution of high concentration was synthesized by the electro-chemical way (Wang et  
85 al., 2015), and then transferred to solid potassium ferrate (VI) after various  
86 purification steps (Li et al., 2005). The ferrate(VI) strength of the resulting dry  
87 product was measured by chromite method and direct spectrophotometric method

88 using a wavelength of 505 nm and an absorbance coefficient of  $1100 \text{ M}^{-1} \cdot \text{cm}^{-1}$  (Jiang  
89 et al., 2009). The purity of ferrate (VI) was continuously monitored on the daily basis.  
90 The other reagents were supplied by Sinopharm Chemical Reagent Co. Ltd.  
91 (Shanghai, China). Experimental water was generated by ultra pure water supplier  
92 (UPHW1-90T, Sichuan europtronic ultra pure Technology Co. Ltd., China). Stock  
93 solutions of AAP were prepared in pure water at  $100 \text{ mg} \cdot \text{l}^{-1}$  for the use of jar test  
94 experiments, identification of oxidation products and kinetic analysis.

## 95 *2.2 Jar test experiment*

96 The oxidation of AAP by ferrate (VI) was studied using a magnetic stirrer (Color  
97 squid, IKA (Guangzhou) equipment Co. Ltd, China) with a mixing speed of 600 rpm.  
98 Pipette (Shanghai Kangmin inspection equipment Co. Ltd, China) was used for  
99 sampling at given reaction time intervals; 1, 2, 5, 10, 20, 40 and 60 min, respectively,  
100 and sodium hyposulfite was used as a quencher.

101 In order to examine the formation of AAP oxidation product as well as to assess  
102 the degradation performance readily, two initial AAP concentrations, 500 and 1000  
103  $\mu\text{g} \cdot \text{l}^{-1}$  respectively, were used for the study. The selected AAP concentrations were  
104 also in line with that used by other researchers (e.g., Yang et al., 2008). The influence  
105 of operating conditions were investigated using 100 mL test solutions with initial AAP  
106 concentrations of  $1000 \mu\text{g} \cdot \text{l}^{-1}$  and by adjusting a number of ferrate (VI) dosages, pH  
107 values and HA concentrations. Ferrate (VI) was dosed into the test solution as dried  
108 powder and the dosage applied was in the molar ratio of ferrate (VI):AAP from 5:1 to  
109 25:1. The pH of test solutions was adjusted by 0.01 M hydrochloric acid and 0.01 M

110 sodium hydroxide to pH 4~11. The HA concentration in testing solutions was 10~50  
111  $\text{mg}\cdot\text{l}^{-1}$ .

112 Test solutions of 200 mL with AAP initial concentration of  $500\ \mu\text{g}\cdot\text{l}^{-1}$  were used  
113 to study the impact of the presence of 0.2~5 mM co-existing ions ( $\text{K}^+$ ,  $\text{Na}^+$ ,  $\text{Mg}^{2+}$ ,  
114  $\text{Ca}^{2+}$ ,  $\text{Al}^{3+}$ ,  $\text{CO}_3^{2-}$ ,  $\text{SO}_4^{2-}$ ,  $\text{PO}_4^{3-}$ ) on the AAP degradation performance by ferrate(VI).  
115 The AAP solutions were mixed with given amount of NaCl, KCl,  $\text{MgCl}_2$ ,  $\text{CaCl}_2$ ,  
116  $\text{Al}_2(\text{SO}_4)_3$ ,  $\text{Na}_2\text{CO}_3$ ,  $\text{Na}_2\text{SO}_4$  and  $\text{Na}_3\text{PO}_4$ , respectively, to achieve the required ion  
117 concentrations. The ferrate (VI) with dosage of the molar ratio of 28:1 (ferrate  
118 (VI):AAP) was mixed with the test solution and the sampling time was 0, 1, 2, 3, 5, 7  
119 and 15 min. All samples in jar test experiments were filtered by  $0.45\ \mu\text{m}$  glass  
120 membrane filters (Shanghai Xingya purifying material factory, China) before  
121 analyzing the residual AAP concentrations. The AAP concentration and removal  
122 percentage of each sample were detected by liquid chromatography (LC) (see sub-  
123 section 2.5).

### 124 *2.3 Identification of degradation products*

125 Test solutions of  $1000\ \mu\text{g}\cdot\text{l}^{-1}$  AAP were prepared in pure water. Ferrate (VI) was  
126 added to the solution of AAP with the molar ratio of 40:1. The samples were obtained  
127 after determined intervals, 0, 1, 5, 15, 30, 45 and 60 min. Detailed procedures of  
128 identification of AAP degradation products can be seen in sub-section 2.5.

### 129 *2.4 Kinetic analysis*

130 Kinetic analysis of AAP with ferrate (VI) was performed at room temperature

131 (20±2<sup>0</sup>C) under pseudo-first-order conditions with ferrate (VI) in excess. The test  
132 solutions of AAP were prepared in pure water. A given ferrate (VI) dose of 32.5 mg·l<sup>-1</sup>  
133 <sup>1</sup> was added into test solutions with AAP concentrations of 300, 500, 700, 900 µg·l<sup>-1</sup>  
134 respectively. On the other hand, several ferrate (VI) doses, 13, 19.5, 26, 32.5 mg·l<sup>-1</sup>  
135 respectively, were dosed into the test solutions with a given AAP concentration of  
136 1000 µg·l<sup>-1</sup>. For the given time intervals as stated above, the reacting solutions were  
137 quenched with sodium hyposulfite solution.

### 138 *2.5 Analytical methods*

139 The concentration of chemical oxygen demand (COD) of test solutions before  
140 and after ferrate (VI) treatment was measured by potassium dichromate method  
141 (APHA et al., 1998).

142 Ion chromatograph (ICS-900, Dionex, US), coupled with an anion column  
143 (IonPac AS19, 4×250 mm) and a flow rate of 0.8 mL·min<sup>-1</sup> of 20 mM KOH solution,  
144 was used for the measurement of inorganic ions' concentrations.

145 The measurement of AAP was conducted by an Agilent 1200 LC system  
146 (Agilent, US) with diode array detector (DAD). The column utilised for the separation  
147 of compounds was a 5 µm, 4.6×150 mm reversed phase Eclipse XDB-C18 column  
148 (Agilent, US). The column was kept at 30 °C and eluted by 15% methanol and 85%  
149 pure water at a flow rate of 0.8 mL·min<sup>-1</sup>. The injection volume was 10 µl and the  
150 DAD detection wavelength for AAP was 257 nm.

151 The oxidation products of AAP treated by ferrate (VI) were analyzed by a GC-  
152 MS system (Saturn, USA) equipped with an SE-54 capillary column (Chromse, UK).



153 For each GC-MS injection, samples were pretreated by hydrochloric acid of 1 M to  
154 pH<1 and then extracted with chloroform (10 times concentrated). The GC conditions  
155 were given as follows: a sample volume of 1  $\mu$ l injected in the splitless mode at 280  
156  $^{\circ}$ C and the oven temperature programmed from 50  $^{\circ}$ C (5 min) to 250  $^{\circ}$ C at 10  $^{\circ}$ C min $^{-1}$   
157 followed by a 5 min hold at 250  $^{\circ}$ C, and helium used as the carrier gas at a flow rate  
158 of 0.8 ml min $^{-1}$ . Mass spectrometer was operated under electron ionization mode at 70  
159 eV with mass scan range of 40~500.

160

### 161 **3. Results and discussion**

#### 162 *3.1. Effect of reaction time and ferrate (VI) dosage*

163

164 Fig. 1. Effect of reaction time and ferrate (VI) dosage on AAP degradation

165 Fig.1 shows the variation of AAP degradation efficiency vs. reaction time and  
166 ferrate (VI) dosages. The removal of AAP by ferrate (VI) mainly occurred within the  
167 first 5 min reactions, followed by a more gradual further removal over the next 10~  
168 55 min. Increasing in the ferrate (VI) dose (as molar ratio of ferrate (VI): AAP) from  
169 5:1 to 25:1, the removal efficiency of AAP increased sharply for the given time of 60  
170 min; that the AAP removal percentage was 50.5, 76.7, 96.9 and 99.6% for the molar  
171 ratio of 5:1, 10:1, 15:1 and 25:1, respectively. On the other hand, for a 10 min  
172 reaction and high ferrate(VI) dose (molar ratio of 25:1), approximate 90% AAP was  
173 removed. In general, ferrate (VI) could remove AAP readily under these conditions.

174            Additionally, COD concentration of the test solution with 10 mg AAP l<sup>-1</sup> was 31  
175 mg l<sup>-1</sup> and after ferrate(VI) treatment (ferrate (VI) dose of 0.325 g/L) the COD was  
176 reduced to 24 mg l<sup>-1</sup> which gives 23% COD reduction, representing the optimal COD  
177 reduction performance.

178

### 179    3.2. *Effect of pH*

180            Fig.2 shows the variation of AAP degradation efficiency vs. pH value and  
181 reaction time. It can be observed that for a given ferrate(VI) dose (25:1 as molar ratio,  
182 ferrate (VI):AAP) and pH 4, AAP removal was about 85% and irrelevant to the  
183 reaction time. For other pHs, AAP removal was less than 70% and pH 11 was not  
184 favorable to the APP removal especially for short reaction time; only 11.3% AAP was  
185 removed for the reaction time of 2 min at pH 11. On the other hand, increasing in  
186 reaction time was favorable to the AAP removal for pH 6-9; 60 min reaction gave the  
187 greatest AAP removal (99.95%) for pH 7. Moreover for pH 4 and 9, the degradation  
188 rate of AAP by ferrate (VI) increased rapidly at the initial reaction period (2 min) but  
189 approached to slight variations after 10 min.

190

191    Fig. 2. Effect of different pH values on AAP degradation

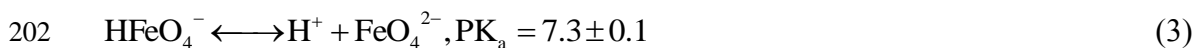
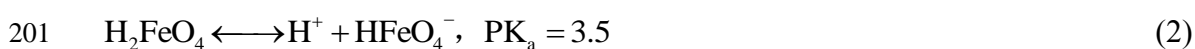
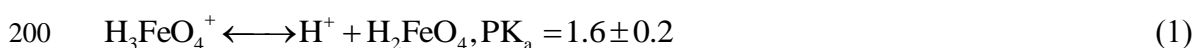
192

193            pH of test solution affects on the oxidation capacity and stability of ferrate (VI).

194    As shown in Fig. 2, degradation rate of AAP by ferrate(VI) at pH 4 was superior to

195 that at pH 11, since ferrate (VI) possesses higher redox potential (2.2 ev) under acidic  
196 conditions than that for alkaline conditions. Moreover, ferrate (VI) has been reported  
197 to be dissociated to form different species in terms of solution pH as shown in  
198 equations 1-3 (Sharma, 2002) and in Fig. S1 of the supplementary material.

199

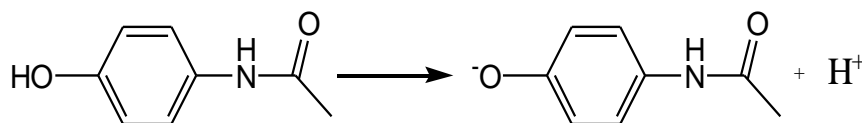


203

204 For pH 4 or less, major ferrate (VI) species are  $\text{H}_3\text{FeO}_4^+$ ,  $\text{H}_2\text{FeO}_4$  and  $\text{HFeO}_4^-$ ,  
205 which are readily self-decomposed, resulting in rapid oxidation of AAP which has  
206 been demonstrated in Fig. 2 where the AAP removal was about 85% and irrelevant to  
207 the reaction time. Relatively for pH 7, ferrate (VI) was stable and still had high  
208 oxidizing ability and then the best AAP removal performance was achieved for a long  
209 reaction duration (60 min).

210 The second effect of pH on the AAP degradation is attributed to the dissociating  
211 products of AAP. The  $\text{PK}_a$  of AAP was 9.5, and dissociating and/or protonated species  
212 could be dominant when pH was 9 (see equation 4). Fig. 2 shows that for pH 9, the  
213 AAP removal efficiency was high and it was close to that at pH 7. Hence, the results  
214 observed from this study demonstrated that high protonated AAP species were readily  
215 degraded by ferrate (VI), which is consistent with that from the reported work where  
216 solutions containing phenol and chlorinated phenols were treated by ozone and ferrate

217 (VI) (e.g., Graham et al., 2004).



(4)

### 221 3.3. Kinetics

222 The rate expression for the reaction of ferrate (VI) with AAP can be expressed as

223 
$$r = -d[\text{AAP}] \cdot dt^{-1} = -k \cdot [\text{Ferrate(VI)}]^a \cdot [\text{AAP}]^b \quad (5)$$

224 where  $r$  represents the reaction rate of ferrate (VI) with AAP,  $k$  represents the overall

225 rate constant of ferrate (VI) with AAP,  $a$  and  $b$  represent the orders of the reaction,

226  $[\text{Ferrate(VI)}]$  and  $[\text{AAP}]$  represent the concentrations of ferrate (VI) and AAP. The

227 kinetic studies were carried out under pseudo-order conditions with ferrate (VI) in

228 excess. Eq. (5) can be rewritten as

229 
$$r = k_1 \cdot [\text{AAP}]^b \quad (6)$$

230 Where

231 
$$k_1 = k \cdot [\text{Ferrate(VI)}]^a \quad (7)$$

232 Eq. (6) can be rewritten as

233 
$$\ln r = \ln k_1 + b \ln[\text{AAP}] \quad (8)$$

234 Eq. (7) can be rewritten as

235 
$$\ln k_1 = \ln k + a \ln[\text{Ferrate(VI)}] \quad (9)$$

236

237 Table1. Kinetic parameters of AAP degradation by ferrate (VI)

238

239 Table 1 shows the initial concentrations of AAP, ferrate (VI) dosage, fitting  
240 equations and initial reaction rate of AAP. It can be seen that the plot of the reciprocal  
241 of AAP concentrations versus reaction time were linear with good coefficient of  
242 correlation ( $R^2 > 0.90$ ) at various concentrations of ferrate (VI), indicating the reaction  
243 was second-order with respect to ferrate (VI). Moreover, the plot of the natural  
244 logarithm of AAP concentrations versus reaction time were linear with good  
245 correlation coefficient ( $R^2 > 0.90$ ) at various concentrations of AAP, indicating the  
246 reaction was first-order with respect to AAP. Although ferrate (VI) was unstable,  
247 ferrate (VI) was always in excess in comparison to AAP within the studied reaction  
248 time. The value  $a$  could be obtained as the slope of  $\ln r$  versus  $\ln[AAP]$  with linear  
249 fitting and the  $b$  is to be determined as the slope of  $\ln k_1$  versus  $\ln[Ferrate(VI)]$  with  
250 linear fitting, and this can be seen in Figure 3. Thus, the values of  $a$  and  $b$  are 1.2  
251 ( $R^2 = 0.999$ ) and 0.38 ( $R^2 = 0.939$ ), respectively. The apparent third-order rate constant  
252 ( $k$ ) for the reaction was calculated through the intercept in vertical axis. The value of  
253  $k$  is  $0.000014 \text{ L}^2 \cdot \text{mg}^{-2} \cdot \text{min}^{-1}$ . The observed rate law can be written in terms of both  
254 ferrate (VI) and AAP as

$$255 \quad r = -d[AAP]d_T^{-1} = -0.000014 \cdot [Ferrate(VI)]^{1.20} \cdot [AAP]^{0.38} \quad (10)$$

256

257 Fig. 3. Kinetic analysis of AAP degradation by ferrate (VI)

258

259 3.4. Oxidation products

260 Based on the measured m/z values and prior literature (Andreozi et al., 2003;  
261 Yang et al., 2009; Moctezuma et al., 2012), the best-fit chemical structures of  
262 oxidation products (OPs) were tentatively proposed by considering the molecule  
263 pattern of target compounds and the mechanism of ferrate (VI) oxidation; and the  
264 probable structures of OPs (AAP-1-3) are presented in Fig. 4. AAP would be attacked  
265 by ferrate (VI) which leads to the cleavage of imino group and the transformation of  
266 acetyl amino group, forming AAP-1 and AAP-2 respectively. The formation of AAP-3  
267 might attribute to further oxidation of intermediate OPs by ferrate (VI). Besides, the  
268  $\text{NO}_3^-$  was detected in the reaction solution which is consistent with previous studies  
269 (Skoumal et al., 2006; Yang et al., 2009), and suggests that the possibility of the  
270 broken of C-N bonds.

271

272 Fig. 4. Detection of oxidation products (a – c) and original compound, AAP (d)

273 Fig. 5. Evolution of OPs and nitrate with decreasing of AAP concentration

274

275 Fig. 5 shows the evolution of OPs and nitrate during the AAP degradation by  
276 ferrate (VI). As it can be observed, AAP-1-2 were formed from the first 1 min  
277 reaction, but almost disappeared, together with the AAP, after 60 min reactions. AAP-  
278 3 was detected after 15 min and trace nitrate ( $C_{\text{max}}=0.038 \text{ mg l}^{-1}$ ) was detected in the  
279 degradation process. These results also indicate that further oxidation of intermediate  
280 OPs by ferrate(VI) occurred.

281 Fig. 6 shows probable pathways of AAP degradation during the treatment by

282 ferrate (VI). The oxidation product, AAP-1, was formed with loss of a C<sub>2</sub>H<sub>4</sub>NO group  
283 from the benzene ring, and the pathway was different with the formation of  
284 hydroquinone (Skoumal et al., 2006; Tao et al., 2015) in other AAP degradation.  
285 AAP-2 was generated by replacing the hydroxyl group with a quinonyl group and the  
286 further loss of a C<sub>2</sub>H<sub>3</sub>O group from the imino group. In accordance with previous  
287 literature ( Skoumal et al., 2006; Yang et al., 2008; Moctezuma et al., 2012), AAP-3  
288 was also detected, which was a further oxidation product from AAP-1 (phenol).  
289 Reference to the prior knowledge (Santos, et al., 2002; Andreozzi et al., 2003; Wang  
290 et al., 2014), phenol would be oxidized into para-benzoquinone, which was then  
291 converted into maleic acid (AAP-3). The further degradation of AAP-3 could produce  
292 oxalic acid and formic acid (Santos, et al., 2002; Skoumal, et al., 2006). Besides, the  
293 formation of NO<sub>3</sub><sup>-</sup> is due to the deamination of AAP and AAP-2. The attack by  
294 ferrate(VI) on the hydroxyl and acetamido groups is consistent with the conclusions  
295 made by Zhou and Jiang (2015), that electron-rich moieties were prone to react with  
296 ferrate (VI).

297 Fig. 6. Possible pathways of AAP degradation by ferrate (VI)

298

299 *3.5. The presence of humic acid*

300

301 Fig. 7. Effect of different HA dosage on AAP degradation

302

303 The influence of the strength of humic acid (HA) on the removal of AAP by  
304 ferrate (VI) treatment was investigated. Fig. 7 shows the changes in residual  
305 concentrations of AAP corresponding to HA doses and for the reaction time. As it can  
306 be observed, the removal of AAP increased during the intervals between 2 and 10 min  
307 after the addition of HA in AAP solutions. However, for 30 and 60 min, the removal  
308 efficiency of AAP with HA was less than that of AAP without HA. This suggests that  
309 the presence of HA could accelerate the reaction rate of ferrate (VI) and AAP. The  
310 observed phenomena might be related to that in the presence of HA, ferrate (VI) could  
311 be dissociated to form ferrate (IV) and ferrate (V) which have even greater oxidation  
312 capacity (Sharma, 2010) and then assists to the removal of AAP. With increasing in  
313 the strength of HA, the removal efficiency of AAP first increased and then decreased,  
314 and finally tended to be constant. The high contents of HA could consume more  
315 ferrate (VI) in a long reaction time and this might cause the reduction of the removal  
316 of PAA for the reaction time of 30 and 60 min.

317

### 318 *3.6. Effect of coexisting ions*

319  $K^+$ ,  $Na^+$ ,  $Mg^{2+}$ ,  $Ca^{2+}$ ,  $CO_3^{2-}$ ,  $SO_4^{2-}$  and  $PO_4^{3-}$  ions are common ions in natural  
320 water. Aluminum based coagulant is also widely used in water treatment. The effects  
321 of above five cations and three anions on the removal percentage of AAP were  
322 studied. In the presence of  $K^+$ ,  $Na^+$ ,  $Mg^{2+}$ ,  $Ca^{2+}$ ,  $Al^{3+}$ ,  $CO_3^{2-}$ ,  $SO_4^{2-}$ ,  $PO_4^{3-}$  ions, the  
323 AAP removal efficiencies vs. reaction time are shown in Fig. 8(a) for the ion  
324 concentrations of 0.2 mM, in Fig. 8(c) for 1 mM and Fig. 8(e) for 5 mM, respectively.



325 As it can be seen,  $K^+$ ,  $Na^+$ ,  $Mg^{2+}$ ,  $Ca^{2+}$  and  $SO_4^{2-}$  ions can enhance the AAP removal,  
326 however,  $Al^{3+}$ ,  $CO_3^{2-}$  and  $PO_4^{3-}$  ions had the opposite effect. The higher the  
327 concentration of  $Mg^{2+}$ , the greater the removal rate of AAP. The performance of  $K^+$ ,  
328  $Na^+$ ,  $Ca^{2+}$  and  $SO_4^{2-}$  mainly remained constant with the increasing concentration from  
329 0.2 to 5 mM.

330

331 Table 2. Kinetic parameters of the AAP degradation in the presence of eight co-  
332 existing ions

333

334 Fig. 8(b), Fig. 8(d) and Fig. 8(f) show the linear fitting curve of the reciprocal of  
335 ferrate (VI) concentration and reaction time in the presence of the above ions. Table 2  
336 shows the pseudo reaction rate constant ( $K_{obs}$ ) and correlation coefficient of the linear  
337 fitting curves for Fig. 8(b), Fig. 8(d) and Fig. 8(f). The good correlation coefficients  
338 ( $R^2 > 0.90$ , except  $Al^{3+}$ ) indicate that the reactions were pseudo second-order with  
339 respect to ferrate (VI), which is consistent with that shown in the previous section.  
340 When raising the ions' concentration from 0.2 to 5 mM, the  $K_{obs}$  of  $CO_3^{2-}$  and  $PO_4^{3-}$   
341 ions decreased, from  $4 \times 10^{-4}$  to  $6.8 \times 10^{-5} \text{ min}^{-1}$  and  $5 \times 10^{-4}$  to  $2.2 \times 10^{-5} \text{ min}^{-1}$ ,  
342 respectively, but the  $K_{obs}$  of  $Mg^{2+}$  increased, from  $3.8 \times 10^{-3}$  to  $8.4 \times 10^{-3} \text{ min}^{-1}$ . The  
343 resulting rate constants are theoretically evident to the observed effect of co-existing  
344 ions on the AAP removal by ferrate(VI); that  $CO_3^{2-}$  and  $PO_4^{3-}$  ions inhibited while  
345  $Mg^{2+}$  ions were beneficial to the reaction between AAP and ferrate(VI).

346 In the presence of metal cations, deprotonation of acid-base functional groups in  
347 AAP molecules can be accelerated due to the metal-AAP binding and this might also

348 reduce the AAP  $pK_a$  value (Jeffrey et al., 2006). In this work, the addition of  $K^+$ ,  $Na^+$ ,  
349  $Mg^{2+}$ ,  $Ca^{2+}$  could enhance the deprotonation of AAP and then to accelerate the  
350 removal rate. Besides, hydrogen ion could be generated through the hydrolysis  
351 reaction of magnesium ion in aqueous solution. The accumulation of hydrogen ions  
352 helped the increase of oxidation potential of ferrate (VI) (Jiang, 2014). It may be the  
353 reason that the addition of  $Mg^{2+}$  has a greater removal rate of AAP than  $Ca^{2+}$ .

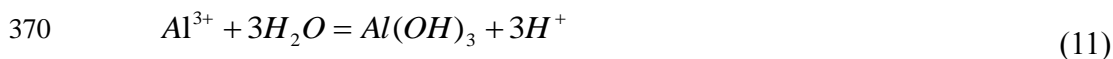
354 In the presence of  $Al^{3+}$ ,  $CO_3^{2-}$  and  $PO_4^{3-}$  ions and when the concentration of each  
355 ion increased from 0.2 to 5 mM, the removal of AAP decreased from 66.7 to 22.4%  
356 for  $Al^{3+}$ , 74.2 to 36.5% for  $CO_3^{2-}$ , and 79.9 to 13.1% for  $PO_4^{3-}$ , respectively. The  
357 hydrolysis of  $CO_3^{2-}$  and  $PO_4^{3-}$  in the aqueous solution could raise the alkalinity and  
358 then decreases the oxidation potential of ferrate (VI) and causes the reduction of AAP  
359 removal efficiency. This phenomenon was even clearly to observe when  
360 concentrations of phosphate and carbonate ions were greater.

361

362 Table 3. Effect of aluminum ions on ferrate (VI) concentration

363

364 In this work, the decomposition of ferrate (VI) caused by aluminium ions was  
365 found (Table 3). As can be seen when 500  $\mu$ l of aluminium ions solution was added,  
366 the ferrate (VI) concentration decreased by 79%. This might be related to the  
367 hydrolysis of  $Al^{3+}$  to produce hydrogen ions into solution, (Eq. 11), which then  
368 accelerates the decomposition of ferrate (VI) and could lower the AAP removal  
369 efficiency.



371

372 Fig. 8. Effect of different ions on AAP degradation

373

#### 374 **4. Conclusions**

375 The treatment of AAP in aqueous solutions by ferrate (VI) was investigated.

376 Results demonstrated that AAP can be removed effectively under the experimental

377 conditions. More ferrate (VI) dosage and a neutral solution environment could bring a

378 better performance on the AAP degradation. Besides, the pseudo rate constant of

379 ferrate (VI) with AAP is  $0.000014 \text{ l}^2 \cdot \text{mg}^{-2} \cdot \text{min}^{-1}$ . Three oxidation products (OPs) were

380 identified. The attack on hydroxyl and acetamido groups of the AAP by ferrate (VI)

381 was proposed to be the main pathway of the AAP degradation scheme. Moreover, in

382 the presence of HA, a short time interval ( $< 30 \text{ min}$ ) would favour to but longer

383 reaction time (30-60 min) decreased the degradation of AAP. The presence of  $\text{K}^+$ ,

384  $\text{Na}^+$ ,  $\text{Mg}^{2+}$  and  $\text{Ca}^{2+}$  ions in aqueous solutions can improve the AAP removal

385 efficiency by ferrate(VI), and the most promoting effect of  $\text{Mg}^{2+}$  was observed. The

386 presence of  $\text{Al}^{3+}$ ,  $\text{CO}_3^{2-}$  and  $\text{PO}_4^{3-}$  would decline the AAP degradation performance

387 significantly. The catalytic function of  $\text{Al}^{3+}$  to the ferrate (VI) decomposition in

388 aqueous solution was found in this work, which explains the negative effect of  $\text{Al}^{3+}$  on

389 the AAP reduction by ferrate (VI).

390

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397

398 **Supplementary material**

399 Supplementary material associated with this article can be found in the online  
400 version.

401

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516

### Figure captions

517 **Fig. 1.** Effect of reaction time and ferrate (VI) dosage on AAP degradation

518 **Fig. 2.** Effect of different pH values on AAP degradation

519 **Fig. 3.** Kinetics analysis of AAP degradation by ferrate (VI)

520 **Fig. 4.** Detection of oxidation products (a – c) and original compound, AAP (d)

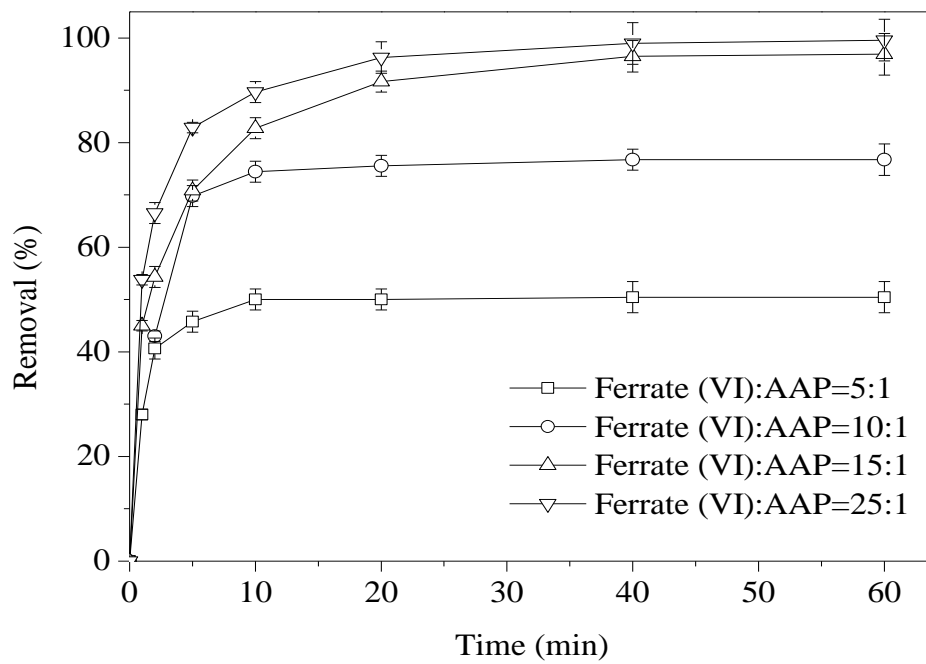
521 **Fig. 5.** Evolution of OPs and nitrate with decreasing of AAP concentration

522 **Fig. 6.** Possible pathways of AAP degradation by ferrate (VI)

523 **Fig. 7.** Effect of different HA dosage on AAP degradation

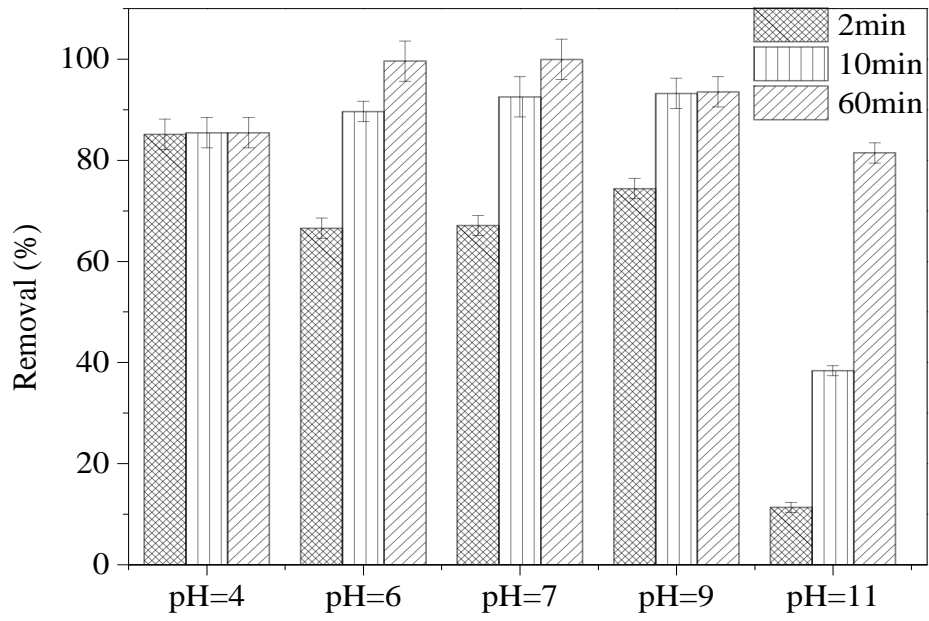
524 **Fig. 8.** Effect of different ions on AAP degradation

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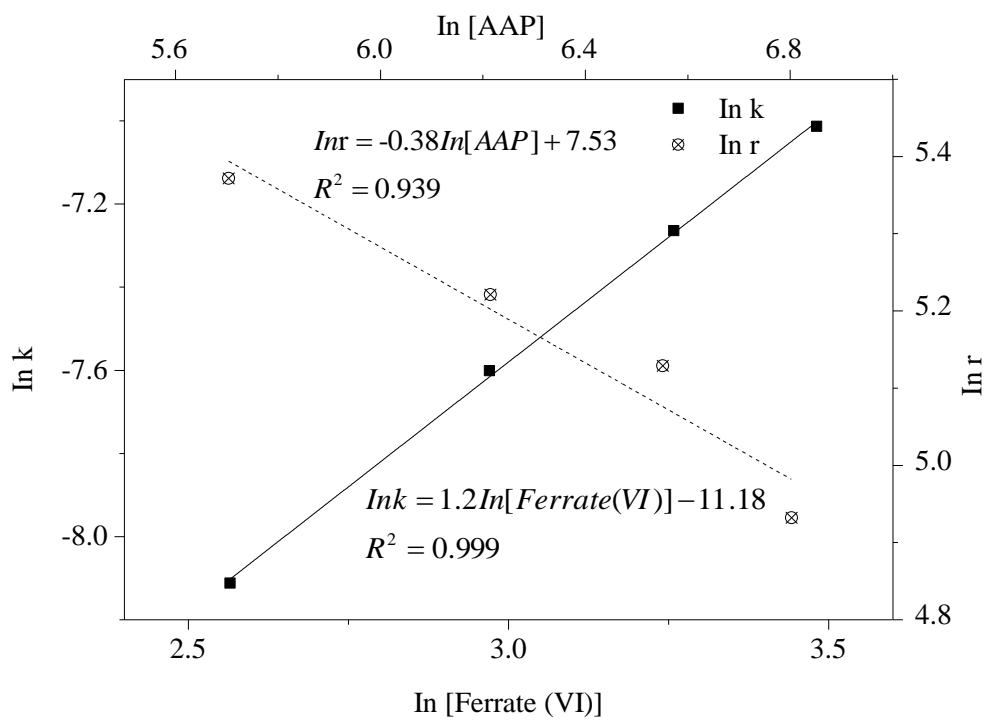
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529 Fig. 2. Effect of different pH values on AAP degradation

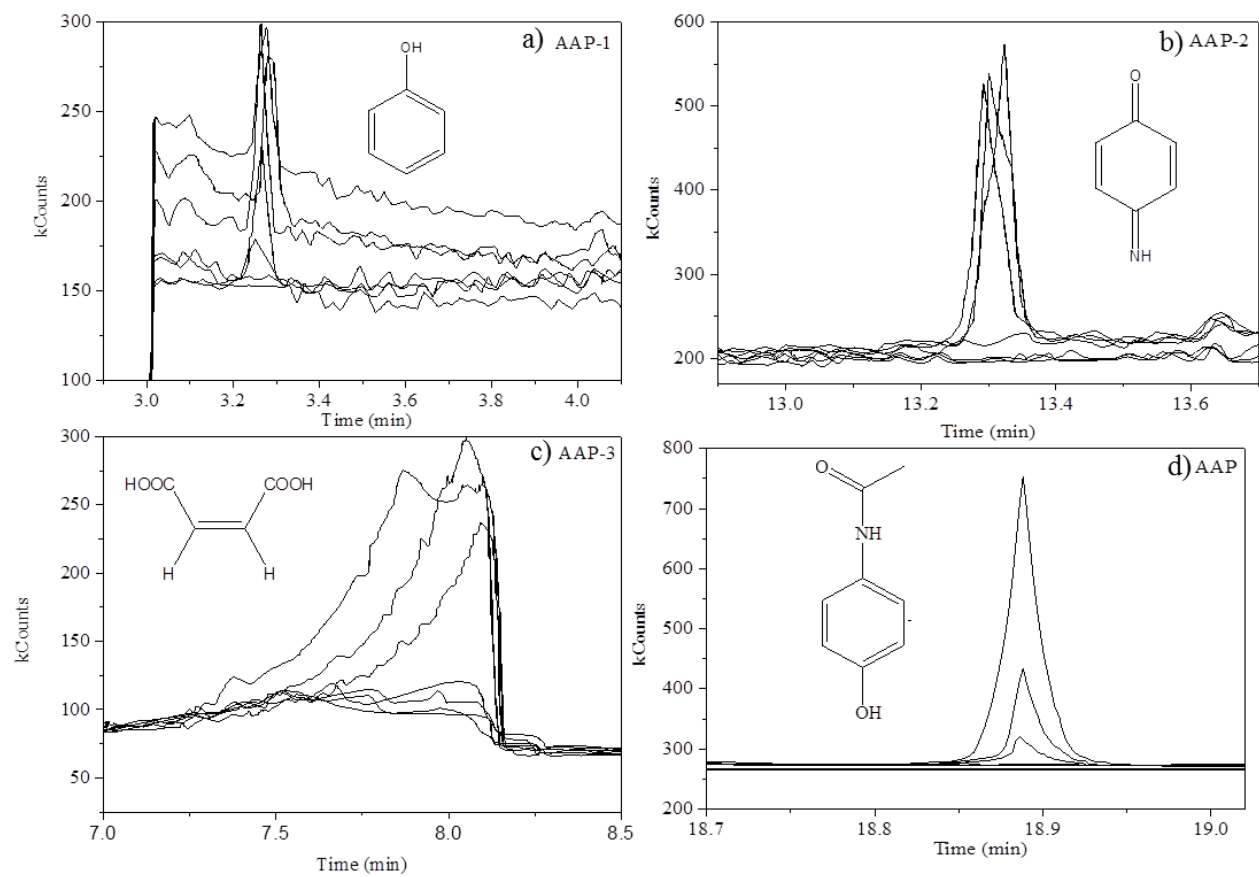
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532 Fig. 3. Kinetics analysis of AAP degradation by ferrate (VI)

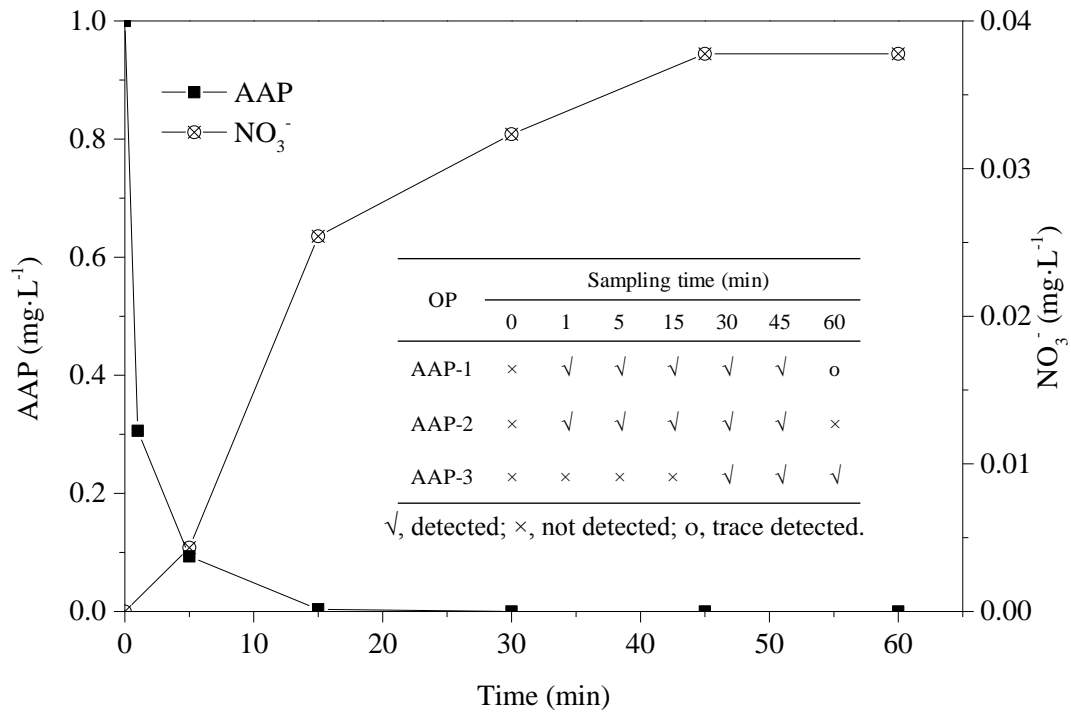
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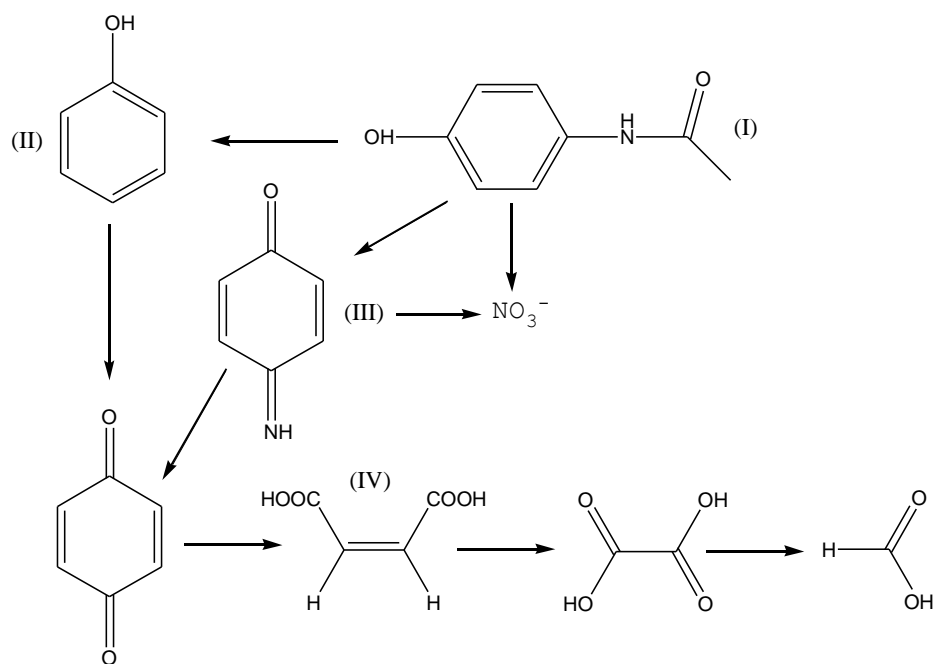
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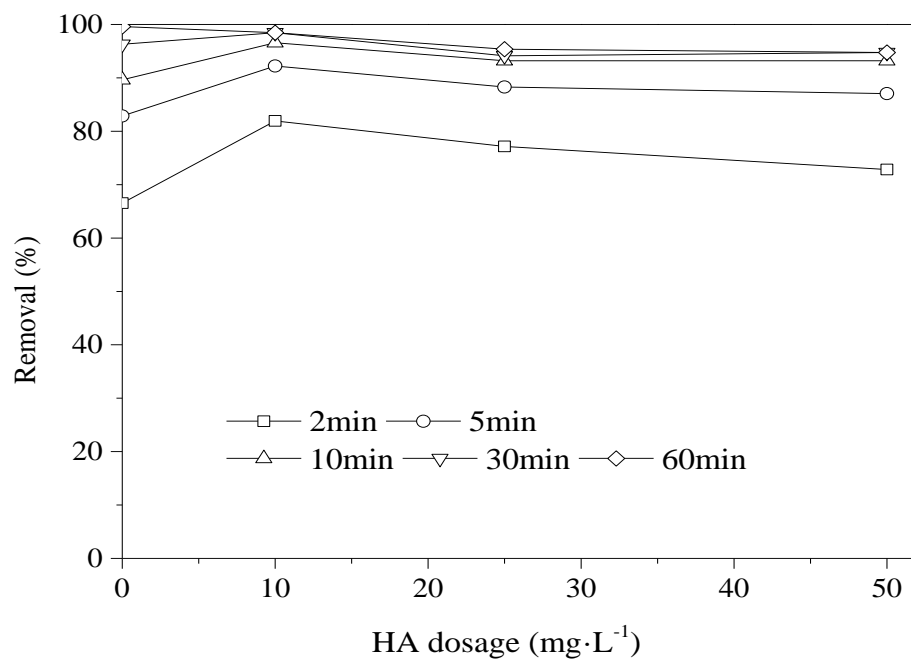
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541 Fig. 6. Possible pathways of AAP degradation by ferrate (VI)





542

543 Fig. 7. Effect of different HA dosage on AAP degradation

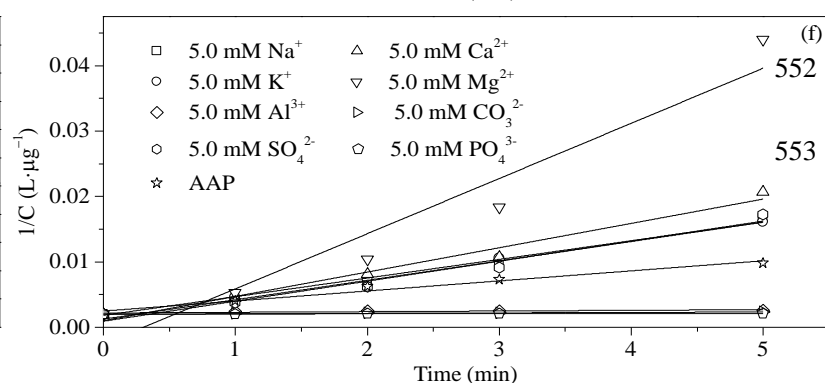
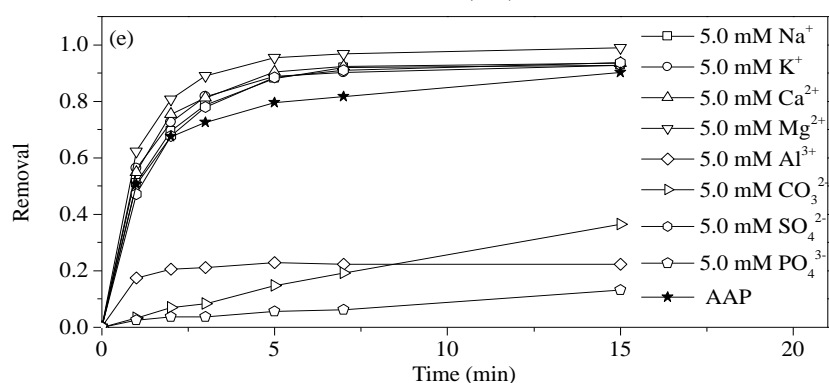
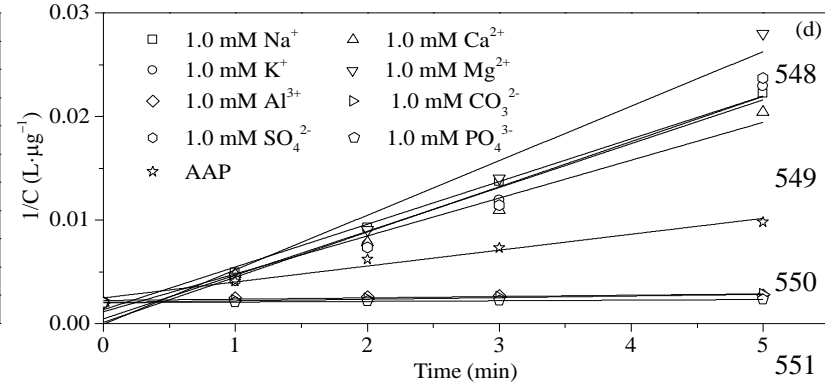
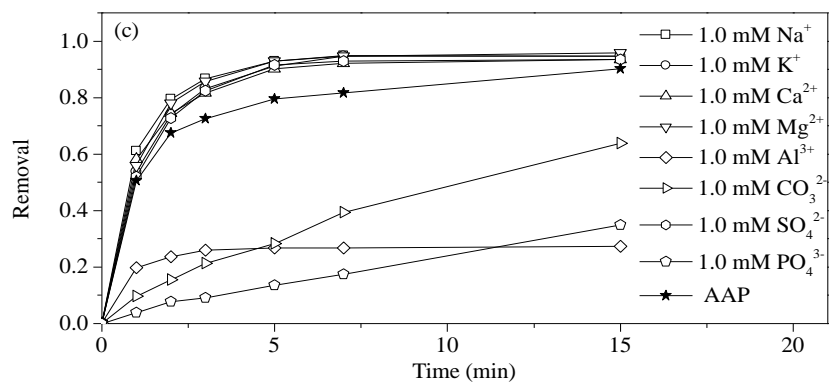
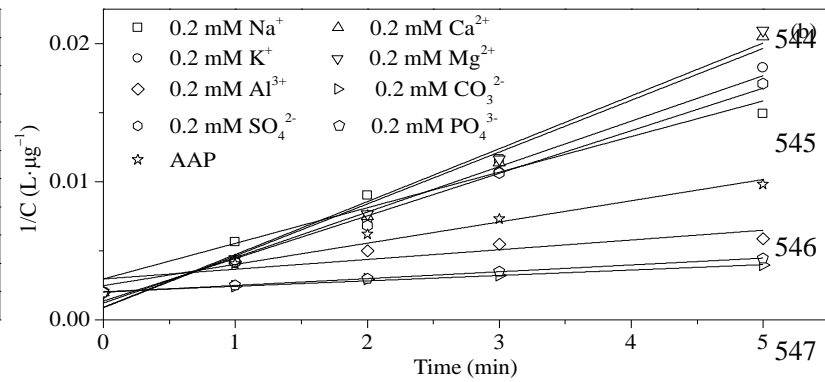
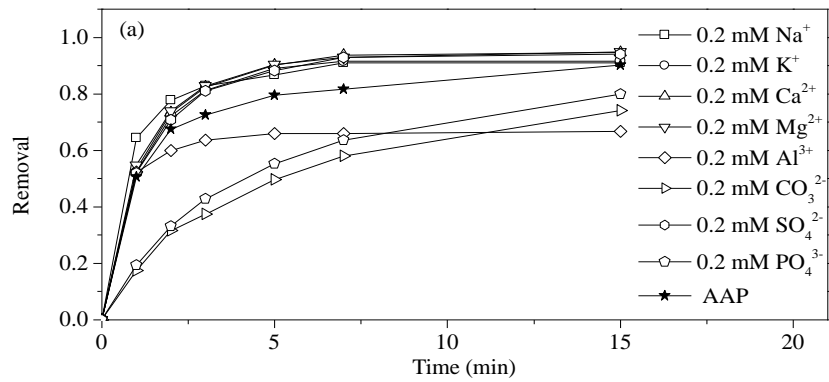


Fig. 8. Effect of different ions on AAP degradation

554 Table 1

555 Kinetic parameters of AAP degradation by ferrate (VI)

$D_{\text{Ferrate (VI)}}$ ( $\text{mg}\cdot\text{L}^{-1}$ )	$C_{\text{IAAP}}$ ( $\mu\text{g}\cdot\text{L}^{-1}$ )	Fitting equation	$K_{\text{obs}}(\text{min}^{-1})$	$R^2$	$R_{\text{IR}}$ ( $\mu\text{g}\cdot\text{L}^{-1}\cdot\text{min}^{-1}$ )
13	1000	$1/C=0.0003X+0.0012$	0.0003	0.9093	208.3
19.5	1000	$1/C=0.0005X+0.0012$	0.0005	0.9946	347.2
26	1000	$1/C=0.0007X+0.0013$	0.0007	0.9943	414.2
32.5	1000	$1/C=0.0009X+0.0012$	0.0009	0.9961	625.0
32.5	900	$\ln C=-0.2647X+6.2611$	0.2647	0.9088	138.6
32.5	700	$\ln C=-0.3920X+6.0656$	0.3920	0.9596	168.9
32.5	500	$\ln C=-0.5504X+5.8182$	0.5504	0.9694	185.1
32.5	300	$\ln C=-0.8308X+5.5569$	0.8308	0.9665	215.2

556  $D_{\text{Ferrate (VI)}}$ : Ferrate (VI) dosage

557  $C_{\text{IAAP}}$ : Initial concentration of AAP

558  $K_{\text{obs}}$ : The pseudo reaction rate constant

559  $R_{\text{IR}}$ : Initial reaction rate

560 Table 2

561 Kinetic parameters of the AAP degradation in the presence of 8 dissolved ions

Parameter	D <sub>ions</sub> (mM)	Na <sup>+</sup>	K <sup>+</sup>	Ca <sup>2+</sup>	Mg <sup>2+</sup>	Al <sup>3+</sup>	CO <sub>3</sub> <sup>2-</sup>	SO <sub>4</sub> <sup>2-</sup>	PO <sub>4</sub> <sup>3-</sup>
K <sub>obs</sub> (min <sup>-1</sup> )	0.2	0.0026	0.0033	0.0038	0.0038	0.0007	0.0004	0.0031	0.0005
R <sup>2</sup>		0.9661	0.9905	0.9837	0.9842	0.7765	0.9944	0.9925	0.9999
K <sub>obs</sub> (min <sup>-1</sup> )	1	0.0041	0.0042	0.0037	0.0053	0.0001	0.0002	0.0044	6.1×10 <sup>-5</sup>
R <sup>2</sup>		0.9963	0.9729	0.9829	0.9700	0.6713	0.9893	0.9583	0.9789
K <sub>obs</sub> (min <sup>-1</sup> )	5	0.0030	0.0029	0.0037	0.0084	0.0001	6.8×10 <sup>-5</sup>	0.0031	2.2×10 <sup>-5</sup>
R <sup>2</sup>		0.9852	0.9989	0.9787	0.9340	0.6352	0.9887	0.9728	0.9012

562 D<sub>ion</sub>:The ions dose

563 K<sub>obs</sub>:The pseudo reaction rate constant

564

Table 3

Effect of aluminum ions on ferrate (VI) concentration

$V_{\text{aluminum}}$ ( $\mu\text{L}$ )	0	10	100	200	300	400	500
$C_{\text{Ferrate (VI)}}$ (mM)	13.2	12.8	11.5	8.9	6.6	4.3	2.8

$V_{\text{aluminum}}$ : The volume of aluminum ions

$C_{\text{Ferrate (VI)}}$ : The concentration of ferrate (VI)