

Optimal Power Flow Using Flower Pollination Algorithm: A Case Study of 500 kV Java-Bali Power System

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Abstract—Flower Pollination Algorithm (FPA) is one of metaheuristic methods that is widely used in optimization problems. This method was inspired by the nature of flower pollination. In this research, FPA is applied to solve Optimal Power Flow (OPF) problems with case study of 500 kV Java-Bali power system in Indonesia. The system consists of 25 bus with 30 lines and 8 generating units. Control variables are generation of active power and voltage magnitude at PV bus and swing bus under several power system constraints. The results show that FPA method is capable of solving OPF problem. This method decreased the generator fuel cost of PT. PLN (Persero), the state-owned company in charge of providing electricity in Indonesia, up to 13.15%.

Keyword— Optimal power flow, flower pollination algorithm, Java-Bali 500 kV system, voltage magnitude, capacity of the transmission line.

I. INTRODUCTION

The total capacity of power plants should be greater than the total electrical load demand so that the electrical energy supply can be adequate. The total installed capacity of power plants in Indonesia reaches 40,265.62 MW, 27,867.88 MW (69.21%) of which are located in the Java Island. When classified by the types of units, steam turbine and combined cycle have the biggest proportion with 53.90% and 28.33% respectively. Hydro plants make up to 8.63%, while gas turbine 7.10%, geothermal 1.24% and diesel 0.80% [1]. Thermal power plants, especially steam turbines and combined cycle, are dominating the composition of installed power plants in Java Island. Thermal power plants are the power plants that convert heat energy from fuel combustion to get the mechanical energy used to drive the turbine and then generates electrical energy. This causes fuel to be an integral part of thermal power plants.

Fuel cost and lubricants have a dominant contribution in the composition of the operations cost. According to statistical reports of PT. PLN (Persero) in 2015 [1], the amount of total electricity operating cost is Rp246 trillion, which consists of power purchasing and diesel rent costs, fuel and lubricating oil, maintenance, staffing, depreciation of fixed assets, and other costs. The cost of power purchasing and diesel rent reached Rp59.3 trillion (24.08%), the cost of fuel and

lubricants Rp120.6 trillion (49.02%), maintenance costs Rp17.6 trillion (7.15%), staffing costs reached Rp20.3 trillion (8.26%), the cost of depreciation of fixed assets Rp21.4 trillion (8.71%), while other expenses reached Rp6.8 trillion (2.78%). Based on the data, it can be seen that the cost of fuel and lubricant oil makes up the majority of total electricity operating costs.

One solution to minimize the operational costs of electric power systems is to optimize the cost of the electrical energy production process. In an interconnection system, one way to minimize fuel cost is done by optimizing the generation of active and reactive power in each plant. This method is called optimal power flow (OPF) [2]. The idea of optimal power flow (OPF) is introduced in early 1960s. It has been developed from economic dispatch that is used to determine the optimal setting of control variables while concerning various constraints. The optimal power flow is an important problem of power systems in which certain control variables are adjusted to minimize an objective function such as the cost of active power generation or the losses, while satisfying physical and operating limits on various controls, dependent variables and function of variables.

One of the techniques to solve the OPF problem is by using the metaheuristic optimization methods. The use of metaheuristic methods has been widely used to solve OPF problems, such as Evolutionary Programming (EP) [3], Differential Evolution (DE) [4], Particle Swarm Optimization (PSO) [5], Genetic Algorithm (GA) [6] and Flower Pollination Algorithm (FPA) [7] - [10].

The use of FPA methods to solve OPF problems has been done by previous researchers [7] - [10]. Researchers use Flexible AC Transmission System (FACTS) to get minimum line power losses and fuel costs with active power generator as control variables [7]. In other studies [8], Thyristor Controlled Series Capacitor (TCSC) is used as a control variable of OPF problems with the objective function of minimizing line power losses. Valve point effect of generator are taken into account in other studies [9] whose objective function is to get the minimal fuel costs. Furthermore, the addition of Static VAR Compensator (SVC) as a control variable and the addition of the influence of valve-point loading effect on the fuel function is shown in other studies [10].

In this study, the FPA method is applied to solve the OPF problem in the 500 kV electrical system of Java-Bali in Indonesia. This research is conducted to obtain minimum fuel costs with active power and voltage magnitude as control variables.

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II. OPTIMAL POWER FLOW FORMULATION

As mentioned in the previous section, fuel cost contributes to almost half of the total operations cost of PT. PLN (Persero). Therefore, this research will formulate the minimization of fuel costs by optimizing active power generation of power plant. The fuel cost function of each plant is described as a second-order quadratic curve. Generally the function is described as:

$$f(P_G) = \sum_{i=1}^{N_g} (\alpha_i + \beta_i P_{Gi} + \gamma_i P_{Gi}^2) \quad (1)$$

where N_g represents the total number of existing plants in the system including the generators on the slack bus. P_{Gi} is an active power generation by the i -th power plant, while α_i , β_i , γ_i are the coefficient of fuel function in the i -th power plant.

A. Control Variable

The control variable is a variable whose values can be modified to get the minimum value of the objective function. Control variable in this research are active power at PV bus except slack bus and magnitude voltage at PV bus include slack bus.

B. Objective Function Constraint

OPF utilizes a number of both equality and inequality constraints as shown below.

1) *Equality Constraint*: When minimizing fuel costs, it must be ensured that the amount of generated power equals the total of load demand coupled to power losses in the lines.

$$P_{Gi} - P_{Di} - \sum_{j=1}^{n_b} V_i V_j (g_{ij} \cos \theta_{ij} + b_{ij} \sin \theta_{ij}) = 0 \quad (2)$$

$$Q_{Gi} - Q_{Di} - \sum_{j=1}^{n_b} V_i V_j (g_{ij} \sin \theta_{ij} + b_{ij} \cos \theta_{ij}) = 0 \quad (3)$$

where,

P_{Gi} : Total active power generated by the generator at bus- i .

P_{Di} : Total active power load at bus- i .

Q_{Gi} : Total reactive power generated by generator on bus- i .

Q_{Di} : Total reactive power load on bus- i .

V_i : Voltage magnitude on bus- i .

V_j : Voltage magnitude on bus- j .

g_{ij} : Real-part of the matrix called the admittance or conductance.

b_{ij} : The imaginary part of the referred to susceptance.

θ_{ij} : Voltage angle element to ij of the admittance matrix.

nb : Bus number on the system.

2) *Inequality Constraints*: The inequality constraints are bounded by an upper and lower limit. Constraints are used to maintain the security of the system.

- **Generator Constraint.**

Active and reactive power of all generators must not exceed the upper and lower limit. Constraint were applied to all generators, including generators on the slack bus.

$$P_{Gi}^{min} \leq P_{Gi} \leq P_{Gi}^{max}, i = 1, \dots, N_g \quad (4)$$

$$Q_{Gi}^{min} \leq Q_{Gi} \leq Q_{Gi}^{max}, i = 1, \dots, N_g \quad (5)$$

where N_g is the number of generator buses.

- **Constraints of Voltage Magnitudes.**

The voltage magnitude is required to be within the range that is permitted by the relevant authorities. These values must be maintained to guarantee the quality of the electric power system.

$$V_i^{min} \leq V_i \leq V_i^{max}, i = 1, \dots, N_{bus} \quad (6)$$

where N_{bus} is the number of buses including load bus, generator bus and swing bus.

- **Power Flow Line Constraint**

Power flow line constraint is used to limit the current passing through each branch so that it does not exceed its maximum capability.

$$S_i < S_i^{max}, i = 1, \dots, N_{br} \quad (7)$$

where N_{br} is the number of transmission lines.

III. FLOWER POLLINATION ALGORITHM

Flower Pollination Algorithm is an algorithm developed by Xin-She Yang in 2012 [11]. FPA is a metaheuristic algorithm inspired by natural phenomena related to flower pollination process. Pollination, specific relationships, and the nature of pollinators can be idealized into four rules [12]:

- Biotic and cross-pollination is considered as global pollination process with pollen-carrying pollinators performing Levy flight.
- Abiotic and self-pollination are considered as local pollination.
- Flower constancy can be considered as the reproduction probability is proportional to the similarity of two flowers involved.
- Local and global pollination are controlled with the probability switch $p \in [0,1]$. Because of a physical approach and other factors such as wind, local pollination can have a significant chance (p) in overall activity of pollination.

Two key steps in this algorithm are global pollination and local pollination. At the global pollination step, pollen is carried by pollinators and can move over long distances. This ensures the most optimal pollination and reproduction (best fitness) of the fitness value is represented as \mathbf{g}^* . The first rule, the specific relationship of interest, mathematically can be represented as follows:

$$\mathbf{x}_i^{t+1} = \mathbf{x}_i^t + \mathbf{L} \cdot (\mathbf{x}_i^t - \mathbf{g}^*) \quad (8)$$

where \mathbf{x}_i^t is the i -th solution in the t -th iteration. Parameter \mathbf{L} is the strength of pollination that is obtained from the Levy distribution.

At the local pollination or second rule, the specific relationship of flowers represented as

$$x_i^{t+1} = x_i^t + \epsilon(x_j^t - x_k^t) \tag{9}$$

where x_j^t and x_k^t are the current pollen from different flowers of the same plant species, t is represent the current generation (iteration) and ϵ is random number between 0 and 1.

Flowchart of FPA method to solve the OPF problems is shown in Fig. 1.

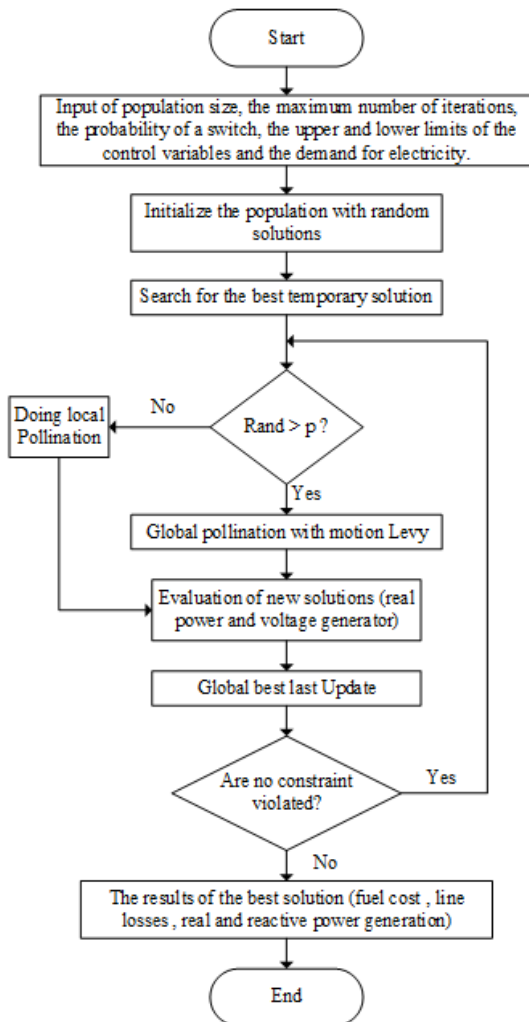


Fig. 1 Flowchart of OPF using FPA.

IV. 500 kV JAVA-BALI POWER SYSTEM

The data of 500 kV Java-Bali power system was obtained from PT. PLN (Persero) which has been used by previous researches [13], [14]. The system has eight generating units which consists of six thermal and two hydro units. Optimization is applied to six thermal generator units, while two units of hydro will operate as its initial condition. The complete electrical system is illustrated in Fig. 2.

Generator data consists of active and reactive power upper and lower limits shown in Table I. Generator fuel function shown in (1) is a form of second order polynomial. The

function is obtained from the regression of generation data at different times. The fuel function of the 500 kV Java-Bali system is shown in Appendix 1.

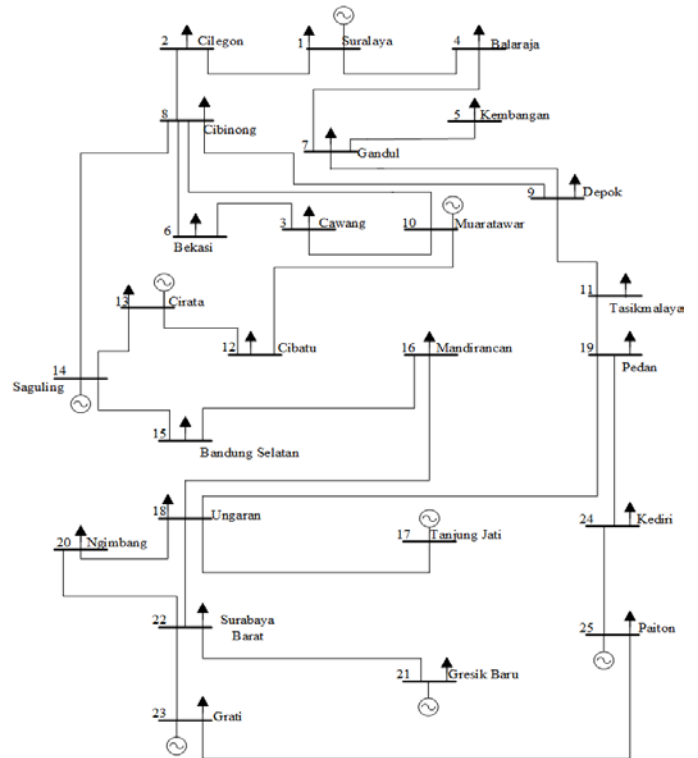


Fig. 2 Single line diagram of 500 kV Java-Bali power System.

TABLE I
POWER LIMIT GENERATOR

No	Name	Pmin (MW)	Pmax (MW)	Qmin (MVar)	Qmax (MVar)
1.	Suralaya	1,610	4,025	-1,478.6	2,494.5
2.	Muara Tawar	1,300.4	3,251	-1,859.1	2,438.2
3.	Saguling	280	700	-460.9	525
4.	Cirata	403.2	1,008	-663.7	756
5.	Tanjung Jati	1,056	2,640	-969.8	1,636.1
6.	Gresik Baru	895.62	2,239	-1,474.4	1,679.3
7.	Grati	305.8	764.5	-341.3	573.4
8.	Paiton	1,886	4,714	-1,750	3,028.3

The control variable used in this research is active power and magnitude voltage generator. Each generator has a different active power limit. The initial condition of the control variable is shown in Appendix 2. The voltage magnitude limit is at $\pm 5\%$ of its nominal value. This is in accordance with the rule of Minister of Energy and Mineral Resources of the Republic of Indonesia regarding Grid Code 2007 [15].

In addition to the voltage magnitude, the current constraints that flow through each line are applied to this system. The value of the constraints is related to the technical factors of the lines which has a different maximum current carrying capacity. Using a 1000 MVA base, data network and line current carrying capability are given in Appendix 3.

TABLE II
RESULTS OF CONTROL VARIABLE USING FPA

No	Control variable	Limitation		Result
		Minimal	Maximal	
1	P1 (MW)	1,610	4,025	1,912.87
2	P10(MW)	1,300.4	3,251	1,400.40
3	P13(MW)	280	700	594
4	P14(MW)	403.2	1,008	662
5	P17(MW)	1,056	2,640	1,856.05
6	P21(MW)	895.62	2,239	895.2
7	P23(MW)	305.8	764.5	305.80
8	P25(MW)	1,886	4,714	4,714
9	V1 (p.u)	0.95	1.05	1.050
10	V10(p.u)	0.95	1.05	1.047
11	V13(p.u)	0.95	1.05	1.050
12	V14(p.u)	0.95	1.05	1.037
13	V17(p.u)	0.95	1.05	1.050
14	V21(p.u)	0.95	1.05	1.050
15	V23(p.u)	0.95	1.05	1.049
16	V25(p.u)	0.95	1.05	1.050

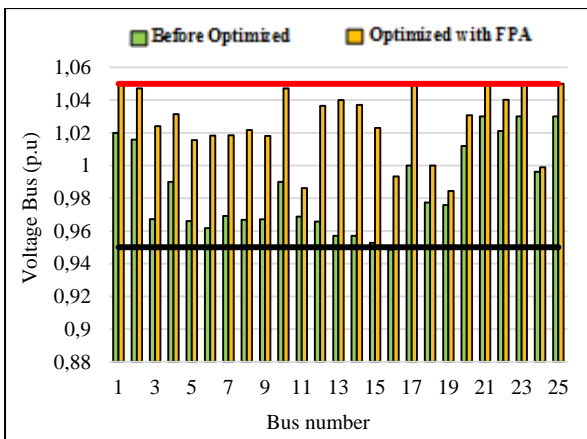


Fig. 3 Comparison of the voltage profile.

Active and reactive power data on each bus is required to perform a power flow analysis. In this study, data of power that occurs during peak loads are shown in Appendix 4.

V. RESULTS AND ANALYSIS

This research was conducted with FPA parameters in which the probability switch value is set at 0.8, population size 20 and number of iterations of 6,000, with tolerance of 0.001. The results are shown in Table II. From these results, note that the value of control variables are still in the normal range.

The voltage magnitude on all buses after optimization is in the range of 0.95 p.u - 1.1 p.u. The lowest voltage value is 0.984 p.u on bus 19, while the highest voltage of 1.05 p.u are on buses 1, 17, 21, and 25. However, the value is still within the allowable range. Comparison of voltage between before and after optimization using FPA is shown in Fig. 3.

In addition to voltage constraints, line current is also a constraint that should not be violated. The current passing through the line must not exceed its current carrying capacity. Of all lines, current through the line is still within safe limits.

The smallest percentage of flowing current is 4.01%, which occurs on line number 11. The largest percentage of line flow occurs on line number 16 of 52.06%. The comparisons of percentage of the line current between before and after optimization using FPA is shown in Fig. 4.

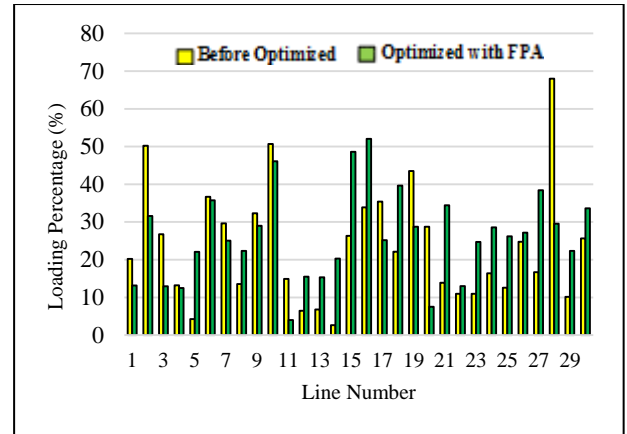


Fig. 4 Comparison of power flow line.

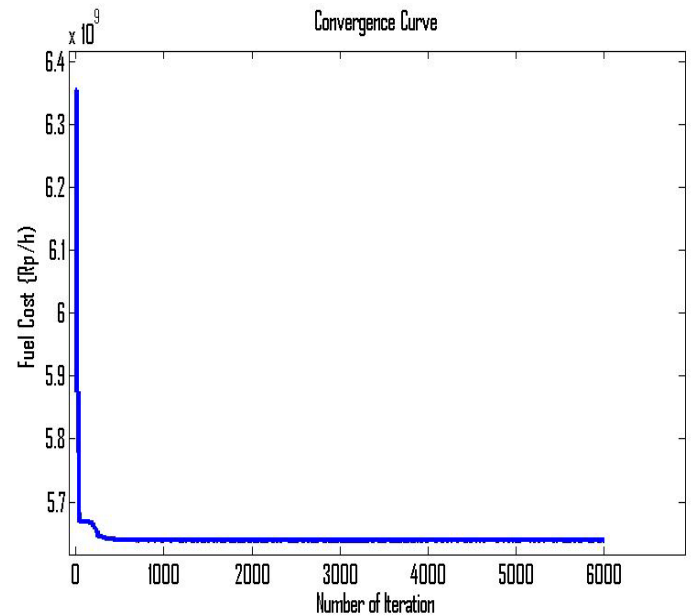


Fig. 5 Convergence curve of FPA.

Convergence in a process of optimization that is important to note and show how the value of objective function reaches the most optimal results. After a certain point, the value will be relatively constant with no significant changes. Fig. 5 shows the convergence graph of total generating costs by the FPA method. Based on the picture, it can be seen that fuel cost function reaches its convergence at the 1000th iteration.

The results of FPA method show a satisfactory performance. FPA method is able to decrease the fuel cost from Rp6,492,201,738/hour to Rp5,638,693,790/hour. This means that fuel costs are reduced by Rp853,507,948/hour (13.15%). Comparison of active power generation, as well as fuel costs before and after optimization are shown in Table III.

TABLE III
COMPARISON OF MINIMIZATION OBJECTIVE FUNCTION

Generator	Data Operation PLN		FPA	
	Power (MW)	Cost (x1000 Rp/hour)	Power (MW)	Cost (x1000 Rp/hour)
Suralaya	2,814.48	1,131,383	1912,87	798,596
Muaratawar	1,785	1,794,021	1400,4	1,427,640
Cirata	594	-	594	-
Saguling	662	-	662	-
Tanjungjati	1,971	633,534	1856,049	595,260
Gresik	1,371	1,226,721	895,62	828,402
Grati	441	732,309	305,8	565,841
Paiton	2,572	972,845	4714	1,422,953
Total	12,210.48	6,492,202	12,340.74	5,638,694
Reduction of costs (x1000 Rp/hour)			853,508	

VI. CONCLUSION

In this study, the FPA method was used to solve OPF problem of 500 kV Java-Bali power system in Indonesia. The system consists of 25 buses with 30 branches and eight generator units. Active power and magnitude voltage optimization are performed on six thermal power plants. The results showed satisfactory performance of FPA method. The proposed method can lower the fuel cost from Rp 6,492,201,738/hour to Rp 5,638,693,790/hour or by 13.15% without violating any constraints.

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APPENDIX

Appendix 1. Fuel Cost Coefficients of 500 kV Java Bali System

No. Bus	Generator	Fuel cost function coefficients		
		α	β	γ
1	Suralaya	47,071,299.8	407,989.965	-7.90
10	Muaratawar	-196,885,587.4	1,322,770.659	-116.23
17	Tanjungjati	104,589,684.8	199,772.387	34.75
21	Gresik	81,256,913.02	831,821.003	2.68
23	Grati	198,252,082.2	1,176,938.992	75.30
25	Paiton	5,575,248.3	466,630.8	-35.21

Appendix 2. Limit of Control Variable

No.	Control Variable	Limitation		Initial
		Minimal	Maximal	
1	P1 (MW)	1,610	4,025	2,735
2	P10(MW)	1,300.4	3,251	1,785
3	P13(MW)	280	700	594
4	P14(MW)	403.2	1,008	662
5	P17(MW)	1,056	2,640	1,971
6	P21(MW)	895.62	2,239	1,371
7	P23(MW)	305.8	764.5	441
8	P25(MW)	1,886	4,714	2,572
9	V1 (p.u)	0.95	1.05	1.020
10	V10(p.u)	0.95	1.05	0.990
11	V13(p.u)	0.95	1.05	0.957
12	V14(p.u)	0.95	1.05	0.957
13	V17(p.u)	0.95	1.05	1.000
14	V21(p.u)	0.95	1.05	1.030
15	V23(p.u)	0.95	1.05	1.030
16	V25(p.u)	0.95	1.05	1.030

Appendix 3. Branch Data of 500 kV Java Bali System

No.	From Bus	To Bus	R (p.u)	X (p.u)	B/2 (p.u)	Current Limit (A)
1.	1	2	0.001	0.007	0	4,800
2.	1	4	0.004	0.035	0	3,960
3.	2	8	0.013	0.147	0.004	2,400
4.	5	7	0.002	0.017	0	4,800
5.	7	9	0.001	0.007	0	3,960

No.	From Bus	To Bus	R (p.u)	X (p.u)	B/2 (p.u)	Current Limit (A)
6.	8	6	0.004	0.043	0	1,980
7.	8	10	0.006	0.060	0	1,980
8.	8	14	0.004	0.046	0.004	4,800
9.	3	6	0.002	0.019	0	1,980
10.	3	10	0.006	0.054	0	1,980
11.	10	12	0.003	0.027	0	3,960
12.	12	13	0.003	0.026	0	3,960
13.	13	14	0.001	0.014	0	3,960
14.	14	15	0.002	0.022	0	4,800
15.	15	16	0.007	0.067	0.006	3,960
16.	16	18	0.013	0.129	0.012	3,960
17.	18	17	0.014	0.151	0.004	4,800
18.	18	22	0.016	0.152	0.004	1,980
19.	18	19	0.009	0.087	0	1,980
20.	22	21	0.001	0.013	0	3,960
21.	22	23	0.004	0.045	0	4,800
22.	9	8	0.001	0.008	0	3,960
23.	9	11	0.014	0.157	0.015	4,800
24.	11	19	0.015	0.171	0.016	4,800
25.	19	24	0.010	0.115	0.011	4,800
26.	24	25	0.010	0.115	0.011	4,800
27.	25	23	0.004	0.050	0.005	4,800
28.	4	7	0.003	0.029	0	1,980
29.	20	18	0.023	0.226	0.101	1,980
30.	20	22	0.006	0.057	0	1,980

Appendix 4. Bus Data of 500 kV Java Bali System

No. bus	Type	Generation		Load	
		MW	MVar	MW	MVar
1	Swing	2,735	1,254	201	98
2	Load	-	-	293	221
3	Load	-	-	322	75
4	Load	-	-	624	-14
5	Load	-	-	522	125
6	Load	-	-	1,118	264
7	Load	-	-	761	132
8	Load	-	-	616	330
9	Load	-	-	641	204
10	Gen.	1,785	859	-	-
11	Load	-	-	219	83
12	Load	-	-	688	467
13	Gen.	594	209	586	232
14	Gen.	662	125	-	-
15	Load	-	-	733	426
16	Load	-	-	309	131
17	Gen.	1,971	58	238	11
18	Load	-	-	417	468
19	Load	-	-	608	229
20	Load	-	-	302	70
21	Gen.	1,371	286	174	64
22	Load	-	-	899	512
23	Gen.	441	58	510	191
24	Load	-	-	627	188
25	Gen.	2,572	611	650	146
Total		12,131	3,460	12,058	4,650