

## Harmonic Contribution Analysis of Electric Arc Furnace by Using Spectrogram

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### ABSTRACT

In this paper, spectrogram, a fast and accurate technique is introduced for the analysis of the contribution. Based on a rule-based classifier and the threshold settings that referred to the IEEE Standard 1159 2009, the analysis of the harmonic and interharmonic contribution of EAF are carried out successfully. Moreover, the impact of contribution is measured using total harmonic distortion (THD) and total non-harmonic distortion (TnHD). In addition, spectrogram also gives 100 percent correct detection and able to analyze the contribution impact. It is proven that the proposed method is accurate, fast and cost efficient for analyzing the impact of harmonic and interharmonic of EAF.

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## 1. INTRODUCTION

Presently electric arc furnace (EAF) is extensively used in iron and steel industry due to the increase in demand for iron such as in the vehicle industry.[1]. Electric arc furnace is used for melting alloys such as steel at high melting point [2]. Electrical energy is converted into thermal energy by electric arc furnaces during the melting of raw materials. Serious power quality problems occurred during the melting process whereas the random property of arc melting process and the control system are the fundamental reasons for the electrical and thermal dynamics [3]. The EAFs create the power quality issues such as unbalanced voltages and currents, voltage flickers as well as odd and even harmonics caused by the time-variant and non-linear loads [4]. The cause of harmonics is predominantly identified with the non-linear voltage-current characteristic of the arc. There is no current standard for identifying the dominant harmonic disturbances [5], [6].

The effect of the harmonic distortion caused several problems in electrical power systems, such as influence operation of devices, non-durable equipment, and increase losses in transmission and distribution networks, overvoltage and overcurrent [2]. As an EAF is a large source of harmonics, causes voltage-current distortion which is a major power quality issue that influences connected load operation in the electric network. Hence, harmonic analysis of EAF has attracted the attention of researchers to solve these power quality issues pertaining to EAF [6]. Harmonics can be analyzed using frequency, time and time-frequency domain methods [7]. The details of the concept and analytical of these methods are briefly explained in this

paper. There are several signal processing based method approaches have been proposed in harmonic detection analysis in order to assess the power quality issues [8].

A frequency-domain analysis method has been introduced called Fourier Transform (FT) [1]. The FT technique is usually used for the spectral and harmonics analysis [9]. The Fast Fourier Transform (FFT) is a reasonable approach for stationary signal, but it loses accuracy under time fluctuating frequency conditions and furthermore have picket and fence problems [10]. The short time Fourier transform (STFT) has overcome the deficiencies of FT by employing a time-frequency window to localize transient in a signal [9]. The Wavelet Transform (DWT) has been proposed by researchers to overcome the fixed resolution problem of STFT for analyzing power quality disturbances. Wavelet-Transform (WT) have been developed as time-frequency domain and it is very good in detecting the beginning of the transients. However, Wavelet Transform have a drawback which is incapable to give accurate result under a noise condition because of poor frequency resolution [8], [11]. A modified version of the STFT known as S-transform (ST) has been proposed for the recognition of power quality disturbance. S-transform is a superior tool to analyze transient disturbances [11]. However, the detection ability of ST also degrades in analyzing some non-stationary transient disturbances [9].

By concerning the mentioned limitations, this paper proposes time-frequency domain of harmonic analysis using spectrogram. The spectrogram is the squared magnitude of the STFT [16]. The point of interest is it involves a compromise between time resolution and frequency resolution. It is mean that a longer window provides less localization in time and more discrimination in frequency [12]. Therefore, it is an effective analyzing technique for voltage variation and capable to give the high precision of the result [11].

## 2. RESEARCH METHOD

### 2.1. Electric Arc Furnace

Large and continuously randomly varying nonlinear loads. The furnace arc impedance varies randomly and extremely asymmetrical since the carbon electrodes in contact with iron have dissimilar impedances between the positive and negative flows of current. The three-phase EAF model developed in Simulink is shown in Figure 1.

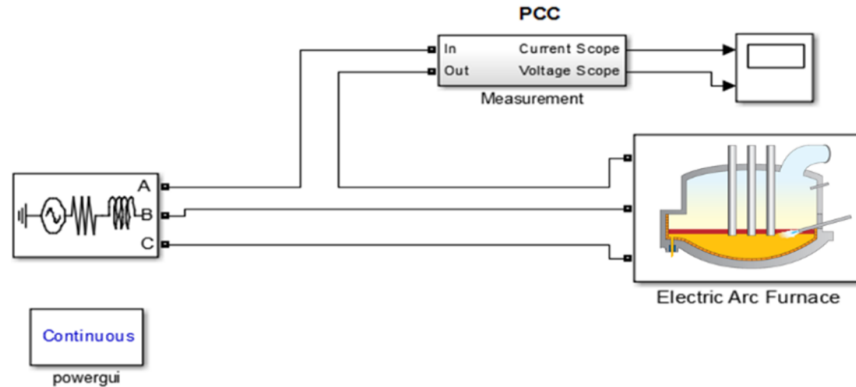


Figure 1. Electric arc furnace model

A controlled voltage source with the resistive and inductive network is used to couple the generated flicker disturbance to a given phase of the power system line. For a three-phase system, three sets of the controlled voltage source and resistive and inductive networks are required. The electric arc furnace model uses a hyperbolic model [13] defined in Equation 1, where  $V_{at}$  is the arc length threshold voltage,  $i$  is the phase current,  $C$  is the arc power, and  $D$  is the arc current

$$v(i) = \left( V_{at} + \frac{c}{D+|i|} \right) \text{sign}(i) \quad (1)$$

The effect of voltage flicker is determined by the threshold voltage shown in Equation (2), where  $V_{at0}$  is the base reference voltage when there is no arc activity,  $m$  is the modulation index, and  $\omega_f$  is the flicker frequency.

$$V_{at}(t) = V_{at0} [1 + m \cdot \sin(\omega_f t)] \quad (2)$$

The EAF model is modeled by using the MATLAB sinusoidal and function block and as displayed in Figure 2. To execute the simulation, the sinusoidal block frequency is set at 55.3 rad/sec, which is approximately 8.8 Hz. Whereby, this is the frequency that can cause the flickering effect and causes inconvenience to the human eye. The C value is 19 kW, while D is fixed at 5 kA and the threshold voltage is 200 V [13]. The model consists of 400V, 1MVA and 50 Hz.

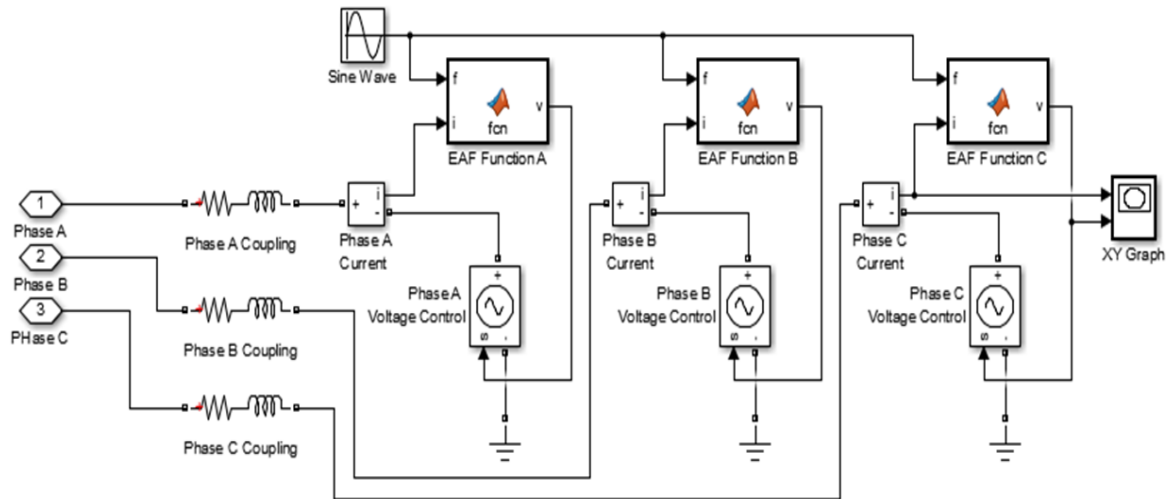


Figure 2. EAF subsystem block

### 2.2. Harmonic Signal Analysis

In the harmonic signal detection, there are four basic stages. The first stage is Time-Frequency Representation (TFR), whereas normalization of the measured signal is performed. The second stage, the signal parameters parameterization will be obtained in this. The third stage, with refer to the IEEE Std. 1159-2009, the signal characterization is implemented and the detection of the harmonic signal is the final stage of harmonic signal analysis.

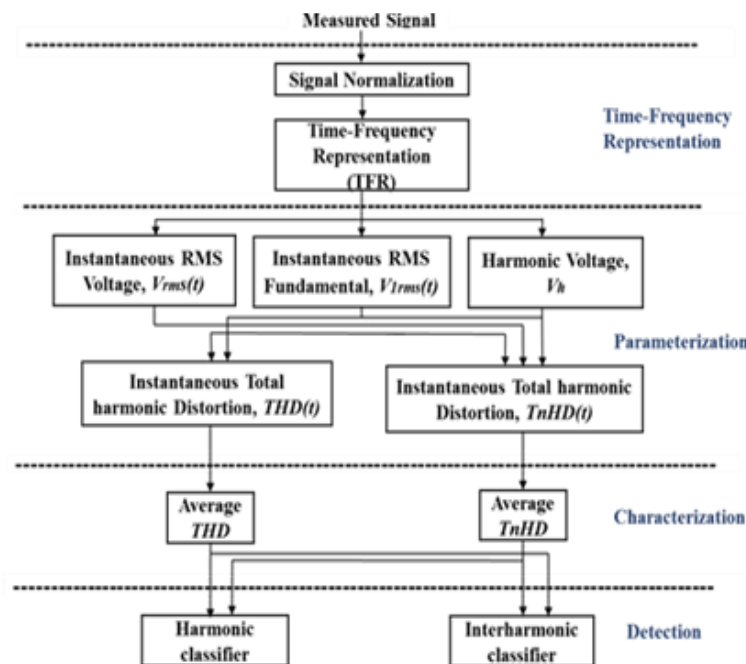


Figure 3. The process of harmonic signal analysis

### 2.3 Spectrogram

The spectrogram is one of the time-frequency representations (TFR) that represents a three dimensional of the signal energy with respect to time and frequency and it is obtained by squared modulus of the STFT. This method generally reflects how frequency content changes over the time. A smaller window size used to create a better time resolution, yet it correspondingly reduces the frequency resolution and it mathematically expressed as [14], [15], [20]:

$$P_x(t, f) = \left| \int_{-\infty}^{\infty} x(\tau) w(\tau - t) e^{-j2\pi f t} d\tau \right|^2 \quad (3)$$

Where  $x(\tau)$  is the input signal and  $w(t)$  is the observation window.

In this research, Hanning window is selected because of its lower peak side lobe which has a small impact on various frequencies around the fundamental value which is 50 Hz.

### 2.4. Signal Classification

The rule-based classifier is a deterministic grouping technique that utilized as a part of genuine application especially in signal classification. The deployment of rule-based classifier base on Equation 4 and 5 [14], [15],[18].

$$THD_{ave} > TnHD_{thres} \text{ and } TnHD_{ave} < TnHD_{thres} \quad (5)$$

$$TnHD_{ave} \geq TnHD_{thres} \text{ and } THD_{ave} < TnHD_{thres} \quad (6)$$

The existence of harmonic and interharmonic components distinguished by  $THD$  and  $TnHD$  indices, respectively. Furthermore, the implementation of signal classification plainly shows in Figure 4. The limitation of the threshold is based on IEEE std. 1159-2009 [19].

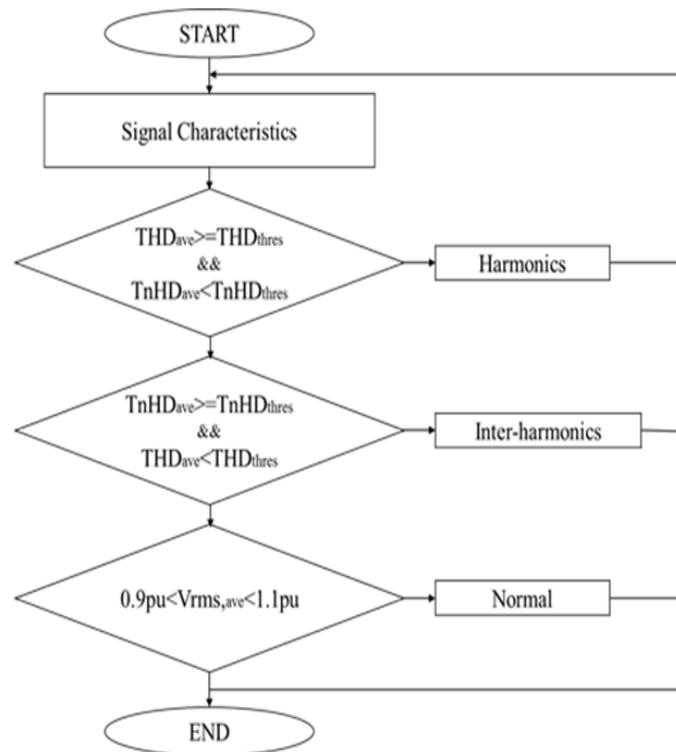
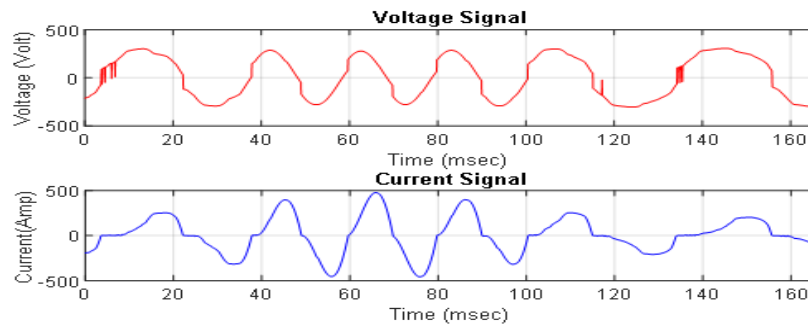


Figure 4. Flow chart of signal classification

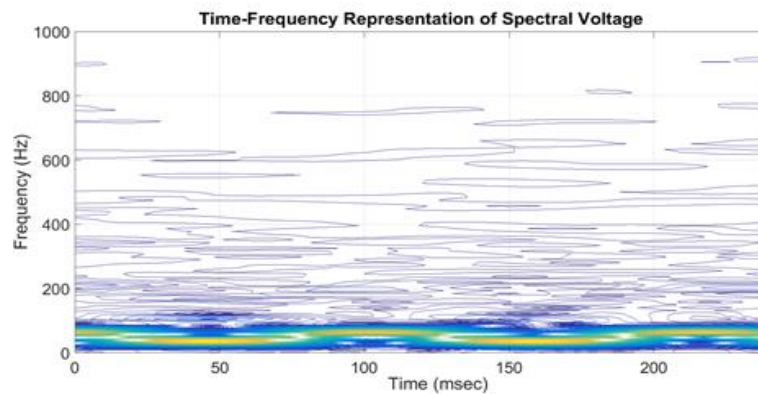
## 3. RESULTS AND ANALYSIS

In this section, it is explained and discuss comprehensively the results of research. Figure 5(a) demonstrates the sample of the instantaneous waveform of measured voltage and current at the PCC. According to the IEEE Std 519-2014, the measurement window width should be minimum of 10 cycles and

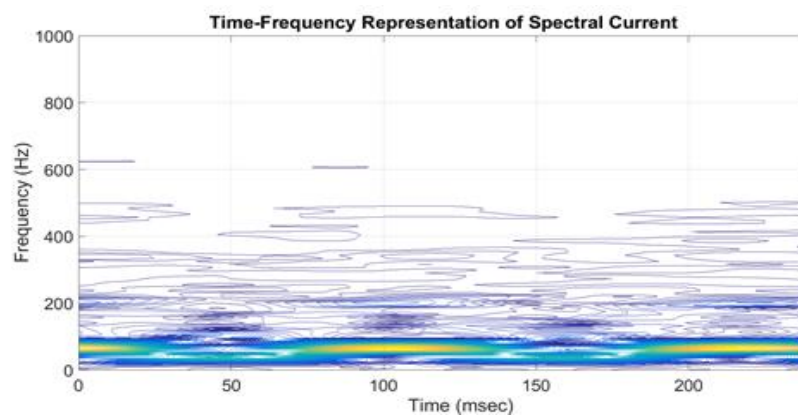
must consider harmonic components up to 50<sup>th</sup> order. With refer to the IEC 61000-4-7, a method based on the grouping concept of Harmonic Groups and Interharmonic Groups, minimum of 5 Hz frequency resolution is used in this study. Possibly the greatest challenge pertaining interharmonics is on the low-frequency and is necessary to examine the model and analysis technique due to determine the applicability to harmonics at a frequency below the fundamental frequency. The TFR of voltage and current are illustrating in Figure 5(b) and Figure 5(c). Nevertheless, using the spectrogram the harmonic and interharmonic components for voltage signal were distinguished from 75 Hz up to 975Hz. In the meantime, the harmonic and interharmonic components for current signal exist between 100 Hz to 625 Hz. To measure the distortion impact onto the system, the harmonic and interharmonic indices which are  $THD(t)$  and  $TnHD(t)$  are introduced. These indices are useful in identifying and to distinguish the harmonic and interharmonic impact in the system.



(a)



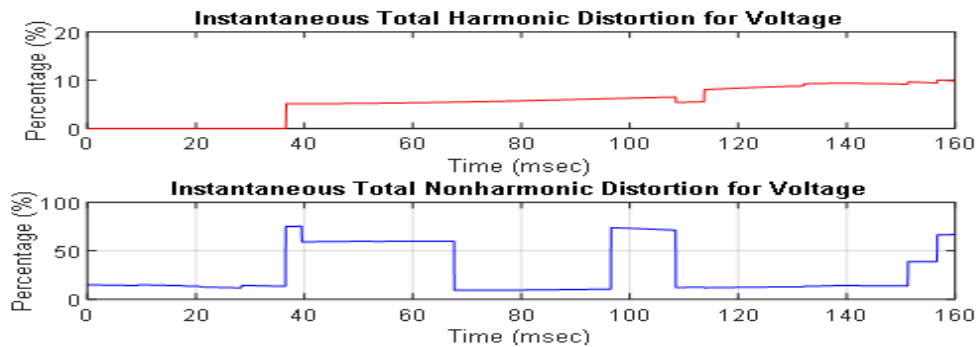
(b)



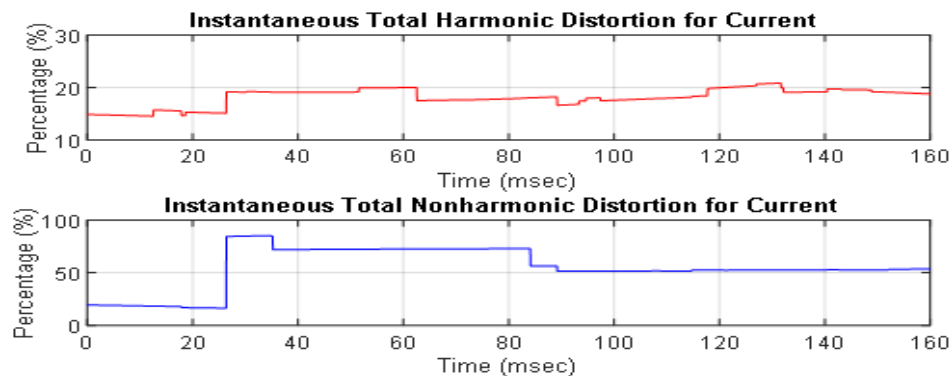
(c)

Figure 5. (a) Instantaneous voltage and current waveform at PCC, (b) TFR of the voltage signal, (c) TFR of the current signal

The harmonic and interharmonic indices are calculated using signal parameters that were obtained from the TFR of voltage and current. Figure 6(a) depicts the  $THD(t)$  and  $TnHD(t)$  of the voltage signal that were obtained from the spectrogram analysis. As can be understood from the figure, the  $THD_V(t)$  is in the range of zero percent to 10 percent, meanwhile, the  $TnHD_V(t)$  value varies from 10 percent to 70 percent, respectively. In the meantime, Figure 6(b) shows that the instantaneous  $THD_I(t)$  and  $TnHD_I(t)$  for the current signal which varies between 15 percent to 20 percent and 20 percent to 80 percent, correspondingly. According to the IEEE Standard 519-2014, any buses or PCC with a nominal voltage less than 1000 V, the limits may allow 8%  $THD_V$  and 5% individual voltage harmonic amplitude. It is shown that the  $THD_V$  has exceeded the standard limit values and the harmonic compensator is required due to improve the power quality. The 3-phase EAF has generated more harmonic distortion as the EAF does not have ground return and also using star connection for the three arc and during unbalanced condition which is in meltdown process, it will cause the harmonic and interharmonic components multiplicity generated.



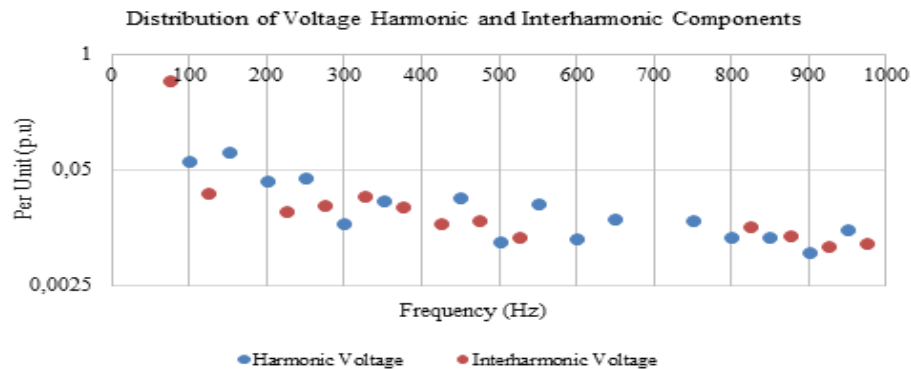
(a)



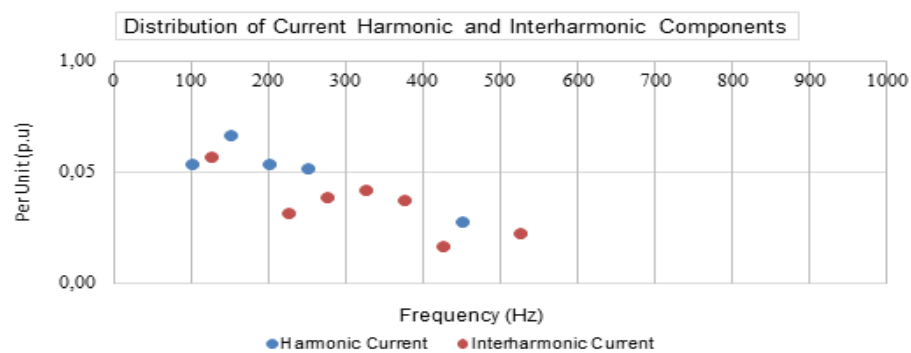
(b)

Figure 6. (a)  $THD_V(t)$  and  $TnHD_V(t)$ , (b)  $THD_I(t)$  and (d)  $TnHD_I(t)$ 

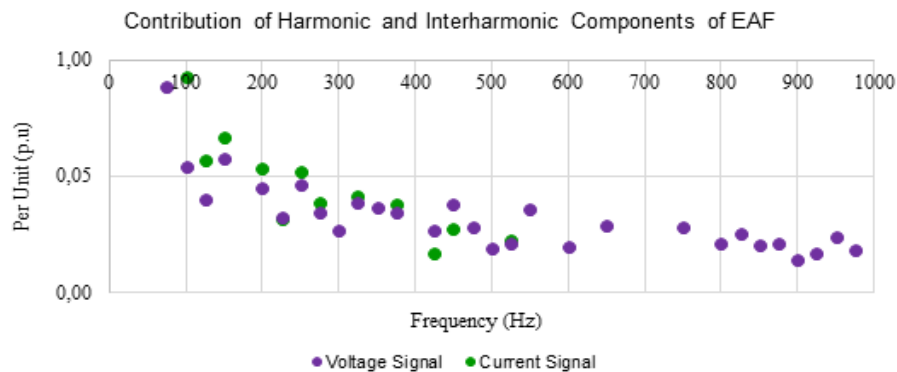
For a better understanding of the harmonic and interharmonic contribution of electric arc furnace in the system, a distribution of voltage and current harmonic and interharmonic components are obtained and observed from TFR. This is done by considering all integer harmonics up to 50<sup>th</sup> and interharmonic components with a minimum resolution of 5 Hz, it is clearly shown that the voltage signal comprises a large number of harmonic and interharmonic components compare to the current signal. Figure 7(a) shows the harmonic and interharmonic distribution of voltage. There are 16 voltage harmonic components while 13 voltage interharmonic components are distinguished in the voltage signal. Meanwhile, Figure 7(b) depicts 5 current harmonic components and 7 interharmonic components. It is observed that the interharmonic components dominantly in the current signal. However, in the voltage signal, the number of harmonic is greater than the interharmonic component. As can be seen from Figure 7(c), the contribution of harmonic and interharmonic of EAF shows that the EAF is considered a voltage harmonic and interharmonic source as well as discussed in [4],[7]. Establishing EAF model accurately is an important prerequisite for determining the impact of its harmonic contribution to the system. Using this model and the proposed method, it is observed that the analysis of harmonic and interharmonic contribution can be defined significantly.



(a)



(b)



(c)

Figure 7. (a) Distribution of EAF Current Harmonic and Interharmonic Components, (b) Distribution of EAF Voltage Harmonic and Interharmonic Components, (c) Contribution of Harmonic and Interharmonic Components by EAF

#### 4. CONCLUSION

The analysis of the harmonic and interharmonic contribution of EAF in the distribution system by using spectrogram successfully implemented in this study. From the analysis, the spectrogram succeeds in distinguishing the harmonic and interharmonic components. In the meantime, the THD(t) and TnHD(t) indices of the signals are calculated using the signal parameters that been obtained from the TFR. The results show that the spectrogram is a fast and accurate in identifying the harmonic and interharmonic contribution. Hence, the spectrogram is an appropriate technique to be implemented for analyzing the harmonic and interharmonic contribution of the EAF.

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