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7 **Life Cycle Assessment of Advanced Oxidation Processes for Olive Mill Wastewater**  
8 **Treatment**

9  
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17  
18 **ABSTRACT**

19 The efficient management of biorecalcitrant agro-industrial effluents, such as olive mill  
20 wastewater (OMW), is a matter of concern along all Mediterranean countries. However,  
21 the applicability of any treatment technique is strongly related, apart from its  
22 mineralization and detoxification efficiency, to its joint environmental impacts. In this  
23 work, the life cycle assessment methodology was utilized to estimate the environmental  
24 footprint of three advanced oxidation processes (AOPs), namely UV heterogeneous  
25 photocatalysis (UV/TiO<sub>2</sub>), wet air oxidation (WAO) and electrochemical oxidation (EO)  
26 over boron-doped diamond electrodes, for OMW treatment. It was observed that both  
27 EO and WAO can be competitive processes in terms of COD, TPh and color removal.  
28 EO was found to be a more environmentally friendly technique as it yields lower total  
29 environmental impacts, including CO<sub>2</sub> emissions to atmosphere. The environmental  
30 impacts of all three AOPs show that human health is primarily affected followed by  
31 impacts onto resources depletion. All in all, it was found that the environmental  
32 sustainability of AOPs is strongly related to their energy requirements and that their  
33 total environmental impacts decline according to the following order: UV/TiO<sub>2</sub> > WAO  
34 > EO.

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2  
3 **Keywords:** LCA; olive mill wastewater; environmental impacts; photocatalysis;  
4 electrolysis; wet air oxidation  
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## 8 **1. Introduction**

9 The foodstuff processing industry based on olive oil extraction constitutes a large part  
10 of agro-industrial activities and is an economically important activity for many  
11 Mediterranean regions. However, this process results in seasonal large quantities of bio-  
12 recalcitrant wastewaters, that come from the vegetation water and the soft tissues of the  
13 olive fruits mixed with the water used in the different stages of oil production. All these  
14 wastewaters together with the industry wash-waters, make up the so-called olive mill  
15 wastewaters (OMW). The main environmental impacts of OMW derive from its high  
16 organic (COD values range between 45 - 170 g/L) and polyphenolic content (0.5 - 24  
17 g/L) that result in high ecotoxicity and strong antibacterial action (Chatzisyneon et al.,  
18 2009a and 2009b). The presence of these biorecalcitrant organic compounds together  
19 with the seasonal production of large OMW quantities (about  $4 \cdot 10^5$  m<sup>3</sup>/y in Greece)  
20 constitute the major obstacles in the efficient effluent management.

21 Up to now, the majority of agro-industrial effluents such as OMW were discharged to  
22 evaporation ponds where they are left to evaporate naturally with the most hazardous of  
23 all being the seepage of organic pollutants into groundwater (Avraamides and Fatta,  
24 2008; Komnitsas et al., 2011; Salomone and Ioppolo, 2012). The direct discharge of  
25 OMW to evaporation ponds was prohibited by Greek legislation. Olive mills operation  
26 is regulated by the new Laws 3982/11 and 4014/11 that establish a classification of  
27 olive mills according to their capacity and their environmental impacts and define the  
28 environmental commitments of each activity (Hellenic Republic, 2011a and 2011b).  
29 These are further specified by the Joint Ministerial Decision 15/4187/266 (Hellenic  
30 Republic, 2012) where it is made clear to olive mill operators that OMW has to undergo  
31 pre-treatment in order to reach an organic load of about 1 g/L COD, thus it can be safely  
32 discharged to evaporation ponds or be reused after further treatment. Hence, researchers  
33 have been focused on the investigation of new treatment strategies that would efficiently  
34 treat OMW and safely discharge it to the environment.

1 A great variety of physical, chemical, thermal and biological processes, as well as  
2 several combinations of them, have been investigated for OMW treatment aiming at  
3 removing the organic matter from the liquid phase in order to make it acceptable for  
4 discharge into the environment. Among them, advanced oxidation processes (AOPs)  
5 have been extensively studied regarding their efficiency to treat OMW, while it is  
6 generally accepted that a process train comprising aerobic/anaerobic biological and  
7 advanced oxidation processes may be the only viable option to treat OMW  
8 (Mantzavinos and Kalogerakis, 2005). Generally, research efforts have been mainly  
9 directed towards the investigation of the operating conditions of AOPs that affect OMW  
10 mineralization and/or detoxification (Chatzisyneon et al., 2009c; Mert et al., 2010),  
11 while there are few studies comparing several processes, including AOPs, from the  
12 economical point of view (Cañizares et al., 2009). However, when designing or  
13 planning a new technology its environmental impacts should be taken into account,  
14 which have not yet been identified for OMW treatment. Therefore, a comparison of  
15 AOPs environmental impacts for agro-industrial effluents treatment is a highly  
16 important subject that is still pending.

17 Regarding wastewater treatment, AOPs have been primarily proposed as a pre- or post-  
18 treatment step to destruct the most bio-recalcitrant organic substances before or after  
19 further biological or physicochemical treatment (Chatzisyneon et al., 2009b).  
20 Comninellis et al. (2008) declared that the higher the polluting load and the extent of  
21 pollution removal needed, the harsher the treatment conditions to be applied are. In this  
22 view, OMW treatment performance can be enhanced only by coupling several of the  
23 above processes including AOPs.

24 The goal and scope of this work is to utilize the life cycle assessment (LCA)  
25 methodology in order to assess the environmental footprint of several AOPs in bench-  
26 scale, under Greek conditions, to identify their advantages and disadvantages in terms  
27 of their environmental impacts, compare them and provide feedback on the most  
28 sustainable process for future scaling-up of the OMW treatment facilities. For this  
29 purpose, three advantageous, regarding organics degradation efficiency, AOPs, for  
30 wastewater treatment, namely UV heterogeneous photocatalysis (UV/TiO<sub>2</sub>), wet air  
31 oxidation (WAO) and electrochemical oxidation (EO) over boron-doped diamond  
32 electrodes, were studied. However, the environmental footprint of each of these  
33 techniques has to be taken into account to get a thorough picture of the whole problem.  
34 Up to now and to the authors' best knowledge, there is no published research dealing

1 with this subject. Moreover, these techniques were compared in terms of organics  
2 degradation efficiency and energy requirements in order to assess their overall  
3 performance from both an environmental and technical point of view.

## 4 5 **2. Materials and Methods**

### 6 **2.1 Description of the studied wastewater**

7 The OMW was once collected by a three-phase olive oil mill company, located in  
8 Chania, Western Crete, Greece. The effluent was subjected to filtration to remove most  
9 of its total solids and it was then kept at 4°C, to ensure that its physicochemical  
10 characteristics will not be lessened or weathered. The effluent had a strong malodor of  
11 degraded olive oil, a dark black-brown color and its main properties prior to and after  
12 filtration are given in Table 1.

13  
14 Table 1.

15  
16 It has to be noted that OMW sample was diluted with distilled water to achieve the  
17 appropriate initial COD value as shown in Table 2.

### 18 19 **2.2 Experimental runs**

20 This work is based on previously published experimental studies used to derive optimal  
21 operating parameters for three common AOP systems, namely photocatalytic  
22 (UV/TiO<sub>2</sub>), electrochemical and wet air oxidation. The main parts and characteristics of  
23 these systems are given at Table 2. More details regarding the experimental set-ups,  
24 their operating mode and conditions of the oxidation processes are given in  
25 Chatzisyneon et al. (2009a, 2009b and 2009c). To meet these operating standards (i.e.  
26 initial COD), AOPs should be utilized as part of a treatment battery incorporating  
27 various physicochemical and biological processes as can schematically be illustrated in  
28 Figure 1.

29  
30 Figure 1.

31  
32 Keeping in mind the potential use of these processes in train treatment schemes (Figure  
33 1), it was decided to investigate whether the bench-scale experimental data obtained  
34 from our previous publications (a summary of which is shown in Table 2) can be used

1 to scale-up the process and further perform an LCA at larger scale. Therefore, a pre-  
2 design cost estimation of the three AOPs was performed for a prospective industrial  
3 AOP treatment plant for OMW treatment. Generally, direct scaling-up from laboratory  
4 to industrial scale bears serious calculating inaccuracies. Hence, performance of the  
5 AOPs technologies should take place at pilot-scale first, before any further larger-scale  
6 application. However, the proposed pre-designing cost methodology can be a useful tool  
7 for researchers to get an indicative view of treatment expenses when scaling-up such  
8 processes.

### 10 **2.3 Impact assessment methodology**

11 The software package SimaPro 7.3.3 (PRe Consultants, 2012) was used in this work and  
12 the mandatory (selection of impact categories, category indicators and characterization  
13 models, classification, and characterization) and optional (normalization, grouping, and  
14 weighting) elements of the life cycle impact assessment (LCIA) according to ISO 14040  
15 were utilized (ISO 14040, 2006; Tsoutsos et al., 2010; Foteinis et al., 2011).  
16 Furthermore, two impact assessment methods were used and these are IPCC 2007  
17 version 1.02 and ReCiPe version 1.06. The first one compares processes based on CO<sub>2</sub>  
18 emissions equivalent (CO<sub>2</sub>-eq), used to measure global warming potential (GWP),  
19 which is a standard indicator of environmental relevance. The ReCiPe framework,  
20 which encompasses GWP indicator, is the most recent impact assessment method that  
21 exhibits certain advantages comparing to other approaches, such as Eco-Indicator 99.  
22 The primary advantage is that ReCiPe comprises a broadest set of midpoint impact  
23 categories, including several environmental issues, one of them being GWP, to assess  
24 sustainability (Goedkoop et al., 2009). Analytically, the ReCiPe method can transform  
25 the life cycle inventory (LCI) results into a limited number of indicator scores that are  
26 expressed per environmental impact category and also as an aggregated single score.  
27 Furthermore the results were simulated using the three different perspectives, namely  
28 individualist (I), hierarchist (H) and egalitarian (E). The latter was finally chosen to  
29 evaluate the results, since it takes into account the long term, precautionary  
30 environmental impacts, which better corresponds to the scope of this study.

#### 32 **2.3.1 System boundaries**

33 First of all, the system boundaries for each AOP were determined (Figure 2). In this  
34 study, OMW generation and its transportation to the laboratory were not included inside

1 the boundaries, since AOPs can be applied as an onsite treatment nearby the olive mill.  
2 Finally, since this work refers to experiments that were carried out in laboratory-scale,  
3 land use was not taken into account. The main system flows of this work were: (i) the  
4 energy inputs (electricity provided from the local grid), (ii) the three laboratory units,  
5 (iii) the materials that were used (TiO<sub>2</sub>, oxygen, etc.), and (iv) their outputs to nature.  
6 Another important factor that should be taken into consideration is the CO<sub>2</sub> formed  
7 during OMW treatment. These CO<sub>2</sub> emissions were left outside of the system  
8 boundaries of this work because: (i) partial oxidation primarily occurs as evidenced by  
9 the relatively moderate COD decrease (18 - 34%), therefore total oxidation reactions  
10 that emit CO<sub>2</sub> are very limited, and (ii) there are no data in the literature that one could  
11 use to measure accurately the extent of total oxidation reactions (i.e. CO<sub>2</sub> emissions)  
12 during OMW treatment by AOPs.

13  
14 Figure 2.  
15

### 16 **2.3.2 Functional unit**

17 Treatment of 1 L of OMW was taken as the functional unit and the three oxidation  
18 processes were compared according to their yield in removing the two main  
19 environmental indicators of OMW, namely COD and TPh. COD is the first indicator  
20 since OMW with values higher than 1 g/L cannot be safely discharged to evaporation  
21 ponds or be reused. Although TPh are part of the COD they are considered as the  
22 second indicator and are examined separately, since if they are left untreated they are  
23 gradually oxidized and/or polymerized rendering OMW highly toxic and biorecalcitrant  
24 (Chatzisyneon et al., 2009b). Hence, AOPs were compared according to their  
25 environmental impacts in removing 1 g of COD and 1 g of TPh per liter of treated  
26 OMW. Finally, AOPs were also compared according to their efficiency in removing  
27 both pollutants. It has to be noted that COD and TPh removal depended on both the  
28 initial physicochemical characteristics of OMW and the applied AOP. Each applied  
29 AOP required different treatment time, energy consumption and was applied for  
30 different effluent volumes, while COD and TPh removal fluctuated, as shown in Table  
31 2. Therefore, laboratory results were normalized to appropriate functional units, namely  
32 the removal of 1 g of COD and 1 g of TPh per liter of treated OMW (Table 2).

### 34 **2.3.3 LCI**

1 The inventory of the three laboratory units is analytically shown in Table 2.  
2 Specifically, the UV/TiO<sub>2</sub> laboratory unit includes a 400 W high-pressure mercury lamp  
3 with a lifespan of 5,000 h, as well as TiO<sub>2</sub> and oxygen. WAO inventory includes an  
4 alloy C-276 high-pressure reactor with a life span of 20 years (Parr Instruments, USA)  
5 and EO inventory includes a DiaCell® (type 100) single-compartment electrolytic flow-  
6 cell manufactured by Adamant Technologies with a life span of 10 years. The  
7 aforementioned inventory was simulated using the Ecoinvent v2.2 database.

8  
9 Table 2.

10  
11 It should be noted that due to the generally high life span of the three laboratory units  
12 their embodied energy (associated with producing the AOP treatment systems) is lower  
13 compared to their operating energy requirements and, therefore, most impacts are  
14 attributed to their operating energy. Moreover, another issue that needs to be mentioned  
15 is that electricity in Greece is currently provided by lignite (54%), oil (11%) and natural  
16 gas (17%), while only 18% is provided by renewables (European Commission, 2012).

17 Regarding WAO treatment, electrical energy is consumed during air compression,  
18 effluent mechanical stirring and heating of the reactor. In the present study, it was  
19 assumed that energy is mainly consumed for reactor heating and, therefore, any other  
20 electrical power requirements were considered as negligible.

21 Finally, during previous studies of our group the operating parameters that significantly  
22 affected UV/TiO<sub>2</sub>, WAO and EO efficiency were estimated by utilising a factorial  
23 design methodology to perform and interpret the results. Based on this methodology the  
24 optimal operating parameters that would bring the best process performance for the  
25 same OMW sample were estimated.

26 It was found that both EO and WAO can be competitive processes in terms of organics  
27 degradation efficiency. However, it should be mentioned that AOPs will be applied in  
28 combination with a suitable process (i.e. physical, biological, etc.) for an integrated  
29 OMW treatment. Hence, apart from the high degradation efficiency of the process, other  
30 important aspects including environmental impacts, should be taken into consideration  
31 in order to proceed and decide on the most suitable oxidation technique for OMW  
32 treatment. In respect of this, an LCA methodology was utilized to assess the  
33 environmental impacts of each process.



### 3. Results and Discussion

#### 3.1. LCIA results

LCIA is shown in Figure 3 for egalitarian where one can see the main contributions to the three processes; it is evident that the contribution of energy consumption to the UV/TiO<sub>2</sub> process is higher than the other two.

Figure 3.

Moreover, the results in terms of GWP for a timeframe of 100 years for the removal of 1 g/L COD and 1 g/L TPh are shown in Figure 4.

Figure 4.

It is obvious that EO is the most environmentally friendly AOP both in terms of COD and TPh removal. Specifically for the removal of 1 g COD, EO releases only 0.16 kgCO<sub>2</sub>eq per liter of treated OMW, while the respective value for WAO is 0.88 kgCO<sub>2</sub>eq. Besides, the UV/TiO<sub>2</sub> process exhibits the highest CO<sub>2</sub>eq emissions since it releases 5.2 kgCO<sub>2</sub>eq per liter of treated OMW. Regarding TPh removal, the results are consistent with those of COD removal; EO is more sustainable than UV/TiO<sub>2</sub> and WAO, releasing 1.24 kgCO<sub>2</sub>eq per liter of treated OMW. WAO and heterogeneous photocatalysis emit 3 and 14.63 kgCO<sub>2</sub>eq per liter of treated OMW, respectively, showing that the latter exhibits an order of magnitude greater GWP than the other two AOPs. This is consistent with the results reported by Chong et al. (2012) who compared several AOPs, including UV/TiO<sub>2</sub>, for decentralized wastewater treatment. They found that CO<sub>2</sub> releases to the atmosphere were higher for UV-based than other AOPs. GWP is strongly related to energy consumption as this is the main reason for increased CO<sub>2</sub> emissions worldwide (Forster et al., 2007). At this point it is worth noticing the fact that the GWP of the three oxidation processes is proportional to their energy consumption. Hence, the lower CO<sub>2</sub>eq emissions during the EO treatment are primarily attributed to the fact that the energy requirements for EO are lower than those for WAO and UV/TiO<sub>2</sub> (Table 2). Hence, the examined AOPs environmental impacts, in terms of their GWP, decline in the order: UV/TiO<sub>2</sub> > WAO > EO, rendering EO a more sustainable and likely to be applied technology than the other two. Therefore, it is concluded that the environmental sustainability of AOPs is strongly related to the

1 energy requirements of these technologies. This statement is consistent with the results  
2 reported by other researchers (Munoz et al., 2005 and 2006; Vince et al., 2008; Chong  
3 et al., 2012; Kohler et al., 2012) who observed that AOPs are more energy-intensive  
4 than material-intensive processes and, consequently, the energy consumption is the  
5 stage that generates the main environmental impacts. In the aforementioned studies,  
6 energy consumption was found to carry the highest environmental burden for several  
7 water and wastewater treatment plants either at laboratory or larger scales.

8 The aforementioned findings regarding GWP were also confirmed when the results  
9 were interpreted utilizing the ReCiPe method. This was used to provide a more holistic  
10 impact assessment of the overall process including the severity of each environmental  
11 impact onto human health, ecosystem and resources. The ReCiPe method transforms the  
12 LCI results into a broadest number of impact categories including the GWP  
13 environmental impact. Moreover, the key advantage of the ReCiPe method lies within  
14 the fact that it takes into account the severity of each impact category to assess the  
15 environmental sustainability of the process. Hence, the single and aggregated  
16 environmental impacts during the AOPs treatment, based on the ReCiPe method, for 1 g  
17 COD and 1 g TPh removal per liter of treated OMW, are presented in Figures 5 and 6.

18  
19 Figure 5.

20  
21 Figure 6.

22  
23 Concerning both COD and TPh removal, it is observed that human toxicity impact  
24 category yields a higher score for the UV/TiO<sub>2</sub> process (Figure 5) than the other two.  
25 All other impact categories are not affected, in relative terms when compared to human  
26 health, by the OMW treatment technique. Furthermore, WAO shows higher severity  
27 level for human toxicity impact category, although it is about 83% lower for COD and  
28 79% lower for TPh removal than UV/TiO<sub>2</sub>. Yet, its environmental impact on fossil  
29 depletion and climate change human health categories can be assumed as very low.  
30 Moreover, EO achieves lower environmental impacts in terms of human toxicity  
31 impact. For example, it is about 97% and 81% lower than UV/TiO<sub>2</sub> and WAO,  
32 respectively for the removal of 1 g COD per liter of treated OMW. Additionally, it is  
33 worth noticing that EO poses very low environmental impacts to the other impact  
34 categories (Figure 5). There is no doubt that the most significant environmental impact

1 during OMW treatment is human toxicity for all the considered processes. This is  
2 primarily associated with the energy consumed during AOPs. Electricity in Greece is  
3 predominantly (i.e. 82%) provided by lignite, oil and natural gas, while only 18% is  
4 provided by renewable energy sources (European Commission, 2012). This mixture  
5 enhances (i) the production of toxic and hazardous by-products released to atmosphere  
6 and the aquatic environment, and (ii) the accumulation of greenhouse gases, thus  
7 increasing the impact of toxicity to humans. The aggregated impact categories  
8 according to the ReCiPe methodology can be seen in Figure 6, where UV/TiO<sub>2</sub> has the  
9 highest score of environmental impacts onto human health, indicating the low  
10 environmental sustainability of a bench-scale UV/TiO<sub>2</sub> laboratory unit operating under  
11 Greek conditions, when this is compared with EO or WAO. The main reason for this is  
12 that the bench-scale UV/TiO<sub>2</sub> laboratory unit is energy-intensive and utilizes non-  
13 environmentally friendly materials (high-pressure mercury lamp). Therefore, a scale-up  
14 unit should focus in reducing its energy demand by utilizing alternative and renewable  
15 energy sources or even move towards the use of solar energy as an irradiation source.  
16 These would make photocatalytic process a highly competitive technique for OMW  
17 treatment. Figure 6 also shows that EO achieves lower environmental impacts onto  
18 human health than the other two while the other damage categories are less affected by  
19 this process, thus leaving a considerable environmentally friendly footprint during  
20 OMW treatment. Accordingly, EO is a more environmentally friendly oxidation process  
21 for OMW treatment, while WAO follows with its total environmental impacts being  
22 twice and four times as much, in terms of TPh and COD removal, respectively.

23

#### 24 **4. Conclusions**

25 The ultimate goal of this work was to identify the key environmental  
26 hotspots of three AOPs using LCA in order to provide feedback to  
27 support the sustainable development of future AOP units for scaling-up. The main  
28 conclusions drawn from this work are summarized as follows:

- 29 • The environmental sustainability of AOPs is strongly related to the energy  
30 requirements of these technologies, thus an increase of the process energy  
31 consumption enhances the environmental impacts of the whole process. This is  
32 consistent with results obtained by other researchers (Munoz et al., 2005 and 2006;  
33 Vince et al., 2008; Chong et al., 2012; Kohler et al., 2012) as AOPs are energy-  
34 intensive techniques.

- 1 • AOPs environmental impacts, in terms of their GWP and total environmental  
2 impacts, decrease in the order: UV/TiO<sub>2</sub> > WAO > EO, rendering EO a more  
3 sustainable technology, which may be applied for OMW treatment.
- 4 • UV/TiO<sub>2</sub> process was found to yield higher score onto human health, fossil  
5 resources and the ecosystem on our bench-scale laboratory unit operating under  
6 Greek conditions. Therefore, future studies should deal with the identification of the  
7 environmental impacts of a scaled-up heterogeneous photocatalysis system with  
8 different energy mixtures and especially renewable energy. On the other hand, EO  
9 shows lower overall environmental impacts onto human health, thus it can be  
10 considered as a more viable and sustainable option to reduce the organic load of  
11 OMW than the other two processes.

12

13 Overall, this work provides decision makers with a feedback regarding the  
14 environmental impacts of various AOPs when applied at bench-scale. So far, the  
15 selection of treatment technologies for agro-industrial effluents has been based on  
16 technical, socioeconomic and political criteria. The need to improve sustainability of the  
17 wastewater management and introduce environmental criteria in the decision making  
18 process is inevitable. Hence, this feedback will be beneficial for a potentially OMW  
19 treatment system implemented at large scale.

20

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1 **List of Tables**

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3 Table 1. Properties of OMW used in this study.

4

5 Table 2. Life cycle inventory and organics degradation efficiency for the three AOPs at  
6 optimal operating parameters.

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9



1 Table 1.

<b>Physicochemical characteristics</b>	<b>OMW before filtration</b>	<b>OMW after filtration</b>
COD, g/L	47	40
Total phenols (TPh), g/L	8.1	3.5
Total solids, g/L	50.3	0.6
pH	4.6	4.4
Conductivity, mS/cm	17	18

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2 Table 2.

	<b>AOP</b>		
	<b>UV/TiO<sub>2</sub></b>	<b>WAO</b>	<b>EO</b>
<b><i>Experimental set-up configuration</i></b>			
Reactor type	Immersion-well	high-pressure reactor (Parr Instruments, USA)	DiaCell® (type100)
Reactor material	Borosilicate glass	Alloy C-276	Boron-doped diamond on silicon
Reactor inputs	UVA-400 W high pressure mercury lamp (Osram, HQL, MBF-U)	25 kg Alloy C-276 2.5 kg Polypropylene	0.26 g Diamond 0.1 g Boron 0.15 kg Silicon 1.6 kg Steel 0.7 kg Polypropylene
<b><i>Operating parameters</i></b>			
Treatment Time, h	4	1	7
COD initial, g/L	5.1	8.1	10
OMW volume, L	0.35	0.35	10
[TiO <sub>2</sub> -P <sub>25</sub> ], g/L	2	-	-
Charge passed, mA/cm <sup>2</sup>	-	-	286
Temperature, °C	27	180	27
Pressure, atm	1	24.7	1
<b><i>Organics removal yield</i></b>			
COD removal (%)	18	34	28
TPh removal (%)	63	94	40
Decolorization (%)	66	74	33
<b><i>Energy requirements</i></b>			
Energy from the Greek grid	Lignite (54%), Oil (11%), Natural gas (17%), Renewable sources (18%)		
kWh for 1 g COD per L OMW removed	5	0.8	0.15
kWh for 1 g TPh per L OMW removed	14.2	2.9	1.2

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1 **List of Figures**

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3 Figure 1. Simplified scheme of the train treatment techniques for OMW treatment.

4

5 Figure 2. System boundaries of this work. (a) EO; (b) UV/TiO<sub>2</sub>; (c) WAO

6

7 Figure 3. Dendrogram of the processes and their main contributions to environmental  
8 impacts for the removal of 1 g/L COD.

9

10 Figure 4. Global warming potential (GWP) in CO<sub>2</sub> equivalents for a timeframe of 100  
11 years for the removal of 1 g/L COD and 1 g/L TPh for the three oxidation processes.

12

13 Figure 5. Severity of impact categories according to the ReCiPe methodology for the  
14 removal of 1 g/L COD and 1 g/L TPh, for the three oxidation processes.

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16 Figure 6. Severity of aggregated damage categories according to the ReCiPe  
17 methodology for the removal of 1 g/L COD and 1 g/L TPh, for the three oxidation  
18 processes.

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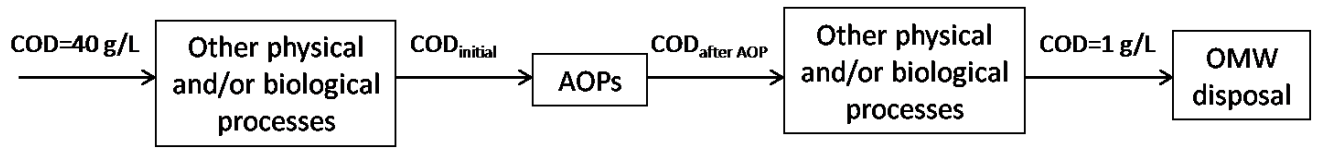
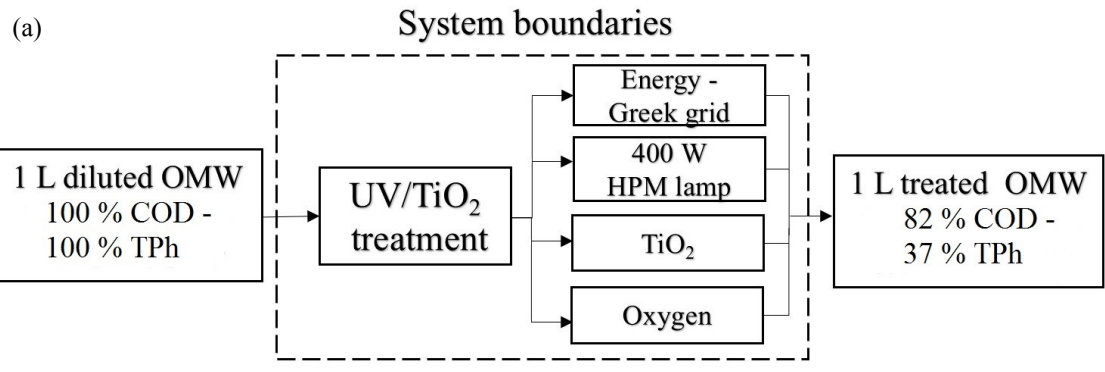
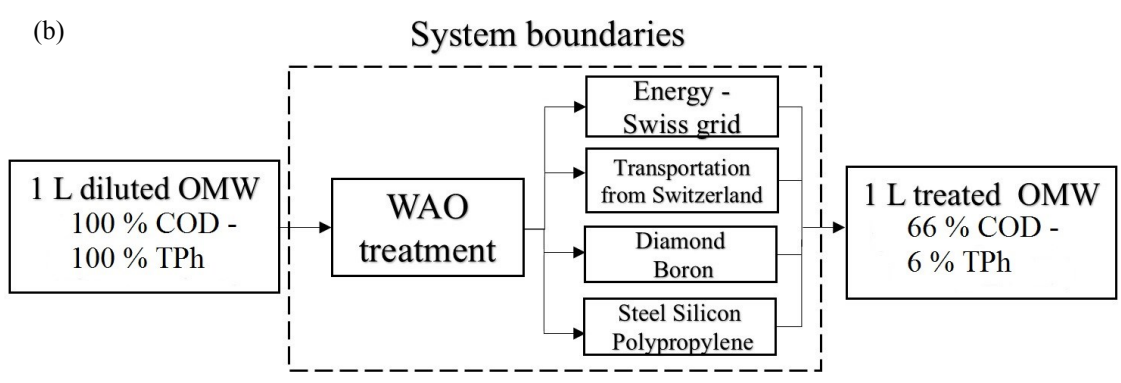


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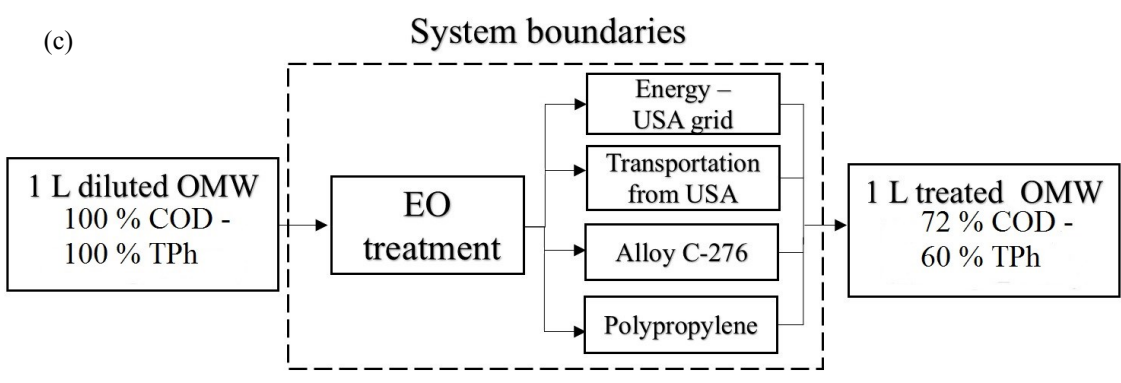
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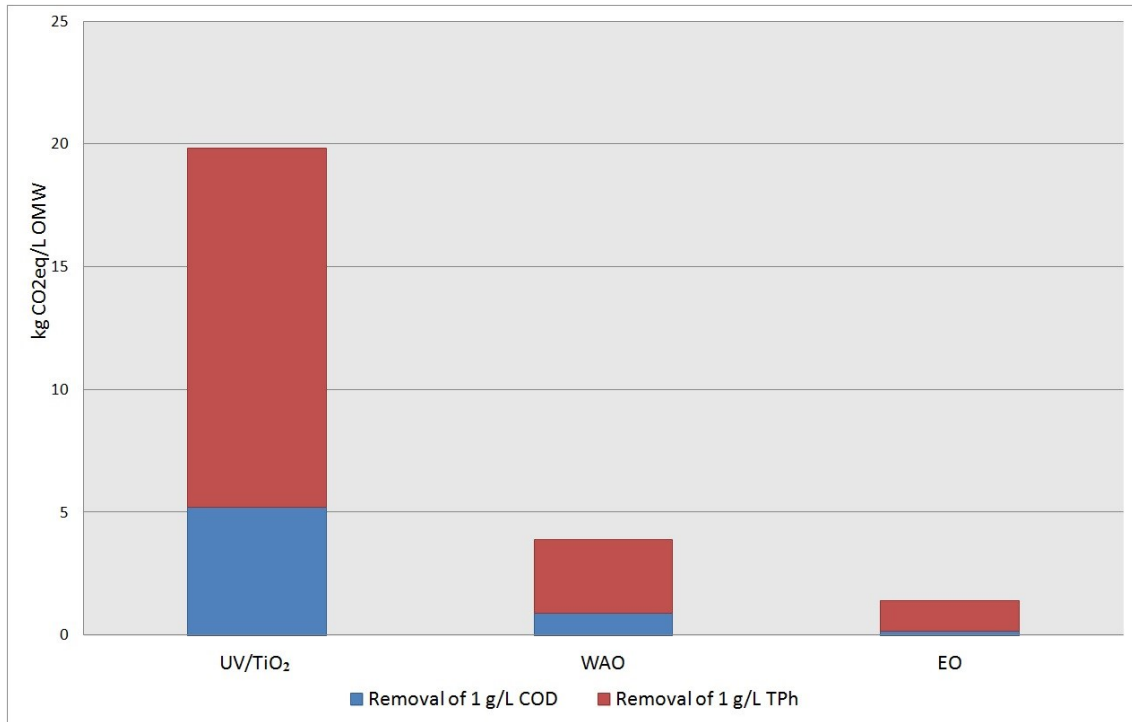
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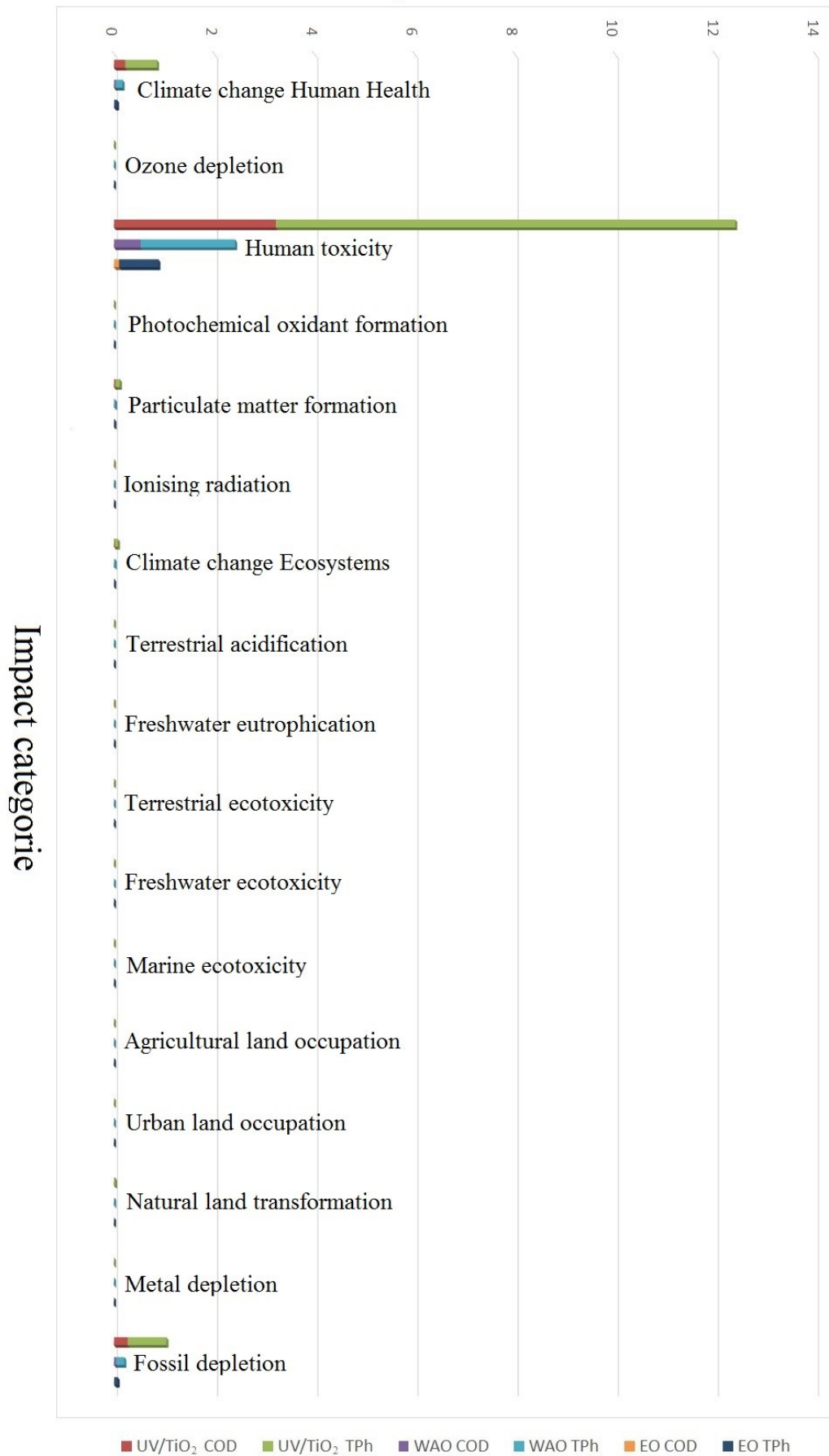
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Figure 4.

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# Impact score





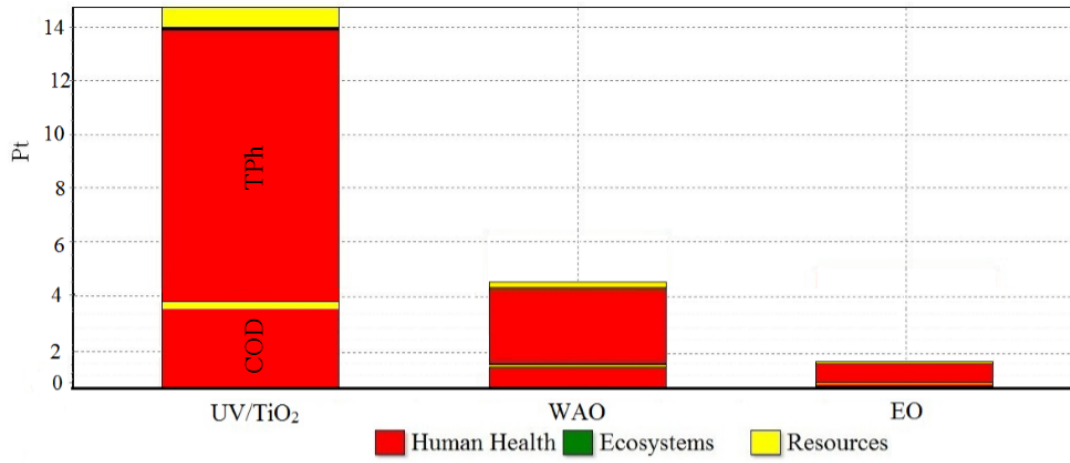
1 Figure 5.

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8 Figure 6.