HASAN KALYONCU UNIVERSITY GRADUATE SCHOOL OF NATURAL & APPLIED SCIENCES

GEOTECHNICAL MAPPING INVESTIGATION OF A DEVELOPING URBAN AREA (NIGDE, TURKEY)

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Geotechnical mapping investigation of a developing urban area (Niğde, TURKEY)

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Civil Engineering

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GRADUATE SCHOOL OF NATURAL & APPLIED SCIENCES INSTITUTE M.Sc. ACCEPTANCE AND APPROVAL FORM

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ABSTRACT

GEOTECHNICAL MAPPING INVESTIGATION OF A DEVELOPING URBAN AREA (NIGDE, TURKEY)

ERBIL, Merve M.Sc. In Civil Engineering Supervisor: Prof. Dr. Ömer ARIÖZ Co. Supervisor: Assist. Prof. Dr. Fatih ÇELİK June 2019, 116 Pages

Definitions of urban geotechnical environments are usually required to provide information about an engineering basis for planners and design engineers in order to prepare a rational land use planning and developing urban areas. Therefore, a engineering geotechnical mapping method can be a beneficial way for defining the urban geotechnical environments as visually. In this thesis, Engineering Geotechnical Mapping Method (EGMM) was used for Niğde city (in Turkey) so as to investigate and present the geotechnical data that were collected from 45 unpublished reports, mostly extracted from geotechnical investigation reports. The main indispensable parameters for geotechnical design engineers such as lithology and topography of the area, water table depth, bearing capacity of the soils, liquefaction of the soils and some critical geotechnical parameters were noted for the preparation of the geotechnical maps. The Geographically Information System (GIS) was used in order to rearrange and control all this information, and also to prepare engineering geotechnical maps.

Key words: Urban Geotechnics, GIS, Geotechnical Mapping, Liquefaction.

ÖZET

YERLEŞİM ALANLARININ GELİŞTİRİLMESİNDE GEOTEKNİK HARİTALAMA YÖNTEMİNİN KULLANILMASI (NİĞDE/TÜRKİYE)

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Yüksek Lisans, İnşaat Mühendisliği Bölümü Tez Danışmanı: Prof. Dr. Ömer ARIÖZ Yardımcı Tez Danışmanı: Dr. Öğr. Üyesi Fatih ÇELİK Haziran 2019, 116 Sayfa

Kentsel yerleşim yerlerinde geoteknik parametrelerin tanımlanması, bu kentlerde doğru imar planlarının yapılması ve kentsel alanların geliştirilmesi için şehir plancıları ve tasarım mühendisleri için mühendislik parametreleri hakkında bilgi vermek için gereklilik arz eder. Bu nedenle geoteknik haritalama yöntemi, bu arazilerde geoteknik parametreleri görsel olarak tanımlamanın faydalı bir yolu olabilir. Bu çalışmada Niğde ili (Türkiye) için Mühendislik Geoteknik Haritalama Yöntemi (EGMM), daha önce yayınlanmamış 45 zemin etüt raporundan toplanan ve çoğunlukla geoteknik araştırma raporlarından elde edilen geoteknik verilerin araştırılması ve sunulması amacıyla kullanılmıştır. Geoteknik haritaların hazırlanmasında, alanın litolojisi ve topografyası, su tablası derinliği, zemin taşıma kapasitesi, zemin sıvılaşması ve bazı kritik geoteknik parametreler gibi geoteknik tasarım mühendisleri için vazgeçilmez parametreler incelenmiştir. Coğrafi Bilgi Sistemi (GIS), tüm bu bilgileri yeniden düzenlemek ve kontrol etmek ve ayrıca mühendislik geoteknik haritaları hazırlamak için kullanılmıştır.

Anahtar Kelimeler: Kentsel geoteknik, GIS, Geoteknik haritalama, Sıvılaşma.



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LIST OF SYMBOLS /ABREVIATIONS

| ASTM | American society for testing and materials |
|----------------------|---|
| В | Width of foundation |
| c | Cohesion of soil |
| С | Species of rocks according to constant of material |
| СН | Inorganic clays of high plasticity, fat clays |
| CL | Inorganic clays of low to medium plasticity, gravely clays, sand clays, |
| | silty clays, lean clays. |
| D_{f} | Depth of foundation |
| EGMM | Engineering Geotechnical Mapping Method |
| GIS | Geographically Information Systems |
| Е | Void ratio |
| n | Porosity |
| Ν | Number of strikes from SPT experiment |
| N_c, N_q, N_γ | Terzaghi bearing capacity factors |
| LL | Liquid Limit |
| k_1 and k_2 | Foundation shape coefficients |
| PI | Plasticity index |
| PL | Plastic Limit |
| Q | Ultimate bearing capacity of soil |
| SM | Silty sands, sand-silt mixtures |
| SPT | Standard Penetration Test |
| Sr | Saturation degree |
| Φ | Internal friction angle |
| γ_n | Unit weight of soil |
| γ_k | Dry unit weight |
| W | Moisture content |
| σ | Effective pressure |
| σ | Total pressure |
| u | Pore water pressure |

CHAPTER 1

INTRODUCTION

1.1. Overview

Since Turkey is located in an active tectonic region and the topography of Turkey is suitable for natural disasters such as landslides, it is necessary to detect areas with better soil conditions and to create scaled maps with relevant soil parameters especially for regions which are open to settlement. Thus, soil parameter maps will be a first step to a better urbanization.

Geotechnical soil parameter maps can be established with collecting, storing and updating the necessary information about fundamental soil parameters which belong to a geographic site. With the help of these maps the duration of obtaining information is decreased and more benefit is made from both manpower and cost aspects.

Aim of any urban geology is not limited to data collection, geological analysis and establishment of some map. The aim is also to provide geological information to planners and politicians for a rational development planning. Several urban geological studies of some cities provide good examples for this approach (Baker, 1975; Akpokodje, 1979; Edbrooke et al., 2003; Haworth, 2003; Nott, 2003; Willey, 2003; Özsan et al., 2007; El May et al., 2009).

Geotechnical mapping is considered as an important asset which can provide geotechnical parameters to develop a fitting map for construction within the framework of urban geology. This can help to establish a safe urban extension.

In this study, geological and geotechnical reports are firstly examined to the geotechnical soil parameter maps are established upon. The reports are also examined to evaluate the effect of soil conditions on planning of the urban area. Within this framework, the selecting and interpreting of unpublished reports and geological maps were completed. 45 unpublished reports that were obtained from the construction works done at around the study area were evaluated as detail. The study area was divided into five different regions that were considered as showing diversity about their geomorphological properties. 137 boreholes in the city were drilled in order to perform Standard Penetration Tests (SPT), and to define the physical properties of the soils obtained from these boreholes. In this study, maps for SPT-N, bearing capacity, liquefaction potential, Soil groundwater table, Atterberg Limits and soil classification have been produced by using a geographically information systems (GIS) based computer software. Accordingly, it is expected that the complete GIS maps could be effectively used by researchers and engineers for further studies on the purpose of urban planning.

The geological and geotechnical report data was taken from the archives of municipality of Niğde. Thematic maps, which are based on GIS, are established with results from available data and research findings to evaluate the suitability for soil condition using GIS's examination ability and different types of goal-oriented inquiries are made.

1.2. Engineering Geotechnical Mapping Method and Geographic Information Systems (GIS)

Engineering Geotechnical Mapping Method (EGMM) has become to be a challenging technic in all over the world recently. Its reason can be explained that the data collected from the sites and analysis of them do not seem enough for the establishment of rational development planning in cities and making more accurate designs for construction of earthworks. Therefore, engineering geotechnical maps should be prepared to virtually provide more information to city planners, politicians and design engineers. (El May et al., 2010).

There are several presented studies that were conducted in different cities related with Engineering Geotechnical Mapping Method. (El May et al., 2010; El May et al., 2009; Özsan et al., 2007; Willey, 2003; Nott, 2003; Haworth, 2003; Edbrooke et al., 2003; Akpokodje, 1979; Baker, 1975).

Furthermore, the researchers also recently have presented some studies that were related with engineering geotechnical and geological maps manipulated by using Geographic Information System GIS software. (Diaz et al., 2017; Masoud, 2016; Chaminé et al., 2016; Labiband Nashed, 2016; Culshawand Northmore, 2015; Faccini, et al., 2012).

In these past studies mentioned above, the researchers generally focused on the collections of geological and geotechnical parameters that are usually required for the establishment of rational development planning in cities and making more accurate designs. Moreover, the collected data from the published works and site investigation reports were virtually presented by using geological and geotechnical mapping method prepared by geographically information systems (GIS).

According to these past studies, it can be concluded that Engineering Geotechnical Mapping Method prepared with GIS is very beneficial and considerable technic for city planners, politicians and design engineers. As a result, much more geological and geotechnical properties of the cities can be locally observed and compared by using these methods. (Diaz et al., 2017; Masoud, 2016; Chaminé et al., 2016).

Therefore, in this study Engineering Geotechnical Mapping Method prepared with a GIS software program was conducted in order to observe and compare some geological and geotechnical properties of Niğde city (in Turkey).

1.3. Importance of Geographic Information Systems (GIS)

GIS applications integrate a wide range of computer-based tools for editing, managing and improving the analysis of spatial data, and can be considered a worldwide breakthrough in Geography and Planning since their origin in the 1960s.

In geographically information systems can also be entered data for each object. These properties can be made of different types examination and produce map information.

1.4. Objective of The Thesis

The main aim of this work is to contribute to preparation of a suitable rational urban planning and developing beneficial urban geotechnical maps for this city. A multidisciplinary analysis was considered to observe urban geological and geotechnical mapping method with the following objectives:

- Examination of the geotechnical parameters of Niğde city.
- Observing of the geology for the surrounding of this Niğde city.

• Discussing further suggestions by considering both geological and geotechnical maps with a geotechnical view to present a feasible map for construction of earth works in engineering applications.

1.5. Organization of The Thesis

The organization of the thesis study was presented as following;

In Chapter 1: General background and introduction of the study were given. General information about the Engineering Geotechnical Mapping Methods prepared with GIS were given.

In Chapter 2: Detailed literature and review information, studies in recent years were presented in a chronological order.

In Chapter 3: Detailed material and methods the geological characteristics of the study area and the data collected in the study area will be explained. The methods which are used to obtain soil parameters will be explained. The interpolation methods which are used to generate soil-parameter maps will be explained.

In Chapter 4: Test results and discussions extracted from the thesis were explained. Soil-parameter maps are presented and the variability of these parameters with respect to regions are discussed.

In Chapter 5: The conclusions obtained from the study are evaluated and concluding remarks are made.

CHAPTER 2

LITERATURE REVIEW

There are several presented studies that were conducted in different cities related with Engineering Geotechnical Mapping Method. Furthermore, the researchers also recently have presented some studies that were related with engineering geotechnical and geological maps manipulated by using GIS software. In the following section, studies in recent years are presented in a chronological order.

One of these studies was implemented by Yarbaşı et al., (2002). The intention of this work is to minimize the seismic hazard by a major possible earthquake in Erzurum which is a city under seismic hazard. According to their geotechnical properties, nine different geotechnical units were described. From each unit different samples were taken and tested for geotechnical properties such as Atterberg Limits and shear strength. Three main areas and nine sub-areas were selected in the study area which is Erzurum Palandöken Atatürk University. The areas were selected with consideration to data and geotechnical maps. Using geo-engineering properties, a shallow geotechnical zone map of the study area was generated.

Another similar study was to display whether the province Duzce was suitable for settlement or not by preparing ground parameter map of Duzce by Zeynan (2006). For this purpose, data which was obtained during development and reconsideration studies of Duzce province was investigated. These studies included 285 ground drilling operations and 185 seismic breaking operations. In addition, data gathered from the ground survey reports in parcel terms that was performed by Duzce Municipality was used. Moreover, these reports led to maps of ground parameters. Looking at the ground type, level of ground water, risk of liquefaction, seismic speeds, and elastic parameter maps changing depending on these speeds, low values was obtained in the area of survey around the city, especially in the city center. Furthermore, higher values were observed towards North of the city when compared with the South of the city.

Xie et al., (2006), studied a GIS based slope stability analysis computer application in 3-D. In this study, GIS grid-based data has been combined with four proposed columnbased models of 3D slope stability analysis and new correspondent GIS grid-based 3D deterministic models have been devised to calculate the safety factor of the slope. A computer program called 3DSlopeGIS was developed to analyze slopes where all the input is in the same format of GIS. If consulting or renewal of data is needed, this approach of the database would be a convenient way. The results well agree with the effective selection of range of Monte-Carlo random variables and the critical slip surface locations as well as the ease in data management.

A study made by Kolat et al., (2006), includes the use of Geographical Information Systems (GIS) to develop a geotechnical microzonation model in Eskişehir downtown area and it is based on Multicriteria Decision Analysis (MCDA). Many model inputs are required such as slope, swelling potential, liquefaction potential and flood susceptibility. Each layer and its classes are assigned several different values such as weight and rank values, respectively. As an output, geotechnical microzonation maps are prepared and the results are found out to be consistent with each other. Also, the results are approved by the experts within the study area. As the final map of the study, geotechnical microzonation map which is generated by AHP method, is recommended.

A study made by Yılmaz (2007), examines the free surface heave in alluvial soils in Yalova, Turkey and it maps the spatial distribution of the heave. The study uses a GIS package to generate a procedure for mapping free surface heave. In an active swelling zone, layers are defined considering their characteristics of swelling. To construct the spatial distribution map, free surface heave values are calculated. It was seen that there exists a wide distribution of soils with high swelling potential. This could create some serious problems on light structures and the potential for problems related to differential movements, is high also. The results indicated that a maximum differential movement of 12.24 cm is expected which categorize as "very severe". When surface heave hazard management and land use planning is concerned, the results of this study can provide beneficial data. Moreover, when probable deformations of light structures are concerned, information obtained from this study can be used to assess the deformation.

Kıyak (2008), aimed to show the vitality of geodynamic data archives for the planning of settlement areas and earthquake risks. This study was applied on the Adapazari province which was exposed many damages in 1999 Earthquake. Totally 2000 drilling and 280 seismic data were collected and transferred into digital form. The soil groups were classified by fuzzy logic system and micro zonation maps were prepared by using GIS. Micro zonation maps showed that most areas in the study area have Z-3 and Z-4 type of soil group. This could be explained by the high ground water levels on the areas under consideration.

El May et al., (2010), studied the procedure for preparation of engineering geological mapping in Tunis city (Tunisia) as a case study. While preparing the maps, main restricting factors for urban development are considered. Some of these factors are: slope, flood susceptibility, seismic-induced effects and topography etc. Using GIS, information layers were manipulated and then combined to generate engineering geological maps. A suitability map is generated to summarize the results and as a result, four different zones were formed in the study area. It was seen that the results agree with the bearing capacity map. The zone map is a beneficial tool for nongeologist planners and deciding bodies for residential area extension. The results can be used to improve geotechnical micro zonation by adding more test results.

Mary et al., (2012), studied in the area along Sheikh Zayed canal in which site investigation was performed to identify rock and soil formation in the area and the emphasis was on the swelling properties of clayey soils. GIS was used to interpret the data and to identify the characteristics of variables while showing their distribution on the map. Then, swelling potential and swelling pressure values are identified over specific areas. Field measurements were done to identify the geotechnical map of Toshka region by using GIS. From different boreholes ninety (90) soil samples were extracted. The samples were examined in the laboratory to identify free swelling, specific gravity, Atterberg Limits etc. according to the Egyptian Standard. This map could be used to determine the soil parameters over the region and could help the planners to evaluate the feasib ity of new projects around Toshka area or when modifications to existing structures are needed.

Fikret et al., (2014), studied to execute a geotechnical assessment and micro zonation for Esenler town located on European side of Istanbul by using geological, geophysical and geotechnical data together. The studies were prepared by utilizing from Geographic Information Systems (GIS) take an effective role in Turkey in the selection of new residential areas and in the planning of the existing residential areas. On the other hand, bearing capacity for shallow foundations and rock sites and consolidation settlement assessment executed in this study due to the re-construction planning in the study area. All the assessment results and geotechnical features of the study area presented with GIS based micro zonation maps. Thus, pre-information and maps created for the study area that could be used in earthquake hazard reduction studies. According to the research results, the northern parts of the study area have much more reliable geotechnical conditions compared to the southern parts in terms of the settlement suitability.

A study by Culshaw et al., (2015), was done to provide necessary geological information to be used in land development and planning. The study was in Bradford Metropolitan District, UK. First part of the study aims to lead the land use planners to use geological data in development and urban planning and also to lead the engineers to use data for ground conditions. (Water et al. 1996) Maps for describe a general geological overview and groups the suitability of deposits such as thickness, engineering fills. The paper briefly describes the content of the maps and how they were produced.

Another study by Masoud (2016), aims to create maps with geological and geotechnical parameters and their spatial distribution. Also, the study concerns over urban land management zonation by considering the geotechnical variability while generating the loading factors for distinct spatial patterns. The study area was in Tanta district in Gharbiya governorate in Egypt. The dataset was comprised of 109 borehole data and certain boreholes were selected to be used as they held the most relevant information such as plasticity, strength, consolidation and soil water condition information. Using GIS and the accumulated data, three different classes were generated and evaluated for geotechnical hazards. Results can be used to create geotechnical hazard zonation maps for better and safer urban extension.

Geophysics and geotechnical examination were conducted within the context of the study in order to define the physical properties of geological segments and underground segments in Çamlıtepe district by Öncül (2016). In this study, to determine the dynamics properties and physical parameters of examined district, six seismic refraction- MASW profiles, tomography operation upon three profiles,

Schlumberger electrode string vertical electric sounding (VES) in four points and geotechnical drill in eight points was conducted. Settlement area of Batman (around of the study area) geologically have clay, conglomerate, sand gravel and alluvium consisting of sand and gravel. This was an important factor for settlement and ground deformation. It was also examined the ground structure, dynamic condition and sandy problematic segments and geotechnical problems and suggest same solutions for these problems.

In another study by Diaz et al., (2017), a GIS-type geotechnical repository is generated for Avilés. To develop the database a geological map is first generated and using this map, a geotechnical map is created by determining the different geotechnical units. Firstly, in the methodology part, all previous research with similar purposes or in the same area was reviewed and geological maps were reviewed. Reviews of 104 different recent geotechnical reports for the area were done. Distribution and thickness of the geological layers are studied, and geotechnical properties are determined from field and laboratory tests. In ArcGIS, a database is generated with the relevant geotechnical and geological data and a geological map is constructed with a scale of 1:25,000. The results of the research were unprecedented. The research categorizes the ground conditions from worst to good in four different categories. The methodology used can be beneficial when investigating other similar geotechnical environments.

| Author Of The Study | Year relea sed | Publication Location | Studying Name | | | | | |
|-----------------------------|---|---|---|----------------|--|--|--|--|
| Yarbasi et al | 2002 | Pamukkale University Engineering College Journal of Engineering sciences | Geotechnical Properties of the soil in the Ataturk University Yenişehir (Erzurum) Urban Area | | | | | |
| Keleş | 2006 | Post graduate thesis | Formation of micro regional parameter maps in Duzce City | GIS | | | | |
| Xie et al | 2006 | Computers and Geotechnics | Geografical Information system-based computational implementation and application of spotial three- dimensional slope stability analysis (Monte Carlo) | GIS | | | | |
| Kolat et al | Kolat et 2006 Engineering Geology Preparation of a geotechnical microzonation model using Geografical information system-based on | | | | | | | |
| Yılmaz | 2007 | Computer and Geosciences | A case study for mapping of spotiol distribution of free surface heave in alluvial soils (<u>Yalova Turkey</u>) by using GIS software | GIS | | | | |
| Kıyak | 2008 | Post Graduate Thesis | Creating microzonotion maps of Adapazarı province by using Geographic Information Systems | GIS, | | | | |
| El May etal | 2010 | Engineering Geology | Urban Geological mapping; Geotechnical data analysis for rational development planning | Fuzzy Logic | | | | |
| Kumaz | 2011 | Doctoral Thesis | Geographic Information Systems based geotechnical microzonation forEsenler soils(Istanbul) | GIS | | | | |
| Kumaz | 2011 | Doctoral Thesis | Geographic Information Systems based geotechnical microzonation for Esenler soils(Istanbul) | GIS | | | | |
| Labib and Nasbed | 2013 | Ain Shams Engineering Journal | GIS and geotechnical mapping of expansive soil in Toshka region.(Egypt) | GIS | | | | |
| Culshaw and Northmore | 2015 | Engineering Geology For Society and Territory | Urban Engineering Geological Maps for Bradford Metropolitan District of West Yorkshire, in the North of England (UK) | GIS | | | | |
| Masoud | 2016 | Saudi Society for Geosciences | Geotechnical site suitability mapping for Urban land management in Tanta District, Egypt | GIS | | | | |
| Öncül | 2017 | Post Graduate Thesis | Assestment and Determination of Engineering parameter with Geophysical and Geotechnical methods of Çamlıtepe District (Batman) of ground | Plaxis | | | | |
| Diaz et all | 2017 | Journal of Maps | Geotechnical map of a coastal and Industralized Urban Area (Aviles, NW Spain) | GIS | | | | |
| Bayrakçı | 2018 | Post Graduate Thesis | Osmaniye city center Evaluation of Geotechnical properties due Microzonation map | Proshake | | | | |

Table 2.1. Literature Review List of Table

CHAPTER 3

MATERIAL AND METHODS

It is possible to create the soils parameter maps for the soils of the studied area by collecting many ground information related to this region, transferring it to digital media and interpreting the results obtained. In this section, soils parameter maps will be formed, the geological characteristics of the study area and the data collected with field, laboratory and office surveying in the study area will be explained. In addition, the interpolation methods which are used to generate soil-parameter maps will be explained.

3.1. Geological Considerations for Study Area

3.1.1. Geology of the Study Area

Niğde city is located at 37°10' – 38°37' north and 33°10' – 35°25' east parallels Figure 3.1a. It spread out to 779.522 ha land area within these limits. Geological, tectonic and hydrogeological characteristics of the region are studied by many researchers (Göncüoğlu, 1985; Atabey and Ayhan, 1986; Toprak and Göncüğlu 1993; Dirik and Göncüoğlu, 1996; Şener et al., 2017). Niğde province is surrounded by high mountainous areas such as Mount Melendiz and Mount İtulumaz from the north and south, respectively Figure 3.1b. Mean elevation of the city center is 1229 m asl. The mountains surrounding study area can be considered in two categories as the volcanic and sedimentary origin. The volcanic mountains consist of Big and Small Hasan Mountains (their heights are 3268 m and 3069 m, respectively), Mount Keçiboyduran (2752 m), Mount Melendiz (2963 m), Mount Göllüdağ (2172 m), Bolkar Mountains (3524 m) and Aladağlar Mountains (3756 m) (Figure 3.1b.).

The study area which hosts Niğde city center extends in NW-SE direction. The basement of the study area consists of metamorphic rocks. The Paleozoic-Mesozoic outcrop metamorphic units in the eastern and southeast border of the study area are represented by gneiss and quartz while uppermost units are represented by Aşıgediği marbles. Upper Cretaceous metagabbros are located in the northwestern part of the

study area. Melendiz volcanism, which belongs to Cappadocia volcanic complex, affected the western and northwestern part of the study area and represented by andesites, basalts and pyroclastic rocks. Pliocene units are represented by terrestrial sediments, but they have limited expansion. The main target of this study is Quaternary units which are composed of colluvial sediments and alluviums and also represented by heterogeneously distributed gravel, sand, clay, and silt Figure 3.2.

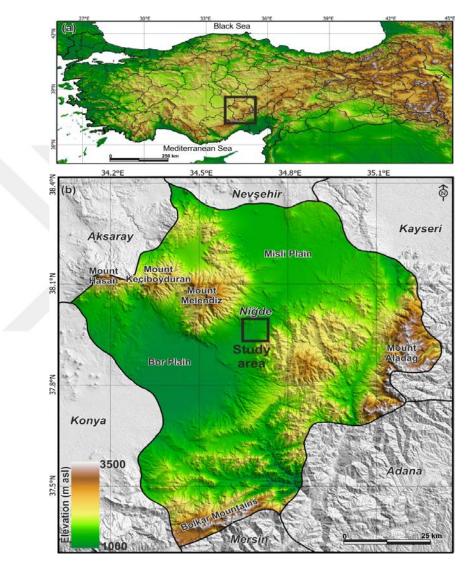


Figure 3.1. Location and digital elevation maps of the study area

3.1.2. Structural Geology-Tectonics

Many active and buried faults are present in the study area and surroundings. However, two primary tectonic structures are affected the study area, namely the Tuz Gölü Fault and the Niğde Fault.

Niğde Fault Zone

The Niğde fault borders the southern margin of the study area Figure 3.2. It strikes NE-SW and is cut and displaced into several segments by the Tuzgölü-Ecemiş fault system. The southern block of the fault is up thrown for about 500 m (Toprak and Göncüoğlu, 1993). This observation was supported by geophysical measurements of stacked fan deposits over 500 m in the hanging-wall.

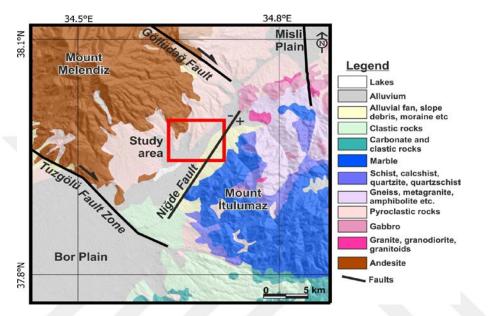


Figure 3.2. Lithology map of the study area (adapted from Senel 2002 a, b)

Tuzgölü Fault Zone

The Tuzgölü Fault Zone (TGFZ), first named by Beckman (1966), was named as "Ş. Koçhisar-Aksaray Fault", "Tuzgölü Fault", "Koçhisar-Aksaray Fault Zone" by various researchers (Uygun 1981; Şaroğlu vd., 1987; Derman vd., 2000). It is one of the most important active intra-continental fault zones in Anatolia. It is almost 200 km in length and the width is between 2 to 25 km. It is a normal fault with minor right-lateral strike-slip component (Figure 3.2.). TGFZ consists of eleven parallel or sub-parallel geometric fault segments and their length ranges from 9 to 30 km. Fault kinematic analysis studies shows that NE-SW trending extensional tectonic regime is dominant in the area and it was activated in the early Pliocene. In the east it is bordered by Tuz Gölü Plio-Quaternary. By the early Pliocene, total normal slip is found 200-268 m. Average annual slip-rate on TGFZ is 0.046 mm based on geologic age and slip amount. (Kürçer and Gökten, 2014).

3.2. Plotting the Geotechnical Maps

There are several criteria for defining the scale for the preparation of a geotechnical map. Before any scale is defined, some questions should be asked (Dearman, 1991), such as; what is the main purpose of preparing a map and are the details that we wish to show and search enough or not? The second criterion that should be taken into consideration to define the scale of the map may be explained as the size of the country including the study area (Price, 1981). The third one that is important for selecting scale of mapping may be given as the complexity of the terrain that must be shown in a map. The last criteria for the choice of map scale can be explained as complementary maps (Price, 1981; El-May et al., 2010). An international scale range was proposed by the UNESCO guidebook (CEGM-IAEGC, No. 15, 1976) and is given as follows: Large-scale maps (1:10.000 and larger), medium-scale maps (less than 1:10.000 and greater than 1:100.000), and small-scale (1:100.000 and less) (El-May et al., 2010).

Niğde city is descriptive of complex geological history and has complicated geomorphologic properties (Clark and Robertson, 2002), because of this reason inthis study 1:25.000 scale of the maps as the very large scale was used in all complimentary maps used. It may not be possible in order to observe the same regional features (for example; fault, aquifer extension, and watercourses) and suitable determination of geological conditions of the studied area in smaller map scales (such as 1:50.000). Therefore, the mapping scale used for the geotechnical mapping of Niğde city (1: 25.000) presents the details and facilities for the successful investigation of the suitability for construction. It is defined, according to the international scale range proposed by the UNESCO, as a medium scale (El-May et al., 2010).

For mapping, two interpolation methods were used. These is the Minimum Curvature Interpolation Methods and the Voronoi Polygons Interpolation Methods.

3.2.1. Interpolation Methods for GIS Aplications

In the subject of spatial information, it is always important to use existing numerous wide-distributed height points adequately. To form curved faces, interpolation must be made to discretely collected height points. Quality, accuracy and follow-up analysis applications are decided by the selection of the spatial interpolation method. When calculating the unknown heights of interested points by referring to the elevation information of neighboring points, interpolation methods are used.

3.2.1.1. The Minimum Curvature Interpolation Methods

In earth sciences, a common method is the minimum curvature method. With this method a surface analogous to a thin, linearly elastic plate is created and this surface passes through each data value with minimal bending. Therefore, it is the smoothest surface possible (Yang et al., 2004).

Minimum curvature method is used for plasticity index, bearing capacity, groundwater table depth and standard penetration test results in this study.

3.2.1.2 The Voronoi Polygons Interpolation Methods

As a result of the growth process, Voronoi polygons are formed. All of the points (nuclei) are assumed to grow uniformly outward at the same time along a circular boundary. After some time, a tightly packed state is reached and points of contact between the circle centered at a given point P and other circles is determined by the composition of points near P and at these contact points, the growth stops. However, the remaining points continue to grow and contact points now become the midpoints of the expanding straight line on which growth boundaries meet and freeze. All of the circles grow at the same speed which means the initial contact point between two circles occurs at the midpoint between their nuclei. Similarly, the expanding line segments must lie at an equal distance to two nuclei. The points are on the common edge of two Voronoi polygons. Elongation of an edge continues until the border of a third growing circle is met. The contact point between these two lies at an equal distance to the centers of all three circles. Therefore, this point is the center of the circumscribed circle of the triangle defined by the three points. After some time, the circles whose nuclei are on the convex hull of S are still growing. The group of complete polygons is named as the Voronoi diagram. The complete and incomplete polygons together form a Voronoi tessellation. The edges created by joining each point with its neighbors is the dual of the Voronoi tessellation and is called the Delaunay tessellation.

Some natural processes could be used to describe certain classes of Voronoi diagrams (Aurenhammer, 1991). Region are obtained by the division of the space by the Voronoi diagram and every region consists of one feature. For every point in a region, this feature is the closest feature to the point than any other one (Masehian and Amin-Naseri, 2004).

For describing soil classification results and liquefaction results, Voronoi polygons (proximity polygons) are used in this study.

3.3. Interpretation of Geotechnical Data

In order to interpret the geotechnical data obtained from the study area, several geotechnical parameters such as soil classification, SPT results, bearing capacity, unconfined compression test results (UCS), groundwater table level, liquefaction potential and some engineering properties of the soils were evaluated. First of all, the study area was divided into five different groups that were considered as showing diversity about their geomorphological properties. In each group, nine unpublished reports were selected and evaluated for investigating the data and plotting the geotechnical maps.

3.4. Methodology of the study Area

Niğde City, with complicated geomorphologic properties, was investigated by the diversity of geological and geotechnical parameters. First of all, the selecting and interpreting of unpublished reports and geological maps were completed. 45 amounts of unpublished reports that were obtained from the construction works done at around the study area were evaluated as detail. Then, the study area was divided into five different regions that were considered as showing diversity about their geomorphological properties. Figure 3.3. In each region nine, unpublished reports were selected and analyzed for interpreting the data and plotting the geotechnical maps. Each point to represent the different lithological units within the sheet and also the distribution maps to be produced in relation to the ground parameters were taken into consideration was paid attention to the distribution of the points to be sampled in proportion to the entire scale.

These unpublished reports include 137 boreholes, field-laboratory test results and office surveying and SPT results conducted for past site investigation in order to present data to many construction and engineering works.

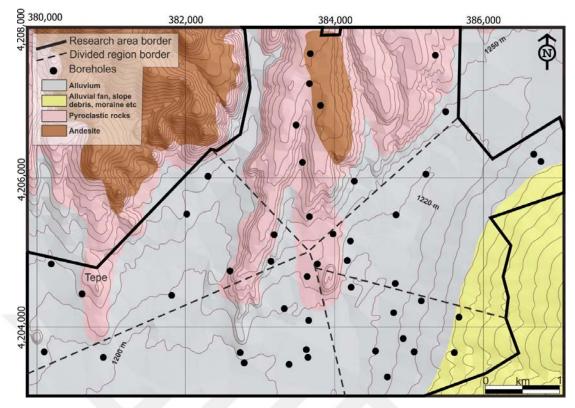


Figure 3.3. Location of the boreholes and lithology map of the study area (Contour intervals is 10 m)

3.4.1. Field, Laboratory and Office Surveying

The study area consisted of the main material soil and rock samples taken from the field. In this section; surveying, field surveying, laboratory surveying and office surveying is done.

3.4.1.1. Field Surveying

This study includes 137 boreholes. During the drilling, penetration resistance of the floors was determined by taking a standard penetration test SPT-N every 1.5 meters on the ground and the abused sample was taken.

3.4.1.1.1 Geotechnics Measure Field Surveying

a) Survey of the Boring Methods

Boreholes are used to determine geological and geotechnical parameters of the ground units in the study area.

The use of Boring Methods;

• Geological data collection

- Geophysics Surveying
- Foundation boring and underground cementing
- Water survey
- Petrol- Natural gas, water circulation survey
- Drainage

Borehole data are used for many subjects as mentioned above. In this study, borings are made for geotechnical purposes and to obtain engineering parameters of the soil SPT is made and both disturbed and undisturbed samples are gathered.

3.4.1.1.2. Field testing for Geotechnical Purposes

a) Standard Penetration Test

SPT is a very common field test in many countries of the world and as well as Turkey (Emrem ve Durgunoğlu, 2000).

This test gives the best results when predicting the engineering properties of clean finemedium sands, very fine gravelly sands and sand with little silt. However, as the coarse grain ratio increases, the accuracy of the test decreases and the results can be misleading. ASTM D 1586 and AASHTO T 206 describes the procedures of the SPT.

1a) The method of the Test

The experiment depends on the penetrating a standard sized split spoon sampler with the free fall of 63.5 kg tilt-hammer from 76.2 cm height. Figure 3.4.

For this experiment, a borehole drill is necessary. After cleaning borehole drill, the depth of experiment is recorded with 0.030 m accuracy. After fixing the SPT tube on boring stem bars, the tubes are swung to the bottom without falling. Then 3,15 cm progressing steps are drawn on stem bars. For each 15 cm step, free dropping number of tilt-hammer is calculated. On hard soils, if in one of 15 cm progressing steps, any 15 cm penetration is not reached then the experiment is stopped, and it is noted refusal value is reached. This situation is noted as 50 penetration quantity. In some cases, the experiment is stopped if less than 300 mm is reached at the end of 100 tilts. If any progress can't be reached at the end of 10 tilts, then the experiment again is stopped.

The first 15 cm is defined as penetration indwelling area and the number of drops here is not considered because of the remolding at the bottom of soil. Then the number of drops for penetration are recorded in the second and third 15 cm as SPT number N. The experiment generally is repeated at 1,5 m wellbore. It is not suggested to apply the experiment for soils where maximum piece size is larger than the diameter of sample collector.

| SPT-N | Consistency of soil | | | | | |
|-------|---------------------|--|--|--|--|--|
| <2 | too soft | | | | | |
| 2-4 | soft | | | | | |
| 4-8 | medium-stiff | | | | | |
| 8-15 | stiff | | | | | |
| 15-30 | very stiff | | | | | |
| >30 | rigid | | | | | |

Table 3.1. Consistency of soils according to SPT-N(Osman Sivrikaya, Ergün Toğrol)

The advantages of the Standard Penetration Test (SPT)

- Both the sample and an N-value are obtained
- Simple to use
- Suits many soil types
- Easy to perform on weak rocks
- Common throughout the U.S.

The disadvantages:

- No undisturbed sample (index tests only)
- N-value is a rough number for many analyses
- Not applicable in soft clays & loose silts
- Variability and uncertainty are high
- Not reliable in gravelly soils

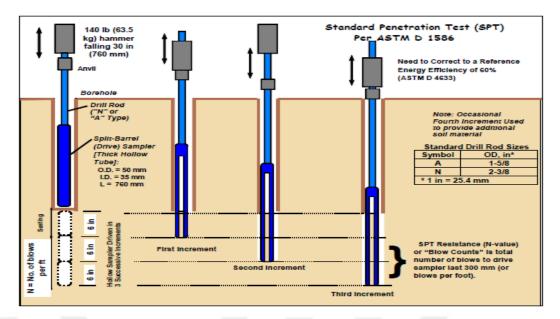


Figure 3.4. Split-barrel type Standard Penetration Test

In this study, 0-5 m depth of the soils is investigated for interpreting the geotechnical data for limiting the soil strata. Field SPT results without making any correction were evaluated and presented in this study. The following table shows SPT-N value according to five the regions.

| Table 2.2. Recording to regions of 1 14 tuble | | | | | | | | | | | | | | |
|---|-----------------|--------|-----------------|-----------------|--------|-----------------|-----------------|--------|-----------------|-----------------|--------|-----------------|-----------------|--------|
| Main regions | Sub- regions | N -TAS | Main regions | Sub- regions | SPT- N | Main regions | Sub- regions | SPT- N | Main regions | Sub- regions | SPT- N | Main regions | Sub- regions | SPT- N |
| | A1 | 16 | | B1 | NP | | C1 | NP | Region-D | D1 | 42,5 | Region-E | E1 | 5 |
| | A2 | 24 | | B2 | NP | | C2 | NP | | D2 | 37 | | E2 | 4 |
| | A3 | NP | Region-B | B3 | NP | | C3 | 9,3 | | D3 | 50 | | E3 | NP |
| ¥. | A4 | NP | | B4 | 40 | ų | C4 | 41 | | D4 | 50 | | E4 | 13 |
| Region-A | A5 | NP | | B5 | NP | Region-C | C5 | 9 | | D5 | 50 | | E5 | 17 |
| Re | A6 | NP | | B6 | NP | Re | C6 | 41 | Re | D6 | 42,5 | | E6 | 3 |
| | A7 | NP | | B7 | NP | | C7 | NP | | D7 | 45 | | E7 | 10,5 |
| | A8 | NP | | B8 | NP | | C8 | 12 | | D8 | 9 | | E8 | 7 |
| | A9 | NP | | B9 | NP | | С9 | NP | | D9 | 10 | | E9 | NP |

Table 2.2. According to regions SPT- N table

b) Disturbed Sampling of Soil

Disturbed samples are taken along the boring or from research pits. Their natural state changes but they can keep their water content. Generally, they are used for characterization and classification. AASHTO T 206 and ASTM D 1586 suggests that

they are usually collected using split-barrel samplers. However, some other methods and equipment can be used for acquisition of disturbed samples.

c) Undisturbed Sampling of Soil

Undisturbed samples represent the soil's natural condition in the field as good as possible. The water content is same with the natural deposit and the structure is the same as well. However, the stress acting on the soil is released. Therefore, it is not possible to obtain a true undisturbed sample, but the aim is to minimize the amount of disturbance. The most common method is to use a thin-walled "Shelby Tube".

Undisturbed samples allow an engineer to determine the geotechnical properties of strength, compressibility, permeability and fracture patterns among others. Results of these analysis are instrumental and the design of a new building.

3.4.1.2 Laboratory Surveying

To identify the soil's lithological and geological conditions, as well as its engineering parameters, borings are made, disturbed and undisturbed samples are taken, and laboratory test are performed.

In order to determine the physical and mechanical properties of the building foundation the disturbed and undisturbed sampling of soil with boreholes in the study area on water content and unit weight tests, sieve analysis, Atterberg limits and laboratory experiments; the specifications of the Public Works and the BS 5930 actions "Code of Practice for Site Investigations "were conducted in accordance with the soil survey specifications.

3.4.1.2.1. Laboratory Index Tests and Analysis for Soils

This section includes geotechnical engineering parameters of the soils such as void ratio, porosity, moisture content, degree of saturation, dry unit weight, particle unit weight, natural unit weight, sieve analysis, unified soil classification, Atterberg limits (liquid limit and plastic limit), as well as triaxial shear test on undisturbed samples, uniaxial test and point load test to determine rock strength parameters.

a) Void Ratio (e)

In soil mechanics is the ratio of the volume of voids (Vv), in the volume of solids (Vs). This ratio is referred to as void ratio (e), is expressed as a percentage as follows : equation 3.1.

$$e(\%) = \frac{V_v}{V_s} * 100 \tag{3.1}$$

b) Porosity (n)

A parameter used the volume of the voids in a given soil mass can be obtained from the ratio of the volume of voids (Vv), to the total volume (V). This ratio is referred to as porosity (n), and is expressed as a percentage as follows: equation 3.2.

$$n(\%) = \frac{v_v}{v} * 100 \tag{3.2}$$

Clearly, the porosity can never be greater than 100%. As a soil mass is compressed, the volume of voids (Vv), and the total volume (V), decrease. Thus, the value of the porosity changes.

c) Moisture Content (w)

The water content in soil mechanics, is the ratio of the weight of the water (W_w) , in the weight of solids (Vs). This ratio is referred to as moisture content (w), is expressed as a percentage as follows: equation 3.3.

$$w(\%) \ \frac{W - w_s}{w_s} = \frac{w_w}{w_s} * 10$$
(3.3)

d) Saturation Degree (s_r)

The saturation degree, in soil mechanics is the ratio of the volume of the water, in the total volume of the voids. This ratio is referred to as saturation degree (s_r) , the term degree of saturation (S_r) , is used as follows: equation 3.4.

$$S_r(\%) = \frac{V_w}{V_v} * 100 \tag{3.4}$$

Clearly, the degree of saturation can never be greater than 100%. When $S_r = 100\%$, all the void space is filled with water and the soil is considered to be saturated. When $S_r = 0\%$, there is no water in the voids and the soil is considered to be dry.

e) Dry Unit Weight (γ_d)

The dry unit weight is the ratio of the dry weight to the total volume. The dry unit weight, (γ_d) can be expressed as follows: equation 3.5.

$$\gamma_d = \frac{W_s}{V} \tag{3.5}$$

f) Particle unit weight (γ_s)

Is the ratio of the volume of solids (Vs), and the total volume weight of solids (Ws). This ratio is referred to as particle unit weight (γ_s), and can be expressed as follows: equation 3.6.

$$\gamma_s = \frac{W_s}{V_s} \tag{3.6}$$

g) Natural unit weight (γ_t)

Is the ratio of the total weight (W), and the total volume (V). This ratio is referred to as natural unit weight (γ s), and can be expressed as follows: equation 3.7.

$$\gamma_t = \frac{W}{V} = \frac{W_{w+}W_s}{V} \tag{3.7}$$

h) Sieve Analysis

In civil engineering, particle size is an important concern since the effectiveness of the final product is dependent on the particle size. The particle size determines the characteristics of the soil such as permeability, bulk density, physical stability. Commonly sieve analysis is used to determine particle size and its distribution. Using the volume and the mass, particle size distribution is determined. In the sieve analysis test procedure, the particles will move through the sieve either vertically or horizontally. Different kinds of sieving procedures are available, depending on the material and needs.

Air-dried material is shaken through a stack of sieves which have decreasing sizes of opening. For every sieve, the retained amount of sample is oven dried and weighed to determine the mass retained as a percentage total sample. Particles having sizes larger than the No. 200 sieve (0.075 mm) are called "coarse-grained" while those with sizes

finer than the No. 200 sieve are called "fine-grained." Shown Figure 3.5.



Figure 3.5. Example of laboratory sieves for mechanical analysis for grain size distributions.

According to the Figure 3.5. (from right to left) are sieve nos. 3/8-in (9,5 mm), No. 10 (2.0 mm), No. 40 (0.425 mm) and No. 200 (0.075 mm). Example soil particle sizes shown at the bottom of the photo include (from right to left): medium gravel, fine gravel, medium-coarse sand, silt and clay.

1) Unified Soil Classification System

This system was developed by Arthur Casagrande in 1942 to be used in airport constructions. To classify the soil, grain size and plasticity are needed. The system uses two letter naming convention. The grouping is done via collecting the soils with similar properties such as grain size, gradation and plasticity (ASTM D 2487).

Group symbols and the soil type represented by the symbols are shown in the table below.

| Primary Component | Secondary Description |
|-------------------|-----------------------|
| G (Gravel) | W (Well Graded) |
| S (Sand) | P (Poorly Graded) |
| M (Silt) | M (Silty) |
| C (Clay) | C (Clayey) |
| O (Organic) | H (High plasticity) |
| Pt | L (Low Plasticity) |

Table 3.3. Group symbols and the soil type represented by the symbols

SM= Primary Component (Sand = S) Secondary Description (M = Silty)

If soil contains greater than or equal to 15% sand, add "with sand" to group name.

- 1) If fines categorize as CL or ML, GC-GM, SC-SM symbols are used.
- 2) If there exists organic content, "with organic fines" is added to the group name.

- If there exists 15% more or greater gravel content, "with gravel" is added to the group name.
- 4) From the liquid limit and plasticity index chart, if the soil falls on the hatched region of the plot, then use CL-ML, silty clay.
- 5) If 15 to 29% coarse grains exist, i.e. larger than No. 200 (0.075 mm), "with gravel" or "with sand" is added.
- 6) If more than 30% of the soil is larger than No. 200 (0.075mm) and is mostly sand the soil contains greater than or equal to 30% plus No. 200 (0.075mm), predominantly sand, add "sandy" to group name.
- 7) If soil contains greater than or equal to 30% plus No. 200 (0.075 mm), predominantly gravel, add "gravelly" to group name

Classification of Coarse-Grained Soils

Two subdivisions exist for coarse grained soils, these are:

a) Gravels (G): If more than 50% of the coarse part is larger than 4.75 mm opening sieve, then it belongs to this subdivision. The symbol is G and this subdivision includes gravelly soil and clean gravel.

b) Sands (S): If more than 50% of the coarse part is smaller than 4.75 mm opening sieve, then it belongs to this subdivision. The symbol is S and this subdivision includes sandy soil and clean sand.

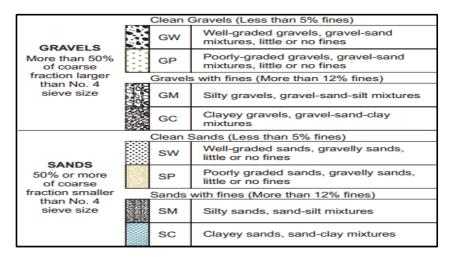


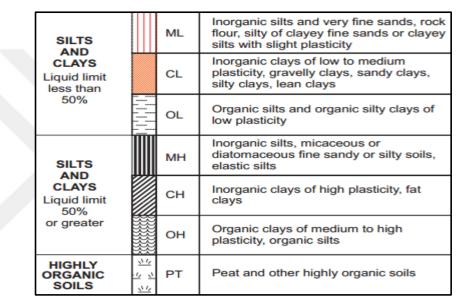
Figure 3.6. Unified Soil Classification System for coarse-grained soils

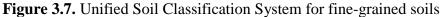
• Classification of Fine-Grained Soils

Fine-grained soils, or "fines," are those in which 50 percent or more by weight pass the No. 200 (0.075 mm) sieve,

Fine grained soils are divided into three sub-divisions:

- a) Inorganic silts and very fine sands: M
- b) Inorganic clays: C
- c) Organic silts and clays and organic matter: O.





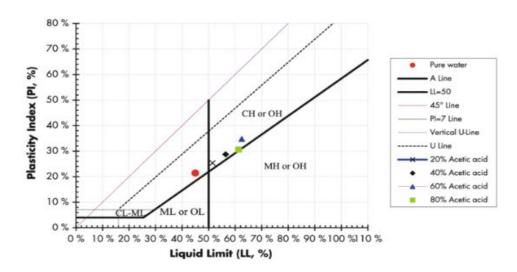


Figure 3.8. Casagrande Plasticity Card

In this study, 0-5 m depth of the soils is investigated for interpreting the geotechnical data for limiting the soil strata. Unified Soil Classification System.

| Maın regions | Sub-regions | classification of soils (uscs) | Maın regions | Sub-regions | classification of soils (uscs) | Maın regions | Sub-regions | classification of soils (uscs) | Maın regions | Sub-regions | classification of soils (uscs) | Maın regions | Sub-regions | classification of soils (uscs) |
|--------------|-------------|-----------------------------------|--------------|-------------|-----------------------------------|--------------|-------------|-----------------------------------|--------------|-------------|-----------------------------------|--------------|-------------|-----------------------------------|
| | A1 | SM | | B1 | Rock | | C1 | Rock | | D1 | SM | | E1 | СН |
| | A2 | CL | | B2 | Rock | | C2 | Rock | | D2 | SM | | E2 | SM |
| | A3 | Rock | | B 3 | Rock | | C3 | SM | | D3 | SM | | E3 | Rock |
| V- | A4 | Rock | P | B4 | SM | ပု | C4 | SM | Ą | D4 | SM | Ē | E4 | CL |
| Region-A | A5 | Rock | Region-B | B5 | Rock | Region-C | C5 | SM | Region-D | D5 | SM | Region-E | E5 | SM |
| Re | A6 | Rock | Re | B6 | Rock | Re | C6 | SM | Re | D6 | SM | Re | E6 | SM |
| | A7 | Rock | | B7 | Rock | | C7 | SM | | D7 | SM | | E7 | CL |
| | A8 | Rock | | B8 | Rock | | C8 | CL | | D8 | CL | | E8 | CL |
| | A9 | CL | | B 9 | Rock | | С9 | Rock | | D9 | СН | | E9 | SM |

Table 3.4. According to regions USCS Table

Atterberg Limits j)

In 1911, Atterberg described the changing behavior of soil depending on its water content experimentally. The engineering behavior of fine-grained soils is affected by their water content. Four different states exist in soil with changing moisture content. These states are solid, semisolid, plastic and liquid. The water content values at these states are called Atterberg Limits. Shrinkage limit is the transition from solid to semisolid state, Plastic limit is the transition from semisolid to plastic state and liquid limit is the transition from plastic to liquid state. Figure 3.9.

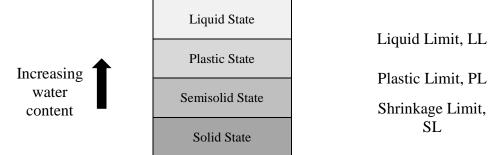


Figure 3.9. Atterberg Limits stages

Plastic Limit, PL Shrinkage Limit,

• Liquid limit (LL)

When the water content of soil changes such that the behavior transitions from a highly viscous fluid to a plastic state, the limit is called liquid limit. Two main methods are used to determine liquid limit. These are Casagrande method and falling cone method.

The water content is expressed as the percentage of the oven-dried weight for the accepted trial.

$$Moisture\ Content\ (w) = \frac{Weight\ of\ water}{weight\ of\ oven-dried\ soil} *\ 100 \tag{3.7}$$

The liquid limit LL, used formula, in which the moisture content (W) expressed as a percent is multiplied by (N/25) 0.12 calculated for specific number of drops: equation 3.8.

$$LL = W(\frac{N}{25})^{0,12}$$
(3.8)

 Table 3.5. According to Range of Liquid limit by Degree of Plasticity (Bell, 2007)

| Rang of Liquid Limit (%) | Degree of Plasticity | Describing |
|-----------------------------|------------------------------|---------------|
| <35 | Low Plasticity Soil | Lean or Silty |
| 35–50 | Medium Plasticity Soil | Middle oil |
| 50–70 | High Plasticity Soil | Fatty |
| | Ultrahigh Plasticity | |
| 70–90 | Soil | Super fatted |
| | Exorbitant Plasticity | |
| >90 | Soil | Ultra fatty |

• Plastic Limit (PL)

This limit is defined as the water content at which cracks are formed over the surface of the soil as the soil is kneaded on a table like dough. In other words, it is the water content value at the transition from semisolid to plastic state.

Calculate the moisture content of each soil sample expressed as a percentage of the weight of the oven dry soil, as follows: equation 3.9.

$$Plastic \ Limit = \frac{Weight \ of \ water}{weight \ of \ oven-dry \ soil} * \ 100$$
(3.9)

•Shrinkage Limit (SL)

This limit is the largest value of water content value at which the loss of water does

not affect the volume anymore. In other words, it is smallest water content value at which the soil is fully saturated.

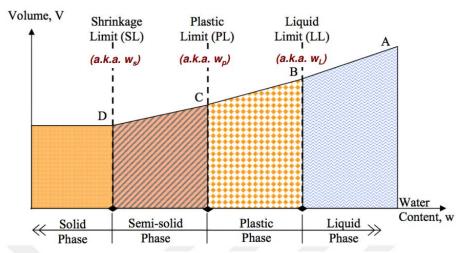


Figure 3.10. Conceptual changes in soil phases as a function of water content (https://vulcanhammernet.files.wordpress.com)

• Plasticity index (PI)

The plasticity index of a soil is the numerical difference between its liquid limit and its plastic limit and it is a dimensionless number. Both the liquid and plastic limits are moisture contents.

Plasticity Index = Liquid Limit - Plastic Limit

$$PI = LL - PL$$

(3.10)

 Table 3.6. Classification of cohesive soils by plasticity index

 (Leonards 1962)

| Plasticity index | Degree of plasticity | | | | | | |
|------------------|----------------------|--|--|--|--|--|--|
| (PI = LL-PL) | | | | | | | |
| 0-5 | Non-Plastic | | | | | | |
| 5-15 | Low Plastic | | | | | | |
| 15-40 | Plastic | | | | | | |
| 40 | Highly Plastic | | | | | | |

•Soils in nature rarely exist separately as gravel, sand, silt, clay or organic matter, but are usually found as mixtures with varying proportions of these components.

•Classifying soils into groups with similar behavior, in terms of simple indices, can provide geotechnical engineers general guidance about engineering properties of the soils through the accumulated experience.

| Plasticity index (PI %) | Smallest diameter (mm) | Degree of plasticity | Description |
|----------------------------|---------------------------|----------------------|---------------|
| 0 | - | Non-Plastic | Silt |
| 1-5 | 6 | Very Low Plastic | Clayey Silt |
| 5-10 | 3 | Low Plastic | Silt and Clay |
| 10-20 | 1.5 | Medium Plastic | Clay and Silt |
| 20-40 | 0.8 | High Plastic | Silty Clay |
| >40 | 0.4 | Very Plastic | Clay |

 Table 3.7. Classification of fine-grained soils according to their plasticity index (Burmister 1951)

In this study, laboratory tests are performed to the fraction that passes through the sieve analysis. These tests are performed to obtain Liquid Limit (LL) and Plastic Limit (PL) which are also known as Atterberg Limits. Plasticity Index (PI) is calculated using these limits. Plasticity Index values are shown in the table below.

Table 3.8. Plasticity Index Values for the Samples Obtained from Borings in the Study Area

| | | | - | | | 10 574 | | | | | | | | |
|-----------------|-----------------|------|-----------------|-----------|----|-----------------|-----------------|----|-----------------|-----------------|----|-----------------|-----------------|----|
| Maın regions | Sub- regions | Η | Maın regions | Sub- | Id | Maın regions | Sub- regions | Η | Maın regions | Sub- regions | Id | Maın regions | Sub- regions | Id |
| | A1 | NP | | B1 | NP | | C1 | NP | | D1 | NP | | E1 | 24 |
| | A2 | 21,2 | | B2 | NP | | C2 | NP | | D2 | NP | | E2 | NP |
| | A3 | NP | | B3 | NP | | C3 | NP | | D3 | NP | | E3 | NP |
| | A4 | NP | | B4 | NP | 7) | C4 | NP | | D4 | NP | | E4 | 19 |
| Region-A | A5 | NP | Region-B | B5 | NP | Region-C | C5 | NP | Region-D | D5 | NP | Region-E | E5 | NP |
| gio | A6 | NP | gio | B6 | NP | gio | C6 | NP | gio | D6 | NP | gio | E6 | NP |
| Re | A7 | NP | Re | B7 | NP | Re | C7 | NP | Re | D7 | NP | Re | E7 | 21 |
| | A8 | NP | | B8 | NP | | C8 | NP | | D8 | 20 | | E8 | 18 |
| | A9 | 19 | | B9 | NP | | C9 | NP | | D9 | 24 | | E9 | NP |
| | | | | | | | | | | | | | | |

k) Triaxial Compressive Strength Test

A cylindrical soil specimen is subjected to an all-round confining pressure in the conventional triaxial test. After that, the specimen is loaded axially in strain or stress-controlled manner. Generally, the dimensions are 200 mm height and 100 mm diameter for cylindrical sample. A rubber membrane contains the specimen. Preparation of the specimen is related with the soil type. Fine grained, cohesive soils can be used directly from undisturbed samples or can be used from remolded compacted samples. Coarse grained, cohesionless soils are compacted in a mold to the required relative density to obtain a cylindrical specimen.

The main reason to perform this test is to obtain shear strength parameters such as cohesion, friction angle or other dependent parameters.

l) Uniaxial Compressive Strength Test (UCS)

UCS test is commonly used to obtain the engineering parameters of rock which is an important concern for mining, civil and geotechnical engineers. Rock strength index can be obtained by Point Load Test (PLT) which is important in geotechnical engineering.

UCS test results were used for estimating the axial load capacity of rock units and undrained shear strength of the soils. UCS test results were selected from the reports with respect to conducting ASTM D2166-16 standard. Diameter to height ratio of cylindrical samples was defined as 1/2 and loading rate was selected as 1 mm/min for all samples according to this standard.

m) Point Load Strength Test

To obtain unconfined compressive strength of the rock, point load strength test is performed. Core samples can be tested as well as fractured rock samples. To perform the test, a piece of rock is squeezed and compressed between two points of cone shaped plates. The sample fails in tension between those two points. Point load strength index is obtained at the end of the test by equation 3.11. and this index is used for classifying rocks.

$$(I_S) = \frac{P}{D_e^2} \tag{3.11}$$

Is: point load strength index

P: breaking load

D_e: equivalent core diameter

| Table 3.9. Classification of rocks based on point load index experiment results |
|--|
| (Bieniawski, 1975) |

| Classification of rocks Strength | Point Load İndex |
|----------------------------------|------------------|
| Ultimate | > 80,00 |
| High | 80,00 - 40,00 |
| Medium | 40,00 - 20,00 |
| Low | 20,00 - 10,00 |
| Very Low | < 10,00 |

| Classification of a transformed to the strength (Trans, 1900) | | | | | | | | | |
|---|----------------|-----------------|-----------------------|------------------------|--|--|--|--|--|
| Classification of | Classification | $UCS (kg/cm^2)$ | | Classification of | | | | | |
| Rocks Strength | Chusshireation | e es (ig/eiii) | (kg/cm ²) | Rocks | | | | | |
| | | . 2200 | . 05 | Quartzite, diabase, | | | | | |
| Ultrahigh | А | >2200 | >95 | dense basalt | | | | | |
| | | | | Magmatic rocks, | | | | | |
| High | В | 1100-2200 | 50-95 | cemented sandstone, | | | | | |
| High | D | 1100-2200 | 30-93 | hard shale, limestone, | | | | | |
| | | | | dolomite | | | | | |
| | | | | shale, porous | | | | | |
| Medium | С | 550-1100 | 25-50 | sandstone, limestone, | | | | | |
| | | | | metamorphic rocks | | | | | |
| | | | | Porous and low | | | | | |
| Low | D | 275-550 | 13-25 | density of rocks, | | | | | |
| LOW | D | 275-550 | 15-25 | sandstone, clay shale, | | | | | |
| | | | | chalk, eroded rock | | | | | |
| | | | | | | | | | |
| Ultralow | Е | <275 <13 Like | | Like groups of soil D | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |

Table 3.10. Classification of rocks based on their strength (Hunt, 1986)

Tests of point load strength and uniaxial compression strength are performed on 82 rock samples taken from the study area. As a result, values which are essential to calculated rock strength parameters, are obtained.

3.5. Determination of Mechanical Properties

Bearing capacity of the soils was calculated according to Terzaghi's theorem with triaxial compressive strength from disturbed and undisturbed sampling. Bearing capacity of the rocks was calculated uniaxial compressive strength from disturbed sample.

3.5.1. Terzaghi's Bearing Capacity Method

The most common method of determining the bearing capacity of the soil is the Terzaghi's bearing capacity method which was developed in 1943. Terzaghi made some assumptions in order to develop a theory. These assumptions are;

- Soil is a homogenous, isotropic and a semi-infinite medium.
- Full friction exists between the foundation base and the soil.
- The depth of foundation is higher than its width.
- Shear strength of the soil= $c' + \sigma' tan \phi'$
- •General shear failure happens under the foundation.

• Foundation is rigid compared to the soil.

•The soil over the foundation base is idealized as distributed load and shear plane of this soil is not of concern.

• The external load that acts on the foundation is normal stress and it is on the centroid of the foundation, there exists no moment.

Terzaghi's theory suggests that the resistance to the applied load P is developed in three zones under the foundation with shear resistance and above the foundation with overburden pressure, Q. Cohesion of the soil can be seen in the first term in the equation, depth and overburden pressure is in the second term and the last term is related with length of the shear stress area and the width of foundation. Three bearing capacity factors, N_c , N_q , N_γ are related with internal friction angle, φ . Terzaghi's Bearing capacity equations:

$$Q = k_1 * c * N_c + \gamma_n * D_f * N_q + k_2 * B * \gamma_n N_{\gamma}$$
(3.12)

Q: Ultimate bearing capacity of soil

k₁ and k₂: Foundation shape coefficients

 $N_c,\,N_q,\,N_\gamma\!\!:$ Terzaghi bearing capacity factors

c: Cohesion of soil

- φ: Internal friction angle
- B: Width of foundation
- D_f: Depth of foundation
- γ_n: Unit weight of soil

| | <u>1</u> | |
|------------------|-----------|-------------|
| Foundation Shape | k1 | k2 |
| Strip | 1 | 0.5 |
| Square | 1.2 | 0.4 |
| Circular | 1.3 | 0.3 |
| Rectangular | 1+0.2*B/L | 0.5-0.1*B/L |

Table 3.11. Foundation shape coefficients

| φ | Nc | Nq | Νγ | φ | Nc | Nq | Νγ |
|----|-------|-------|------|----|--------|--------|--------|
| 0 | 5,70 | 1 | 0 | 26 | 27.09 | 14.21 | 9.84 |
| 1 | 6 | 1.1 | 0.01 | 27 | 29.24 | 15.9 | 11.6 |
| 2 | 6.3 | 1.22 | 0.04 | 28 | 31.61 | 17.81 | 13.7 |
| 3 | 6.62 | 1.35 | 0.06 | 29 | 34.24 | 19.98 | 16.18 |
| 4 | 6.97 | 1.49 | 0.1 | 30 | 37.16 | 22.46 | 19.13 |
| 5 | 7.34 | 1.64 | 0.14 | 31 | 40.41 | 25.28 | 22.65 |
| 6 | 7.73 | 1.81 | 0.2 | 32 | 44.04 | 28.52 | 26.87 |
| 7 | 8.15 | 2 | 0.27 | 33 | 48.09 | 32.23 | 31.94 |
| 8 | 8.6 | 2.21 | 0.35 | 34 | 52.64 | 36.5 | 38.04 |
| 9 | 9.09 | 2.44 | 0.44 | 35 | 57.75 | 41.44 | 45.41 |
| 10 | 9.61 | 2.69 | 0.56 | 36 | 63.53 | 47.16 | 54.36 |
| 11 | 10.16 | 2.98 | 0.69 | 37 | 70.01 | 53.8 | 65.27 |
| 12 | 10.76 | 3.29 | 0.85 | 38 | 77.5 | 61.55 | 78.61 |
| 13 | 11.41 | 3.63 | 1.04 | 39 | 85.97 | 70.61 | 95.03 |
| 14 | 12.11 | 4.02 | 1.26 | 40 | 95.66 | 81.27 | 115.31 |
| 15 | 12.86 | 4.45 | 1.52 | 41 | 106.81 | 93.85 | 140.51 |
| 16 | 13.68 | 4.92 | 1.82 | 42 | 119.67 | 108.75 | 171.99 |
| 17 | 14.6 | 5.45 | 2.18 | 43 | 134.58 | 126.5 | 211.56 |
| 18 | 15.12 | 6.04 | 2.59 | 44 | 151.95 | 147.74 | 261.6 |
| 19 | 16.57 | 6.7 | 3.07 | 45 | 172.28 | 173.28 | 325.34 |
| 20 | 17.69 | 7.44 | 3.64 | 46 | 196.22 | 204.19 | 407.11 |
| 21 | 18.92 | 8.26 | 4.31 | 47 | 224.55 | 241.8 | 512.84 |
| 22 | 20.27 | 9.19 | 5.09 | 48 | 258.28 | 287.85 | 650.87 |
| 23 | 21.75 | 10.23 | 6 | 49 | 298.71 | 344.63 | 831.99 |
| 24 | 23.36 | 11.4 | 7.08 | 50 | 347.5 | 415.14 | 1072.8 |
| 25 | 25.13 | 12.72 | 8.34 | | | | |

Table 3.12. Terzaghi's Bearing Capacity Factors (Terzaghi, K., 1943)

In this study, bearing capacity of the soils was calculated according to Terzaghi's theorem with making some assumptions and keeping some parameters as constant. These assumptions can be explained as; (1) depth of foundation (D_f) was kept constant as 2 meter, (2) foundation type was considered as mat foundation (20 x 20 m). Foundation shape coefficients k_1 and k_2 values were calculated as 1,2 and 0,4 respectively and used as constant for all calculations because of constant width of foundation (for B=20 m).

3.5.2. Point Load Strength

The point load test provides an index value for the compressive strength, usual practice is to calibrate the results with a limited number of uniaxial compression tests on prepared core samples. Index-to-strength conversion factors are used to estimate uniaxial compressive strength. These factors have been proposed by various researchers and are dependent upon rock type.

qun = (C) Is (Beiniawski 1989)

(3.13)

Is: Point Load İndex

C: Material Constant for Rock Properties

Qun: Average uniaxial compressive strength of the sample

Qa: Bearing Capacity =Ks* qun

| 1 | | (Hoek ve Brown 19 | 97) | | |
|--------------------------|----|-------------------|-----|----------------|----|
| Sedimentary Rocks | С | Metamorphic Rocks | С | Magmatic Rocks | С |
| Conglomerate | 22 | Marble | 9 | Granite | 32 |
| Sandstone | 17 | Hornfels | 19 | Diorite | 25 |
| Siltstone | 7 | Metasandstone | 19 | Granodiorite | 29 |
| Claystone | 4 | Quartzite | 20 | Gabbro | 27 |
| Graywacke | 18 | Migmatite | 29 | Norite | 20 |
| Shale | 6 | Amphibolite | 26 | Dolerite | 16 |
| Marn | 7 | Gneiss | 28 | Profirite | 20 |
| Crystalline Limestone | 12 | Schist | 12 | Peridotite | 25 |
| Sparteine | 10 | Phyllite | 7 | Rhyolite | 25 |
| Biomicrite | 9 | Slate | 7 | Dacite | 25 |
| Dolomite | 9 | | | Andesite | 25 |
| Gypsum | 8 | | | Basalt | 25 |
| Anhydride | 12 | | | Aglomerate | 19 |
| Chalkstone | 7 | | | Breccia | 19 |
| | | | | Tuff | 13 |

Table 3.13. Species of rocks according to constant of material (C) (Hoek ve Brown 1997)

Table 3.14. Discontinuity spacing

| · · · · | Ŭ |
|---------------------------|------|
| Discontinuity spacing (m) | Ks |
| >3.00 | 0.40 |
| 3.00-0.90 | 0.25 |
| 0.90-0.30 | 0.10 |

In this study the bearing capacity of the rocks are found with point load test strength calculations.

As a result, Terzaghi's bearing capacity calculations and the bearing capacity values calculated from point load strength are presented in the table below.

| | | | | | | | - ap a - | 109 .0 | | | - 8-0- | | | |
|-----------------|-----------------|------------------------|-----------------|-----------------|------------------------|-----------------|-----------------|------------------------|-----------------|-----------------|------------------------|-----------------|-----------------|------------------------|
| Maın regions | Sub- regions | q _{ult} (kPa) | Main regions | Sub- regions | q _{ult} (kPa) | Maın regions | Sub- regions | q _{ult} (kPa) | Maın regions | Sub- regions | q _{ult} (kPa) | Main regions | Sub- regions | q _{ult} (kPa) |
| | A1 | 540 | | B1 | 846. 3 | | C1 | 447 | | D1 | 425 | | E1 | 140 6 |
| | A2 | 389 | | B2 | 1307 | | C2 | 513 | | D2 | 105 0 | | E2 | 439 |
| | A3 | 138 8 | | B3 | 1375 | | C3 | 117 0 | | D3 | 115 4 | | E3 | 415 |
| A | A4 | 490 | B | B4 | 1417 | c | C4 | 211 6 | Q | D4 | 466 | E | E4 | 542 |
| Region-A | A5 | 109 8 | Region-B | B5 | 1976 | Region-C | C5 | 148 9 | Region-D | D5 | 821 | Region-E | E5 | 506 |
| Ŗ | A6 | 169 1 | R | B6 | 1409 | R | C6 | 384 | R | D6 | 596 | R | E6 | 457 |
| | A7 | 842 | | B7 | 1653 | | C7 | 109 7 | | D7 | 710 | | E7 | 374 |
| | A8 | 133 2 | | B8 | 1313 | | C8 | 101 5 | | D8 | 570 | | E8 | 159 9 |
| | A9 | 509 | | B9 | 834 | | С9 | 119 2 | | D9 | 103 2 | | E9 | 176 7 |

Table 3.15. The bearing capacity values of the regions

3.4.1.3. Office Surveying

The geographic, geotechnical and geophysical surveys conducted in the field examined 45 soil investigation report surveys in the office environment and the coordinates of the soil investigation report surveys were examined in Netcad environment. These coordinates were transferred to the Geotechnical Information System environment with the necessary conversion parameters.

3.6. Liquefaction of Soils

Soil liquefaction occurs when waterlogged soil behaves like a liquid. Some people refer to it as earthquake liquefaction. The vibrations of earthquake shockwaves in water-saturated soils trigger the phenomenon.

Earthquakes are a very common origin of soil liquefaction damage, but other vibrationcreating events can be a factor. This includes construction activities, such as blasting, soil compaction, and similar tasks. Sometimes, people insert a vibrating probe into the ground to induce the effect intentionally. This process is vibroflotation.

Soil liquefaction occurs most frequently in sandy, silt-laden, gravel-based, loose or poorly drained soils. Quicksand is an example of this phenomenon. The watersaturated sandy soil cannot bear the weight of items, causing them to sink.

Liquefaction can be defined as a "liquid" behavior as a result of the effect of seismic waves of water-saturated fine-grained sand and silt-like layers as a result of the effect

of an increase in the pore water pressure and the effective stress by losing completely its ultimate carrying capacity.

In an environment without drainage conditions, liquefaction occurs as a result of the seismic pressure increase due to earthquake waves and equal to the total pressure or exceeds the total pressure.

$$\sigma' = \sigma - u \tag{3.12}$$

 σ' = Effective Stress

 σ =Total Stress

u =Pore Water Pressure

Soils of liquefaction potential is determined by land test results. These test results; Standard Penetration Test, Cone Penetration resistance, shear wave velocity, dilatometer, acceleration thresholding method.

In this study, the liquefaction potential was measured according to the acceleration thresholding method.

Acceleration thresholding method;

Acceleration thresholding method safety factor, for Fa;

Fa=1,6 a_t / a_{max}

 $Fa \le 1$ high liquefaction zone

Fa>1 low liquefaction zone

Using site investigation reports, liquefaction potential of certain regions are determined. Liquefaction potential of the regions was considered as high liquefaction zone (HLZ), low liquefaction zone (LLZ) and none liquefaction zone (NLZ) according to soils condition and groundwater table level information of each region.

| | 50 | - | | | | | <u>~</u> | | | 20 | - | | 5 | |
|----------|-------------|----------------------------|----------|-----------------|----------------------------|----------|-------------|----------------------------|----------|-------------|----------------------------|----------|-------------|----------------------------|
| Main | Sub-regions | Liquefactio n Potential | Main | Sub- Regions | Liquefactio n Potential | Main | Sub-regions | Liquefactio n Potential | Main | Sub-regions | Liquefactio n Potential | Main | Sub-regions | Liquefactio n Potential |
| | A1 | LLZ | | B1 | NLZ | | C1 | NLZ | | D1 | NLZ | | E1 | LLZ |
| | A2 | NLZ | | B2 | NLZ | | C2 | NLZ | | D2 | NLZ | | E2 | HLZ |
| | A3 | NLZ | | B 3 | NLZ | | C3 | LLZ | | D3 | NLZ | | E3 | NLZ |
| ¥- | A4 | NLZ | Ą | B4 | NLZ | ပု | C4 | NLZ | Ą | D4 | NLZ | щ | E4 | HLZ |
| Region-A | A5 | NLZ | Region-B | B5 | NLZ | Region-C | C5 | HLZ | Region-D | D5 | NLZ | Region-E | E5 | NLZ |
| Re | A6 | NLZ | Re | B6 | NLZ | Re | C6 | NLZ | Re | D6 | NLZ | Re | E6 | HLZ |
| | A7 | NLZ | | B7 | NLZ | | C7 | NLZ | | D7 | NLZ | | E7 | LLZ |
| | A8 | NLZ | | B8 | NLZ | | C8 | HLZ | | D8 | LLZ | | E8 | HLZ |
| | A9 | NLZ | | B9 | NLZ | | C9 | NLZ | | D9 | HLZ | | E9 | NLZ |

 Table 3.16. According to regions Liquefaction Potential assessment

3.7. Ground Water Table (GWT)

According to geotechnical investigation reports evaluated for this study, ground water table levels were examined for all regions. The ground water table depth is less than 5 m in the center,

| Main regions | Sub-regions | Groundwate r table level | Main regions | Sub-regions | Groundwate r table level | Main regions | Sub-regions | Groundwate r table level | Main regions | Sub-regions | Groundwate r table level | Main regions | Sub-regions | Groundwate r table level (m) |
|--------------|-------------|-----------------------------|--------------|-------------|-----------------------------|--------------|-------------|-----------------------------|--------------|-------------|-----------------------------|--------------|-------------|------------------------------------|
| | A1 | 5 | | B1 | NP | | C1 | NP | | D1 | NP | | E1 | 1,3 |
| | A2 | NP | | B2 | NP | | C2 | NP | | D2 | NP | | E2 | 1,5 |
| | A3 | NP | | B3 | NP | | C3 | 3,5 | | D3 | NP | | E3 | NP |
| ¥- | A4 | NP | ę | B4 | NP | ပု | C4 | NP | Ģ | D4 | NP | E | E4 | 3 |
| Region-A | A5 | NP | Region-B | B5 | NP | Region-C | C5 | 2,8 | Region-D | D5 | NP | Region-E | E5 | 2,7 |
| Ř | A6 | NP | R | B6 | NP | R | C6 | NP | R. | D6 | NP | R | E6 | 3 |
| | A7 | NP | | B7 | NP | | C7 | NP | | D7 | NP | | E7 | 3 |
| | A8 | NP | | B8 | NP | | C8 | 2 | | D8 | 2,9 | | E8 | 4 |
| | A9 | NP | | B9 | NP | | С9 | NP | | D9 | 3 | | E9 | NP |

Table 3.17. According to regions ground water table assessment

The physical and the mechanical properties of the regions in the study area are shown in the table below with their respective minimum and maximum values.

| Physical and Mechanical properties | A-Re | | | egion | 1 | egion | | egion | Ε | -Region |
|---|------|------|------|-------|------|-------|------|-------|------|---------|
| | Min. | Max. | Min. | Max. | Min. | Max. | Min. | Max. | Min. | Max. |
| Particle unit weight, <i>y_s</i> (kN/m ³) | 25.9 | 27.1 | 26.0 | 27.1 | 26.0 | 27.3 | 19.1 | 26.0 | 26,0 | 27 |
| Natural unit weight, y _n (kN/m ³) | 17.3 | 22.8 | 18.3 | 22.5 | 15.8 | 22.6 | 16.2 | 18.9 | 16 | 22.8 |
| Dry unit weight, <i>y</i> _d (kN/m ³) | 14.3 | 17.0 | 17.2 | 18.2 | 13.5 | 17.7 | 13.5 | 18.3 | 14 | 17 |
| Moisture content, w (%) | 6.7 | 21.9 | 4.0 | 6.0 | 2.2 | 36.9 | 2.5 | 38.6 | 24 | 34 |
| Void ratio, v (%) | 57.0 | 84.0 | 41.0 | 52.8 | 47.0 | 99.0 | 42.0 | 92.0 | 52 | 87 |
| Porosity, n (%) | 37.0 | 46.0 | 33.0 | 47.5 | 32.0 | 50.0 | 29.0 | 48.0 | 43 | 46 |
| Degree of saturation | 29.0 | 72.0 | 25.0 | 31.0 | 13.0 | 100.0 | 20.0 | 100.0 | 86 | 90 |
| Liquid limit, w _L (%) | 36.1 | 47.7 | - | - | 41.5 | 42.5 | 51.0 | 52.0 | 37 | 51 |
| Plastic limit, w _p (%) | 18.2 | 24.3 | - | - | 23.1 | 23.3 | 27.0 | 28.0 | 17 | 20 |
| Plasticity Index, PI (%) | 17.9 | 23.4 | NP | NP | 18.2 | 19.4 | 24.0 | 25.0 | 20 | 29 |
| Cohesion, c (kPa) | 14 | 40 | 6.6 | 7.6 | 3.2 | 57.0 | 5.0 | 47.0 | 7,8 | 44 |
| Internal friction angle, Ø (°) | 3.5 | 16 | 17.7 | 18.1 | 8.0 | 22.3 | 3.3 | 21.0 | 2 | 15,33 |
| Specific gravity, G _s (%) | | | | | | | | | | |
| Point load index, Isc (kg/cm ²) | 5.4 | 10.9 | 6.4 | 11.5 | 8.7 | 11.8 | - | - | 6,2 | 13,5 |
| С | 13.0 | 19.0 | 13.0 | 19.0 | 13.0 | 19.0 | - | - | 13 | 19 |
| TCR, (%) | 30.0 | 70.0 | 40.0 | 75.0 | 70.0 | 80.0 | - | - | | |
| SCR, (%) | 20.0 | 55.0 | 30.0 | 65.0 | 50.0 | 65.0 | - | - | | |
| Rock quality degree, RQD (%) | 5.0 | 20.0 | 5.0 | 40.0 | 20.0 | 30.0 | - | - | | |
| Bearing Capacity (Kpa) | 389 | 1691 | 846 | 1976 | 383 | 2115 | 422 | 1049 | 338 | 1406 |

Table 3.18. Physical and Mechanical Properties

CHAPTER 4

TEST RESULTS AND DISCUSSIONS

As it was presented by the past studies, geotechnical mapping method applied for this work includes the drawing of some maps. Each map was prepared as a separate section in the Geographic Information System (GIS) database. GIS is a talented method to combine the associated ground data into conventional geotechnical databases for presenting more generic view of the specific region (Kaâniche et al., 2000). For this type of studies, GIS data provides ground observation of complicated geological systems (Kolat et al., 2006; Xie et al., 2006; Yilmaz, 2008, 2009).

In this study, several types of geotechnical maps expressing some geotechnical parameters those have significant effects on defining the area for the suitability of construction works were drawn by using the data obtained from the different boreholes for Niğde city. These drawn maps by GIS technic for this study present: (1) ground water table, (2) liquefaction zone, (3) plasticity index, (4) bearing capacity, (5) soil classification and (6) SPT results. All maps were presented and discussed below sections.

4.1. Ground Water Table (GWT) Map

One of the main parameters influencing the stability of the earth works as well as the application of the excavations for foundation design under several construction works is ground water table depth. Moreover, the level of ground water table should be predicted especially for granular sandy soils to analysis the liquefaction potential of soil strata. The shallow unconfined aquifers formed by the lithological units given in this study because of the plenty of alluvium type soils can be easily observed. The static ground water level was determined by considering of the highest elevation of the static water levels obtained from boreholes and piezometer data.

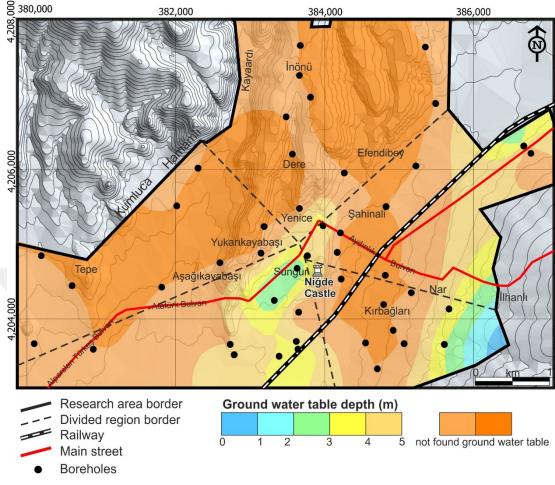


Figure 4.1. Ground water table map depths for the study area

The ground water table depth is less than 5 m in the center, East and South side of Niğde city. Especially in South-West side of the city, the ground water table depth is very near to the ground surface. However, no water table is observed in the other side of the city. Fig. 4.1. Water table is very near to the ground surface in specific regions which have lower ground elevations or alluvium type of soils. This can clearly be understood from lithological and morphological structure of the city. However, for regions in higher ground elevations and regions with rock units such as Tuff and Agglomerate, ground water table is not observed. This is shown in Fig. 4.6. Therefore, for construction purposes; while the regions with shallow static ground water layer (0-5 m) can be considered as the least favorable, some regions with static ground water layer (static ground water layer greater than 10 m, these types of areas are known as the most favorable for evaluating the liquefaction potential of soils (El-May et al., 2010).

4.2. Liquefaction Zone Map

As it is commonly known that soil liquefaction potential will be present in the areas, where coarse silty, sandy soil and shallow groundwater level are present and when long duration of strong earthquake occurs (Ozdemir and Ince, 2004). Therefore, it must be analyzed for obtaining better risk and mitigation determinations. The liquefaction potential of the studied area has been investigated due to its socioeconomic aspect and its growing population. Generally, liquefaction potential of soils is analyzed by using some decisional flow chart for determination of earthquake-induced effects regarding on obtained data such as paleo-liquefaction, geological features, groundwater table depth, seism-tectonics, sedimentary properties and geotechnical parameters of soils (El-May et al., 2010; El May et al., 2009).

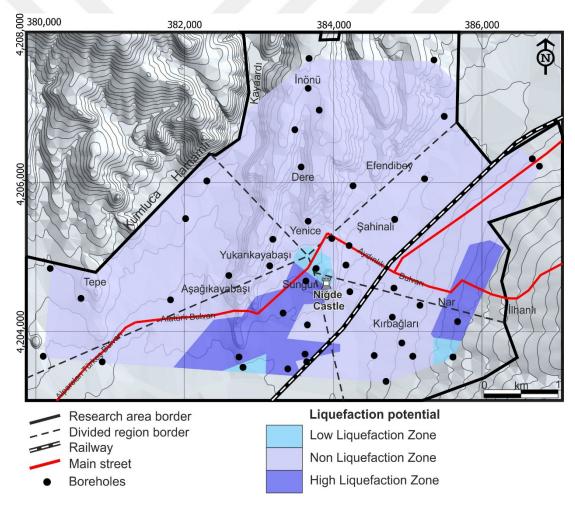


Figure 4.2. Liquefaction zones map for the study area

While some regions given in Fig.4.2 have high soil liquefaction potential according to the site investigation reports used for this study, some regions have low soil liquefaction potential. On the other hand, some part of the study area has no soil

liquefaction potential. Therefore, the soil liquefaction potential of the study area was showed as Low liquefaction zone (LLZ), High liquefaction zone (HLZ) and Noliquefaction zone (NLZ). Most of the study area has no soil liquefaction potential according to Fig. 4.2. As it is clearly seen from Fig.5, in a little part of South-East and South side of study area has soil liquefaction potential. When these regions are observed, ground water table is very near to ground surface and their soil profile includes generally granular and fine soils. However, the regions that have no soil liquefaction potential have rock units such as Tuff and Agglomerate.

4.3. Plasticity Index Map

Soil plasticity is defined as the ability to undergo deformations before any cracks are formed. For fine grained soil, it is a crucial index property especially for clays and clayey soils. Plasticity is the effect of the adsorbed water in the voids. The water in the voids allows the fine-grained clay particles to slip over one another and prevents the particles from returning to their initial position. Therefore, plastic deformations occur. This property can only be seen with clay particles. An interesting observation is that the effect of consistency limits with engineering properties of clayey soils. Due to some common set of factors, consistency limits and engineering properties have similar uses. Clay content governs the plasticity index. Therefore, clayey soils tend to be highly plastic. As the amount of clay particles increase, the plasticity index increases proportionally. In Fig.4.3 plasticity index of some areas in the study area is shown. As it is clearly shown in Fig. 4.3, most of the study area is non-cohesive soil. Rock units such as Tuff and Agglomerate are the main reason why plasticity does not exist. Generally, plasticity index value ranges between 15 % and 25 % in where the plasticity index is existent. Plasticity index can be obtained from the North-West side as well as South part of the study area Fig. 4.3.

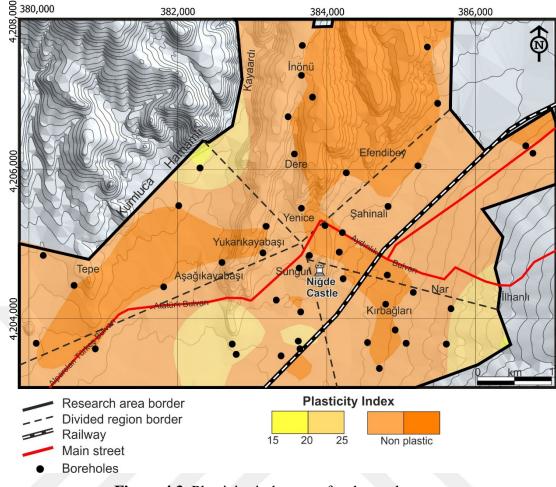


Figure 4.3. Plasticity index map for the study area

4.4. Bearing Capacity Map

The load bearing capacity of soils is very important parameter when any construction work is designed. The bearing capacity of soil can also be defined as acceptable load carrying capacity of soil without any collapse (Kadhim et al., 2003; Castelli et al., 2012). After entering the data of bearing capacity and UCS results for rock units into a GIS program, this program produced geotechnical color maps represent bearing capacity of the study area distributed to residential areas for 5 m depth as shown in Fig. 4.4. As it is clearly seen from Fig. 4.4., there is a very large range for bearing capacity values in the study area. While the bearing capacity values obtained from the different part of the study area have very low values (0-250 kpa), some have very high values (2000-2500 kPa). According to Fig. 4.4., the bearing capacity values of the North side of the study area are greater than one of the South sides of this region. This can be explained that the North side of the study area mostly includes rock units as a soil layer. It can be said that the South-East side of the study area can be explained as the most problematic soil based on bearing capacity. Some part of this region has

bearing capacity lower than 250 kPa. On the other hand, most of the study area has bearing capacity higher than 750 kPa. Some parts of this region have bearing capacity greater than 1000 kPa because of having rock units as soil layer. As a result, it can be concluded that many parts of the study area is very safer in terms of bearing capacity for construction works. However, this cannot be said for a little part of the study especially for the South-East part of this region.

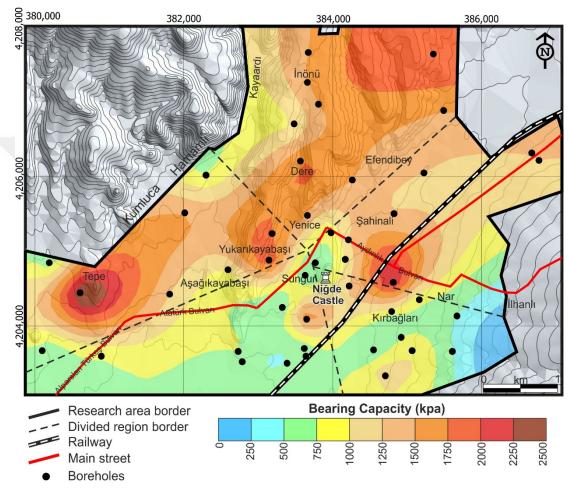


Figure 4.4. Bearing capacity map for the study area

4.5. SPT Results Map

Standard Penetration Test (SPT) is a very common test that is used for defining some important geotechnical properties of soil layers. In geotechnical surveying, in order to define some geotechnical parameters such as internal friction angle, relative density, bearing capacity and compressibility of soils, geotechnical experts may benefit from SPT-N values. Therefore, this test is very simple and helpful test for site investigation in geotechnical works. In this study a SPT map was prepared for Niğde city by using the GIS method as clearly seen in Fig. 4.5. All SPT values taken from the study area

were determined for 5 m depth layer of ground. According to Fig. 4.5. the regions, which have SPT-N value greater than 50, have generally rock units. Whereas most of the regions in this city have SPT-N values greater than 40, very limited area has lower SPT-N values. Especially, South and South-East side of the study area have SPT-N values lower than 30. And more, in some part of the South-West side of the study area it is observed that SPT-N values are ranged between 20 and 30. The areas in which the lowest SPT-N values are seen are shown in green color as given in Fig. 4.5. These areas have either very low bearing capacity or very high liquefaction potential as it was discussed in Fig. 4.4 and Fig. 4.2.

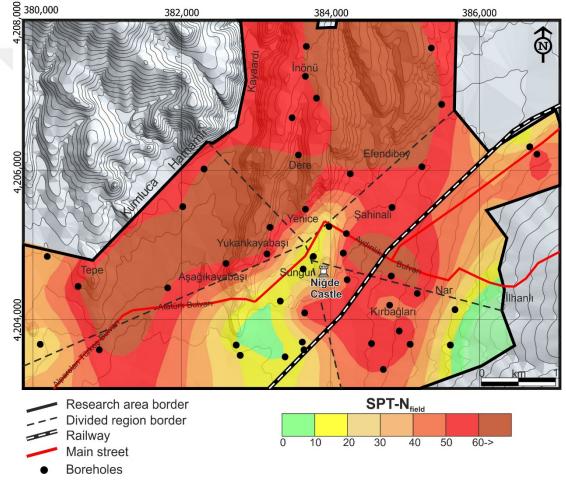


Figure 4.5. SPT-N results map for the study area

4.6. Soil Classification Map

As it is clearly seen from fig. 4.6. different types of soils, which are low and high plasticity clay, silty sand, agglomerate and tuff, can be observed in lithology of the study area for 5 m depth layer. While a little part of the study area was formed by clay type soil, a very big part of this area was existed by sandy and rock type of soils see

Fig. 4.6. North-West side of the study area is mostly seen rock type of soil (agglomerate and tuff); in contrast South-East side of this area is generally layered as silty sand. Some part of the study area such as little part of middle south side, end of South-East side, small part in the city center and middle part of the North-West side include high and low plasticity clay.

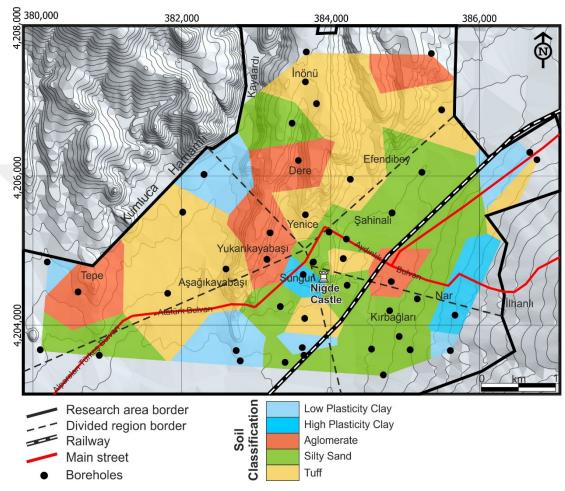


Figure 4.6. Soil classification map for the study area

4.7. General Consideration about this Study

When we look at the past studies related with cases of urban mapping methods given in the literature (Campolunghi et al., 2006; Özsan et al., 2007), most of them do not cover geological, seism-tectonic and geotechnical data such as assessment for liquefaction potential and bearing capacity. Therefore, this study can be accepted as a very good example because of its very complicated geomorphological feature with significant urban growth where decision makers and city planners need some beneficial maps that present detailed information such as geotechnical zoning for a safe urban growth. The Geotechnical Mapping Method used in this study was applied based on Geographic Information System (GIS) utility. This method includes multidisciplinary analysis. In this study it was concluded that the liquefaction phenomenon is very important parameter for Nigde city in terms of natural disaster effect. High liquefaction potential, which is considered as a hazard phenomenon that should be taken under control for especially providing safety of developing urban area, can be observed in many urban areas (Lee et al., 2003; Krinitzsky, 2005). Therefore, a rational planning should be conducted by city planners and decision makers for providing sustainable growing in developing urban areas.



CHAPTER 5

CONCLUSIONS

In this study Engineering Geotechnical Mapping Method (EGMM) prepared with a GIS software program was conducted in order to observe and compare some geological and geotechnical properties of Niğde city (in Turkey). Some conclusions can be drawn from this study are presented below.

- 1. GIS data provided the ground observation of complicated geological systems in Nigde city.
- 2. Several types of geotechnical maps expressing some geotechnical parameters those have significant effects on defining the area for the suitability of construction works were drawn by using the data obtained from the different boreholes for Nigde city. These drawn maps by GIS technic for this study present: (1) ground water table, (2) liquefaction zone, (3) plasticity index, (4) bearing capacity, (5) soil classification and (6) SPT results. All maps were presented and discussed below sections.
- 3. When we look at the lithological and morphological structure of the city, it can be clearly understood that ground water table is very near to the ground surface in the specific regions those are either in lower ground elevations or in alluvium type soils.
- 4. For construction purposes; while the regions with shallow static ground water layer (0-5 m) can be considered as the least favorable, some regions with static ground water layer (5-10 m) can be considered as favorable. And more, if the region has static ground water layer greater than 10 m, these types of areas are known as the most favorable in order for evaluating the liquefaction potential of soils.
- 5. In a little part of South-East and South side of study area has soil liquefaction potential.

- 6. The regions where plasticity index is not observed have generally rock units such as Tuff and Agglomerate. When the regions where plasticity index is obtained are surveyed, it can be seen that plasticity index value range between 15 % and 25 % in these regions.
- 7. The bearing capacity values of North side of study area are greater than one of South side of this region. This can be explained that North side of the study area mostly includes rock units as a soil layer. It can be said that the South-East side of the study area can be explained as the most problematic soil based on bearing capacity.
- 8. The areas where the lowest SPT-N values are seen in Nigde city, have either very low bearing capacity or very high liquefaction potential.
- 9. Different types of soils, which are low and high plasticity clay, silty sand, agglomerate and tuff, can be observed in lithology of the study area for 5 m depth layer.
- 10. All of the geotechnical properties that belong to the study area, are average, general properties. For any building or structure that is to be constructed in the area, a ground investigation must be made beforehand. The properties should be re-evaluated according to the chosen foundation system and ground conditions.

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APPENDIX

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| YAI | PI SAHİ | Bİ | | DMR DAY. 7 | AY. TÜK. MAL. EL. AK. ÜR. TİC. LTD. ŞTİ. | | | | | | | | | | | marsı | | K16-2377-Z | | | | | | | | | | | | | | | | | |
| YAI | PININ A | DRES | șî 🛛 | YAĞDAN M/ | H. / MERKE | Z / NÍĞD | E | | | | | | ~ | | Rapor Ta | arihi | | 14.12.2016 | | | | | | | | | | | | | | | | | |
| PAR | FTA/AD | A/PA | R\$EL | 2833 ADA / | 14 PARSEL | | | | | | | | | | Rapor N | umarası | | R16-2377-2 | 1 | | | | | | | | | | | | | | | | |
| | | | | TOP | LU DEN | NEY SC | DNUÇL | ARIR | APOF | ٤U | | | | | Bakanlık | Rap. No | | 11722763 | | | | | | | | | | | | | | | | | |
| | 1 | Jumune | | Doğal Su | Doğai Birim | Elek | Analizi | Atte | rberg Lin | nitleri | | Nokta | Üç Eks Basınç | | Konsol | Idasyon | 1 | Direkt Kesr | ne Deneyi | | | | | | | | | | | | | | | | |
| Kuy | | oi ve Idi | Derinlik | Muhtevası (%) | Hacim Ağırlık (gr/cm ³) | #4 Kalan (%) | #200 Geçen (%) | LL (%) | PL (%) | PI (%) | USCS | Yükleme Dayanımı (kgf/cm2) | * C _{up} (kgf/cm ²) | *f _{up} (°) | Şişme Yüzdesi (%) | Şişme Basıncı (kN/m²) | Gs | * c _{up} (kgf/cm ²) | *f _{up} (°) | | | | | | | | | | | | | | | | |
| SK | | | 1.50-1.95 | 3,62 | 1,83 | 8,72 | 25,26 | | NP | | SM | | | | | | | | | | | | | | | | | | | | | | | | |
| SK | | | 2.50-3.00 | 2,85 | 1,84 | 5,86 | 26,92 | | NP | | SM | | | | | | | 0,0632 | 29,1 | | | | | | | | | | | | | | | | |
| SK | | | 2.50-3.00 | 3,45 | 1,84 | 7,88 | 27,72 | | NP | | SM | | | | | | | 0,0681 | 28,9 | | | | | | | | | | | | | | | | |
| | | | 6.00-6.45 | 3,75 | 1,84 | 4,84 | ; 25,45 | | NP | | SM | | | 114 | | | | | 00.7 | | | | | | | | | | | | | | | | |
| | | | 2.50-3.00 | 2,19 | 1,85 | 9,27 | 28,64 | | NP | | SM | | | | | | | 0,0753 | 28,7 | | | | | | | | | | | | | | | | |
| SK | | | 6.00-6.45 | 3,65 | 1,84 | 7,68 | 26,36 | | NP NP | | SM SM | | | | | | | 0,0618 | 29,2 | | | | | | | | | | | | | | | | |
| . SK | (-4) 0 | D | 2.50-3.00 | 2,45 | 1,84 | 6,02 | 24,51 | | NP | | 511 | · | | | | | · · · | 0,0010 | 23,2 | | | | | | | | | | | | | | | | |
| * Lab | boratuvarimiz rapor, sadece | z Çevre v e deneyî y | e Schircilik Ba yapılan numun | - 1900-2 ve TS kanhānın 11.0 o için geçerlidir. I YAPAN | .2011 tarih ve | | | | | anmızın izni | olmaksızın d | leğiştirilemez ve | | Beki | nn guveniliriigi SORATUVAI PAKA Ioji Yuk. N Beige No | R DENETÇÎ | oaşma bir i İSÎ | ikir vermez. | | | | | | | | | | | | | | | | | |
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| ZEMİ | | NIĜI LABO | RATUV | ARI | | | | ADRES:M | <u>EST ZEIV</u> IELÍKGA | Zİ MH.AŞ | TEL :035 | E LABORATUVA L BUL.BARIŞMA 2 333 55 44 ZEMTEST.COM | NÇO KOI | NAĞI N | 0:4/A | | | | T.C ÇE BA | VRE V | E ŞEHİ GI | RCILIK | |
|--------------------------------|--|--|--|-----------------------|--------------------|---------------------|----------------|----------------|----------------------------|-------------------------|----------------|--|---------------------------|-----------|-------------|------------|------------------------------------|---------|------------------|---------------|---------------------------|---------------------|----------------------------|
| | | | | | | | ABOR | | | FNEY | TER | TOPLU SO | | RAPC | R FO | RMU | | | | | | | |
| üklenic roje Ad tapor No | 1 | | ADER MÜ NÍĞDE ILI 3759-17 | | | | | | | | | | | | | | Sayfa No Numune G Rapor Tarl | | irihi | | 1/1 11.07.2 20.07.2 | | |
| Sondaj | 1 | umune | Doğal Su İçeriği | Atte | erberg Lin | nitleri | Elek A | nalizi | Zemin Sınıfı | | OrtDbha | Serbest Basing Deneyi(qu) | Oç Ekse /(C | nii (UU) | Kons | sisme bas. | Bakanlık F Bha | aporN | No oktor | CBR 2.5 mm | 0zg01 | | t Kesme Ø |
| Kuyu No: | Tipi ve Adı | Deriniik (m-m) | (%) | | PL (%) | | +4 Kalan | - 200 Geçen | USCS | Ort.ls (50) (Kg/cm2) | Yn (gr/em*) | kg/cm2 | C Kgt/cm2 | 1 | şişme 96 | kN/m2 | (g/cm*) W | opt (%) | Ykmax (c/cm*) | % | ağırlık | Kohezyon Kgf/cm2 | içsel sürtünme nctai |
| SK-1 | UD | 1,50-2,00 | 26,3 | 41,5 | | 18,2 | (%) 0,00 | (%) 75,30 | CL | - | 1,85 | - | 0,57 | 8 | X | X | - | - | - | - | | | - |
| SK-1 SK-1 | SPT SPT | 3,00-3,45 | 20,6 | NP | NP | NP | 6,70 29,50 | 37,20 | SM | | 1,71 | | - | - | - | - | - | - | - | - | - | - | - |
| SK-1 | SPT | 6,00-6,45 | 18,8 | NP | NP | NP | 55,80 | 6,10 | GP | - | 1,75 | - | - | - | - | | | - | | - | | - | |
| SK-1 | SPT | 7,50-7,95 | 17,4 | NP | NP | NP | 59,20 67,10 | 4,60 | GP | | 1,76 | | | | - | | - | - | | | - | | - |
| 5K-1 SK-2 | SPT UD | 9,00-9,45 | 20,8 | NP | NP | NP | 6,50 | 36,60 | SM | | 1,69 | - | - | - | | - | - | - | - | - | - | 0,185 | 22 |
| SK-3 SK-4 | | 1,50-2,00 | 21,6 | NP 42,5 | NP | NP 19,4 | 4,40 | 31,90 | SM CL | - | 1,70 | - | - 0,54 | - 9 | | | | - | + | | | 0,197 | 22 |
| Söz kor Tüm ha ' Labora | kları Zemtes atuvarımız 47 Deney | nsiz hiçbir şekild conuçları,sadece st Zemin Araştırı 708 sayılı kanun yi Yapan ŞAF Çeç Müh 1 NØ:14982 | e test ediler ma ve Lab.l n gereği T.C | n deney Hiz Ltd. 1 | numun Sti.'ve a | elerine a ittir. | | n verilen | 02.03.0: | 16 tarih ve | ≥ 539 No'l | u laboratuvar izir | belgesine | e sahipti | r. | | | | | aleres 1 | <i>He</i> | 190000 1965- | falanan) |
| Isibudit white the star | Suvey a Nerve OFAL | | | | -17 | | | | ZE VE Ban | MTES LABOR Melikg | T ZEN | IN ARAŞT A HIZMET L G HIX Melikgazi 997 070 850 420630646000 | IRMA ID. ŞTİ KAYSER | - | | | | | | | | | |

| | n) | | | | | 1 | n) | HİZ. | MÜH Çakma | . MAL | 0. SAN | . VE T | ORATU ic. LTD Karatay / Ki | . ŞTİ. | | | | CEVICE V | E SEHIRCELIK BAKANLIĞI | | - | - |
|----|----|---------------------------|--------------------------------|-----------------|---|---|-----------------------------------|------------------------------------|--|----------------------------|---------------|---------------|----------------------------------|-------------------------------|-------------------------|----------------------------------|-----------------------------|----------|--|-------------------------|---|---|
| ς. | | YAPI E BAŞVU YAPI S | SİLGİLE RU SAHİ | Rİ İBİ | HAKAN MÜ MUSA AYGÜ SARIKÖPRÜ | N | RKEZ / NIC | SDE | | | | | | | | Deney Ba Kayıt Nu Rapor Ta | marsı arihi | | 14.06.2017 14.06.2017 K17-1380-Z 16.06.2017 | 2 | | |
| | | PAFTA | ADA/PA | RSEL | 3195 ADA / TOP | 1 PARSEL | IEY SC | NUÇL/ | ARIR | APOP | U | | | | | Rapor No Bakanlık | | | R17-1380-Z 12774201 | | | |
| | | | Numune | | Doğal Su | Doğal Birim | Elek | Analizi | Atte | rberg Lin | nitleri | | Nokta | Üç Ek Basınç | | Konsol | idasyon | | Direkt Kesn | me Deneyi | | |
| | | Sondaj Kuyusu Adı | Tipi ve Adı | Derinlik | Muhtevası (%) | Hacim Ağırlık (gr/cm ³) | #10 Kalan (%) | #200 Geçen (%) | LL (%) | PL (%) | PI (%) | USCS | Dayanımı (kgf/cm2) | * c _{up} (kg/cm²) | *f _{up} (°) | Şişme Yüzdesi (%) | Şişme Basıncı (kN/m²) | Gs | * c _{up} (kg/cm ²) | *f _{up} (°) | | |
| | | SK-1 | UD | 1.00-1.50 | 27,61 | 1,88 | 0,00 | 92,89 | 51 | 26 | 25 | CH | | | | | | | 0,6630 | 6,2 | | |
| | | SK-1 | | 3.50-3.95 | | 1,87 | 0,00 | 39,79 | | NP | | SM | | | | | | | | | | |
| | | SK-1 | | 5.00-6.00 | | | | | | | | | 10,47 | | | | | | 0,6718 | 6,2 | | |
| | | SK-2 | | 1.00-1.50 | 27,35 | 1,88 | 0,00 | 93,24 | 51 | 28 | 23 | CH | 11,52 | | | | | | 0,6/18 | 0,2 | | |
| | | SK-2 | KAROT | 5.00-6.00 | | | | | | | | | 11,52 | | | | | | | | | |
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| | | Not ve Act | | TS - 1900-1 , 7 | rs - 1900-2 ve 7 | 'S 1500 | | | | | | | | | | | | | | | | |
| | | * Laboratu * Bu rapor, | varuniz Çevre , sadece dene | MERM | akanlığının 11.0 ne için geçerlidir İ YAPAN ET ESE AL MÜİ | . Numunenin al | e 273 sayılı"L lındığı yere ai | aboratuvar İzi it bilgiler möşt | n Belgess ^w r eriye ait ol | e sahiptir. up, laboran | varımızın izi | ai olmaksızın | değiştirilemez v | e kısmen çoğa | B Je | BORATUVA EKİR Oloji Y | AKARS | U üh. | fikir vermez. | | | |

| | N | | | | | SOND | AJ | LOGU | Sondaj N | 0/Bori | ng No | ; | S | K-1 |
|--|------------------------|---------|---------|---------------|-----------------|---|--|---|--|--------------------------|-----------------------|--|---|----------------------|
| SKAN MÜHE | NDISU | HA | VKA | M | | BORE | 101 | E LOG | Sayfa No | D/Sheet | No | ; | | 1/1 |
| 100 | MU | ME | ND | ÍSL | 1er | | | | Sondör / | Contractor of | - | ; | J. M.S. | Ferhat |
| Proje Adı/P | roject N | ame | | | : | Niğde İli, Merkez İlce, | Sarıkö | prü Mahallesi, 3195 Ad | - | - | - | | DAĞO | GLU |
| Sondaj Yer | Boring | Loca | tion | | : | 3195 Ada, 1 Parsel | | Koordinat / Coordinate X | | | [| | | |
| Sondaj Der | inliği/£ | Boring | Dep | th (m |): | 10.00 Metre | | Koordinat / Coordinate Y | (N) | | | | | |
| Başlama Ta | | - | | te | : | - | | Sondaj Kotu/Elevation (r | n) | | | | | |
| Bitiş Tarihi | / Finis | h Da | ate | | : | - | - | Yeraltısuyu Der/Ground | lwater D. | | 1.30 | m | | |
| 0 | Der. h(m) | | STA | | | ENETRASYON DENEY | iji Alo | | | ¥ | B | | | |
| ik ne No | Ine De Depth(m) | | be Sa | ayısı | | 1 | Zemin Sınıfı Soil Catogory | ZEMİN TANIMLAMASI | PROFIL | Dayanımlılık Strength | Ayrışma Weathering | Kirik Fracture | TCR % | % Q |
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| 2 SPT-1 | | 2 | 2 | 3. | 5 | | Ե | Yüksek Pilastisiteli | | | L. | | T | |
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| 20 KIVAN | 1 DURU | MU/S | CIFFN | ESS | | SIKILIK / DENSTY | 4 | ORANLAR / PROPORT | TON | - | AÇIKL | AMAI | AR / EX | CPL. |
| N = 0-2 N = 3-4 | Çok yu Yumuşı | | | V.soft | | N=0-4 Cok gevşek/V.loose N= 5-10 Gevşek/Leose | 96 | 00-10 Pek Az / Slight(trace) 10-20 Az / Little | | | | | | s.Sample b.Sample |
| N = 5 - 8 N = 9 - 15 | Orta ka Katı | | ' | M.St Stiff | iff | N =11-30 Orta sıkı M.loose N =31-50 Sıkı/Dense - | 96 | 20-35 Sıfat / Adjective 35-50 Ve / And | | SPT: S | tandart] | Penetr. | Testi / SP | T Test |
| N = 16-30 N > 30 | Çok ka Sert | tı | | V.sti Hard | ff | N>50 Çok Sıkı/V.Dense | 1 | | | | | | / Core Sa | |
| AYR | IŞMA/W | EATI | IERI | | - | DAYANIMLILIK/STRENG | the second second second second second second second second second second second second second second second s | KIRIKLAR/ FRACTU | the second second second second second second second second second second second second second second second s | _ | - | Contraction of the local division of the loc | and the second se | MI/RQD |
| W1 Taze/F W2 Az Ayn | resh şmuş / Sliş | ghtly V | v. | | | I Çok Zayıf / Very Weak II Zayıf / Weak | < 2- | | W M | % 0-25 %25-50 | | | Kôtů / V 1 / Pour | ery Poor |
| W3 Orta D. | Ayrışmış rışmış / H | / Mod | areatly | W. | | III Orta Zayıf / Moderatly Weak IV Orta Dayanımlı/ Moderatly S | | 10 Sik / Close(Cl) 1-20 Colc Siki / Intense(I) | Cl I | %50-73 %75-9 | | | / Fair Good | Rin |
| W5 Tamama | en Ayrış A | Compl | ctely V | | | V Dayanımlı / Strong | | 20 Parçalı / Crushed(Cr) | Cr ONAY / / | \$690-1 | 00 | - | lyi / Exc | ollent |
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| üklenici | Firma | | ADER MU | HENDIS | LÍK | | | 10 | | | | | | | | | Sayfa N | 0 | | | 1/1 | | |
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| roje Adı | 1 | | NIĞDE ILI | MRKZ IL | C.SARIK | ÖPRÜ N | IH. 3195 A | DA 2 PAR | SEL | | | | | | | | Numun | e Geliş Tar | rihi | | 26.04.2 | 017 | |
| apor No | 0 | | 2983-17 | | | | | | | | | | | | | | Rapor T | arihi | | | 02.05.2 | 017 | |
| | | | 1 | | | | | | | | | | | | | | Bakanlı | k Rapor N | 0 | | 124668 | 77 | |
| | | | Doğal Su | 1 | | | | | Zemin | | Ort.Dbha | Serbest Basing | Oc Ekse | nli (UU) | Hidro | metre | Rha | Brok | lder | | Direkt | Kesme | |
| Sondaj | | Numune | İçeriği | Atte | rborg Lin | nitieri | Elek | Analizi | Sinfi | Ort.Is (50) | Ort.Dbha | Deneyi(qu) | /(0 | U) | -0,075 | -0,002 | ai | | | | Özgül | c | \$ |
| Kuyu No: | Tipl ve Adı | Derintik (m-m) | (%) | LL (%) | PL (%) | PI (%) | +4 Kalan (%) | - 200 Geçen (%) | USCS | (Kg/em2) | Yn (gr/cm²) | kg/cm2 | C Kgflcm2 | ф Derece | % | % | (g/cm²) | Wopt (%) | Ykmax (g/cm³) | % | ağırlık | Kohezyon Kgf/cm2 | sürtünm acisi |
| SK-1 | UD | 1,50-2,00 | 18,1 | NP | NP | NP | 25,60 | 47,60 | 1 SC | - | 1,75 | - | - | - | - | - | - | - | - | - | - | 0,156 | 21 |
| SK-1 | SPT | 3,00-3,45 | 20,5 | NP | NP | NP | 33,40 | 39,70 | 1 SC | - | 1,77 | - | - | - | - | - | - | - | - | - | - | - | - |
| SK-1 | CR | 4,50-5,00 | - | - | - | - | - | - | - | 8,2 | 2,19 | - | - | - | - | - | | - | - | | - | - | - |
| SK-2 | UD | 1,50-2,00 | 17,2 | NP | NP | NP | 23,90 | 45,10 | SC | 100 | 1,74 | - 1 | | - 1 | - | - | - | | - | - | - | 0,169 | 21 |
| SK-3 | UD | 1,50-2,00 | 19.7 | NP | NP | NP | 19,90 | 46,70 | SC | | 1,72 | _ | | | - | - | | - | - | - | | 0,174 | 22 |

Kowall Office Molecter (Ville) Beller No:19652

*Bu deney formu izinsiz hiçbir şekilde çoğaltılıp kopya edilemez.

*Söz konusu deney sonuçları,sadece test edilen deney numunelerine aittir

*Tüm hakları Zemtest Zemin Araştırma ve Lab.Hiz Ltd. Ştl.'ye aittir.

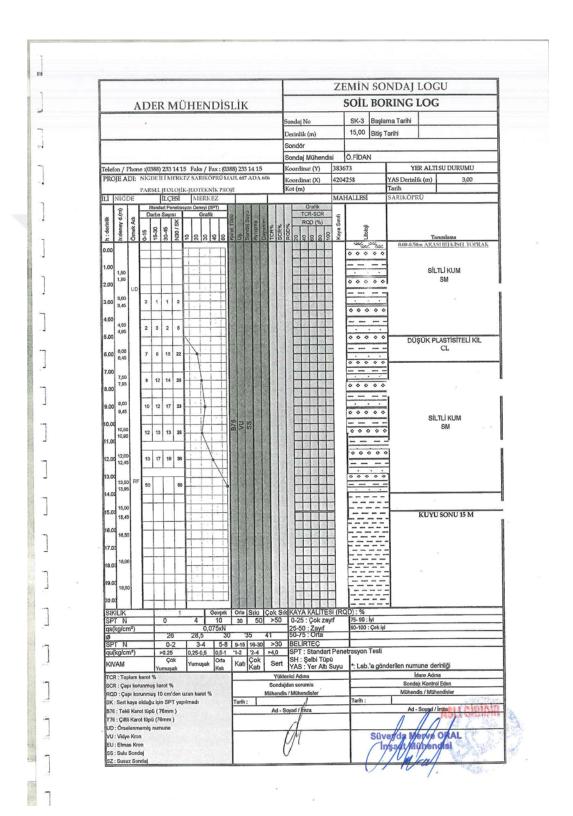
* Laboratuvarımız 4708 sayılı kanun gereği T.C.Çevre ve Şehircilik Bak. tarafından verilen 02.03.016 tarih ve 539 No'lu laboratuvar izin belgesine sahiptir.

-Deneyi Yapan -Serhat DAVSAL (jeo Müh) Oda Sicil No. 14982-----

ZEMTEST ZEMIN ARAŞTIRMA VE LABORATUYAR HIZMET LTD, ŞTİ. Melikgazi Mir Aşıkveysel Bulvarı Banş Manço Konağı No' 4/A Melikgazi/KAYSERİ Erciyas V.D./997 070 8501 Mersis No: 0142063064600013

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| | | | | 1 | ABOR | ATUV | | ENEY | LERIT | OPLU SOI | JUC R | APO | R FO | RMU | | | | _ | | | | | | | | | |
| | ADER MU | HEND | SLİK | | 1001 | | | ball then I | | 0. 20 00. | 10 ý 10 | | | | Sayfa N | 0 | | | 1/1 | | | | | | | | |
| | NIĞDE ILI | MRKZ. | ILÇ.SAR | KÖPRÜ N | AH. 687 A | DA 606 PA | ARSEL | | | | | | | | Numun | e Geliş Ta | rihi | | 27.02.2 | 017 | | | | | | | |
| | 2362-17 | | | | | | | | ÷ | | | | | | Rapor T | arihi | | | 20.03.2 | :017 | | | | | | | |
| | 1 | | | | | | | | | | | | | | Bakanlı | k Rapor M | No | | 121914 | 41 | | | | | | | |
| Mumauna | Doğal Su | | terberg Li | mitteri | Flak | Apalial | Zemin | | Ort Dhha | Serbest Basing | Og Ekser | nii (UU) | Konso | lidasyon | Rha | Pro | ktor | CBR | | Direkt | Kesme | | | | | | |
| rtuntune | İçeriği | 1 ~ | converg as | | | | Siniti | Ort.Is (50) | | Deneyi(qu) | /(C | 0) | şişme | şişme bas | | | | 2.5 mm | Özgül | c | • | | | | | | |
| e Derinlik (m-m) | (%) | LL (%) |) PL (%) | PI (%) | +4 Kalan (%) | Geçen | USCS | (Kg/cm2) | Yn (gr/cm*) | kg/cm2 | C Kgf/cm2 | ф Derece | % | | (g/cm³) | Wopt (%) | Ykmax (g/cm³) | % | agaan | Kohezyon Kgf/cm2 | lçsel sürtünme ncisi | | | | | | |
| 3,00-3,50 | 20,1 | | | | 0,00 | 30,10 | SM | - | 1,69 | - | - | - | - | - | - | - | - | - | - | 0,225 | 19 | | | | | | |
| 4,50-4,95 | | | | | | | | - | 1,68 | | - | - | - | | - | | - | - | - | - | - | | | | | | |
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| | YAPI BİLGİ BAŞVURU SA YAPI SAHİBİ YAPININ AD PAFTA/ADA/ | LERÍ HİBİ RESİ | HAKAN MÜH ER-NA İNŞA ESKİSARAY 3475 ADA / | AT MAH. / MER | | | | ABO | 211 | | | | | Numune Deney Ba Kayıt Nu Rapor Ta Rapor Nu Bakanlık | nş. Tarihi marsı urihi umarası | | 28.02.201 28.02.201 K18-331-Z 28.02.201 R18-331-Z 14411972 | 8 | | | |
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| | Numun | e | - | Doğal Birim | Elek | Analizi | Atte | rberg Lin | nitleri | | Nokta | Üç Eks Basınç | | Konsoli | idasyon | | Direkt Kesn | e Deneyi |
| Sondaj Kuyusu Adı | | Derinlik | Doğal Su Muhtevası (%) | Hacim Ağırlık (gr/cm ³) | #4 Kalan (%) | #200 Geçen (%) | LL (%) | PL (%) | . PI (%) | USCS | Yükleme Dayanımı (kgf/cm2) | * c _{up} (kgf/cm ²) | *f _{up} (*) | Şişme Yüzdesi (%) | Şişme Basıncı (kN/m ²) | Gs | * c _{up} (kgf/cm ²) | *f _{up} (°) |
| SK-1 | UD | 0.50-1.00 | 2,37 | 1,81 | 18,44 | 10,85 | | NP | | SM | | | | | | | 0,0488 | 31,7 |
| SK-1 | SPT | 1.50-1.95 | | 1,82 | 17,96 | 13,48 | 1. | NP | | SM | | | | | | | | 22.2 |
| SK-2 | UD | 0.50-1.00 | | 1,81 | 15,30 | 12,11 | | NP | | SM | | | | | | | 0,0635 | 32,3 |
| SK-2 | SPT | 4.50-4.95 | | 1,81 | 19,30 | 11,96 | | NP | | SM | | | | | | | 0.0550 | 31,9 |
| SK-3 | UD | 0.50-1.00 | 3,76 | 1,80 | 18,05 | 10,30 | | NP | | SM | | | | | | | 0,0560 | 51,9 |
| SK-3 | SPT | 9.00-9.45 | 2,05 | 1,81 | 17,43 | 12,28 | | NP | | SM | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | cikiamalar: | | | | | | l | | | | | | | | | | | |
| | uvarimiz Çevr r, sadece dene | e ve Şehircilik B yi yapılan numu | s - 1900-2 ve TS alcanlığının 11.0 ne için geçerlidir YAPAN GAN ahendisi | 4.2011 tarih ve . Numunenin al | 273 sayılı"Lı ındığı yere ail | aboratuvar İzir t bilgiler müşte | a Belgesi"ne riye ait olu | e sahiptir. ıp, laboratu | varımızın İzn | i olmaksızın | değiştirilemez ve | re kısmen çoğalt | Bel | tin givenilirligi BORATUVA (ÎP-APA Gloji / Uk. tçî Belge N | ARSU | | fikir vermez. | |
| 3 | | A 09 8 3 10 | | | € nat | ÷ | | | | | | 1 | | | | | | |

| Sondaj Kuyusu Adı Tipl ve Adı Doğal Su Multevası (%) Birim Hacim (%) Mathewasi Hacim (%) Mathewasi Hacim (%) Mathewasi Hacim (%) Mathewasi (%) Mathewas | 3-Z 116 3-Z 8 esme Den *fu (*) 29, |
|--|---|
| YAPININ ADRESI PAFTA/ADA/PARSEL KIRBAĞLARI MAH. / MERKEZ / NİĞDE 1797 ADA / 7 PARSEL 1797 ADA / 7 PARSEL TOPLU DENEY SONUÇLARI RAPORU Numune Doğal Su Adı Doğal Su (%) Doğal Su (%) Doğal Su (%) Doğal Su (%) Elek Analizi Atterberg Limitleri (%) Nokta (%) Nokta Yükleme Dayanımı (kgf/cm2) Šişme (kgf/cm2) Şişme Sişme (kgf/cm2) Şişme Sişme (kgf/cm2) Sişme Sişme (kgf/cm2) Sişme Sişme (kgf/cm2) Sişme Sişme (kgf/cm2) Sişme Sişme (kgf/cm2) Sişme Sişme (kgf/cm2) Sişme Sişme Sişme (kgf/cm2) Sişme Sişme (kgf/cm2) Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Doğal Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme Sişme <th>116 3-Z 8 esme Den *f_u (*) (*) 29,</th> | 116 3-Z 8 esme Den *f _u (*) (*) 29, |
| Namue Doğal Su Multiveration Doğal Su Multiveration Doğal Su Multiveration Elek Analizi (%) Atterberg Limitleri< (%) USCS Nokta Yüklem Dayanımı (kgf/cm²) Üç Eksen!! Basınç (UU) Konsolidasyon (%) Ge (%) Direkt (kgf/cm²) Sister Doğal Su Multiveration Multiveration (%) Atterberg Limitleri (%) USCS Nokta Yüklem Dayanımı (kgf/cm²) Üç Eksen!! (%) Konsolidasyon (%) Ge Direkt Sister Doğal Su Multiveration Multiveration (%) Atterberg Limitleri (%) USCS Nokta Yüklem Dayanımı (kgf/cm²) Öç Eksen!! (%) Konsolidasyon (%) Ge Direkt Six-1 UD 0.50-1.00 2,61 1,79 2,81 5,98 NP SM 0,085 SK-1 SPT 4.50-4.95 3,35 1,81 4,63 7,79 NP SM 0,085 SK-2 UD 0.50-1.00 2,89 1,80 3,78 7,20 NP SM 0,085 SK-2 UD 0. | 3-Z 8 esme Den *f" (*) (*) 29, |
| Numune Doğal Sirini Elek Analizi Atterberg Limitleri USC Notta Yükleme Tüyletem Sondaj vikleme Tüyletem < | 8 esme Den *f., (°) 29, |
| Numume Doğal Su Doğal Su Birin Elek Analizi Atterberg Limitleri USCS Notta Basinc (UU) Konsolidasyon Ge Direktive Sondaj Adi Tipi ve Adi Derinlik Değal Su Hacim (%) #4 #200 LL PL PJ Witkleme Dayanımi % Sişme | esme Den *fu (°) 29, |
| Sondaj Ruyusu Adi Tipi ve Adi Adi Derinlik Multevasi (%) Doğal Su Multevasi (%) Birim Hacim (%) Birim Hacim (%) Basinç (UU) Konsolidasyon Ge Direkt (%) 5K-1 UD 0.50-1.00 2,61 1,79 2,81 5,98 NP SM - - 0,085 0,085 SK-1 SPT 4,50-4.95 3,35 1,81 4,63 7,79 NP SM - - 0,085 SK-2 UD 0.50-1.00 2,89 1,80 3,78 7,20 NP SM - - - 0,085 SK-2 UD 0.50-1.00 2,89 1,80 3,78 7,20 NP SM - - 0,089 SK-2 SPT 6.00-6.45 4,51 1,80 3,78 7,20 NP SM - - - 0,089 SK-2 SPT 6.00-6.45 4,51 1,80 2,55 6,75 NP SM - - <t< td=""><td>*f_m (°) 29,</td></t<> | *f _m (°) 29, |
| Sondaj Adi Adi Adi Tipl ve Adi (%) Derinlik (%) Muttevasi (%) #4 Raian (gr/cm ³) #200 (%) LL (%) PI (%) USCS Tayaning (kgf/cm ²) *5 (%) \$15me (%) < | 5) (°) 29, |
| SK-1 SPT 4.50-4.95 3.35 1.81 4.63 7.79 NP SM Image: Constraint of the second seco | |
| SK-2 UD 0.50-1.00 2,89 1,80 3,78 7,20 NP SM 0,089 SK-2 SPT 6.00-6.45 4,51 1,80 2,55 6,75 NP SM 1 | 30, |
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| Not ve Acudamalar: * Kullanian Standartiar: TS - 1900-2 ve TS 1500 | |
| * Kullanian Standartiar: TS - 1900-1 , TS - 1900-2 ve TS 1500 | |
| * Kullanılan Standartlar: TS - 1900-1, TS - 1900-2 ve TS 1500 | |
| * Kullanılan Standartlar: TS - 1900-2 ve TS 1500 | |
| * Kullanılan Standartlar: TS - 1900-1, TS - 1900-2 ve TS 1500 | |
| Laboratuvarımız Çevre ve Şehircilik Bakanlığının 11.04.2011 tarih ve 273 sayılı"Laboratuvar İzin Belgesi"ne sahiptir. Bu rapor, sadcce deneyi yapılan numure için geçeridir. Numunenin alındığı yere ait bilgiler müşteriye ait olup, laboratuvarımızın izni olmaksızın değiştirilemez ve kısmen çoğalılamaz. Yapının güvenilirliğine yönelik tek başana bir fikir vermez. LABORATUVAR DENETÇİSİ IBCLET ABAN Jecloji Mühendişi | |

| (| Contraction of the second | | | | Ad | res:Sah | abive M | ah.Otak | (Sk.No: | :39/a Ko | ocasina | NKAYS | .LTD.ŞTİ. ERİ 1.com.tr | ÷ | | | | CEV | | ENIROLUS AKANLISI |
|-------------------|---------------------------|-----------------------------------|-----------------|------------------------------|---------------------------------------|-----------|------------|-------------|--|----------------------------|-------------------------|---|--|-------------------------------------|------------------|-------------------------|--------------|------------------|--|----------------------|
| Yü | klenici fi | rma : | DAĞOĞL | | IENDÍS | LİK | | | | | | | | | | | | | | Sayfa No: |
| P | roje | : | NİĞDE İI | İ MERK | KEZ İLÇ | | | | | 2456 A | DA 5 P | ARSEL | Bakanlık | No : | | | | | | 1/1 |
| | apor Tari | | 31.12.201 | | ncim 13) | EL | ek Lizi | AT | 2-1401 TARBER IMITLER ERBERG LU | 2Î | CMA | (cm ²) | | Üç Ek Basınç TRIA COMPRESS | Deneyi | Kesmel Den DIRECT | eyi SHEAR | Konsol (CONSO | Idasyon LIDATOIN) | FIRE |
| f Cipi Cype | Sondaj No: Boring No: | c(Samp Derinlik Depth(n | e No : e No: | Doğal Su İçeriği: (Wn)(%) | Doğal Birim Hacim Ağırlık (gr/cm3) | (SIEVE A) | -200" | LL (%) | PL (%) | РІ (%) | SINIFLANDIRMA (USCS) | NOKTA YÜKLEME İNDEKSİ (kg/cm²) | Serbest Basınç Deneyi(qu) (kgf/cm ²) | C Kgf/cm ² | D erece | C Kgf/cm² | Ф Derece | Şişme Basıncı | Şişme Yüzdesi(%) | HIDROMETRE |
| CR | ഗ് ല SK-1 | ತ,00 | N-1 | | 1,92 | - | - | - | - | - | | 6,2 | - | - | - | - | - | - | - | |
| | SK-2 | 3,00 | | - | 1,86 | | | - | - | - | - | 7,3 | - | - | | - | - | - | - | - |
| CR | SK-2 | 3.00 | | | 1,98 | - | - | - | - | - | - | 8,7 | - | - | - | - | - | - | - | - |
| | DENE | vi YAPA î.Scrhat C.No.14982 | DAYSAI | | 1 | | Soz ko | onusu deney | 4708 sayılı | sadece test kanun gerej | gi Çevre ve | y numunelet Sehicilik B Japóratuvar I KADENCI H. MIM, MM TD STI. Catirk Is Mere J 222 6f 53 J 222 f 53 J 222 f 53 J 222 f 53 J 222 f 53 J 225 J 25 J 225 f 53 J 25 | akaningi Tapi | İşleri Genel M sahiptir | نتر Aodarlaga | | Abdulk | adir B | <u>YLAYA</u> ULDU Mulh. 5:15693 | |

| | | HİZ | DNEVÎ YAF . MÜH. Ma zi Çakmak Ma Tel/Fa | AD. SAN | . VE T | İC. LTD. Karatay / Kü | ŞTİ. | | L | L | ÇE | VRE VE SEMIRCILI BAKANLA | 2. XX | | |
|--|---|---|--|--------------------------|---------------|----------------------------------|-------------------------------|-------------------------|----------------------------------|-----------------------------|-----------|-------------------------------|-------------------------|---|-----|
| YAPI BİLGİLERİ | | • | | | | | | | Numune | | hi | 19.09.2017 | | | |
| BASVURU SAHİBİ | HAKAN MÜHENDİSLİK | | | | | | | | Deney Ba | | | 19.09.2017 | | | |
| YAPI SAHİBİ | NARGÜL İNŞ. LTD. ŞTİ | | | | | | | | Kayıt Nur | | | K17-2090-2 | | | |
| YAPININ ADRESI | KIRBAĞLARI MAH. / M | ERKEZ / NÍĞDE | | | | | | | Rapor Ta | | | 20.09.2017 R17-2090-2 | | | |
| PAFTA/ADA/PARSEL | 55 ADA / 256 PARSEL | | | | | | | | Rapor Nu | | | 13357046 | | | |
| | TOPLU DE | NEY SONUÇI | ARI RAPO | DRU | | | | | Bakanlık | кар. No | | 13337040 | | 1 | |
| Numune | Doğal | Elek Analizi | Atterberg | Limitleri | | Nokta | Üç Eks Basınç | | Konsoli | dasyon | | Direkt Kess | ne Deneyi | | |
| Sondaj Kuyusu Adı Adı Derinlik | Doğal Su Muhtevası (%) Ağırlık (gr/cm ³) | #10 #200 Kalan Geçen (%) (%) | LL P (%) (% | | USCS | Yükleme Dayanımı (kgf/cm2) | * c _{up} (kg/cm²) | *f _{up} (°) | Şişme Yüzdesi (%) | Şişme Basıncı (kN/m²) | Gs | * C _{ep} (kg/cm²) | *f _{up} (*) | | |
| SK-1 UD 1.50-2.0 | 3,62 1,83 | 30,38 21,91 | | | SM | | | | | | | 0,0754 | 29,7 | | |
| SK-1 SPT 3.00-3.4 | | 28,56 22,08 | | | SM | | | | | | | 0,0763 - | 30 | | |
| SK-2 UD 1.50-2.0 | | 25,74 23,29 | | | SM | | | | | | | 0,0703 | | | |
| SK-2 SPT 9.00-9.4 | 5 3,06 1,84 | 26,62 22,09 | NF | , | SM | | | | | | | | | | |
| | | <u> </u> | | | | | | | | | | | | | |
| | | | | | - | | | 1 | | | | | | | - |
| Not ve Acıklamaları * Kullanılan Standartlar: TS - 1900-1 * Laboratuvarımız Çevre ve Şehircilik * Bu rapor, sadece deneyi yapılan nun | Bakanlığının 11.04.2011 tarih une için geçerlidir. Numunenin | ve 273 sayılı"Laboratuvar alındığı yere ait bilgiler m | İzin Belgesi"ne sahip İşteriye ait olup, labo | tir. watuvarumizin iz | ni olmaksızın | değiştirilemez v | e lasmen çoğal | tılamaz.Yaj | punin güvenilirliği BORATUVAI | ne yönelik tek | başma bir | fikir vermez. | | | |
| DENE | VI VAPAN | | | | | | | | FKTRA | VADC | | | | | 100 |

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BEKIR AKARSU Jeoloji Yük, Müh. Deneter Dene No:10360

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| | MEKAN | NIĞI LABO | RATUVA | RI | | ^ | ZEMTES DRES:ME | T ZEMİ | İ MH.AŞIK \ TEL | VEYSEL BI L :0352 33 | ABORATUVAR UL.BARIŞMANG 33 55 44 MTEST.COM | HİZMET L ÇO KONA | ĞI NO | r <u>i.</u> :4/A | | | | T. Ç | C. EVRE V AKANL | /E ŞE | IRCILIK | |
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| | | | | | | ABOR | | | | ERI TO | PLU SON | UC RA | APO | R FO | RMU | | | | | | | |
| üklenici | Firma | | ADER MÜ | HENDÍSI | | | 1017 | | | -11110 | 1 20 0011 | ¢ÿiu | | | | Sayfa N | lo | | | 1/1 | | |
| roje Ad | | | | | .Ç. KIRBAĞLA | RI MH. 1764 | ADA 3 PA | RSEL | | | | | | | | Numun | e Geliş T | arihi | | 25.09.2 | 017 | |
| apor No | | | 5348-17 | | | | | | | | | | | | | Rapor | | | | 29.09.2 | | |
| | | | | | | | | | | | | | | | | Bakanlı | k Rapor | No | | 139266 | | |
| Sondaj | N | umune | Doğal Su | Atto | rberg Limitleri | Flek | Analizi | Zemin | | Ort.Dbha | Serbest Basing | Ug Ekser | nti (UU) | | ometre | Bha | P | roktor | CBR | - | | Kesme |
| Connag | N | | İçeriği | | | | | Sinifi | Ort.Is (50) | | Deneyi(qu) | /(C | | -0,075 | -0,002 | | | | 2.5 mm | Özgül ağırlık | c | φ içsel |
| Kuyu No: | Tipi ve Adı | Derinlik (m-m) | (%) | LL (%) | PL (%) PI (| () Kalan | - 200 Geçen | USCS | (Kg/cm2) | Yn (gr/om ³) | kg/cm2 | C Kgf/cm2 | ф Derect | % | % | (g/cm ³) | Wopt (% |) Ykmax (g/cm ³) | % | | Kohezyon Kgf/cm2 | sürtünme açısı |
| SK-1 | UD | 1,50-2,00 | 2.6 | NP | NP N | 0,00 | 35,50 | SM | | 1,70 | - | - | - | - | 1 1 | - | - | - | - 1 | - | 0,224 | 22 |
| SK-1 SK-2 | UD | 1,50-2,00 | 6,5 | NP | NP N | | 33,60 | | - | 1,72 | - | - | - | - | - | 141 | - | - | | - | 0,236 | 22 |
| | | | | | | | | | | | ı laboratuvar izi | il beigesiii | C Jurn | | | | | | | | | |

| ZEMITEST | ZEMTEST ZEMİN ARAŞTIRMA VE LABORATUVAR HİZMET LTD STİ. ADRES:MELİKGAZİ MH.AŞIK VEYSEL BUL.BARIŞMANÇO KONAĞI NO:4/A TEL :0352 333 55 44 MAİL:İNFO@ZEMTEST.COM | T.C. ÇEVRE VE SEHİRCİLİK BAKANLIĞI |
|----------------------------------|---|--|
| | ABORATUVAR DENEYLERİ TOPLU SONUÇ RAPOR FORML | J |
| Yüklenici Firma ADER MÜHENDİSLİK | | Sayfa No 1/1 |

| Yüklenici | Firma | | ADER MÜ | HENDIS | LĨK | | 2000 | | | | | | | | | | Sayfa N | 0 | | | 1/1 | | |
|-------------|----------|-----------------------|---------------|-----------|-----------|---------|--------------------|----------------|-------|-------------|----------------|----------------|-----------|-------------|--------|--------|---------|------------|------------------|--------|---------|---------------------|----------------------------|
| Proje Adı | | | NIĞDE ILI I | MRKZ. IL | C.KIRB/ | AĞLARIN | AH. 1813 | ADA 2 PAR | RSEL | | | | | | | | Numun | e Geliş Ta | rihi | | 21.09.2 | 017 | |
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| itapor ito | | | | | | | | | | | | | | | | | Bakanlı | k Rapor N | lo | | 133937 | | |
| | | | Doğul Su | | | | | | Zemin | | | Serbest Basing | Oc Ekse | nli (UU) | Hidro | metre | Bha | | ktor | CBR | | Direkt | Kesme |
| Sondaj | | Numune | İçeriği | Atte | rberg Lin | nttieri | Elek / | Analizi | Sinth | Ort.Is (50) | Ort.Dbha | Deneyi(qu) | 1(0 | U) | -0,075 | -0,002 | Bria | 1 10 | aor | 2.5 mm | | c | \$ |
| Kuyu No: | Tipl ve | Derinlik (m-m) | (%) | LL (%) | PL (%) | PI (%) | +4 Kalan (%) | - 200 Geçen | USCS | (Kg/em2) | Yn (gr/cm³) | kg/em2 | C Kgflem2 | ¢ Derece | 96 | % | (g/cm*) | Wopt (%) | Ykmax (g/cm³) | % | ağırlık | Kohezyon Kgf/cm2 | içsel sürtünme acisi |
| SK-1 | UD | 3,00-3,50 | 12.8 | NP | NP | NP | 0.00 | 28,80 | SM | - | 1,67 | - | | - | - | - | - | - | - | - | - | 0,221 | 21 |
| SK-2 | UD | 3,00-3,50 | 13,9 | NP | NP | NP | 0,00 | 31,40 | SM | - | 1,72 | - | - | - | - | - | - | - | - | - | - | 0,229 | 20 |
| | Yayın Ta | : 03.12.2015 Revi | izyon No/Ta | ar: 00 | | | | | | | | | | | | | | | | | | | |
| *Bu dene | y formu | izinsiz hiçbir şekile | de çoğaltılır | o kopya e | edileme | ez. | | | | | | | | | | | | | | | | | |

te çogaitilip kopya

*Söz konusu deney sonuçları,sadece test edilen deney numunclerine alttir

*Tüm hakları Zemtest Zemin Araştırma ve Lab.Hiz Ltd. Şti.'ye aittir.

* Laboratuvanımız 4708 sayılı kanun gereği T.C.Çevre ve Şehircilik Bak. tarafından verilen 02.03.016 tarih ve 539 No'lu laboratuvar izin belgesine sahiptir.

Deneyi Yapan Serhat DAY SAL (ico Muh) SICI

Barke No:19652



ZEMTEST ZEMIN ARAŞTIRMA VE LABORATUYAR HIZMET LTD. ŞTİ. Melikgazi Mir Aşıkveysel Bulvan Banş Manço Konağı No' 4/A Melikgazi/KAYSERİ Erciyes V.D./997 070 8501 Mersis No: 01/42063064600013

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| | | | | | ÷ | HİZ. | MÜH Çakma | MAD | . SAN | . VE T | ORATU C. LTD Caratay / KC | ŞTİ. | | | | ÇE | T. VRE VE SEMIRCIL BAKANLI | c. Ik Gi |
| 0 | | | boratuve | ari | | | | | | | | · | | Numune | Gelis Tari | ihi | 11.03.2017 | |
| YAPI I | BILGILE | RI | | | | | | | | | | | | Deney Ba | as. Tarihi | | 11.03.2017 | |
| | RU SAHİ | | HAKAN MÜH | | | | | | | | | | | Kayıt Nu | | | K17-453-Z | |
| YAPI S | | | ORHAN KUŞ | | | | | | | | | | | Rapor Ta | | | 13.03.2017 | |
| | IN ADRE | | KIRBAĞLAR | | RKEZ / NI | GDE | | | | | | | | Rapor Nu | | | R17-453-Z | |
| PAFTA | ADA/PA | RSEL | 1754 ADA / | 6 PARSEL | IEV SO | NUCLA | ARTR | APOR | 20 | | | | : | Bakanlık | | | 12151826 | |
| | Numune | | IOF | Doğal | | Analizi | I. | erberg Lin | | | Nokta | Üç Eks Basınç | | Konsoli | idasyon | | Direkt Kesm | ne Deneyi |
| Sondaj Kuyusu Adı | Tipi ve Adı | Derinlik | Doğal Su Muhtevası (%) | Birim Hacim Ağırlık (gr/cm ³) | #4 Kalan | #200 Geçen (%) | LL (%) | .PL (%) | . PI (%) | USCS | Yükleme Dayanımı (kgf/cm2) | * Cup | *fup (°) | Şişme Yüzdesi (%) | Şişme Basıncı (kN/m ²) | Gs | * c _{up} () (kgf/cm ²) | *f _{up} 0 |
| | | | | | (%) | 26,03 | | · NP | | SM | | | | | | | 0,1033 | 28 |
| SK-1 | UD | 1.00-1.50 | . 3,86 | 1,84 | 8,09 9,81 | 29,34 | | NP | | SM | | | | | | | | |
| SK-1 | SPT | 4.50-4.95 | 3,29 | 1,85 | 9,81 | 25,45 | | NP | | SM | | | | | | | 0,1015 | 28 |
| SK-2 | UD | 1.00-1.50 | -2,58 | 1,84 | 11,01 | 23,43 | | | | | | | | | | | | |
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* Bu rapor, sadece denoyi yapılan numune için geçerlidir. Numunenin almdığı yere ait bilgiler müşteriye ait olup, laboratuvarınızın izni olmaksızın değiştirilemez ve kısmen çoğaltılamaz. Yapının güvenilirligine yönelik tek başına bir fikir vermez. ABORATUVAR DENEYÎ YAPAN

Jmur DOĞAN

Bokir SKARSU Man laololi Yük. Denetçi Belgo No. 10300

| | A AR SUMPA | MEKANIGI LABORAT | | | | | | | | | | | | | | | | | | ÇEVRE | VE ŞI | T.C EHIRCILII AKANLIĞ | ŝ |
|--------------|----------------|---|-------------------------------|---------|-----------|--------------------|------------|----------|-------------|----------------|-------------------------|-----------------------------|-----------|-------------|--------|--------|---------|----------|---------------------|--------|----------|-----------------------------|----------------------------|
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| roje Ad | | | ADER MÜHEND NİĞDE İLİ MRKZ | | | | FORADA | O DADCEL | | | | | | | | | | k Rapor | No | | 85485 | | |
| Rapor No | | | ZO656-15 | ILÇ. AŞ | AGIKA | ABAŞI MH | 598 ADA 5 | U PARSEL | | | | | | | | | | tandarti | | | | 0 / TS 1900 | -1/2 |
| Rapor Ta | | | 26.06.2015 | | | | | | | | | | | | | | yfa N | | | | 1/1 | | |
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| Sonda) | ' | Numune | Doğat Su İçeriği | Atterb | berg Limi | čjeri E | ek Analizi | Sinifi | Ort.ls (50) | a | Konsol | lidasyon | /(CI | J) | -0,075 | -0,002 | Bha | Standart | Modifiye Proktor | 2.5 mm | Özgül | c | |
| Kuyu No: | Tipi ve Adı | Derinlik (m-m) | (%) | LL (%) | PL (%) | PI (%) Kala (%) | | USCS | (Kg/cm2) | Yn (gr/cm²) | Şişme Yüzdesi (%) | Sisme Basinci (kN/m2) | G Kgf/cm2 | ¢ Derece | . % | % (| y/cm") | % | g/cm² | % | ağırlık | Kohezyon Kgf/cm2 | içce) sürtünme actsi |
| SK-1 | UD | 2,00-2,50 | 7,3 | | | NP 36, | 0 8,20 | | - | 1,65 | - | - | - | - | | - | - | - | - | - | - | 0,285 | 14 |
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| Telefon / Fhone :(0388) 233 14 15 Faks / Fax : (0388) 23 PROJE ADI: NIĞDE ILI MERKEZ İLÇESİ, | 33 14 15 Koordinat (Y) Koordinat (X) | | | YER ALTI YAS Derinlik (m) | SU DURUMU YOK |
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1 ZEMTEST ZEMÍN ARASTIRMA VE LABORATUVAR HÍZMET LTD STÍ. ZEN 251 1 ADRES:MELİKGAZİ MH.ASIK VEYSEL BUL.BARISMANCO KONAĞI NO:4/A ZEMIN MEKANIĞI LABORATUVARI TEL :0352 333 55 44 MAIL:INFO@ZEMTEST.COM ÇEVRE VE ŞEHİRCİLİK BAKANLIĞİ < 9. LABORATUVAR DENEYLERI TOPLU SONUC RAPOR FORMU 1/1 Yüklenici Firma ADER MÜHENDİSLİK Sayfa No NIGDE MERKEZ AHIPAŞA MAH. 364 ADA 41 PARSEL Numune Geliş Tarihi 17.03.2016 Proje Adı Rapor Tarihi 21.03.2016 Rapor No 0040-16 Bakanlık Rapor No 10052649 Direkt Kesme Oç Eksenli (UU) / (CU) Hidrometre CBR Serbest Basing Deneyl(qu) Doğal Su İçeriği Zemin Sınıfı Ort.Dbha Bha Proktor Sonda] Numune Atterberg Limitleri Elek Analizi -0,075 -0,002 2.5 mm Özgül ф Ort.1s (50) c lçsel sürtünme - 20 Kohezyon Kgf/cm2 Tipl ve Adı Yn (gr/cm³) Ykmax (g/cm³) Kuyu No: Derintik USCS (Kg/om2) ф Derece 96 % PI (%) kg/em2 96 Wopt (%) (%) LL (%) PL (%) C Kgf/om2 (g/cm²) (%) Geçen (m-m) acisi SK-1 CR 2,50-3,00 8,7 2,18 ------SK-2 CR 3,50-3,00 9,3 2,20 -*R FR 19 Yayın Tar: 03.12.2015 Revizyon No/Tar: 00 *Bu deney formu izinsiz hiçbir şekilde çoğaltılıp kopya edilemez. *Söz konusu deney sonuçları, sadece test edilen deney numunelerine aittir *Tüm hakları Zemtest Zemin Araştırma ve Lab.Hiz Ltd. Şti.'ye alttir. * Laboratuvarımız 4708 sayılı kanun gereği T.C.Çevre ve Şehircilik Bak. tarafından verilen 02.03.016 tarih ve 539 No'lu laboratuvar izin belgesine sahiptir.

Deneyi Yapan Darsal Headrich)

ZEMTEST ZEMIN ARAŞTIRMA VE LABORATUYAR MIZMET LTD, STI. Melikyazi Mf/ Aşıkveysel Sulvan Baniş Manço Konağı VG 4/A Melikgazi/KAYSERI Ercivas X. D. 997 (270 8501 Mersis Ne: 01/2063064600013

| (| Carl Carl | | | | Aa | res:Sał | HENDİS nabiye M | lah.Otal | M. YAP | :39/a K | VE ZEN ocasina | n/KAYS | S.LTD.ŞTİ. SERİ n.com.tr | | | | | ÇE | | T.C. EHIROLLIK |
|-----------------------------|-----------------------------|----------------------|---------------------------|------------------------------|---------------------------------------|---------|------------------------|--|--|-----------|--|--|--|---|--------------------|------------------------|----------------|------------------|-----------------------|----------------------------|
| Yü | klenici fi | | ADER M | | | | | | | | | | | | | | | | | |
| P | roje | | NİĞDE İI | | Z. İLÇE | Sİ SAR | IKÖPRÍ | | | A 4 PA | RSEL | | | | | | | | | Sayfa No: 1/1 |
| | apor Tar | hi: 1 e(Sample | 8.03.20 | | lacim m3) | EL | EK LIZI NALYSIS) | AT | 4-2804 TARBER IMITLER ERBERG LI | ti is | RMA | (cm ²) | Bakanlık | No : Üç Ek Basınç TRIA COMPRESS | Deneyi | Kesme Der DIRECT | SHEAR | Konso (CONSO | lidasyon LIDATOIN) | ERE ER |
| Tipi Type | Sondaj No: Boring No: | Derinlik Depth(m) | Numune No : Sample No: | Doğal Su İçeriği: (Wn)(%) | Doğal Birim Hacim Ağırlık (gr/cm3) | +4" | -200" | LL (%) | PL (%) | РІ (%) | SINIFLANDIRMA (USCS) | NOKTA YÜKLEME İNDEKSİ (kg/cm²) | Serbest Basınç Deneyi(qu) (kgt/cm²) | C Kgf/cm ² | P Derece | C Kgf/cm² | D erece | Şişme Basıncı | Şişme Yüzdesi(%) | HIDROMETRE (HYDROMETER) |
| CR | SK-1 | 2,50-3,00 | N-1 | - | 1,99 | - | - | - | - | - | - | 8,6 | | - | - | - | - | - | - | - |
| CR | SK-2 | 2,50-3,00 | N-2 | - | 2,01 | - | - | - | - | - | | 9,2 | - | - | - | - | - | - | - | - |
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| and the state of the second | DENEI CONTINA SILVANA | t VAPAN Sethet D | AYSAL | - | | | | bilgileri Firm nusu deney ş tuvarımız 4' dan verilen (ge firmanın) | - | | tilen deney Cerro vo 8 I. No'lu Lah Into Terro Vo Orak Tak Orak Sk. As Tric J. Terro Vo Tric I. Terro Vo 8 No 9 No 9 No 9 No 9 No 9 No 9 No 9 No 9 | numunelerii ettiviik Ba ojaduvar Lis Mihlamaz Mihamaz | ne aittir. kanlığı Yapı İş in Belgesi'ne sı K. H. ezi | leri Genel M hiptir | adarlaga | | bdulk | | | <u>v</u> |

| | | | | | | HIZ. | MÜH Çakma | k Mah. : | D. SAN 10569 Sk | . VE TI | IC. LTD. Caratay / KC | . ști. | | | | ÇEVRE V | T.C. E SEHIRCILIK BAKANLIĞI | |
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| BASVU | RU SAHİ | Bİ | AKNUR MÜH | ENDÍSLÍK | | | | | | | | | | Deney Ba | | | 16.02.2013 | |
| YAPI S | AHİBİ | | GÖRKEMLÌ S | | | | | | | | | | | Kayıt Nu | | | K13-142-Z 20.02.2013 | |
| YAPINI | IN ADRE | | SARIKÖPRÜ | | RKEZ / NÍČ | 5DE | | | | | | | | Rapor Ta | | | | |
| PAFTA/ | ADA/PA | RSEL | 2202 ADA / | | | | | | | | | | | Rapor Nu | | | R13-142-Z | |
| | | | TOP | LU DEN | IEY SO | NUÇLA | ARI R | APOF | RU . | | | | | Bakanlık | Rap. No | | 3971132 | |
| — | Numune | - | Doğal Su | Doğal Birim | Elek | Analizi | Atte | rberg Lin | nitleri | | Serbest Basınç | Üç Eks Basınç | | Konsol | idasyon | | Direkt Kesr | ne Deneyi |
| Sondaj Kuyusu Adı | Tipi ve Adı | Derinlik | Muhtevası (%) | Hacim Ağırlık (gr/cm ³) | #4 Kalan (%) | #200 Geçen (%) | LL (%) | PL (%) | PI (%) | USCS | * q _u (kg/cm2) | * c _{up} (kg/cm²) | *f _{up} (°) | Şişme Yüzdesi (%) | Şişme Basıncı (kN/m²) | Gs | * C _{up} (kg/cm ²) | *f _{up} (°) |
| SK-1 | UD-1 | 3,50 | 23,24 | 1,93 | 7,26 | 66,47 | 40 | 22 | 18 | CL | | 0,64 | _3 | | | | | |
| SK-1 | SPT-1 | 3,00 | 2,01 | | 6,26 | 2,06 | | NP | | SW | | | | 8 | | | | |
| SK-2 | UD-1 | 3,50 | 22,69 | 1,92 | 6,49 | 68,40 | 39 | 20 | 19 | CL | | 0,65 | 3 | | | | 0.0000 | 15.00 |
| SK-2 | UD-2 | 6,00 | 9,78 | 1,88 | 6,45 | 7,35 | | NP | | SM | | | | | | | 0,0089 | 15,66 |
| SK-3 | UD-1 | 3,50 | 15,24 | 1,90 | 4,23 | 56,82 | 37 | 18 | 19 | CL | | 0,6 | 4 | | | | | |
| SK-4 | UD-1 | 3,50 | 17,94 | 1,91 | 2,14 | 65,32 | 38 | 17 | 21 | CL | | 0,66 | 3 | | | | | |
| SK-4 | SPT-1 | 3,00 | 2,06 | | 2,93 | 1,65 | | NP | | SW | | | | | | | | |
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Not ve Acıklamalar:

* Kullanılan Standartlar: TS - 1900-1 , TS - 1900-2 ve TS 1500

* Laboratuvarımız Çevre ve Şehircilik Bakanlığının 11.04.2011 tarih ve 273 sayılı"Laboratuvar İzin Belgesi"ne sahiptir.

* Bu rapor, sadece deneyi yapılan yerler için geçerlidir. Numunenin alındığı yere ait bilgiler müşteriye ait olup, laboratuvarımızın izni olmaksızın değiştirilemez ve kısmen çoğaltılamaz. Yapının güvenilirliğine yönelik tek başına bir fikir vermez. LABORATUVAR DENETÇİSİ

DENEYİ YAPAN

Ba Yok. Mah. Denetçi Belge No: 10360

| GEDIK M | VRE VE SEHIR BAKA | NLIGI | - | aboratuv | | 1 | Numaral | u 1.400 | ver fo | lzin Be | elgesi"r | nuau ie Sah | iptir. | larafu | idan Ve | erilen 1 | 12 | 7 | | 8 | edik |
|--------------------|--------------------------------|--|---------------------------|-------------------------|--------------------|------------------|---------------|-----------------|----------------|--------------|--|----------------|------------|--------|--------------------|------------|--------------------|--------------------------|------------------------------------|----------------------------|-----------------|
| STI. 284/ IZMIR | 1 SOKAK NO 462534 10:1/5 | TLERI TIC. LTD. 6/B BORNOVA TEL: | | - | | | | Y SON GE | UÇLAR DİK F | RI ÖZ ORM | ET TA :19 | BLO. | SU | | | | | Rev. no Rev. To | rihi : 10 .su : 01 rihi : 01 | .01.2009 | |
| PROJE A | | 2589 | PA | AHIP. FTA | 4ŞA MA 20L 11-2 | H. YEN OL III | ÎÇARȘI PAR | ÎŞ MERK ISEL | EZÌ NO. | 206 NI | ĞDE TA | RÍH | 30,0 | 1,2015 | RAPO | R NO : | | Sayfa n | o.su : 1/1 723246/2 | 1 2015/238/ ENDÌSLÌI | TRIYAS K |
| KUTUNO | ÓRNEK NO | DERINLIK | su trendo | NOKTA YÜKLEME DENETİ | tei ter vivi in | TITINA WAT | ATTE | ERBERG LIMI | TLERI | XTRUŞV 10500 | TEK EKSEVILI BASDAÇ DENETÎ (Aş(caz) | В | H.A (Gr/ci | m 3) | DC EKGENL I AATINC | DENERI | Provent for center | DENEM | | PROKTOR DENETI | I JUNE IN SWELL |
| SK-1 | KAROT | (m) 0,00-5,00 | * | Kg/cm2 | #10(+) | # 200(-) | NLL | 76 PL | 76 PI | gr/cmJ | No. | ¥45 | KURU | NSU | \$(0) | C (kg/cm2) | MV | GY | MUX YOON | | TSE 1500 |
| SK-2 | KAROT | 0,00-5,00 | | 6,39 6,53 | | | | | | | | | | - | | | | | + | | |
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ZEMTEST ZEMİN ARAŞTIRMA VE LABORATUVAR HİZMET LTD ŞTİ. ADRES:MELİKGAZİ MH.AŞIK VEYSEL BUL.BARIŞMANÇO KONAĞI NO:4/A ZEMİN MEKANİĞİ LABORATUVARI TEL :0352 333 55 44 T.C. CEVRE VE ŞEHIRCİLİK BAKANLIĞI MAIL:INFO@ZEMTEST.COM LABORATUVAR DENEYLERİ TOPLU SONUÇ RAPOR FORMU 1/1 Sayfa No Yüklenici Firma ADER MÜHENDISLİK Numune Geliş Tarihi 07.05.2018 NIĞDE İLİ MRKZ. İLÇ. TEPE MH. 95 ADA 60 PARSEL Proje Adı 10.05.2018 Rapor Tarihi Rapor No 1446-18 Bakanlık Rapor No 14860414 Direkt Kesme Hidrometre CBR Úç Eksenli (UU) / (CU) Doğal Su İçeriği Zemin Sınıfı Serbest Basing Bha Proktor Ort.Dbha Elek Analizi Sondaj Numune Atterberg Limitler Deneyi(qu) -0,075 -0,002 2.5 mm Özgül ağırlık c ф Ort.ls (50 icsel +4 - 200 Kalan Geçen (%) (%) 14,70 18,70 Kohezyon Kgf/cm2 Ykmax (g/cm^a) Yn (gr/cm³) ф Deres % 96 sürtünn Kuyu No: Tipl ve Adı Derintik (m-m) USCS (Kg/cm2) kg/cm2 Kgf/cm2 % (g/cm*) Wopt (%) (%) LL (%) PL (%) PI (%) açısı 0,213 22 NP NP NP SM 1,78 UD 1,00-1,50 7,6 SK-1 0,229 21 SK-2 UD 1,00-1,50 6,7 NP NP NP 12,40 23,40 SM 1,74 *R FR 19 Yayın Tar: 03.12.2015 Revizyon No/Tar: 00 *Bu deney formu izinsiz hiçbir şekilde çoğaltılıp kopya edilemez. *Söz konusu deney sonuçları, sadece test edilen deney numunelerine aittir *Tüm hakları Zemtest Zemin Araştırma ve Lab.Hiz Ltd. Şti.'ye aittir. * Laboratuvarımız 4708 sayılı kanun gereği T.C.Çevre ve Şehircilik Bak. tarafından verilen 02.03.016 tarih ve 539 No'lu laboratuvar izin belgesine sahiptir.

icil NO.14982



Köksai ÖZNAEN Genetçi Müh) Belge No:19652

| | BİLGİL | | | | | | | | | | | | | Numune | Gelis Tar | ihi | 13.02.2016 | |
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| | JRU SAH | İBİ | ADER MÜHI | and the second se | | | | | | | | | | Deney B | aş. Tarihi | | 13.02.2016 | |
| | SAHİBİ | | ADER MÜHL | | | | | | | | | | | Kayrt Nu | marsi | | K16-213-Z | |
| | IIN ADRI | | SARIKÖPRÜ | | RKEZ / NI | ĞDE | | | | | | | 1 | Rapor T | arihi | | 23.02.2016 | |
| PAFTA | ADA/P | ARSEL | 956 ADA / 7 | | | | | | | | | the second | Rapor N | umarası | | R16-213-2 | |
| 1 | • | | TOP | LU DEN | IEY SC | DNUÇL | ARIR | APOF | RU | | | | | Bakanlı | Rap. No | | 9900283 | |
| Sondaj | Numan | ¢ | Doğal Su | Doğal Birim | Elek | Analizi | Atte | rberg Lin | nítleri | | Nokta Yükleme | Üç Ek Basınç | | Konso | lidasyon | | Direkt Kesn | е Белсуі |
| Adı | Adt | Derinlik | Muhtevası (%) | Hacim Ağırlık (gr/cm ³) | #9 Kalan (%) | #200 Geçen (%) | u. (%) | PL (%) | PI (%) | USCS | Dayanımı (kgf/cm2) | * Cup (kgt/cng ²) | * F _{up} (*) | Şişme Yüzdesi (%) | \$1şme Basıncı (kN/m²) | Gs | * c _{up} (kgf/cm ²) | *f _{up} (°) |
| SK-1 | UD-1 | 1,50-2,00 | 33,38 | 1,92 | 0,00 | 92,23 | 45 | 24 | 21 | CL | | (0,75) | (5) | 3,1 | 1 | 2,66 | | |
| SK-2 | UD-1 | 1,50-2,00 | 19,29 | 1,90 | 0,00 | 90,33 | | NP | | ML | | | C | | | | 0,5663 | 10,8 |
| * Laboratu | vermax Çevre | TS - 1900-1, T ve Şelürcilik Ba vi vapılan namını DENEY | kanlığının 11.04 | 1.2011 tarilt ve | | | | | anatzar izm | olmalcszan d | teğiştirdensoz ve | kamet yogahi | | | ne yoneld, tek b R DENETCI | | ikar vermez | |
| | | | hritet f | SEN | | B= C= . | 12 12 | ; | je. | | | | | | AKAR AKAR | | | |

| <u>ا</u> ـــــا | Yap | J L Martine Den | M. C. W | | • | | Hiz. | MÜP zi Çakm | ak Mah. | D. SA | N. VET | ORATU IC. LTD Karatay / k 40 | . STI. | | Economi | K | s | EVRE VE SEHRCILI BAKANLIC | |
|---------------------|------------------|--------------------|------------------|-----------------------|-----------------------------------|----------------|----------------|----------------|--------------|---|----------------|---------------------------------------|--|-------------------------|--|---------------------------------|---------------|--|-------------|
| | YAPI | BILGIL | ERİ | | | | | | | | | | | | Numune | Gelis Tar | ihi | 05.09.2017 | |
| | BAŞVL | IRU SAH | İBİ | HAKAN MÜ | IENDÍSLÍK | | | | | 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - | | and successive the successive state | | | | aş. Tarihi | | 05.09.2017 | |
| | | SAHİBİ | | SERDAR DE | MİRCİ (SEL | MA TURAL |) | | | | | | | | Kayıt Nu | | | K17-1962-2 | |
| | YAPIN | IN ADR | ESI | KIRBAĞLAR | I MAH. / ME | RKEZ / N | ĞØE | | | | | | | | Rapor Ta | | | 07.09.2017 | |
| | PAFTA | ADA/P | ARSEL | 1720 ADA / | 12 PARSEL | | | | | | | | | | Rapor N | umarası | | R17-1962-2 | |
| | | | | TOP | LU DEN | VEY SC | DNUÇL | ARIF | RAPOR | zu | | | | | Bakanlık | Rap. No | | 13273606 | |
| | | Numun | e | | Doğal | Elek | Analizi | Atte | erberg Lir | nittori | T | | Üç Ek | | Koncol | idasyon | | Direkt Kesn | Donaud |
| | Sondaj Kuyusu | Tipi ve | Derintik | Doğal Su Muhtevası | Birim Hacim | #10 | #200 | | 1 | | USCS | Nokta Yükleme Dayanımı | Basinç | | Şişme | Şişme | Gs | | |
| | Ada | Adı | Dermin | (%) | Ağırtılı (gr/cm ³) | Kalan (%) | Geçen (%) | LL (%) | PL (%) | PI (%) | | (kgf/cm2) | * c _{up} (kg/cm ²) | *f _{up} (°) | Yüzdesi (%) | Basinci (kN/m ²) | | * c _{up} (kg/cm ²) | *fup (°) |
| | SK-1 | UD | 1.50-2.00 | 24,61 | 1,92 | 0,00 | 88,12 | 44 | 23 | 21 | CL | | | | | | | 0,6131 | 8 |
| | SK-1 | SPT | 2.00-2.45 | 29,83 | 1,94 | 0,00 | 87,31 | 45 | 23 | 22 | CL | | | | | | | | |
| | SK-2 | UD | 1.50-2.00 | 23,47 | 1,92 | 0,00 | 89,33 | 43 | 25 | 18 | CL | | | | | | | 0,6183 | 8,1 |
| | SK-2 | UD | 3.50-4.00 | 34,62 | 1,95 | 0,00 | 91,26 | 48 | 25 | 23 | CL | | | | | | | 0,5840 | 9,1 |
| | SK-3 | UD | 8.00-8.50 | 38,59 | 1,88 | 0,00 | 38,32 | | NP | | SM | | | | | | - | | |
| | SK-3 SK-4 | SPT UD | 7.50-7.95 | 37,05 | 1,89 | 0,00 | 40,18 | | NP | | SM | | | | | · · | | | |
| | SK-4 | SPT | 6.50-6.95 | 24,69 36,13 | 1,92 | 0,00 | 89,29 43,54 | 45 | 24 NP | 21 | CL SM | | | | | | | 0,6190 | 7,9 |
| | 31-4 | 5F1 | 0.50-0.95 | 50,15 | 1,09 | 0,00 | 45,54 | 1 | NP- | | 514 | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |
| | Not ve Act | klamalar; | | | C | | | | ليستعمل | | | | | | | | | | |
| * | * Kullanılar | Standartlar; | TS - 1900-1 , T | S - 1900-2 ve T | S 1500 | | | | | | | | 5.0 | | | | | | |
| | | | ve Şehircilik Ba | | | | | | | | | | | | | | | | |
| | * Bu rapor, | sadece dener | | | Numunezin alı | ndığı yere ait | bilgiler müşte | riye ait olı | op, laboratu | saranazan ize | i olmaksızın (| leğiştirilernez ve | ə kısmen çoğalı | BI | mn güvenlirliğ GORATUVAL EKİR OlOJI Vetçi Belg | KARS | si U ih | | |
| (Junar de Maringan | Suveyda Mer | 1 | ASLI (| · | | | | | | | | | | | | | | | |

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| ZEMİ | N MEK | ANIĞI LABO | DRATUV | ARI | rad L | | | | H.AŞIK VEYS TEL :03 | L BUL.BARIŞMA 52 333 55 44 92EMTEST.COM | NÇO KONA | | | | | | | T C. | vre vr | TESEH | incluie | | |
|-------------|------------|-------------------|------------|------------|-----------------|------------|------------|-------------|------------------------|---|-------------|-------------|-------|-----------|-------|-----------|----------|-----------|----------------------------------|------------------|------------------|------------|-----|
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| | | | | | | LABOR | VUTAS | AR DEN | FYLERI | TOPLU SO | NUC R | APO | | PMII | | | | | | | | - | _ |
| üklenici | Firma | | ADER MÜ | HENDIS | LİK | -/ | | ANDER | | 101 20 30 | NUÇIU | | 110 | KINO | Savt | a No | | | - 1 | 1/1 | | | - |
| roje Ad | | | NIĞDE İLİ | MRKZ. IL | Ç. KIRBAĞLA | RI MH 1873 | ADA 6 PA | RSEL | | | | | | | | une Ge | s Tarihi | | | 28.02.2 | 2018 | | |
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| Sondaj | | Numune | Doğal Su | Atte | rberg Limitleri | Elek | Analizi | Zemin | Ort.Dbh | Serbest Basing | Üç Eksen | li (UU) | Konse | lidasyon | Bh | | Proktor | | CBR | | Di | rekt Kesme | |
| | | | lçeriği | | | +4 | - 200 | Sinifi Ort | s (50) | a Deneyi(qu) | / (CL | 0 | şişme | şişme bas | s on | | FIGRIOF | | 2,5 mm | Özgül | c | | Ф |
| Kuyu No: | :Tipi ve · | Derinlik (m-m) | (%) | LL (%) | PL (%) PI (? | Kalan | Gegen | USCS (Kg | cm2) Yn (gr/cm) | kg/cm2 | C Kgf/cm2 | ф Derece | % | | (g/cr | ma) Wop | (%) Y | (max | % | agiriik | Kohezy Kgf/cm | on | sel |
| SK-1 | UD | 1,00-1,50 | 7,9 | NP | NP NF | (%) | (%) | SM | - 1,62 | | - | - | - | | - | _ | (9) | - | - | | 0,243 | aç aç | 3 |
| SK-2 | UD | 1,00-1,50 | . 6,4 | NP | NP NF | | 17,10 | | 1,63 | - | - | | - | | | | _ | - | - | - | 0,19 | | 3 |
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| Yap | K Om | m a w | li tuvari | | | HIZ. Fevz | i Çakma | k Mah. | 10569 Sk | . VE T. . No:34 k 342 41 4 | İC. LTD Karatay / KC 0 | DNYA | | | | | T.C. SEHIRCILİK BAKANLIĞI | |
|-------------------------|--|---------------|------------------------------|--|--------------------|----------------------|-----------|-----------|-----------|----------------------------------|------------------------------|--|-------------------------|-------------------------|-----------------------------|----|--|-------------------------|
| YAPI | BİLGİLE | | Geliş Tar | ihi | 16.02.2013 | | | | | | | | | | | | | |
| BASVU | VURU SAHİBİ AKNUR MÜHENDİSLİK I SAHİBİ GÖRKEMLİ SİTESİ-A BLOK ININ ADRESİ SARIKÖPRÜ MAH. / MERKEZ / NİĞDE TA/ADA/PARSEL 2202 ADA / 10 PARSEL | | | | | | | | | | | | | | aş. Tarihi | | 16.02.2013 | 3 |
| YAPI S | | | | | | | | | | | | | | | marsı | | K13-142-Z | |
| YAPIN | | | | | | | | | | | | | | | arihi | | 20.02.2013 | |
| PAFTA | | | | | | | | | | | | | | | Rap. No | | R13-142-Z | _ |
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| | Numune | senli (UU) | Konsol | idasyon | | Direkt Kesr | ne Deney | | | | | | | | | | | |
| Sondaj Kuyusu Adı | Tipi ve Adı | Derinlik | Doğal Su Muhtevası (%) | Birim Hacim Ağırlık (gr/cm ³) | #4 Kalan (%) | #200 Geçen (%) | LL (%) | PL (%) | PI (%) | USCS | * q _u (kg/cm2) | * C _{up} (kg/cm ²) | *f _{up} (°) | Şişme Yüzdesi (%) | Şişme Basıncı (kN/m²) | Gs | * c _{up} (kg/cm ²) | *f _{up} (°) |
| SK-1 | UD-1 | 3,50 | 23,24 | 1,93 | 7,26 | 66,47 | 40 | 22 | 18 | CL | | 0,64 | _3 | | | | | |
| SK-1 | SPT-1 | 3,00 | 2,01 | | 6,26 | 2,06 | | NP | | SW | | | | ~ | | | | |
| SK-2 | UD-1 | 3,50 | 22,69 | 1,92 | 6,49 | 68,40 | 39 | 20 | 19 | CL | | 0,65 | 3 | | | | | 45.00 |
| | UD-2 | 6,00 | 9,78 | 1,88 | 6,45 | 7,35 | | NP | | SM | | | | | | | 0,0089 | 15,66 |
| SK-2 | UD-1 | 3,50 | 15,24 | 1,90 | 4,23 | 56,82 | 37 | 18 | 19 | CL | | 0,6 | 4 | | | | | |
| SK-2 SK-3 | | 3,50 | 17,94 | 1,91 | 2,14 | 65,32 | 38 | 17 | 21 | CL | | 0,66 | 3 | | | | | _ |
| | UD-1 | 5,50 | | | | 1,65 | | NP | | SW | | | | | | | | |

Not ve Açıklamalar:

* Kullanılan Standartlar: TS - 1900-1 , TS - 1900-2 ve TS 1500

* Laboratuvarımız Çevre ve Şehircilik Bakanlığının 11.04.2011 tarih ve 273 sayılı"Laboratuvar İzin Belgesi"ne sahiptir.

* Laboratuvarımız Çevre ve Şehircilik Bakanlığımı 11.04.2011 tarın ve 2/3 suyur-Laboratuvarızın zen Beigesi ne sampur. * Bu rapor, sadece deneyi yapılan yerler için geçerlidir. Numunenin alındığı yere ait bilgiler müşteriye ait olup, laboratuvarımızın izni olmaksızın değiştirilemez ve kısınen çoğaltılamaz. Yapının güvenilirilğine yönelik tek başına bir fikir vermez. DENEYT YAPAN LABORATUVAR DENETÇİSİ

DENEYİ YAPAN

BAMIFARARSU Denetçi Belge No: 10360

| GEDIK M | RE VE SEHIR BAKA | NLIGI | | aboratuv | | 1 | VILIFICAT LAS | 1 1400 | ulgi xaj ratuvar VEY FO | IZIN BE | lgesi''n | Müdü 1e Sahi | rlüğü) iptir. | l'arafin | idan Ve | erilen 1 | 12 | 1 | | g | edik | |
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| ADA | | 2589 | PA | FTA | 20L 11-20 | H. YEN OL III | IÇARŞI PAK | İŞ MERK İSEL | EZÌNO | :206 NI 8 | ĞDE TA | RÍH | 30,01 | 1,2015 | RAPO | R NO : | | BN:77 | 23246/2 | 2015/238/ ENDİSLİI | TRIYAS K | |
| KUTUNO | ORVEK NO | DERINLIK | SU ICENCI | NOKTA YÜKLEME DENEY | id init as is | | ATTE | RBERG LIM | TLERI | OZGOL AĞIRLIK | TEX EKSENLİ BASINÇ Diğileti (Ağlanı) | В | .H.A (Gr/cn | n3) | DATA A LANGUAR DO | LENEL | KONSOLIDASYON | DENETI | | PROKTOR DENERI | ZEAdiv Similer | |
| SK-1 | KAROT | € 0.00-5.00 | ж | Kg/cm2 | #10(+) | # 200(-) | NLL | % PL | 36 PI | gr/osJ | No. | 245 | KURU | 9450 | \$ (a) | C (kg/cm2) | MV | cv | MUX YOON | | TSE 1500 | - |
| SK-2 | KAROT | 0,00-5,00 | | 6,39 6,53 | | | | | | | | | | | - | | | | | | | - |
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| idendijsto | And I | JEOLOJI | SAVRA | DISI: | | | • | nek Alumi Ve | | | | | × | | | ر ⁻ ر | EOLOJ | NETÇİ 1 YÜKS SUNGU | EKMO | HENDIS | t: | |

| EMIN | MEKA | ANİĞİ LABOI | RATUVA | RI | | | | | | TE MAİL:İ | L :0352 3 INFO@ZE | BUL.BARIŞMAN(333 55 44 EMTEST.COM | | | | 8 | | | T.K GE BA | S. EVRE V AKANL | VE ŞEH | RCILIK | |
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| iklenici | | | ADER MÜ | | | | | 10051 | | | | | | | | | Numune | | rihi | | 07.05.2 | 018 | |
| roje Adı | | | NIĞDE ILI N 1446-18 | VRKZ. IL | Ç. TE | EPE MH. 95 | ADA 60 P | ARSEL | | | | | | | | | Rapor Ta | | | | 10.05.2 | 018 | 11.1.1.1 |
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| | | Numune Doğal Su İçorâji Atterberg Limitleri Elek Analizi Zamin Sınıfı Ort. İbha Serbest Basınçı Deneyi(qu) Oç Eksanli (UU) Hidrowert Bita Proktor | | | | | | | | | | | | | | CBR | | Direkt | Keame | | | | |
| Sondaj | | Numune Doğal Su İşeriği Atterberg Limitleri Elek Analizi Zemin Sırıfı Ort. Daha Örr. D | | | | | | | | | | | | | 2.5 mm | Özgül | c | Φ | | | | | |
| Kuyu No: | Tipi ve | Derinlik (m-m) | (%) | LL (%) | PL (| %) PI (%) | +4 Kalan | - 200 Geçen | USCS | (Kg/cm2) | Yn (gr/cm*) | kg/cm2 | C Kgf/cm2 | ф Derece | % | 96 | (g/cm*) | Wopt (%) | Ykmax (g/cm²) | % | ağırlık | Kohezyon Kgf/cm2 | içsel sürtünme açısı |
| SK-1 | UD | Ipi ve Derinitik (%) LL (%) PL (%) PI (%) Kain General CK g/cm ² Mg/cm ² CK gf/cm ² Derine % % (g/cm ²) (g/cm ²) Adr (m-m) (%) LL (%) PL (%) PI (%) Kain General Ggr/cm ² (g/cm ²) Rg/cm ² CKgf/cm ² Derine % % (g/cm ²) | | | | | | | | | | | | | - | - | 0,213 | 22 | | | | | |
| SK-2 | UD | 1.00-1.50 | 6,7 | NP | NF | | 12,40 | 23,40 | SM | 194 - | 1,74 | - | - | - | - | - | - | - | - | 1.41 | - | 0,229 | 21 |
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| Tüm ha | kları Zem tuvarımı Ser Kat | ey sonuçları,sadec itest Zemin Araştır z 4708 sayılı kanu eneyri Yapan payışdu ileçi. Mül | e test ediler ma ve Lab. | liz Ltd. S | num Sti.'y | unelerine e aittir. | | an verilen | 02.03.0 | | ST ZEM | Ness TIRMA | n belgesine | e sahipti | r. | | | / | KOKSAĨŎ | | | / Mah) | |

2 ZEMTEST ZEMİN ARASTIRMA VE LABORATUVAR HİZMET LTD STİ. ZEN = 5 1 4 ADRES:MELİKGAZİ MH.AŞIK VEYSEL BUL.BARIŞMANÇO KONAĞI NO:4/A ZEMÍN MEKANÍĞI LABORATUVARI TEL :0352 333 55 44 T.C. MAIL:INFO@ZEMTEST.COM ÇEVRE VE ŞEHİRCİLİK BAKANLIĞİ 3.16 LABORATUVAR DENEYLERI TOPLU SONUÇ RAPOR FORMU ADER MÜHENDÍSLÍK Sayfa No 1/1 Yüklenici Firma 17.03.2016 Proje Adı NİĞDE MERKEZ AHİPAŞA MAH. 364 ADA 41 PARSEL Numune Geliş Tarihi Rapor No 0040-16 Rapor Tarihi 21.03.2016 10052649 Bakanlık Rapor No Hidrometre CBR Direkt Kesme Doğal Su İçeriği Zəmin Sınıfı Serbest Basing Deneyl(qu) Úc Eksenli (UU) / (CU) Ort.Dbha Bha Proktor Sondaj Atterberg Limitiori Elek Analizi Numune -0,075 -0,002 2.5 mm Ort.In (50) Özgül ağırlık • ф +4 Kalan (%) - 200 Geçen (%) içzel sürtünme Kuyu No; Tipl ve Adı Derinlik (m-m) Yn (gr/cm²) Ykmax (g/cm³) Kohezyon Kgf/om2 ¢ Derec (%) LL (%) PL (%) PI (%) USCS (Kelom2) kg/cm2 Kgf/cm 26 % (g/cm³) Wopt (%) 96 acisi SK-1 CR 2,50-3,00 --8,7 2,18 --. -SK-2 CR 3,50-3,00 9,3 2,20 -. . *R FR 19 Yayın Tar: 03.12.2015 Revizyon No/Tar: 00 *Bu deney formu izinsiz hiçbir şekilde çoğaltılıp kopya edilemez. *Söz konusu deney sonuçları, sadece test edilen deney numunelerine aittir *Tüm hakları Zemtest Zemin Araştırma ve Lab.Hiz Ltd. Şti.'ye alttir. * Laboratuvarımız 4708 sayılı kanun gereği T.C.Çevre ve Şehircilik Bak. tarafından verilen 02.03.016 tarih ve 539 No'lu laboratuvar izin belgesine sahiptir. Beneyi Yapan

ALLEDACH) DA

ZEMTEST ZEMIN ARAŞTIRMA VE LABORATUVAR HIZMET LTD, ŞTİ. Mellişazi MA Aşıkveysel Bulvan Bariş Manço Konağı NG HiA Melikgazi/KAYSERİ Erolyası Vo 1997 C70 8501 Mersis NC: 0142063064600013

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| Yü | klenici fir | ma : | ADER N | 1ÜHENI | DİSLİK | | | | | | | | | | | | | | | |
| P | roje | : | NİĞDE İI | Lİ MRK | Z. İLÇE | Sİ SAR | IKÖPRŰ | | | A 4 PA | RSEL | | | | | | | | | Sayfa No: 1/1 |
| | apor Taril | hi : e(Sampl | 18.03.20 | T | lacim m3) | EL | apor No: LEK LIZI NALYSIS) | AI | 4-2804 TARBER IMITLER TRBERG LIP | ut i | RMA | LEME (cm²) | Bakanlık | No : Üç Ek Basınç TRIA COMPRESS | Denevi | Kesme Der DIRECT | Kutusu Ieyi SHEAR | Konso (CONSO | lidasyon LIDATOIN) | TRE ^{III} |
| Тірі Туре | j No: g No: | Derinlik Depth(m | e No: e No: | Doğal Su İçeriği: (Wn)(%) | Doğal Birim Hacim Ağırlık (gr/cm3) | +4" | -200" | LL (%) | PL (%) | РІ (%) | SINIFLANDIRMA (USCS) | NOKTA YÜKLEME İNDEKSİ (kg/cm²) | Serbest Basınç Deneyi(qu) (kgf/cm²) | с | Ф Derece | C Kgf/cm² | Ф | Şişme Basıncı | Şişme Yüzdesi(%) | HIDROMETRE (HYDROMETER) |
| CR | SK-1 | 2,50-3,00 | 0 N-1 | - | 1,99 | - | - | - | - | - | - | 8,6 | - | - | - | - | - | - | - | - |
| CR | SK-2 | 2,50-3,00 | 0 N-2 | - | 2,01 | - | - | - | - | - | | 9,2 | - | - | - | - | - | - | - | - |
| CR | SK-3 | 2,50-3,00 | 0 N-3 | | 2,03 | · - | - | - | - | - | - | 10,1 | - | - | - | - | - | - | - | - |
| and the share of the second | ooluh | ASLICED | <u>N:</u> AYSAL | - | | | | - | na Beyanıdı sonuçları, sa 708 sayılı kı 30.05.2011 izni olmada | | illen deney : Cevre ve At No'la Laho UGATIAS NISC ATCA TIC. LT Otak Sk. As TIC. LT - Tak (060) aslow VO. 3 | numunelerin filti ili Bal antiamaz Atbarnaz ADEMCLI Mita, MUD STI. STI. STI. STI. STI. STI. STI. STI. | ie aittiir. canlığı Yapı İşi a Belgesi'ne sə K H. ızl | leri Genel Mi | ıdarlaga | | bdulk | ONAI adil BI Senetçi I elge No | | <u>v</u> |

| ZEMİ | N MEK | ANİĞİ LABC | RATUV | ARI | 9 | | | | | MH.AŞIK TE | VEYSEL L:0352 | LABORATUVA BUL.BARIŞMAN 333 55 44 EMTEST.COM | | | | | | | 7 C GE 19 / | WRE V KANL | e șen Gi | irci.k | |
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| | | | | | | LAB | ORAT | TUVA | AR DE | NEYLE | ERÍ T | OPLU SON | IUÇ RA | POF | RFO | RMU | | | | | | | |
| üklenici roje Ad | | | ADER MÜ | | | | | | | | | | | | | | Sayfa No | | | | 1/1 | | |
| apor No | | | 503-18 | VIKKZ. II | LÇ. KIRBAĞL | ARIMH 1 | 1873 AD | DA 6 PAR | SEL | | | | | | | | Numune Rapor Ta | | arihi | | 28.02. | | |
| | | | | | | | | | | | | | | | | | Bakanlık | | No | | 14469 | 284 | |
| Sondaj | l | Numune | Doğat Su İçeriği | Atte | arberg Limitleri | | Elek Anali | lizi | Zemin Sinifi | Ort.Is (50) | Ort.Dbha | Serbest Basinç Deneyi(qu) | Üç Eksenli / (CU) | (UU) | | lidasyon şişme bas | Bha | Pr | oktor | CBR 2.5 mm | 0 | Direk | Kesme |
| Kuyu No: | Tipi ve · | Derintik | (%) | 11.(%) | PL (%) PI (| (%) Kal | | - 200 Gogon | | | Yn (gr/cm*) | kg/am2 | 0 K - K - 0 | Φ | 319 <i>m</i> e | şışme bas | (g/cm*) | | Ykmax | 2.5 mm | Özgül ağırlık | c Kohezyon | ф içsəl |
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| ADER MÜHENDİSLİK SOİL BORING LOG Sondaj No SK-2 Başlarna Tarihi Derihlîk (m) 15.00 Bitiş Tarihi Sondör |
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| and a second sec |
| Sondaj Mühendisi Ö.FİDAN elefon / Phone :(0388) 233 14 15 Faks / Fax : (0388) 233 14 15 Koordinat (Y) YER ALTISU DURUMU |
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| <u> </u> | - | Ne Qemi | | l û wari | <u> </u> | LB | HİZ. | MÜH. Çakmal | MAC | . SAN | No:34 K | C. LTD. | ŞTİ. | | | Gelis Tari | | T.C. SEHIRCILIK BAKANLIĞI | |
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| | Sondaj Kuyusu Adı | Tipi ve Adı | Derinlik | Doğal Su Muhtevası (%) | Birim Hacim Ağırlık (gr/cm ³) | #4 Kalan (%) | #200 Geçen (%) | LL (%) | PL (%) | PI (%) | USCS | * q _u (kg/cm2) | * C _{up} (kg/cm ²) | *f _{up} (°) | Şişme Yüzdesi (%) | Şişme Basıncı (kN/m²) | Gs | * c _{up} (kg/cm ²) | *f _{up} (°) |
| | SK-1 | UD-1 | 2,50-3,00 | 24,31 | 1,83 | 5,63 | 27,89 | | NP | | SM | | | | | | | 0,1165 | 23,2 |
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| | SK-2 | UD-1 | 2,50-3,00 | 26,56 | 1,84 | 7,39 | 30,82 | | NP | | SM | | | | | | | 0,1229 | 23,3 |
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| | SK-3 | SPT-1 | 4,50-4,95 | 36,12 | 1,86 | 0,00 | 87,79 | 46 | 24 | 22 | CL | | | | | | | | |
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Not ve Acıklamalar:

* Kullanılan Standartlar: TS - 1900-1 , TS - 1900-2 ve TS 1500

* Laboratuvarımız Mülga Bayındırlık ve İskan Bakanlığı'nın 11.04.2011 tarih ve 273 sayılı "Laboratuvar İzin Belgesi"ne sahiptir.

* Bu rapor, sadece deneyi yapılan yerler için geçerlidir. Numunenin alındığı yere ait bilgiler müşteriye ait olup, laboratuvarımızın izni olmaksızın değiştirilemez ve kosmen çoğaltılamaz. Yapının güvenilirliğine yönelik tek başına bir fikir vermez.

Menmet ESE

Jeoloj Yek Müh Denetçî Belge No: 10360

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KENEVIEVE I BERIN LABORATUVAR HÌZ. MÜH. MAD. SAN. VE TÌC. LTD. ȘTİ. Fevzi Çakmak Mah. 10569 Sk. No:34 Karatay / KONYA CLUICE VE SEHIRGI IK BARANJOI Tel/Faks: (0 332) 342 41 40 YAPI BİLGİLERİ Numune Geliş Tarihi 13.02.2016 BAŞVURU SAHİBİ ADER MÜHENDİSLİK Deney Baş, Tarihi 13.02.2016 YAPI SAHİBİ ADER MÜHENDİSLİK Kayıt Numarsı K16-213-Z YAPININ ADRESI SARIKÖPRÜ MAH. / MERKEZ / NİĞDE Rapor Tarihi 23.02.2016 PAFTA/ADA/PARSEL 956 ADA / 7 PARSEL Rapor Numarasi R16-213-2 **TOPLU DENEY SONUCLARI RAPORU** Bakanlık Rap. No 9900283 Nuprone Doğal Üç Eksenli Elek Analizi Atterberg Limitieri Konsolidasydn Direkt Kesme Deneyi Nokta Basinc (UU) Doğal Su Birim Sondai Yükleme Tipi ve Muhtevası Hacim USCS Kuyusu Derinlik #4 #200 Gs Sisme Dayanımı Şişme 11 * Cup Adı (%) Ağırlık PI PI * fup * Cup *fup Kalan Geçen Adı (kgf/cm2) Yilzdesi Basinci (%) (%) (kgt/cm2) (gr/cm³) (%) (") (kgf/cm²) (°) (%) (%) (%) (kN/m2) SK-1 1,50-2,00 0,75 5 UD-1 33,38 1,92 0,00 92,23 45 24 21 CL 3,1 2,66 SK-2 UD-1 1,50-2,00 19,29 1.90 0.00 90,33 NP ML 0,5663 10,8 Not ve Aceklamalar: * Kullandan Standartlar: TS - 1900-1 , TS - 1900-2 ve TS 1500 ⁶ Laboratuvarmuz Çevre ve Şehircifik Bakanlığının 11.04.2011 tarih ve 273 sayılı"Laboratuvar İzm Beigoal'ne sahiptir. * Sur topot, sindece Jenevi vapilan namme igin gegenlidir, Namancain alualog yooc an bilgiler miljetriye miljetriye miljetriye an oling, helverativannarzar kan olmaktazan değiştirdamaz vo konner çogafilarınaz. Yapının gövenliktigane yonaldı, tek buşına bit fikar vermez DENEYİ YAPAN LABORATUVAR DENETÇİSİ B= 12 C= 12 Mennet ESEN Bokit AKARSU

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| | | | | Sondaj Kuyusu Adı | Tipi ve Adı | Derintlik | Doğal Su Muhtevası (%) | Hacim Ağırtık (gr/cm³) | #10 Kalan (%) | #200 Geçen (%) | LL (%) | PL (%) | PI (%) | USCS | Yüldeme Dayanımı (kgf/cm2) | * C _{up} (kg/cm ²) | *f _{up} (°) | Şişme Yüzdesi (%) | Şişme Basıncı (kN/m ²) | Gs | * c _{up} (kg/cm ²) | *f _{up} (°) | |
| | | | - 10 C | SK-1 | UD | 1.50-2.00 | 24,61 | 1,92 | 0,00 | 88,12 | 44 | 23 | 21 | CL | | | | | | | 0,6131 | 8 | |
| | | | | SK-1 | | 2.00-2.45 | | 1,94 | 0,00 | 87,31 | 45 | 23 | 22 | CL | | | | | | | | | 1 |
| | | | | SK-2 | UD | 1.50-2.00 | | 1,92 | 0,00 | 89,33 | 43 | 25 | 18 | CL | | | | | | | 0,6183 | 8,1 | |
| | | | | SK-2 | | 3.50-4.00 | 34,62 | 1,95 | 0,00 | 91,26 | 48 | 25 | 23 | CL | | | | | | | 0,5840 | 9,1 | |
| | | | | SK-3 | | 8.00-8.50 | | 1,88 | 0,00 | 38,32 | | NP | | SM | | | | | | | | | |
| | | | | SK-3 | | 7.50-7.95 | | 1,89 | 0,00 | 40,18 | | NP | | SM | | | | | 14° | | | | |
| | | | | SK-4 | | 1.50-2.00 | | 1,92 | 0,00 | 89,29 | 45 | 24 | 21 | CL | | | | | | | 0,6190 | 7,9 | |
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| | | | | | | TS - 1900-1 , T ve Şehircilik Ba | | | 273 sayah'L | aboratuvar İzir | Belgesi'n | sahiptir. | | | | | × . | | | | | | |
| | | | | | | i yapılan numun | | | | | | | arımızın izni | olmaksizin | leğiştirilemez ve | e kusmen çoğalt | lamaz. Yap | mn güvenilirliği | ne yönelik tek | başına bir fi | ikir vermez. | | |
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ZEMTEST

ZEMTÉST ZEMÍN ARASTIRMA VE LABORATUVAR HÍZMET LTD STÍ. ADRES:MELÍKGAZÍ MH.AŞÍK VEYSEL BUL:BARIŞMANÇO KONAĞI NO:4/A

TEL:0352 333 55 44 MAIL:INFO@ZEMTEST.COM T.C. ÇEVRE VE ŞEHİRCILİK BAKANLIĞI

| üklenici | Firma | | ADER MÜ | HENDIS | LİK | | | | | | | | | | | | Sayfa N | 0 | | | 1/1 | | |
|-------------|----------------|-------------------|-----------|---------|-----------|---------|--------------------|-----------------------|-------|-------------|----------------|----------------|-----------|-------------|--------|--------|---------|------------|------------------|--------|---------|---------------------|---------------------------|
| roje Ad | r i | | NIĞDE İLİ | MRKZ. İ | LÇ. HIDI | RLIK MI | H. 2169 AL | DA 18 PAR | SEL | | | | | | | | Numun | e Geliş Ta | rihi | | 26.05.2 | 016 | |
| apor No | > | | 0471-16 | | | | | | | | | | | | | | Rapor T | arihi | | | 31.05.2 | 016 | |
| | | | | | | | | | | | | | | | | | Bakanlı | k Rapor N | lo | | 105370 | 14 | |
| Sondaj | | Numune | Doğal Su | Atte | rberg Lin | nitteri | Elek | Analizi | Zemin | | Ort.Dbha | Serbest Basing | Og Elæe | | Hidro | metre | Bha | Pro | ktor | CBR | | Direkt | Kesme |
| | | | İşeriği | | | | | | Smfr | Ort.Is (50) | | Deneyi(qu) | / (0 | (U: | -0,075 | -0,002 | | | | 2.5 mm | | c | \$ |
| Kuyu No: | Tipl ve Adt | Derinlik (m-m) | (%) | LL (%) | PL (%) | PI (%) | +4 Kalan (%) | - 200 Geçen (%) | USCS | (Kg/cm2) | Yn (gr/cm²) | kg/cm2 | C Kgf/cm2 | ф Derece | % | * | (g/cm*) | Wopt (%) | Ykmax (g/cm?) | % | ağırlık | Kohezyon Kgffem2 | içsel sürtünm acısı |
| SK-1 | UD | 1,50-2,00 | 12,9 | NP | NP | NP. | 1,90 | 36,40 | SM | - | 1,70 | - | - | - | | - | - | | - | - | - | 0,215 | 21 |
| SK-2 | UD | 1,50-2,00 | 14.2 | NP | NP | NP | 2.20 | 39.10 | SM | - | 1.72 | - | - | | - | - 1 | - | - | - | - | - | 0,213 | 21 |

*Söz konusu deney sonuçları,sadece test edilen deney numunelerine aittir

*Tüm hakları Zemtest Zemin Araştırma ve Lab.Hiz Ltd. Şti.'ye alttir.

.* Laboratuvarımız 4708 sayılı kanun gereği T.C.Çevre ve Şehircilik Bak. tarafından verilen 02.03.016 tarih ve 539 No'lu laboratuvar izin belgesine sahiptir.

Denevi Yapan chat DAYSAL (ico Muh)



ZEMTEST ZEMÍN ARASTIRMA VE LABORATUÁR HIZMET LTD. STI. - Melikazi Mr. Apliceguei Bulvan Bang Konst Kor Melikazi/KAYSERI Eropez (D. Jón Melikazi/KAYSERI Marais No: 01/#2063064600013

| · · · · · · · · · · · · · · · · · · · | | | ADRES:ME | LİKGAZİ MH.AŞI MAİ | IK VEYSEL B TEL :0352 3 L:ÍNFO@ZE | UL.BARIŞMANO 33 55 44 MTEST.COM | HİZMET LTD STİ. 50 KONAĞI NO:4 | /A | - | T, B | C. EVRE V AKANL | E SEHIRO | SILIK | |
|---------------------------------------|-----------------|--------------------------------|------------------|-----------------------|---|---------------------------------------|-----------------------------------|------------|----------|----------------|-----------------------|------------|---|---|
| 1 | | LA | BORATUVA | R DENEY | LERI TO | PLU SON | UÇ RAPOR | FORMU | | | | | | |
| | Yüklenici Firmə | ADER MÜHENDISLIK | | | | | | | Sayfa No | | | 1/1 | | |
| | | NIĞDE İLİ MRKZ. İLÇ. YAĞDAN MH | 2507 ADA 9 PARSE | L | | | | | | e Geliş Tarihi | | 14.01.2017 | and the second se | |
| | | 1990-17 | | | | | | | Rapor T | | | 18.01.2017 | | |
| | | | | | | | | | Bakanlı | k Rapor No | CBR | 11099282 | Direkt Kesme | |
| | Numuna | Doğal Su Atterberg Limitleri | Elek Analizi | Zemin | Ort.Dbha | Serbest Basing | Oç Eksenli (UU) / (CU) | Hidrometre | Bha | Proktor | 2.5 mm | Özgül | c | + |

/ (CU) Deneyi(qu) -0,075 0,002 Sinfi Sondaj İçeriği Ort.Is (50) içsel Kohezyor Kgt/cm2 Ykmax (g/cm³) - 200 % 44 Yn (gr/cm³) ¢ Derec 96 96 (g/cm^s) Wopt (%) sürtün USCS (Kg/cm2) kg/cm2 C Kgflcm2 Kuyu No: Tipl ve Ads Derinlik (m-m) (%) LL (%) PL: (%) PI (%) Kalan (%) Geçen (%) acisi -9,8 2,25 ---1,00-1,50 --..... SK-1 CR ---11,0 2,29 --. --~ SK-2 CR 1,00-1,50 ---*R FR 19 Yayın Tar: 03.12.2015 Revizyon No/Tar: 00

*Bu deney formu izinsiz hiçbir şekilde çoğaltılıp kopya edilemez.

*Söz konusu deney sonuçları,sadece test edilen deney numunelerine aittir

*Tüm hakları Zemtest Zemin Araştırma ve Lab.Hiz Ltd. Şti.'ye aittir.

.* Laboratuvarımız 4708 sayılı kanun gereği T.C.Çevre ve Şehircilik Bak. tarafından verilen 02.03.016 tarih ve 539 No'lu laboratuvar izin belgesine sahiptir.

Deneyi Yapan Serbat DAYSAL (jeo Müh) Oda Sicil No.14982

5

ZEMTEST ZEMIN ARAŞTIRMA VE LABORATUVAR HIZMET LTD. ŞTİ. Melikgazi Mir Aşıkveysel Bulvan Banş Março Konağı No' 4/A Melikgazi/KAYSERİ Erciyas X.D./997 070 8501 Mersis No: 01/42063064600013

Katural OZMENTOOLAN



201 100

ZEMTEST ZEMİN ARASTIRMA VE LABORATUVAR HİZMET LTD STİ. ADRES:MELİKGAZİ MH.AŞIK VEYSEL BUL.BARIŞMANÇO KONAĞI NO:4/A TEL :0352 333 55 44 MAİL:İNFO@ZEMTEST.COM

T.C. CEVRE VE ŞEHİRCİLİK BAKANLIĞI

LABORATUVAR DENEYLERI TOPLU SONUÇ RAPOR FORMU Yüklenici Firma ADER MÜHENDÍSLÍK Sayfa No 1/1 Proje Adı NIGDE ILI MRKZ. ILÇ. YENICE MH. 148 ADA 426 PARSEL Numune Geliş Tarihi 22.03.2017 Rapor No 2600-17 Rapor Tarihi 27.03.2017 Bakanlık Rapor No 12233978 CBR Direkt Kesme Doğal Su İçeriği Konsolidasv Zemin Smith Serbest Basing Deneyl(qu) Oç Eksenli (UU) / (CU) Sondaj Numune Atterberg Limitleri Elek Analizi Ort.Dbha Bha Prokto Ort.Is (50) 2.5 mm Özgül ağırlık sisme şişme ba: c ф lçsel - 20 Kuyu No: Tipi ve Adı Derintik (m-m) Yn (gr/cm*) Ykmax (g/cm²) Kohezyon Kgt/cm2 Kalan (%) Geçer (%) (Kg/cm2) ф (%) LL (%) PL (%) PI (%) USCS kg/cm2 C Kgffer Wopt (%) % 96 (g/cm Jerec actst SK-1 CR 0,50-1,00 2,26 . ---10,5 SK-2 CR 1,00-2,00 11,4 2,28 -------SK-3 CR 0,50-1,00 10,1 2,25 SK-4 CR 0,50-1,00 ---10,3 2,26 *R FR 19 Yayın Tar: 03.12.2015 Revizyon No/Tar: 00 *Bu deney formu izinsiz hiçbir şekilde çoğaltılıp kopya edilemez. *Söz konusu deney sonuçları,sadece test ed!len deney numunelerine aittir

*Tüm hakları Zemtest Zemin Araştırmə ve Lab.Hiz Ltd. Şti.'ye aittir.

.* Laboratuvarımız 4708 sayılı kanun gereği T.C.Çevre ve Şehircilik Bak, tərəfindan verilen 02.03.016 tarih ve 539 No'lu laboratuvar izin belgesine sahiptir,

-Deneyj Yapan DAVSAL (GROWTCH)

ZEMTEST ZEMIN ARAŞTIRMA VE LABORATUVAR'HIZMET LTD. STI. Melikgezi MM Aşıkveysel Bulvan Banş Manço Konağı NG AlA Melikgezi/KAVSERİ Erolysev 201997 070 8501 Mersis No: 01/2063064600013

| | X O | m e W | | | | HIZ. Fevzi | Cakmal | K Mah. 1 | 0569 Sk. | No:34 K 342 41 4 | aratay / KC | SII. NYA | | | | | T.C. SEHIRCILIK BAKANLIĞI | |
|-------------------------|----------------|-----------|------------------------------|--|--------------------|----------------------|-----------|-----------|-----------|---------------------|----------------------------------|---|-------------------------|-------------------------|-----------------------------|----|---------------------------------|-------------------------|
| | | | avan | | | | | | | | | | | Numune | | hi | 11.03.2017 | |
| | BİLGİLE | | HAKAN MÜH | END TO TH | | | | | | | | | | Deney Ba | | | 11.03.2017 | |
| BAŞVU | RU SAHİ | | | | / | | | | | | | | | Kayıt Nu | | | K17-451-Z | |
| YAPI S | | | ZEYNEP ÖZD | DEM ERTUR | ACDICEZ / P | ITCDE | | | | | | | | Rapor Ta | | | 13.03.2017 | |
| | IN ADRE | | AHMETPINA | | IERKEZ / I | NIGDE | | - | | | | | | Rapor Nu | imarasi | | R17-451-Z | |
| PAFTA, | ADA/PA | RSEL | 1488 ADA / | LU DEN | EV CO | NUCL | DTP | APOR | 211 | | | | | Bakanlık | Rap. No | | 12148103 | |
| | Numune | | TOP | Doğal | | Analizi | 1 | rberg Lin | ····· | | Nokta | ÜÇ Eks Basınç | | Konsol | idasyon | | Direkt Kesn | ne Deneyi |
| Sondaj Kuyusu Adı | Tipi ve Adı | Derinlik | Doğal Su Muhtevası (%) | Birim Hacim Ağırlık (gr/cm ³) | #4 Kalan (%) | #200 Geçen (%) | LL (%) | PL (%) | PI (%) | USCS | Yükleme Dayanımı (kgf/cm2) | * C _{up} (kgf/cm ²) | *f _{up} (°) | Şişme Yüzdesi (%) | Şişme Basıncı (kN/m²) | Gs | * c _{up} (kgf/cm²) | *f _{up} (°) |
| | MARGT | 1 50 5 00 | | | 1.07 | | | | | | 10,22 | | | | <i>i</i> | | | |
| SK-1 | KAROT | 1,50-5,00 | | | | | | | | | 11,45 | | | | | | | |
| SK-2 | KARUT | 1,50-5,00 | | | | | | | | | | | | | | | 1 | |
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Not ve

303896.755 ··· #889388

* Kullanılan Standartlar: TS - 1900-1 , TS - 1900-2 ve TS 1500

* Laboratuvanımız Çevre ve Şehircilik Bakanlığının 11.04.2011 tarih vo 273 sayılı"Laboratuvar İzin Belgesi'ne sahiptir. Bu rapor, sadece deneyi yapılan numune için geçerlidir. Numunenin alındığı yere alt bilgiler müşteriye ait olup, laboratuvarmuzn izni olmaksızın değiştirilemez ve kısınen çoğaltılamaz. Yapının güvenilirliğine yönellik tek başına bir fikir vermez.
 LABORATUVAR DENETÇİSİ
 DENEYİ YAPAN

Umur DOĞAN Jeoloji Münendisi

Bekir AKARSU Jeoloji Yük. Müth. Benergi Beige No: 10350

| | | L | ` | () () | <u> </u> | <u> </u> |
|------------------|--|--------------------|--|--------------------------------|----------|----------|
| ROAL | KONEVÍ YAPI-ZEMÍN LABORATUVA HÍZ. MÜH. MAD. SAN. VE TÍC. LTD. Ş Fevzi Çakmak Mah. 10569 Sk. No:34 Karatay / KONY. Tel/Faks: (0 332) 342 41 40 | TÎ. 4 . | L | Va gertiseli te Bateani iga | * | |
| YAPI BİLGİLERİ | | | Geliş Tarihi | 09.09.2016 | | |
| BAŞVURU SAHİBİ | HAKAN MÜHENDİSLİK | Deney Ba | | 09.09.2016 | | |
| YAPI SAHİBİ | SALÍHLER ÍNŞAAT | Kayıt Nu | and the second sec | K16-1659-Z | | |
| YAPININ ADRESI | YAĞDAN MAH. / MERKEZ / NIĞDE | Rapor Ta | | 10.09.2016 | | |
| PAFTA/ADA/PARSEL | 85 / 42 / 23 | Rapor Nu | imarasi | R16-1659-Z | | |
| PATTA/ADA/TARGEL | TOPLU DENEY SONUÇLARI RAPORU | Bakanlık | Rap. No | 11164894 | | |
| Nomune | | Üç Eksenli Konsoli | daguan | Direkt Kesme Deneyi | | |

| | Nomune | | Doğal Su | Doğal Birim | Elek | Analizi | Atte | rberg Lin | itleri | | Nokta | Üç Eka Basınç | | Konsol | Idasyon | | Direkt Kesm | te Deney |
|-------------------------|----------------|-----------|------------------|---|--------------------|----------------------|-----------|-----------|-----------|------|-----------------------------------|---|-------------|--------------------------|-----------------------------|----|---|-------------------------|
| Sondaj Kuyusu Adı | Tipi ve Adı | Derinlik | Muhbevası (%) | Hacim Ağırlık (gr/cm ³) | #4 Kalan (%) | #200 Geçen (%) | LL (%) | PL (%) | PI (%) | USCS | Yiikleme Dayanımı (kgf/cm2) | * C _{up} (kgf/cm ²) | *fup (°) | Şişme Ylizdesi (%) | Şişme Basıncı (kN/m²) | Gs | * c _{up} (kgf/cm ²) | *f _{up} (°) |
| SK-1 | UD | 1,00-1,50 | (4,61/ | (1,83) | 2,25 | 15,92 | | NP | | SM | | | | | | | 0,0992 | 25,8 |
| SK-1 | SPT | 3,50-3,95 | 3,28 | 1,82 | 3,13 | 14,60 | | NP | | SM | | | | | | | | |
| SK-2 | UD | 1,00-1,50 | 5,96 | 1,84 | 2,53 | 17,41 | | NP | | SM | | | | | | | 0,1114 | 26,2 |
| SK-2 | SPT | 3,50-3,95 | 3,15 | 1,84 | 3,75 | 16,94 | | NP | | SM | | | | | | | | |
| SK-3 | UD | 1,00-1,50 | 4,05 | 1,83 | 3,17 | 15,72 | | NP | | SM | | | | | | | 0,1053 | 26,3 |
| SK-3 | SPT | 3,50-3,95 | 3,26 | 1,83 | 2,80 | 14,74 | | NP | | SM | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | L | |

Not ye Aciklamalar:

* Kulianian Standartlar: TS - 1900-1 , TS - 1900-2 ve TS 1500

* Laboratuvarınız Çevre ve Şebireilik Bakanlığının 11.04.2011 tarih ve 273 sayılı*Laboratuva İzin Belgesi'ne sahiptir.

* Laboratuvarnnuz (czre vo Schirolik Bakaulginn 11,04,201) tazih vo 273 sayari Laboratuvar izm Betges ne sangur. * Bu rapor, sadece deneyj yapılan nanune için geçetidir. Nanuncina alındığı yere ait bilgiler müşteriye ak olup, laboratuvarnızın izmi olmaksızın değişirilemez ve kısmen çoğalınlamaz, Yapının gövenlirtiğine yönelik, tek başına bir fildr vennez. LABORATUVAR DENETÇİSİ

YARADEN Mainney

Bekir AKARSU Jeoloji Yak Müh. Denetçi Belge No: 10360



| | | | | | e | | | <u>م</u> | <u>.</u> | 1 I | | 5 | - | | | | | |
|-------------------------|----------------|----------|------------------|---|-------------|----------------------|---------|-----------|-----------|-----------|-----------------------|---|-------------------------|----------------|---------------------------------|-----|------------------------------|-----------|
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| | | | 1 2 ml | | | KOI | VEVI | YAPI | ZEMİ | N LAB | ORATU | VAR | | / | | | Link | |
| and a second | Color Store | | | | | HIZ. | MÜH. | . MAC | . SAN | . VE T | C. LTD. | SIL. | | | | | THE WE SELIDOL | c. |
| 0000 | (新建等)(引 | | | | | Fevz | i Çakma | k Mah. 1 | L0569 Sk | . No:34 P | atay / KC | JNYA | | | | | CEVRE VE SEHIRCIL BAKANLI | iði |
| Va | IK O | D m & | Boratuva | -1 | | | 1 | el/Faks: | (0 332) | 342 41 4 | 0 | ×. | | | | L | | |
| 1 | | | | | | | | | | | | | | Numune | Geliş Tar | ihi | 16.05.2016 | |
| API | BILGILE | RI | 1 9 9 | | | | | | | | | | | Deney Ba | aş. Tarihi | | 16.05.2016 | |
| 3AŞVU | RU SAHİ | BÎ | DAĞOĞLU M | | K | | | | | | | | | Kayit Nu | | | K16-963-Z | |
| | AHİBİ | | HARUN DİK | | | - | | | | | | | | Rapor Ta | rihi | | 18.05.2016 | |
| | IN ADRE | | KAYARDI MA | | Z / NIGD | E | | | | | | | | Rapor Nu | umarası | | R16-963-Z | |
| PAFTA | /ADA/PA | RSEL | 112 ADA / 9 | PARSEL | | | TOT D | ADOD | 211 | | | | | Bakanlık | | | 10451371 | |
| | | | TOP | LU DEN | IEY SC | NUÇL | AKIR | APOP | | | | | | 1 | | T | | |
| | Numune | | 1 | Doğal | Elek | Analizi | Atte | rberg Lin | nitleri | | Nokta | Üç Eks Basınç | | Konsoli | idasyon | | Direkt Kesm | ne Deneyi |
| | | | Doğal Su | Birim | | | | | | USCS | Yükleme | | | Sisme | Şişme | Gs | * C | *fup |
| Sondaj Kuyusu Adı | Tipi ve Adı | Derinlik | Muhtevası (%) | Hacim Ağırlık (gr/cm ³) | #4 Kalan | #200 Geçen (%) | (%) | PL (%) | PI (%) | 0.000 | Dayanımı (kgf/cm2) | * c _{up} (kgf/cm ²) | *f _{up} (°) | Yüzdesi (%) | Basinci (kN/m ²) | | (kgf/cm ²) | (°) |
| - sale | | | | | (%) | | 43 | 23 | 20 | CL | | | | | | | 0,6108 | 10,1 |
| AC-1 | TORBA | 1,00 | 12,53 | 1,90 | 0,00 | 85,51 86,55 | 43 | 25 | 19 | CL | | | | | | | 0,6184 | 10,2 |
| | TORBA | 1,00 | 13,62 | 1,91 | 1 (1)(1) | 66.00 | 1 44 | 23 | 1.2 | | | | | | i | | | |

Not ve Acıklamalar:

* Kullanılan Standartlar: TS - 1900-1 , TS - 1900-2 ve TS 1500

* Laboratuvarımız Çevre ve Şehircilik Bakanlığının 11.04.2011 tarih ve 273 sayılı"Laboratuvar İzin Belgesi"ne sahiptir.

| PAFTA/ADA/PARSEL 85 | HMETPINARI MH / NİČ 53 ADA / 1 PARSEL TOPLU DEN Doğal Su Birim | | | | | | | | | | Kayıt Nur Rapor Ta | | | K13-767-Z 04.07.2013 | |
|---|---|----------------------------------|--------------------------------------|--------------|---------------------------|----------------|--------------|----------------------------------|--|-------------------------|--|-----------------------------|---------------------|--|-------------------------|
| Numuse Sondaj Kuyusu Adi Derinlik | TOPLU DEN Doğal Su Birim | IEY SO | | | | | | | | | Rapor Nu | marası | | R13-767-Z | |
| Sondaj Kuyusu Adı Derinlik | Doğal Su Birim | | NUÇLA | | APOR | RU | | | | | Bakanlık | Rap. No | | 4647840 | _ |
| Sondaj Tipi ve Kuyusu Adı Derinlik M | | Elek | Analizi | | rberg Lin | | | Nokta | Üç Eks Basınç | | Konsoli | dasyon | | Direkt Kesm | e Dene |
| | Muhtevası Hacim (%) Ağırlık (gr/cm ³) | #4 Kalan (%) | #200 Geçen (%) | LL (%) | PL (%) | PI (%) | USCS | Yükleme Dayanımı (kgf/cm2) | * c _{up} (kg/cm ²) | *f _{up} (°) | Şişme Yüzdesi (%) | Şişme Basıncı (kN/m²) | Gs | * c _{up} (kg/cm ²) | *f _{op} (°) |
| SK-1 KAROT 3,50 | | | | | | | | 7,62 9,28 | | | | | | | |
| SK-2 KAROT 3,50 | | | | | | | | 8,44 | | | | | | | |
| SK-3 KAROT 3,50 | | | | | | | | - 6/11 | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | 1 | | | | _ |
| Not ve Acuklamalari * Kullanulan Standartlar: TS - 1900-1, TS - Laboratuvarımız Çevre ve Şehircilik Baka * Bu rapor, sadeco deneyi yapılan yerler içir DENEYÎ Y JEOFIZİK M | anhğının 11.04.2011 tarih ve in geçerlidir. Numunenin alm YAPAN | 273 sayılı"Lı dığı yere ait b | aboratuvar İzin Dilgiler müşteriy | a Belgesi"ne | e sahiptir. Jaboratuva | ermizin izni c | lmaksızın de | giştirilemez ve k | usmen çoğaltıla | Bek | in güvenilirliğine BORATUVA ÎF' AKA Dioji Yük, M Şi Bolge No | PCII | şına bir fik İSİ | ir vennez. | |

| | MEK | | RATUV | ARI | | | А | ZEMTES DRES:MI | ELİKGAZ | zi MH.AŞII T | K VEYSEL | LABORATUVAR BUL.BARIŞMAN 333 55 44 EMTEST.COM | HİZMET IÇO KONA | <u>LTD STİ</u> (ĞI NO:4 | <u>.</u> \$/A | | | | T.C ÇE | | ŞEHİF | RCILIK | |
|--------------------|------------------|--|------------------------|------------|-----------|-----------|----------------|-------------------|-----------------|-----------------|-----------------------|---|--------------------|----------------------------|------------------|-----------|----------|------------|------------------|--------|----------|---------------------|-------------------|
| | | | | | | | | | | | | | | | | | | | ВА | KANLI | 31 | | |
| | | | | | | L/ | ABOR | ATUV | AR D | ENEYL | ERI T | OPLU SON | NUÇ R | APOF | R FOI | RMU | Sayfa No | | | | 1/1 | | |
| üklenic | Firma | | ADER MÜ | | | | | | | | | | | | | | | e Geliş Ta | rihi | | 22.07.20 | 016 | |
| roje Ad | | | NİĞDE İLİ I 0754-16 | MRKZ IL | Ç. AHME | TPINARI | MH 3019 | ADA 5 PA | RSEL | | + | | | | | | Rapor Ta | arihl | | | 10.10.20 | 016 | _ |
| apor No | | | 0/54-16 | | | | | | | | | | | | | | Bakanlık | RaporN | 0 | CBR | 113193 | 03 Direkt I | Kesme |
| Sondaj | | Numune | Doğal Su | Atte | rberg Lim | itleri | Elek A | Analizi | Zemin Stnift | Ort.1s (50) | Ort.Dbha | Serbest Basing Dencyl(qu) | Üç Ekser /(C | nli (UU) U) | | sisme bas | Bha | Pro | ktor | 2.5 mm | Özgül | c | \$ |
| | | | İçeriği | | 1 1 | | +4 | - 200 | | (Kg/cm2) | Yn | kg/cm2 | C Kgt/cm2 | ¢ Derece | % | | (g/cm*) | Wopt (%) | Ykmax (g/cm²) | % | ağırlık | Kohezyon Kgt/cm2 | içsel sürtünme |
| Kuyu No: | Tipi va Adı | Derinlik (m-m) | (%) | | - | PI (%) | Kalan (%) | Geçen (%) | USCS | | (gr/cm ²) | | | Derece - | | | - | - | - | | - | 0,117 | 23 |
| SK-1 | UD | 3,50-4,00 | (15,5_ | NP | NP | NP | 0,70 | 37,20 | SM SM | | 1,73 1,75 | | | | | - | - | - | - | - | - | - | - |
| SK-1 | SPT | 4,50-4,95 | 23,1 | NP | NP | NP | 22,80 27,90 | 37,40 32,30 | SM | | 1,75 | - | | - | - | - | - | - | - | - | - | - | - |
| SK-1 SK-1 | SPT SPT | 6,00-6,45 7,50-7,95 | 25,8 | 39,9 | 22,6 | 17,3 | 32,80 | 53,10 | CL | - | 1,87 | - | - | - | - | - | - | | - | - | - | | - |
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| SK-2 | UD | 3,50-4,00 | 14,3 | NP | NP | NP | 12,00 | 32,80 | SM | - | 1,74 1,78 | | | | - | | - | | - | - | - | 0,105 | 23 |
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| SK | <-1 | UD-1 | 3,00 | | 21,2 | | 17,86 | 14,74 | 4,2 | 54,0 | 36,1 | 19,0 | 17,1 | CL | | | | | 0,55 | 5 | | |
| SK | K-2 | UD-1 | 3,00 | | 15,6 | | 18,43 | 15,95 | 8,1 | 44,7 | 41,7 | 20,8 | 20,9 | SC | | | 0,274 | 11 | | | | |
| SK | K-3 | UD-1 | 3,00 | | 21,9 | | 18,12 | 14,86 | 4,6 | 54,9 | 47,7 | 24,3 | 23,4 | CL | | | | | 0,63 | 7 | | |
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| SM | K-5 | UD-1 | 3,00 | | 19,5 | | 18,01 | 15,07 | 0,0 | 88,2 | 45,3 | 20,5 | 24,8 | CL | | | | | 0,54 | 7. | | |
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*Söz könüst deney sonuçlar. exerce test edilen deney numunelerine aittir. *Deney sonuçlar kaboratuvarımızın izni olmadan kışırınen kopyalanamaz ve çoğaltılamaz. *Laboratuvarımız 4708 Sayılı Kanun Gereği Bayındırlık ve İskan Bakanlığı Yapı İşleri Genel Müdürlüğü tarafından verilen 17/10/2003 tarih ve 67 No' lu Laboratuvar İzin Belgesine Sahiptir.

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| | | e(Sample | | | Jacim (2m3) | ANA | EK LİZİ NALYSIS) | L | ITARBEI İMİTLEI ERBERG LI | al a | RMA | LEME /cm ²) | sinç | Uç El Basınç TRIA COMPRES | XIAL | DIRECT | Kutusu neyi shear | Konsol (CONSO | lidasyon Lidatoin) | ETRE ER |
| Гірі Гуре | Sondaj No: Boring No: | Derinlik Depth(m) | | Doğal Su İçeriği: (Wn)(%) | Doğal Birim Hacim Ağırlık (gr/cm3) | +4" | -200" | LL (%) | PL (%) | PI (%) | SINIFLANDIRMA (USCS) | NOKTA YÜKLEME İNDEKŞİ (kg/cm²) | Serbest Basınç Deneyi(qu) (kgf/cm²) | C Kgf/cm ² | Derece | C Kgf/cm ² | ф Derece | Şişmə Basıncı | Şişmə Yüzdesi(%) | HIDROMETRE |
| UD | SK-1 | 3,00-3,50 | N-1 | 15,5 | 1,62 | 0,00 | 38,50 | NP | NP | NP | SM | - | - | - 2 - | | 0,320 | 16 | - | - | - |
| SPT | SK-1 | 4,50-4,95 | N-2 | 27,5 | 1,83 | 0,00 | 55,70 | 37,9 | 21,6 | 16,3 | CL | | - | | | Same . | - | | - | - |
| SPT | SK-1 | 6,00-6,45 | | 21,1 | 1,65 | 3,80 | 44,20 | NP | NP | NP | SM | - | - | | - | - | | | · · | |
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| UD · | SK-2 | 3,00-3,50 | | 16,6 | 1,59 | 0,60 | 33,20 | NP | NP | NP | SM | | | - | - | 0,290 | 14 | | | |
| SPT | SK-2 | 7,50-7,95 | | 14,7 | 1,62 | 13,20 | /32,60 | NP | NP | NP | SM | - | | | | 0,275 | 14 | 1 | - | |
| UD | SK-3 | 3,00-3,50 | | 16,8 | 1,58 | 0,00 | 33,50 | NP | NP | NP | SM | - | | | - | 0,210 | 14 | | | |
| SPT | SK-3 | 7,50-7,95 | | 15,5 | 1,63 | 15,80 | 32,20 36,70 | NP | NP NP | NP | SM . SM | | | - | | 0.293 | 15 | | | |
| UD | SK-4 SK-4 | 3,00-3,50 | | 17,2 | 1,61 | 0,00 | 23,40 | NP | NP | NP | SM | | | | - | - | | - | - 1 | - |
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| Kuyu | Tipl ve | Derinlik | (%) | LL (%) | PL (%) PI (%) | +4 Kalan | - 200 Geçen | USCS | (Kg/cm2) | Yn (gr/cm*) | kg/cm2 | C Kgffem2 | ¢ Derece | % | 56 | (g/cm²) | Wopt (%) | Ykmax (g/cm³) | % | agiriik | Kohezyon Kgt/cm2 | içsel sürtünme acisi |
| No: SK-1 | Adı CR | (m-m) 0,50-1,50 | - | - | | (%) | (%) | - | 9,8 | (gr/em-) 2,25 | - | - | - | - | - | - | - | - | - | - | - | - |
| SK-2 | CR | 0,50-1,50 | - | - | | - | - | - | 10,2 | 2,27 | - | | - | - | - | | | - 0 | - | - | | - |
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| *Tüm hə .* Labor | Bene Bene Bene | y sonuçları,sadec est Zemin Araştır 4708 sayılı kanur 201 Yapan 4546 (jeo Müh 11 NO:14982 | rma ve Lab. n geraği T.C | Hizltd | Stil 've alttir. | | dan veriler | 02.03.0 | 16 tarih v | e 539 No' | lu laboratuvar izl | n belgesine | sahipt | tir. | | | | | Kalensi | OZKAL BATER | No:1965 | 1000) |
| Amger syllighter | Süvovida Alervo Ov | ASLI GIBID | | | | | | * . | ZEMT VE LAE | EST Z SORATL | EMIN ARA NAR HIZME I Agikveysel V.D /987 070 1 01/420630644 | STIRM | A ri. | | | | | | | | | |



SAFIR İŞ.GÜV.DAN.İNS.TAAH.TEST.LAB.LTD.STİ ADRES:Yıldırım Beyazıt Mah.Konaklar Cad.No.12/E Kocasinan/KAYSERİ TEL:0(352) 240 56 36 M:info@safirlab.com W: www.safirlaboratuvari.com



| füklenici | Firma | | ADER MÜHEND | | | | | | | | | | | | | | | | L.I.B.I | N No: | | 1 | 2.07.2013 | 441 |
|-------------|----------------|-------------------|--|-----------|----------|---------|---------------------|----------------------|-----------------|-------------|----------------|-------------------------|-----------------------------|-------------------|-------------|--------|--------|---------|---------------------|----------|--------|---------|---------------------|---------------------------|
| roje Adı | | | NIĞDE İLİ MRKZ | Z. ILÇ. A | HMET | PINARI | MH.125 | ADA 130 | PARSEL | | | | | · . | | | | Denev | Standarth | arı | | TS 1500 |) / TS 1900- | 1/2 |
| Rapor No | > | | Z171315 | | | | | | | | | | | | | | | Sayfa N | | | | 1/1 | | |
| Rapor Ta | rihi | | 23.11.2015 | | | - | | | | | | - | | | | Hidron | | | | ktor | CBR | | Direkt | Kesme |
| Sondaj | | Numune | Doğal Su İçeriği | Atter | berg Lin | nitteri | Elek A | Analizi | Zemin Sınıfı | Ort.Is (50) | Ort.Dbha | Konsol | idasyon | Oç Ekser / (Ci | | | -0,002 | Bha | Standart Proktor | Modifiye | 2.5 mm | Özgül | c | ¢ |
| Kuyu No: | Tipi ve Adı | Derinlik (m-m) | (%) | LL (%) | PL (%) | PI (%) | #10 Kalan (%) | #200 Geçen (%) | USCS | (kg(cm2) | ¥n (gr/cm*) | Şişme Yüzdesi (%) | Şişme Basıncı (kN/m2) | C Kgf/cm2 | ф Derece | * | % | (g/cm²) | % | g/cm* | % | aginik | Kohezyon Kgf/cm2 | içsel sürtünm açısı |
| AÇ-1 | BLOK | 0,80-1,20 | - | - | - | - | - | - | - | 9,6 | 2,20 | - | - | - | | - | - | - | - | - | - | - | | |
| | BLOK | 0,80-1,20 | · · | - | - | - | - | - | - | 10,9 | 2,22 | - | - | - | - | - | - | - | | - | - | - | - | - |
| Söz ko | nusu de | ney sonuçları, | şekilde çoğaltı adece test edi AN.İNŞ.TAAH.T | len der | ney nu | munel | erine ait | tir | | | | | | | | | | | | | | | | |

Defront fron Misercar Construction Parsfill NO:23944

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SAPIR VAPS ZEMIN I COV. DAN. US- HAN. (EST LABLID. ST. Michard Buy 2003: 45 Melikgaz/KAYSERI Tat (0.352) 2403: 45 Melikgaz/KAYSERI ECTYES VD. 737 050 2932 Mersis No: 2338431387115636

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ZEMİN MEKANİĞİ LABORATUVARI

2 2 2 2 2 2 3 3 3 3 1 4 E 0 . ZEMTEST ZEMİN ARAŞTIRMA VE LABORATUVAR HİZMET LTD ŞTİ. ADRES:MELİKGAZİ MH.AŞIK VEYSEL BUL.BARIŞMANÇO KONAĞI NO:4/A TEL :0352 333 55 44 MAIL:INFO@ZEMTEST.COM

C. C. CEVRE VE SEHIRCILIK

Köksal Özhlen Denerri Müh) Belge No:19653

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| | | | ADER MÜ | ur un la | luc. | | 0010 | | | | | | | | 1 | | Sayfa No | D | | | 1/1 | - | |
| Yüklenici | | | | | | | | | | | | | | | | | Numune | e Geliş Tar | rihi | | 18.11.2 | 017 | |
| Proje Adı | | | NIGDE ILI I | MRKZ. IL | Ç. TEPE | MH. 89 | ADA 217 | PARSEL | | | | | | | | | Rapor Ta | arihi | | | 19.12.2 | 017 | |
| Rapor No | | 1.001 | 5379-17 | | | | | | | | | | | | | | | Rapor N | 0 | | 139581 | .83 | |
| | | | - | | | | | | | | | Serbest Basing | Üc Ekser | | Hidro | metre | | | | CBR | | Direkt | Kesme |
| Sondaj | | Numune | Doğal Su İçeriği | Atte | rberg Lim | itleri | Elek / | Analizi | Zemin Sınıfı | Ort.Is (50) | Ort.Dbha | Deneyi(qu) | / (C | | -0,075 | -0,002 | Bha | Prol | ktor | 2.5 mm | Özgül | c | ф |
| Kuyu No: | Tipi ve Adı | Derinlik (m-m) | (%) | LL (%) | PL (%) | PI (%) | +4 Kalan (%) | - 200 Gegen (%) | USCS | (Kg/cm2) | ¥n (gr/cm³) | kg/cm2 | C Kgf/cm2 | ф Derece | % | % | (g/cm³) | Wopt (%) | Ykmax (g/cm³) | % | ağırlık | Kohezyon Kgf/cm2 | içsel sürtünme açısı |
| | CR | 2,00-3,00 | - | | - | - | | - | - | _10,4 | 2,23 | - | | - | - | | - | 14 | - | - | ~ | | - |
| SK-1 | | | | | | | | | 1.00 | 10,6 | 2,24 | - | - | 10 | - | - | | - | - | 10 | - | - | - |
| SK-2 | CR | 2,00-3,00 | - | - | - | | | | | | 2,24 | | - | ~ | - | - | - | - | - | - | - | | - |
| SK-3 | CR | 2,50-3,50 | - | - | - | - | - | - | | 10,8 | | | | | | | | | - | - | | - | - |
| SK-4 | CR | 2,50-3,50 | - | - | -2 | - | - | - | - | 10,9 | 2,25 | - | - | - | - | - | | | | | | | |
| *R FR 19 | Yayın Ta | r: 03.12.2015 Rev | izyon No/Ta | ar: 00 | | | | | | | | | | | | | | | | | | | |

*Bu deney formu izinsiz hiçbir şekilde çoğaltılıp kopya edilemez.

*Söz konusu deney sonuçları, sadece test edilen deney numunelerine aittir

*Tüm hakları Zemtest Zemin Araştırma ve Lab.Hiz Ltd. Şti.'ye aittir.

.* Laboratuvarımız 4708 sayılı kanun gereği T.C.Çevre ve Şehircilik Bak. tarafından verilen 02.03.016 tarih ve 539 No'lu laboratuvar izin belgesine sahiptir.

Yapan LEG WIC da Sicil NO:14982



| | | RATUV | ARI | | | | ZEMT ADRES:N | <u>est zen</u> Aelikg/ | ZI MH.A | SIK VEYSE TEL :035 | <u>E LABORATUV</u> L BUL.BARIŞM/ 2 333 55 44 ZEMTEST.COM | ANÇO KO | <u>ET LŤD</u> NAĞI N | <u>sti.</u> 10:4/A | | | | T.C CE B/ | | E ŞEH | IRCILIK | - |
|---|---|---|--------------------------------|----------------------|----------------------|-------------|-----------------|---------------------------|--------------|-------------------------|---|----------------|-------------------------|-----------------------|------------|----------------------|--------------------|-------------------|----------|---------|--|-------------------|
| | | · | | | L | ABO | RATU | ARI | DENEY | LERI | TOPLU SC | NUÇ I | RAPO | DR FO | RMU | | | · | | | <u> </u> | |
| Yüklenici Firm Proje Adı | a | ADER MÜ NÍĞDE ÍLÍ | | | LANL CT | | ADADCE | | | | · | | | | | Sayfa N | o e Geliş Ta | ribi | | 1/1 | 2017 | |
| Rapor No | | 3055-17 | WIRK6.9 | AHINAL | 1 IVIPI. 07 | ADA I. | 24 PARSEL | | | | | | | | | Rapor T | arihi | | | 10.05. | 2017 | |
| | x | | , i | | | | | | | | | | | 1 | lidasyon | Bakanlıl | k Rapor N | 10 | CBR | 125223 | | Kesme |
| Sondaj | Numune | Doğal Su İçeriği | Atte | orberg Lin | nitleri | Elek | Analizi | Zemin Sinfi | Ortis (60) | Órt.Dbha | Serbest Basing Denbyi(qu) | Oç Ékse /(C | nli (UU) U) | şişme | şişme bas. | Bha | Pro | lator | 2.5 mm | Öźgül | c | • |
| Kuyu Tipi No: As | ve Derintik | (%) | LL (%) | PL (%) | PI (%) | +4 Kalan | - 200 Gecen | USCS | (Kg/em2) | Yn | kd/cm2 | C Kgf/cm2 | d Derèce | 96 | kN/m2 | (g/cm ^a) | Wopt (%) | Ykmax (g/cin*) | 96 | ağırlık | Kohezyon Kat/cm2 | içsel sürtünme |
| SK+1 C | | | - | - | - | . (%) | (%) | - | 10,9 | (gr/cm [*]) . | | - | Derece | - | | - | - | | 1 | | | acts |
| SK-2 C | R 5,00-6,00 | | -, | - | - | | - | - | 11,2 | 2,26 | | | ÷ | - | - | - | - | - | - | | | |
| SK-3 CI | | | | - | - | | · ·- | - | 11,3 | .2,28 | | | + | + | | - | - | - | | - | | |
| SK-4 CI SK-5 CI | | | | | - | | - | | 11,4 | 2,27 | | - | | 1 | | - | | | - | | | - |
| SK-6 CI | | | 1 | - | | | - | - | 10,9 | .2,25 | | | 4 | - | | | - | | - | | | |
| SK=7 C | | - | - | - | - | | - | - | 11,2 | 2,26 | | | - | - | | - | - | - | | - | | |
| SK-8 C | | | | - | | | - | - | 11,3 11,1 | 2,27 | | | + | | | - | | | | | | |
| SK-10 C | | | - 2 | | - | | - | | 11,4 | 2,28 | | - | | · - | | - | - | | | | | |
| SK-11 C | R 5,00-6,00 | | | - | - | - | - | - | 10,9 | 2,26 | | | ÷ | - | | - | - | - | - | | | - |
| SK-12 C | | | | - | -÷- | | - | | 10,9 | .2,27 | | - | 4 | | | - | - | - | | | | |
| SK-13 CI SK-14 CI | | | | - | | | | | 11,2 | 2,29 | | | - | | - | - | - | - | - | | | |
| Bu deney for Söz konusu d Tüm hakları Z | n Tar: 03.12.2015 Rev mu izinsiz hiçbir şekile eney sonuçlari,sadece emtest Zemin Araştır tımız 4708 sayılı kanur | le çoğaltılıp e test edilen ma ve Lab.H | kopya e denéy Hiz Ltd. (| numuna Sti.'ye al | elerine ai ittir. | | n verilen | 02.03.0; | 16 tarih ve | 539 No'li | ı laboratuvar izir | n belgeşine | sahįpti | r. | | | une Deservings = 1 | | | ¥ | | |
| | eneyi Yapan DATSAL Beo Müh Seri NO:14982 |) | | | | | | | | | | | | | | | | ĸ | eleven e | | Vidyan Vidyan Vidyan Vo:19652 | (Клан) |

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ZEMTEST ZEMÍN ARASTIRMA VE LABORATUVAR HÍZMET LTD STÍ. ADRES:MELÍKGAZÍ MH.AŞIK VEYSEL BUL.BARIŞMANÇO KONAĞI NO:4/A TEL :0352 333 55 44 MAÍL:INFO@ZEMTEST.COM

T.C. CEVRE VE SEHIRCILIK BAKARLIGI

Kalenii Ozyfeyran (Mach) Better No 19652 1

| üklenic | í Fírma | | ADER MÜ | HENDIS | LİK | * | | | | | | OPLU SO | | | | | | | | | | | |
|-------------|----------------|-------------------|---------------------|--------|-----------|-----------|-------------|----------------|----------------|-------------|----------|------------------------------|-----------|--------|-------------|-----------|---------|------------|---------|--------|------------------|---------------|------------|
| roje Ad | 1 | | NIĞDE İLİ | MRKZ. | C. YEN | CEMH | 1021 404 | 24 04 000 | -1 | | | | | | | | Sayfa N | | | | 1/1 | | |
| apor No | D | | 2602-17 | | -9.1210 | CE IWITI. | TOPT NDA | 24 PARSE | :L | | | | | | | | Numun | e Geliş Ta | rihi | | 22.03.2 | 017 | |
| | | | | | | | | | _ | | | | | | | | Rapor 1 | arihi | | | 27.03.2 | 017 | |
| | 1 | | - | | | | | | | | | | | | | | Bakanlı | k Rapor N | lo | | 122340 | 29 | |
| Sondaj | | Numune | Doğal Su İçeriği | Atte | rborg Lin | nitieri | Elok | Anallei | Zemin Smrti | Ort.ls (50) | Grt.Dbha | Serbest Basing Denoyi(qu) | Üç Eksel | | | lidasyon | Bha | Pro | ktor | CBR | | Direkt | Kasme |
| Kuyu No: | Tipi ve Adı | Derinlik (m-m) | (%) | LL (%) | PL (%) | PI (%) | +4 Kalan | - 200 Geçen | USCS | (Kg/cm2) | Yn | kg/cm2 | C Kgffem2 | φ | şişme 26 | şişme bas | | | Ykmax | 2.5 mm | Özgül ağırlık | c Kohezyon | d Icsel |
| SK-1 | CR | 1,00-2,00 | | | - | | (%) | (%) | | 10.0 | (gr/cm*) | -ground | CKgweinz | Derece | 76 | | (g/cm*) | Wopt (%) | (g/cm²) | % | | Kgf/cm2 | sürtünn |
| SK-Z | CR | 1,00-2,00 | | | - | | | | | 10,2 | 2,27 | - | | | - | - | - | - | - | - | - | - | - |
| SK-3 | CR | 1,00-2,00 | | | | | | | | 10,8 | 2,29 | | - | - | - | - | | - | - | - | - | - | - |
| SK-4 | CR | 1.00-2.00 | | | | | | | | 11,5 | 2,33 | | - | - | - | - | - | - | - | - | - | - 1 | - |
| FR 19 | Yavin Tai | : 03.12.2015 Revi | TION No/To | - 00 | _ | - 1 | | - | - 1 | 11,1 | 2,31 | - | - | 1.1 | - | - | - | · | - | - | | - | - |

*Söz konusu deney sonuçları,sadece test edilen deney numunelerine aittir

*Tüm hakları Zemtest Zemin Araştırma ve Lab.Hiz Ltd. Şti.'ye aittir.

.* Laboratuvarımız 4708 sayılı kanun gereği T.C.Çevre ve Şehircilik Bak. tarafından verilen 02.03.016 tarih ve 539 No'lu laboratuvar izin belgesine sahiptir.

-Deneyi Yapan Serhat DAYSAL (jeo Muh) Oda Sicil No. 14982

ZEMTEST ZEMIN ARASTIRMA VE LABORATUYAR HIZMET LTD. STI. Melikgazi Min Ashkveysel Bulvan Bans Manoo Konagi NO 4/A Melikgazi KAYSERI Erdyes XD /997 070 8501 Mersis No: 01/22083054500013

1 83 63 ZEMTEST ZEMIN ARASTIRMA VE LABORATUVAR HIZMET LTD STI. ADRES:MELIKGAZI MH.AŞIK VEYSEL BUL.BARIŞMANÇO KONAĞI NO:4/A TEL:0352 333 55 44 ZEMİN MEKANİĞİ LABORATUVARI

T.C. ÇEVRE VE ŞEHİRCİLİK BAKANLIĞİ

| üklenici | Firma | | ADER MU | HENDIS | LİK | | | | | | | | | | | | Sayfa N | 0 | | | 1/1 | | |
|-------------|----------------|-------------------|---------------------|----------|-----------|----------|--------------------|-----------------------|----------------|-------------|----------------|------------------------------|-----------------|-------------|-----------------|--------|---------|-------------|------------------|---------------|---------|---------------------|---------------------------|
| roje Adı | 6 | | NIĞDE ILI | MRKZ. IL | Ç. HIDI | RLIK NIH | 1. 2169 AD | A 18 PAR | SEL | | | | | | 1.1 | | Numun | e Geliş Tar | rihi | | 26.05.2 | 016 | |
| apor No | > | | 0471-16 | | | | | | | | | | | | | | Rapor 1 | arihi | | | 31.05.2 | 016 | |
| | | | | | | | | | | | | | | | | | Bakanlı | k Rapor N | 0 | | 105370 | 14 | |
| Sondaj | | Numune | Doğal Su İçeriği | Atte | rberg Lin | itleri | Elek | Analizi | Zemin Smrti | Ort.ls (50) | Ort.Dbha | Serbest Basinç Deneyi(qu) | Oç Ekse / (C | | Hidro -0,075 | -0,0£2 | Bha | Prol | ktor | CBR 2.5 mm | Özgül | Dire kt | Kesme |
| Kuyu No: | Tipl ve Adı | Derinlik (m-m) | (%) | LL (%) | PL (%) | PI (%) | +4 Kajan (%) | - 200 Geçen (%) | USCS | (Kg/cm2) | Yn (gr/cm²) | kg/cm2 | C Kgf/cm2 | ф Derece | 76 | 96 | (g/cm*) | Wopt (%) | Ykmax (g/cm²) | % | ağırlık | Kohezyon Kgf/cm2 | içsel sürtünn actsi |
| SK-1 | UD | 1,50-2,00 | 12,9 | NP | NP | NP. | 1,90 | 36,40 | SM | - | 1,70 | - | - | - | | - | - | | - | - | - | 0,215 | 21 |
| SK-2 | UD | 1,50-2,00 | 14,2 | NP | NP | NP. | 2,20 | 39,10 | SM | - | 1,72 | - | - | | - | - | - | - | - | - | - | 0,213 | 21 |

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*Söz konusu deney sonuçları, sadece test edilen deney numunelerine aittir

*Tüm hakları Zemtest Zemîn Araştırma ve Lab.Hiz Ltd. Şti.'ye alttir.

ZEN

.* Laboratuvarımız 4708 sayılı kanun gereği T.C.Çevre ve Şehircilik Bak. tarafından verilen 02.03.016 tarih ve 539 No'lu laboratuvar izin belgesine sahiptir.

Denevi Yapan DAYSAL GODACH)



ZEMTEST ZEMÍN ARASTIRMA VE LABORATUÝR (HZMET LTD. STI. - Molikari Mý Agkreyzei Bulvan Bang Mango (om Mý Agkreyzei Bulvar Bang Mango (om Mý Agkreyzei KAYSER) Eryszk Orikaria (horikaria) Manzie No: 01/42063064600013

| | MEKA | NIĞI LABC | RATUV | ARI | | | | | | | TEL :0352 | BUL.BARIŞMA 333 55 44 ZEMTEST.COM | | | | | | | 0 | .C. | VE SEH | RCILIK | |
|-------------|--------------------------------------|--|---------------------|---------|--------------|---------|-------|-----------------------------------|---------|-------------|-----------------------------|---|------------|-------------|-------------|-----------|---------|------------|---------------|---------|---------|-------------------------------|------------------|
| | | | | | | | | | | | | | | | | | | | . 8 | BAKANI | LIGI | | |
| | | | | | | | LA | BORATUV | ARD | ENEY | LERÍ T | OPLU SO | NUÇ R | APO | R FO | RMU | | | | | | | |
| rüklenici | | 200 Barrison (1990) | ADER MÜ | | | | | | | | | | 7 | | | | Sayfa N | | | | 1/1 | | |
| Proje Adı | | | | MRKZ. | ILÇ.ŞAHİ | INALI N | MH. 1 | 520 ADA 1 PARS | EL | | | | | | | | | e Geliş Ta | rihi | | 22.03.2 | | _ |
| Rapor No | | | 2601-17 | | | | | | | | | | | | | | Rapor | k Rapor N | lo | | 27.03.2 | | |
| | | | Doğal Su | | | | T | | Zemin | 1 | | Serbest Basing | Üç Ekse | nii (UU) | Kons | olidasyon | | 1 | | CBR | | Direkt | Kesme |
| Sondaj | N | lumune | Doğal Su İçeriği | A1 | tterberg Lin | nitleri | | Elek Analizi | Sinth | Ort.Is (50) | Ort.Dbha | Deneyi(qu) | /(0 | DU) | şişme | şişme bas | Bha | Pro | ktor | 2.5 mr | n Özgül | c | ¢ |
| Kuyu No: | Tipi ve Adi | Derintik (m-m) | (%) | LL (% | 6) PL (%) | PI (% | 96) | +4 -200 Kalan Geçen (%) (%) | uses | (Kg/cm2) | Yn (gr/cm ³) | kg/cm2 | C Kg#em2 | ¢ Derece | 96 | | (g/cm³) | Wopt (%) | ¥kma (g/cm | × % | agiruk | Kohezyon Kgf/cm2 | lçsel sürtünm |
| SK-1 | CR | 1,00-1,50 | - | - | - | - | | | - | 9,8 | 2,25 | - 1 | - | - | - | - | - | | - | - | - | - | actst |
| SK-2 | CR | 1,00-1,50 03.12.2015 Rev | - 1 | - | 1 - | - | | | - | 10,3 | 2,32 | | - | - | - | | - | - | - | | - | - | - |
| Tüm hal | darı Zemtes | | ma ve Lab.H | Hiz Ltd | d. Şti.'ye a | ittir. | | | 02.03.0 |)16 tarih v | re 539 No' | lu laboratuvar izi | n belgesin | ie sahipti | r. | | | | | | a | | |
| *Tüm hal | darı Zemtes tuvarımız 4 Deneyi | st Zemin Araştıı 1708 sayılı kanu | ma ve Lab.H | Hiz Ltd | d. Şti.'ye a | ittir. | | | 02.03.0 | 916 tarih v | re 539 No' | lu laboratuvar izi | n belgesin | ie sahipti | ir. | | | | | Kelurel | Bolko | Vlavon Vo:19652 | throw a |
| *Tüm hal | darı Zemtes tuvarımız 4 Deneyi | st Zemin Araştıı 1708 sayılı kanu Yapan | ma ve Lab.H | Hiz Ltd | d. Şti.'ye a | ittir. | | | 02.03.0 | 916 tarih v | re 539 No' | lu laboratuvar izi | n belgesin | ie sahipti | ir. | | | | 4 | Kelendi | Bolke | Vayan Nasolota No:19652 | through the |
| *Tüm hal | darı Zemtes tuvarımız 4 Deneyi | st Zemin Araştıı 1708 sayılı kanu Yapan | ma ve Lab.H | Hiz Ltd | d. Şti.'ye a | ittir. | | | 02.03.0 | 916 tarih v | re 539 No' | lu laboratuvar izi | n belgesin | ae sahipti | I r. | | | | 4 | Kulurd | Barko | VI3V90 V7560 V0:19652 | thrown in the |
| *Tüm hal | darı Zemtes tuvarımız 4 Deneyi | st Zemin Areştı 1708 sayılı kanu Yapan Al- (ico yıŭh) No 14982 | ma ve Lab.H | Hiz Ltd | d. Şti.'ye a | ittir. | | | | | | MIN ARAS AR'HIZMET Asikveysel B No. 4/A Meikig D. 997 070 85 01 4206306460 | | | ir. | | | | 4 | Koluci | Burko | Vayan 97500 No:19652 | tham ? |

| | G |) | | - | FARI Ac Tel:C | KIM MÜ Ires:Sal 352 22 | HENDIS | SLİK Mİ Mah.Ota | SO M. YAP k Sk.No 52 2310 | 1 MALZ 39/a K | VE ZEI ocasina | n/KAYS | .LTD.ŞTI ERİ n.com.tr | | • | | | CE | | T.G. BEHIRCİLİK BAKANLIĞI |
|--------------|--------------------------|---------------------|--------------|------------------------------|---------------------------------------|------------------------------|--|--|---|---|---|--|---|---------------------------|----------------|--------------|-------------|---------------------------------|---------------------|---------------------------------|
| Yi | klenici fi | rma : | ADER | MÜHEN | DİSLİK | | | | | | | | | | | | | | | |
| P | roje | : | NİĞDE | Lİ MRK | Z. İLÇ. | YAĞDA | AN MH. | | | RSEL | | | | | | | | | | Sayfa No. 1/1 |
| R | apor Tar | ihi : | 08.04.20 | 013 | | | apor No: | | 3-1794 | PC . | | | Bakanlık | No: Úc El | reanli | Kesme | Kutusu | | | |
| I | Vumun | e(Samp | le) | , iği: | Hacim cm3) | ANA | LEK LİZİ NALYSIS) | L | IMITLEI ERBERG LI | RÍ | RMA | LEME /cm ²) | (n (n | Basinç TRIA COMPRES | Deneyi XIAL | DIRECT | SHEAR | Konso (CONSC | lidasyon | UTRE ER) |
| ʻipi ʻype | Sondaj No: Boring No: | Derinlik Depth(n | | Doğal Su İçeriği: (Wn)(%) | Doğal Birim Hacim Ağırlık (gr/cm3) | +4." | -200" | LL (%) | PL (%) | PI (%) | SINIFLANDIRMA (USCS) | NOKTA YÜKLEME İNDEKSİ (kg/cm²) | Serbest Basınç Deneyi(qu) (kgf/cm ²) | C Kgf/cm ² | Derece | C Kgf/cm² | ф Derece | Şişme Basıncı | Şişme Yüzdesi(%) | HIDROMETRE (HYDROMETER) |
| CR | SK-1 | 3,00 | N-1 | - | 2,21 | - | - | - | - | | - | 8,7 | - | - | - | - | - | - | - | |
| | | Siver of APA | N: DAYSAI | | ĸ | | Adres I Söz kö Labora Tarafin Bu bel | Bilgileri Firri nusu deney tuvarımız 4 dan verilen ge firmanın | na Beyanid sonuçları, s 708 sayılı k 03.05.2011 izni olmada | ar anun geregi tarih ve 28 na kopyalan FARK-II YAPI M. San More Govern | lilen deney Çevre ve Ş . No'lu Lat Anmaz ye çoğ A DOGAHT A DOGAT Ma Que ye Ne Tic Ma Que ye Ne store V.D | numunckyrin chirydify Bal orgywar Lei adulamaz Si MADENC S MADENC | e aittir: canlığı Yapı İş a Belgesi'ne s İLİK Gli 1. rkezi | yleri Genel M ahiptic | aderitiga | | betulka | Alir Bi Denetçi I elge No | | <u>v</u> |

| 1 1-1 | <u>1</u>) | <u> </u> | 1 |) (L | 2 IL- | | ŗ | 1 | 1 | ب | I ! | | | . * | | | ₫ | | | | I / | / | |
|-------|------------|--|--------------------------|-----------------------|--------------------------------------|---|------------------------------|--|----------------|------------------------|---------------|--------|---|-----------------------------|--------------------------|---|----------------------------|----|---|--------------------------------------|------------|-----------|--|
| | | All and a second s | 200 1. 200 | | | | | HİZ. | MÜH i Çakma | MAL | . SAN | . VE T | ORATU IC. LTD Karatay / K | . ŞTİ. | | | | 0 | CARANCE SEMERCLE | C. HL Gi | | | |
| | | YAPI | BİLGİLE | Rİ | | | | | | | | | | | | Numune Deney Ba | Geliş Tari | | 23.06.2018 | | 1 | | |
| | | | RU SAHİ | | HAKAN MÜH | | | | | | | | | | | Kayıt Nu | | | K18-1113-Z | | 1 | | |
| | | YAPI S | | | HANIFE AKP | | | | | | | | | | | | | | 26.06.2018 | | 1 | | |
| | | YAPIN | IN ADRE | | KIRBAĞLARI | | RKEZ / NI | IGDE | | | | | | | | Rapor Ta | | | | | 1 | | |
| | | PAFTA | ADA/PA | RSEL | 1759 ADA / | 6 PARSEL | | | | | | | | | | Rapor Nu | marasi | | R18-1113-2 | 2 | 1 | | |
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| | | | | | | LU DEN | IEY SC | DNUÇL/ | ARI R | APOF | lU . | | | | | Bakanlık | Rap. No | | 15130767 | |] | | |
| | | | Numune | | тор | Doğal | | | | APOF | | | Nokta | Üç Eks Basınç | | Bakanlık | Rap. No | | 15130767 Direkt Kesn | me Deneyi | | | |
| | | Sondaj Kuyusu Adı | | | | | | | | | | USCS | Nokta Yükleme Dayanımı (kgf/cm2) | | | Bakanlık | | Gs | T | me Deneyi *f _{up} (°) | | | |
| | | Kuyusu | Numune Tipi ve | | TOP Doğal Su Muhtevası | Doğal Birim Hacim Ağırlık | Elek #10 Kalan | Analizi #200 Geçen | Atte | rberg Lin PL | nitleri PI | USCS | Yükleme Dayanımı | Basınç * c _{up} | (UU) *f _{op} | Bakanlık Konsoli Şişme Yüzdesi | dasyon Şişme Basıncı | Gs | Direkt Kesn * c _{up} (kg/cm ²) | *f _{up} (") | | | |
| | | Kuyusu Adı | Numune Tipi ve Adı | Derinlik | TOP Doğal Su Muhtevası (%) | Doğal Birim Hacim Ağırlık (gr/cm ³) | #10 Kalan (%) | Analizi #200 Geçen (%) | Atte | rberg Lin PL (%) | nitleri PI | | Yükleme Dayanımı | Basınç * c _{up} | (UU) *f _{op} | Bakanlık Konsoli Şişme Yüzdesi | dasyon Şişme Basıncı | Gs | Direkt Kesn * c _{up} (kg/cm ²) 0,0563 | *f _{up} (*) 30 | | | |
| | | Kuyusu Adı SK-1 | Numune Tipi ve Ada | Derinlik 1,50-1,95 | Doğal Su Muhtevası (%) 3,36 | Doğal Birim Hacim Ağırlık (gr/cm ³) 1,82 | #10 Kalan (%) 15,88 | Anafizi #200 Geçen (%) 20,05 | Atte | PL (%) NP | nitleri PI | SM | Yükleme Dayanımı | Basınç * c _{up} | (UU) *f _{op} | Bakanlık Konsoli Şişme Yüzdesi | dasyon Şişme Basıncı | Gs | Direkt Kesn * c _{up} (kg/cm ²) | *f _{up} (") | | | |

Not ve Aciklamalar:

* Kullandan Standartlar: TS - 1900-1 , TS - 1900-2 ve TS 1500

** Laboratuvarımız Çevze ve Şehircilik Bakanlığının 11.04.2011 tarih ve 273 sayılı"Laboratuvar izin Belgesi"ne sahiptir

* Bu rapor, sødece densyk veplan om kanangen i norskolf i som et alle sogen i som ogen i som en som en sogen i en som en s

DENEYİ YAPAN GÜLÜ, KAPUSUZ

BEKİR AKARSU Jeoloji Yük. Müh. Denetçi Belge No:10360

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|-------------------------|-----------|---------------------------------------|------------------------|-------------------------|-------------------------------------|------------------------------------|----------------------|--|--------------------------------|------------------------------|---|--|
| | | | KAYAI | A TEK EK | SENLİ VE | NOKTA Y | ÜKÜ DENEY | FORMU | | | 1/ | - |
| | | | | | | | | | Sayfa No: | | 23,04, | |
| | | | 26 | | | | | | Num.Gel.Ta Rapor Tarihi | | 29,04, | |
| FİRMA ADI | : | SONSAN MÜHI | | | 25 2 1 | nčor | | | Lab. Kayıt N | | AKD-11 / | |
| PROJE ADI | : | 300 Ada, 29 Pars Jeolojik - Jeotek | | ayabaşı Mah | Merkez / I | NIGDE . | | 5 | Bayındırlık k | | 1431 | 292 |
| PROJE TIPI Sondaj No | Numune No | Derinlik (m) | Numune Boyu (mm) | Numune Çapı (mm) | Elastisite Modülü ε Gpa | Poisson Oranı V | Num. Ağırlığı (g) | Doğal Birim Hacim Ağırlık (kN/m ³) | Numune Kesit Alanı (cm²) | Yenilme Yükü P (kg) | Tek Eksenli Basınç Deneyi q _u (kg/cm ²) | Nokta Yüklem Deneyi I _s (kg/cm ² |
| SK-1 | KAROT | 5,00 | 118 | 58 | | | 688,69 | 21,67 | 26,42 | 1849 | 70 | |
| | KAROT | 5,00 | 109 | 49 | | | 460,63 | 21,98 | 18,86 | 1584 | 84 | |
| SK-2 | | | | | | | 702,76 | 22,49 | 26,42 | 2563 | 97 | |

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*Adres bilgilan müşter beyrindir. *Söz konusü denöy öğnuçları, sadece test edilen deney numunelerine aittir. *Deney sonuçları faberatuyarımızın Erri olmadan kısmen kopyalanamaz ve çoğaltılamaz. *Laboratuyarımız 4708-Şayılı Kanun Gereği Bayındırılık ve lakan Bakanlığı Yapı İşleri Genel Müdürlüğü tarafından verilen 17/10/2003 tarih ve 67 No' lu Laboratuvar İzin Belgesine Sahiptir.

FR.61 / REV.NO/TARIHI:02/11.02.2011