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Graphene-engineered automated sprayed mesoscopic structure for perovskite device scaling-up.

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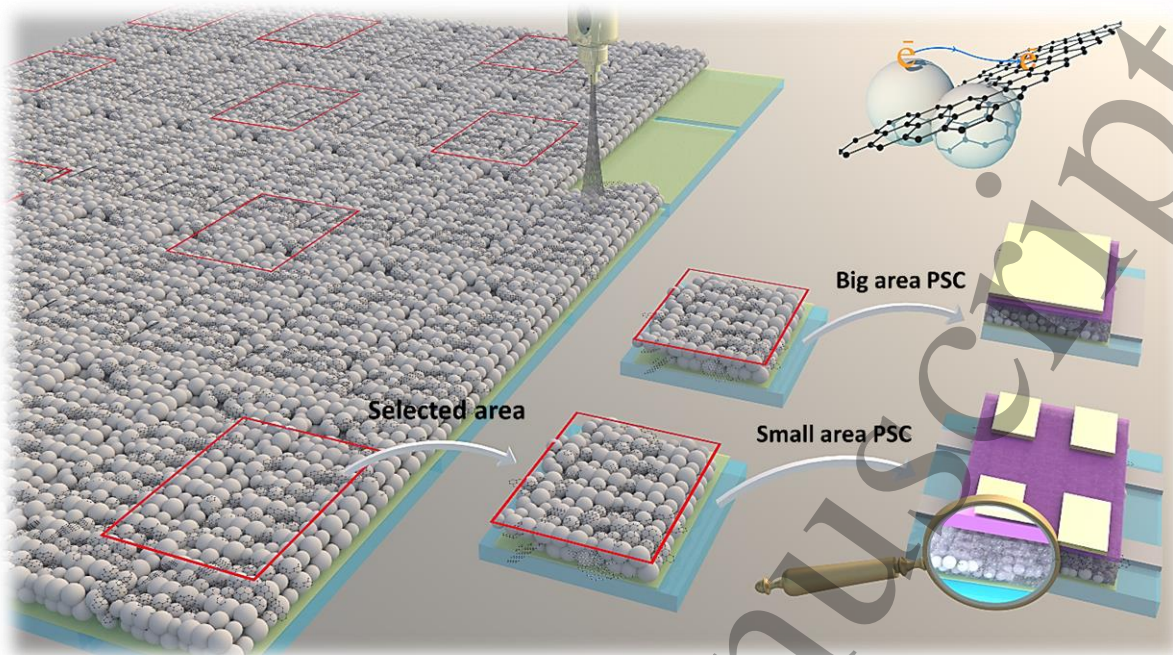
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Abstract

One of the most thrilling developments in the photovoltaic field over recent years has been the use of organic-inorganic lead halide perovskite, such as $\text{CH}_3\text{NH}_3\text{PbI}_3$ (MAPbI_3), as a promising new material for low-cost and highly efficient solar cells. Despite the impressive power conversion efficiency (PCE) exceeding 22% demonstrated on lab-scale devices, large-area material deposition procedures and automated device fabrication protocols are still challenging to achieve high-throughput serial manufacturing of modules and panels. In this work, we demonstrate that spray coating is an effective technique for the production of mesoscopic small- and large-area perovskite solar cells (PSCs). In particular, we report a sprayed graphene-doped mesoporous TiO_2 (mTiO_2) scaffold for mesoscopic PSCs. By successfully combining the spray coating technique with the insertion of graphene additive into the sprayed mTiO_2 scaffold, a uniform deposition and a significant enhancement of the electron transport/injection at the mTiO_2 /perovskite electrode is achieved. The use of graphene flakes on the sprayed scaffold boosts the PCE of small-area cells up to 17.5% that corresponds to an increase of more than 15% compared to standard cells. For large-area (1.1 cm^2) cells, a PCE up to 14.96% is achieved. Moreover, graphene-doped mTiO_2 layer enhances the stability of the PSCs compared to standard devices. The feasibility of PSC fabrication by spray coating deposition of the mesoporous film on large-area $21 \times 24 \text{ cm}^2$ provides a viable and low-cost route to scale up the manufacturing of low-cost, stable and high-efficiency PSCs.

Keywords: Automated Spray Coating, Perovskite Solar Cell, Graphene, mesoporous TiO_2 , interface engineering



1. Introduction

The power conversion efficiency (PCE) of solution-processed solar cells underwent a rapid progress, especially in the case of the organic-inorganic hybrid perovskite solar cells (PSCs), showing a record high PCE value of 22.7% in 2017 [1]. A prototypical PSC architecture comprises an organometal halide perovskite-based light-harvesting layer, sandwiched between a hole-transporting layer (HTL) and an electron-transporting layer (ETL). [2, 3] In particular, for the so-called mesoscopic structure, a mesoporous TiO_2 (m TiO_2) ETL is usually deposited onto a compact TiO_2 (c TiO_2) hole-blocking layer as photoelectrode (PE) scaffold. The m TiO_2 layer has a dual role consisting in both extracting the photo-generated electrons from the perovskite layer and transporting the charge towards the transparent conductive oxide (TCO) [2, 3]. The mesoporous scaffold structure accelerates the charge separation and the electron injection from the perovskite to the ETL [4], which allows the most efficient [5] and stable [6] PSCs to be fabricated. The photovoltaic performance achieved by PSCs with mesoscopic TiO_2 architectures (PCE > 20%) [7, 8] is encouraging the scientific community to scale up this technology. The possibility to fabricate large-area mesoscopic PSCs has already been proved in our recent work on graphene-based modules by adopting spin coating-based manufacturing. However, in this case, the module dimension is limited by the spin coater dimensions, which restricts the module active area to a few tens of cm^2 [9, 10]. Alternative deposition techniques, such as screen printing [11], blade coating [12], spray coating [13] and electrospray coating [14, 15], have been considered with efficiency on small area cells of 9.3%, 9.7%, 16% and

15%, respectively. However, their applicability to large-area format compatibly with the controlled deposition of uniform m TiO_2 films is still an open issue [15].

Differently from a wet film deposition (typical of spin and blade coating, as well as screen printing techniques), during spray coating of m TiO_2 films, small droplets of material are deposited onto the substrate [16]. Consequently, spray coating is not affected by the roughness of the underlying layer or by the substrate pattern [17] and it can be applied on irregular surfaces with high reproducibility [18]. Moreover, it allows the whole device area to be covered in a second timespan without any restriction in term of dimensions and geometry. Lastly, the possibility to spray any solution independently by the mixed precursors or doping materials makes the spray coating advisable to speed up and scale up the perovskite modules fabrication [13, 19] for their market entry [20-22]. Based on these considerations, Huang et al. [13] demonstrated superior charge transport properties for sprayed m TiO_2 nanoparticles compared to the corresponding spin-coated film, allowing PSCs to reach PCE higher than 16%. Moreover, PCE above 15% has been recently demonstrated for small-area PSCs based on electrospray-coated m TiO_2 as PE scaffold [15]. Despite these advances, the application of spray coating techniques to large-area PSCs is still limited to few cases [23-25], and the all-sprayed devices achieved PCEs which are still far ($\leq 11.7\%$) from the state-of-the-art [1]. Recently, both PCE and the stability of PSCs have been improved by exploiting 2D materials, *e.g.*, graphene or MoS_2 , to control the interface properties between the different layers in the PSC architecture [9, 10]. The advantage of this strategy, named as ‘‘Graphene Interface Engineering’’ (GIE), is linked with the possibility to

create and design layered artificial structures with on-demand electrochemical properties [26-30] by means of scalable, cost-effective and solution-processed methods [31-36]. In fact, the possibility to produce 2D materials from the exfoliation of their bulk counterparts in suitable liquids [37-43] enables functional inks to be formulated [44-47]. Subsequently, 2D material inks can be deposited on different substrates by well-established printing/coating techniques [48-53].

Based on the aforementioned considerations, graphene-based hole-blocking layer (or ETL) have demonstrated to reduce the energy barriers for electron collection at the PE, improving the short-circuit current density (J_{SC}) [54-56]. For example, graphene/metal oxide composites improved the J_{SC} of 23% compared to the one of graphene-free counterpart [54]. Graphene quantum dots (GQDs) and a lithium neutralized graphene oxide (GO-Li) have been used as interlayers between $mTiO_2$ and perovskite absorber in a mesoscopic PSCs [55, 56] to accelerate the electron injection. Consequently, GQDs-based PSCs exhibit faster electron extraction time (90-106 ps) if compared with the PSCs without GQD (260-307 ps), while the use of GO-Li improved the linear trend of J_{SC} - P_{inc} curves with respect to that expressed by the reference cells. Additionally, graphene has also been used to dope the $mTiO_2$ [57, 58]. Actually, the presence of graphene into $mTiO_2$ -based ETLs reduced the interfacial resistance and improved the electron collection efficiency at the PE by demonstrating around a two-fold faster electron diffusion coefficient than the native ETL [57]. In particular, graphene-doped $mTiO_2$ (Gr- $mTiO_2$) layer deposited by spin coating has shown a record PCE above 16% and also improved stability, retaining more than 88% of the initial performance over 16 h of prolonged 1 SUN illumination at maximum power point (MPP) [58]. Actually, it is well-established that GIE is also an effective tool for the fabrication of efficient and durable PSCs [59].

Herein, we report the use of the GIE in order to fabricate PSCs *via* Automated Spray Coating (ASC) technique. The ASC enables Gr- $mTiO_2$ to be deposited compatibly with high-throughput serial manufacturing of PSCs. The optimization of sprayed $mTiO_2$ is assessed by studying its morphological, structural and electronic properties as a function of the substrate temperature and the concentration of $mTiO_2$ paste. The sprayed Gr- $mTiO_2$ paste allows PSCs to reach a PCE of 17.5 % and 14.96 % on 0.1 cm² and 1.1 cm² active areas, respectively. The use of graphene enables the PSC efficiency to be improved more than 16% compare to the reference device. Finally, electro-optical analysis exhaustively points out the role of graphene in the electron injection, trap states and charge transporting into the PE. Lastly, we show that the use of graphene into the $mTiO_2$ partially mitigates the degradation phenomenon at perovskite/ETL interface, thus increasing the PSCs time life under operative conditions.

Methods

Graphene ink preparation

Liquid phase exfoliation of graphite flakes [60] (Sigma-Aldrich) in N-methyl-2-pyrrolidone (NMP) and subsequent solvent exchange process [61] were used to prepared graphene flakes ink in ethanol (EtOH, Sigma-Aldrich, + 99.8 %) at a concentration of 0.9 mg mL⁻¹. Experimentally, 3g of graphite flakes were dispersed in 300 mL of NMP and ultrasonicated for 6h. The obtained dispersion was then ultra-centrifuged at 16 000 g (in a Beckman Coulter Optima™ XE-90 with a SW32Ti rotor) for 30 min at 15 °C, exploiting sedimentation-based separation to remove thick flakes and un-exfoliated graphite. After the ultracentrifugation process, 80% of the supernatant was collected by pipetting. The pipetted sample was dried using a rotary evaporator at 70 °C, 5 mbar, then 500 mL of EtOH were added to the dried samples. The sample was then dispersed using a sonic bath for 10 min. Subsequently, the samples were centrifuged at 800 g (in a Beckman Coulter Optima™ XE-90 with a SW32Ti rotor). Then, the sediments were collected while the supernatant was discarded. This process of decantation was repeated twice, with the objective to wash out the NMP residuals. Finally, the sediments were dispersed in 200 mL of EtOH.

Solar cells fabrication

The solar cells were fabricated on Glass/FTO substrates, which were washed for 10 min with acetone, deionized water and EtOH, in an ultrasonic bath, consecutively. A TiO_2 dispersion for spray pyrolysis deposition of $cTiO_2$ consisted of 0.16 M diisopropoxytitaniumbis acetylacetonate (TiAcAc) and 0.4 M acetylacetonate (AcAc) in EtOH. The final thickness was 50 nm of the spray pyrolysis at 450°C onto the pre-cleaned laser patterned FTO glass. For $mTiO_2$ film deposition, anatase TiO_2 nanoparticles paste (18NR-T, Dyesol) was used. The $mTiO_2$ paste was dissolved into EtOH *via* stirring and ultrasonic bath to obtain 1.4 M, 1.6 M, 1.7 M and 1.8 M concentrations. Mesoscopic TiO_2 films based on aforementioned concentrations were deposited by ASC technique. Then 0.4 M of TiAcAc was added to the $mTiO_2$ dispersion, which was stirred for 1h. Then, the obtained dispersion was doped with graphene flakes dispersion in EtOH (concentration of 0.5%, 1% and 2% v/v were tested). The $mTiO_2$ was then deposited onto the FTO/compact TiO_2 substrates through ASC using setting deposition parameters reported in **Table S1**. For reference spin-coated $mTiO_2$ -based devices, TiO_2 paste (18NR-T, Dyesol) was diluted with EtOH, (w/w ratio of 1:5), and spin-coated onto the $cTiO_2$ surface at 1500 rpm for 20 s. The formed $mTiO_2$ films were sintered at 480°C for 30 min using a previously reported protocol [62]. The $CH_3NH_3PbI_3$ absorber layer was deposited by a previously reported crystal engineering method in

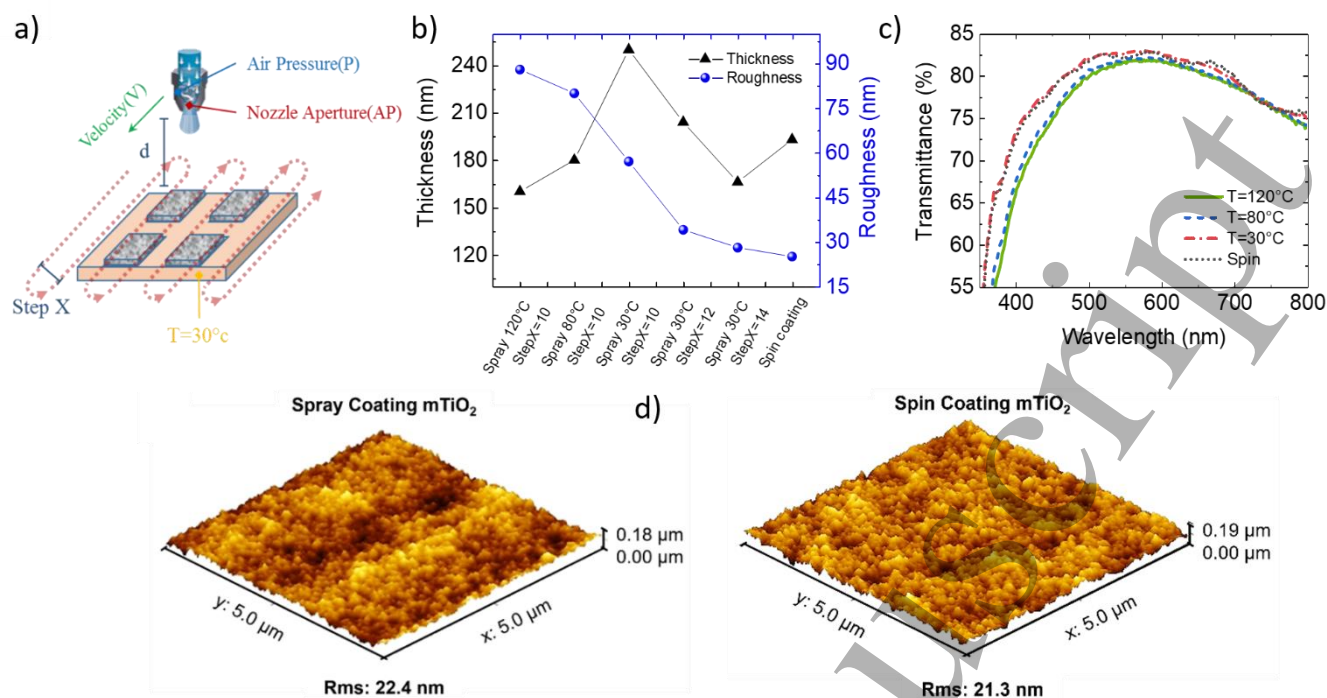


Figure 1. a) Scheme of the Automated Spray Coating. b) Thickness and roughness of TiO₂ films, by spray coating deposition at 30°C, 80°C, 120 °C and by spin coating one. c) Transmittances of TiO₂ film spray-coated on different temperature of substrate. d) AFM topography of the different mTiO₂ thin films prepared by ASC at 30°C (left) and by spin coating (right).

atmospheric condition [62]. Briefly, 535 mg of PbI₂ powder was dissolved in 1 ml DMF and spin-coated at 6000 rpm for 10 s, while the temperature of the solution was set to 70 °C, on the surface of the preheated (70 °C) mTiO₂ film. Subsequently, the devices were annealed at 40 °C for 2 min (temperature raise time = 1 min) and at 60 °C for 1 min (temperature raise time = 1 min). In the second step, the cooled PbI₂ layers were dipped in a solution of methylammonium iodide (CH₃NH₃I in anhydrous 2-propanol 10 mg mL⁻¹) for 10 min at room temperature while the solution was kept under mechanical stirring during the dipping time. Then, the devices were washed immediately by spin coating 2-propanol with an acceleration rate of 6000 rpm for 10 sec. Finally, the devices were heated at 70 °C for 2 min (temperature raise time = 1 min), and at 115 °C for 4 min (temperature raise time = 3 min) with relative humidity of about 40% on a hotplate. After heat treatment, 100 µl of spiro-OMeTAD (73.5 mg ml⁻¹) in chlorobenzene (CB) solution doped with 26 µl of tert-butylpyridine (TBP), 16.6 µl of Lithium Bis (Trifluoromethanesulfonyl) Imide (Li-TFSI) of stock solution (520 mg in 1 ml acetonitrile), and 7.2 µl of cobalt (III) complex solution (FK209 from Lumtec) was deposited as HTL by spin coating at 2000 rpm for 20 s. Finally, 80 nm of Au was deposited as counter electrode by thermal evaporation.

Characterization

Masked devices were tested by acquiring I-V curves under a Class A solar simulator (ABET Sun 2000) at AM1.5 and 100 mW cm⁻² illumination conditions calibrated with a reference silicon cell (RERA Solutions RR-1002), using a Keithley 2420 as a source-meter in ambient condition without sealing. Sun simulator spectrum and class were measured with a BLACK-Comet UV-VIS Spectrometer.

The atomic force microscopy (AFM) analysis of the surface of the TiO₂ thin films realized by spray and spin coating, was performed through an A.P.E. Research Atomic Force Microscope. Measurements were performed in non-contact mode with a silicon tip with a radius of 8 nm, mounted on a cantilever (resonance frequency=325 kHz) with a spring constant of 40 N m⁻¹.

Dark I-V, transient photovoltage (TPV), stability stress test at the MPP, and illumination intensity dependence of the V_{oc} and J_{sc} were performed with a high speed four channel source meter. A white LED array (4200 Kelvin) tuneable up to 200 mWcm² of optical power density-based measurement system

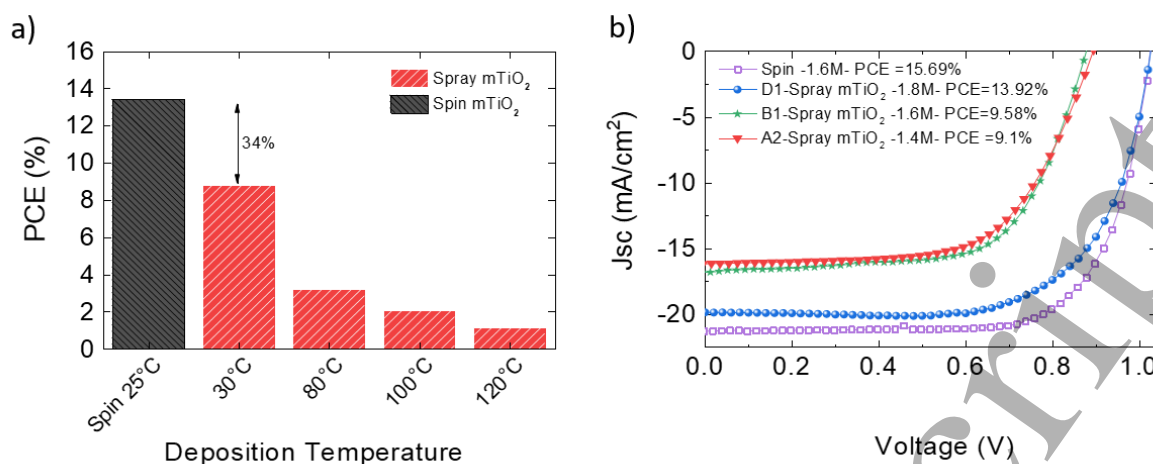


Figure 2. a) PCE under 1 SUN illumination for sprayed-mTiO₂-based PSCs, realized by varying the substrate deposition temperature. b) Density of current-voltage (I-V) curves under 1 sun for complete PSCs realized by using three different mTiO₂ dispersion concentrations with optimum deposition setting.

(Arkeo-Cicci research s.r.l.) was used as light source. A spring contact-based sample holder was used to improve the repeatability of the experiments.

Incident power conversion efficiency (IPCE) spectra were acquired by using a homemade setup.

Electrochemical measurements were performed in dark conditions at room temperature using an Auto-lab 302N Modular Potentiostat from Met Rohm in the two-electrode configuration with a bias voltage ranging from 0.6 to 1 V. The sinewave perturbation used was 10 mV of amplitude with frequencies from 1 MHz to 1 Hz.

The surface morphology of mesoporous layers and cross section image were obtained by using Scanning Electron Microscope (SEM) FE-SEM ZEISS.

Results and Discussion

In mesoscopic PSCs, the light enters from the PE to excite the photoactive layer. Therefore, the light passes through the mTiO₂ layer before reaching the perovskite over-layer. For this reason, the control of optical transparency, thickness and roughness of the TiO₂ film are crucial to achieve efficient PSCs [63, 64].

The morphological and optoelectronic properties of the final sprayed mTiO₂ layer depend by several deposition parameters, *i.e.*, the substrate temperature, the number of spray cycles, the distance between the spray nozzle and the substrate, the nozzle aperture, the air pressure, and, lastly, the distance between two adjacent spray lines (StepX).[65, 66] (see **Figure 1a**).

As a first step in the deposition optimization of the ASC process, we studied the influence of the substrate (FTO) temperature on the roughness and transparency of the resultant mTiO₂ layer. Spin coating deposition of mTiO₂ was also considered for comparison. Spray coating of commercial

mTiO₂ nanoparticles (18NRT) dispersed in EtOH (1:5 w/w ratio) was accomplished on the substrate heated at different temperatures (30 °C, 80 °C and 120 °C). As shown in **Figure 1b,c**, the highest substrate temperature (120 °C) resulted in a rough mTiO₂ surface (> 80 nm), which caused a decrease of the average electrode transmittance (81.4%) with respect to that obtained for the other temperatures (83% for mTiO₂ obtained by spray at 30°C and spin coating). On the other hand, the low substrate temperatures (30 and 80 °C) allowed the solvent to reach the substrate surface with a consequent flattening of the mTiO₂ surface. Notably, the RMS roughness of the layer was also influenced by the overlap of two adjacent spray lines. The mTiO₂ film deposited by using a distance between two adjacent spray lines of 14mm (StepX = 14 mm) had the best width overlap of each sprayed spot (5 mm), since it results in lower roughness (28 nm) with respect to other StepX values. Atomic force microscopy topographies (**Figure 1d**) show that the sample realized by ASC had a root means square (RMS) roughness (22.4 nm) comparable to that of the spin-coated samples (21.3 nm) (see also **Table S2**).

The mTiO₂ film morphology obtained for the deposition at 30 °C enabled the PSCs performance to be enhanced compared to that of the PSCs produced with higher temperatures, *i.e.*, 80, 100 and 120°C (**Figure 2a**). More in detail, the PCE decreased by almost 60% and 80% when the substrate temperature for the mTiO₂ spray coating increased from 30 to 80 °C and 120 °C, respectively. However, it is noteworthy that the highest PCE obtained for sprayed mTiO₂-based PSCs (13.92%) was still 34% lower than that of reference PSCs produced by spin coating mTiO₂ (15.69%).

In order to optimize the sprayed mTiO₂ layer morphology, different concentrations of TiO₂ dispersion (1.4 M, 1.6 M, 1.7 M and 1.8 M) were employed and titanium diisopropoxide bis acetylacetonate (TiAcAc) was added to the sprayed dispersion

Cell Type	V_{oc} (V)	J_{sc} (mA/cm ²)	FF (%)	PCE (%)	J_{sc} form integrated IPCE (mA/cm ²)
A2 Spray coating 1.4M (nozzle AP=8, P=1.5 bar)	0.871	-15.88	66.34	9.18	-14.95
Spray coating 1.6M without TiAcAc (nozzle AP=9, P=1.5 bar)	0.857	-15.41	65.80	8.69	-14.67
B1 Spray coating 1.6M (nozzle AP=9, P=1.5 bar)	0.873	-16.60	66.10	9.58	-16.09
D1 Spray coating 1.8M (nozzle AP=9, P=1 bar)	1.021	-19.77	68.94	13.92	-19.40
Standard Spin coating	1.018	-21.16	72.82	15.69	-20.65

Table 1. PSCs V_{oc} , J_{sc} , FF and PCE values for three different mTiO₂ dispersion concentrations with about 180 nm of sprayed mTiO₂ thickness, compared with those of standard spin-coated mTiO₂-based cells. Deposition have been performed with 30°C of substrate temperature and with StepX of 14 mm.

to improve the connectivity between the mTiO₂ nanoparticles [13] (details about the analysed concentrations are reported in the methods section). By adjusting spray parameter settings, (Table S1), the mTiO₂ film with thicknesses ranging from 150 to 200 nm [5, 67, 68] exhibited the lowest RMS roughness values (about 22 nm) (Figure S1). Therefore, small-area (0.1 cm²) PSCs were produced with a mTiO₂ film thicknesses of 180 nm, as shown by a representative cross-sectional SEM image (Figure S2). The as-prepared cells without TiAcAc resulted in maximum PCE of 9.1%. The addition of TiAcAc into mTiO₂ dispersion resulted in a cell PCE improvement of +10% (Table 1). Notably, the highest average PCE of 13.92% was achieved for the PSCs produced by using a mTiO₂ concentration of 1.8 M. As shown in Figure 2b, the PCE enhancement was a consequence of the higher current density (J_{sc}) (-19.77 mA cm⁻²) and Fill Factor (FF) (69%) compared with those of the PSCs fabricated with other mTiO₂ dispersion concentrations (1.4 M, 1.6 M and 1.7 M). We assign these effects to an effective crystallization of the perovskite into the 22 nm-rough mTiO₂, which help to reduce the carrier recombination and improve carrier transport and collection abilities [69-71].

The pore size for efficient infiltration of the perovskite into the mTiO₂ (Error! Reference source not found.) leads to the highest electron mobility and the lowest disorder in the interface with perovskite.

Although the sprayed mTiO₂-based PSCs achieved PCE of ~14%, their J_{sc} and FF were still 10% lower than those of spin-coated mTiO₂-based-based PSCs (Table 1), suggesting that the electron recombination at mTiO₂/perovskite interface significantly affected the cell performance for sprayed mTiO₂ based devices compared to that of spin-coated mTiO₂-based ones [72, 73].

With the aim to further improve the physical and electrical sprayed mTiO₂ film.

With the aim to boost further the performance of the PSCs obtained by ASC the mTiO₂ dispersion was enriched with graphene flakes, resulting in hybrid mesoscopic films herein

named Gr-mTiO₂). Graphene flakes were produced by the LPE [44], in NMP. The synthetic procedure is detailed in [58] and summarized in the Experimental section. Three different concentrations of graphene flakes dispersion (0.5%, 1% and 2% v/v) were tested by fabricating PSCs with area of 0.1 cm². In agreement with the SEM images of the mTiO₂ surface morphology (Figure S3), the Gr-mTiO₂ films did not show any difference with respect to the pristine mTiO₂ films. Moreover, the films deposited by spray and spin coating have shown the same surface morphology with an average mTiO₂ particle size of ~21 nm.

In term of photovoltaic performance of the PSCs, the optimum concentration of graphene inside mTiO₂ was 1% v/v, which results in an increase of J_{sc} and PCE of 13% and 23%, respectively, with respect to those of graphene-free reference (Figure S4). This means that a concentration of 1% v/v of graphene dispersion concentration into mTiO₂ dispersion can suppress the electron recombination, *i.e.*, to increase the J_{sc} . However, once graphene concentration exceeded 1% v/v, the PSC performance decreased. This trend can be ascribed to the increase of Gr-mTiO₂ light absorption by increasing graphene flakes concentration that strongly affects the optical transmittance of the PE (see Figure S5) [74]. This effect is also observed in the performance of graphene-based cells, in which J_{sc} begins to decrease beyond the optimum graphene loading of 1% v/v (see Figure S4a).

Perovskite solar cells with and without graphene and for both spray and spin coating of mTiO₂ were fabricated and compared. To deposit mTiO₂ by ASC, the optimized graphene dispersion with a concentration of 1% v/v of was incorporated into the 1.8 M mTiO₂ dispersion. In order to demonstrate the uniformity of large-area mTiO₂ obtained by ASC, firstly the spray coating was accomplished on a large-area substrate (24×20 cm²). Secondly, the substrate was divided into 2.5×2.5 cm² pieces, subsequently selected from different areas of the initial substrate, to finalize the fabrication of entire PSCs. On these substrates, devices were made with different active areas 0.1 cm² and 1.1 cm² (herein named small- and large-area

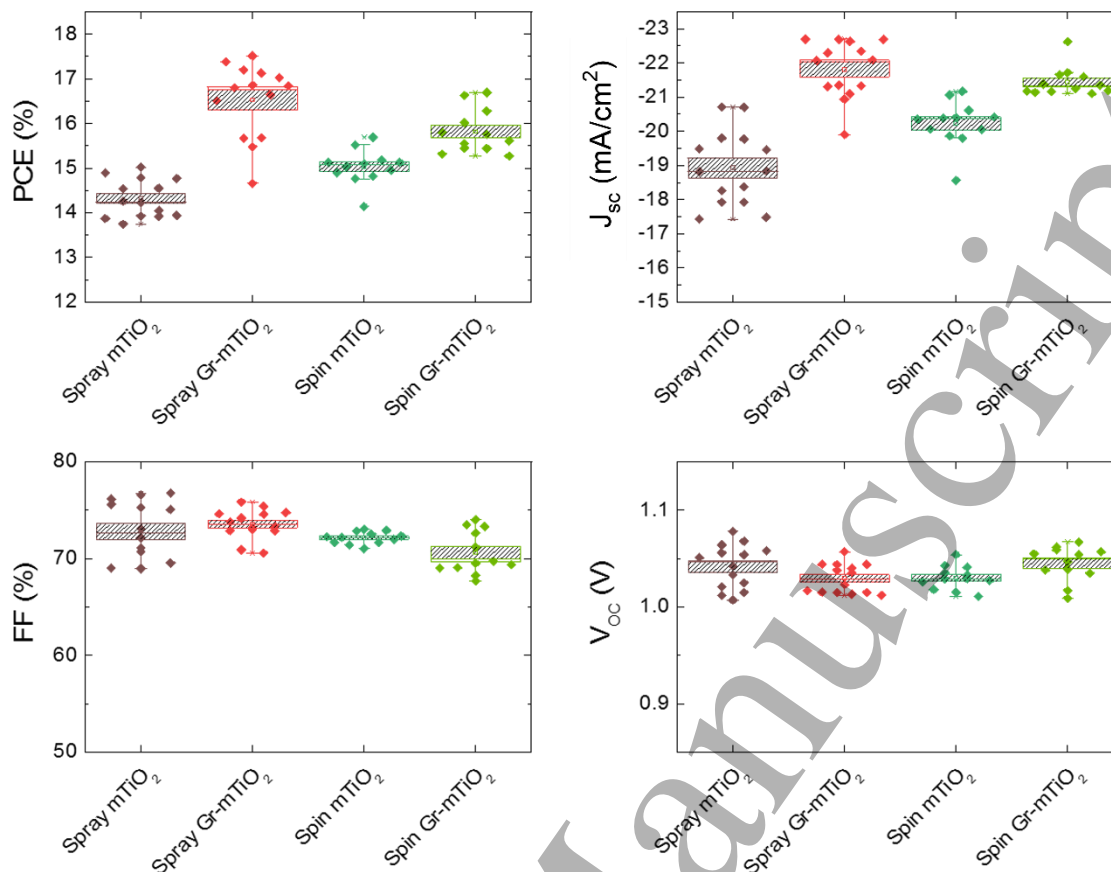


Figure 3. Comparison of electrical parameter statistics for 26 small-area (0.1 cm^2) PSCs based on pristine mTiO_2 and 26 small-area PSCs based on Gr-mTiO_2 scaffold deposited by ASC and spin coating techniques. The cells were measured under 1 SUN AM 1.5G illumination.

PSCs, respectively) by using the deposition parameter settings previously optimized (see Methods section for details).

Figure 3 reports the electrical parameters (PCE, J_{sc} , FF and V_{oc}) for PSCs based on pristine mTiO_2 and Gr-mTiO_2 deposited by ACS and spin coating techniques. Notably, for both deposition techniques, the Gr-mTiO_2 led to a significant enhancement of J_{sc} with respect to pristine mTiO_2 . In particular, for small-area cells (0.1 cm^2), the spray-deposited

Gr-mTiO_2 led to a $\sim 16\%$ increase of J_{sc} with respect to the mTiO_2 -based PSCs, whereas the graphene doping for spin-coated mTiO_2 improved the J_{sc} of 5% with respect to the graphene-free reference.

The average PCE of spray Gr-mTiO_2 based devices was 16.8%, *i.e.*, higher than the spin-coated mTiO_2 -based PSCs (15.6%). For pristine sprayed mTiO_2 -based PSC, the average

Type of cells	V_{oc} (V)	J_{sc} (mA/cm^2)	FF (%)	PCE (%)
Spray Pristine mTiO_2	1.063 (1.05 ± 0.012)	-18.571 (-18.91 ± 0.46)	66.712 (65.15 ± 2.14)	13.165 (12.94 ± 0.26)
Spray Gr-mTiO_2	1.059 (1.06 ± 0.005)	-20.199 (-19.79 ± 0.43)	69.957 (67.25 ± 2.54)	14.963 (14.21 ± 0.80)
Spin mTiO_2	1.031 (1.04 ± 0.008)	-17.039 (-18.12 ± 0.96)	65.488 (62.6 ± 2.50)	11.503 (11.78 ± 0.29)
Spin Gr-mTiO_2	1.030 (1.04 ± 0.01)	-19.224 (-19.02 ± 0.19)	68.199 (65.22 ± 4.11)	13.506 (12.91 ± 0.91)

Table 2. Electrical parameters of sprayed large-area (1.1 cm^2) PSCs with and without graphene into mTiO_2 compared with the ones exploiting spin-coated mTiO_2 . All the devices were measured under 1 sun AM 1.5G illumination.

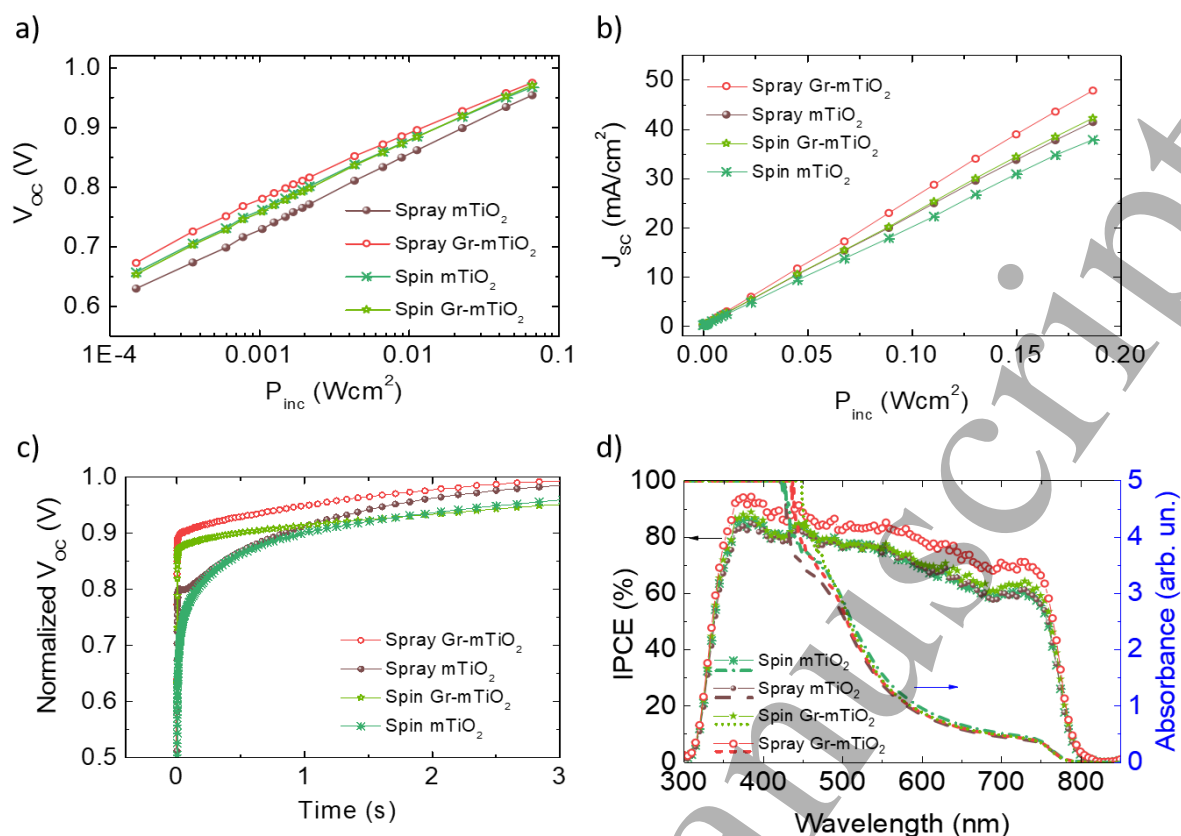


Figure 4. a) V_{oc} vs. P_{inc} , b) J_{sc} vs. P_{inc} and c) V_{oc} rise profiles normalized at the maximum value, d) Absorption and IPCE spectra for the tested PSCs.

J_{sc} , FF and V_{oc} values were 18.7 mA cm^{-2} , 0.72 and 1050 mV, respectively. By introducing graphene flakes into the mTiO₂, average J_{sc} increased up to 22.2 mA cm^{-2} , while V_{oc} and FF values did not undergo significant variations. Therefore, our champion cell exhibited 17.5% PCE, exceeding the highest PCE previously reported for a two-step process (0.1 cm^2 active area) CH₃NH₃PbI₃-based PSC using spin-coated mTiO₂ layer (PCE 17%) [62, 75].

The characterization of large-area (1.1 cm^2) cells (see **Table 2** and **Figure S6**) confirmed the J_{sc} enhancement for Gr-mTiO₂-based cells with respect to that of pristine mTiO₂-based reference (from -18.5 to -20.1 mA cm^{-2}).

Time-dependent PCE response (**Figure S7a**) and I-V curves as a function of the scan voltage direction (**Figure S7b**) did not evidence the presence of hysteresis [8].

The role of graphene in mTiO₂ film: electro-optical analysis

Mesoporous scaffold sintered at 450°C	Resistivity ρ (ohm cm)	Conductivity σ (Siemens cm)
Spray mTiO ₂	3.6E+5	2.7E-6
Spray Gr-mTiO ₂	2.4E+5	4.2E-6

Table 3. The sheet resistance of pristine mTiO₂ and the Gr-mTiO₂, measured by four-point probe system.

With the aim to fully understand the differences between the pristine mTiO₂ and the Gr-mTiO₂ based devices, complementary electrical measurements (V_{oc}/J_{sc} vs. light intensity) were performed for each device typology.

The relation between V_{oc} and the incident light power (P_{inc}) (**Figure 4a**) allowed the recombination processes at the mTiO₂/perovskite interface to be evaluated [76, 77]. V_{oc} vs. P_{inc} trends recorded for all the tested device typologies showed a logarithmic increase with similar slope values (124 mV dec^{-1} for spray reference-mTiO₂, 119 mV dec^{-1} for spray Gr-mTiO₂ and 122 mV dec^{-1} for spin mTiO₂ and spin Gr-mTiO₂). This means that Gr-mTiO₂ based ETL did not significantly influence charge recombination rate over a wide operating light intensity window (from 0.1 mW cm^{-2} to 100 mW cm^{-2}). The higher V_{oc} absolute values recorded for Gr-mTiO₂ based device compared to that of free-graphene devices was correlated with the reduced interfacial charge recombination at TiO₂/perovskite, in accordance with previous reports [78].

In addition, the variation of J_{sc} vs. P_{inc} was recorded, as reported in **Figure 4b**. Since the J_{sc} - P_{inc} slope increases with the efficiency of charge collection at the device contacts [79], we concluded that sprayed Gr-mTiO₂ layer with 266 mA W⁻¹ slope effectively collected the photo-generated electrons from the perovskite absorber. Finally, transient V_{oc} rise measurements represented in **Figure 4c** were carried out by suddenly switching on the 1 SUN illumination from the dark steady state condition ($t = 0$ s) and monitoring the subsequent rise in photovoltage. The time rise of V_{oc} for PSC with Gr-mTiO₂ was shorter than the reference device. This indicated that an efficient active layer regeneration and/or charge-transfer process between the active and the transport layers occurred in presence of graphene flakes [80]. The fast rises for PSC with Gr-mTiO₂ can be ascribed to a fast filling and stabilization of charge trap states by injected or photogenerated electrons, reducing the availability of trap sites to mediate non-radiative recombination [81]. The rise time of V_{oc} obtained for our PSCs evidenced an electron injection improvement at perovskite/mTiO₂ interface when mTiO₂ is doped with graphene [82].

According to the electrical parameter statistic graphs (**Figure 3**), a dual effect of the Gr-mTiO₂ on device performance is evidenced. First, the presence of graphene in the mTiO₂ scaffold can deform the perovskite grain due to ferroelectric distortion at graphene/perovskite interfaces which affects the perovskite crystallization process [78, 82]. This can cause an efficient electron injection at the Gr-mTiO₂/perovskite interface [58]. Second, graphene can assist the negative carrier transport within the TiO₂ layer by increasing electron mobility, which results in increasing the PSCs photocurrent density [83].

In order to further investigate the enhancement of the device performance through the incorporation of graphene in mTiO₂, the effects of the absorber layer and conductivity of TiO₂ layer were characterized. A four-point probe system was employed to measure the sheet resistance of pristine and Gr-mTiO₂. As reported in **Table 3**, Gr-TiO₂ showed a 55% increase of the conductivity with respect to that of pristine mTiO₂.

As a further confirmation, sprayed Gr-mTiO₂-based PSCs have shown an improvement in the photocurrent density which is defined by integrating IPCE over the absorption wavelength range. Actually, $IPCE(\lambda)$ is the product of three factors: light harvesting efficiency (η_{LH}) depending on the perovskite layer, the quantum yield of charge injection from exited perovskite to ETL and HTL (η_{INJ}) and the charge carrier collection efficiency (η_{COL}) at the electrodes ($IPCE = \eta_{LH} \eta_{INJ} \eta_{COL}$) [84]. In addition, the η_{INJ} is defined as the product between the electron injection (η_{Einj}) and hole injection (η_{Hinj}) efficiency, as well as collection efficiency is defined as the product between the electron collection (η_{ECOL}) and hole collection efficiencies η_{HCOL} respectively:

$$\eta_{INJ} = \eta_{EINJ} \eta_{HINJ}$$

$$\eta_{COL} = \eta_{ECOL} \eta_{HCOL}$$

Figure 4d shows the absorption spectra of perovskite grown on both mTiO₂ and Gr-mTiO₂ scaffolds, evidencing that they are perfectly overlapped. This means that the modified Gr-TiO₂ layer did not affect the perovskite light harvesting properties. Consequently, since the two structures differed only in the addition of graphene within the ETL, the η_{LH} , η_{Hinj} and η_{HCOL} can be considered equal for both structures. Therefore, enhancement of IPCE in graphene-based devices can be likely ascribable to higher η_{Einj} at the perovskite/HTL interface and improved η_{ECOL} at the PE. Such analysis agrees with the V_{OC} rise and V_{OC}/J_{SC} vs. P_{inc} trends previously discussed.

Stability test

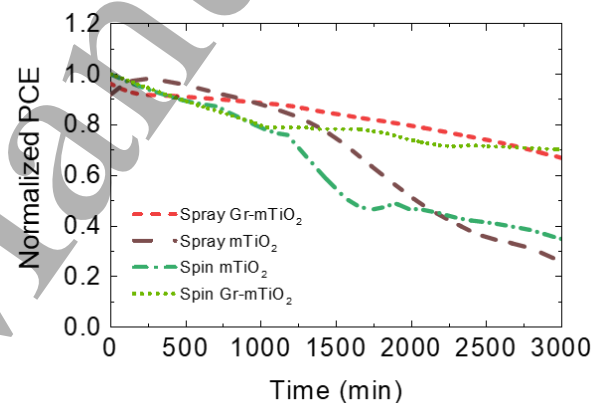


Figure 5. PCE aging trends under prolonged 1 SUN white LED illumination at MPP for the tested device typologies.

One of the most crucial challenges for mesoscopic PSCs is the stability under real working condition [85]. Despite numerous efforts by the scientific community to develop more stable cells, many issues are still opened since perovskite degradation depends strongly on light, moisture, and temperature [86-88].

Based on these considerations, we compared the stability of encapsulated PSCs based on pristine sprayed mTiO₂ and Gr-mTiO₂, respectively, by exposing them continuously under 1 SUN illumination for 2 days at 50 °C and 55% relative humidity of ambient air. The I-V characteristics were progressively acquired during the ageing time at MPP. The extracted electrical parameters are reported in **Figure 5**, normalized to the value obtained at $t = 0$ min. Notably, the cells based on sprayed Gr-mTiO₂ showed a remarkable stability by retaining more than 80% of the initial PCE value

after more than 40 h of the stress test, whereas the PCE of the spray pristine mTiO₂ cells decayed by 50% over the first 25 h.

As discussed in the previous section, the Gr-mTiO₂ has an electrical conductivity that can optimize charge collection [89-92] and separation [80,91] at the PE. The improved charge extraction at the PE drastically reduces the trapped charges accumulated at the mTiO₂/perovskite interface. This slows down the perovskite degradation [92]. Moreover, as discussed by Busby et al. [93] through ToF-SIMS measurements, the presence of graphene into the mTiO₂ limits the Ti-I bonding preserving a compact CH₃NH₃PbI₃ layer upon the light-induced ageing. We should also point out that 2D materials can improve thermal stability by reducing surface degradation of perovskite [94].

Conclusion

The field of perovskite solar cells (PSCs) is rapidly moving toward consolidating deposition processes that can be extended to large-area for industrial exploitations. In this work, we reported that the combined use of automatized spray coating techniques and graphene doping of mTiO₂ is an effective strategy to improve photovoltaic performances of PSCs with respect to the conventional, lab-scale device produced by spin coating process. More in detail, the PSC fabricated on a small-area with spray-coated Gr-mTiO₂ has shown an average power conversion efficiency (PCE) of 16.8% (max 17.5%), which is remarkably superior to that obtained for PSC using graphene-free sprayed (14.3%) or spin-coated mTiO₂ (15.1%). These results were also confirmed on large-area cells, which achieved a PCE of 14.96% using spray-coated Gr-mTiO₂, against 13.1% obtained by the reference PSCs. Electro-optical characterizations and transient measurements have shown that graphene doping of TiO₂ can improve the electron transport in ETL and charge injection at perovskite/ETL interface. In addition, Gr-mTiO₂ layer strongly affected the stability of PSCs under prolonged (47h) light soaking conditions by enlarging the lifetime of the devices, which retained more than 80% of the initial PCE value. These results pave the way to realize stabilized mesoscopic perovskite solar modules with a versatile, low-cost and roll-to-roll compatible printing technique.

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