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Key Words:	Skeletal muscle bioengineering, muscle stem cell, muscle hypertrophy, electrical stimulation, mechanical overload

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REVIEW

Mimicking exercise in three-dimensional bioengineered skeletal muscle to investigate cellular and molecular mechanisms of physiological adaptation.

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Abstract

Bioengineering of skeletal muscle *in-vitro* in order to produce highly aligned myofibres in relevant three dimensional (3D) matrices have allowed scientists to model the *in-vivo* skeletal muscle niche. This review discusses essential experimental considerations for developing bioengineered muscle in order to investigate exercise mimicking stimuli. We identify current knowledge in the use of electrical stimulation and co-culture with motor neurons to enhance skeletal muscle maturation and contractile function in bioengineered systems *in-vitro*. Importantly, we provide a current opinion on the use of acute and chronic exercise mimicking stimuli (electrical stimulation and mechanical overload) and the subsequent mechanisms underlying physiological adaptation in 3D bioengineered muscle. We also identify that future studies using accelerating bioreactor technology, providing simultaneous electrical and mechanical loading and flow perfusion *in-vitro*, may provide the basis for advancing knowledge into the future. We also envisage, that more studies using genetic, pharmacological and hormonal modifications applied in human 3D bioengineered skeletal muscle may allow for the discovery in-depth mechanisms underlying the response to exercise in relevant human testing systems. Finally, that 3D bioengineered skeletal muscle could be used as a pre-clinical *in-vitro* test-bed to investigate the mechanisms underlying catabolic disease, whilst modelling disease itself via the use of cells derived from human patients without exposing animals or humans (in phase I trials) to the side effects of potential therapies.

Introduction

In this review the authors discuss how recent advances in skeletal muscle bioengineering systems *in-vitro* may provide a physiologically relevant model to investigate adaptation to exercise. Recent evidence suggests that *in-vitro* bioengineered systems can provide relevant three-dimensional (3D) human models of skeletal muscle via the use of cells derived from human muscle biopsies seeded within biological scaffolds under tension that mimic the native skeletal muscle more accurately (Martin et al., 2013; Powell et al., 2002). These novel systems may also provide an experimentally pliable environmental niche *in-vitro*, for example via genetic modification and/or pharmacological manipulation, to investigate underlying molecular mechanisms of physiological adaptation than is currently available from *in-vivo* human study. Furthermore, in conjunction with the advances in the use of bioreactors (Donnelly et al., 2010; Huang et al., 2005; Player et al., 2014), bioengineering can provide technological advancements that enable the physiological simulation of skeletal muscle contraction by means of electrical stimulation and/ or mechanical loading for sustained/repetitive periods. The potential advantage of this *in-vitro* experimentation is that studies are not limited by infrequent sampling due to animal number or repeated bioptic sampling in humans. Furthermore, together with the use of bioreactors, experiments could potentially be higher-throughput, avoid ethical constraints of animal or human study *in-vivo* and therefore help elucidate fundamental mechanisms of physiological adaptation in relevant human systems.

Overview

This review will therefore include a discussion of the current advances in the bioengineering of skeletal muscle, outlining important experimental research considerations when attempting to create the most physiologically relevant 3D skeletal muscle constructs *in-vitro*. The use of electrical stimulation to provide a surrogate neural input for muscle contraction, in order to create the most native skeletal muscle phenotype and optimize contractile properties will also be of focus. Furthermore, we will outline the current understanding in the use of electrical stimulation to mimic chronic exercise and the assessment of the mechanisms leading to adaptation in 3D bioengineered skeletal muscle. Also, we will touch upon recent advances in the co-culturing of motor-neurons with muscle derived cells in 3D bioengineered skeletal muscle in an attempt to form neuromuscular junctions and establish the optimal environmental niche *in-vitro* that mimics contractile properties and displays the characteristics of mature adult skeletal muscle *in-vivo*. Furthermore, we will provide an overview of the use of mechanical overload/stretch regimes in 3D bioengineered skeletal muscle. Finally, we suggest that the use of novel bioreactors allowing simultaneous mechanical and electrical stimulation will potentially provide the most physiologically relevant *in-vitro* exercise systems in future study. Furthermore, 3D bioengineered skeletal muscle could be used as a pre-clinical *in-vitro* test-bed to investigate the cellular and molecular mechanisms underlying catabolic disease without exposing animals or humans (in phase I trials) to the side effects of drugs/therapies and therefore the potential identification of novel therapeutic strategies to counteract muscle wasting.

Experimental research considerations for deriving skeletal muscle cells and bioengineering 3D skeletal muscle

Adult muscle fibres past birth are terminally differentiated or post-mitotic. As a result, muscle turnover, regeneration and repair processes are dependent upon residing adult

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3 muscle stem cells/satellite cells and their ability to undergo cellular division. Under various
4 biochemical, mechanical and hormonal cues, satellite cells are activated (their immediate
5 progeny - termed myoblasts). They then proliferate, migrate, and fuse to muscle fibres to
6 provide additional/replace myonuclei and repair the existing fibres [reviewed in (Sharples
7 and Stewart, 2011; Sharples et al., 2016)]. It is therefore possible to isolate these cells from
8 bioptic sampling via explant (Martin et al., 2013), enzymatic digest (Danoviz and Yablonka-
9 Reuveni, 2012), or a combination of the two methods (Owens et al., 2015). Cells can
10 subsequently be expanded under high serum conditions and stored for long periods under
11 liquid nitrogen for future experimentation. Studies have also shown that once skeletal
12 muscle stem cells have been isolated from primary animal (Juhas and Bursac, 2014; Mudera
13 et al., 2010; Smith et al., 2012) and human tissue (Martin et al., 2013; Powell et al., 2002)
14 and placed under uniaxial tension within representative extracellular matrices,
15 multinucleated fibres can form in an aligned structure in parallel (Breslin and O'Driscoll,
16 2013; Martin et al., 2013). This is in comparison with monolayer cultures that have no
17 mechanical stimuli/tension, and myotubes form in seemingly spontaneous and even swirling
18 formations as they become larger (Figure 1 A & B). Furthermore, as skeletal muscle
19 contraction is fundamental to skeletal muscle function, both spontaneous (Bursac et al.,
20 1999) and electrically induced contraction of monolayer cultures (Brevet et al., 1976;
21 Kawahara et al., 2007; Thelen et al., 1997; Wehrle et al., 1994) results in non-uniaxial force
22 production, as the fascicles are not aligned in parallel, whereas 3D culture systems allow for
23 the functional measurement of force in aligned skeletal muscle fibres (Dennis and Kosnik,
24 2000; Khodabukus et al., 2007; Martin et al., 2015). Furthermore, contractions
25 (spontaneous or induced) can cause the myotubes to pull off monolayer cell culture dishes
26 and therefore time in culture and/or maturation of myotubes can therefore be enhanced in
27 bioengineered skeletal muscle as the myotubes are supported by a 3D matrix that allows
28 contractile activity. It has therefore been hypothesised that *in-vitro* monolayer models may
29 therefore fail to accurately biologically mimic *in-vivo* muscle, whereas 3D muscle systems
30 *in-vitro* may replicate the structure and niche of *in-vivo* skeletal muscle more closely (Seale and
31 Rudnicki, 2000; Sharples and Stewart, 2011). However, despite the more relevant cellular
32 architecture and extra-cellular matrix composition in 3D bioengineered skeletal muscle
33 constructs, there are still few direct comparisons with two-dimensional monolayer cultures
34 with respect to the cellular and molecular adaptation to exercise related cues such as
35 electrical stimulation or mechanical stretch. Indeed, there have been several studies
36 investigating electrical stimulation in isolation in monolayer cultures only (Brevet et al.,
37 1976; Kawahara et al., 2007; Thelen et al., 1997; Wehrle et al., 1994), as well as mechanical
38 stretch (Chang et al., 2016; Chen et al., 2013; Kook et al., 2008; Kumar et al., 2004; Pardo
39 et al., 2011; Vandeburgh and Kaufman, 1979). There have also been studies to investigate
40 electric stimulation in 3D bioengineered skeletal muscle in isolation (Cheng et al., 2016;
41 Donnelly et al., 2010; Hinds et al., 2011; Huang et al., 2006; Juhas et al., 2014; Langelaan
42 et al., 2011; Park et al., 2008; Rangarajan et al., 2014; Stern-Straeter et al., 2005) and 3D
43 studies that include mechanical stretch (Heher et al., 2015; Player et al., 2011; Player et al.,
44 2014; Powell et al., 2002; van der Schaft et al., 2011). To the authors knowledge, there are
45 limited comparisons of monolayer vs. 3D bioengineered skeletal muscle with the most
46 notable suggesting that after electrical stimulation, high voltage stimulation (2-2.5 V/mm)
47 could evoke considerable cell death in the monolayer mouse myoblast C2C12 cell line,
48 whereas 2.5 V/mm was shown to be optimum versus 1.25 and 5 V/mm for improved
49 contractile properties (greater peak force and excitability) within 3D bioengineered muscle
50 (Donnelly et al., 2010). However, electrical stimulation regimes in monolayer have broadly
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3 mimicked a cell signalling exercise response, such as increased AMPK (Nedachi et al., 2008),
4 enhanced glucose metabolism (uptake and oxidation) and complete fatty acid oxidation
5 (Nikolic et al., 2012) in response to continuous low-frequency stimulation, where high-
6 frequency stimulation to C2C12 myotubes resulted in an increase in protein synthesis
7 (Donnelly et al., 2010), both of which are well defined responses observed in skeletal muscle
8 tissue following *in-vivo* aerobic and resistance exercise, respectively. Therefore, the most
9 suitable *in-vitro* model warrants further investigation before monolayer cultures are simply
10 discarded for the determination of the mechanisms underlying exercise mimicking stimuli
11 over 3D *in-vitro* systems. This is particularly important given the greater time and cost
12 required for creating such 3D systems. Additionally, there are considerable technical
13 challenges requiring unique expertise to create and undertake exercise mimicking stimuli in
14 both monolayer and 3D bioengineered muscle *in-vitro*. An in-depth discussion of the
15 response of skeletal muscle cells in monolayer and 3D culture to electrical and mechanical
16 overload stimuli are detailed later in this review.
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20 Although animal models may allow for elucidation of underlying molecular mechanism due
21 to the ability to knock-out or overexpress specific target genes (Bodine et al., 2001;
22 Jørgensen et al., 2005; Leick et al., 2009; Leone et al., 2005; Shima et al., 1998), 3D
23 bioengineered 'mini-muscles' may be of further advantage in certain situations. Indeed,
24 animal studies can be extremely expensive, have relatively low throughput, and can
25 sometimes be criticised for the lack of relation to human populations. Equally, although
26 there is often limited practicality of such trials, human studies have been utilised to
27 investigate mechanisms of adaptation to exercise (Coffey and Hawley, 2007; Drummond et
28 al., 2008; Holloszy, 1973; Hood, 2009; Joseph et al., 2006). However, these experiments
29 may also be extremely costly, time consuming, and are somewhat limited to fixed quantity
30 biopsy collections (due to ethical considerations), therefore limiting the number of time
31 points for sampling. In addition, once specific cellular and molecular targets associated with
32 exercise adaptation *in-vivo* are determined, the regulatory pathways responsible for the
33 precise control of these systems cannot always be investigated, as genetic modification or
34 pre-clinical drug therapy cannot be undertaken *in-vivo* in human participants. However,
35 muscle derived cell isolation procedures from human muscle biopsies are becoming more
36 routine under local anaesthetic within academic research environments. Therefore, once
37 these techniques are well established, 3D muscle systems can make use of cells expanded
38 from one or two biopsy events, and allow for development of several constructs to examine
39 multiple time points as oppose to taking numerous biopsies over an acute time course from a
40 single human subject. This is despite isolated primary human muscle cells being
41 programmed to undergo minimal rounds of proliferation before they senesce due to their
42 drive to differentiate (O'Connor et al., 2009). However, even after 4-5 passages, enough
43 primary human cells can be derived from a single biopsy (approximately 5-15 million cells
44 dependent on biopsy size due to technique e.g. needle biopsy yields 20-30 mg whereas a
45 conchotome biopsy can yield 100-250 mg), with bioengineered human muscles only
46 requiring 200-400 thousand cells seeding density to make aligned 3D mature muscle fibres
47 *in-vitro* over a 2-3 week period (Martin et al., 2013). The use of bioengineered systems also
48 permits deeper investigation into mechanistic properties (as discussed above) and responses
49 to various simulated exercise regimens in tightly control environmental conditions (e.g. prior
50 nutritional status) through mechanical and/or electrical stimulation.
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3 Muscle cells must first proliferate then physically fuse to differentiate into multinucleated
4 fibres and importantly be orientated in fascicles that will allow uniaxial contraction. In order
5 for this to occur, the temporal requirements of nutrients, growth factors (both endogenous
6 and exogenous), matrix type and composition and the mechanical signal given by the custom
7 designed culture chamber are of primary concern when bioengineering skeletal muscle
8 (Khodabukus and Baar, 2016) and therefore not discussed extensively in the current review.
9 The majority of literature within this area looking to investigate mechanisms to exercise
10 stimuli utilize either rodent self-assembling fibrin or pre-assembled collagen gels, using
11 electrical stimulation and ramp, static or cyclic mechanical stretch to investigate the cellular
12 and molecular response to acute contraction or mechanical overload. There are numerous
13 studies investigating the use of non-biological, non-biodegradable or synthetic
14 materials/scaffolds. However, biological scaffolds such as collagen or fibrin have more *in-*
15 *vivo* like mechanical properties (e.g. stiffness) (Heher et al., 2015) and therefore have been
16 used much more frequently to investigate physiological adaptation to electrical and
17 mechanical stimuli to mimic *in-vivo* muscle contraction. Furthermore, even synthetic
18 scaffolds that are biodegradable are generally used for engraftment of bioengineered muscle
19 to treat muscle injury or disease and therefore the use of non-biological scaffolds are not
20 discussed in the present manuscript and are reviewed elsewhere (Mertens et al., 2014). The
21 majority of studies investigating exercise mimicking stimuli include *in-vitro* models that are
22 pre-cast/assembled matrices or self-assembling constructs. As alluded to above, the former
23 includes biological scaffold materials (such as collagen), where cells are seeded into the
24 collagen matrix often in pre-cast molds, which are then chemically polymerised and cast into
25 position under tension (Figure 1E-G). Where self-assembling constructs, originally known as
26 myooids (Dennis and Kosnik, 2000) use laminin and/or fibrinogen pre-polymerised
27 matrices, where contraction from cells adhering to the matrix grown in high serum (e.g. 10-
28 20%) media for a period of 2 days, lift and roll the thin polymerised fibrin/laminin gel from
29 the surface of a silicone coated plate into a muscle 'bundle' towards the points of tension that
30 are supplied by pre-prepared aligned sutures under strain from opposing aligned sterilised
31 stainless steel pins (Figure 1C, D). Together with this mechanical stimulus, upon initial self-
32 assembly cells are switched to low serum media (typically 2% sometimes with exogenous
33 IGF-I in human cells, or without in the C2C12 cell line that spontaneously differentiate
34 following serum withdrawal) to enable differentiation. After 2 days of myotube formation,
35 fibrin constructs are usually switched to 7% serum for a further 8-14 days to enable myotube
36 maturation (Khodabukus and Baar, 2009).

The early use of electrical stimulation to investigate skeletal muscle contraction *in-vitro*

37 Both monolayer and tissue engineered muscle myotubes have been shown to spontaneously
38 twitch during formation (Bursac et al., 1999). To enable sustained and repeated contraction,
39 researchers have utilised electrical stimulation of skeletal muscle cultures in monolayer
40 (Brevet et al., 1976; Kawahara et al., 2007; Thelen et al., 1997; Wehrle et al., 1994) and 3D
41 bioengineered constructs (Cheng et al., 2016; Donnelly et al., 2010; Hinds et al., 2011; Huang
42 et al., 2006; Juhas et al., 2014; Khodabukus and Baar, 2012; Langelaan et al., 2011; Park et
43 al., 2008; Rangarajan et al., 2014; Stern-Straeter et al., 2005). Indeed, in 1976, Brevet and
44 colleagues first developed a monolayer model of electrical stimulation to model skeletal
45 muscle contraction *in-vitro*. They isolated primary cells from the breast of 12-13 day old
46 chick embryos, cells were grown to confluence and differentiated for 4-5 days in low serum
47 media to enable the fusion of the muscle derived cells into myotubes. They subsequently
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3 provided electrical stimulation over a 34h period (0.6 s train of 10- to 20-ms biphasic pulses,
4 every 4 seconds making the stimulation approximately 7 hours with the remaining time as
5 rest)(Brevet et al., 1976). Even though the authors did not directly measure the effects of
6 electrical stimulation on morphological changes (myotube number and size), and the
7 stimulatory regimes in frequency and duration were more analogous to slow twitch fibre
8 recruitment patterns, electrical stimulation was sufficient to increase total myosin
9 accumulation (via SDS-PAGE) and protein synthesis (via incorporation of [³H] Leucine into
10 myosin extracts) by an average of 21% versus unstimulated controls. To the authors
11 knowledge, it was not until nearly 2 decades later that the effects of alternative chronic
12 electrical stimulatory regimes on fibre type properties within skeletal muscle cells isolated
13 from newborn rat hindlimbs (encompassing mixed fibre types) in an attempt to mimic both
14 slow and fast twitch activation patterns (Naumann and Pette, 1994). Specifically, electrical
15 stimulation duration was maintained for 20 days at bursts of 250 ms, every 1, 4 and/or 100 s
16 with pulse frequencies of either 15, 40, and 100 hz. Indeed, it was suggested that 250 ms
17 duration of stimulatory bursts, regardless of pulse frequency (15 Hz, 40 Hz, or 100 Hz),
18 repeated either every 1 or 4 s (burst frequency) induced an increase in the abundance of slow
19 myosin heavy chains whereas high frequency 250 ms bursts, even at 100Hz, but with bursts
20 repeated less often (every 100 s), enhanced the expression of faster myosin heavy chains but
21 not slow isoforms. The authors therefore suggested that the increased bursts rather than
22 pulse frequency resulted in a slower muscle phenotype and higher pulse frequencies with
23 less bursts being advantageous for evoking a fast fibre formation (MYHCI). With the
24 exception that, following an increased number of bursts (every 1 to 4s) at higher pulse
25 frequencies (100 Hz), slower fibre formation was still predominant. These stimulatory
26 regimes somewhat mimicked what is observed *in-vivo* skeletal muscle after aerobic exercise
27 (e.g. more repetitive/continuous contraction, akin to 1 or 4 s bursts in 3D muscle) where
28 lower force contractions (affiliated to pulse frequencies of 15 or 40 Hz *in-vitro*) elicit slow
29 fibre type adaptation vs. less frequent (bursts every 100s) but more forceful contractions
30 (e.g. 100 Hz pulse frequency) that elicit faster fibre formation mimicking resistance type
31 exercise. This group then went on to investigate the effects of higher number of bursts within
32 the regimes (14 days of 250 ms trains, 40 hz, every 4 s) on muscle cells isolated from
33 different adult rat muscle groups possessing different starting fibre-types (*soleus*, slow;
34 *tibialis anterior*, fast) (Wehrle et al., 1994). The protein abundance for the MYHCI isoform,
35 was found to be highest in cells derived from slow-twitch soleus muscle and lowest in the
36 cells derived from fast-twitch tibialis anterior. Therefore, this early monolayer work *in-vitro*
37 suggested that the fibre type of the originating muscle cells and the electrical stimulation
38 regime would be an important consideration in enabling suitable electrical stimulation
39 regimes in 3D bioengineered skeletal muscle. Since these studies it has now been observed in
40 3D bioengineered muscle that contractile properties and MYHC content are representative of
41 the originating fibre type of the bioptic tissue (Huang et al., 2006). Fibrin self-assembling
42 bioengineered skeletal muscle myooids using primary muscle derived cells originating from
43 slow soleus or fast tibialis anterior muscle were matured over 14 days and contractile
44 properties assessed via single twitch and tetanic electrical stimuli. Here, cells originating
45 from slow soleus muscle had altered contractile dynamics, with 30% slower half-relaxation
46 times (1/2RT) and time to peak tension (TPT), as well as reduced total MYHC content
47 compared with muscle constructs using cells originating from the fast tibialis anterior
48 (Huang et al., 2006). More recently, these data were confirmed in order to elucidate the
49 biochemical and molecular mechanisms for these fibre type specific observations in 3D
50 muscle. Following 10 days of construct maturation (2 days high serum, 8 days low serum),
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3 both single twitch and tetanic electrical stimulation was implemented to assess contractile
4 properties. Here, TPT and 1/2RT were slower in constructs made with cells isolated from
5 primary (C57BL/6) mice soleus muscles compared with tibialis anterior (Khodabukus and
6 Baar, 2015). These soleus 3D constructs were also more fatigue resistant and contained
7 higher levels of the mitochondrial proteins (SDH and ATP synthase), the fatty acid
8 transporter, Carnitine palmitoyltransferase 1 (CPT-1) as well as increased content of beta
9 oxidation enzymes (LCAD and VLCAD), alongside lower phosphofructokinase (PFK) activity,
10 representative of lower glycolytic flux and oxidative slow fibres. Muscle-fibrin constructs
11 made from cells isolated from the fast tibialis anterior had increased fast MYHC and fast
12 troponin C, I, and T isoforms, together with increased levels of sex determining region Y)-
13 box 6 (SOX6) and the six transcriptional complex (STC) proteins, EYA transcriptional
14 coactivator and phosphatase 1 (Eya1) and Six4 (Khodabukus and Baar, 2015). Indeed, it has
15 previously been observed that elimination of Six1, Six4, and the cofactor Eya1 can prevent
16 fast-twitch muscle fibre formation (Grifone et al., 2004; Niro et al., 2010; Richard et al.,
17 2011). Therefore, an increase in these proteins would serve to improve fast-fibre formation.
18 Taken together, this data suggests that cells remember or possess a memory of the niche
19 from which they were derived, in this instance the fibre type [reviewed in (Sharples et al.,
20 2016)]. Therefore, originating fibre types and donor source of isolated muscle derived cells
21 should be an important consideration when attempting to engineer skeletal muscle *in-vitro*.
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26 **Acute electrical stimulation to assess basal contractile properties of** 27 **bioengineered skeletal muscle *in-vitro***

28 Together with an appreciation for the origin of muscle derived cells and the subsequent
29 maturation of 3D bioengineered muscle, researchers have also been required to validate the
30 functional performance/contractile properties of the self-assembling 3D myocoid constructs
31 in order to establish their similarities and differences vs. *in-vivo* tissue and therefore their
32 potential utility in future research to investigate more chronic stimulation and subsequent
33 physiological/molecular adaptation. The first studies to do this provided single twitch and
34 tetanus electrical stimulation via custom-made transducers to self-assembling laminin
35 myocoids produced from primary rat muscle derived cells that had been allowed to
36 differentiate and mature over 15 days and contractile properties assessed over a period of 50
37 days (Dennis and Kosnik, 2000; Dennis et al., 2001). It was shown that when the 3D muscle
38 myocoids contracted spontaneously, they produced approximately 25 μN of force. When
39 stimulated electrically they produced a peak twitch force of 320 μN and a tetanic force of 575
40 μN (Dennis et al., 2001). Furthermore, by increasing the proportion of myogenic cells to
41 88% vs. non-myogenic cells via a pre-plating technique during cell isolation from bioptic
42 material (despite authors not stating the average myogenic purity without pre-plating, which
43 is typically between 40-75%), it was later shown that after 14 days of maturation, these
44 myogenically enriched cell populations myocoids could produce a tetanic force of 805 μN using
45 fibrin as the matrix within the self-assembling constructs (Huang et al., 2005). Indeed, all of
46 the authors above also observed qualitatively similar contraction profiles to adult muscle,
47 specifically the general appearance of a positive force-frequency relationship (depicted in
48 Figure 2) and normal length-tension relationships, as well as normal metabolic profiles
49 (Baker et al., 2003; Dennis and Kosnik, 2000; Huang et al., 2005). Furthermore, where the
50 enriched myogenic population were used, twitch-to-tetanus ratios of 2.5 were observed,
51 which is close to adult muscle range of 3 to 5 (Huang et al., 2005). Also, the specific force
52 (force relative to size of the muscle) of these constructs was 36.3 kN/m^2 which is similar to
53 44 kN/m^2 in the soleus muscle of 1-day-old Wistar rats (Close, 1964), albeit the specific force
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3 was not as large as 260 kN/m² that has been observed in adult skeletal muscle (Urbanek et
4 al., 2001). However, the specific force of 36.3 kN/m² reported by Huang et al., (2005) using
5 myogenically enriched fibrin constructs was 12.5-fold higher than the 2.9 kN/m² previously
6 described using laminin myooids unenriched with primary derived muscle cells (Dennis and
7 Kosnik, 2000). Furthermore, myotube size in these constructs was typically 10 µm in
8 diameter (Huang et al., 2005), similar to aneural rat primary myotubes (Wilson and Harris,
9 1993; Wilson et al., 1988). However, this was around 10-fold smaller than adult human
10 muscle fibres which are approximately 100 µm. Indeed, it has previously been reported that
11 when muscles are denervated *in-utero*, aneural myotubes fail to develop into fully adult
12 myofibre phenotypes, perhaps contributing to this discrepancy (Fredette and Landmesser,
13 1991; Harris et al., 1989; Wilson and Harris, 1993; Wilson et al., 1988). Therefore, as the
14 constructs are essentially aneural, it was suggested by these authors that perhaps more
15 chronic innervation of the bioengineered muscle would enable maturation from aneural
16 myotubes to more adult like fibres (Huang et al., 2005).
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20 **Chronic electrical stimulation of bioengineered skeletal muscle *in-vitro***

21 Following initial experiments described above exploring the contractile properties of 3D
22 bioengineered muscle in response to acute electrical stimulation, investigators have
23 implemented the use of electrical stimulation regimes over more chronic periods to enable
24 more mature adult phenotypes and improve functional contractile properties. For example,
25 after 14 days of maturation followed by 14 days of chronic low frequency electrical
26 stimulation (5 pulses at 20 Hz every 4 seconds, pulse width 1.5 ms and voltage 5V) resulted
27 in improved contractile dynamics with an average 15% longer TPT and a 14% increase in
28 1/2RT duration in the fibrin self-assembling myooid constructs with primary cells derived
29 from rat fast muscle tibialis anterior (Huang et al., 2006). However, this observation
30 occurred without a change in the total amount of force produced. Furthermore, TPT and
31 1/2RT were not increased in 3D constructs made from cells derived from the slow rat soleus,
32 although the same 14 day stimulation was able to increase the force produced in the slow
33 soleus 3D bioengineered constructs by 80% (Huang et al., 2006). Furthermore, Donnelly *et*
34 *al.*, (2010) undertook 7 days of electrical stimulation of bioengineered skeletal muscle using
35 the same fibrin self-assembling myooids as above, yet with a combination of 90% myogenic
36 population (C2C12's mouse cell line) and 10% 3T3 fibroblast cells to model a mixed
37 population of enriched primary isolated muscle derived cells yet using commercially
38 available cell lines. A regime of 4 pulses x 0.1 ms pulse width delivered in a 400 ms train
39 followed by 3.6 s recovery for a 7 day period was undertaken at either 1.25 V/mm, 2.5V/mm
40 and 5 V/mm. Indeed, 1.25 V/mm stimulation over 7 days resulted in increased force yet
41 lower excitability, shown by an increased rheobase (where rheobase refers to the electric
42 field required to produce 50% peak twitch force at a given pulse width, therefore, a decrease
43 in rheobase is a measure of increased excitability). Stimulation at 2.5V/mm increased force
44 production and excitability. However, force and excitability was decreased at 5 V/mm versus
45 relevant controls. This suggested that slower-moderate voltage stimulation was required to
46 improve functional performance of 3D bioengineered muscle and indirectly suggested that
47 the improved maturation of 3D bioengineered muscle was as a consequence of electrical
48 stimulation (albeit at lower voltages) versus controls. It is important to note that myotube
49 diameter was not investigated within this study to ascertain if more chronic electrical
50 stimulation could produce increases above 10 µm observed in aneural bioengineered muscle
51 discussed above, in order to move towards a more adult muscle fibre phenotype of closer to
52 100 µm fibre diameters. While this study established that 5 V/mm can cause decreased
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3 function as a consequence of electrochemical damage and established that 2.5 V/mm was
4 optimum, researchers also wished to identify the optimum pulse widths especially given that
5 *in-vivo* force of skeletal muscle increases as an increased number of motor units are
6 activated (Henneman et al., 1965) and this can be modelled *in-vitro* by increasing pulse
7 width or amplitude (Dennis and Dow, 2007; Dennis and Kosnik, 2000; Dennis et al., 2001).
8 Indeed, even in the presence of tetrodotoxin induced-denervation that blocks voltage-gated
9 sodium channels, pulse widths greater than 0.5 ms have been shown to lead to calcium
10 influx suggesting that a longer pulse width, for example that of 1.5 ms used in the study
11 above by Huang et al., (2006), maybe not as physiological (Cairns et al., 2007). Investigators
12 in 2012 attempted to investigate the optimum pulse width to evoke increases in force
13 production and excitability in 3D bioengineered skeletal muscle (90% all myogenic
14 population C2C12's plus 10% 3T3 fibroblast cells) after 24 hrs of continuous electrical
15 stimulation. Here, there was no significant increase or decrease in force when pulse widths
16 were increased from 0.25 to 1, 4, 9 and 16 ms (Khodabukus and Baar, 2012). Furthermore,
17 because excitability (refers to the ability to initiate and propagate depolarisation in skeletal
18 muscle) is an important function of skeletal muscle contraction, investigators also wished to
19 identify the excitability following different voltages and currents by determining rheobase
20 (defined above). Indeed, acute single twitch and tetanus stimulation at a pulse amplitude
21 greater than six-times rheobase, resulted in a reduction of 50% peak force (measure of
22 maturity), impaired contractile dynamics shown by a 2.4-fold slowed half relaxation time
23 (dynamics) and a 58% increase in fatigability. In comparison 4 x rheobase (pulse widths
24 ranging from 1 to 4 ms) resulted in the largest tetanic force, improved dynamics and reduced
25 fatigability without electrochemical damage (Khodabukus and Baar, 2012). Finally,
26 continuous stimulation for 24 h induced increases in force production when the electric field
27 was greater than 0.5 V/mm regardless of the pulse width i.e. electric fields at 0.7, 1 and 1.4
28 V/mm resulted in a 2.5-fold increase in force (0.30 vs. 0.67 kN/m²) versus controls. In this
29 investigation, the mTOR inhibitor rapamycin was able to prevent 40% of the increase in
30 force observed as a result of 24 hrs electrical stimulation. However, there were also no
31 observable changes in downstream p70s6K phosphorylation, alongside no increase in total
32 MYHC suggesting no changes in muscle size. Therefore, the increase in force observed after
33 24 hrs of stimulation was perhaps more likely due to cytoskeletal rearrangement rather than
34 increases in muscle size. This data combined suggest overall that pulse widths ranging from 1
35 to 4 ms, voltages of 0.7-2.5 V/mm and electric fields at 4 x Rheobase are required to elicit the
36 most advantageous maturity (assessed via force), improved force dynamics (assessed via
37 TPT and 1/2RT) and improved resistance from fatigue in 3D bioengineered skeletal muscle.
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Chronic electrical stimulation to mimic exercise regimes in 3D bioengineered skeletal muscle *in-vitro*

45 Khodabukus et al. (2015) was one of the first studies to attempt to mimic a continuous
46 exercise mimicking stimuli and investigate the physiological, biochemical and molecular
47 adaptation in 3D bioengineered skeletal muscle. This was achieved via altering contraction
48 duration (0.6, 6, 60, and 600 sec) of 14 days of stimulation in 3D bioengineered muscles
49 created from primary muscle derived cells from both the soleus and tibialis anterior of
50 C57BL/6 mice, while using a constant pulse frequency of 10 Hz. This regime was an attempt
51 to optimise slow fibre formation that would mimic more closely chronic endurance/aerobic
52 exercise *in-vivo* (Khodabukus et al., 2015). The authors suggested that all contraction
53 durations evoked a similar slowing of TPT and similar increases in total MYHC content and a
54 reduction in total fast myosin. Specifically, the greatest reductions in fast MYHC IIX were
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3 observed with contraction durations of 60 and 600 seconds as well as slower $1/2RT$'s in
4 these conditions. Finally, all regimes induced an oxidative fibre type phenotype via an
5 increased capacity for glucose transport (GLUT4), metabolic activity (SDH and
6 ATPsynthase), mitochondrial biogenesis (PGC, MEF2) as well as fat oxidation (CPT-1).
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10 Therefore, chronic low frequency stimulation of contraction durations of 60 and 600
11 seconds appear most advantageous to evoke similar metabolic adaptation to what occurs *in-*
12 *vivo* after aerobic exercise. However, at present, there are limited chronic stimulation studies
13 in 3D bioengineered skeletal muscle longer than 14 days, and/or that mimic resistance
14 exercise type stimulation regimes via higher frequency contractions, and the subsequent
15 adaptation with respect to anabolic/catabolic signaling pathways or gene regulatory systems.
16 It is worth mentioning that Donnelly et al., 2010 undertook higher frequency contractions in
17 myotubes (100 Hz) in monolayer and observed a greater increase in total protein synthesis
18 following higher 100 Hz stimulation vs. lower 10 Hz using the same stimulation protocol
19 (pulses delivered in 400 ms trains with 3.6 s recovery). Therefore, future experimentation in
20 3D bioengineered skeletal muscle should investigate higher frequency stimulation protocols
21 interspersed with recovery to mimic resistance exercise to evoke increases in muscle size.
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24 **Co-culture of neurons in aneural 3D bioengineered skeletal muscle**

25 Co-culture of neurons with engineered muscle have also been observed to improve muscle
26 development and maturation. However, the formation of functional neuromuscular
27 junctions (NMJs) within bioengineered tissues are rare (Larkin et al., 2006). Nonetheless,
28 functional NMJs have been identified when bioengineered skeletal muscle (generated using
29 C2C12 myoblasts embedded within Matrigel) are co-cultured with mouse neural stem cells,
30 as evidence by the myotube contractile response to chemical neuronal activation and the
31 subsequent dampening following NMJ chemical blockade (Morimoto et al., 2013). More
32 recently, co-culture of rat embryo (gestational age E14) motor neurons taken from the
33 ventral horn, seeded within a 3D type-I collagen matrix 4 days after the primary muscle
34 derived cells from neonatal rat muscle, were shown to enhance mRNA expression of a
35 number of markers of skeletal muscle maturation (Smith et al., 2016), suggesting that the
36 addition of a neural input may drive the contractile maturity of bioengineered skeletal
37 muscle. Indeed, further evidence for enhanced skeletal muscle phenotype as a result of
38 innervation within bioengineered skeletal muscle has been generated in 3D fibrin self-
39 assembling constructs. Again, using embryonic rodent motor neurons co-cultured with
40 neonatal primary muscle derived cells, it was established that the presence of motor neurons
41 can improve contractile properties after 18 days of total time in culture (Martin et al., 2015).
42 Indeed, following electrical field stimulation (1.2 ms pulse width, 100 Hz impulse frequency
43 train at 3.5 V/mm), the addition of embryonic motor neurons promoted increased maximal
44 twitch and tetanic force. Furthermore, cytoskeletal organisation improved, assessed via
45 immunohistochemistry analysis of desmin and MAP2 to highlight the muscle intermediary
46 protein filament and motor neurons respectively, and revealed myotube formation was in a
47 fascicular arrangement and that there was neurite outgrowth from motor neuron cell bodies
48 toward the aligned myotubes. Furthermore, chemical antagonism of the acetylcholine
49 receptor (AChR) using D-tubocurarine negated the increase in twitch frequency that was
50 improved in the presence of motor neurons, suggesting the presence of NMJ formation and
51 indicative of a successful innervation of the 3D engineered skeletal muscle constructs
52 (Martin et al., 2015). At present, the use of these motor neuron muscle derived cell co-
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3 cultures have not been used to investigate the role of acute or chronic exercise mimicking
4 stimuli, however these data may suggest that these models represent even more
5 physiologically relevant innervated muscle phenotype vs. an aneural constructs and
6 therefore their response to chronic stimulation would be an interesting area for future
7 investigation. This would be especially pertinent given that whilst contractile function was
8 improved following motor neuron addition, no hypertrophy was observed (Martin et al.,
9 2015), yet it maybe hypothesised that chronic electrical stimulation of these cultures may
10 evoke hypertrophy versus aneural cultures.
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12 **Mechanical loading of 3D bioengineered skeletal muscle**

13 Mechanical loading plays an important role in skeletal muscle tissue *in-vivo* and can regulate
14 muscle size, muscle cell differentiation as well as matrix remodelling. Indeed, continuous
15 passive tension to skeletal muscle by bone growth of approximately 2 mm/wk during
16 neonatal development influences muscle weight, length and myofibrillar organisation (Olwin
17 et al., 1994; Stewart, 1972). Following the first work by Goldberg that demonstrated a rapid
18 hypertrophic response after only 24 hr post tenotomy of a synergistic muscle (synergistic
19 ablation) (Goldberg, 1967), several groups have used this model of overload induced
20 hypertrophy (Armstrong et al., 1979; Esser and White, 1995; Kandarian et al., 1992;
21 Linderman et al., 1996). Indeed, using this model, mechanical overload can result in
22 increased amino acid transport (Goldberg, 1967; Goldberg and Goodman, 1969; Henriksen
23 et al., 1993) and satellite cell activation and proliferation (Rosenblatt and Parry, 1992;
24 Schiaffino et al., 1972) and a total increase in protein synthesis (Goldspink, 1977) along with
25 increases in protein sub-fractions within skeletal muscle (Cuthbertson et al., 2006).
26 Vandeburgh and colleagues initially laid down the foundations for the investigation of
27 mechanical cyclic stretch in skeletal muscle cells cultures using a collagen matrix and found
28 that stretch elicited an increase in total protein and myotube hypertrophy (Vandeburgh et
29 al., 1989; Vandeburgh and Karlisch, 1989; Vandeburgh et al., 1988). The first study to
30 mechanically stimulate 3D muscle used collagen coated elastic substratum's seeded with
31 muscle cells isolated from embryonic avian pectoralis muscle was Vandeburgh and Karlisch
32 (1989). The authors subjected these constructs to mechanical stretch of 300% of starting
33 collagen substratum length over 3 days at a rate of 0.35 mm/h (which is same rate that
34 which stretch stimulates *in-vivo* bone elongation during development) (Vandeburgh and
35 Karlisch, 1989). In these stretched constructs the authors observed increased myoblast
36 proliferation and fusion as well as increases in myotube length (Vandeburgh and Karlisch,
37 1989). Furthermore, to the authors knowledge the first study to mechanically load primary
38 human skeletal muscle cells (vastus lateralis) in 3D collagen/matrigel solutions cast in
39 silicone moulds was over a decade later (Powell et al., 2002). Once cast, muscle derived cells
40 were grown for a period of 2 days, and induced to differentiate in low serum media for 5
41 days, before being mechanically loaded after 8 days of myotube maturation (fibre diameter
42 average 6.4 μm). The mechanical load regime included stretch at 5% strain (1 mm) for 2
43 days, 10% strain (2 mm) for 2 days, and 15% strain (3 mm) for 4 days (total of 16 days, 8 days
44 maturation, 8 days loading). This loading regime induced an increase in myotube diameter
45 by 12% and area by 40% (Powell et al., 2002), suggestive that mechanical load evoked
46 considerable hypertrophy in 3D bioengineered human muscle. In an attempt to look more
47 closely at the molecular mechanisms of loading 3D muscle, Cheema *et al.*, (2005)
48 mechanically stretched 3D matrices seeded with C2C12 cells and polymerised in type I
49 collagen. Following differentiation to promote myotube formation (6 days low serum) they
50 elicited ramp and cyclic stretch regimes with 10% stretch of resting length applied as either 1,
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3 5 or 10 cycles/h for 12 h, and ramp stretch of 10% resting length over 10 min, 1 and 12 hr (10
4 min and 1 hr ramp load held at 10% stretch for the remaining 12 hrs). The authors observed
5 an increase in gene transcription of IGF-IEa that would code for IGF-I isoform IEa, shown
6 previously to be involved in myoblast differentiation (Yang and Goldspink, 2002) following a
7 single 10% ramp stretch over 1hr (and held at 10% for the remaining 12 hrs) but not after any
8 of the cyclic stretch regimes. Indeed, IGF-IEa actually decreased in a dose response manner
9 with increasing 10% stretch cycling per hour. In contrast, mechano growth factor
10 (MGF/IGF-IEb in rodents/IGF-IEc in humans), involved in the proliferation and self-
11 renewal of myoblasts, yet inhibition of differentiation (Yang and Goldspink, 2002), was
12 upregulated by both a single 1hr 10% ramp stretch and by 1 cycle/hr cyclic loading.
13 Therefore, this study was suggestive of a suitable anabolic response (IGF-IEa) following
14 ramp stretch that mimics bone growth, whereas cyclic stretch (that would not occur during
15 development) perhaps evoked enhanced proliferation and self-renewal of muscle cells. The
16 authors stated however, that due to only 6 days maturation, only 5% of all cells were
17 myotubes in the 3D collagen matrices. Therefore, as IGF-IEa and Eb are involved in
18 proliferation, differentiation and self-renewal in myoblasts, this study perhaps represented
19 model of muscle development following bone growth (e.g. ramp stretch) and therefore its
20 results cannot be necessarily extrapolated to the effect of mechanical loading on mature
21 skeletal myotubes. Subsequent studies confirmed that the application of mechanical static
22 load (10% stretch of resting length for 6 hrs per day, separated by 18 hrs of 3% stretch for a
23 total of 6 days- 3 days after initial cell seeding) during C2C12 myoblast differentiation
24 (rather than of mature myotubes) within 3D fibrin cast bioengineered skeletal muscle did
25 lead to increased differentiation, myotube formation (myotube number), size (diameter and
26 length), and increases in myogenic regulator factors gene expression, myogenin as well as
27 sarcomeric patterning more similar to native skeletal muscle tissue (Heher et al., 2015).
28 However, loading of constructs following extensive myotube maturation was also not
29 provided in this study. Therefore, studies using smaller collagen gel sponge constructs
30 attempted to differentiate constructs for longer (7 days) and in the presence of exogenous
31 IGF-I to promote myotube formation and hypertrophy and applied again both ramp and
32 cyclic loading (Auluck et al., 2005) to the resultant myotubes. In these studies, 3D collagen
33 sponges containing human craniofacial muscle derived cells were stretched to 15% of resting
34 length that was continuously held over 6 hrs. While authors did not investigate IGF-I gene
35 expression, the regime evoked higher protein activity of the matrix metalloproteinase 2
36 (MMP-2) versus non-loaded controls and vs. cyclic stretch e.g. 1.5 min stretch, 1.5 min hold
37 followed by 1.5 min release of strain repeated for 6 hrs (Auluck et al., 2005). MMP-2 is an
38 enzyme produced by muscle cells used to degrade and turnover the matrix around it in order
39 to enable matrix remodelling. Therefore, this data suggests that ramp loading *in-vitro*, may
40 enable the enhanced matrix remodelling for subsequent myotube formation and
41 hypertrophy if stimuli was chronically applied. However, authors were unable to characterise
42 myotube formation as the collagen sponges did not permit immunohistological analysis to be
43 performed, and therefore again these studies were unable to confirm the maturation of the
44 3D muscle myotubes. In an attempt to somewhat rectify this issue, 3D constructs using type
45 I collagen (similar to that used by Cheema et al., 2005 described above), were matured for
46 the longer period of 14 days (vs. 6 days by Cheema et al., 2005)(Player et al., 2014). This
47 maturation period was also similar to that used previously in fibrin 3D muscle (discussed
48 extensively above) that possessed a more mature muscle phenotype vs. shorter maturation
49 periods. Indeed, immunohistological images presented in the manuscript displayed highly
50 aligned myotubes in parallel Figure 1E&F (Player et al., 2014). Mechanical load was applied
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3 to these more mature constructs via static loading comprising of 10% stretch that was held
4 for 1 hr to mimic synergistic ablation *in vitro* vs. ramp load which was a continuous increase
5 over 1 hr until 10% stretch was attained. IGF-I and matrix metalloproteinase 9 (MMP-9)
6 gene expression was higher with static loading vs. ramp loading suggesting a positive
7 anabolic response to static loading as well as producing an elevated signal for matrix
8 remodelling that would potentially preceding hypertrophy if the signal was chronically
9 maintained. Furthermore, there was no changes observed following loading for negative
10 regulators of muscle mass, myostatin mRNA or ubiquitin ligases (MuRF and Marfbx)
11 involved in protein degradation of muscle specific proteins gene expression. Interestingly,
12 there was increased IGFBP2 in static loading conditions and reduced IGFBP5 gene
13 expression in both static and ramp loading conditions. At the protein level, these binding
14 proteins act as soluble clearance molecules for IGF. Therefore, modulating the ability of IGF-
15 I to bind to its receptors depends on whether IGF is bound to the binding proteins or
16 cleaved. Indeed, higher/ lower IGFBP2 results in impaired differentiation and myotube
17 atrophy vs. improved differentiation and myotube hypertrophy in myoblasts (Sharples et al.,
18 2013; Sharples et al., 2010), and excess IGFBP2 expression in mice reduces muscle size
19 (Rehfeldt et al., 2010) suggesting that potential positive anabolic response of increased IGF-I
20 could be compromised with elevating IGFBP2 in static load conditions. However, both
21 conditions saw reductions in IGFBP5 that would potentially increase the availability of IGF-I
22 in loaded 3D muscle constructs.
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27 Overall, these studies suggest that mechanical loading experimentation within 3D muscle to
28 investigate lengthening and relaxing of muscle and the subsequent molecular responses to
29 load in adult skeletal muscle phenotypes has been somewhat limited by the lack of
30 experimentation in fully mature myotubes in 3D constructs. Furthermore, there are
31 currently limited investigations into relevant anabolic cell signalling allowing relevant
32 comparisons to acute exercise *in-vivo*. To further compound these issues, contradictory
33 evidence in monolayer studies suggests that cyclic stretch in differentiated rat L6 myoblasts
34 actually impairs protein synthetic associated cell signalling as well as protein synthesis itself,
35 albeit increasing the activity of the potential mechanosensor, focal adhesion kinase (FAK)
36 (Atherton et al., 2009). This suggests that there may be an alternative molecular response to
37 lengthening contractions vs. what is observed following shortening concentric contraction.
38 Alternatively however, stretch in C2C12 myotubes in monolayer has been shown to increase
39 P70S6K activation (Baar et al., 2000). Also, the use of more mature aligned myotubes in 3D
40 collagen constructs or via the use of fibrin/laminin self-assembling 3D muscle that has been
41 shown to produce mature aligned myotubes (specially following electrical stimulation/motor
42 neuron co-culture) may be important to elucidate the influence of mechanical stretch on the
43 molecular mechanisms (and perhaps in combination with electrical stimulation for
44 concentric contraction) to determine the underlying physiological adaptation to exercise
45 mimicking stimuli. Furthermore, studies are limited to fairly acute stimulation and therefore
46 limited with respect to assessing the impact of mechanical load on longer term muscle
47 hypertrophy and the associated mechanisms. Also, there are currently limited studies that
48 combine the use of electrical stimulation and mechanical load that would be more relevant to
49 physiological contraction *in-vivo* and could potentially mimic more closely both shortening
50 concentric and lengthening eccentric contraction. Indeed, the only study to the authors
51 knowledge to combine these two modes of stimulation included intermittent cyclic stretch
52 (5% amplitude, 1 Hz for 1 h with 5 h of rest for total of 7 days) and electrical stimulation
53 (4 V/cm) to C2C12 cells seeded within synthetic aligned electro-spun polyurethane (PU)
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3 fibers (Liao et al., 2008). This regime increased the percentage of striated myotubes from 70
4 to 85%, which was accompanied by an increase in contractile proteins such as α -actinin and
5 myosin heavy chain. Despite this, the combination of mechanical load and electrical
6 stimulation was unable to elicit larger increases versus the individual modes of stimulation
7 alone. However, it is worth mentioning that this was conducted using non-biological
8 scaffolds that perhaps do not mimic the response that may be observed using biological
9 matrices. Also, the stimulation was low frequency and continuous mimicking aerobic
10 exercise where even greater increases in myotube hypertrophy maybe observed after higher
11 frequency intermittent contractions with adequate rest cycles repeated over time.
12 Furthermore, given the discrepancy within the literature over the lack of cell signaling
13 response to acute lengthening (Atherton et al., 2009) versus acute electrically stimulated
14 contractions and the limited work conducted into the investigation of the underlying
15 mechano-signal transduction thought to lead to hypertrophy, for example the potential role
16 of focal adhesion kinase (FAK) (Crossland et al., 2013; Fluck et al., 1999), phospholipase D/
17 phosphatidic acid (Hornberger et al., 2006), mTOR (Baar and Esser, 1999), mitogen
18 activated protein kinases e.g. ERK (Miyazaki et al., 2011) in 3D muscle in response to high
19 frequency intermittent regimes, the investigation of these pathways following the
20 combination of electrical stimulation and mechanical stimulation in 3D bioengineered
21 skeletal muscle requires future investigation. More recently the latest technology bioreactors
22 are becoming more commercially available that allow both mechanical stretch and electrical
23 stimulation of 3D cultures (depicted in Figure 3), and are fully aseptic with perfused media
24 control, potentially also allowing more chronic exercise mimicking regimes to be applied,
25 especially if using self-assembling myoids using biological scaffolds and primary derived
26 muscle cells that incorporate matrix maintaining fibroblasts that have been shown to be
27 viable for 50 days (Dennis and Kosnik, 2000; Dennis et al., 2001). To the authors knowledge
28 however, there have been no studies undertaken in 3D skeletal muscle that have combined
29 both chronic mechanical loading and electrical stimulation, therefore this also warrants
30 future investigation.
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36 **Summary and Future directions**

37 There are currently some exciting advances into optimising the maturation of the most adult
38 like skeletal muscle tissue in 3D bioengineered constructs using electrical stimulation, motor
39 neuron co-culture and mechanical loading. However, the molecular mechanisms
40 underpinning the adaptation of 3D bioengineered muscle with a mature adult phenotype
41 following acute continuous stimuli, mimicking aerobic exercise, are only just beginning to
42 emerge with a distinct lack of investigations focusing on investigating higher frequency,
43 intermittent stimulation regimes mimicking resistance type exercise. Therefore, it is
44 envisaged that technology that allows both concentric shortening and eccentric lengthening
45 via the use of the latest bioreactor technology that permits simultaneous mechanical and
46 electrical stimuli, will enable experimentation into this field to progress in the future
47 (depicted in Figure 3). Importantly, while genetic modification in 3D cultures have been
48 performed previously (examples include (Du et al., 2014; Evans et al., 2017; Romero et al.,
49 2016), the use of this molecular tool has only emerged recently in bioengineered skeletal
50 muscle (Cheng et al., 2016). Therefore, we envisage, in the near future, that these 3D *in-vitro*
51 skeletal muscle systems may more easily allow for genetic modification (gene
52 silencing/overexpression) (Cheng *et al.*, 2016), pharmacological inhibition (Khodabukus and
53 Baar, 2012), alterations in the hormonal background (Huang et al., 2005) and/ or pre-
54 clinical therapeutics being applied to more biologically relevant human muscle testing
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3 systems that cannot be readily undertaken within *in-vivo* human experimentation due to
4 ethical and safety concerns. Additionally, studies have also attempted to mimic aged-related
5 muscle loss in 3D bioengineered skeletal muscle (Sharples et al., 2012) opening up the
6 possibility to investigate the associated mechanisms of anabolic resistance to load and
7 nutrients observed in ageing muscle *in-vivo* following the mimicking of exercise and/or
8 nutrient manipulation in 3D bioengineered skeletal muscle. Finally, because isolated muscle
9 cells from different environmental niches *in-vivo* (e.g. physically active, diabetic, cancer
10 cachectic, obese and sarcopenic) remember their prior environment once isolated *in-vitro*,
11 and take on characteristics of their disease state, reviewed in detail by our group recently
12 (Sharples et al., 2016), bioengineering of skeletal muscle may enable the application of
13 potential therapies in models of human age-related muscle loss and muscle loss disease
14 using cells isolated from the skeletal muscle from patients (e.g. sarcopenia, sarcopenic obese,
15 type II diabetic, cancer cachectic).
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19
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22

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For Peer Review

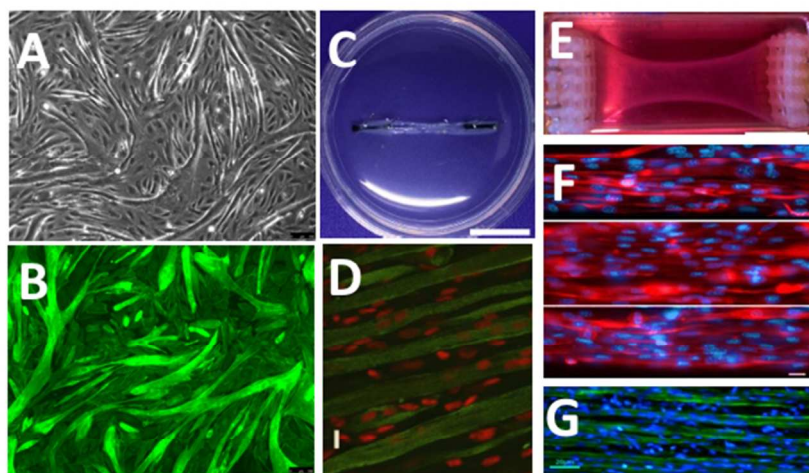


Figure 1. A) Typical Light and, B) fluorescent microscope images (10X, actin- green) of skeletal muscle cells (C2C12) in monolayer cultures and the resulting swirling myotube formations that occur when no tension is applied to cultures (scale bar 100 μ m) (images from unpublished images taken by Sharples Lab). C) Fibrin 3D bioengineered skeletal muscle using human derived muscle cells (scale bar 1 cm), used with permission from Martin et al. (2013) D) Aligned myotube formation in 3D bioengineered fibrin/human muscle derived cell constructs under tension (scale bar 20 μ m) demonstrated by fluorescently staining for desmin (green) and nuclei (red), used with permission from Martin et al., (2013). E) Type I collagen 3D bioengineered skeletal muscle using myoblast cell line C2C12s (scale bar 10 mm), used with permission from Player et al. (2014). F) Aligned myotube formation muscle using C2C12 myoblasts in collagen type I bioengineered constructs under unilateral tension (scale bar 20 μ m), used with permission from Player et al., 2014. G) Fluorescently stained muscle fibres from muscle tissue suggesting that bioengineered muscle morphologically mimics native skeletal muscle tissue (scale bar 20 μ m), used with permission from Smith et al. (2012).

Figure 1

338x190mm (54 x 54 DPI)

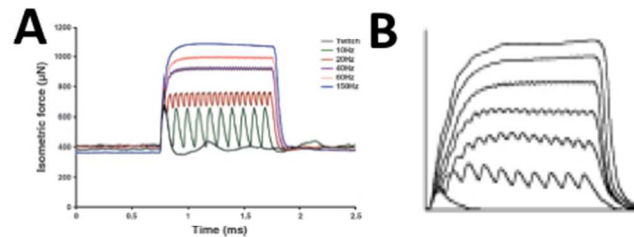


Figure 2. Data suggest that force-frequency traces (A, left) produced by 3D bioengineered skeletal muscle at different frequencies of electrical stimulation with summation beginning at 20 Hz and the constructs reaching a fused tetanus above 80 Hz are similar with (B) force frequency relationship of in-vivo muscle tissue observed in men and women. when stimulating at 1, 10, 15, 20, 30, 50 and 100 Hz (in ascending order). A) Used with permission from Huang et al. (2005) B) Used with permission from Wust, et al. (2003).

Figure 2

338x190mm (54 x 54 DPI)

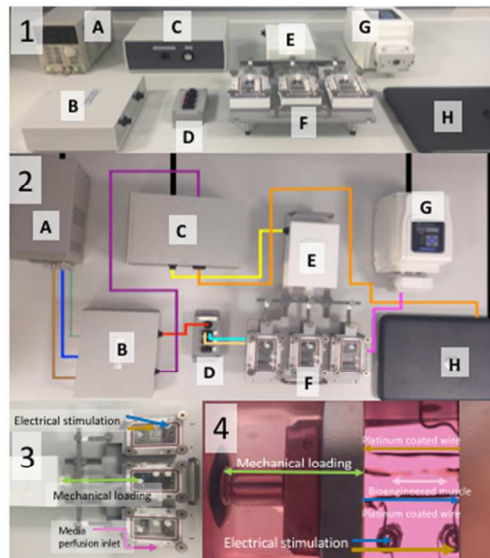


Figure 3. 1) An example of a novel bioreactor system allowing mechanical loading, electrical stimulation and perfused 3D cell culture chamber that can all be housed into an humidified Co₂ incubator. A) Electrical stimulation module, B) Electrical stimulation output box, C) Control Module, D) Electrode anode/cathode Splitter, E) Bioreactor mechanical stimulation box, F) Bioreactor 3D cell culture chambers, G) Peristaltic pump/ perfusion Box, H) Laptop and controlling software. 2) Depicts electrical connection setup of the bioreactor. Black - Mains power, Orange - Laptop (G) to Control Module (C), Yellow - Control Module (C) to Bioreactor mechanical stimulation box (E), Brown - Anode (+ve) from Electrical Stimulation Module (A) to electrical stimulation output box (B) Green - Neutral from electrical stimulation module (A) to electrical stimulation output box (B), Blue - Cathode (-ve) from electrical stimulation module to electrical stimulation output box (B), Purple - Control Module (C) to electrical Stimulation Module (B), Red - Electrical Stimulation Output Box (B) to Electrode Anode/Cathode Splitter (D). Peach/Gold - Anode (+ve) from Electrode Anode/Cathode Splitter (D) to Bioreactor 3D cell culture chambers (F), Light blue - Cathode (-ve) from Electrode anode/cathode splitter (D) to Bioreactor 3D cell culture chambers (F), Pink - Perfusion Box (G) to bioreactor 3D cell culture chambers (F). 3) Detailed image of the bioreactor allowing simultaneous mechanical loading, electrical stimulation and media perfusion into the 3D cell culture chambers. 4) Detailed image of the bioreactor 3D cell culture chamber with a C2C12 fibrin self-assembling 3D myoid inserted. Image shows that the 3D muscle can be mounted and mechanically loaded via movement of the mechanical arm as well as electrically stimulated via surrounding platinum coated wires from the incoming electrical stimulation input.

Figure 3

338x190mm (54 x 54 DPI)