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# A Novel Compact Fractal UWB Antenna with Triple Reconfigurable Notch Reject Bands Applications

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**Abstract:** A compact, circular UWB fractal antenna with triple reconfigurable notch rejection bands is proposed. It rejects the crowded frequency bands WiMAX, WLAN and X band interferences produced in UWB communication systems. The proposed fractal structure consists of a basic circular patch with circular fractal iterations. By employing this new structure of fractals, the overall size of antenna is reduced 53% to 21x25 mm, in comparison with traditional circular monopole antenna. The implemented antenna operates at 3.1-10 GHz. Reconfigurability is realized by designing slots and split ring resonators in desired frequencies with the attached PIN diodes. WLAN band rejection was realized by creating a pair of optimized L-shaped slots in the ground plane. By etching a split ring resonator and a U-shaped slot, X and WiMAX bands were also rejected. Furthermore, by attaching diodes to aforementioned slots and designating the diodes on/off, different bands can be included or rejected. In time domain, the antenna properties are evaluated by a figure of merit called fidelity factor. Finally, the antenna properties are measured in anechoic chamber and the results agrees with simulation findings.

## 1. Introduction

The allocation of 3.1 to 10.6 GHz band by FCC as Ultra-Wide Band (UWB) application is now well established for both UWB systems and antenna designers. Studying some antenna designers attempts [1,2], by designing different slots such as T and L slots as well as tuning stubs, the 80% band width is achieved with a less-than-satisfactory gain. In [3], electromagnetic band gap structures (EBG) and defected ground are used to attain a wide band scenario. Another method studied in [4], employs multilayer structures and places gaps between patch and ground plane to provide a 66% bandwidth with average gain of 3dB. It must be emphasized that, most of the considered methods have limitations in fabrication and antenna specs enhancement. Another possible method for designing an UWB antenna is the use of fractal structures. Fractal structures are usually utilized because of their suitable radiation patterns and UWB bandwidth, which are a result of fractals self-similarity and space-filling properties [5, 6]. Fractal antennas have compact sizes, impedance compatibility, high directivity, and can be designed for

multiband and broadband applications. Some of the most popular fractal geometries are Minkowski fractals, Serpienski fractals, recursive trees, Hilbert curves, and Koch structures [7, 8]. Within such a wide band that UWB is situated, many different systems with their appropriate bands exist that could well produce frequency interferences. The three major narrow band systems, Worldwide Interoperability for Microwave Access (WiMAX) in 3.3–3.8GHz band, Wireless Local Area Network (WLAN) in 5.15–5.85GHz band, and X-band (military satellite communication) in 8–10GHz band, not mentioning many different RFID bands that could exist within UWB bands regions can cause interference over UWB antennas. To overcome such interferences, UWB antennas with notches in the mentioned frequencies are required. In [9-19], several UWB antennas with notch band characteristics are presented that employs EBG and defected structures for rejecting application. Moreover, as WLAN is more prone to interference in comparison with WiMAX and X-band, so single-band/dual-band selectivity for WiMAX and X-band can be very useful [20-23]. Indeed, employment of antennas with configurable notch band selectivity can be desirable. But this method makes antenna bigger in size and more complex in design. In [24] unwanted band is rejected by placing a T-type slot on the patch microstrip. In [25], a pair of parasitic strips are placed beside the feed line to reject WLAN band. Other means of unwanted frequency band rejection, studied in the literature, include placing half wavelength and quarter wavelength resonators as well as cutting away H-shaped slots from the radiating patch [26, 27]. In [28], a desired band-notch antenna is achieved by etching a narrowband dual resonance fractal binary tree into the radiating element of UWB antenna. In this paper, a new UWB circular fractal reconfigurable antenna with band rejection capability is proposed. Two L-shaped slots are used besides feed line to reject WLAN band. For WiMAX and X band rejections, a simple U-shaped slot and a C-shaped split ring resonator are employed, respectively. In order to enable reject band selectivity, PIN diodes are embedded in the middle of the defined slots appropriately, so that by switching diodes, unwanted frequency bands can be filtered out. The switches cause changes in the current path and antenna electrical length. In fact, by placing switches on the slots, the electrical length and antenna notch frequencies can be altered [29, 30]. In 3GHz and higher bands, the antenna simulated and measured  $S_{11}$  is below -10dB. The substrate is FR-4 with  $\epsilon_r = 4.4$  and loss tangent of 0.025. The antenna dimensions are 21x25mm<sup>2</sup>. Design and fabrication of this fractal antenna is much simpler and cheaper in comparison with many other fractal counterparts.

## 2 Antenna design procedure

### 2.1 Design of Fractal Circular Patch Antenna (FCPA)

In this section, a new Fractal Circular Patch Antenna (FCPA) design process is explained in details. The original antenna is a circular patch set by smaller circular patches (CPs) with fixed distances from center point of the original CP. In figure 1, the constitutive parameters of fractal antenna is demonstrated.  $r_1$  represents basic patch radii and  $r_2, r_3, \dots$  are the radius of other iterations. The  $a_n$  acts as sequential coefficients between sequential  $r_n$  ( $r_n = a_n \times r_{n-1}$ ). This figure also shows that, in each iteration two new CP enter the antenna design process. The

angle between two adjacent CP at the center from previous iteration CP is shown by  $\gamma_n$ . Another factor that makes crucial effect on antenna size and operation is  $D_n$ . This is formulated as:

$$D_n = \frac{P_n}{r_n + r_{n-1}} = \frac{r_n + r_{n-1} - d_n}{r_n + r_{n-1}} = 1 - \frac{d_n}{r_n + r_{n-1}} = 1 - \frac{1}{1 + a_n} \cdot \frac{d_n}{r_{n-1}} \quad (1)$$

In fact,  $D_n$  stands for how much overlapping two sequential CPs may have.

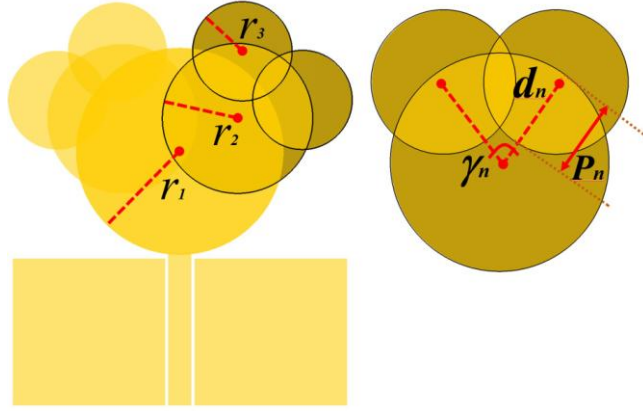


Fig. 1 The general sketch of FCPA with the antenna depiction at second iterations.

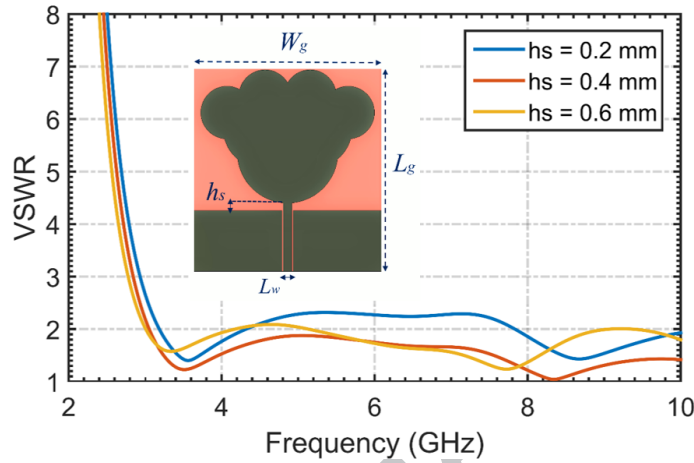
By changing any parameters, the antenna size and bandwidth will alter. Thus, the best results must be chosen, i.e., high bandwidth and minimum size. This could be achieved by various optimization methods. In this paper the FCPA is fulfilled at second iterations.

### 2.1.1 A practical problem

In figure 2,  $W_g$  and  $L_g$  are the substrate length and width at 21mm and 25 mm, respectively.  $h_s$  is the distance between antenna and ground plane.  $L_w = 1.5mm$  that denotes the feed line width.  $L_w$  and the distance between feed line and ground plane are chosen such that the feed line is matched with  $50\Omega$  impedance. The substrate which is used in simulations is FR-4 with  $\epsilon_r = 4.4$  and loss tangent of 0.025 To define the constitutive parameters  $a_n$ ,  $r_n$ ,  $\gamma_n$  and  $D_n$  of the proposed FCPA (Fig. 1), by which the antenna operates in desired bandwidth of 3-12 GHz, a genetic optimization algorithm is employed. To make the optimization algorithm faster and easier, it is assumed that the parameters value of  $D_1$  and  $D_2$  are the same and  $\gamma_n = \gamma_1 = \gamma_2$ . And after optimization process, the following parameter are found as;  $r_1=6.6mm$ ,  $a_2=0.8$ ,  $a_3=0.6$ ,  $D_1=0.6$ ,  $D_2=0.6$ ,  $\gamma_n=65^\circ$ .

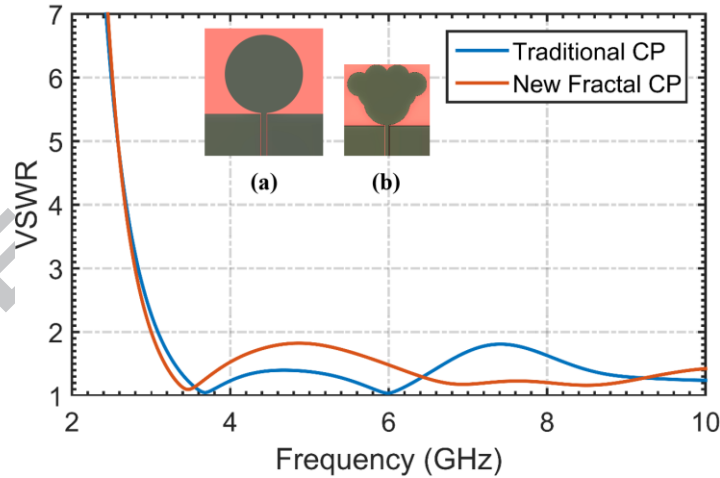
The result of analysis of  $h_s$  parameter is shown in figure 2. To find the efficiency of this method, the FCPA is compared with simple CP. The relation between dimensions and resonant frequency in circular patch antenna at initial stage are as reference [31]. According to [31], the radius of a simple circular patch for resonating at 3GHz is

14mm and by simulation, the overall size of 30x36 for simple CP. Considering same bandwidth for FCPA and simple CP by applying the proposed fractal, the miniaturization of %53 is achieved as shown by figure 3. In figure 5, the original antenna and iterations one and two are shown. All the three antenna dimensions are considered the same, i.e., taking into account fractal iterations effect. The radius of the initial antenna (Fig. 5(a)) is 9mm, and the radius of basic antenna in first and second iterations (Fig. 5(b) - Fig. 5(c)) are 8mm and 6.6 mm respectively. The results of the return loss for different antenna iterations can be observed in figure 6.

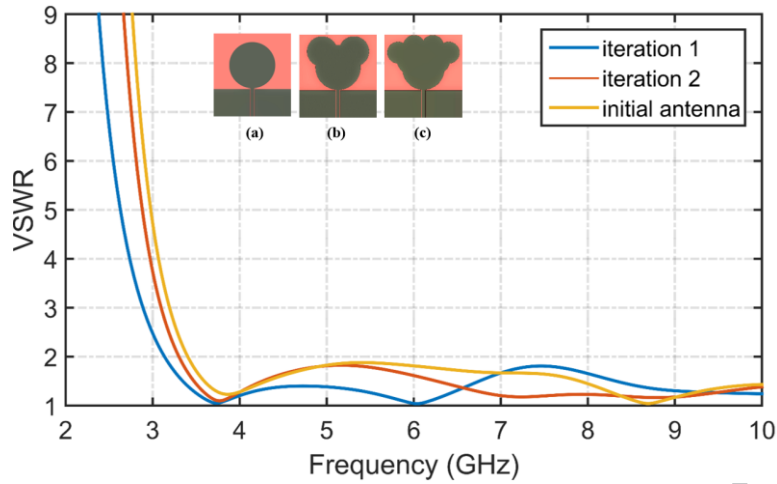


**Fig. 2** Proposed FCPA configuration with  $h_s$  parameter demonstration, VSWR optimization in terms of  $h_s = 0.2, 0.4, 0.6$

As demonstrated in figure 2, changes in  $h_s$  (the distance between patch and ground plane), have considerable effect on impedance matching and return loss.



**Fig. 3** Comparison between return loss of (a)-Traditional circular patch(CP), (b)- Second iteration of the proposed fractal antenna



**Fig. 4** (a) Geometry of the simple traditional CP. (b) Iteration-1 of the fractals. (c) Iteration-2 of the fractals, shown in figure 1

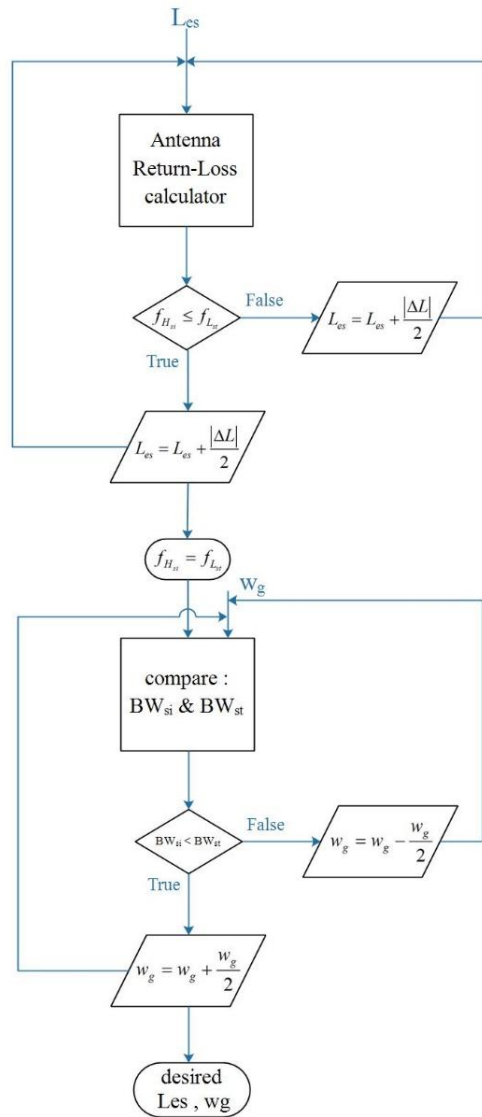
As it can be seen in figure 4, the bandwidth in iteration 2 is increased to 3.05-10 GHz that, in respect to initial antenna of 3.6-10GHz, a significant increase can be observed. It can be observed that, by making the antenna a fractal kind, the impedance matching in the lower frequencies has improved. The fractal shaped boundary increases the electrical length and thereby magnetic current path of antenna.

## 2.2 Notch Band Rejection Implementation

By etching two modified L-shaped slots beside the feed line, a notch in WLAN frequency band is implemented. Also, by designing of a C-type slot and a split ring resonator, WiMAX and X bands are rejected too. Approximate length of each slot is calculated by:

$$L_{notch} = \frac{c}{2f_{notch}\sqrt{\epsilon_{eff}}} = \frac{\lambda_g}{2} \quad (2)$$

where  $L$ ,  $c$ , and  $\epsilon_{eff}$  denote slot length, speed of light in free space, and effective dielectric constant, respectively [32]. Because of the approximations involved in (2) and variations in conditions of the environment, in general, total band rejection is not achieved. To overcome this problem, an optimization algorithm to calculate appropriate slot length is proposed. Flowchart of the algorithm is shown in figure 7. The embedded slots over the FCPA is shown in figure 8.



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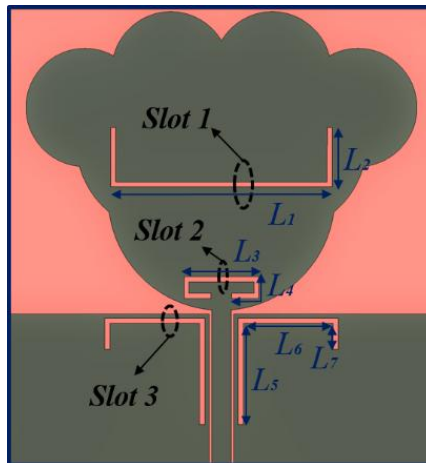
**Fig.5** Flowchart for the optimized design algorithm

The parameters given in figure 5 are as follows:

$L_{eff} = L_{effective}$

$L_{es} = L_{estimated}$

$|\Delta L| = |L_{es} - L_{eff}|$



**Fig. 6** The embedded slots shape to reject the mentioned bands

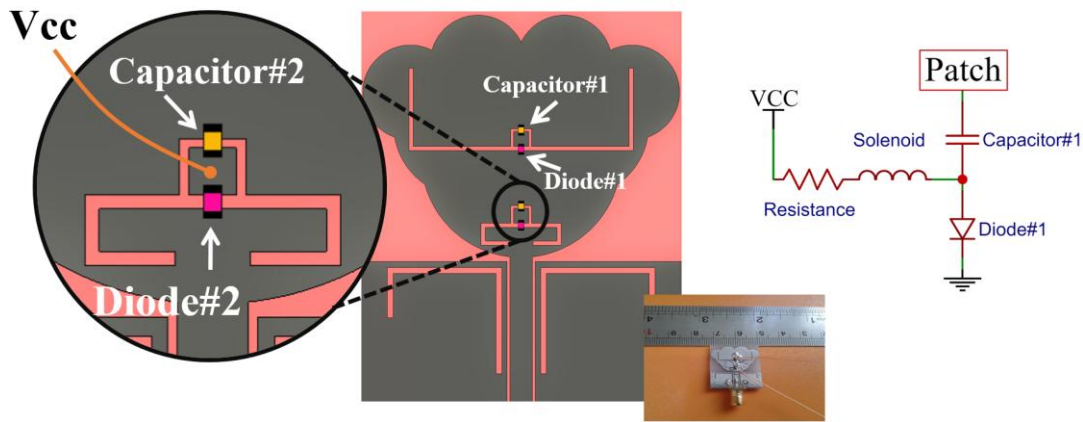
So, the purposes of the slots in figure 6 are slot one to reject the WiMAX band and slots 2 and 3 to reject X-band and WLAN, respectively. Considering (2) and figure 6, the slot sizes can be calculated as,

$$\begin{aligned} L_{slot1} &= L1 + 2 * L2 \approx \lambda_g/2 \\ L_{slot2} &= L3 + 2 * L4 \approx \lambda_g/2 \\ L_{slot3} &= L5 + L6 + L7 \approx \lambda_g/2 \end{aligned} \quad (3)$$

Implementing the flowchart of figure 5, the optimized values of the slot sizes are,

$$L1 = 15, L2 = 5.6, L3 = 4.6, L4 = 3.4, L5 = 7.2, L6 = 7.5, L7 = 3.4$$

As shown in figure 7, by attaching two PIN diodes on slot 1 and slot 2, they become reconfigurable. So, by biasing the diodes and switching them on or off, each band can be rejected at will. For this purpose, two Infineon BAR50-02v PIN diodes were chosen. Some experimental researches [33-36] are carried out employed PIN diodes as means of antenna reconfiguration that present technical biasing tips. In the biasing circuit, a 100pF capacitor is used to isolate DC and RF signals. Diodes are biased with a DC power supply (VCC) to a common node of the each capacitor and diode. A series inductor-resistor with values of 3nH and 50Ω is used in DC supply path in order to prevent RF signal from damaging DC supply.



**Fig. 7** Geometry parameter of the proposed reconfigurable fractal UWB antenna with PIN diode configuration and Fabricated antenna with DC biased diodes

### 3 Simulation Results

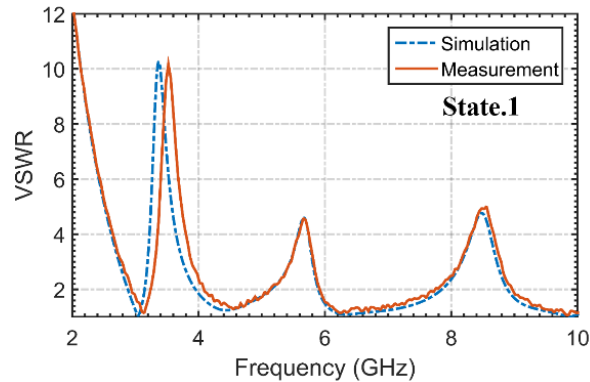
#### 3.1 Antenna Reconfigurability

In figure 8, simulation and measurement results for S11 parameter of the reconfigurable circular fractal patch antenna is shown. Diodes D1 and D2 are placed on U-slots, so that by switching them on and off, WiMAX and X bands can be reconfigurably rejected. Measurement is performed using Agilent E5071C Vector Network Analyzer.

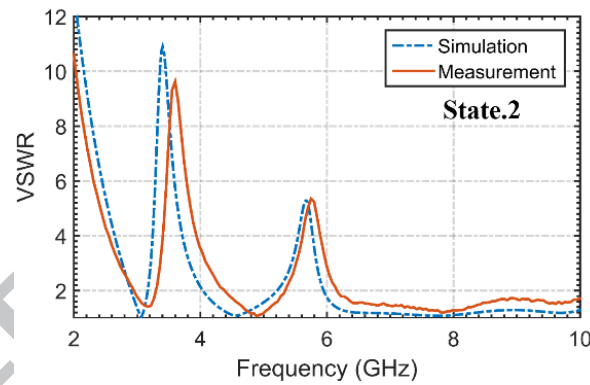


It is observed that, good agreement exists between measurement and simulation results. VSWR graph shown in figure 8 for different band rejection configurations are described by 4 states as below:

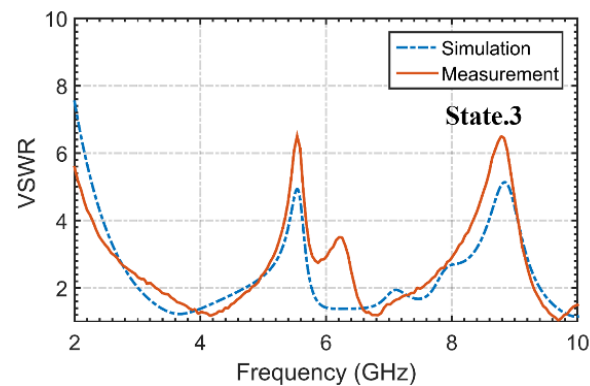
- (a)- state1, when both diodes are off, UWB antenna with triple notch band rejection is achieved.
  - (b)- state2, when Diode1 is switched off and Diode2 is switched on, the antenna rejects WiMAX and WLAN bands.
  - (c)- state3, when Diode1 is switched on and Diode2 is switched off, the antenna acts as a UWB antenna with WLAN and X-band rejection.
  - (d)- state4, when both diodes are switched on, antenna radiates in all UWB frequency range, except WLAN band.
- As demonstrated in figure 8, changes in switching state of the diodes provides reconfigurable notch band rejection.



(a)



(b)



(c)

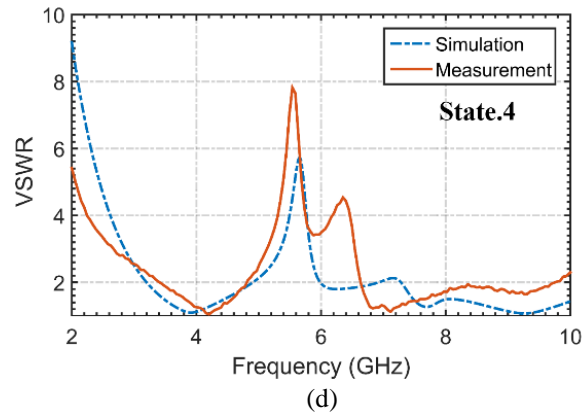


Fig 8. Simulation and measurement results for  $S_{11}$

In figure 9, surface current density distribution in reject-band frequencies can be observed. In notch band frequencies, most of the current flows through edges of the slots which causes low gain and low radiation.

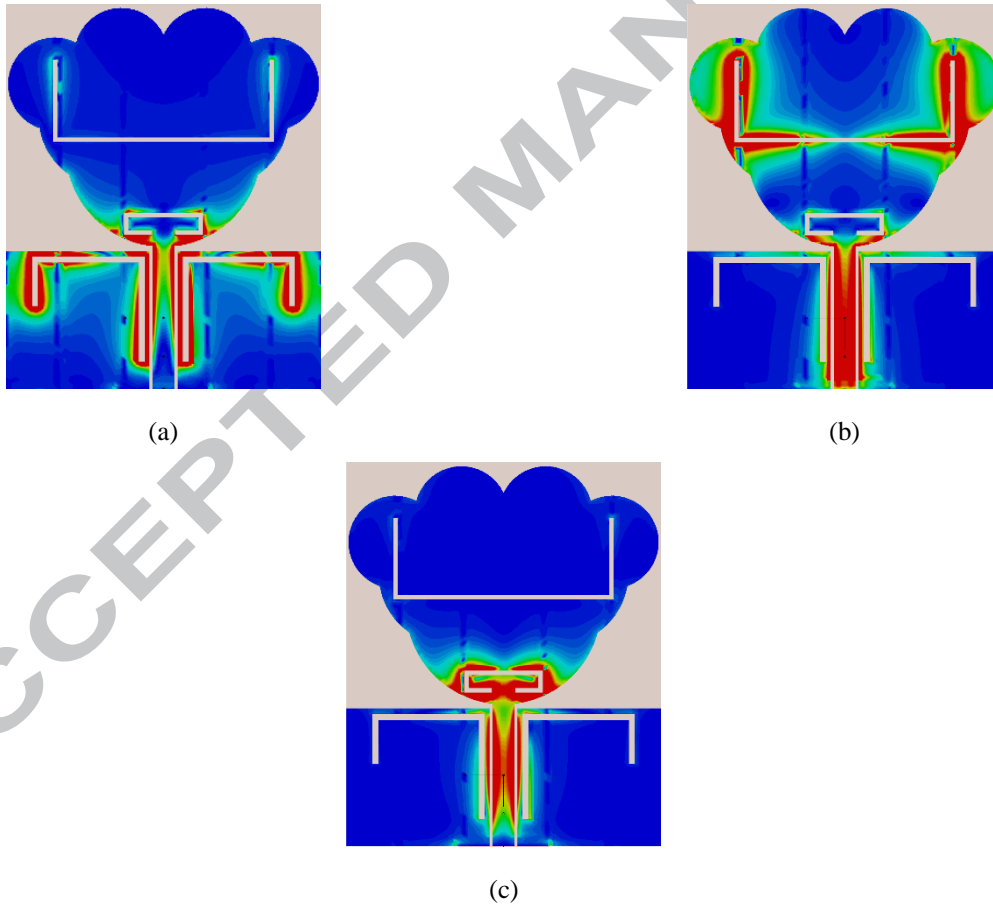
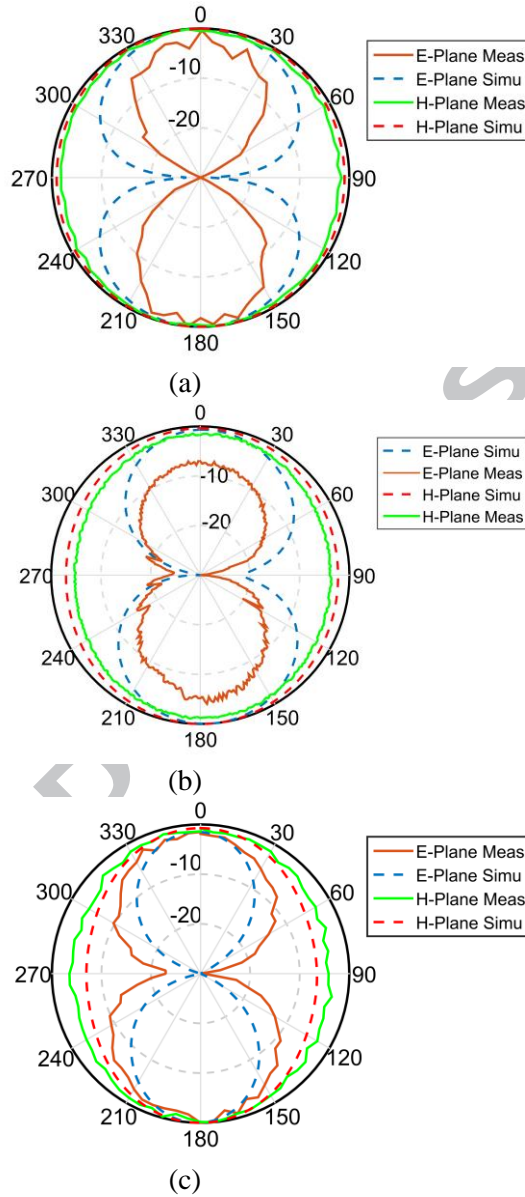


Fig.9 Surface current density distribution for (a). 3.6GHz (b). 5.6GHz (c) 9GHz

The current flow, around the slot reveals that the direction of current in either edges of the slots are opposite each other. This creates destructive interference and makes the antenna non-radiating at 3.6GHz, 5.6GHz and 9GHz.

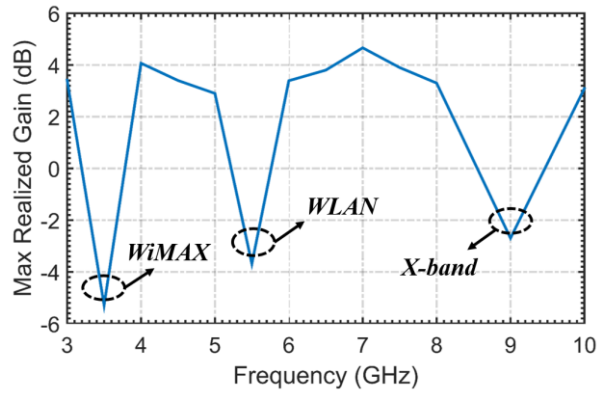
### 3.2 Radiation Performance

Measured and simulated radiation patterns of the proposed antenna in E-plane (yz-plane) and H-plane (xz-plane) at resonant frequency is depicted in figure 10. The measurements are carried out at the state1.

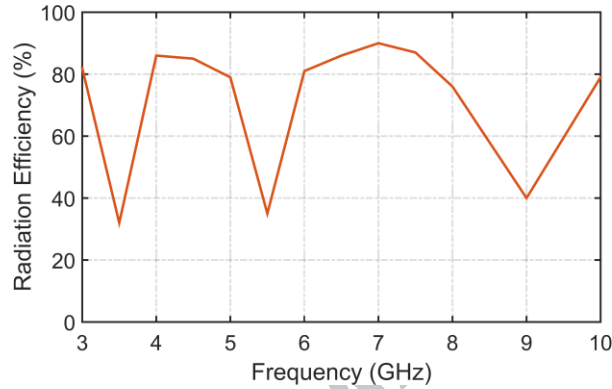


**Fig.10** Measured and simulated E-plane and H-plane radiation patterns of the proposed antenna at resonant frequencies of (a) 4.3 GHz, (b) 6.7 GHz, and (c) 10 GHz

In figure 11, measured gain value of the proposed antenna in different frequency ranges is demonstrated. It can be seen that, the measured gain in notch frequencies is decreased to its lowest level. Also the results of antenna efficiency is depicted in figure 12.



**Fig.11** Measured gain value of the proposed UWB reconfigurable fractal antenna



**Fig.12** Radiation Efficiency proposed UWB reconfigurable fractal antenna

The proposed FCPA is presented in table 1 in comparison with some of the already published identical antennas.

**Table 1.** Comparison of the proposed FCPA with other recent UWB antennas

Ref	BW	Size(mm)	Notches	Switching capability
[37]	UWB	34x35.9	2	yes
[38]	UWB	24x32	2	no
[39]	UWB	35x35	3	no
[40]	UWB	30x35	3	no
[21]	UWB	25x28	1	no
[41]	UWB	27x30.5	3	no
[42]	UWB	27x32	2	yes
[43]	UWB	26.8x38.7	3	yes
[44]	UWB	26x30	3	no
[45]	UWB	27x36	4	no
[46]	UWB	25x25	0	no
[47]	UWB	50x50	3	no
[18]	UWB	32x24	1	no
[13]	UWB	32x24	2	no
[17]	UWB	30x32	3	yes
<b>Proposed antenna</b>	UWB	21x25	3	yes

### 3.4 Time-domain Analysis

It is vital to analyze the UWB structures in time-domain. Signals transmitted by UWB structures are prone to amplitude, and phase distortion. In order to investigate this problem, the structure group delay must be calculated. If the group delay is less than or equal to 1ns, distortion caused by the system is negligible. In other words,

transmitted and received signal must be almost the same. Hence, correlation between transmitted and received signal is expressed as fidelity factor which is given by:

$$\rho = \max_{\tau} \left\{ \left| \frac{\int S(t)R(t-\tau)dt}{\sqrt{\int S^2(t)dt} \sqrt{\int R^2(t)dt}} \right| \right\} \quad (4)$$

Where  $\tau, S(t)$  and  $R(t)$  represent delay, source pulse, and received pulse, respectively. When correlation of two signals is 1, the signals are basically the same and have no distortion. In order to investigate group delay in simulation, Gaussian modulated pulse with 3-12 GHz spectrum by CST software package is chosen, which fulfills the FCC indoor and outdoor power mask criteria. A virtual probe in antenna far field is employed, situated 70 cm away from the antenna, with angles of 0, 45 and -45 degrees. For appropriate matching of the radiated pulse and the source pulse, fidelity factor must be above 0.71. [48, 49]

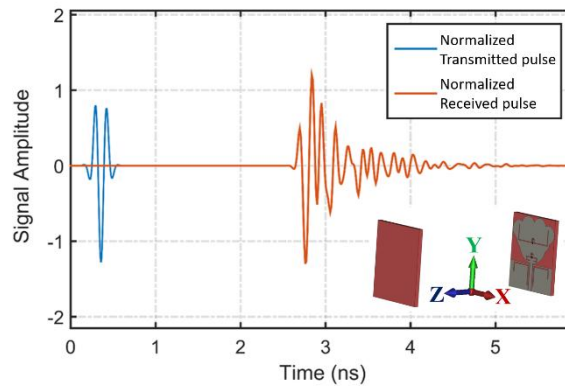


Fig.12 Normalized source and received signal at plane z-y ( $\theta = 0, \varphi = 90$ ). The investigation is carried out for state I

Table 2. Calculated fidelity factor for six different situations

Probe Positions x-z plane	Fidelity Factor	Probe Positions z-y plane	Fidelity Factor
$\theta$	0.745	$\theta$	0.721
$\theta = 0, \varphi = 0$	0.832	$\theta$	0.805
$\theta$	0.792	$\theta$	0.796

As shown in table 2, it can be observed that, present antenna causes little distortion and fulfills the requirements in time domain, as well as the frequency domain.

#### 4. Conclusions

A compact UWB fractal antenna with triple reconfigurable notch rejection bands is implemented, to reject the crowded frequency bands WiMAX, WLAN and X band interferences produced in UWB communication systems. The proposed structure consists of a basic antenna with 2 circular fractal iterations. By employing this new structure

of fractal, the overall size of antenna is reduced %53, to 21x25. This antenna size is smaller than many available UWB antennas and has a suitable gain too. The designed antenna is also investigated in time domain to prove the employment of the antenna for UWB applications.

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