

# Successes and Challenges Associated with Solution Processing of Kesterite $\text{Cu}_2\text{ZnSnS}_4$ Solar Cells on Titanium Substrates

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**ABSTRACT:** Roll-to-roll (R2R) processing of solution-based  $\text{Cu}_2\text{ZnSn}(\text{S},\text{Se})_4$  (CZT(S,Se)) solar cells on flexible metal foil is an attractive way to achieve cost-effective manufacturing of photovoltaics. In this work we report the first successful fabrication of solution-processed CZTS devices on a variety of titanium substrates with up to 2.88% power conversion efficiency

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3 (PCE) collected on flexible 75  $\mu\text{m}$  Ti foil. A comparative study of  
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5 device performance and properties is presented aiming to address  
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7 key processing challenges. First, we show that a rapid transfer of  
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9 heat through the titanium substrates is responsible for the  
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11 accelerated crystallisation of kesterite films characterised with  
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13 small grain size, a high density of grain boundaries and numerous  
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15 pore sites near the Mo/CZTS interface which affect charge transport  
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17 and enhance recombination in devices. Following this, we  
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19 demonstrate the occurrence of metal ion diffusion induced by the  
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21 high temperature treatment required for the sulfurization of the  
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23 CZTS stack:  $\text{Ti}^{4+}$  ions are observed to migrate upwards to the Mo/CZTS  
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25 interface whilst  $\text{Cu}^{1+}$  and  $\text{Zn}^{2+}$  ions diffuse through the Mo layer  
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27 into the Ti substrate. Finally, residual stress data confirm the  
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29 good adhesion of stacked materials throughout the sequential  
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31 solution process. These findings are evidenced by combining  
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33 electron imaging observations, elemental depth profiles generated  
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35 by secondary ion mass spectrometry, and x-ray residual stress  
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37 analysis of the Ti substrate.  
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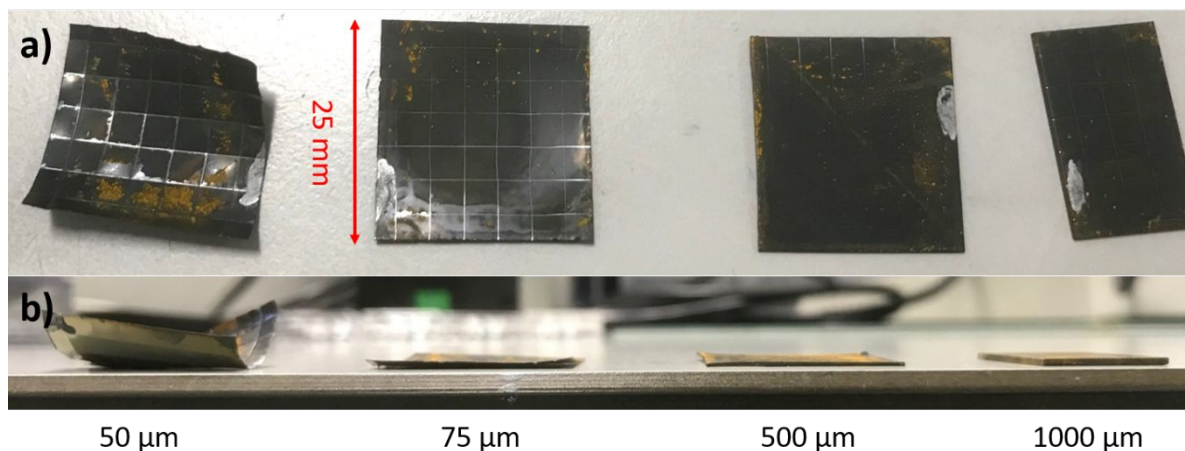
## 45 **INTRODUCTION**

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47 Recent advances in thin film compound semiconductor photovoltaics  
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49 have demonstrated much of the high potential of these technologies  
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51 for generating sustainable and cost-efficient energy. Both  
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53  $\text{Cu}(\text{In},\text{Ga})\text{Se}_2$  (CIGS) and  $\text{CdTe}$  have achieved power conversion  
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3 efficiencies (PCEs) above 20% and they are well developed  
4 industrially.<sup>1</sup> Emerging light absorbing materials such as  
5  $\text{Cu}_2\text{ZnSn}(\text{S}, \text{Se})_4$  (CZT(S,Se)) only contain earth abundant elements,  
6 providing more sustainable alternative to 2<sup>nd</sup> generation PV  
7 technologies. A number of research teams have now successfully  
8 fabricated over 10% efficiency CZT(S,Se) solar cell devices at the  
9 laboratory scale<sup>2-4</sup>, encouraging further development aiming towards  
10 higher economic impact.<sup>5-6</sup> To address manufacturing costs, light-  
11 weight flexible materials such as metal or polymer foils can be  
12 used as substrates in roll-to-roll manufacturing. The high power-  
13 to-mass ratio of flexible solar cells favours their use in sectors  
14 such as building integrated photovoltaics (BIPV), aerospace and  
15 automotive power generation, and powering Internet of Things  
16 (IoT). Recent advances have been made in the vacuum fabrication of  
17 CZT(S,Se) solar cells produced on flexible substrates. For  
18 instance, CZT(S,Se) light absorbers were successfully grown  
19 directly on stainless steel foil to make photovoltaic devices  
20 reaching just over 6% efficiency.<sup>7-8</sup> Other metallic substrates such  
21 as molybdenum foil<sup>9-10</sup> and flexible glass<sup>11</sup> have been tested with  
22 PCEs reaching up to 6.78% and 3.09%, respectively. In comparison,  
23 the performance of devices fabricated with solution processed  
24 absorbers remains much lower than their vacuum counterpart with  
25 cell efficiencies of 1.94% reported on aluminium foil-based  
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3 devices<sup>12</sup>, 4.4%<sup>13</sup> and 2.42%<sup>14</sup> on molybdenum foil, and 0.49% on  
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5 polyimide<sup>15</sup>.  
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8 Whilst most metal foils appear suitable for roll-to-roll  
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10 manufacturing of PV devices owing to their flexibility and high  
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12 electrical conductivity, other parameters need to be considered  
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14 when optimising the manufacturing CZTS devices. For instance, it  
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16 is desirable that the substrate is characterised with good chemical  
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18 stability and has durable mechanical properties. In addition, the  
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20 behaviour of the metal foil at high temperature (required for the  
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22 preparation of the CZTS film) is also of great importance. In this  
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24 work, we report the first successful preparation of solution-  
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26 processed CZTS solar cells on titanium flexible (thickness: 50  $\mu\text{m}$   
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28 and 75  $\mu\text{m}$ ) and rigid (thickness: 500  $\mu\text{m}$  and 1000  $\mu\text{m}$ ) substrates  
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30 (shown in **Figure 1**) and compare their performance to devices built  
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32 on 1 mm soda-lime glass. A two-step stack-building process was  
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34 applied where the active layer was spin-coated from a liquid  
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36 precursor and sulphurisation carried out according to a procedure  
37  
38 described in previous work.<sup>16-17</sup> Cross sectional electron microscopy  
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40 observations, secondary ion mass spectrometer analysis (SIMS), and  
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42 residual stress analysis of the Ti substrates were applied to  
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44 understand the performance trends in CZTS devices.  
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**Figure 1.** Flexible and rigid CZTS solar cells fabricated on 50-1000 μm Ti substrates: a) top view; b) side view.

## EXPERIMENTAL SECTION

### 1) Substrates and cleaning procedure

Four types of Ti substrates were investigated which thickness (50 μm, 75 μm, 500 μm and 1000 μm), Ti content 99.6-99.9% w.t., and processing have been summarised in **Table S1**, together with those of the control soda-lime glass substrate. Cleaning was operated in an ultrasonic bath sequentially using soap water, deionised water, acetone, and isopropanol. Oxygen plasma treatment followed to remove any residual surface contaminants.

### 2) Preparation of Mo, CZTS layers, and top contacts

A 400 nm-thick molybdenum (Mo) film was deposited at room temperature by direct current (DC) magnetron sputtering using Kurt Lesker PVD 75 system. The C-Z-T-S precursor solutions were prepared by dissolving  $\text{CuCl}_2 \cdot 2\text{H}_2\text{O}$  (98% Alfa Aesar),  $\text{SnCl}_2$  (98% Sigma-Aldrich),  $\text{ZnCl}_2$  (99.95% Alfa Aesar) and thiourea  $\text{SC}(\text{NH}_2)_2$  (99% Sigma-Aldrich) in 5mL DMSO (99.9% Sigma-Aldrich). The  $\text{CuCl}_2 \cdot 2\text{H}_2\text{O}$

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3 concentration was 0.55 M and the targeted molar ratio of  
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5  $\text{SnCl}_2:\text{ZnCl}_2:\text{CuCl}_2\cdot 2\text{H}_2\text{O}:\text{thiourea}$  was 1.31:0.69:1:1.84. All the  
6  
7 precursor solution was doped with 0.14M NaCl. After the back  
8  
9 contact deposition, the CZTS layers were grown on Mo/Ti substrates  
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11 by spin-coating of the C-Z-T-S solution precursors. Samples were  
12  
13 subsequently sulphurised in a rapid thermal processing furnace  
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15 (RTP, MTI Corporation) at 560 °C for 20 mins. The thickness of the  
16  
17 CZTS absorbers was 1.0–1.5  $\mu\text{m}$ . After coating CZTS layers, a ~70 nm  
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19 thick CdS layer was deposited by chemical bath deposition. ZnO  
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21 (~75nm) and Al:ZnO (~500 nm) were radio frequency (RF) sputtered  
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23 with respective power density of 1.87  $\text{Wcm}^{-2}$  and 2.46  $\text{Wcm}^{-2}$  served  
24  
25 as a transparent top contact using a Moorfield Nanolab 60  
26  
27 sputtering system. The transmittance and reflectance of AZO film  
28  
29 were shown in **Figure S1**. The single cells (0.4 cm x 0.4 cm = 0.16  
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31  $\text{cm}^2$ ) were defined by manual mechanical scribing.

### 37 **3) Characterisation of materials and devices**

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39 Residual stress measurements were carried out with a Bruker D8  
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41 Discover X-ray diffraction system with a 0.07° step size, at a  
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43 time of 7 s per step. The undertaken scans covered the full 0–0.9  
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45  $\sin^2(\psi)$  in both positive and negative  $\psi$  tilts to confirm the  
46  
47 absence of shear stress. Peak evaluation was undertaken using the  
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49 Pearson VII fitting and stresses were calculated using a biaxial  
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51 stress model, assuming  $\sigma_{33}=0$ .  
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3 CZTS/Mo/Ti samples were cross-sectioned using an FEI Helios  
4 NanoLab 600 combined focused ion beam/scanning electron  
5 microscope. Initially, protective platinum deposits of 20  $\mu\text{m}$  x 2.5  
6  $\mu\text{m}$  x 1  $\mu\text{m}$  thickness were made within the instrument using gas-  
7 assisted deposition in the presence of a platinum-bearing  
8 organometallic gas, in conjunction with a gallium focused ion beam.  
9  
10 Vertical trenches (20  $\mu\text{m}$  length x 10  $\mu\text{m}$  width x 10  $\mu\text{m}$  depth) were  
11 cut into the materials stack using a gallium focused ion beam of  
12 30 keV energy and 20 nA beam. The vertical face of the section was  
13 then cleaned with the gallium ion beam at a reduced current of  
14 6.5nA to produce high-quality surfaces enabling electron  
15 microscopy observations.  
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30 High magnification (x 25,000) images of the vertical sections  
31 were acquired using a JEOL-JSM-7800F field emission scanning  
32 electron microscope in secondary electron mode (10 keV beam energy  
33 and 0.34 nA beam current, 10 mm WD).  
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39 Secondary ion mass spectrometry (SIMS) depth profiles were  
40 obtained using an instrument built by the Interface Analysis  
41 Centre, at the University of Bristol. This system is featured with  
42 an electronically variable aperture type gallium ion gun (FEI SD  
43 gallium LMIS EVA focusing column) fitted to a double focusing  
44 magnetic sector mass analyser (Vacuum Generators model 7035). The  
45 experimental details can be found in our previous report<sup>17</sup>. Signals  
46 for sodium, titanium, copper, zinc, molybdenum and tin were  
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3 collected with dwell times of 1s per element, cycling through the  
4 elements for a total period of 30 minutes.  
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7 Current-density-voltage ( $J$ - $V$ ) curves were measured under  
8 simulated AM1.5G spectrum and 100 mW/cm<sup>2</sup> (1 sun) illumination. The  
9 external quantum efficiency (EQE) measurements were performed in  
10 AC mode with a chopping frequency of 67 Hz using a QEX10 system  
11 (PV Measurements) calibrated with a NIST-certified Si photodiode.  
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## 19 **RESULTS AND DISCUSSION**

### 20 **1) Device performance**

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22 Substrate characteristics including thermal expansion  
23 properties, surface roughness, substrate composition and  
24 processing condition are critical elements to enable manufacturing  
25 of CZTS solar cells on flexible metal substrates.<sup>18-20</sup> Here, we  
26 selected Ti as our substrate material rather than commonly used  
27 stainless steel foil (SS) due to the smaller mismatch of  
28 coefficient of thermal expansion (CTE) of Mo/Ti than Mo/SS<sup>18, 21</sup>  
29 and their chemically stability as thin Ti coatings (50-60 nm-  
30 thick) were introduced as a diffusion barrier on SS based device  
31 in a previous report<sup>7, 22-23</sup>. We choose rigid (thickness: 500  $\mu$ m and  
32 1000  $\mu$ m) Ti substrate to give a direct comparison to SLG substrate.  
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34 For most flexible (thickness: 50  $\mu$ m) Ti substrate, there is no  
35 apparent deformation through the whole coating processes until the  
36 mechanical scribing. Some layer-stack were peeled off due to its  
37 softness and sensitive to pressure variation caused by mechanical  
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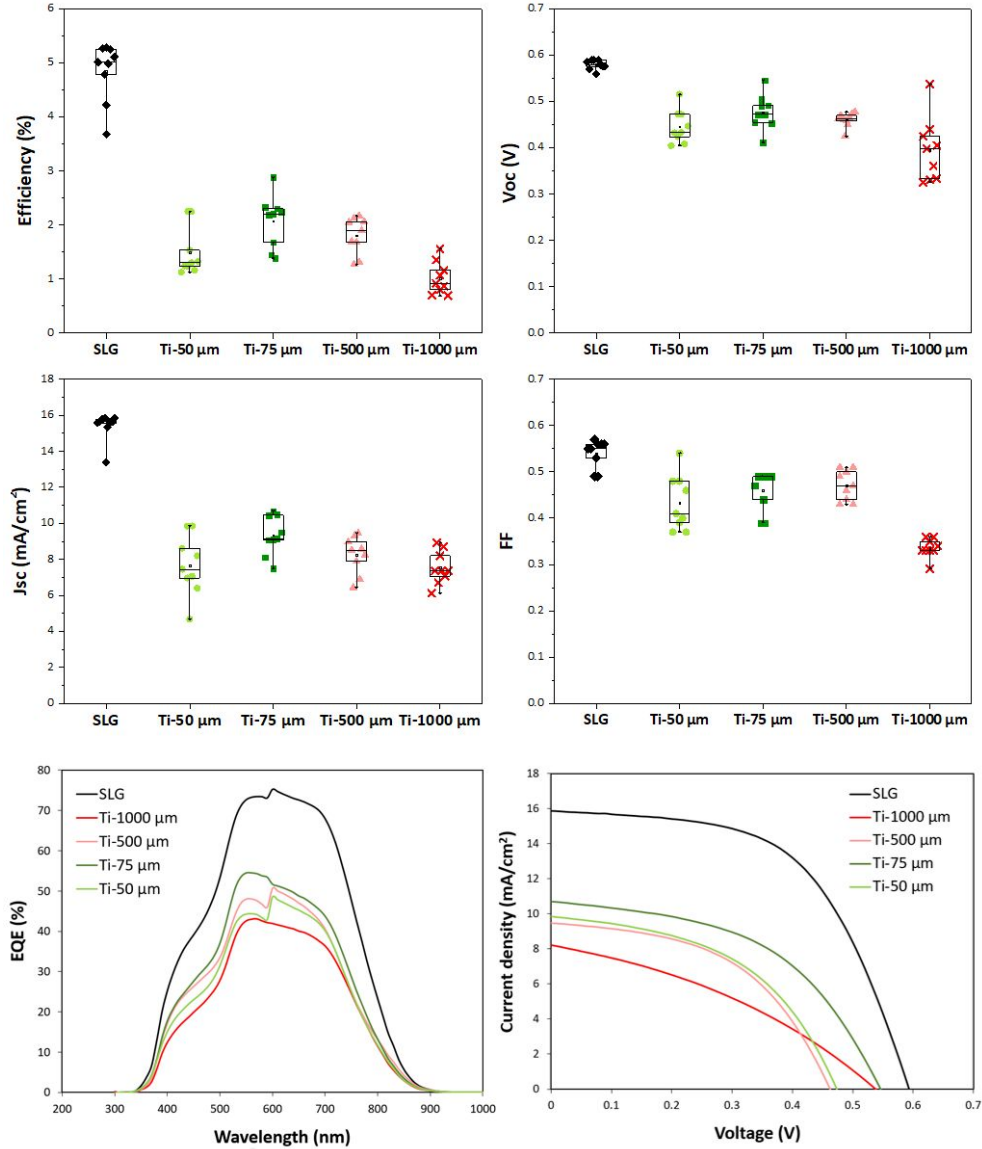
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3 scribing. The 75  $\mu\text{m}$ -thick Ti foil shows the best flexibility versus  
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5 mechanical stability of fabricated final solar cell device.  
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8 The PCE,  $V_{OC}$ ,  $J_{SC}$ , and  $FF$  of CZTS cells built on Ti and SLG  
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10 substrates are compared in **Figure 2** and best-performing cells  
11  
12 parameters summarised in **Table 1**. Overall, cells prepared on  
13  
14 titanium substrates recorded encouraging outputs with average PCEs  
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16 of 1.49%, 2.08%, 1.81%, and 1.02% for 50, 75, 500, and 1000  $\mu\text{m}$  Ti-  
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18 based cells. The highest Ti-based device performance of 2.88% was  
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20 collected on 75  $\mu\text{m}$  flexible titanium substrate. However, this was  
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22 lower than control SLG-based devices characterised with average  
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24 PCEs of 4.85 % and a maximum at 5.29%. The gap in performance  
25  
26 between Ti-based and SLG-based devices was associated with an  
27  
28 important difference in  $J_{SC}$  related to high levels of porosity  
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30 (**Figure 3, 4 and S2**) linking with elements diffusion (**Figure 5**)  
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32 and overall higher series resistances ( $R_s$ ) of Ti-based devices,  
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34 which may stem from the formation of highly resistive secondary  
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36 phases such  $\text{MoS}_2$ <sup>24</sup> and  $\text{Ti}_2\text{S}_5$ <sup>25</sup> at the back contact as evidenced by  
37  
38 XRD and SIMS (**Figure S3 A, B and Figure 5**). Raman spectra of CZTS  
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40 films prepared on 50, 75, 500, and 1000  $\mu\text{m}$  Ti substrates and on  
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42 SLG (**Figure S3 C and D**) show almost no difference on the spectra  
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44 of these samples, which means three samples have similar  
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46 crystalline phases at CZTS film surface. An examination of samples  
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48 cross sections (**Figure 3, 4 and Figure S2**) revealed that CZTS films  
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50 prepared over Ti substrates had similar thickness ( $\sim 1\text{-}1.5 \mu\text{m}$ ) but  
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3 smaller grain size (< 200 nm) compared to films produced on SLG  
4 (up to 700-800 nm). Smaller crystals and higher densities of grain  
5 boundaries have been shown to hinder charge transport across CZTS  
6 films<sup>26-27</sup> and are here responsible for decreased  $R_{SH}$ . The Ti-based  
7 films also displayed high levels of porosity compared to SLG-based  
8 films. The absence of active material in pore sites greatly  
9 affected the density of charges produced and impacted on average  
10 device  $J_{SC}$ . This was in good agreement with the EQE data which  
11 confirmed lower levels of charge generation across the entire  
12 wavelength range (Figure 2). Higher levels of charge recombination  
13 evidenced by lower  $R_{sh}$  data,  $J_{SC}$  and fill factor were assigned to  
14 the enhanced density of CZTS/void and CZTS/CZTS grain boundaries  
15 which are prone to defects and known to act as recombination  
16 sites.<sup>27-28</sup> Finally, the  $V_{OC}$  of Ti-based devices, ranging between  
17 0.40-0.47 V, was also found to be systematically lower than the  
18  $V_{OC}$  of SLG-based devices averaging 0.57 V. EQE data (**Figure 2**)  
19 demonstrated very little variations in the bandgap of CZTS films  
20 across all samples (1.547-1.575 eV for the Ti-based films compared  
21 to 1.562 eV for the SLG-based film). Hence, we suspect the  
22 difference in  $V_{OC}$  is attributed to the formation of a thicker  $MoS_2$   
23 layer<sup>7</sup> enabled by the effective conduction of heat through Ti  
24 substrates. This is evidenced by increased  $R_s$  which is caused by  
25 high resistivity of the thick  $MoS_2$  layer<sup>29</sup> and XRD peaks at  $26^\circ$   
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3 32° in Ti-based devices as compared to SLG-based devices<sup>24</sup> (**Table**  
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5 **S2 and Figure S3 A and B**).

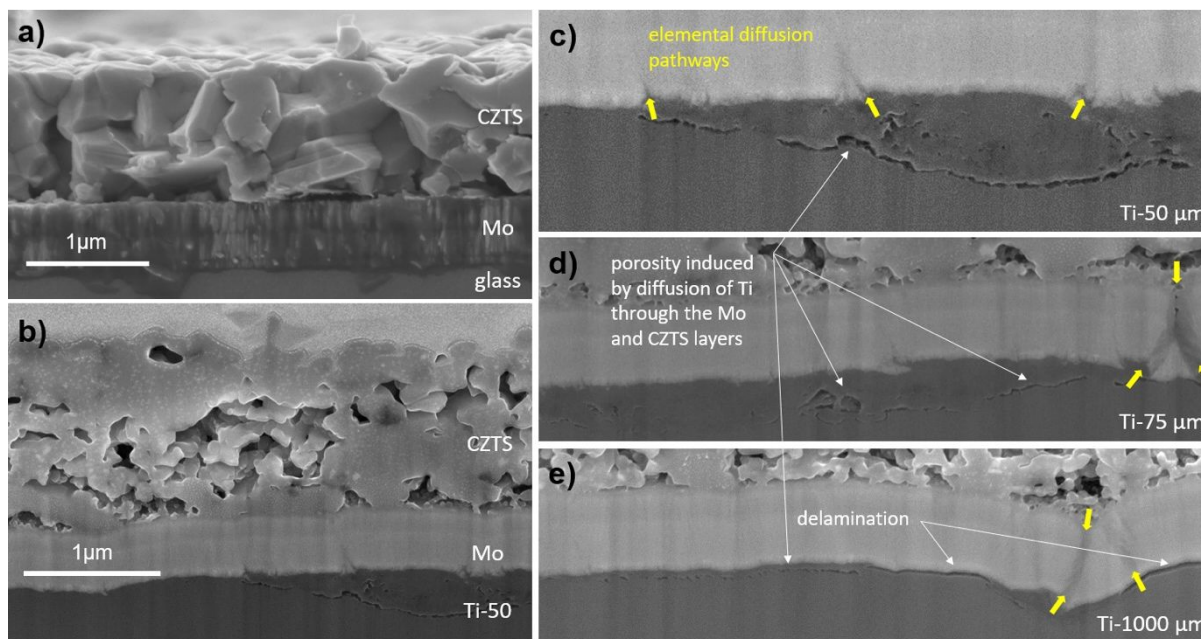
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8 A comparison of photovoltaic performance for Ti-based devices  
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10 only showed little effect of the substrate thickness. However,  
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12 devices built over 50  $\mu\text{m}$  and 1000  $\mu\text{m}$  Ti substrates were  
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14 characterised with lower average PCEs of 1.49 % and 1.02% compared  
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16 to 2.08 % and 1.81 % for devices built over 75  $\mu\text{m}$  and 500  $\mu\text{m}$  Ti  
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18 substrates. In the case of devices prepared on Ti-1000  $\mu\text{m}$ , lower  
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20 average FF and  $R_{\text{sh}}$  were assigned to localized delamination between  
21  
22 the Mo and Ti layers in areas characterised with higher interface  
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24 roughness, as illustrated in **Figure 3e**. The lower performance of  
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26 devices prepared on 50  $\mu\text{m}$  Ti substrates was attributed to the  
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28 mechanical failure of the CZTS stack near mechanically scribed  
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30 cell edges. The local deformation of the substrate, evidenced by  
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32 the formation of ridges apparent at the top edge of the sample in  
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34 **Figure 1a**, is thought to be responsible for the loss of CZTS  
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36 material which translated into lower average  $J_{\text{sc}}$ . The other  
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38 samples, built on far less flexible Ti substrates, remained  
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40 unaffected by this process.  
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**Figure 2.** Box plots of J-V characteristics for CZT(S,Se) devices prepared on soda-lime glass (SLG) and 50, 75, 500, and 1000  $\mu\text{m}$  Ti substrates.

**Table 1.** Summary of device parameters for the average values and the best-performing values of CZTS solar cells fabricated on 50, 75, 500, and 1000  $\mu\text{m}$  Ti substrates and SLG.

| Substrate                              | $\eta$          |      | $V_{oc}$        |      | $J_{sc}$                         |       | FF              |      |
|--|-----------------|------|-----------------|------|----------------------------------|-------|-----------------|------|
|  | (%)             |      | (V)             |      | $(\text{mA}\cdot\text{cm}^{-2})$ |       |                 |      |
| <b>Glass (SLG)</b>                     | 4.84 $\pm$ 0.55 | 5.29 | 0.58 $\pm$ 0.01 | 0.59 | 15.41 $\pm$ 0.78                 | 15.87 | 0.54 $\pm$ 0.03 | 0.56 |
| <b>Ti-50 <math>\mu\text{m}</math></b>  | 1.49 $\pm$ 0.45 | 2.25 | 0.45 $\pm$ 0.04 | 0.47 | 7.67 $\pm$ 1.67                  | 9.85  | 0.43 $\pm$ 0.06 | 0.48 |
| <b>Ti-75 <math>\mu\text{m}</math></b>  | 2.08 $\pm$ 0.48 | 2.88 | 0.48 $\pm$ 0.04 | 0.55 | 9.34 $\pm$ 1.08                  | 10.69 | 0.46 $\pm$ 0.04 | 0.49 |
| <b>Ti-500 <math>\mu\text{m}</math></b> | 1.81 $\pm$ 0.34 | 2.17 | 0.46 $\pm$ 0.02 | 0.46 | 8.25 $\pm$ 1.03                  | 9.45  | 0.47 $\pm$ 0.03 | 0.50 |
| <b>Ti-1000<math>\mu\text{m}</math></b> | 1.02 $\pm$ 0.30 | 1.56 | 0.40 $\pm$ 0.07 | 0.54 | 7.54 $\pm$ 0.92                  | 8.20  | 0.34 $\pm$ 0.02 | 0.35 |



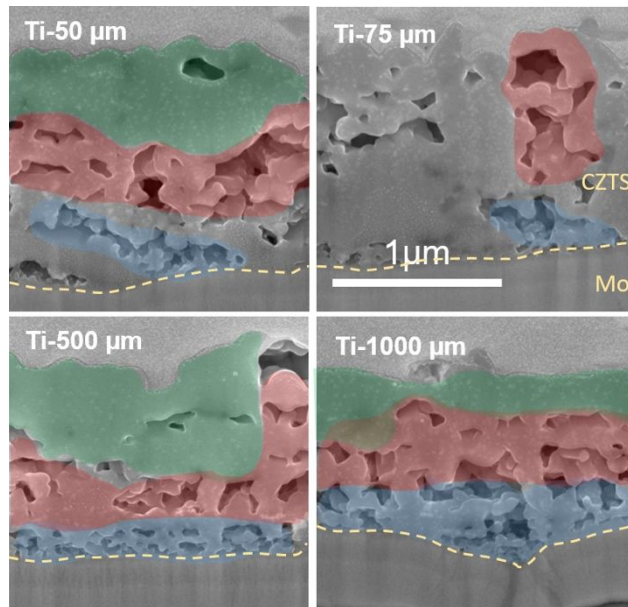
**Figure 3.** Cross-section SEM images of CZTS samples on (a) Mo/SLG-1000  $\mu\text{m}$ ; (b) Mo/Ti-50  $\mu\text{m}$ . Selected areas of CZTS devices prepared on Ti substrates highlighting Ti diffusion pathways, residual Ti-

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3 porosity and areas of delamination: (c) Mo/Ti-50  $\mu\text{m}$ ; (d) Mo/Ti-75  
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5  $\mu\text{m}$ ; (e) Mo/Ti-1000  $\mu\text{m}$ .  
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## 10 **2) Manufacturing challenges for Ti-based CZTS devices**

11  
12 Controlling the crystallisation of the CZTS layer to achieve  
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14 large grains is critical to obtain efficient charge transport and  
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16 optimum device performance.<sup>26, 28</sup> Various deposition methods have  
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18 been developed to address these processing challenges.<sup>7-9</sup> In the  
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20 case of solution processed films, it was demonstrated that is  
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22 particularly important to tailor the heat treatment applied during  
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24 this fabrication stage.<sup>9</sup> Here, a CZTS precursor containing metal  
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26 chloride salts was spin coated onto Mo/Ti substrates and  
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28 sulphurised in a rapid thermal processing furnace at 560 °C for 20  
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30 mins. Despite the great care taken in optimizing this process for  
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32 SLG-based devices<sup>16-17</sup> results here show that further work is needed  
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34 to achieve similar CZTS films on Ti substrates. As previously  
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36 mentioned, a comparison of CZTS film cross-sections **Figure 3a** and  
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38 **Figure 3b** showed overall much smaller crystals in Ti-based samples  
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40 compared to SLG-based samples. A systematic assessment of crystal  
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42 size across samples showed that all Ti-based samples were  
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44 characterised with smaller CZTS crystals near the Mo/CZTS  
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46 interface compared to the top part of the film. This has been  
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48 evidenced in **Figure 4** where coloured areas highlight the occurrence  
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50 of < 100 nm size crystals at the bottom of the films (in blue)  
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3 over > 150 nm crystals (in red) at the centre and top parts of the  
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5 films. An increasing crystal size upwards through the CZTS film  
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7 suggests a gradient in the nucleation rate. This was not the case  
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9 of SLG-based CZTS film where the size distribution of crystals was  
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11 much larger and consistent across the thickness of the film.  
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13 Titanium is known to conduct heat a lot more effectively than glass  
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15 with a thermal conduction coefficient of 24 W/m·K, almost 25 times  
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17 higher than soda lime glass ranging between 0.7-1.3 W/m·K. Here,  
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19 we can conclude that the temperature of Ti substrates raised faster  
20  
21 than that of the SLG substrate, causing an acceleration of  
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23 nucleation events at the bottom of the films. In terms of  
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25 manufacturing, there may be an opportunity to develop low heat  
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27 conduction layers allowing a finer control over CZTS  
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29 crystallization. Alternately, the heat treatment applied to  
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31 sulphurize the CZTS film should be optimized based on the nature  
32  
33 of the substrate. Whilst the temperature profile of the  
34  
35 sulphurization process may be adjusted, it may be of interest to  
36  
37 investigate the application of selective heating techniques such  
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39 as demonstrated for the crystallisation of perovskite light  
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41 absorbers.<sup>30</sup>  
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**Figure 4.** FEG-SEM cross sectional views of CZTS films built over Ti substrates highlighting areas characterised with small CZTS crystals (blue), large CZTS crystals (red), low levels of porosity (green).

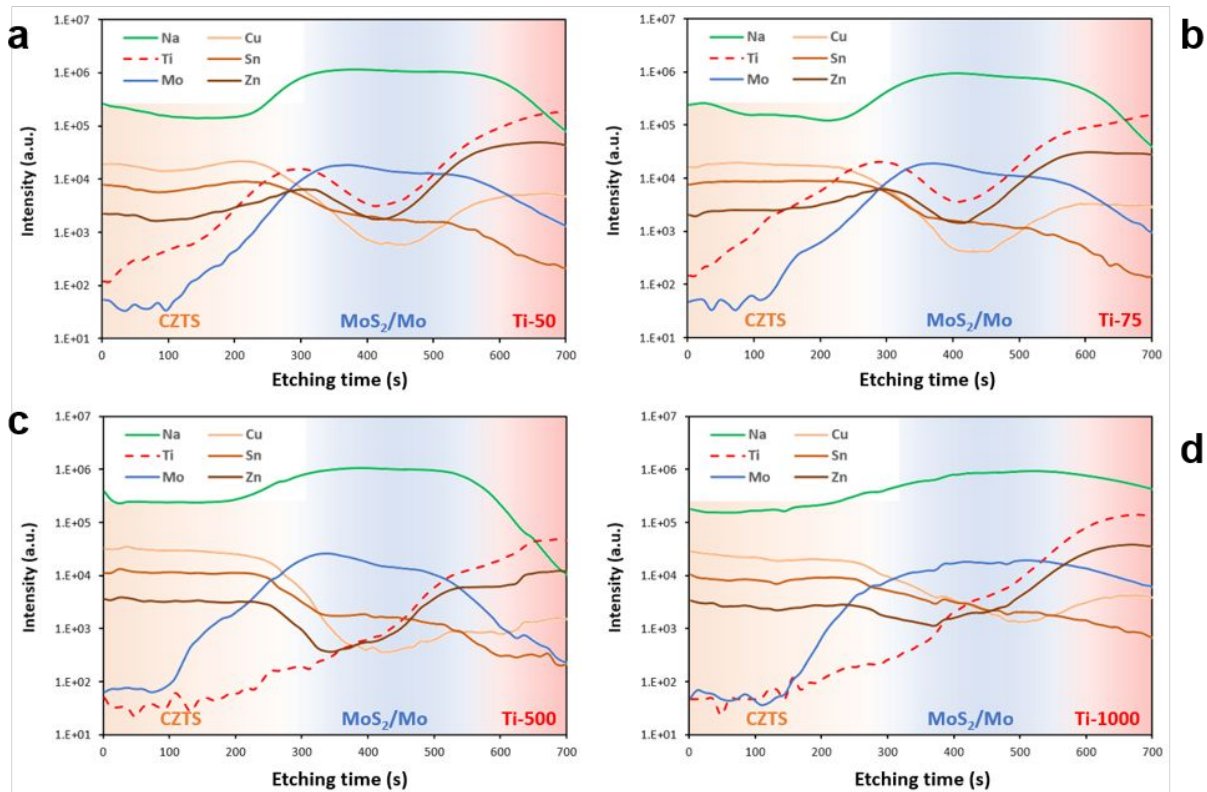
Another challenge for the manufacturing of efficient metal-based CZTS devices is the diffusion of elements across layers of materials. The sulfurization of the molybdenum layer, an unwanted side effect of the high temperature sulphurization process, is already well documented.<sup>17, 29, 31</sup> But there are fewer published accounts addressing the diffusion of other elements, namely metallic ions.<sup>7-8, 22</sup> Sun *et al.* reported on the use of a Ti barrier layer aiming to prevent the diffusion of substrate Fe ions to the CZTS film.<sup>7</sup> To confirm the suitability of Ti with this regard, we investigated the motion of Ti ions of Ti-based CZTS stacks by combining cross-section imaging observations and secondary ion



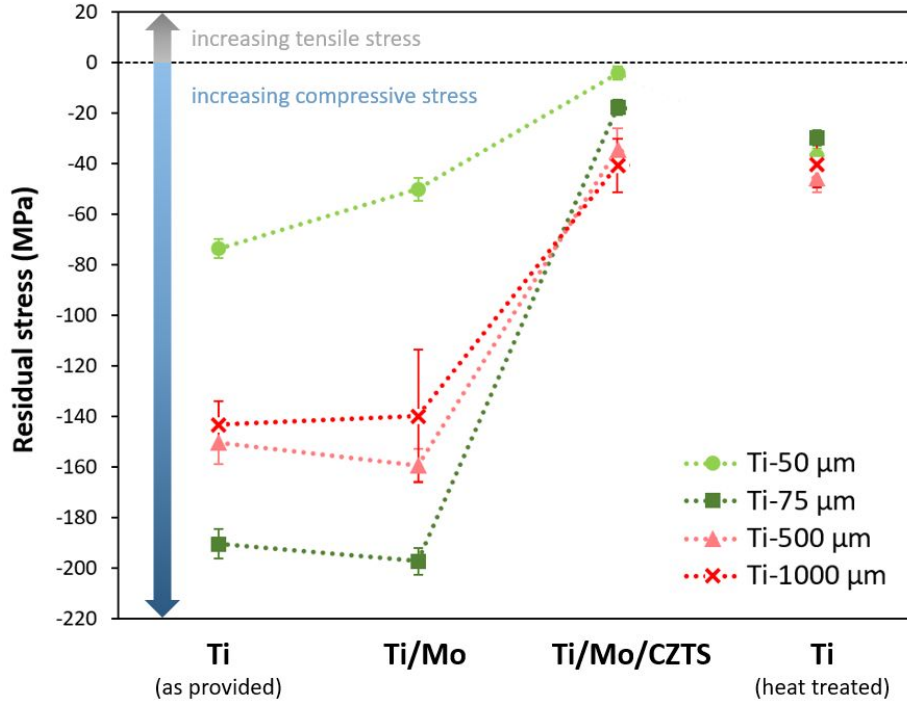
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3 mass spectrometry elemental depth profiling. At high  
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5 magnification, the examination of the Mo/Ti interface (**Figure 5.a-**  
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7 **d)** revealed the presence of pores in the Ti layer near the  
8  
9 interface. Directly above these in the Mo layer, darker linear  
10  
11 contrasts indicative of lower atomic weight elements was observed,  
12  
13 sometimes extending across the entire thickness of the Mo layer.  
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15 These strongly suggested the diffusion of Ti ions upwards areas,  
16  
17 causing the formation of pores at the top of the Ti layer. These  
18  
19 features were particularly pronounced in Ti-50  $\mu\text{m}$  and Ti-75  $\mu\text{m}$   
20  
21 stacks where heat conduction was more effective than in much  
22  
23 thicker Ti-500  $\mu\text{m}$  and Ti-1000  $\mu\text{m}$ . This hypothesis was further  
24  
25 confirmed by SIMS depth profile data. **Figure 6** shows elemental  
26  
27 signals collected for Cu, Sn, Zn, Ti, Mo, and Na plotted against  
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29 the etching time. All samples exhibited common features: 1) between  
30  
31 0-250 s etching time, high levels of Cu, Zn, and Sn were recorded  
32  
33 which were assigned to the CZTS layer; 2) between 250-550 s etching  
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35 time, decreasing levels of Cu, Zn, and Sn but high levels of Na  
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37 and Mo suggested a transition to the Na-doped Mo layer; 3) over  
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39 550s etching time, the Ti signal became predominant as the etching  
40  
41 gun reached the top of the metallic substrate. Similar elemental  
42  
43 profiles had been collected for a SLG-Mo-CZTS stack in previous  
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45 work.<sup>17</sup> However, in thin Ti-50 and Ti-75  $\mu\text{m}$  substrates, a peak in  
46  
47 Ti signal intensity was observed at approximately 300s, suggesting  
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49 the accumulation of Ti atoms near the CZTS/Mo interface. This  
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3 confirms the diffusion of Ti across the Mo layer for these two  
4 samples (**Figure 3c** and **Figure 3d**). The same Ti peak was absent  
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6 from depth profiles of samples built over thick Ti-500 and Ti-1000  
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8  $\mu\text{m}$  substrates for which heat transfer was too slow to cause as  
9  
10 significant diffusion of Ti (**Figure 5c** and **Figure 5d**). Another  
11  
12 important finding relates to Cu and Zn elemental signals increasing  
13  
14 after 500s of etching time, indicative the high concentrations of  
15  
16 these elements at the Mo/Ti interface and in the depth of the Ti  
17  
18 substrate. Increased Cu and Zn signals over 550s likely stems from  
19  
20 oxygen enhancement effects (so called SIMS matrix effects) by  
21  
22 formation of  $\text{TiO}_2$  between the Mo layer and Ti substrate.<sup>32-34</sup> This  
23  
24 suggests the occurrence of an inverse diffusion phenomenon where  
25  
26 the upwards movement of  $\text{Ti}^{4+}$  ions was compensated by downwards  
27  
28 migrations of  $\text{Cu}^{1+}$  and  $\text{Zn}^{2+}$  ions, possibly through the same pathways  
29  
30 (**Figure 5b & 5c**). The diffusion of Cu and Zn also correlate higher  
31  
32 densities of pores observed at the bottom of the CZTS film (**Figure**  
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34 **4** - blue areas) compared to the top of the films generally  
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36 characterised with lower levels of porosity (**Figure 4** - green  
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38 areas).

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**Figure 5.** SIMS elemental depth profiles of CZTS samples on Ti substrates: (a) Mo/Ti-50  $\mu\text{m}$ ; (b) Mo/Ti-75  $\mu\text{m}$ ; (c) Mo/Ti-500  $\mu\text{m}$ ; (d) Mo/Ti-1000  $\mu\text{m}$  CZTS,  $MoS_2/Mo$  and Ti are shown with orange, blue and red backgrounds, respectively.



**Figure 6.** Residual stress analysis of Ti substrates in the  $\sigma_{11}$  direction using a biaxial model, following the application of a Mo layer (Mo/Ti), after the deposition and sulphurisation of the CZTS layer at 560 °C for 20 mins (CZTS/Mo/Ti), and for bare Ti substrates heated at 560 °C for 20min.

The mechanical stability of stacked layers of materials plays an important role in ensuring a successful transfer of photovoltaic technologies from lab scale to large roll-to-roll manufacturing. In previous work<sup>17</sup>, we demonstrated that the sequential deposition of thin layers of  $\text{Si}_x\text{N}_y$  over Mo could induce compressive stress inside the Mo layer later on responsible for the delamination of the CZTS layer. In this work, the mechanical stability of our stacked layers was assessed by collecting x-ray residual stress

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3 ( $\sigma_{11}$  and  $\sigma_{22}$  directions) data generated at the surface of the Ti  
4 layer, at each stage of the stack building process. Results  
5 presented in **Figure 6** indicate that all Ti substrates initially  
6 held compressive stresses of varying magnitude induced by the  
7 rolling of Ti bulk material into sheets and foils; this is despite  
8 the annealing treatment provided at the end of the manufacturing  
9 process which usually aims to release some of these stresses by  
10 promoting the re-organisation of the metallic crystalline matrix  
11 at high temperature. The data collected for Ti/Mo samples show  
12 that the deposition of a 400 nm Mo layer, operated at ambient  
13 temperature, had little effect over surface stress for most samples  
14 except for the Ti-50  $\mu\text{m}$  samples which compressive stress decreased  
15 by 26% from  $-76.4 \pm 2.6$  MPa to  $-58.1 \pm 4.2$  MPa. However, the deposition  
16 and sulphurisation of the CZTS layer operated at 560 °C for 20  
17 mins drastically reduced surface compressive stress in all Ti  
18 substrates. In particular, flexible Ti/Mo/CZTS samples with built  
19 on Ti-50  $\mu\text{m}$  and Ti-75  $\mu\text{m}$  displayed > 90 % loss whilst rigid samples  
20 built on Ti-500  $\mu\text{m}$  and Ti-1000  $\mu\text{m}$  displayed close to 75 % loss in  
21 surface compressive stress compared to their initial (Ti, as  
22 provided) state. The difference in stress release experienced by  
23 flexible compared to rigid Ti substrates may be assigned to faster  
24 temperature rise of the surface in the thinner substrates. The  
25 relaxation of Ti substrates throughout the stack building steps  
26 correlates the good mechanical adhesion observed between the Ti  
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3 and Mo layers in all samples. Hence, localised short ranged  
4 delamination features observed at the Ti/Mo interface of the Ti-  
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6 1000  $\mu\text{m}$  sample (**Figure 3e**) are mostly assigned to locally high  
7  
8 roughness. Further testing was carried out on Ti substrates taken  
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10 at 560 °C for 20 mins in the absence of other materials to confirm  
11  
12 the impact of heat over the relaxation of Ti. As expected, we found  
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14 that compressive stress was drastically reduced in heat-treated  
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16 samples. However, it was not reduced as much as in Ti substrates  
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18 of Ti/Mo/CZTS samples. This suggests that in the stack of  
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20 materials, the re-organisation of Ti atoms at the surface of the  
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22 Ti substrate was more efficient, supported by the bi-directional  
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24 diffusion of metallic ions, namely  $\text{Ti}^{4+}$ ,  $\text{Cu}^{1+}$ , and  $\text{Zn}^{2+}$  ions.  
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## 30 CONCLUSIONS

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32 With this work we demonstrated the successful solution processing  
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34 of CZTS solar cells on flexible Ti substrate with up to 2.88% power  
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36 conversion efficiency achieved on 75  $\mu\text{m}$  thick foil. Whilst this was  
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38 achieved on a metal substrate readily usable for roll-to-roll  
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40 manufacturing, specific issues related materials processing were  
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42 highlighted. The unexpectedly efficient conduction of heat through  
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44 the Ti substrate (compared to a sodium lime glass substrate, even  
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46 at comparable thickness) led to the fast nucleation of CZTS  
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48 crystals at the bottom of the layer, favouring the formation of  
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50 small crystals and pores which are detrimental to device  
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52 efficiency. The top of the films crystalized much slower and  
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3 displayed larger crystals together with lower levels of porosity.  
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5 Another undesirable phenomenon related to the diffusion of  
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7 metallic ions: we observed the diffusion of  $\text{Ti}^{4+}$  ions from the  
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9 substrate to the bottom part of the CZTS film whilst  $\text{Cu}^{1+}$  and  $\text{Zn}^{2+}$   
10  
11 leached out of the film and diffused downwards to the metallic  
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13 substrate, contributing to further porosity. However, this may be  
14  
15 prevented by introducing barrier layers, a method already  
16  
17 successfully reported to minimize the conversion of Mo to  $\text{MoS}_2$ .<sup>17</sup>  
18  
19 In terms of device characteristics, increased recombination and  
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21 resistance losses were found in the bulk of the CZTS film prepared  
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23 on Ti substrates compared to SLG-based devices. These were  
24  
25 associated with thermally induced porosity and high density of  
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27 grain boundaries, pronounced  $\text{MoS}_2$  formation and metallic ions  
28  
29 diffusion. These results suggest that further optimization of the  
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31 sulfurisation process is necessary and may result in the  
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33 fabrication of devices with outputs comparable to SLG-based  
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35 devices.  
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#### 44 **ASSOCIATED CONTENT**

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46 **Supporting Information** Available: Characteristics of substrates,  
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48 Transmittance and reflectance of AZO film, SEM images and  
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50 photovoltaic performance parameters of the CZTS devices fabricated  
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52 with different Ti substrate thicknesses are presented. This  
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3 material is available free of charge via the Internet at  
4  
5 <http://pubs.acs.org>.  
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### Graphical abstract

