

1 **Improvement of biomethane potential of sewage sludge anaerobic co-digestion by**
2 **addition of “Sherry-wine” distillery wastewater.**

3 **Authors**

4 Vanessa Ripoll²

5 Cristina Agabo-García¹

6 Montserrat Perez¹

7 Rosario Solera¹

8 **Affiliation**

9 ¹ Department of Environmental Technologies, University of Cadiz, Campus de Puerto
10 Real, 11500 Puerto Real, Cadiz, Spain.

11 ² Biosciences Research Institute. School of Experimental Science, Universidad
12 Francisco de Vitoria, UFV, Building E, Ctra. M-515 Pozuelo-Majadahonda Km 1800,
13 28223, Pozuelo de Alarcón, Madrid, Spain.

14 **Corresponding author: Rosario Solera**

15 **E-mail addresses**

16 vanessa.ripoll@ufv.es (V. Ripoll)

17 cristina.agabo@uca.es (C. Agabo-García)

18 montserrat.perez@uca.es (M. Perez)

19 rosario.solera@uca.es (R. Solera)

20 **Abstract**

21 Co-digestion of sewage sludge (SS) with other unusually treated residues has been
22 reported as an efficient method to improve biomethane production. In this work, Sherry-
23 wine distillery wastewater (SW-DW) has been proposed as co-substrate in order to
24 increase biomethane production and as a breakthrough solution in the management of
25 both types of waste. In order to achieve this goal, different SS:SW-DW mixtures were
26 employed as substrates in Biomethane Potential (BMP) tests. The biodegradability and
27 biomethane potential of each mixture was determined selecting the optimal co-substrate
28 ratio. Results showed that the addition of SW-DW as a co-substrate improves the
29 anaerobic digestion of SS in a proportionally way in terms of CODs and biomethane
30 production. The optimal co-substrates ratio was 50:50 of SS:SW-DW obtaining
31 $\%VS_{\text{removal}} = 54.5\%$; $Y_{\text{CH}_4} = 225.1 \text{ L CH}_4/\text{kg}_{\text{sv}}$ or $154 \text{ L CH}_4/\text{kg}_{\text{COD}_t}$ and microbial
32 population of 5.5 times higher than sole SS. In this case, $\%VS_{\text{removal}} = 48.1\%$; Y_{CH_4}
33 $= 183 \text{ L CH}_4/\text{kg}_{\text{sv}}$ or $135 \text{ L CH}_4/\text{kg}_{\text{COD}_t}$. The modified Gompertz equation was used for
34 the kinetic modelling of biogas production with successful fitting results ($r^2 = 0.99$). In
35 this sense, at optimal conditions, the maximum productivity reached at an infinite
36 digestion time was $(Y_{\text{CH}_4}^{\text{MAX}}) = 229 \pm 5.0 \text{ NL}/\text{kg}_{\text{sv}}$; the specific constant was $K = 25.0 \pm$
37 $2.3 \text{ NL}/\text{kg}_{\text{sv}} \cdot \text{d}$ and the lag phase time constant was $(\lambda) = 2.49 \pm 0.19$.

38

39 **Keywords:** *biochemical methane potential, anaerobic digestion and co-digestion,*
40 *sewage sludge, kinetic parameters, biogas production.*

41

42

43 **1 Introduction**

44 Sewage sludge is produced in large quantities in urban areas all over the world. This
45 waste is usually managed by wastewater treatment plants (WWTP) where digesters are
46 often oversized and the cost of sludge treatment representing approximately 50% of the
47 total running cost of WWTPs. For this reason, in the context of circular economy
48 established in H2020 European strategy, Anaerobic Digestion (AD) process is of great
49 importance due to that this process achieve the highest utility of the sewage sludge (SS),
50 replacing other energy resources and limiting the associated CO₂ emissions derived
51 from SS disposal (Gherghel et al., 2019). There have been multiple studies about how
52 improve the production of biomethane in WWTP such as pretreatments or co-digestion
53 (Kor-Bicakci, and Eskicioglu, 2019). In this sense, co-digestion with agro-industrial
54 wastes has been reported as an efficient method to improve biomethane production of
55 SS as well as to manage other unusually treated residues (Maragkaki et al., 2017). In
56 general, the main advantages of anaerobic co-digestion (ACoD) are related to the
57 optimization of the required ratio of nutrients, the dilution of potential toxic compounds
58 (Sosnowski et al., 2003), as well as supplying buffering capacity and establishing the
59 required moisture content (Mshandete et al., 2004).

60

61 In the South of Spain (Cádiz region) there were 83 WWTP according to Andalusian
62 Ministry of Environment and Town Planning (AMET 2017). Seven 7 of them were
63 located in the “Sherry-wine” cellar region. “Sherry-wine” (SW) is the most important
64 wine produced in Cádiz region. The winemaking process of Sherry wine is marked by
65 specific climatic conditions and unique industrial process (“solera” system) used
66 exclusively in the Sherry area (Roldán et al., 2010). In this region, according to
67 Regulatory Council of D.O "Jerez-Xérès-Sherry"- "Manzanilla-Sanlúcar de Barrameda"
68 - "Vinagre de Jerez"; RCDO Sherry, 2017) there are 63 cellars focusing not only on

69 wine aging but also winemaking. However, as others winemaking industries, these
70 generate large volumes of sherry-wine distillery wastewater (SW-DW) (also called wine
71 vinasses).

72

73 SW-DW is a mixture of produced wastewater on the bottom of the distillery unit, grape
74 juice spills and chemical cleaning products of equipment and tanks. This waste
75 constitutes an environmental issue due to its strongly acidic pH and high organic load
76 (around Chemical oxygen demand (COD) = 40 g O₂/L), which includes several
77 recalcitrant pollutants such as polyphenols (e.g tannins) (Petta et al., 2017) and other
78 chemical compounds such as melanoidins, (Yavuz 2007) fertilizer and pesticides (rich
79 in nitrogen and phosphorous) or caustic soda (Ioannou et al., 2013). Consequently,
80 wineries must manage this waste using effective technologies in order to comply with
81 environmental policies (Siles et al., 2011). In this sense, these industrial wastes are
82 generated in a limited production period, so ACoD with SS could be economically
83 advantageous in terms of sharing installations, ease of handling of the wastes (avoiding
84 disposal) and improving economic viability (Mata-Álvarez et al., 2014). In addition, the
85 co-digestion of both substrates will avoid the disposal of SW-DW on soils/evaporation
86 lagoon. Moreover, in the case of using SW-DW as an agro-industrial co-substrate, it
87 could enhance the C/N ratio of SS substrate (Zeshan et al., 2012). This is a simple way
88 of improving biomethane production of SS, avoiding other expensive and complex
89 techniques proposed in bibliography such as pre-treatments (Siles et al., 2011).

90

91 Furthermore, a proper kinetic study is helpful for reproducing the AD process and
92 understanding the feasible inhibitory mechanism. In addition, it is important to develop
93 an up-to-date model taking into account the different variables involved: operational

94 conditions, mode of operations, origin of feed, type of inoculum, etc. Continuing with
95 this approach, several mathematical models such as Logistic, Gompertz, Sigmoid
96 (Martín et al., 2018) or Chen-Hashimoto model (Borja et al., 2003) have been applied.

97

98 AD kinetics models have been developed mainly in sewage sludge feedstock as well as
99 in pig and crop wastes and recently, in other ago-wastes (Martín et al., 2010). In this
100 sense, the AD of sole SW-DW has been previously studied (including kinetic
101 evaluation) as a successful biological treatment for controlling the pollution of this
102 waste and to recover energy in semi-continuous mode in different technologies: fixed-
103 film reactors (Pérez et al., 2005a); high rate reactors (Pérez et al., 2005b) and after
104 different pre-treatments such as biological (Jiménez et al. 2006) and advanced oxidation
105 (Siles et al., 2011). However, there are no kinetics contributions to batch mode of the
106 co-digestion of these both residues without any pretreatment. So, it is important to study
107 its potential, operational feasibility and kinetic in order to evaluate the possibility of
108 scaling-up such process as method of management of these both substrates together
109 (Chowdhary et al., 2018).

110

111 In the present study, ACoD of sewage sludge (SS) and SW-DW is proposed as an
112 effective new alternative in order to improve biomethane production in WWTPs from
113 Sherry-wine region. The main objective of this work has been to study the influence of
114 SW-DW in anaerobic co-digestion with SS on biodegradability and biomethane
115 production. In addition, a kinetic model as a previous step for co-digestion scaling up
116 process has been proposed.

117

118 **2 Material and methods**

119 **2.1 Substrates and co-digestion mixtures**

120 The substrates used in the experimental stage were collected directly from two real
121 industrial facilities. The SS came from a secondary treatment floatation unit from
122 Guadalete WWTP in Jerez (Cádiz, Spain). The SW-DW was obtained from Gonzalez-
123 Byass, an ethanol producing wine-distillery plant located in Jerez. Substrates were
124 collected fresh and stored at 4 °C for a maximum of one month. The pH values of co-
125 digestion mixtures were in the range of 6.0-7.0 for this reason it was adjusted to 7.0-8.0
126 using 2 M sodium hydroxide solution prior to digestion. Different mixtures of SS:SW-
127 DW (% v/v) were employed in the present study (75:25; 50:50; 25:75), as well as sole
128 SS and sole SW-DW.

129 **2.2 Inoculum characteristics**

130 The inoculum was collected from a mesophilic 5-L laboratory-scale Continuously
131 Stirred Tank Reactor (CSTR) available in the Research Group operating at HRT = 20 d
132 and fed with SS coming from secondary decanter of WWTP from Jerez (Cádiz-Spain).
133 The characteristics of the inoculum are shown in Table 1.

134 **2.3 Experimental set-up and procedures**

135 BMP tests were carried out according to Angelidaki et al., (2009). Serum bottles were
136 used as reactors with total volume of 250 mL. The effective volume was 150mL and the
137 head space was 100 ml. Reactors were placed in an orbital shaker at 85 rpm under
138 mesophilic conditions (35 ± 1 °C). The digesters were loaded with a mixture of
139 inoculum and substrate, resulting in a final concentration of 40% w/w of inoculum
140 which is considered optimum for biogas production and substrate acclimatization
141 (Montañés et al., 2014). The wastes were then added to the reactors in different
142 proportions to obtain the following SS:SW-DW (% v/v) ratios: 75:25, 50:50, 25:75
143 (Table 2) as well as only SS and SW-DW. The control reactor, containing only

144 anaerobic inoculums and water, was also incubated in order to determine background
145 gas production.

146 Due to the strong influence of the microbial activity of the inoculum on methane yield
147 and methane production rate, pre-incubation of the inoculum was carried out at 35 °C
148 for 7 days before starting the BMP assays. This procedure, which is used to reduce the
149 endogenous methane production of the inoculum, is recommended by several authors
150 with the aim of developing a standardized method for BMP assays (Hollinger et al.,
151 2016).

152

153 All the reactors were run in triplicate and the averages of the data collected were
154 calculated and reported. All the reactors were subsequently purged with 100% N₂ for 3-
155 4 min to maintain anaerobic conditions at the appropriate pH and then sealed with
156 natural rubber stoppers and plastic screw caps. BMP tests were performed until daily
157 methane production meant less than 1% of total (25 days)

158 Biogas production and biogas composition were determined daily during the digestion
159 period. At the end of the digestion period, pH and data on total and volatile solids (TS,
160 VS), Volatile Fatty Acids (VFA) and total and soluble chemical oxygen demand (COD_t,
161 COD_s) were collected for all the reactors so as to calculate the efficiency of the
162 biological treatment.

163 **2.4 Analytical methods**

164 pH, TS, VS, COD_t, COD_s and TN were determined according to Standard Methods
165 (APHA et al., 2005). pH determination was taken by pHmeter type CRISON
166 MICROPH 2001 with a temperature probe. For TS, VS and FTS, samples were weighed
167 in ceramic boats in a laboratory balance Cobos type and drying in oven type ELF14 de
168 CARBOLITE.

169 TN was determined by using a total nitrogen analyzer provided by Skalar Company,
170 mod. FormacsHT and FormacsTN.

171 VFA (acetic, propionic, iso-butyric, butyric, iso-valeric, valeric, iso-caproic, caproic and
172 heptanoic acid) were determined by gas chromatography (GC-2010 Plus Shimadzu).
173 Total acidity was calculated by the sum of the individual fatty acids.

174 Gas composition was determined employing a gas chromatography technique (GC-2010
175 Shimadzu). The analysed gases (H₂, CH₄, CO₂, O₂ and N₂) were measured by means of
176 a thermal conductivity detector (TCD) at 250 °C using a Supelco Carboxen 1010 Plot
177 column. The oven temperature was programmed between 35 and 200 °C. Manual
178 injection was carried out employing a sample volume of 250 µL. The carrier gas was
179 helium at 35 kPa of pressure (Montañés et al., 2014).

180 **2.5 Microbial analysis**

181 FISH technique was used to determine the percentage of each microbial population
182 group in best operational condition and in sample with sole SS in order to compare
183 them. In FISH methodology, probe(s) 16S ribosomal ribonucleic acid (rRNA)-targeted
184 oligonucleotide were used to identify the group of microorganisms (Zahedi et al., 2018).
185 The counting of microorganisms had been developed using an Axio Imager Upright
186 epifluorescence microscope (Zeiss) equipped with a 100 W mercury lamp and a
187 100 × oil objective. Microbial groups determined were: *Eubacteria*, *Archaea*, butyrate
188 utilising acetogens (BUA) propionate utilizing acetogens (PUA), hydrogen
189 utilizing methanogens (HUM) and acetate utilizing methanogens (AUM). Percentages
190 of each group were calculated taking as total the sum of the relative
191 amounts of *Eubacteria* and *Archaea*. Acetogens were calculated as the sum of the
192 relative amounts of PUA and BUA. Hydrolytic acidogen bacteria (HAB) were
193 calculated as the difference in the relative amounts of *Eubacteria* and Acetogens

194 (Zahedi et al., 2018). The microbiological analyses were carried out in triplicate at the
195 end of BMP test.

196

197 **2.6 Data analysis**

198 *2.6.1 Methane production and methane productivity.*

199 Biogas production was daily determined by indirect measuring of the cumulative
200 pressure inside the bottles with pressure transducers. Pressure data were used to infer
201 the volume of biogas at standard temperature and pressure conditions, according to the
202 ideal law of gases, Eq. (1).

$$203 \quad P \cdot V = n \cdot R \cdot T \quad (1)$$

204 where P is absolute pressure (kPa), V is volume (m^3), n is amount of substance (moles)
205 T is temperature (K), and R is the universal gas constant ($8.3145 \text{ L} \cdot \text{kPa} / \text{K} \cdot \text{mol}$).

206 Cumulative methane volume production was calculated by means of the sum of the
207 daily methane volume as indicated in Eq. (2):

$$208 \quad V_{CH_4}^t(NL) = \sum_{i=1}^{i=t} (V_{CH_4}^i - V_{control}^i) \quad (2)$$

209 Where $V_{CH_4}^t$ is the net volume of methane, $V_{CH_4}^i$ is the experimental volume of methane
210 measured when co-substrate is used and $V_{control}^i$ is the volume of methane produced in
211 the control experiment. Methane productivity (Y_{CH_4}) in base of initial VS was
212 calculated as $V_{CH_4}^t$ per kg of initial VS (NL_{CH_4}/kg_{VS}) in order to developed the kinetic
213 modelling. Experimental biomethane potential (BMP_{exp}) was calculated as the
214 asymptote of the methane productivity curve. Methane productivity (Y_{CH_4}) in base of
215 initial COD was calculated as $V_{CH_4}^t$ per kg of initial COD (NL_{CH_4}/kg_{CODi}) in order to
216 compare the results with bibliography.

217 *2.6.2 Substrate biodegradability.*

218 Substrate biodegradability was related to the removal rates obtained after AD in terms
219 of biodegradability parameters removal as shown in Eq. (3):

$$220 \quad \text{parameter}(P) \text{ removal}(\%) = \frac{P_0 - P_t}{P_0} \cdot 100 \quad (3)$$

221 Where “P” is the biodegradability parameter analysed in this study: COD_t, COD_s, VS,
222 VFA and P₀ and P_t are the initial and final value of the respective parameter.

223 2.6.3 Kinetic modelling.

224 Biogas production during AD involves a complex reactions network with many stages
225 (hydrolysis, acidogenesis, acetogenesis, and methanogenesis). Therefore, it is necessary
226 to assume several simplifications in order to mathematically describe the macroscopic
227 system behaviour. In the present study, the modified Gompertz model (Eq. 5) was used
228 to predict biogas production. This model has been the most widely applied kinetic
229 model for describing anaerobic digestion by previous studies (Awais et al., 2016; Zhen
230 et al., 2016; Zhao et al., 2018). The modified Gompertz model assumes that biogas
231 production is proportional to microbial activity and that gas production follows an
232 exponential rise to reach maximum level.

$$233 \quad Y_{CH_4} \left(\frac{NL_{CH_4}}{kg_{SVO}} \right) = Y_{CH_4}^{MAX} \cdot \exp \left[-\exp \left(-\frac{K \cdot e^1}{Y_{CH_4}^{MAX}} \cdot (\lambda - t) + 1 \right) \right] \quad (5)$$

234 Three kinetic parameters are required in the modified Gompertz model to predict the
235 evolution of the methane productivity: the maximum yield reached at an infinite
236 digestion time ($Y_{CH_4}^{MAX}$), the specific constant rate (K) and the lag phase time constant (λ).

237 Kinetic modelling was performed employing OriginPro® software. Simple non-linear
238 curve fitting was carried out to reproduce the biogas methane production for each assay.

239

240 3 Results and Discussion

241 The characteristics of raw co-substrates are shown in Table 1. As it can be observed the
242 characterization values in SS are in the common range presented in bibliography

243 (Thorin et al., 2018). SW-DW also showed values of COD, TS, VS, and pH in the
244 common range reported by bibliography: COD_t = 0.8-182 g O₂/L, TS = 2-127 g/L, VS
245 = 0.12-1.33 g/L and pH = 3.5-7.3 (Beltrán et al., 1999; Petrucciouli et al., 2000; Benítez
246 et al., 2003; Eusebio et al., 2004; Pérez et al., 2006; Lucas et al., 2009). However, VFA
247 value was lower than bibliography (VFA = 1.33-77 g/L). This fact can be explained
248 because the type of grape that was used in the sherry-wine making process (“palomino”
249 grape) which contains low values of total acidity and high pH values (García et al.,
250 2009).

251 Moreover, SS showed a low C/N ratio (Table 2). Using only SS could affect AD by
252 rapid consumption of nitrogen. This could affect AD operation by accumulation of
253 VFAs (Li et al., 2011) and inhibiting methanogens leading to low biogas production.
254 However, when SW-DW was increased, the C/N ratios were higher (Table 2)
255 contributing to enhance AD development. In spite of C/N ratio varies with type of
256 substrates (Li et al., 2011); it is known that the optimal C/N ratio for a proper AD is 20-
257 30 (Zeshan et al., 2012); which is reached in this work when concentrations of SW-DW
258 were 75 and 100%.

259

260 **3.1 Substrate biodegradability**

261 Substrate biodegradability was measured by removal of initial characteristics in serum
262 bottle. Characterization parameters at the beginning and at the end of the BMP tests are
263 shown in Table 2. In general, all the parameters were slightly reduced when SW-DW
264 was increased because the lower content of organic matter. In order to compare
265 reduction tendency, it has been calculated the removal percentage of each parameter
266 (Figure 1). The biodegradability of SS in terms of COD_{t,removal} is similar than co-
267 substrate mixtures when SS ≥ 50% obtaining values around 48.5 ± 1.11%. Whereas, the

268 biodegradability values of co-substrates were enhanced when proportion of SS < 50%
269 obtaining, %COD_{tremoval} values of 56.3% ± 4.1 for 25:75 and 66.5 ± 8.7 % for SW-DW .
270 The increasing in COD_{tremoval} tendency is more remarkable regarding CODs. In this case,
271 in order of decreasing removal of CODs: 86% for SW-DW > 76.7% for 25:75 of
272 SS:SW-DW (v/v) > 65% for 50:50 of SS:SW-DW (v/v) > 54% for 75:25 of SS:SW-DW
273 (v/v) > 40.8% for only SS. In fact, there was a linear relationship (%COD_{Sremoval} =
274 0.452·%SW-DW + 41.9; r² = 0.995) for this parameter as it can be seen in Figure 1. So,
275 in spite of linear augmentation of CODs elimination, COD_t removal did not follow this
276 tendency until proportion of SW-DW was > 50%. At this point, SW-DW soluble
277 compounds were in high quantity and the contribution of CODs in the mixture with SS
278 to COD_t was higher (70%).

279 Attending to %VS_{tremoval}, a similar tendency that COD_t was observed. In this case, the
280 %VS_{tremoval} values obtained for SS, 75:25 and for 50:50 of SS:SW-DW (%v/v) were
281 50.0% ± 0.8. After that, when SW-DW was 75% the values were increased to 54% ±
282 0.4 and when SW-DW was 100% the VS%_{tremoval} was 61.4% ± 2.7. So, in general the
283 increment of SW-DW proportion in the co-substrate mixture improves the removal rate
284 of main biodegradability parameters of SS after biological treatment, due to the higher
285 content of dissolved organic matter provided.

286 Finally, in general, the analysis of VFA content at the end of BMP test showed that
287 there was an accumulation of 8% of VFA after AD of SS as it was expected by poor
288 C/N ratio. However, this accumulation is not enough for inhibiting the whole process of
289 AD but reducing biomethane production as it can be seen in the next section. However,
290 after ACoD the elimination of VFA was higher when %SW-DW was increased, being
291 complete at concentration ≤ 75% of SW-DW where C/N ratios was between 20-30.

292

293 3.2 *Biogas production in BMP tests*

294 The evolution of the cumulative gross methane volume for each run (including the
295 control test) can be observed in Figure 2 (A). It can be seen that the methane production
296 was increasing with content of SS. The highest methane production was obtained for
297 both anaerobic digestion of SS and 75:25% v/v of SS:SW-DW, and the lowest methane
298 production was obtained when the substrate was only SW-DW. In all the cases, the
299 maximum percentage of CH₄ in biogas was 70%. Initial characterization of the
300 employed substrates showed that SS contains a higher organic load (in terms of VS, as
301 well as COD_t) than SW-DW (Table 2). Thus, the higher net amount of biodegradable
302 organic matter in SS leads to a higher gross methane volume production.

303

304 However, in order to compare the biomethane potential from different wastes, methane
305 productivity in base of organic matter (VS and COD_t) must be calculated to normalize
306 the values. In this sense, the evolutions of the methane yield during the sole digestion of
307 SS and SW-DW and the co-digestion of different mixtures are shown in Figure 2 (B).
308 According to these results, the methane yield in base of VS of co-digested mixtures was
309 proportional to the composition employed. In this respect, the addition of SW-DW as a
310 co-substrate in the anaerobic digestion of SS improved the methane yield in all the
311 studied cases. In order of decreasing it was obtained 300 NL CH₄/kg_{VS0} for SW-DW >
312 250 NL CH₄/kg_{VS0} for 75% of SW-DW > 225 NL CH₄/kg_{VS0} for 50% v/v of SW-DW >
313 210 NL CH₄/kg_{VS0} for 25% v/v of SW-DW > 175 NL CH₄/kg_{VS0} for SS (Figure 2A).

314

315 Regarding CH₄ yield with respect COD_{t0} (data not shown), the maximum yield was 154
316 L CH₄/kg_{COD_t} for 50:50% v/v of SS:SW-DW; following by 146 LCH₄/kg_{COD_t} for 75:25%
317 v/v of SS:SW-DW and 135 LCH₄/kg_{COD_t} for the rest (sole digestions of SW-DW and SS

318 and co-digestion at 25:75% v/v SS:SW-DW proportion). So, the maximum productivity
319 obtained was achieved by mixing 50:50% v/v of both co-substrates. Similar CH₄ yield
320 results were obtained from previous studies using pretreated sludge by microwave
321 disintegration as a substrate of anaerobic digestion (Kavitha et al., 2018), being the
322 mixture with SW-DW more economically feasible.

323 It should be noted that pre-incubation of the inoculum at mesophilic temperature for 7
324 days was found to be an appropriate treatment to reduce endogenous methane
325 production, as it can be seen from the results of the blank assay. Some authors have
326 previously established that inoculum production should be below 20 % of total methane
327 production in the BMP test (Hollinger et al., 2016). In the present study, endogenous
328 methane production did not exceed 11 % of the production from co-digestion of the
329 studied substrates. Furthermore, the inoculum still remained metabolically active after
330 pre-incubation, as it is assumed in initial methane production in BMP tests. Therefore,
331 the results obtained in this work validate the experimental procedure.

332

333 **3.3 Kinetic modelling**

334 For each assay, the modified Gompertz model was fitted to experimental data as shown
335 in Figure 3. Generally, there is an excellent overall agreement between the model
336 prediction and the experimental data, reaching the highest regression coefficients in all
337 cases (r^2 results above 0.99). This means that this model might explain 99% of the total
338 variation of experimental data (Figure 3). As it can be seen in the Figure 3, when
339 proportion of SW-DW was increased, the inflection point (K/e) appeared sooner: 7.5 d
340 (A) > 7 d (B) > 6.5 d (C) > 5d (D) > 4d (E). So, the slope of the lineal growing from
341 ending of lag phase to inflection point was higher when higher SW-DW was used,
342 leading to higher growing velocity.

343 The values for each kinetic parameter and their statistical errors as well as those for the
344 experimental BMP are summarized in Table 4. When proportion of SW-DW was
345 increased, the K was augmented and the lag phase was reduced. These both facts are the
346 consequence of more available organic matter that permit microorganisms to grow
347 sooner (lower λ) and easily, reaching higher K values. In this sense, methanogenic
348 population growing lead to more production of methane and hence higher $Y_{CH_4}^{MAX}$ values.
349 Regarding this parameter, the meaning of the theoretical kinetic parameter is directly
350 related to the experimental one. The relative error between both parameters had a
351 difference below 7% in all runs (Table 4), showing an excellent model prediction of the
352 studied system. It is also important to remark that the lag phase is higher when higher
353 proportion of SS is used in the co-digestion.

354

355 Table 4 also summarizes the values of the kinetic parameter of the modified Gompertz
356 model previously published by other authors. When SW-DW is used as co-substrate, the
357 $Y_{CH_4}^{MAX}$ parameter is higher (218-294 NL/kg_{vs}) than those obtained using only SS (167
358 NL/kg_{vs}) (Cordova et al., 2017) or in co-digestion with synthetic organic fraction of
359 municipal WWTP or microalgae (148 and 164 NL/kg_{vs} respectively) (Nielfa et al., 2015
360 and Zhen et al., 2016).

361 However, when SS was used as substrate the kinetic parameters K and $Y_{CH_4}^{MAX}$ were
362 similar than bibliography values (Table 4) supporting the repeatability and reliability of
363 the BMP method. Only lag phase was higher when using inadapted inoculum.

364 In this study, when SW-DW is used alone or as co-substrate, the $Y_{CH_4}^{MAX}$ parameter was
365 also higher than those obtained for only SW-DW in previous research (Syaichurroz et
366 al., 2013 and Budiyo 2013-2014, Table 4) probably because the origin of the vinasses
367 was the sugarcane production instead of sherry-wine production. This underline the

368 availability of organic matter presents in SW-DW that is also reflected in higher K and
369 lower λ parameters.

370

371 The influence of feedstock composition on the value of the kinetic parameters is shown
372 in Figure 4. As previously stated, BMP depends directly on the composition of the
373 employed substrate, being proportional to the ratio of the mixture.

374 The influence of substrate composition on the specific constant rate seems to be
375 analogous to the observed trend for maximum methane production. The lowest value
376 was obtained for anaerobic digestion of SS, while the highest value was observed for
377 SW-DW. In the co-digestion assays, the specific constant rate is proportional to the
378 composition of the mixture. Consequently, co-digestion of SS with SW-DW leads to a
379 faster rate of anaerobic degradation and its associated biogas production than anaerobic
380 digestion of SS alone.

381 Finally, the lag phase time constant (λ) shows the duration of the first stage of the
382 process, during which methane production occurs at a slow rate. This macroscopic
383 kinetic parameter is probably associated with the hydrolysis stage, which is the main
384 rate-determining step in anaerobic digestion. In this sense, SW-DW contains many
385 simple organic compounds that anaerobic bacteria are able to metabolize easily into
386 biogas such as organic acids, carbohydrates and ethanol (Nayak et al., 2018). On the
387 other hand, SS

388 contains a high amount of lignocellulosic compounds, which need more time to be
389 degraded increasing the lag phase (Syaichurrozi et al., 2013). Regarding the results of
390 this work, biogas started to be produced after a lag phase of 0.43 days during SW-DW
391 fermentation, compared to 2.58 days in SS fermentation. It should be emphasized that
392 co-digestion reduces lag phase time considerably, as it can be seen in Figure 4 (C).

393

394 **3.4 Microbial population at optimal conditions**

395 A summary of the main microbial groups involved in the co-digestion of SS:SW-DW %
396 v/v 50:50 (the best conditions) and mono-digestion of SS is shown in Table 5. Figure 5
397 shows some photomicrograph of microbial groups in the SS:SW-DW 50:50 % BMP
398 test. Increasing in biomethane production is mainly reflected in total microbial
399 population augmentation. Total microbial population obtained in BMP of SS:SW-DW%
400 v/v 50:50 was $2.46 \cdot 10^{10}$ cell/ml, 5.5 times higher than those obtained in SS BMP test
401 ($4.49 \cdot 10^9$ cell/ml). Microbial population groups also showed different profiles at these
402 both conditions. Thus, *Eubacteria* percentage was higher in the case of using only SS as
403 substrate than in the case of 50:50% v/v of SS:SW-DW. Specifically, acetogenic
404 bacteria was 53.4% in the case of SS and 18% in the case of 50:50% v/v SS:SW-DW.
405 However, because higher population in the former case, it was $2.39 \cdot 10^9$ cell/ml of
406 acetogenic bacteria in SS against $4.42 \cdot 10^9$ cell/ml of 50:50% v/v SS:SW-DW.
407 Attending sub-groups in acetogenic bacteria the proportion BUA/PUA were 2.23 and 3
408 for SS and 50:50% v/v of SS:SW-DW respectively. On the other hand, in both cases
409 HAB was low (0-1%) due to hydrolytic stage had been concluded. In addition, when
410 50:50% v/v of SS:SW-DW was used, 81.9% of population was *Archaea* (being the
411 majority AUM, 74.4%) against only 45.2% when SS is used as substrate (being the
412 majority also AUM, 41.8%).

413 Hence, in general, it can be said that the different ratios *Eubacteria:Archaea* were
414 observed in the SS and SS:SW-DW BMP tests: 54.8:45.2 and 18.1:81.9, respectively;
415 making co-digestion microbial population more rich in *Archaea* (above all aceticlastic
416 methanogens).

417 **4 Conclusions**

418 The addition of SW-DW, as a co-substrate, improves the anaerobic digestion of SS in a
419 proportionally way in terms of $COD_{S_{removal}}$ and biomethane production. Optimal
420 conditions were 50:50% v/v SS:SW-DW with removal values of $\%VS_{removal} = 54.5\%$;
421 $BMP_{exp} = 225 \text{ L CH}_4/ \text{kg}_{VS}$ and productivity values of $154 \text{ L CH}_4/\text{kg}_{COD_t}$. The
422 experimental results indicate that, the Gompertz model can explain the final behaviour
423 and kinetics of the process with high degree of reliability ($r^2 > 0.99$) and pointing to the
424 best co-digestion configuration. In this sense, kinetic parameters determined at optimal
425 conditions 50:50% v/v of SS:SW-DW were ($K = 25.0 \pm 2.3 \text{ NL/ kg}_{VS} \cdot \text{d}$; $\lambda = 2.49 \pm 0.19$
426 and $Y_{MAX} = 229 \pm 5.0 \text{ (NL/kg}_{VS})$). This results are also supported by microbial analysis
427 where there was an enrichment of *Archaea* group in co-digestion, particularly in
428 aceticlastic methanogens. This optimal co-digestion mixture, can be used as starting
429 point in order to study the scaling up of the process. Controlled co-digestion of SS and
430 SW-DW should be desirable in order to obtain higher amount of methane in WWTPs of
431 “Sherry-wine” area by regularly addition of SW-DW collected. In this sense, because
432 the proximity and the volume of generation of both substrates, “Sherry-wine” region
433 can be considered as being well placed geographically for a successful management of
434 both substrates by co-digestion without using any pre-treatment saving energy and cost.

435

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439

440 **Nomenclature**

441 Acet Acetogenic bacteria

442 Arch Archaea

| | | |
|-----|------------------|---|
| 443 | AUM | Acetogens utili |
| 444 | BMP | Biomethane potential (NL_{CH_4}/kg_{SV}) |
| 445 | BUA | Butyrate utilising acetogens |
| 446 | CODs | Chemical oxygen demand (soluble) |
| 447 | CODt | Chemical oxygen demand (total) |
| 448 | Eub | Eubacteria |
| 449 | g_{H-Ac}/L | Acetic acid concentration (g/L) |
| 450 | HAB | Hydrolitic acidogenic bacteria |
| 451 | HRT | Hydraulic retention time (d) |
| 452 | HUM | Hydrogen utilising bacteria |
| 453 | K | Kinetic parameter from the modified Gompertz model ($NL_{CH_4}/kg_{SV}\cdot d$) |
| 454 | PUA | Butirate utilising acetogens |
| 455 | TS | Total solids |
| 456 | SS | Sewage sludge |
| 457 | Y_{CH_4} | Methane yield (NL_{CH_4}/kg_{SV}) |
| 458 | $Y_{CH_4}^{MAX}$ | Maximum methane yield from the modified Gompertz model measured |
| 459 | in | NL_{CH_4}/kg_{SV} . |
| 460 | $V_{CH_4}^t$ | Net volume of methane (NL_{CH_4}) |
| 461 | VFA | Volatile Fatty Acids |
| 462 | VS | Volatile solids |
| 463 | SW-DW | Sherry-wine distillery wastewater |
| 464 | WWTP | Wastewater treatment plant |
| 465 | λ | Lag-phase parameter from the modified Gompertz model (d) |
| 466 | | |
| 467 | Subscript | |

468 t Relating to time t
469 0 Relating to the initial condition
470 H-Ac Relating to acetic acid
471
472
473
474

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669 **TABLES**

670 **Table 1** Inoculum and raw co-substrates characteristics

671 **Table 2** Initial and final characteristics of substrates in serum bottle.

672 **Table 3** Kinetic parameter of the Gompertz model.

673 **Table 4** Summary of published studies on kinetic modelling of SS and WDW
674 employing the modified Gompertz model: value of the kinetic parameter
675 of the model.

676 **Table 5** Percentages of groups of microbiota for sole SS and 50:50% v/v of
677 SS:SW-DW.

678 **FIGURES**

679 .

680 **Figure 1** Influence of feedstock composition on the %removal of main
681 biodegradability parameters.

682 **Figure 2** (A) Evolution of gross methane volume production for each assay

683 (B) Evolution of methane yield for each substrate

684 **Figure 3** Evolution of methane yield and kinetic Gompertz model prediction for
685 each substrate and co-digestion mixtures: (A) SS (B) SS:SW-DW 75:25
686 (% v/v); (C) SS:SW-DW 50:50 (% v/v); (D) SS:SW-DW 25:75 (% v/v);
687 (E) SW-DW.

688 **Figure 4** Influence of feedstock composition on the kinetic parameters of the
689 modified Gompertz model (A) Maximum yield obtained, (B) specific
690 constant rate, and (C) lag phase time constant.

691 **Figure 5** Electron Microscopy photos of microbial population from different
692 groups of microorganisms after BMP test. Operational conditions: 50:50
693 SS:SW-DW, T = 35 °C, Dilution Factor (DF) = 1:200.

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695 **Figure Captions**

696 **Figure 1** CODt: square; CODs: circle; VS: upward triangle; VFA: downward
697 triangle.

698 **Figure 2** Control: square; SS:circle; 75:25 (% SS:SW-DW): upward triangle;
699 50:50 (% SS:SW-DW): downward triangle; 25:75 (% SS:SW-DW):
700 diamond; SW-DW: star.

701 **Figure 3** Methane yield: square; kinetic Gompertz model prediction: line.

702 **Figure 4** Kinetic parameters of the modified Gompertz model.

703 **Figure 5.** White dots : ufc.

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710 **Table 1** Inoculum and raw co-substrates characteristics

| Parameters | Inoculum | SS | SW-DW |
|---|-----------------|-------------|--------------|
| pH | 7.8 | 7.6 | 6.4 |
| CODt (kg/m ³) | 19.9 ± 0.4 | 53.9 ± 1.2 | 24.6 ± 2.2 |
| CODs (kg/m ³) | 9.7 ± 0.3 | 19.0 ± 0.3 | 20.7 ± 0.6 |
| TS (%) | 2.09 ± 0.03 | 3.67 ± 0.01 | 1.47 ± 0.11 |
| VS (%) | 1.21 ± 0.01 | 2.69 ± 0.03 | 1.06 ± 0.09 |
| VS/TS (%) | 58.0 ± 1.3 | 73.8 ± 0.5 | 72.6 ± 2.9 |
| Alkalinity (g _{CaCO3} /L) | 5.81 | 3.53 | 0.019 |
| VFA _t (g _{H-Ac} /L) | 0.41 | 2.85 | 0.75 |
| TN (kg/m ³) | 2.15 | 14.8 | 1.09 |
| C/N | 9.2 | 5.2 | 17.5 |

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Table 2

Initial and final characteristics of substrates in serum bottle.

| Parameters (kg/m ³) | SW-DW (% v/v) | | | | |
|------------------------------------|---------------|-------------|-------------|-------------|-------------|
| | 0 | 25 | 50 | 75 | 100 |
| COD _{t0} | 35.5 ± 0.2 | 32.0 ± 1.3 | 26.7 ± 0.4 | 24.5 ± 0.4 | 20.6 ± 0.9 |
| COD _{tf} | 18.8 ± 0.4 | 16.1 ± 1.0 | 13.7 ± 0.6 | 10.7 ± 0.6 | 6.9 ± 0.6 |
| COD _{s0} | 15.7 ± 0.3 | 16.2 ± 0.2 | 16.3 ± 0.3 | 17.2 ± 0.1 | 16.2 ± 0.4 |
| COD _{sf} | 9.3 ± 0.4 | 7.4 ± 0.4 | 5.7 ± 0.3 | 5.9 ± 0.6 | 2.3 ± 0.1 |
| VS ₀ * | 1.96 ± 0.05 | 1.73 ± 0.04 | 1.52 ± 0.09 | 1.20 ± 0.02 | 0.95 ± 0.03 |
| VS _f * | 1.03 ± 0.01 | 0.89 ± 0.01 | 0.70 ± 0.01 | 0.54 ± 0.02 | 0.37 ± 0.01 |
| VFA _{t0} ** | 1.68 | 1.21 | 1.19 | 0.92 | 0.63 |
| VFA _{tf} ** | 0.12 | 0.05 | 0.0247 | n. d. | n. d. |
| C/N ₀ | 5.2 | 10.8 | 16.4 | 21.9 | 27.5 |

* Unit: %; ** unit : gH-Ac/L.

Table 3 Kinetic parameter of the modified Gompertz model.

| SS:SW-DW (% v/v) | $Y_{CH_4}^{MAX}$ (NL/kgvs) | K (NL/ kgvs·d) | λ (d) | r^2 | BMP_{exp} (NL/kgvs) | Relative error (%) |
|----------------------------|---|-----------------------------|------------------------------------|-------------------------|--|----------------------------------|
| SS | 195.8 ± 4.6 | 13.4 ± 0.9 | 2.58 ± 0.22 | 0.995 | 183 ± 11.6 | 6.7 |
| 75:25 | 218.8 ± 5.8 | 19.8 ± 1.8 | 2.60 ± 0.24 | 0.989 | 210 ± 16.2 | 4.0 |
| 50:50 | 229.8 ± 5.0 | 25.0 ± 2.3 | 2.49 ± 0.19 | 0.990 | 225 ± 23.4 | 2.1 |
| 25:75 | 256.0 ± 2.0 | 26.2 ± 0.8 | 1.25 ± 0.07 | 0.998 | 255 ± 13.4 | 0.2 |
| SW-DW | 294.6 ± 3.5 | 31.7 ± 1.8 | 0.43 ± 0.12 | 0.995 | 301 ± 15.4 | 2.5 |

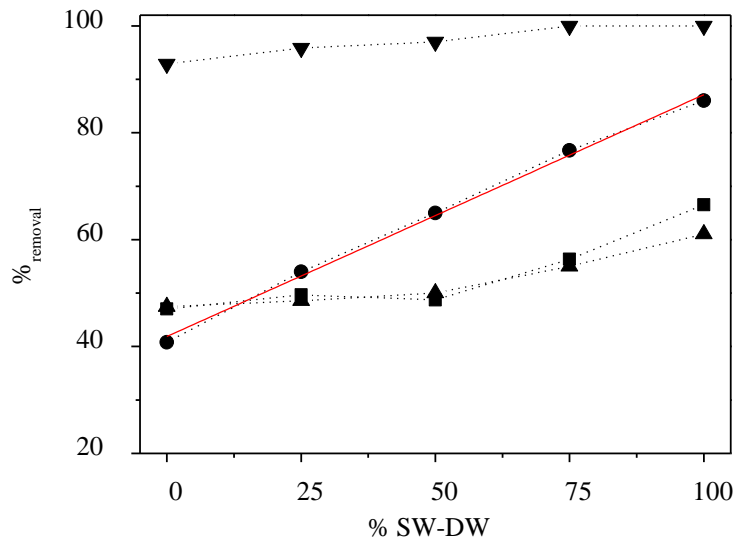
Table 4 Summary of published studies on kinetic modelling of SS and wine distillery wastewater employing the modified Gompertz model: value of the kinetic parameter of the model.

| Feedstock | $Y_{CH_4}^{MAX}$ (NL/kgvs) | K (NL/ kgvs·d) | λ (d) | r^2 | Reference |
|-------------------------------|--|-------------------------------|-------------------------------------|-------------------------|-------------------------------|
| Sewage Sludge | 148.1 | 31.4 | 0.00 | 0.96 | Nielfa et al. (2015) |
| | 167.0 | 32.4 | < 0.01 | 0.98 | Cordova et al. (2017) |
| | 163.5 | 13.4 | 0.00 | 0.94 | Zhen et al. (2016) |
| | 195.8 | 13.4 | 2.58 | 0.99 | This study |
| Wine Distillery Wastewater | 140.1 | 16.1 | 0.21 | 0.97 | Syaichurrozi et al. (2013) |
| | 115.0 | 24.7 | 0.80 | 0.99 | Budiyono et al. (2013) |
| | 39.4 | 7.0 | 0.96 | 0.99 | Budiyono et al. (2014) |
| | 296.6 | 31.7 | 0.43 | 0.99 | This study |

Table 5. Percentages of groups of microbiota for sole SS and 50:50% v/v of SS:SW-DW.

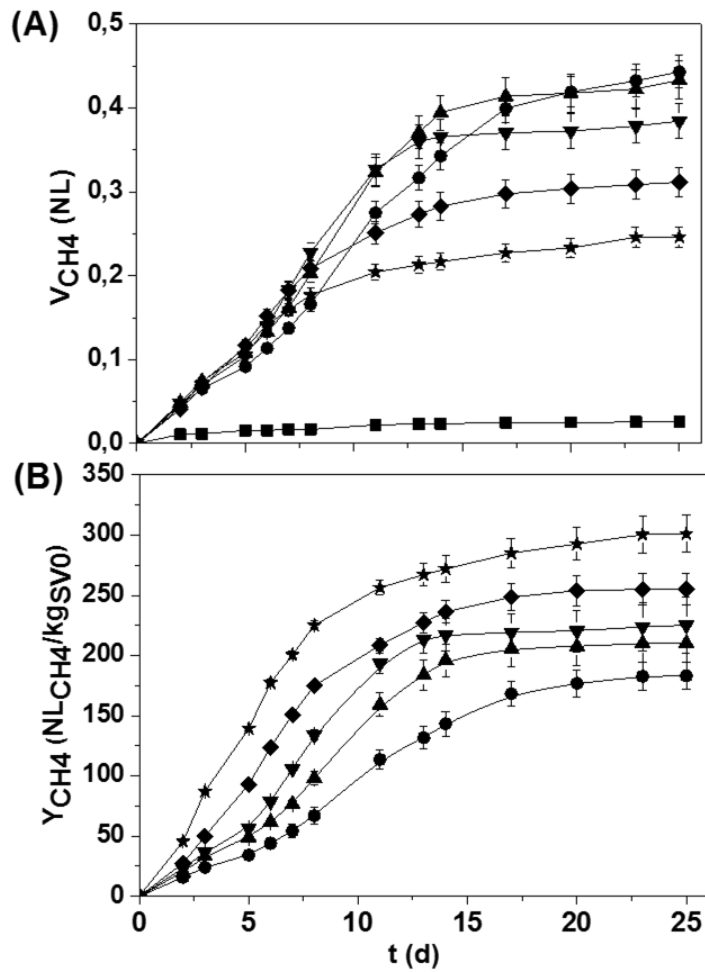
| % SW-DW | Microbial population | | | | | | | |
|---------|----------------------|-----|------|------|------|------|-----|------|
| | Eub | HAB | Acet | PUA | BUA | Arch | HUM | AUM |
| 0% | 54.8 | 1.5 | 53.4 | 16.2 | 37.2 | 45.2 | 3.4 | 41.8 |
| 50% | 18.1 | 0.1 | 18.0 | 4.41 | 13.5 | 81.9 | 7.5 | 74.4 |

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3 **Figure 1.** Influence of feedstock composition on the %removal of main
4 biodegradability parameters. (CODt: square; CODs: circle; VS: upward triangle; VFA:
5 downward triangle; red line: linear adjustment of data).



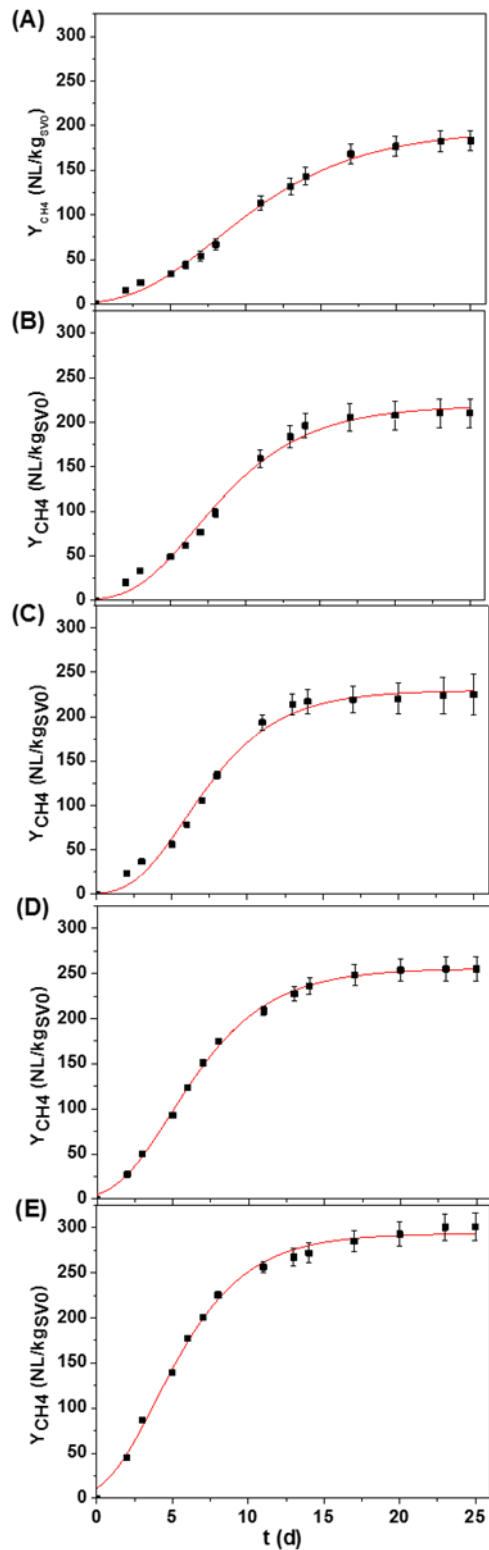
6

7 **Figure 2** (A) Evolution of gross methane volume production for each assay (B)

8 Evolution of methane yield for each substrate (control: square; SS: circle; 75:25 (%

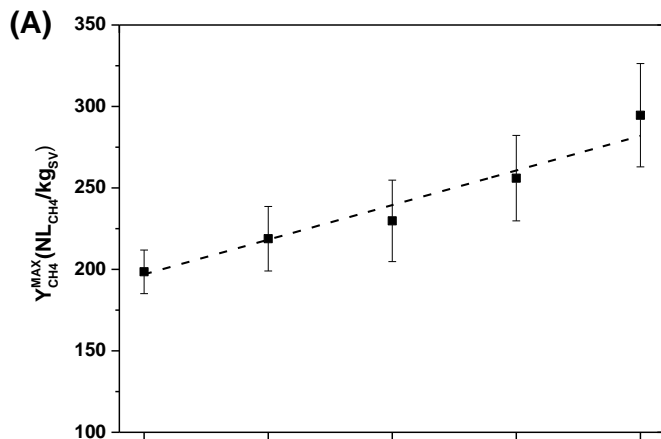
9 SS:SW-DW): upward triangle; 50:50 (% SS:SW-DW): downward triangle; 25:75 (%

10 SS:SW-DW): diamond; SW-DW: star).

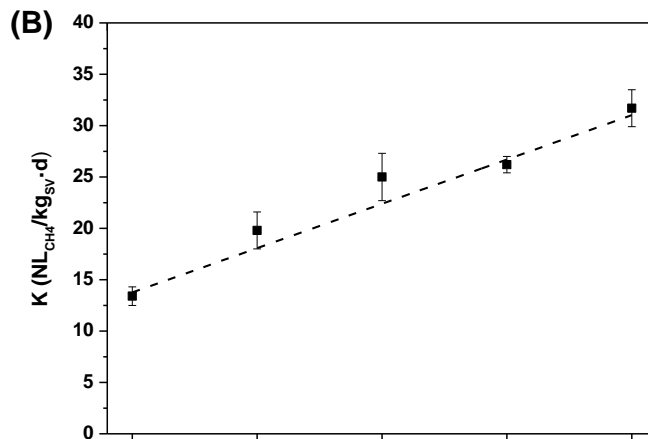


11

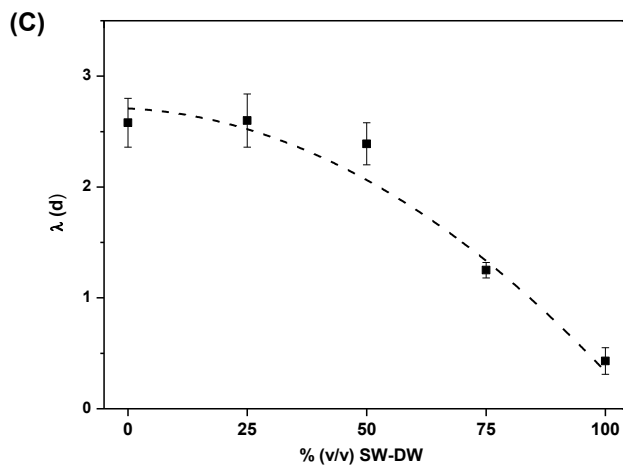
12 **Figure 3** Evolution of methane yield (square) and kinetic Gompertz model
 13 prediction (line) for each substrate and co-digestion mixtures: **(A)** SS v/v); **(B)** SS:SW-
 14 DW 75:25 (% v/v); **(C)** SS:SW-DW 50:50 (% v/v); **(D)** SS:SW-DW 25:75 (% v/v); **(E)**
 15 SW-DW



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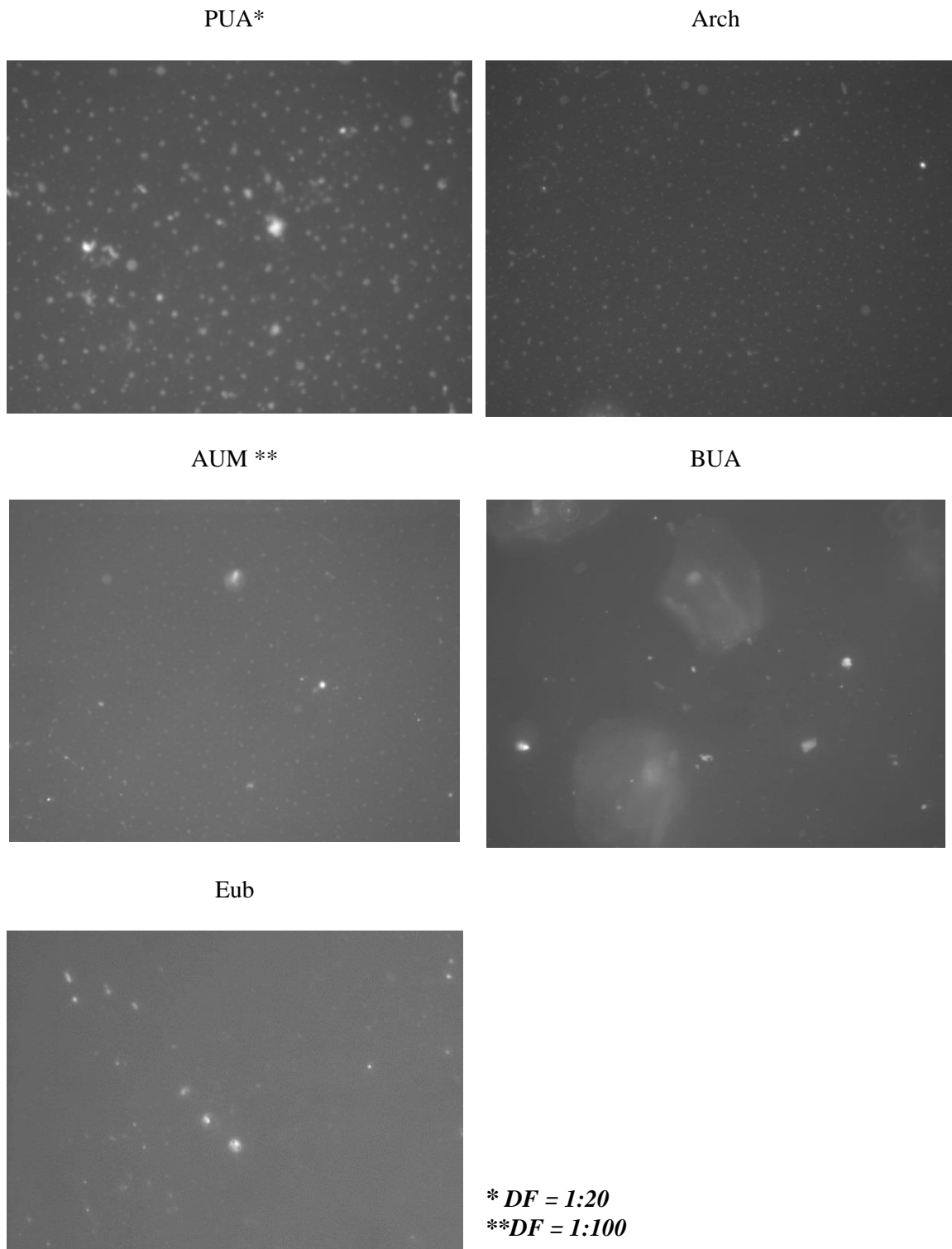
18

19 **Figure 4** Influence of feedstock composition on the kinetic parameters of the
 20 modified Gompertz model (A) Maximum productivity obtained, (B)
 21 specific constant rate, and (C) lag phase time constant.

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27 **Figure 5.** Electron Microscopy photos of microbial population from different groups of
 28 microorganisms after BMP test. Operational conditions: 50:50 SS:SW-DW, $T^a = 35\text{ }^\circ\text{C}$,
 29 Dilution Factor (DF) = 1:200.