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Claret, A., Cukanovaite, E., Burdge, K. et al. (3 more authors) (2020) Gravity and limb-darkening coefficients for compact stars : DA, DB, and DBA eclipsing white dwarfs. Astronomy & Astrophysics, 634. A93. ISSN 0004-6361

https://doi.org/10.1051/0004-6361/201937326

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Gravity and limb-darkening coefficients for compact stars: DA, DB, and DBA eclipsing white dwarfs

A. Claret^{1, 2}, E. Cukanovaite³, K. Burdge⁴, P.-E. Tremblay³, S. Parsons⁵, and T. R. Marsh³

Instituto de Astrofísica de Andalucía, CSIC, Apartado 3004, 18080 Granada, Spain

Dept. Física Teórica y del Cosmos, Universidad de Granada, Campus de Fuentenueva s/n, 10871, Granada, Spain

3 Department of Physics, University of Warwick, Coventry CV4 7AL, UK

Division of Physics, Mathematics and Astronomy, California Institute of Technology, Pasadena, CA 91125, USA

Department of Physics and Astronomy, University of Sheffield, Sheffield S3 7RH, UK

ABSTRACT

Context. The distribution of the specific intensity over the stellar disk is an essential tool for modeling the light curves in eclipsing binaries, planetary transits, and stellar diameters through interferometric techniques, line profiles in rotating stars, gravitational microlensing, etc. However, the available theoretical calculations are mostly restricted to stars on the main sequence or the giant branch,

Aims. The main objective of the present work is to extend these investigations by computing the gravity and limb-darkening coefficients for white dwarf atmosphere models with hydrogen, helium, or mixed compositions (types DA, DB, and DBA).

Methods. We computed gravity and limb-darkening coefficients for DA, DB, and DBA white dwarfs atmosphere models, covering the transmission curves of the Sloan, UBVRI, Kepler, TESS, and Gaia photometric systems. Specific calculations for the HiPERCAM instrument were also carried out. For all calculations of the limb-darkening coefficients we used the least-squares method. Concerning the effects of tidal and rotational distortions, we also computed for the first time the gravity-darkening coefficients $y(\lambda)$ for white dwarfs using the same models of stellar atmospheres as in the case of limb-darkening. A more general differential equation was introduced to derive these quantities, including the partial derivative $(\partial \ln I_o(\lambda)/\partial \ln g)_{T_{eff}}$. *Results.* Six laws were adopted to describe the specific intensity distribution: linear, quadratic, square root, logarithmic, power-2, and

a more general one with four coefficients. The computations are presented for the chemical compositions $\log[H/He] = -10.0$ (DB), -2.0 (DBA) and He/H = 0 (DA), with log g varying between 5.0 and 9.5 and effective temperatures between 3750 K-100 000 K. For effective temperatures higher than 40 000 K, the models were also computed adopting nonlocal thermal equilibirum (DA). The adopted mixing-length parameters are ML2/ $\alpha = 0.8$ (DA case) and 1.25 (DB and DBA). The results are presented in the form of 112 tables. Additional calculations, such as for other photometric systems and/or different values of $\log[H/He]$, $\log g$, and T_{eff} can be

Key words. stars: binaries: close; stars: evolution; stars: white dwarfs; stars: atmospheres; planetary systems

discovery of new exoplanetary systems. The LDCs play a very important role in their characterization. However, these coefficients are limited to main-sequence stars and stars on the giant branch. An exception to this rule is the pioneering work of Gianninas et al. (2013). These authors have focused their studies on more compact stars, specifically, white dwarfs (hydrogen-rich, DA, model atmospheres). As far as we know, the only study of the gravity-darkening exponents (GDE) for compact stars is that by Claret (2015), who used an analytical method to investigate how the temperature is distributed over distorted neutron stars.

The main motivation of the present work is to extend the investigations by Gianninas et al. (2013) by computing LDC for white dwarf atmosphere models of types DA, DB, and DBA. As a complement to the LDC calculations, we present for the first time the gravity-darkening coefficients (GDC) calculations for white dwarfs.

In the past decade, the number of known close binary systems containing compact stars has vastly expanded. Many of these systems exhibit photometric variability in the form of eclipses, ellipsoidal modulation, Doppler beaming, etc. Their light curves can therefore serve as a powerful tool for constraining system parameters because light-curve modeling can be used to infer parameters such as the mass ratio, the ratio of component radii to the semi-major axis of the orbit, and inclination. This information can then be combined with information such as spectroscopically measured radial-velocity semi-amplitudes or measured orbital decay due to gravitational wave emission to further constrain the properties of the system. However, a great limitation in modeling binaries involving one or two compact stars has been the absence of accurate limb- and gravity-darkening coefficients for these objects, which determine the surface flux distribution, and thus are crucial in determining the photometric

Send offprint requests to: A. Claret, e-mail:claret@iaa.es. Tables 1-112 are available in electronic form at the CDS via anonymous ftp or directly from the authors.

variability of the object. While the effects of limb darkening can be subtle (altering fluxes at the few percent level), modern astronomical cameras such as ULTRACAM (Dhillon et al. 2007) and its successor HiPERCAM (Dhillon et al. 2018) are able to routinely reach this level of precision for white dwarf binaries (e.g., Parsons et al. 2017; Rebassa-Mansergas et al. 2019) and thus accurate limb darkening coefficients are necessary to fully use these facilities for white dwarf science.

Limb darkening affects the shape of the ingress and egress of a white dwarf that is eclipsed. In principle, accurate limbdarkening coefficients permit measuring the binary inclination from just the eclipse, even in well-detached binaries (e.g., Littlefair et al. 2014), bypassing other expensive or indirect methods for constraining inclinations (Parsons et al. 2017). Moreover, limb-darkening coefficients are invaluable when white dwarfs are modeled in accreting binaries such as cataclysmic variables or AM CVn systems. In these cases, the white dwarf ingress and egress can be affected by accretion processes (e.g., flickering, or light from the accretion disk). Accurate limb-darkening coefficients lift much of the degeneracy when these light curves are modeled (e.g., McAllister et al. 2019). Limb darkening must also be considered when the light curves of transiting planetary debris around a metal-polluted white dwarf such as WD 1145+017 (Hallakoun et al. 2017) is modeled.

The most complete set of limb-darkening coefficients for white dwarfs so far has been presented by Gianninas et al. (2013). These coefficients span a wide range of possible white dwarf parameters, but do not cover the very hot end of the distribution ($T_{\rm eff} > 40,000$ K). However, newly discovered systems such as ZTF J1539+5027 (Burdge et al. 2019a) contain one or more hot components that fall within this very hot range. Moreover, the small difference in the filter bandpasses between the Large Synoptic Survey Telescope (LSST) filters used in Gianninas et al. (2013) and the HiPERCAM filters also introduces small systemic errors and thus needs to be taken into account when work at high precision is conducted. Additionally, many of the most compact binary systems involving white dwarfs (e.g., ZTF J1539+5027 and SDSS J0651+2844; Brown et al. 2010, Hermes et al. 2012) are at such a short orbital period that one of the white dwarfs begins to exhibit tidal deformation. This leads to a periodic modulation of the light curve at twice the orbital frequency. This phenomenon strongly depends on the gravity-darkening coefficient and has never been systematically computed for white dwarfs, likely because until recently, no detached binary systems exhibited measurable tidal deformation.

The paper is organized as follows: Section 2 is dedicated to the description of the atmosphere models of white dwarfs we adopted here. Section 3 is devoted to the LDC calculations, while in Section 4 we present the calculations for the GDC and a brief description of the tables.

2. Description of the DA, DB, and DBA atmosphere models

For this study we computed three separate grids of 1D DA, DB, and DBA models. Calculations for helium-dominated atmospheres are motivated by the recent discovery of a DBA in a close binary system (Burdge et al. 2019b).

The DA grid spans the same surface gravities, $\log g$, as the DA grid of Gianninas et al. (2013): $5.0 \le \log g \le 9.5$. We extended the effective temperature range to $3750 \text{ K} \le T_{\text{eff}} \le 100\,000 \text{ K}$, however. Because DA white dwarfs have nearly pure hydrogen atmospheres, we used a helium-to-hydrogen ra-

tio, He/H, equal to 0. The atmosphere code described in Gianninas et al. (2013), Bergeron et al. (2011), and Tremblay & Bergeron (2009) was employed to calculate the DA models in local thermodynamic equilibrium (LTE). We refer to this code as the Montréal code in the rest of the paper. For $T_{\rm eff} \ge 40\,000$ K, we computed two subgrids of DA models with and without nonlocal thermodynamic equilibrium (NLTE) effects. This was done in order to test the NLTE effects on LDC and GDC. The LTE models computed above $T_{\rm eff} = 40\,000$ K were computed with the Montréal code, whereas the NLTE models were computed using TLUSTY (Hubeny & Lanz 1995). For all DA models we used ML2/ $\alpha = 0.8$ (Tremblay et al. 2010).

Our DB grid spans the same surface gravity range as the DA grid, but with different step sizes (see tables). The effective temperature range spanned by the grid is 11 000 K $\leq T_{\rm eff} \leq$ 40 000 K. For this grid we used the hydrogen abundance of log H/He = -10.0, effectively describing a helium-pure atmosphere. The DBA grid spans the same surface gravity and effective temperature range as for the DB models, but the hydrogen abundance was set to log H/He = -2.0 in the number of atoms. The majority of helium-dominated atmosphere white dwarfs do show traces of hydrogen, with typical log H/He values in the range of -4.0 to -5.0 (Bergeron et al. 2011). We used the large log H/He = -2.0 hydrogen on the LDC and GDC. For the DB and DBA models we used ML2/ α = 1.25 (Bergeron et al. 2011).

For each grid we calculated the spectral intensity as a function of both wavelength and μ , where $\mu = \cos \theta$ and θ is the angle between the line of sight and the outward surface normal. We used 20 μ values in all cases, unlike Gianinnas et al. (2013), who used 101 individual μ values. On the other hand, 3D convective effects have so far been neglected in the calculations of LDC and GDC coefficients for white dwarfs, but we are planning to apply our techniques to existing 3D DA ($T_{\rm eff} \leq 14,000$ K; Tremblay et al. 2013) and DB(A) (Cukanovaite et al. 2019) grids in a future paper, or upon request to the authors.

Limb-darkening coefficients for DA, DB, and DBA white dwarfs

The six LDC laws adopted here are written below. The coefficients are identified in the respective tables.

The linear law (Schwarzschild 1906, Russell 1912, Milne 1921)

$$\frac{I(\mu)}{I(1)} = 1 - u(1 - \mu),\tag{1}$$

the quadratic law (Kopal 1950)

$$\frac{I(\mu)}{I(1)} = 1 - a(1 - \mu) - b(1 - \mu)^2,$$
(2)

the square-root law (Díaz-Cordovés&Giménez 1992),

$$\frac{I(\mu)}{I(1)} = 1 - c(1 - \mu) - d(1 - \sqrt{\mu}),\tag{3}$$

the logarithmic law (Klinglesmith& Sobieski 1970)

$$\frac{I(\mu)}{I(1)} = 1 - e(1 - \mu) - f\mu \ln(\mu), \tag{4}$$

the power-2 law (Hestroffer 1997)

$$\frac{I(\mu)}{I(1)} = 1 - g(1 - \mu^h),\tag{5}$$

and a four-term law (Claret 2000a)

$$\frac{I(\mu)}{I(1)} = 1 - \sum_{k=1}^{4} a_k (1 - \mu^{\frac{k}{2}}), \tag{6}$$

where I(1) is the specific intensity at the center of the disk and u, a, b, c, d, e, f, g, h, and a_k are the corresponding LDCs. The specific intensities of the model atmosphere were convolved with the transmission curves for the Sloan (u'g'r'i'z'y'), UB-VRI, HiPERCAM, Kepler, TESS, and Gaia passbands. It is not straightforward to apply the least-squares method (LSM) to the original 20 μ points because they are not equally spaced. The original distribution can lead to very large weights for the μ s near the limb. To avoid this problem, the LDCs were computed for 100 interpolated (equally spaced) μ points instead of 20, as provided originally by the Montréal code described in Tremblay & Bergeron (2009) and Bergeron et al. (2011).

Two numerical methods for computing the LDC are available: LSM, and flux conservation (FCM). The advantages and disadvantages of each method are exhaustively discussed in Claret (2000a). Based on this discussion, we here adoped the LSM to adjust the coefficients of Eqs. 1-6. For each law, we computed the merit function, given by

$$\chi^2 = \sum_{i=1}^{N} (y_i - Y_i)^2, \qquad (7)$$

where y_i is the model intensity at point *i*, Y_i is the fitted function at the same point, and *N* is the number of μ points. We recall that the biparametric laws are only relatively accurate for some regions of the Hertzsprung-Russel (HR) diagram. Therefore, we recommend adopting Eq. 6 because it meets the following conditions: a) it uses a single law that is accurate for the whole HR diagram, b) it is capable of reproducing the intensity distribution very well, c) the flux is conserved within a very small tolerance, d) it is applicable to different filters as well as to monochromatic values, and e) it is applicable to different chemical compositions, effective temperatures, local gravities, and microturbulent velocities.

The biparametric laws (Eqs. 2-5) cannot reproduce the intensity distribution accurately along the HR diagram, although they do it better than the linear law. When these laws are able to represent the intensity distributions well, they are only marginally accurate in certain intervals of effective temperatures and/or log g (see Figs. 4 and 5). As a consequence, the user has to divide the HR diagram into areas of laws in order to use the LDC adequately (see below). Moreover, Eq. 6 provides merit functions of the order of 2 magnitudes smaller than any of the laws quoted previously, mainly in regions close to the limb, as we describe in the next paragraph.

Figs. 1 and 2 display the relative differences between the intensities from the model and those from the adjustments given by [I(model) - I(fit)]/I(model) as a function of μ for two cases: the four-term law (Fig. 1) and the power-2 law (Fig. 2). The two figures are on the same scale to facilitate comparison. The superiority of the four-term law over the power-2 law is clear and the relative differences provided by this approach may be of some orders of magnitude smaller than those corresponding to the power-2 law, mainly near the limb. When we compare the quality of the adjustments using Eq. 6 with those from the other biparametric laws, the quality of the adjustments provided in the first one is still even better than in the case of the power-2 law.

In order to avoid a biased interpretation of the quality of the adjustments illustrated in Figs. 1 and 2, we include in Figs. 3 and 4 the merit function for all DA models and all six Sloan passbands adopted in this study. A direct comparison between these two figures shows that the fit quality of the four-term law is always far higher than that of the power-2 law (almost 2 orders of magnitude). They are only similar in the interval 4.4-4.6 in log $T_{\rm eff}$, but even so, the four-term law is superior. In this interval the specific intensities behave more smoothly, which explains the similarity in the behavior of the merit function of these two laws.

For the biparametric laws alone, we illustrate in Fig. 5 the behavior of the square-root law for the same conditions as in Figs 3 and 4. The χ^2 provided by the power-2 law is similar to those given by the square-root law. The square-root law provides smaller χ^2 than the power-2 law for DB models, showing lower effective temperatures. When a biparametric law is to be adopted, we therefore recommend an inspection of the values of the merit function for each law, for each model, and for each passband to select the most accurate.

It has been known for a long time that the linear law does not adequately describe the distribution of specific intensities when realistic stellar atmosphere models are used. Despite this deficiency, this law can be used, for example, to compare models with different input physics. In Fig. 6 we compare the linear LDC for the DB, DA, and DBA models to analyze the effect of the hydrogen content on the distribution of specific intensities for a constant value of $\log g = 7.00$. The influence of hydrogen content on the slope is clear: DBA models have higher LDCs up to $T_{eff} \approx 20.000$ K, while the opposite occurs for higher effective temperatures. For the DA models, LDCs show an almost linear dependence on effective temperature. Only the DA and DBA models have similar LDCs for a narrow range of effective temperatures (10900 K-15500 K, and this is within the semiempirical errors). On the other hand, it is important to note that the global differences in the LDC for the three sets of models are larger or of the order than the typical semi-empirical errors that can be derived in the case of high-quality light curves. As a consequence, the three types of white dwarfs investigated here might be distinguishable observably using the appropriate LDCs.

As mentioned, the linear approximation is not very adequate, but on the other hand, it facilitates visualizing the differences between the LDCs that were computed from different model grids. A comparison of our results with the previous ones from Gianninas et al. (2013) is a good consistency check. In Fig. 7 we show this comparison for the *g* filter. The agreement between the two computations is very good, and the small differences may be due to the modifications that have recently been introduced in the code and numerical precision.

4. Calculating the gravity-darkening coefficients

As is well known, rotation and/or tides distort the shapes of stars. Such distortions have been investigated by Kopal (1959), who used spherical harmonics to describe them. The studies are in particular important in close binary systems or in planetary systems where both mechanisms act simultaneously: tides tend to elongate the star, while rotation tends to flatten it at the poles.



Fig. 1: Relative differences $\Delta \equiv [I \pmod{1} - I \pmod{1} / I \pmod{2}]$ as a function of μ for the Sloan passbands. Four-term law, log g = 5.5, $T_{\text{eff}} = 10000$ K, and DA models (LTE).

The corresponding deviations from a sphere are functions of the rotational rates and of the mass ratio q. A mathematical summary will help us understand the results obtained by Kopal. Consider the total potential of a rotating star. We assume that the angle between the normal and the radius vector is small and that only the radial component of the derivative is considered to compute the local gravity. Thus, we have

$$\frac{g-g_o}{g_o} = \sum_j \left(1 - \frac{5}{\Delta_j}\right) \left(\frac{r}{a} - 1\right),\tag{8}$$

where g_o is the local gravity (taken as reference), $\Delta_j = 1 + 2k_j$ and k_j is the apsidal motion constant of order *j*. For j = 2, the radius of an equipotential *r* can be written as

$$r = a \left(1 - f_2 P_2(\theta, \phi) \right), \tag{9}$$

where f_2 is given by

$$f_2 = \frac{5\omega^2 a^3}{3GM_{\psi}(2+\eta_2)}.$$
(10)

In the above equation ω is the angular velocity, $P_2(\theta, \phi)$ is the second surface harmonic, *a* is the mean radius of the level surface, η_2 is the logarithmic derivative of the spherical harmonic defined through Radau's equation, and M_{ψ} is the mass enclosed by an equipotential. The importance of Eq. 10 is that it establishes a dependence of the GDE on the shape of the distorted stellar configuration, on its internal structure, and also on the details of the rotation law. More details on these calculations have been presented by Claret (2000b).





Fig. 2: Relative differences $\Delta \equiv [I \pmod{1} - I \pmod{1} / I \pmod{2}]$ as a function of μ for the Sloan passbands. Power-2 law, log g = 5.5, $T_{\text{eff}} = 10\,000$ K, and DA models (LTE).



Fig. 3: Merit function χ^2 for all models of the sample. Four-term law, all Sloan passbands, and DA models (LTE).

From the physical point of view, more than the geometrical changes must be considered. von Zeipel (1924) showed that for configurations in pure radiative equilibrium (pseudo-barotrope), the emerging flux is not constant on the surface of a distorted star and depends on the value of the local gravity:



Fig. 4: Merit function χ^2 for all models of the sample. Power-2 law, all Sloan passbands, and DA models (LTE).



Fig. 5: Merit function χ^2 for all models of the sample. Square root-law, all Sloan passbands, and DA models (LTE).

$$F = -\frac{4acT^3}{3\kappa\rho} \frac{dT}{d\Phi} g^{\beta_1} \tag{11}$$

or

 $T_{\rm eff}^{4} \propto g^{\beta_1},\tag{12}$



Fig. 6: Linear LDC as a function of the effective temperature for the V passband. Asterisks denote DB models, DBAs (LTE) are represented by the continuous line, and the dashed line indicates DA models. Log g = 7.0.



Fig. 7: Comparison between our linear LDCs (continuous line) and those computed by Gianninas et al. (2013), which are denoted by asterisks. DA models, $\log g = 6.0$.

where g is the local gravity, Φ is the total potential, T is the local temperature, κ is the opacity, ρ is the local density, a is the radiation pressure constant, c the velocity of light in vacuum, T_{eff} is the effective temperature, and β_1 =1.0 is the GDE, a bolometric quantity.

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However, significant deviations from von Zeipel's theorem have been found when the GDEs are calculated at the upper layers of a distorted star (Claret 2012). This is a consequence of using a transfer equation that is more elaborate than the diffusion approach that was adopted by von Zeipel. This theorem is therefore not strictly valid at lower optical depths. For details on the calculations of β_1 , recent results and different methods, see for example, Claret (2012, 2016) and Zorec et al. (2017). The non-validity of von Zeipel's theorem also extends to compact stars. As previously commented in the Introduction, Claret (2015) used a perturbation theory and derived an equation for the GDE for neutron stars as a function of the rotation law, of the colatitude, and of the logarithmic derivatives of the opacity. This equation predicts significant deviations from the von Zeipel's theorem for differentially rotating neutron stars.

Concerning the passband gravity-darkening coefficients $y(\lambda)$ (GDC), Kopal (1959) assumed a simple but ingenious approach six decades ago in the absence of reliable atmosphere models: the distorted configurations radiate like a blackbody. By expanding the ratio between the monochromatic and total radiation in a Taylor series, he derived the GDC as a function of the temperature (effective) and of the wavelength. Of course, the blackbody radiation is not a good approximation, and more elaborate atmosphere models are needed to permit a consistent light-curve analysis. Later, Martynov (1973) refined the calculation of the GDC introducing the following equation:

$$y(\lambda, T_{\text{eff}}, \log[H/He], \log g) = \frac{1}{4} \left(\frac{\partial \ln I_o(\lambda)}{\partial \ln T_{\text{eff}}} \right)_g,$$
(13)

where λ is the wavelength, log [H/He] is the content of hydrogen relative to the content of helium, $I_o(\lambda)$ is the specific intensity at a given wavelength at the center of the stellar disk, and the subscript g indicates a derivative at constant surface gravity. At that time and for many years, the blackbody approach was used to calculate the partial derivative. We also note that Eq. 13 also presents some simplifications. The factor 1/4 indicates that in its derivation, β_1 was assumed to be 1.0 for any effective temperature. However, as we previously commented, β_1 is a function of the physical conditions in the upper layers and can be different from 1.0, mainly for stars presenting convective envelopes (see below).

Claret & Bloemen (2011) considered the effects of the partial derivative $(\partial \ln I_o(\lambda)/\partial \ln g)_{T_{\text{eff}}}$ and of more realistic stellar atmosphere models (PHOENIX and ATLAS) in calculating the GDC,

$$y(\lambda, T_{\text{eff}}, \log[H/He], \log g,) = \left(\frac{d \ln T_{\text{eff}}}{d \ln g}\right) \left(\frac{\partial \ln I_o(\lambda)}{\partial \ln T_{\text{eff}}}\right)_g + \left(\frac{\partial \ln I_o(\lambda)}{\partial \ln g}\right)_{T_{\text{eff}}}.$$
(14)

Following the arguments presented above, the term $\left(\frac{d \ln T_{\text{eff}}}{d \ln g}\right)$ can be written as $\beta_1/4$, and finally we have

$$y(\lambda, T_{\rm eff}, \log[H/He], \log g) = \left(\frac{\beta_1}{4}\right) \left(\frac{\partial \ln I_o(\lambda)}{\partial \ln T_{\rm eff}}\right)_g + \left(\frac{\partial \ln I_o(\lambda)}{\partial \ln g}\right)_{T_{\rm eff}}.$$
(15)

We used the same DA, DB, and DBA models as described in Section 2 to compute the GDC for all passbands considered here. The corresponding GDC tables consist of two lines per model:





Fig. 8: Theoretical gravity-darkening coefficients for the SLOAN passbands (DB models). The continuous line represents the calculations for log g = 8.0, and asterisks denote the calculations by adopting the blackbody approach.

the first line refers to the first term of Eq. 15 considering $\beta_1 = 1.0$, and the second line refers to the second term of this equation. We chose to separate the two contributions so that the value of β_1 can be adjusted during the synthesis of the light curves. In this case, the first term only needs to be multiplied by the value of β_1 to be iterated.

Figures 8 and 9 (DB and DBA, respectively) show the comparison between the GDC given by Eq. 15 (continuous line) and those calculated using the blackbody approach (asterisks). As anticipated, the blackbody radiation is not a good approximation. This is particularly valid for passbands with short effective wavelengths. Similar effects have been detected in main-sequence and giant stars (see Fig. 4 in Claret 2003). The influence of the second term in the GDC in Eq. 15 is not important, but not negligible (see the second lines of the corresponding tables). We also detected a decrease in GDC for all Sloan passbands around 20000 K for the DB and DBA models. This feature might be connected to the onset of He II convection (Cukanovaite et al. 2019).

As explained in Sect. 2, we also computed DA NLTE models. GDC calculations can serve as an indicator (although not the definitive) of the effective temperature limit for which it is necessary to adopt NLTE. Fig. 10 shows the comparison between LTE (continuous line) and NLTE (asterisks) models. For all Sloan filters, this effective temperature limit is at about 40 000 K, in good agreement with previous estimates (Gianninas et al. 2013). This effective temperature is practically independent of local gravity. The systematic and small offsets that we show in Fig. 10 at lower effective temperatures are probably due to the use of different codes for LTE and NLTE. Therefore we can conclude that the effect of considering NLTE is practically negligible in GDC

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Fig. 9: Effects of hydrogen content on the GDC (DBA models). The captions are the same as for Fig. 8.

calculations. A discussion for the onset of NLTE effects can be found in Liebert, Bergeron, & Holberg (2005).

Because 1D convection is limited, the theoretical GDC (DA models) for $T_{\text{eff}} = 5000 \text{ K}$ show some discontinuities at the shortest wavelengths (passbands *u* and *U*). We have preferred to keep these discontinuities in the respective tables and leave the task of smoothing them to the user according to their needs.

Acknowledgements. We thank the anonymous referee for helpful comments that have improved the manuscript. The Spanish MEC (AYA2015-71718-R and ESP2017-87676-C5-2-R) is gratefully acknowledged for its support during the development of this work. A.C. also acknowledges financial support from the State Agency for Research of the Spanish MCIU through the "Center of Excellence Severo Ochoa" award for the Instituto de Astrofísica de Andalucía (SEV-2017-0709). The research leading to these results has received funding from the European Research Council under the European Union's Horizon 2020 research and innovation programme n. 677706 (WD3D). This research has made use of the SIMBAD database, operated at the CDS, Strasbourg, France, and of NASA's Astrophysics Data System Abstract Service.

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Fig. 10: Effects of NLTE on the GDC (DA models). The continuous line indicates LTE models, and asterisks denote NLTE models. Sloan passbands. Log g = 8.25.

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Appendix A: Brief description of tables A1, A2, and A3

In order to provide users with the complementary tools for the synthesis of light curves, we also computed the Doppler beaming for each photometric system. The Doppler beaming factors adopting the BB approach were computed according to Eq. 3 (parameter α) in Loeb&Gaudi (2003). Tables A1, A2, and A3 summarize the type of data available as well as the central intensities for each photometric system in ergs/cm²/s/Hz/ster, and the Doppler beaming for the BB approach. For more details, see the ReadMe file on the CDS.

Table	A.1: Gravity	and limb-dar	kening coeffici	ents for the	Sloan and U	JBVRI p	hotometric s	ystems
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Table 1 DB 10000 K 40000 K $5.5 \cdot 9.5$ 1000 $u^*gr^*r^*yr^*$ LSM/Eq. 1 Table 2 DB 10000 K 40000 K $5.5 \cdot 9.5$ 1000 $u^*gr^*r^*yr^*$ LSM/Eq. 4 Table 4 DB 10000 K 40000 K $5.5 \cdot 9.5$ 1000 $u^*gr^*r^*yr^*$ LSM/Eq. 6 Table 5 DB 10000 K 40000 K $5.5 \cdot 9.5$ 10.00 $u^*gr^*r^*yr^*$ LSM/Eq. 6 Table 6 DB 10000 K 40000 K $5.5 \cdot 9.5$ 10.00 $u^*gr^*r^*r^*yr^*$ $LSM/Eq. 7r^*r^*r^*r^*r^*r^*r^*r^*r^*r^*r^*r^*r^*r$	Name	Source	range T _{off}	range log g	log [H/He]	Filters	Fit/equation
Table 2DB10000 K $55.9.5$ 1000 $u^2g'r^1r^2y'$ LSM/Eq.3Table 3DB10000 K $55.9.5$ 100 $u^2g'r^1r^2y'$ LSM/Eq.3Table 4DB10000 K $55.9.5$ 100 $u^2g'r^1r^2y'$ LSM/Eq.4Table 5DB10000 K 40000 K $55.9.5$ 100 $u^2g'r^1r^2y'$ LSM/Eq.4Table 6DB10000 K 40000 K $55.9.5$ 100 $u^2g'r^1r^2y'$ LSM/Eq.6Table 7DB10000 K 40000 K $55.9.5$ 100 $u^2g'r^1r^2y'$ LSM/Eq.6Table 9DB10000 K 40000 K $55.9.5$ 100 UBVRILSM/Eq.4Table 10DB10000 K 40000 K $55.9.5$ 100 UBVRILSM/Eq.4Table 11DB10000 K 40000 K $55.9.5$ 100 UBVRILSM/Eq.4Table 12DB10000 K 40000 K $5.9.5$ 100 UBVRILSM/Eq.4Table 13DB10000 K 40000 K $7.0.9.0$ -2.0 $u^2g'r^1r^2y'$ LSM/Eq.4Table 16DBA11000 K 40000 K $7.0.9.0$ -2.0 $u^2g'r^1r^2y'$ LSM/Eq.4Table 18DBA11000 K 40000 K $7.0.9.0$ -2.0 $u^2g'r^1r^2y'$ LSM/Eq.4Table 20DBA11000 K 40000 K $7.0.9.0$ -2.0 $u^2g'r^1r^2y'$ LSM/Eq.4Table 21DBA11000 K 40000 K $7.0.9.0$ -2.0 $u^2g'r^1r^2y'$ <	Table1	DB	10000 K-40000 K	5.5-9.5	-10.0	$\frac{1}{u'g'r'i'z'v'}$	LSM/Eq. 1
Table3DB10000 K $5.5 \cdot 9.5$ -10.0 $u^*_B (r^*) r^*_S r^*_S$ LSM/Eq. 4Table4DB10000 K $5.5 \cdot 9.5$ -10.0 $u^*_B (r^*) r^*_S r^*_S$ LSM/Eq. 4Table5DB10000 K $5.5 \cdot 9.5$ -10.0 $u^*_B (r^*) r^*_S r^*_S$ LSM/Eq. 6Table6DB10000 K $40000 K$ $5.5 \cdot 9.5$ -10.0 $u^*_B (r^*) r^*_S r^*_S$ LSM/Eq. 6Table7DB10000 K $40000 K$ $5.5 \cdot 9.5$ -10.0 UBVRILSM/Eq. 2Table8DB10000 K $40000 K$ $5.5 \cdot 9.5$ -10.0 UBVRILSM/Eq. 2Table10DB10000 K $40000 K$ $5.5 \cdot 9.5$ -10.0 UBVRILSM/Eq. 4Table12DB10000 K $40000 K$ $5.5 \cdot 9.5$ -10.0 UBVRILSM/Eq. 6Table13DB10000 K $40000 K$ $5.5 \cdot 9.5$ -10.0 UBVRILSM/Eq. 6Table14DB10000 K $40000 K$ $5.5 \cdot 9.5$ -10.0 UBVRILSM/Eq. 6Table15DBA11000 K $40000 K$ $7.0 \cdot 9.0$ -2.0 $u^*_B (r^*_B r^*_S r^*_S)$ LSM/Eq. 6Table17DBA11000 K $40000 K$ $7.0 \cdot 9.0$ -2.0 $u^*_B r^*_B r^*_S r^*_S$ LSM/Eq. 6Table29DBA11000 K $40000 K$ $7.0 \cdot 9.0$ -2.0 $u^*_B r^*_B r^*_S r^*_S$ LSM/Eq. 6Table210DBA11000 K $40000 K$ $7.0 \cdot 9.0$ -2.0 $u^*_B r^*_B r^*_S r^*_S$ LSM/Eq. 6 <t< td=""><td>Table2</td><td>DB</td><td>10000 K-40000 K</td><td>5.5-9.5</td><td>-10.0</td><td>u'g'r'i'z'v'</td><td>LSM/Eq. 2</td></t<>	Table2	DB	10000 K-40000 K	5.5-9.5	-10.0	u'g'r'i'z'v'	LSM/Eq. 2
Table4DB10000 K40000 K5.5.9.510.0 $u^*g'r^*r^*y'$ LSM/Eq. 4Table5DB10000 K40000 K5.5.9.510.0 $u^*g'r^*r^*y'$ LSM/Eq. 4Table6DB10000 K40000 K5.5.9.510.0 $u^*g'r^*r^*y'$ LSM/Eq. 6Table7DB10000 K40000 K5.5.9.510.0UBVRILSM/Eq. 7Table9DB10000 K40000 K5.5.9.510.0UBVRILSM/Eq. 7Table10DB10000 K40000 K5.5.9.510.0UBVRILSM/Eq. 3Table11DB10000 K40000 K5.5.9.510.0UBVRILSM/Eq. 4Table12DB10000 K40000 K5.5.9.510.0UBVRILSM/Eq. 6Table13DB10000 K40000 K5.5.9.510.0UBVRILSM/Eq. 6Table14DB10000 K40000 K7.0.9.0-2.0 $u^*g'r^*r'x'$ LSM/Eq. 6Table15DBA11000 K40000 K7.0.9.0-2.0 $u^*g'r^*r'x'$ LSM/Eq. 4Table16DBA11000 K40000 K7.0.9.0-2.0 $u^*g'r^*r'x'$ LSM/Eq. 4Table21DBA11000 K40000 K7.0.9.0-2.0 $u^*g'r^*r'x'$ LSM/Eq. 4Table23DBA11000 K40000 K7.0.9.0-2.0U#g'r'r'x'LSM/Eq. 4Table23DBA11000 K40000 K7.0.9.0-2.0UBVRILSM/Eq. 4Table24DBA <td>Table3</td> <td>DB</td> <td>10000 K-40000 K</td> <td>5 5-9 5</td> <td>-10.0</td> <td>u'g'r'i'z'v'</td> <td>LSM/Eq. 2</td>	Table3	DB	10000 K-40000 K	5 5-9 5	-10.0	u'g'r'i'z'v'	LSM/Eq. 2
Table 5 DB 10000 K +0000 K 5.5.9.5 -10.0 $u^* g r^* i^* z y^*$ LSM/Eq. 5 Table 6 DB 10000 K +0000 K 5.5.9.5 -10.0 $u^* g r^* i^* z y^*$ GDC. $y(u^* g^* r^* z^* y^*)$ Table 8 DB 10000 K +0000 K 5.5.9.5 -10.0 UBVRI LSM/Eq. 4 Table 10 DB 10000 K +0000 K 5.5.9.5 -10.0 UBVRI LSM/Eq. 4 Table 10 DB 10000 K +0000 K 5.5.9.5 -10.0 UBVRI LSM/Eq. 4 Table 11 DB 10000 K +0000 K 5.5.9.5 -10.0 UBVRI LSM/Eq. 4 Table 13 DB 10000 K +0000 K 5.5.9.5 -10.0 UBVRI LSM/Eq. 4 Table 14 DB 10000 K +0000 K 7.0.9.0 -2.0 $u^* g r^* i^* z r^*$ LSM/Eq. 4 Table 15 DBA 11000 K +0000 K 7.0.9.0 -2.0 $u^* g r^* i^* z r^*$ LSM/Eq. 4 Table 17 DBA 11000 K +0000 K 7.0.9.0 -2.0 $u^* g r^* r^* z r^*$ LSM/Eq. 4 <td>Table4</td> <td>DB</td> <td>10000 K-40000 K</td> <td>5 5-9 5</td> <td>-10.0</td> <td>$u'\sigma'r'i'z'v'$</td> <td>LSM/Eq. 4</td>	Table4	DB	10000 K-40000 K	5 5-9 5	-10.0	$u'\sigma'r'i'z'v'$	LSM/Eq. 4
InduceDB10000 K10000 K5.5-9.51000 $u^2 g^* r^2 z^* y^* LSM_{Eq.4}^{-1}$ Table7DB10000 K40000 K5.5-9.5-10.0 $u^2 g^* r^2 z^* y^* LSM_{Eq.4}^{-1}$ Table9DB10000 K40000 K5.5-9.5-10.0UBVRILSM/Eq.3Table10DB10000 K40000 K5.5-9.5-10.0UBVRILSM/Eq.3Table11DB10000 K40000 K5.5-9.5-10.0UBVRILSM/Eq.3Table12DB10000 K40000 K5.5-9.5-10.0UBVRILSM/Eq.4Table13DB10000 K40000 K5.5-9.5-10.0UBVRILSM/Eq.4Table14DB10000 K40000 K7.0-9.0-2.0 $u^2 g^* r^* z^* y^* LSM/Eq.4$ Table15DBA11000 K40000 K7.0-9.0-2.0 $u^2 g^* r^* z^* y^* LSM/Eq.3$ Table16DBA11000 K40000 K7.0-9.0-2.0 $u^2 g^* r^* z^* y^* LSM/Eq.4$ Table20DBA11000 K40000 K7.0-9.0-2.0 $u^2 g^* r^* z^* y^* LSM/Eq.4$ Table21DBA11000 K40000 K7.0-9.0-2.0UBVRILSM/Eq.4Table22DBA11000 K40000 K7.0-9.0-2.0UBVRILSM/Eq.4Table23DBA11000 K40000 K7.0-9.0-2.0UBVRILSM/Eq.4Table24DBA11000 K40000 K7.0-9.0-2.0UBVRILSM/Eq.4Table25DBA11000 K </td <td>Table5</td> <td>DB</td> <td>10000 K-40000 K</td> <td>5 5-9 5</td> <td>-10.0</td> <td>u'g'r'i'z'y'</td> <td>LSM/Eq. 1</td>	Table5	DB	10000 K-40000 K	5 5-9 5	-10.0	u'g'r'i'z'y'	LSM/Eq. 1
HalleroDB10000 K10000 K5.2-9.510.00u g r1 2 yGDC (u g r' r 2 y')Table8DB10000 K40000 K5.5-9.5-10.0UBVRILSM/Eq. 1Table10DB10000 K40000 K5.5-9.5-10.0UBVRILSM/Eq. 2Table11DB10000 K40000 K5.5-9.5-10.0UBVRILSM/Eq. 4Table12DB10000 K40000 K5.5-9.5-10.0UBVRILSM/Eq. 6Table13DB10000 K40000 K5.5-9.5-10.0UBVRILSM/Eq. 6Table14DB10000 K40000 K7.0-9.0-2.0u g r' r' z' y'LSM/Eq. 6Table15DBA11000 K40000 K7.0-9.0-2.0u g r' r' z' y'LSM/Eq. 4Table18DBA11000 K40000 K7.0-9.0-2.0u g r' r' z' y'LSM/Eq. 4Table19DBA11000 K40000 K7.0-9.0-2.0u g r' r' z' y'LSM/Eq. 4Table20DBA11000 K40000 K7.0-9.0-2.0u g r' r' z' y'LSM/Eq. 4Table21DBA11000 K40000 K7.0-9.0-2.0U g r' r' z' y'LSM/Eq. 4Table22DBA11000 K40000 K7.0-9.0-2.0U g r' r' z' y'LSM/Eq. 4Table23DBA11000 K40000 K7.0-9.0-2.0UBVRILSM/Eq. 4Table24DBA11000 K40000 K7.0-9.0-2.0UBVRILSM/Eq. 4 <tr<< td=""><td>Table6</td><td>DB</td><td>10000 K 40000 K</td><td>5505</td><td>10.0</td><td>ugiiZy</td><td>LSM/Eq. 5</td></tr<<>	Table6	DB	10000 K 40000 K	5505	10.0	ugiiZy	LSM/Eq. 5
Table PDB10000 K5.2-9.5-10.0U g 11.2 yClub (M g 11.2 y)Table PDB10000 K4-0000 K5.5-9.5-10.0UBVRILSM/Eq. 1Table 10DB10000 K4-0000 K5.5-9.5-10.0UBVRILSM/Eq. 3Table 11DB10000 K4-0000 K5.5-9.5-10.0UBVRILSM/Eq. 4Table 12DB10000 K4-0000 K5.5-9.5-10.0UBVRILSM/Eq. 6Table 13DB10000 K4-0000 K5.5-9.5-10.0UBVRILSM/Eq. 6Table 14DB10000 K1000 K-0.9.0-2.0u g' ri'z' y'LSM/Eq. 6Table 15DBA11000 K4-0000 K7.0-9.0-2.0u g' ri'z' y'LSM/Eq. 4Table 16DBA11000 K4-0000 K7.0-9.0-2.0u' g' ri'z' y'LSM/Eq. 4Table 17DBA11000 K4-0000 K7.0-9.0-2.0u' g' ri'z' y'LSM/Eq. 4Table 20DBA11000 K4-0000 K7.0-9.0-2.0U g' ri'z' y'LSM/Eq. 4Table 23DBA11000 K4-0000 K7.0-9.0-2.0UBVRILSM/Eq. 4Table 24DBA11000 K4-0000 K7.0-9.0-2.0UBVRILSM/Eq. 4Table 25DBA11000 K4-0000 K7.0-9.0-2.0UBVRILSM/Eq. 4Table 26DBA11000 K4-0000 K7.0-9.0-2.0UBVRILSM/Eq. 4Table 27	Table7		10000 K-40000 K	5505	-10.0	u g f f z y	GDC v(u'a'r'i'z'v')
HallesDB10000 K10.0010.0010.00CBVRILSM/Eq. 2Table10DB10000 K40000 K5.5.9.5-10.0UBVRILSM/Eq. 3Table11DB10000 K5.5.9.5-10.0UBVRILSM/Eq. 4Table12DB10000 K5.5.9.5-10.0UBVRILSM/Eq. 6Table13DB10000 K5.5.9.5-10.0UBVRILSM/Eq. 6Table14DB10000 K40000 K5.5.9.5-10.0UBVRILSM/Eq. 4Table15DBA11000 K40000 K7.0.9.0-2.0u'g'ri'z'y'LSM/Eq. 2Table16DBA11000 K40000 K7.0.9.0-2.0u'g'ri'z'y'LSM/Eq. 4Table17DBA11000 K40000 K7.0.9.0-2.0u'g'ri'z'y'LSM/Eq. 4Table20DBA11000 K40000 K7.0.9.0-2.0u'g'ri'z'y'LSM/Eq. 5Table21DBA11000 K40000 K7.0.9.0-2.0U'g'ri'z'y'LSM/Eq. 4Table22DBA11000 K40000 K7.0.9.0-2.0UBVRILSM/Eq. 3Table23DBA11000 K40000 K7.0.9.0-2.0UBVRILSM/Eq. 3Table24DBA11000 K40000 K7.0.9.0-2.0UBVRILSM/Eq. 3Table25DBA11000 K40000 K7.0.9.0-2.0UBVRILSM/Eq. 5Table26DBA11000 K40000 K7.0.9.0-2.0UBVRI <td< td=""><td>Table?</td><td></td><td>10000 K-40000 K</td><td>5505</td><td>-10.0</td><td>UDVDI</td><td>$UDC y(u g r i \chi y)$</td></td<>	Table?		10000 K-40000 K	5505	-10.0	UDVDI	$UDC y(u g r i \chi y)$
HalleryDB10000 K10000 K10	Tableo		10000 K-40000 K	5.5-9.5	-10.0		LSM/Eq. 1
Table IIDB10000 K-40000 K5.5-9.5-10.0UBVRILSM/Eq. 4Table I2DB10000 K-40000 K5.5-9.5-10.0UBVRILSM/Eq. 5Table I3DB10000 K-40000 K5.5-9.5-10.0UBVRILSM/Eq. 6Table I4DB10000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq. 1Table I5DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq. 1Table I6DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq. 3Table I5DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq. 4Table I9DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq. 6Table I2DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq. 6Table I2DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 4Table I2DBA<	Table 9		10000 K-40000 K	5.5-9.5	-10.0		LSM/Eq. 2
Table 1DB10000 K-40000 K5.3-9.5-10.0UBVRILSM/Eq. 4Table 13DB10000 K-40000 K5.5-9.5-10.0UBVRILSM/Eq. 6Table 14DBDB10000 K-40000 K5.5-9.5-10.0UBVRIGDC $(UBVRI)$ Table 15DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq. 2Table 17DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq. 2Table 17DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq. 4Table 19DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq. 4Table 21DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq. 4Table 22DBA11000 K-40000 K7.0-9.0-2.0U'g'ri'z'y'DD'g'g'r'z'y'Table 23DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 1Table 23DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 3Table 24DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 4Table 25DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 4Table 26DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 6Table 27DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 6Table 29DA3750 K-60000 K5.0-9.50.0u'g'ri'z'y'LSM/Eq. 6Tabl			10000 K-40000 K	5.5-9.5	-10.0		LSM/Eq. 5
Iable12DB10000 K-40000 K5.3-9.5-10.0UBVRILSM/Eq. 3Table13DB10000 K-40000 K5.5-9.5-10.0UBVRIISM/Eq. 1Table16DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq. 1Table16DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq. 3Table17DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq. 3Table18DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq. 4Table20DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq. 5Table21DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'GDC yu'g'r'z'y'Table22DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 1Table23DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 4Table24DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 4Table25DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 6Table29DA3750 K-60000 K5.0-9.50.0u'g'ri'z'y'LSM/Eq. 6Table30DA3750 K-60000 K5.0-9.50.0u'g'ri'z'y'LSM/Eq. 1Table31DA3750 K-60000 K5.0-9.50.0u'g'ri'z'y'LSM/Eq. 4Table31DA3750 K-60000 K5.0-9.50.0u'g'ri'z'y'LSM/Eq. 4Table31DA			10000 K-40000 K	5.5-9.5	-10.0		LSM/Eq. 4
Table13DB10000 K40000 K5.5-9.5-10.0UBVRICDC y(UBVR)Table15DBA11000 K40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq.1Table16DBA11000 K40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq.2Table17DBA11000 K40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq.3Table19DBA11000 K40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq.4Table20DBA11000 K40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq.6Table21DBA11000 K40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq.6Table22DBA11000 K<40000 K			10000 K-40000 K	5.5-9.5	-10.0		LSM/Eq. 5
Table 1DB1000 K-40000 K5.9-9.3-10.0UBVRIGDC y(UBVR)Table 16DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq.1Table 17DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq.3Table 18DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq.4Table 19DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'LSM/Eq.4Table 20DBA11000 K-40000 K7.0-9.0-2.0u'g'ri'z'y'GDC y(u'g'r'tz'y')Table 21DBA11000 K-40000 K7.0-9.0-2.0U'g'ri'z'y'GDC y(u'g'r'tz'y')Table 22DBA11000 K-40000 K7.0-9.0-2.0U'g'ri'z'y'GDC y(u'g'r'tz'y')Table 23DBA11000 K-40000 K7.0-9.0-2.0U'g'ri'z'y'LSM/Eq.4Table 24DBA11000 K-40000 K7.0-9.0-2.0U'g'ri'z'y'LSM/Eq.4Table 25DBA11000 K-40000 K7.0-9.0-2.0U'g'ri'z'y'LSM/Eq.4Table 28DBA11000 K-40000 K7.0-9.0-2.0U'g'ri'z'y'LSM/Eq.5Table 29DA3750 K-60000 K5.0-9.50.0u'g'ri'z'y'LSM/Eq.4Table 23DA3750 K-60000 K5.0-9.50.0u'g'ri'z'y'LSM/Eq.4Table 23DA3750 K-60000 K5.0-9.50.0u'g'ri'z'y'LSM/Eq.4Table 30DA3750 K-60000 K5.0-9.50.0u'g'ri'z'y' <td></td> <td>DB</td> <td>10000 K-40000 K</td> <td>5.5-9.5</td> <td>-10.0</td> <td>UBVRI</td> <td>LSM/Eq. 0</td>		DB	10000 K-40000 K	5.5-9.5	-10.0	UBVRI	LSM/Eq. 0
Table15DBA11000 K-40000 K7.0-9.0-2.0u g ri z yLSM/Eq. 2Table16DBA11000 K-40000 K7.0-9.0-2.0u g ri z yLSM/Eq. 2Table18DBA11000 K-40000 K7.0-9.0-2.0u g ri z yLSM/Eq. 4Table19DBA11000 K-40000 K7.0-9.0-2.0u g ri z yLSM/Eq. 4Table20DBA11000 K-40000 K7.0-9.0-2.0u g ri z yLSM/Eq. 5Table21DBA11000 K-40000 K7.0-9.0-2.0u g ri z yLSM/Eq. 6Table22DBA11000 K-40000 K7.0-9.0-2.0U g ri z yLSM/Eq. 1Table23DBA11000 K-40000 K7.0-9.0-2.0U BVRILSM/Eq. 3Table24DBA11000 K-40000 K7.0-9.0-2.0U BVRILSM/Eq. 4Table25DBA11000 K-40000 K7.0-9.0-2.0U BVRILSM/Eq. 5Table26DBA11000 K-40000 K7.0-9.0-2.0U BVRILSM/Eq. 6Table27DBA11000 K-40000 K5.0-9.50.0u g ri z y'LSM/Eq. 6Table28DA3750 K-60000 K5.0-9.50.0u g ri z y'LSM/Eq. 4Table30DA3750 K-60000 K5.0-9.50.0u g ri z y'LSM/Eq. 4Table33DA3750 K-60000 K5.0-9.50.0u g ri z y'LSM/Eq. 6Table33DA3750 K-60000 K5.0-9.50.0U g ri z y'LSM/Eq. 6Table39DA <td></td> <td>DB</td> <td>10000 K-40000 K</td> <td>5.5-9.5</td> <td>-10.0</td> <td>UBVRI</td> <td>GDC y(UBVRI)</td>		DB	10000 K-40000 K	5.5-9.5	-10.0	UBVRI	GDC y(UBVRI)
Table 10DBA11000 K-40000 K7.0-9.0-2.0u g r i z yLSM/Eq. 3Table 18DBA11000 K-40000 K7.0-9.0-2.0u g r i z yLSM/Eq. 4Table 19DBA11000 K-40000 K7.0-9.0-2.0u g r i z yLSM/Eq. 5Table 20DBA11000 K-40000 K7.0-9.0-2.0u g r i z yLSM/Eq. 6Table 21DBA11000 K-40000 K7.0-9.0-2.0u g r i z yLSM/Eq. 6Table 22DBA11000 K-40000 K7.0-9.0-2.0U g r i z yLSM/Eq. 2Table 23DBA11000 K-40000 K7.0-9.0-2.0U B V RILSM/Eq. 2Table 24DBA11000 K-40000 K7.0-9.0-2.0U B V RILSM/Eq. 4Table 25DBA11000 K-40000 K7.0-9.0-2.0U B V RILSM/Eq. 4Table 26DBA11000 K-40000 K7.0-9.0-2.0U B V RILSM/Eq. 4Table 27DBA11000 K-40000 K7.0-9.0-2.0U B V RILSM/Eq. 4Table 28DA3750 K 60000 K5.0-9.50.0u g r i z ' y'LSM/Eq. 4Table 29DA3750 K 60000 K5.0-9.50.0u g r i z ' y'LSM/Eq. 5 </td <td>Table 15</td> <td>DBA</td> <td>11000 K-40000 K</td> <td>7.0-9.0</td> <td>-2.0</td> <td>ugrizy</td> <td>LSM/Eq. 1</td>	Table 15	DBA	11000 K-40000 K	7.0-9.0	-2.0	ugrizy	LSM/Eq. 1
Table IDBA11000 K-40000 K7.0-9.0-2.0u g'r'i'z'y'LSM/Eq.3Table IDBA11000 K-40000 K7.0-9.0-2.0u'g'r'i'z'y'LSM/Eq.4Table IDBA11000 K-40000 K7.0-9.0-2.0u'g'r'i'z'y'LSM/Eq.6Table IDBA11000 K-40000 K7.0-9.0-2.0u'g'r'i'z'y'GDC yu'g'r'z'y'Table IDBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.1Table IDBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.3Table IDBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.3Table IDBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.4Table IDA3750 K-60000 K5.0-9.50.0u'g'r'iz'y'LSM/Eq.4Table IDA3750 K-60000 K5.0-9.50.0u'g'r'iz'y'LSM/Eq.4Table IDA3750 K-60000 K5.0-9.50.0u'g'r'iz'y'LSM/Eq.4Table IDA3750 K-60000 K5.0-9.50.0u'g'r'iz'y'LSM/Eq.4Table IDA3750 K-60000 K	Table 16	DBA	11000 K-40000 K	7.0-9.0	-2.0	ugrizy	LSM/Eq. 2
Table18DBA11000 K-40000 K7.0-9.0-2.0u g'r'iz'y'LSM/Eq.4Table20DBA11000 K-40000 K7.0-9.0-2.0u'g'r'iz'y'LSM/Eq.5Table21DBA11000 K-40000 K7.0-9.0-2.0u'g'r'iz'y'GDC (u'g'r'tz'y'Table22DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.1Table23DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.2Table24DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.4Table25DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.4Table26DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.4Table27DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.4Table28DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.4Table30DA3750 K-60000 K5.0-9.50.0u'g'r'iz'y'LSM/Eq.4Table32DA3750 K-60000 K5.0-9.50.0u'g'r'iz'y'LSM/Eq.4Table33DA3750 K-60000 K5.0-9.50.0u'g'r'iz'y'LSM/Eq.4Table33DA3750 K-60000 K5.0-9.50.0u'g'r'iz'y'LSM/Eq.4Table34DA3750 K-60000 K5.0-9.50.0u'g'r'iz'y'LSM/Eq.4Table35DA3750 K-60000 K5.0-9.50.0U'g'r'iz'y'LSM/Eq.4Table33DA3750 K-60000 K <td< td=""><td>Table1 /</td><td>DBA</td><td>11000 K-40000 K</td><td>7.0-9.0</td><td>-2.0</td><td>ugrizy</td><td>LSM/Eq. 3</td></td<>	Table1 /	DBA	11000 K-40000 K	7.0-9.0	-2.0	ugrizy	LSM/Eq. 3
Table19DBA11000 K-40000 K7.0-9.0-2.0u g'r'i'z'y'LSM/Eq. 5Table21DBA11000 K-40000 K7.0-9.0-2.0u'g'r'iz'y'GDC y(u'g'r'i'z'y')Table22DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 1Table23DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 2Table24DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 2Table25DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 3Table26DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 4Table27DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 5Table29DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 1Table30DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 2Table31DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 4Table33DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 4Table34DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 6Table35DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 6Table33DA3750 K-60000 K5.0-9.50.0U'g'r'i'z'y'LSM/Eq. 6Table34DA3750 K-60000 K5.0-9.50.0U'g'r'i'z'y'LSM/Eq. 4Table35DA <td>Table 18</td> <td>DBA</td> <td>11000 K-40000 K</td> <td>7.0-9.0</td> <td>-2.0</td> <td>ugrizy</td> <td>LSM/Eq. 4</td>	Table 18	DBA	11000 K-40000 K	7.0-9.0	-2.0	ugrizy	LSM/Eq. 4
Table20DBA11000K-40000 K7.0-9.0-2.0u'g'r'i'z'y'LSM/Eq.6Table21DBA11000K-40000 K7.0-9.0-2.0UBVRILSM/Eq.1Table23DBA11000K-40000 K7.0-9.0-2.0UBVRILSM/Eq.2Table24DBA11000K-40000 K7.0-9.0-2.0UBVRILSM/Eq.2Table25DBA11000K-40000 K7.0-9.0-2.0UBVRILSM/Eq.4Table26DBA11000K-40000 K7.0-9.0-2.0UBVRILSM/Eq.4Table27DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.6Table28DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.6Table29DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq.1Table30DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq.2Table31DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq.4Table33DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq.5Table34DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq.1Table35DA3750 K-60000 K5.0-9.50.0U'g'r'i'z'y'LSM/Eq.4Table37DA3750 K-60000 K5.0-9.50.0U'g'r'i'z'y'LSM/Eq.4Table35DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq.4Table30<	Table 19	DBA	11000 K-40000 K	7.0-9.0	-2.0	uˈɡˈrˈıˈzˈy	LSM/Eq. 5
Table21DBA11000K-40000 K7.0-9.0-2.0 $Ugr'r'z'y'$ GDC $y(u'gr'r'z'y')$ Table23DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.1Table24DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.3Table25DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.4Table26DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.4Table27DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.6Table28DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.4Table29DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq.1Table30DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq.3Table31DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq.4Table33DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq.4Table34DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq.4Table35DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'GDC $y(u'g'r'i'z'y')$ Table36DA3750 K-60000 K5.0-9.50.0U'g'r'i'z'y'GDC $y(u'g'r'i'z'y')$ Table37DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq.4Table38DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq.4Table39DA	Table20	DBA	11000 K-40000 K	7.0-9.0	-2.0	u'g'r'i'z'y'	LSM/Eq. 6
Table22DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 1Table23DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 2Table25DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 3Table26DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 6Table27DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 6Table28DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 6Table29DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 2Table30DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 2Table31DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 4Table32DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 4Table33DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 4Table35DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 4Table36DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 2Table37DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table37DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table39DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 5Table39DA3750 K-60000 K5.0-9.5 <td< td=""><td>Table21</td><td>DBA</td><td>11000 K-40000 K</td><td>7.0-9.0</td><td>-2.0</td><td>u'g'r'i'z'y'</td><td>GDC $y(u'g'r'i'z'y')$</td></td<>	Table21	DBA	11000 K-40000 K	7.0-9.0	-2.0	u'g'r'i'z'y'	GDC $y(u'g'r'i'z'y')$
Table23DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 2Table24DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 3Table25DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 4Table26DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 4Table27DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 6Table28DBA11000 K-40000 K7.0-9.0-2.0UBVRICD(UBVRI)Table30DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 1Table31DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 3Table32DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 4Table33DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 4Table34DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 6Table35DA3750 K-60000 K5.0-9.50.0u'g'r'iz'y'LSM/Eq. 1Table36DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table37DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table39DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table39DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table40DA3750 K-60000 K5.0-9.5	Table22	DBA	11000 K-40000 K	7.0-9.0	-2.0	UBVRI	LSM/Eq. 1
Table24DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 3Table25DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 4Table26DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 5Table27DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 6Table28DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 6Table30DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 2Table31DA3750 K-60000 K5.0-9.50.0u'g'r'iz'y'LSM/Eq. 3Table32DA3750 K-60000 K5.0-9.50.0u'g'r'iz'y'LSM/Eq. 4Table33DA3750 K-60000 K5.0-9.50.0u'g'r'iz'y'LSM/Eq. 6Table34DA3750 K-60000 K5.0-9.50.0u'g'r'iz'y'LSM/Eq. 6Table35DA3750 K-60000 K5.0-9.50.0u'g'r'iz'y'LSM/Eq. 2Table36DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 2Table37DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 3Table39DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table37DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 6Table38DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 6Table43DA-NLTE40000 K-100000 K6.0-9.5	Table23	DBA	11000 K-40000 K	7.0-9.0	-2.0	UBVRI	LSM/Eq. 2
Table25DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 4Table26DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 6Table27DBA11000 K-40000 K7.0-9.0-2.0UBVRIGDC $y(UBVRI)$ Table29DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 1Table30DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 2Table31DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 3Table32DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 4Table33DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 6Table34DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 6Table35DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'GDC $y(u'g'r'i'z'y')$ Table36DA3750 K-60000 K5.0-9.50.0U'g'r'i'z'y'GDC $y(u'g'r'i'z'y')$ Table37DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table38DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table39DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table39DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table40DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table43DA-NLTE <td< td=""><td>Table24</td><td>DBA</td><td>11000 K-40000 K</td><td>7.0-9.0</td><td>-2.0</td><td>UBVRI</td><td>LSM/Eq. 3</td></td<>	Table24	DBA	11000 K-40000 K	7.0-9.0	-2.0	UBVRI	LSM/Eq. 3
Table26DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 5Table27DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq. 6Table28DBA11000 K-40000 K7.0-9.0-2.0UBVRIGDC y(UBVRI)Table30DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 1Table31DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 3Table32DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 4Table33DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 4Table34DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 6Table35DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 6Table36DA3750 K-60000 K5.0-9.50.0U'g'r'i'z'y'LSM/Eq. 1Table36DA3750 K-60000 K5.0-9.50.0U'g'r'i'z'y'LSM/Eq. 4Table37DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table38DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table39DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table40DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table41DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 6Table43DA-NLTE40000 K-100000 K	Table25	DBA	11000 K-40000 K	7.0-9.0	-2.0	UBVRI	LSM/Eq. 4
Table27DBA11000 K-40000 K7.0-9.0-2.0UBVRILSM/Eq.6Table28DBA11000 K-40000 K7.0-9.0-2.0UBVRIGDC $y(UBVRI)$ Table29DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq.1Table30DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq.2Table31DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq.3Table32DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq.4Table33DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq.6Table34DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq.6Table35DA3750 K-60000 K5.0-9.50.0U'g'r'i'z'y'GDC $y(u'g'r'z'y')'$ Table37DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq.2Table37DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq.3Table38DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq.3Table39DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq.5Table40DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq.6Table41DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq.4Table42DA-NLTE40000 K-100000 K6.0-9.50.0u'g'r'i'z'y'LSM/Eq.6Table43DA-NLTE40000 K-100000 K<	Table26	DBA	11000 K-40000 K	7.0-9.0	-2.0	UBVRI	LSM/Eq. 5
Table28DBA11000 K-40000 K7.0-9.0-2.0UBVRIGDC $y(UBVRI)$ Table29DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 1Table30DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 2Table31DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 3Table32DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 4Table33DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 4Table35DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'LSM/Eq. 6Table35DA3750 K-60000 K5.0-9.50.0u'g'r'i'z'y'GDC $y(u'g'r'i'z'y')$ Table36DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 1Table37DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 3Table39DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table40DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 6Table41DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table42DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table43DA-NLTE40000 K-100000 K6.0-9.50.0u'g'r'i'z'y'LSM/Eq. 6Table44DA-NLTE40000 K-100000 K6.0-9.50.0u'g'r'i'z'y'LSM/Eq. 4Table45DA-NLTE	Table27	DBA	11000 K-40000 K	7.0-9.0	-2.0	UBVRI	LSM/Eq. 6
Table29DA3750 K-60000 K5.0-9.50.0 $u^*g'r^{i'}z'y'$ LSM/Eq. 1Table30DA3750 K-60000 K5.0-9.50.0 $u^*g'r^{i'}z'y'$ LSM/Eq. 2Table31DA3750 K-60000 K5.0-9.50.0 $u^*g'r^{i'}z'y'$ LSM/Eq. 3Table32DA3750 K-60000 K5.0-9.50.0 $u^*g'r^{i'}z'y'$ LSM/Eq. 4Table33DA3750 K-60000 K5.0-9.50.0 $u^*g'r^{i'}z'y'$ LSM/Eq. 6Table34DA3750 K-60000 K5.0-9.50.0 $u^*g'r^{i'}z'y'$ LSM/Eq. 6Table35DA3750 K-60000 K5.0-9.50.0 $u^*g'r^{i'}z'y'$ LSM/Eq. 6Table36DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 1Table37DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 2Table38DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table39DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table40DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table41DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table42DA3750 K-60000 K5.0-9.50.0UBVRILSM/Eq. 4Table43DA-NLTE40000 K-100000 K6.0-9.50.0 $u^*g'r^{i'}z'y'$ LSM/Eq. 4Table44DA-NLTE40000 K-100000 K6.0-9.50.0 $u^*g'r^{i'}z'y'$ LSM/Eq. 3Tab	Table28	DBA	11000 K-40000 K	7.0-9.0	-2.0	UBVRI	GDC y(UBVRI)
Table30DA3750 K-60000 K $5.0-9.5$ 0.0 $u^*g'r^{+}i'z'y'$ LSM/Eq. 2Table31DA3750 K-60000 K $5.0-9.5$ 0.0 $u^*g'r^{+}i'z'y'$ LSM/Eq. 4Table32DA3750 K-60000 K $5.0-9.5$ 0.0 $u^*g'r^{+}i'z'y'$ LSM/Eq. 4Table33DA3750 K-60000 K $5.0-9.5$ 0.0 $u^*g'r^{+}i'z'y'$ LSM/Eq. 4Table34DA3750 K-60000 K $5.0-9.5$ 0.0 $u^*g'r^{+}i'z'y'$ LSM/Eq. 6Table35DA3750 K-60000 K $5.0-9.5$ 0.0 $u^*g'r^{+}i'z'y'$ LSM/Eq. 6Table36DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 1Table37DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 2Table38DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 4Table39DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 4Table40DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table41DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table42DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table43DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $u^*gr'i^*z'y'$ LSM/Eq. 1Table43DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $u^*gr'i^*z'y'$ LSM/Eq. 3Table45DA-NLTE40000 K-100000 K $6.0-9.5$ <	Table29	DA	3750 K-60000 K	5.0-9.5	0.0	u'g'r'i'z'y'	LSM/Eq. 1
Table31DA 3750 K-60000 K $5.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 3Table32DA 3750 K-60000 K $5.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 4Table33DA 3750 K-60000 K $5.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 4Table34DA 3750 K-60000 K $5.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 6Table35DA 3750 K-60000 K $5.0-9.5$ 0.0 $u'g'r'i'z'y'$ GDC $y(u'g'r'i'z'y')'$ Table36DA 3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 1Table37DA 3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 2Table38DA 3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 4Table39DA 3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 4Table40DA 3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 5Table41DA 3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table43DA-NLTE 40000 K-10000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table43DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 1Table43DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'iz'y'$ LSM/Eq. 2Table44DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'iz'y'$ LSM/Eq. 5 </td <td>Table30</td> <td>DA</td> <td>3750 K-60000 K</td> <td>5.0-9.5</td> <td>0.0</td> <td>u'g'r'i'z'y'</td> <td>LSM/Eq. 2</td>	Table30	DA	3750 K-60000 K	5.0-9.5	0.0	u'g'r'i'z'y'	LSM/Eq. 2
Table32DA3750 K-60000 K $5.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 4Table33DA3750 K-60000 K $5.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 6Table34DA3750 K-60000 K $5.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 6Table35DA3750 K-60000 K $5.0-9.5$ 0.0 $u'g'r'iz'y'$ LSM/Eq. 6Table36DA3750 K-60000 K $5.0-9.5$ 0.0 $u'g'r'iz'y'$ LSM/Eq. 1Table37DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 1Table38DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 3Table39DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 4Table40DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table41DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table41DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table42DA3750 K-60000 K $5.0-9.5$ 0.0 $u'g'r'iz'y'$ LSM/Eq. 1Table43DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'iz'y'$ LSM/Eq. 1Table44DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'iz'y'$ LSM/Eq. 4Table45DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'iz'y'$ LSM/Eq. 6Table47DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 <td< td=""><td>Table31</td><td>DA</td><td>3750 K-60000 K</td><td>5.0-9.5</td><td>0.0</td><td>u'g'r'i'z'y'</td><td>LSM/Eq. 3</td></td<>	Table31	DA	3750 K-60000 K	5.0-9.5	0.0	u'g'r'i'z'y'	LSM/Eq. 3
Table33DA3750 K-60000 K $5.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 5Table34DA3750 K-60000 K $5.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 6Table35DA3750 K-60000 K $5.0-9.5$ 0.0 $u'g'r'i'z'y'$ GDC $y(u'g'r'i'z'y')$ Table36DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 1Table37DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 2Table38DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 3Table39DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 4Table40DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 4Table41DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table41DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table42DA3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table43DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'iz'y'$ LSM/Eq. 1Table43DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'iz'y'$ LSM/Eq. 4Table44DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'iz'y'$ LSM/Eq. 4Table45DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'iz'y'$ LSM/Eq. 5Table46DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0	Table32	DA	3750 K-60000 K	5.0-9.5	0.0	u'g'r'i'z'y'	LSM/Eq. 4
Table34DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 6$ Table35DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 $u'g'r'i'z'y'$ $GDC y(u'g'r'i'z'y')$ Table36DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 1$ Table37DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 2$ Table38DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 3$ Table39DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 4$ Table40DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 4$ Table41DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 4$ Table42DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 4$ Table43DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 1$ Table43DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 2$ Table45DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 4$ Table46DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 4$ Table47DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 5$ Table48D	Table33	DA	3750 K-60000 K	5.0-9.5	0.0	u'g'r'i'z'y'	LSM/Eq. 5
Table35DA 3750 K-60000 K $5.0-9.5$ 0.0 $u'g'r'i'z'y'$ GDC $y(u'g'r'i'z'y')$ Table36DA 3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 1Table37DA 3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 2Table38DA 3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 3Table39DA 3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 4Table40DA 3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table41DA 3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table42DA 3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table43DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 1Table43DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 2Table44DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 3Table45DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 4Table46DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 4Table47DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'iz'y'$ LSM/Eq. 6Table50DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 UBVRI <t< td=""><td>Table34</td><td>DA</td><td>3750 K-60000 K</td><td>5.0-9.5</td><td>0.0</td><td>u'g'r'i'z'y'</td><td>LSM/Eq. 6</td></t<>	Table34	DA	3750 K-60000 K	5.0-9.5	0.0	u'g'r'i'z'y'	LSM/Eq. 6
Table36DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 1Table37DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 2Table38DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 3Table39DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 4Table40DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 5Table41DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table42DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table43DA-NLTE40000 \text{ K}-100000 \text{ K} $6.0-9.5$ 0.0 $u^*gritzy'$ LSM/Eq. 1Table44DA-NLTE40000 \text{ K}-100000 \text{ K} $6.0-9.5$ 0.0 $u^*gritzy'$ LSM/Eq. 4Table45DA-NLTE40000 \text{ K}-100000 \text{ K} $6.0-9.5$ 0.0 $u^*gritzy'$ LSM/Eq. 3Table46DA-NLTE40000 \text{ K}-100000 \text{ K} $6.0-9.5$ 0.0 $u^*gritzy'$ LSM/Eq. 4Table47DA-NLTE40000 \text{ K}-100000 \text{ K} $6.0-9.5$ 0.0 $u^*gritzy'$ LSM/Eq. 6Table48DA-NLTE40000 \text{ K}-100000 \text{ K} $6.0-9.5$ 0.0 $u^*gritzy'$ LSM/Eq. 6Table49DA-NLTE40000 \text{ K}-100000 \text{ K} $6.0-9.5$ 0.0 $u^*gritzy'$ CDC $y(u'g'r'tzy')$ Table50DA-NLTE40000 \text{ K}-100000 \text{ K}	Table35	DA	3750 K-60000 K	5.0-9.5	0.0	u'g'r'i'z'y'	GDC $y(u'g'r'i'z'y')$
Table37DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 2Table38DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 3Table39DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 4Table40DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 4Table41DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table42DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table43DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $5.0-9.5$ 0.0 $ug'r'i'z'y'$ LSM/Eq. 1Table43DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 2Table45DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'iz'y'$ LSM/Eq. 4Table45DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'iz'y'$ LSM/Eq. 4Table46DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'iz'y'$ LSM/Eq. 4Table47DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'iz'y'$ LSM/Eq. 6Table48DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'iz'y'$ LSM/Eq. 6Table50DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 UBVRILSM/Eq. 3Table51DA-NLTE $40000 \text{ K}-100000 $	Table36	DA	3750 K-60000 K	5.0-9.5	0.0	UBVRI	LSM/Eq. 1
Table38DA $3750 \text{ K-}60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 3Table39DA $3750 \text{ K-}60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 4Table40DA $3750 \text{ K-}60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table41DA $3750 \text{ K-}60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table42DA $3750 \text{ K-}60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table43DA-NLTE $40000 \text{ K-}100000 \text{ K}$ $6.0-9.5$ 0.0 $u^3 \text{ g}^* \text{ i}^* \text{ z}^* \text{ y}^*$ LSM/Eq. 1Table44DA-NLTE $40000 \text{ K-}100000 \text{ K}$ $6.0-9.5$ 0.0 $u^3 \text{ g}^* \text{ i}^* \text{ z}^* \text{ y}^*$ LSM/Eq. 2Table45DA-NLTE $40000 \text{ K-}100000 \text{ K}$ $6.0-9.5$ 0.0 $u^3 \text{ g}^* \text{ i}^* \text{ z}^* \text{ y}^*$ LSM/Eq. 4Table46DA-NLTE $40000 \text{ K-}100000 \text{ K}$ $6.0-9.5$ 0.0 $u^3 \text{ g}^* \text{ i}^* \text{ z}^* \text{ y}^*$ LSM/Eq. 4Table47DA-NLTE $40000 \text{ K-}100000 \text{ K}$ $6.0-9.5$ 0.0 $u^3 \text{ g}^* \text{ i}^* \text{ z}^* \text{ y}^*$ LSM/Eq. 5Table48DA-NLTE $40000 \text{ K-}100000 \text{ K}$ $6.0-9.5$ 0.0 $u^3 \text{ g}^* \text{ i}^* \text{ z}^* \text{ y}^*$ LSM/Eq. 6Table50DA-NLTE $40000 \text{ K-}100000 \text{ K}$ $6.0-9.5$ 0.0 $u^3 \text{ g}^* \text{ i}^* \text{ z}^* \text{ y}^*$ LSM/Eq. 1Table51DA-NLTE $40000 \text{ K-}100000 \text{ K}$ $6.0-9.5$ 0.0 UBVRILSM/Eq. 3Table53DA-N	Table37	DA	3750 K-60000 K	5.0-9.5	0.0	UBVRI	LSM/Eq. 2
Table39DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 4Table40DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 5Table41DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table42DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.0$ 0.0 UBVRILSM/Eq. 6Table43DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u^*g'r'i^*z'y'$ LSM/Eq. 1Table44DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u^*g'r'i^*z'y'$ LSM/Eq. 2Table45DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u^*g'r'i^*z'y'$ LSM/Eq. 4Table45DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u^*g'r'i^*z'y'$ LSM/Eq. 4Table46DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u^*g'r'i^*z'y'$ LSM/Eq. 4Table47DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u^*g'r'i^*z'y'$ LSM/Eq. 5Table48DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u^*g'r'i^*z'y'$ LSM/Eq. 6Table50DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 UBVRILSM/Eq. 1Table51DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 UBVRILSM/Eq. 3Table52DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 UBVRILSM/Eq. 4Table53DA-N	Table38	DA	3750 K-60000 K	5.0-9.5	0.0	UBVRI	LSM/Eq. 3
Table40DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 5Table41DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table42DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.0$ 0.0 UBVRIGDC $y(UBVRI)$ Table43DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 1Table44DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 2Table45DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 3Table46DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 4Table47DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 4Table47DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 6Table48DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 6Table50DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ GDC $y(u'g'r'i'z'y')$ Table51DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 UBVRILSM/Eq. 1Table51DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 UBVRILSM/Eq. 3Table52DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 UBVRILSM/Eq. 4T	Table39	DA	3750 K-60000 K	5.0-9.5	0.0	UBVRI	LSM/Eq. 4
Table41DA 3750 K-60000 K $5.0-9.5$ 0.0 UBVRILSM/Eq. 6Table42DA 3750 K-60000 K $5.0-9.0$ 0.0 UBVRIGDC $y(UBVRI)$ Table43DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 $u^*g'r'i^*z'y'$ LSM/Eq. 1Table44DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 $u^*g'r'i^*z'y'$ LSM/Eq. 2Table45DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 $u^*g'r'i^*z'y'$ LSM/Eq. 3Table46DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 $u^*g'r'i^*z'y'$ LSM/Eq. 4Table47DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 $u^*g'r'i^*z'y'$ LSM/Eq. 5Table48DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 $u^*g'r'i^*z'y'$ LSM/Eq. 6Table49DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 $u^*g'r'i^*z'y'$ LSM/Eq. 6Table50DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 $u^*g'r'i^*z'y'$ GDC $y(u'g'r'i'z'y')'$ Table51DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 UBVRILSM/Eq. 2Table52DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 UBVRILSM/Eq. 3Table53DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 UBVRILSM/Eq. 5Table54DA-NLTE 40000 K-100000 K $6.0-9.5$ 0.0 UBVRILSM/Eq. 5Table55DA-NLTE	Table40	DA	3750 K-60000 K	5.0-9.5	0.0	UBVRI	LSM/Eq. 5
Table42DA $3750 \text{ K}-60000 \text{ K}$ $5.0-9.0$ 0.0 UBVRIGDC $y(UBVRI)$ Table43DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 1$ Table44DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 2$ Table45DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 3$ Table46DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 3$ Table47DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 4$ Table48DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 6$ Table49DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 6$ Table50DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $GDC y(u'g'r'i'z'y')$ Table51DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 1$ Table52DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 3$ Table53DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 3$ Table54DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 5$ Table55DA-NLTE $40000 \text{ K}-100000 \text{ K}$ $6.0-9.5$ 0.0 <t< td=""><td>Table41</td><td>DA</td><td>3750 K-60000 K</td><td>5.0-9.5</td><td>0.0</td><td>UBVRI</td><td>LSM/Eq. 6</td></t<>	Table41	DA	3750 K-60000 K	5.0-9.5	0.0	UBVRI	LSM/Eq. 6
Table43DA-NLTE $40000 \text{ K} - 100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 1$ Table44DA-NLTE $40000 \text{ K} - 100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 2$ Table45DA-NLTE $40000 \text{ K} - 100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 3$ Table46DA-NLTE $40000 \text{ K} - 100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 4$ Table47DA-NLTE $40000 \text{ K} - 100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 4$ Table48DA-NLTE $40000 \text{ K} - 100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 6$ Table49DA-NLTE $40000 \text{ K} - 100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 6$ Table50DA-NLTE $40000 \text{ K} - 100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $GDC y(u'g'r'i'z'y')$ Table51DA-NLTE $40000 \text{ K} - 100000 \text{ K}$ $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 2$ Table51DA-NLTE $40000 \text{ K} - 100000 \text{ K}$ $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 3$ Table52DA-NLTE $40000 \text{ K} - 100000 \text{ K}$ $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 4$ Table53DA-NLTE $40000 \text{ K} - 100000 \text{ K}$ $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 5$ Table54DA-NLTE $40000 \text{ K} - 100000 \text{ K}$ $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 5$ Table55DA-NLTE $40000 \text{ K} - 100000 \text{ K}$	Table42	DA	3750 K-60000 K	5.0-9.0	0.0	UBVRI	GDC $y(UBVRI)$
Table44DA-NLTE $40000 \text{ K} \cdot 100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 2$ Table45DA-NLTE $40000 \text{ K} \cdot 100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 3$ Table46DA-NLTE $40000 \text{ K} \cdot 100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 3$ Table47DA-NLTE $40000 \text{ K} \cdot 100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 4$ Table47DA-NLTE $40000 \text{ K} \cdot 100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 6$ Table48DA-NLTE $40000 \text{ K} \cdot 100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq. 6$ Table49DA-NLTE $40000 \text{ K} \cdot 100000 \text{ K}$ $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $GDC y(u'g'r'i'z'y')$ Table50DA-NLTE $40000 \text{ K} \cdot 100000 \text{ K}$ $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 1$ Table51DA-NLTE $40000 \text{ K} \cdot 100000 \text{ K}$ $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 2$ Table52DA-NLTE $40000 \text{ K} \cdot 100000 \text{ K}$ $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 3$ Table53DA-NLTE $40000 \text{ K} \cdot 100000 \text{ K}$ $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 5$ Table54DA-NLTE $40000 \text{ K} \cdot 100000 \text{ K}$ $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 5$ Table55DA-NLTE $40000 \text{ K} \cdot 100000 \text{ K}$ $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq. 5$ Table55DA-NLTE $40000 \text{ K} \cdot 100000 \text{ K}$ $6.$	Table43	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	u'g'r'i'z'y'	LSM/Eq. 1
Table45DA-NLTE40000 K-100000 K6.0-9.50.0 $u'g'r'i'z'y'$ LSM/Eq. 3Table46DA-NLTE40000 K-100000 K6.0-9.50.0 $u'g'r'i'z'y'$ LSM/Eq. 4Table47DA-NLTE40000 K-100000 K6.0-9.50.0 $u'g'r'i'z'y'$ LSM/Eq. 4Table48DA-NLTE40000 K-100000 K6.0-9.50.0 $u'g'r'i'z'y'$ LSM/Eq. 6Table49DA-NLTE40000 K-100000 K6.0-9.50.0 $u'g'r'i'z'y'$ LSM/Eq. 6Table50DA-NLTE40000 K-100000 K6.0-9.50.0 $u'g'r'i'z'y'$ GDC $y(u'g'r'i'z'y')$ Table51DA-NLTE40000 K-100000 K6.0-9.50.0UBVRILSM/Eq. 1Table51DA-NLTE40000 K-100000 K6.0-9.50.0UBVRILSM/Eq. 3Table52DA-NLTE40000 K-100000 K6.0-9.50.0UBVRILSM/Eq. 3Table53DA-NLTE40000 K-100000 K6.0-9.50.0UBVRILSM/Eq. 3Table54DA-NLTE40000 K-100000 K6.0-9.50.0UBVRILSM/Eq. 4Table55DA-NLTE40000 K-100000 K6.0-9.50.0UBVRILSM/Eq. 5Table55DA-NLTE40000 K-100000 K6.0-9.50.0UBVRILSM/Eq. 6Table56DA-NLTE40000 K-100000 K6.0-9.50.0UBVRILSM/Eq. 6Table56DA-NLTE40000 K-100000 K6.0-9.50.0UBVRILSM/Eq. 6	Table44	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	u'g'r'i'z'v'	LSM/Eq. 2
Table46DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 4Table47DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 4Table48DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 6Table49DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ LSM/Eq. 6Table50DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ GDC $y(u'g'r'i'z'y')$ Table51DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 UBVRILSM/Eq. 1Table51DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 UBVRILSM/Eq. 2Table52DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 UBVRILSM/Eq. 3Table53DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 UBVRILSM/Eq. 4Table54DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 UBVRILSM/Eq. 5Table55DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 UBVRILSM/Eq. 6Table54DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 UBVRILSM/Eq. 6Table55DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 UBVRILSM/Eq. 6Table56DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 UBVRILSM/Eq. 6	Table45	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	u'g'r'i'z'v'	LSM/Eq. 3
Table47DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq.5$ Table48DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq.6$ Table49DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $LSM/Eq.6$ Table50DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $u'g'r'i'z'y'$ $GDC y(u'g'r'i'z'y')$ Table50DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq.1$ Table51DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq.2$ Table52DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq.3$ Table53DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq.4$ Table54DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq.5$ Table55DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq.6$ Table54DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq.6$ Table55DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq.6$ Table56DA-NLTE40000 K-100000 K $6.0-9.5$ 0.0 $UBVRI$ $LSM/Eq.6$	Table46	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	u'g'r'i'z'v'	LSM/Eq. 4
Table 48 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 u'g'r'i'z'y' LSM/Eq. 6 Table 49 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 u'g'r'i'z'y' GDC y(u'g'r'i'z'y') Table 50 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 u'g'r'i'z'y' GDC y(u'g'r'i'z'y') Table 50 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 1 Table 51 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 2 Table 52 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 3 Table 53 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 4 Table 54 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 5 Table 55 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 6 Table 55 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 6 Table 55 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0	Table47	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	u'g'r'i'z'v'	LSM/Eq. 5
Table49DA-NLTE40000 K-100000 K6.0-9.50.0 $u^*g'r'i^*z'y'$ GDC $y(u'g'r'i'z'y')$ Table50DA-NLTE40000 K-100000 K6.0-9.50.0UBVRILSM/Eq. 1Table51DA-NLTE40000 K-100000 K6.0-9.50.0UBVRILSM/Eq. 2Table52DA-NLTE40000 K-100000 K6.0-9.50.0UBVRILSM/Eq. 3Table53DA-NLTE40000 K-100000 K6.0-9.50.0UBVRILSM/Eq. 3Table53DA-NLTE40000 K-100000 K6.0-9.50.0UBVRILSM/Eq. 4Table54DA-NLTE40000 K-100000 K6.0-9.50.0UBVRILSM/Eq. 5Table55DA-NLTE40000 K-100000 K6.0-9.50.0UBVRILSM/Eq. 6Table56DA-NLTE40000 K-100000 K6.0-9.50.0UBVRILSM/Eq. 6Table56DA-NLTE40000 K-100000 K6.0-9.50.0UBVRILSM/Eq. 6	Table48	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	u'g'r'i'z'v'	LSM/Eq. 6
Table 50 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 1 Table 51 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 1 Table 51 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 2 Table 52 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 3 Table 53 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 4 Table 54 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 4 Table 55 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 5 Table 55 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 6 Table 55 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 6 Table 56 DA-NLTE 40000 K-100000 K 6.0-9.0 0.0 UBVRI LSM/Eq. 6	Table49	DA-NITE	40000 K-100000 K	6 0-9 5	0.0	u'g'r'i'z'v'	GDC $v(u'o'r'i'z'v')$
Table51 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 2 Table52 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 2 Table52 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 3 Table53 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 4 Table54 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 5 Table55 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 6 Table56 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 6 Table56 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 6	Table 50	DA-NITE	40000 K-100000 K	6 0-9 5	0.0	UBVRI	LSM/Eq 1
Table 52 DA-NLTE 40000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 2 Table 52 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 3 Table 53 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 4 Table 54 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 5 Table 55 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 6 Table 56 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 6	Table51	DA-NITE	40000 K-100000 K	6 0-9 5	0.0	UBVRI	LSM/Eq. 1
Table52 DA-NLTE 40000 K 100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 4 Table53 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 4 Table54 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 5 Table55 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 6 Table56 DA-NLTE 40000 K-100000 K 6.0-9.0 0.0 UBVRI CDC v(UBVR)	Table52	DA-NI TE	40000 K-100000 K	6.0-9.5	0.0	UBVRI	LSM/Eq. 2
Table55 DA-NLTE 40000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 4 Table55 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 6 Table55 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 6 Table56 DA-NLTE 40000 K-100000 K 6.0-9.0 0.0 UBVRI CDC v(UBVR)	Table53	DA-NI TE	40000 K-100000 K	6.0-9.5	0.0	UBVRI	LSM/Eq. 5
Table55 DA-NLTE 40000 K-100000 K 6.0-9.5 0.0 UBVRI LSM/Eq. 6 Table56 DA-NLTE 40000 K-100000 K 6.0-9.0 0.0 UBVRI LSM/Eq. 6 Table56 DA-NLTE 40000 K-100000 K 6.0-9.0 0.0 UBVRI GDC v(URVR)	Table54	DA-NI TE	40000 K 100000 K	6.0-9.5	0.0	URVRI	LSM/Eq. 7
Table 56 DA-NLTE 40000 K-100000 K 6 0.9 0 0.0 URVRI GDC v(URVR)	Table55	DA-NITE	40000 K-100000 K	6.0-9.5	0.0	URVRI	LSM/Eq. 5
	Table56	DA-NITE	40000 K-100000 K	6 0-9 0	0.0	URVRI	GDC v(I/RVRI)

Table A.2:	Gravity and	limb-darkening	coefficients for the	he HiPERCAM	photometric	system
					r · · · · · ·	

Name	Source	range T _{eff}	range log g	log [H/He]	Filters	Fit/equation
Table57	DB	10000 K-40000 K	5.5-9.5	-10.0	HiPERCAM	LSM/Eq. 1
Table58	DB	10000 K-40000 K	5.5-9.5	-10.0	HiPERCAM	LSM/Eq. 2
Table59	DB	10000 K-40000 K	5.5-9.5	-10.0	HiPERCAM	LSM/Eq. 3
Table60	DB	10000 K-40000 K	5.5-9.5	-10.0	HiPERCAM	LSM/Eq. 4
Table61	DB	10000 K-40000 K	5.5-9.5	-10.0	HiPERCAM	LSM/Eq. 5
Table62	DB	10000 K-40000 K	5.5-9.5	-10.0	HiPERCAM	LSM/Eq. 6
Table63	DB	10000 K-40000 K	5.5-9.5	-10.0	HiPERCAM	GDC y(HiPERCAM)
Table64	DBA	11000 K-40000 K	7.0-9.0	-2.0	HiPERCAM	LSM/Eq. 1
Table65	DBA	11000 K-40000 K	7.0-9.0	-2.0	HiPERCAM	LSM/Eq. 2
Table66	DBA	11000 K-40000 K	7.0-9.0	-2.0	HiPERCAM	LSM/Eq. 3
Table67	DBA	11000 K-40000 K	7.0-9.0	-2.0	HiPERCAM	LSM/Eq. 4
Table68	DBA	11000 K-40000 K	7.0-9.0	-2.0	HiPERCAM	LSM/Eq. 5
Table69	DBA	11000 K-40000 K	7.0-9.0	-2.0	HiPERCAM	LSM/Eq. 6
Table70	DBA	11000 K-40000 K	7.0-9.0	-2.0	HiPERCAM	GDC y(HiPERCAM)
Table71	DA	3750 K-60000 K	5.0-9.0	0.0	HiPERCAM	LSM/Eq. 1
Table72	DA	3750 K-60000 K	5.0-9.0	0.0	HiPERCAM	LSM/Eq. 2
Table73	DA	3750 K-60000 K	5.0-9.0	0.0	HiPERCAM	LSM/Eq. 3
Table74	DA	3750 K-60000 K	5.0-9.0	0.0	HiPERCAM	LSM/Eq. 4
Table75	DA	3750 K-60000 K	5.0-9.0	0.0	HiPERCAM	LSM/Eq. 5
Table76	DA	3750 K-60000 K	5.0-9.0	0.0	HiPERCAM	LSM/Eq. 6
Table77	DA	3750 K-60000 K	5.0-9.0	0.0	HiPERCAM	GDC y(HiPERCAM)
Table78	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	HiPERCAM	LSM/Eq. 1
Table79	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	HiPERCAM	LSM/Eq. 2
Table80	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	HiPERCAM	LSM/Eq. 3
Table81	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	HiPERCAM	LSM/Eq. 4
Table82	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	HiPERCAM	LSM/Eq. 5
Table83	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	HiPERCAM	LSM/Eq. 6
Table84	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	HiPERCAM	GDC y(HiPERCAM)

Table A.3: Gravit	v and limb-darkening	coefficients for the Ker	pler. TESS, and Gaia	photometric systems
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Name	Source	range T _{eff}	range log g	log [H/He]	Filters	Fit/equation
Table85	DB	10000 K-40000 K	5.5-9.5	-10.0	KeplerTESSGaia	LSM/Eq. 1
Table86	DB	10000 K-40000 K	5.5-9.5	-10.0	KeplerTESSGaia	LSM/Eq. 2
Table87	DB	10000 K-40000 K	5.5-9.5	-10.0	KeplerTESSGaia	LSM/Eq. 3
Table88	DB	10000 K-40000 K	5.5-9.5	-10.0	KeplerTESSGaia	LSM/Eq. 4
Table89	DB	10000 K-40000 K	5.5-9.5	-10.0	KeplerTESSGaia	LSM/Eq. 5
Table90	DB	10000 K-40000 K	5.5-9.5	-10.0	KeplerTESSGaia	LSM/Eq. 6
Table91	DB	10000 K-40000 K	5.5-9.5	-10.0	KeplerTESSGaia	GDC y(KeplerTESSGaia)
Table92	DBA	11000 K-40000 K	7.0-9.0	-2.0	KeplerTESSGaia	LSM/Eq. 1
Table93	DBA	11000 K-40000 K	7.0-9.0	-2.0	KeplerTESSGaia	LSM/Eq. 2
Table94	DBA	11000 K-40000 K	7.0-9.0	-2.0	KeplerTESSGaia	LSM/Eq. 3
Table95	DBA	11000 K-40000 K	7.0-9.0	-2.0	KeplerTESSGaia	LSM/Eq. 4
Table96	DBA	11000 K-40000 K	7.0-9.0	-2.0	KeplerTESSGaia	LSM/Eq. 5
Table97	DBA	11000 K-40000 K	7.0-9.0	-2.0	KeplerTESSGaia	LSM/Eq. 6
Table98	DBA	11000 K-40000 K	7.0-9.0	-2.0	KeplerTESSGaia	GDC y(KeplerTESSGaia)
Table99	DA	3750 K-60000 K	5.0-9.5	0.0	KeplerTESSGaia	LSM/Eq. 1
Table100	DA	3750 K-60000 K	5.0-9.5	0.0	KeplerTESSGaia	LSM/Eq. 2
Table101	DA	3750 K-60000 K	5.0-9.5	0.0	KeplerTESSGaia	LSM/Eq. 3
Table102	DA	3750 K-60000 K	5.0-9.5	0.0	KeplerTESSGaia	LSM/Eq. 4
Table103	DA	3750 K-60000 K	5.0-9.5	0.0	KeplerTESSGaia	LSM/Eq. 5
Table104	DA	3750 K-60000 K	5.0-9.5	0.0	KeplerTESSGaia	LSM/Eq. 6
Table105	DA	3750 K-60000 K	5.0-9.5	0.0	KeplerTESSGaia	GDC y(KeplerTESSGaia)
Table106	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	KeplerTESSGaia	LSM/Eq. 1
Table107	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	KeplerTESSGaia	LSM/Eq. 2
Table108	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	KeplerTESSGaia	LSM/Eq. 3
Table109	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	KeplerTESSGaia	LSM/Eq. 4
Table110	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	KeplerTESSGaia	LSM/Eq. 5
Table111	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	KeplerTESSGaia	LSM/Eq. 6
Table112	DA-NLTE	40000 K-100000 K	6.0-9.5	0.0	KeplerTESSGaia	GDC y(KeplerTESSGaia)