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Concurrent factors determine toughening in the hydraulic fracture of poroelastic composites

Alessandro Lucantonio · Giovanni Noselli

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Abstract Brittle materials fail catastrophically. In consequence of their limited flaw-tolerance, failure occurs by localized fracture and is typically a dynamic process. Recently, experiments on epithelial cell monolayers have revealed that this scenario can be significantly modified when the material susceptible to cracking is adhered to a hydrogel substrate. Thanks to the hydraulic coupling between the brittle layer and the poroelastic substrate, such a composite can develop a toughening mechanism that relies on the simultaneous growth of multiple cracks. Here, we study this remarkable behaviour by means of a detailed model, and explore how the material and loading parameters concur in determining the macroscopic toughness of the system. By extending a previous study, our results show that rapid loading conveys material toughness by promoting distributed cracking. Moreover, our theoretical findings may suggest innovative architectures of flaw-insensitive materials with higher toughness.

Keywords Hydraulic fracture · Toughening · Multiple cracking · Brittle layer · Hydrogel · Cohesive zone

1 Introduction

Nature has adopted diverse, remarkable strategies to enhance the flaw-tolerance of biological tissues, such as bone and tooth [7]. As a result, they can sustain relatively high levels of strain while maintaining their integrity. Epithelium is another example of such tissues.

A. Lucantonio · G. Noselli (✉)
SISSA–International School for Advanced Studies, via
Bonomea 265, 34136 Trieste, Italy
Tel.: +39 040 3787 432
E-mail: giovanni.noselli@sissa.it
Authors contributed equally to this work.

Despite the intrinsic brittle behavior of the cell monolayer [9], this can display a high fracture toughness, as it has recently been shown experimentally [3]. In a previous work [11] we have demonstrated that this behavior is determined by the hydraulic coupling between the epithelial layer and the extracellular matrix, which can be regarded as a poroelastic, hydrogel-like material. Specifically, because fracture requires flow into the crack to fill its volume, the kinetics of solvent migration within the hydrogel controls the velocity of crack propagation, so that decreased permeability promotes multiple-cracking at cell-cell junctions. Then, this distributed cracking mechanism maximizes the external work performed on the system before failure (which is a measure of toughness), since cell-cell separation requires a significant amount of work and is accompanied by dissipation due to solvent flow.

The just described behavior sharply contrasts with that of brittle materials, which are highly flaw-sensitive and typically fail catastrophically, by localized fracture [1]. For instance, the equilibrium of two edge cracks with the same length in an elastic brittle layer under tensile load is unstable, so that any perturbation will cause only one of the cracks to propagate dynamically [12]. In general, since toughening of soft materials typically relies on energy dissipation [14], studying the energetics of crack propagation [13] is crucial to understand the interplay of different physics involved in fracture phenomena and for the implementation of toughening strategies in synthetic materials [8]. Therefore, we here reconsider the problem studied numerically in [11], where a brittle layer containing two pre-cracks and bonded to a hydrogel substrate is subject to a remote strain. In particular, we analyze the relative influence of the different dissipative mechanisms on the macroscopic toughness of the system. Moreover, we focus on

the effect of the strain rate on the transition from distributed to localized cracking.

The paper is organized as follows. We first establish the model accounting for the poroelasticity of the hydrogel substrate, the elasticity of the brittle layer and its hydraulic fracture. Then, the weak formulation of the model is presented, which is suitable for its implementation into a finite element code. Numerical results are shown and discussed concerning the dissipations for both the regimes of distributed and localized fracture.

2 Model for the hydraulic fracture of a brittle layer bonded to a hydrogel substrate

In this section, we derive the governing equations for the nonlinear model of hydraulically driven crack propagation in a brittle layer bonded to a hydrogel substrate. Both the brittle solid and the hydrogel are modelled as layers of finite thickness and infinite length. To simplify notation, the derivation is presented for the case of a single crack. Then, in the following section, the numerical model is extended to account for two competing cracks.

2.1 Notation and kinematics

We introduce an orthonormal basis $\{\mathbf{e}_i\}$, $i = \{1, 2, 3\}$, for the three-dimensional Euclidean space \mathcal{E} . We denote by $\mathcal{B}_t^g \subset \mathcal{E}$ and $\mathcal{B}_t^e \subset \mathcal{E}$ the current configurations at time t of the hydrogel and the brittle layer, respectively; the corresponding reference configurations are indicated by dropping the subscript t . Further, we introduce two Cartesian coordinate systems $\{X_i\}$ and $\{x_i\}$, for the reference and the current configuration of the system, respectively. A material point X of the reference solid domain $\mathcal{B} = \mathcal{B}^g \cup \mathcal{B}^e$ with coordinates X_i is mapped into a spatial point x with coordinates $x_i = f_i(X_j, t)$ in the current configuration \mathcal{B}_t (Fig. 1), where f_i are the coordinate representations of the motion of the solid domain. We will use the symbol \mathbf{F} for the deformation gradient, and write $J = \det \mathbf{F}$ for its determinant and $\mathbf{F}^* = J\mathbf{F}^{-T}$ for its cofactor. We assume plane strain conditions, such that all the quantities do not depend on X_3 and thus $x_\alpha = f_\alpha(X_1, X_2, t)$, $\alpha = \{1, 2\}$, whereas $x_3 = f_3(X_3, t) = X_3$. We take all of the three-dimensional domains to be of unit-depth, so that, in the ensuing derivation, volume integrals and area integrals over the cross-section corresponding to the cut plane $X_3 = x_3 = 0$ coincide.

The brittle layer contains an initially closed pre-crack with length a_0 , whose faces belong to the referential segments \mathcal{J}^\pm , being \mathcal{J}_t^- and \mathcal{J}_t^+ their current

counterparts. For the reference configuration \mathcal{L} of the longitudinal crack axis, we choose the segment aligned with the X_2 -axis: $\mathcal{L} = \{X \in \mathcal{E} \mid X_1 = X_3 = 0, X_2 \in [0, h] = \mathcal{H}\}$, where h is the thickness of the brittle layer. We assume that the axis \mathcal{L}_t remains straight and vertical upon deformation, and that the crack undergoes a plane motion symmetric with respect to such axis. Thus, the axis of the crack stretches by the amount $\lambda(X_2, t) = \partial f_2^c / \partial X_2(X_2, t)$ to follow the vertical motion $f_2^c(X_2, t) = \lim_{X_1 \rightarrow 0^\pm} f_2(X_1, X_2, t)$, with $X_2 \in \mathcal{H}$.

We define the material description of the crack opening $\delta(X_2, t)$ as

$$\delta(X_2, t) = \llbracket f_1(0, X_2, t) \rrbracket = 2f_1^c(X_2, t), \quad (1)$$

where the symbol $\llbracket \cdot \rrbracket$ denotes the jump operator, whereas $f_1^c(X_2, t) = \lim_{X_1 \rightarrow 0^+} f_1(X_1, X_2, t)$ and the second equality follows from symmetry. By composing δ with the inverse of the deformation mapping, we obtain the crack opening as a function of the spatial location along \mathcal{L}_t : $\delta_s(x_2, t) = \delta(X_2, t) \circ (f_2^c)^{-1}(x_2, t)$. The velocity of the crack faces may be readily computed as

$$\mathbf{v}_c^\pm(x_2, t) = \pm \frac{1}{2} \dot{\delta}_s(x_2, t) \mathbf{e}_1 + w(x_2, t) \mathbf{e}_2, \quad (2)$$

where $w(x_2, t) = \dot{f}_2^c(X_2, t) \circ (f_2^c)^{-1}(x_2, t)$ is its vertical component. Here, a superposed dot denotes the material time derivative (at X_2 fixed), so that

$$\begin{aligned} \dot{\delta}_s(x_2, t) &= \dot{\delta}(X_2, t) \circ (f_2^c)^{-1}(x_2, t) = \\ &= \frac{\partial \delta_s(x_2, t)}{\partial t} + w(x_2, t) \frac{\partial \delta_s(x_2, t)}{\partial x_2}. \end{aligned} \quad (3)$$

We call $\mathcal{B}_t^f \subset \mathcal{E}$ the fluid domain, that is, the spatial volume with longitudinal axis \mathcal{L}_t enclosed by the crack faces and filled with solvent. Finally, we denote by $\mathbf{v}(x, t)$, $x \in \mathcal{B}_t^f$, the spatial velocity field of the solvent within the crack.

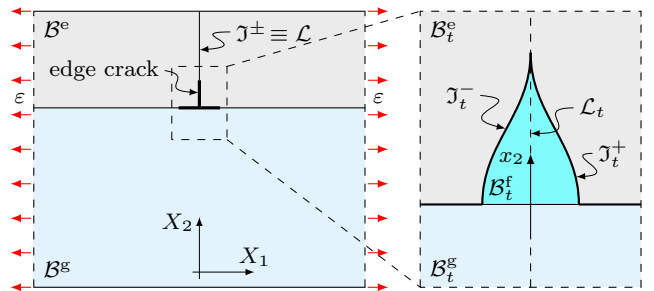


Fig. 1: Sketch of the reference configuration of the system (left) and of the current configuration of the edge crack (right) in the cut plane $X_3 = x_3 = 0$.

2.2 Solvent flow within the crack

In this section, we establish a reduced one-dimensional model for the solvent flow within the crack. Specifically, we derive a set of equations, defined over the axis \mathcal{L} , by localizing the integral balance laws for the fluid expressed in terms of resultant quantities over horizontal cross-sections. A related model was introduced in [5] without accounting for stretching along the axis. We consider the steady flow of an incompressible, viscous fluid under the assumption that the motion is quasi-1D, *i.e.* the velocity field \mathbf{v} is independent of x_3 and is dominated by the longitudinal component $v_2 = \mathbf{v} \cdot \mathbf{e}_2$.

We define a control volume $\mathcal{V}_t \subset \mathcal{B}_t^f$, enclosed by the cross-sections that are located at two fixed positions \bar{x}_2 and \bar{x}'_2 along \mathcal{L}_t , and the crack faces \mathcal{J}_t^\pm .

2.2.1 Conservation of solvent mass

The equation of conservation of mass for the incompressible fluid in \mathcal{V}_t reads

$$\int_{\partial\mathcal{V}_t} \mathbf{v} \cdot \mathbf{n} \, da = 0, \quad (4)$$

where \mathbf{n} is the outward unit normal to $\partial\mathcal{V}_t$. On the crack faces this is given by the following relation

$$\mathbf{n}_c^\pm = \frac{1}{\|\mathbf{n}_c\|} \left(\pm \mathbf{e}_1 - \frac{1}{2} \frac{\partial \delta_s}{\partial x_2} \mathbf{e}_2 \right), \quad (5)$$

with $\|\mathbf{n}_c\| = \sqrt{1 + 1/4(\partial \delta_s / \partial x_2)^2}$. Notice that the area element along the crack faces in Eq. (4) transforms according to $da = \|\mathbf{n}_c\| dx_2 dx_3$. Using eqs. (2) and Eq. (5) the volume flux contributions over parts of \mathcal{J}_t^\pm in Eq. (4) may be evaluated as

$$\int_{\bar{x}_2}^{\bar{x}'_2} \left(\dot{\delta}_s - w \frac{\partial \delta_s}{\partial x_2} \right) dx_2, \quad (6)$$

while the net flux through the cross-sections delimiting \mathcal{V}_t is

$$Q(\bar{x}'_2, t) - Q(\bar{x}_2, t) = \int_{\bar{x}_2}^{\bar{x}'_2} \frac{\partial Q}{\partial x_2} dx_2, \quad (7)$$

with

$$Q(x_2, t) = \int_{-\delta_s(x_2, t)/2}^{\delta_s(x_2, t)/2} v_2(x_1, x_2, t) dx_1 \quad (8)$$

the solvent volume flux per unit depth. By summing these two contributions, Eq. (4) may be recast as

$$\int_{\bar{x}_2}^{\bar{x}'_2} \left(\dot{\delta}_s - w \frac{\partial \delta_s}{\partial x_2} + \frac{\partial Q}{\partial x_2} \right) dx_2 = 0. \quad (9)$$

To express this equation in the reference configuration \mathcal{L} , we first observe that

$$\frac{\partial w(x_2, t)}{\partial x_2} = \left(\frac{1}{\lambda(X_2, t)} \frac{\partial \lambda(X_2, t)}{\partial t} \right) \circ (f_2^c)^{-1}(x_2, t), \quad (10)$$

$$\frac{\partial \delta_s(x_2, t)}{\partial x_2} = \left(\frac{1}{\lambda(X_2, t)} \frac{\partial \delta(X_2, t)}{\partial X_2} \right) \circ (f_2^c)^{-1}(x_2, t). \quad (11)$$

Then, upon exploiting Eq. (3) and localizing, we obtain

$$\frac{\partial(\delta\lambda)}{\partial t} + \frac{\partial q}{\partial X_2} = 0, \quad (12)$$

where $q(X_2, t) = q_s(x_2, t) \circ f_2^c(X_2, t)$ is the material description of the solvent flux

$$q_s(x_2, t) = Q(x_2, t) - w(x_2, t) \delta_s(x_2, t) \quad (13)$$

relative to the material particles on the crack faces.

2.2.2 Balance of forces

Upon neglecting inertia, the balance of forces for the solvent within the crack along the longitudinal axis of \mathcal{V}_t reads

$$\mathbf{e}_2 \cdot \int_{\partial\mathcal{V}_t} \mathbf{T}_f \mathbf{n} \, da = 0. \quad (14)$$

As a constitutive law for the stress tensor we take the representation for an incompressible, Newtonian viscous fluid, such that

$$\mathbf{T}_f = -p_s \mathbf{I} + 2\eta \text{sym}(\text{grad } \mathbf{v}), \quad (15)$$

with p_s and η the pressure and the viscosity of the solvent, respectively. Following lubrication theory [2], we assume that: i) the velocity profile is parabolic along the cross-sections, *i.e.*

$$v_2(x_1, x_2, t) = 4(w - v_2^{\max}) \left(\frac{x_1}{\delta_s} \right)^2 + v_2^{\max}, \quad (16)$$

where $v_2^{\max} = (3Q/\delta_s - w)/2$; ii) the pressure $p_s(x_2, t)$ is uniform over each cross-section; iii) the components of the velocity gradient along x_2 are negligible. Under these hypotheses, the traction on the crack faces is

$$\begin{aligned} \mathbf{t}_f^\pm &= \mathbf{T}_f \mathbf{n}_c^\pm \approx \\ &\approx -p_s \mathbf{n}_c^\pm - 6\eta \frac{q_s}{\delta_s^2} (\mathbf{e}_1 \otimes \mathbf{e}_2 + \mathbf{e}_2 \otimes \mathbf{e}_1) \mathbf{n}_c^\pm, \end{aligned} \quad (17)$$

where in the last equality we have used the representation (16) evaluated at $x_2 = \pm \delta_s/2$. With this, the contribution to the integral in (14) extending over the crack faces may be computed as

$$-12 \int_{\bar{x}_2}^{\bar{x}'_2} \frac{q_s}{\delta_s^2} dx_2 + \int_{\bar{x}_2}^{\bar{x}'_2} p_s \frac{\partial \delta_s}{\partial x_2} dx_2. \quad (18)$$

Moreover, the force resultant over the cross-sections at \bar{x}_2 and \bar{x}'_2 is

$$-p_s(x_2, t)\delta_s(x_2, t)\Big|_{\bar{x}_2}^{\bar{x}'_2} = -\int_{\bar{x}_2}^{\bar{x}'_2} \frac{\partial(p_s\delta_s)}{\partial x_2} dx_2. \quad (19)$$

Finally, by expressing the sum of eqs. (18)-(19) in the reference crack axis \mathcal{L} and by localizing we obtain

$$q = -\frac{\delta^3}{12\eta\lambda} \frac{\partial p_f}{\partial X_2}, \quad (20)$$

where $p_f(X_2, t) = p_s(x_2, t) \circ f_2^c(X_2, t)$.

2.3 Cohesive zone model

To model crack propagation, we employ a cohesive zone approach [6]. We take the cohesive tractions \mathbf{s}_c^\pm per unit reference area acting on the crack faces \mathcal{J}^\pm to be orthogonal to the reference longitudinal axis \mathcal{L} of the crack, and such that their magnitude is a function of the crack opening:

$$\mathbf{s}_c^\pm = \mp\sigma(\delta) \mathbf{e}_1. \quad (21)$$

We choose a bilinear traction-separation law for $\sigma(\delta)$, such that

$$\sigma(\delta) = (1-d) \frac{\sigma_o}{\delta_o} \delta, \quad (22)$$

where σ_o is the cohesive strength (attained for $\delta = \delta_o$) and $d(X_2, t) \in [0, 1]$ is the damage. We prescribe the following evolution law for the damage:

$$d = \frac{\delta_c(\delta^m - \delta_o)}{\delta^m(\delta_c - \delta_o)}, \quad (23)$$

where $\delta^m(X_2, t)$ is the maximum value attained by the opening during crack evolution and δ_c is the crack opening at failure ($d = 1$). The fracture energy Γ is related to the parameters of the cohesive zone model through the equation $\Gamma = \sigma_o\delta_c/2$.

In addition to the cohesive tractions, the crack faces \mathcal{J}_t^\pm are subject to the pressure and to the shear stress exerted by the fluid, which contributes to the traction with the term $-\mathbf{t}_f^\pm$, see Eq. (17). The corresponding reference traction is

$$\mathbf{s}_f^\pm = \pm p_f \mathbf{F}^* \mathbf{e}_1 + 6\eta \frac{q}{\delta^2} [(\mathbf{F}^* \mathbf{e}_1 \cdot \mathbf{e}_1) \mathbf{e}_2 + (\mathbf{F}^* \mathbf{e}_1 \cdot \mathbf{e}_2) \mathbf{e}_1], \quad (24)$$

such that the total reference traction acting on the crack faces is given by $\mathbf{s}^\pm = \mathbf{s}_f^\pm + \mathbf{s}_c^\pm$.

2.4 Elasticity of the brittle layer

By assuming inertia negligible, the balances of forces and moments in \mathcal{B}^e read

$$\operatorname{div} \mathbf{S} = \mathbf{0}, \quad \operatorname{skw} \mathbf{S} \mathbf{F}^T = \mathbf{0}, \quad (25)$$

where \mathbf{S} denotes the first Piola-Kirchhoff stress tensor.

We model the brittle layer as an impermeable, elastic solid characterized by the compressible neo-Hookean free energy density

$$\psi(\mathbf{F}) = \frac{G_e}{2} (\mathbf{F} \cdot \mathbf{F} - 2 \log J - 3) + \frac{\Lambda}{2} (\log J)^2, \quad (26)$$

where G_e and $\Lambda \gg G_e$ are the Lamé moduli. The corresponding first Piola-Kirchhoff stress is given by

$$\mathbf{S} = \frac{\partial \psi}{\partial \mathbf{F}} = G_e \left(\mathbf{F} - \frac{1}{J} \mathbf{F}^* \right) + \Lambda \frac{\log J}{J} \mathbf{F}^*. \quad (27)$$

Notice that, because of Eq. (27) and the plane strain hypothesis, $\mathbf{S} \mathbf{e}_1 \cdot \mathbf{e}_3 = \mathbf{S} \mathbf{e}_2 \cdot \mathbf{e}_3 = \mathbf{S} \mathbf{e}_3 \cdot \mathbf{e}_1 = \mathbf{S} \mathbf{e}_3 \cdot \mathbf{e}_2 = 0$ and the out-of-plane balance equation in (25)₁ is trivially satisfied. Hence, the balance of forces and moments may be formulated in terms of the plane components of \mathbf{S} only.

2.5 Poroelasticity of the hydrogel layer

In the following, we briefly summarize the non-linear swelling theory for hydrogels introduced in [10]. The state of the hydrogel is described by the motion f of the polymer network and the solvent concentration c per unit reference volume. The chemical potential μ of the solvent within the hydrogel quantifies the energy carried by the solvent and represents the driving force of solvent migration. The corresponding solvent molar flux \mathbf{h} characterizes the relative motion of the solvent with respect to the polymer matrix. Consistently with the plane strain hypothesis, we assume that solvent migration takes place in the plane \mathbf{e}_1 - \mathbf{e}_2 , so that $c(X_1, X_2, t)$, $\mu(X_1, X_2, t)$, and $\mathbf{h} \cdot \mathbf{e}_3 = 0$.

The polymer matrix and the solvent are considered to be separately incompressible; hence, the change in volume of the hydrogel is related to the change in solvent concentration:

$$J = 1 + \Omega(c - c_o), \quad (28)$$

where Ω is the solvent molar volume and $c_o = (J_o - 1)/(\Omega J_o)$ is the solvent concentration per unit reference volume associated to the initial free swelling from the dry configuration to \mathcal{B}^s . Here, J_o is the volume ratio between the reference and the dry configuration. The

constraint of Eq. (28) is enforced through the Lagrange multiplier p .

Swelling processes are governed by the equations of balance of forces and moments, which are the same as those for the brittle layer, see Eqs. (25), and by the balance of solvent mass in \mathcal{B}^s

$$\dot{c} = -\operatorname{div} \mathbf{h}, \quad (29)$$

subject to the initial condition $c(X_1, X_2, 0) = c_o$.

As concerns the constitutive equations, we prescribe the following Flory-Rehner representation for the free energy density of the hydrogel [4, 10]

$$\psi(\mathbf{F}, c) = \psi_e(\mathbf{F}) + \psi_m(c), \quad (30)$$

where

$$\psi_e(\mathbf{F}) = \frac{G_d}{2J_o} (J_o^{1/3} \mathbf{F} \cdot \mathbf{F} - 3) \quad (31)$$

and

$$\psi_m(c) = \mathcal{R}Tc \left[\log \left(\frac{\Omega J_o c}{1 + \Omega J_o c} \right) + \chi \frac{1}{1 + \Omega J_o c} \right] \quad (32)$$

are the neo-Hookean elastic energy and the Flory-Huggins free energy of mixing, respectively. Here, G_d is the shear modulus of the dry polymer, \mathcal{R} is the universal gas constant, T is the absolute temperature of the environment, and χ is the polymer-solvent mixing parameter. For the consistency with thermodynamical principles, the corresponding constitutive equations are given by:

$$\mathbf{S} = \frac{\partial \psi_e}{\partial \mathbf{F}} - p \mathbf{F}^*, \quad (33)$$

$$\mu = \frac{\partial \psi_m}{\partial c} + \Omega p, \quad (34)$$

$$\mathbf{h} = -\frac{cD}{\mathcal{R}T} \nabla \mu, \quad (35)$$

where D is the diffusivity of the solvent within the hydrogel. In the reference configuration \mathcal{B}^s , the hydrogel is in equilibrium with the external solvent whose chemical potential is μ_o . Specifically, we consider an external solvent in equilibrium with its vapor, such that $\mu_o = 0$ J/mol. Thus, the reference configuration is identified by the conditions $\mathbf{F} = \mathbf{I}$, $\mu = \mu_o$ and $\mathbf{S} = \mathbf{0}$, which together determine the swelling ratio J_o as the solution of following equation

$$\log \left(1 - \frac{1}{J_o} \right) + \frac{1}{J_o} + \frac{\chi}{J_o^2} + \frac{G_d \Omega}{\mathcal{R}T} \frac{1}{J_o^{1/3}} = 0. \quad (36)$$

2.6 Boundary and interface conditions

In the numerical implementation, we refer to a computational domain which is limited along the \mathbf{e}_1 -axis by vertical boundaries of normal $\mathbf{m} = \pm \mathbf{e}_1$. In order for the computational model to appropriately approximate the theoretical setting, we choose its length to be sufficiently larger than the thickness of the composite.

Starting from the equilibrium state of free swelling with $\mu = \mu_o$, the system is subject to a homogeneous, horizontal strain of constant rate $\dot{\epsilon}$. Correspondingly, the vertical component $\mathbf{u} \cdot \mathbf{e}_1$ of the displacement field $\mathbf{u}(X_1, X_2, t)$ is prescribed along the vertical boundaries $\partial_{\mathbf{u}} \mathcal{B}$ of the composite, while the vertical component $\mathbf{u} \cdot \mathbf{e}_2$ of the displacement field is constrained at the bottom boundary of the hydrogel only. In order to ease crack opening, continuity of the displacements is relaxed at the interface between the brittle layer and the hydrogel along small segments near the cracks. The remaining parts of the boundary $\partial \mathcal{B}$ are traction-free.

As regards the boundary conditions for solvent migration, we assume zero solvent flux on $\partial \mathcal{B}^s$. For short times, no significant exchange of solvent with the exterior can take place. At the crack inlet, we impose the continuity of solvent pressure: $\mu = \Omega p_f$, where μ/Ω is the pressure within the hydrogel. At the crack tip, we impose zero solvent flux: $q = 0$.

2.7 Power balance

As mentioned in the introduction, we are interested in analyzing the breakdown of dissipative contributions upon the toughness enhancement of the system. To this aim, we write the total power balance for the brittle layer-hydrogel composite as

$$P_t = \dot{E} + P_{\text{coh}} + P_v - P_s \quad (37)$$

where

$$\dot{E} = \frac{d}{dt} \int_{\mathcal{B}} \psi, \quad (38)$$

$$P_t = \int_{\partial_{\mathbf{u}} \mathcal{B}} \mathbf{S} \mathbf{m} \cdot \dot{\mathbf{u}}, \quad (39)$$

$$P_{\text{coh}} = \int_{\mathcal{J}^+} \sigma(\delta) \dot{\delta} = \int_{\mathcal{J}^-} \sigma(\delta) \dot{\delta}, \quad (40)$$

$$P_v = 2\eta \int_{\mathcal{V}_t} \|\operatorname{sym} \nabla \mathbf{v}\|^2 \approx 12\eta \int_{\mathcal{L}} \lambda \frac{q^2}{\delta^3}, \quad (41)$$

$$P_s = - \int_{\mathcal{B}^s} \mathbf{h} \cdot \nabla \mu \quad (42)$$

are the total free energy of the system, the mechanical power expended by the applied tractions, the power expended by the cohesive tractions in fracture processes,

the power dissipated by transport of the fluid within the cracks, and the power dissipated by solvent transport within the hydrogel, respectively. Notice that there is no contribution associated to solvent transport across the boundary of the system because we have assumed the hydrogel to be impermeable for short times.

2.8 Weak form of the governing equations

In order to solve the problem set in the previous paragraphs by means of the finite element method, we recast the governing equations (12), (25)₁, (28), and (29) in weak form. The continuity of the solvent pressure at the crack inlet (subscript ‘in’) is enforced through the Lagrange multiplier g corresponding to the (concentrated) solvent mass flux per unit length. Then, the weak formulation of the problem reads: find p_f , \mathbf{u} , c , p and g such that the following equations

$$\int_{\mathcal{L}} \left(-\frac{\partial}{\partial t} (\delta\lambda) \tilde{p}_f + q \frac{\partial \tilde{p}_f}{\partial X_2} \right) + \Omega(g \tilde{p}_f)_{\text{in}} = 0, \quad (43)$$

$$\int_{\mathcal{B}} \mathbf{S} \cdot \nabla \tilde{\mathbf{u}} = \int_{\mathcal{J}^+} \mathbf{s}^+ \cdot \tilde{\mathbf{u}}^+ + \int_{\mathcal{J}^-} \mathbf{s}^- \cdot \tilde{\mathbf{u}}^-, \quad (44)$$

$$\int_{\mathcal{B}^s} (J - 1 - \Omega c + \Omega c_o) \tilde{p} = 0, \quad (45)$$

$$\int_{\mathcal{B}^s} (-\dot{c} \tilde{\mu} + \mathbf{h} \cdot \nabla \tilde{\mu}) - (g \tilde{\mu})_{\text{in}} = 0, \quad (46)$$

$$(\mu(c, p) - \Omega p_f)_{\text{in}} \tilde{g} = 0, \quad (47)$$

hold for arbitrary test fields (indicated with a superposed tilde) compatible with the Dirichlet conditions. The weak form of the governing equations is complemented by Eq. (20) and by the constitutive relations (33)-(35). This, and the corresponding boundary conditions, have been implemented into the finite element software COMSOL Multiphysics v5.2. Specifically, quadratic shape functions were used for all the unknown fields, except for the pressure field p , which was discretized using linear shape functions to get a reliable approximation of the volume constraint. The implicit, variable-order (from 1 to 5), adaptive step-size BDF solver was used for time-stepping. A quasi-Newton algorithm was employed to solve iteratively the non-linear algebraic system resulting from the finite element discretization at each time step. The direct solver MUMPS was chosen for the solution of the linearized system at each iteration. The mesh consisted of about 2×10^4 triangular elements corresponding to about 10^5 degrees of freedom, and was made symmetric with respect to the vertical symmetry axis of the computational domain to avoid introducing any numerical bias in the distribution of solvent flux between the cracks. Local mesh refinement

along the crack paths was performed to ensure that the cohesive zones were discretized with at least 20 elements. Notice that the faces \mathcal{J}^+ and \mathcal{J}^- are modeled as distinct (but overlapping) segments in the numerical model where the tractions \mathbf{s}^\pm are prescribed.

3 Numerical results

We apply the just described model to the analysis of the ideal case of a brittle layer containing two edge pre-cracks of initial length a_o and separation s . To break symmetry, we introduce a 10% difference between the toughnesses Γ_R and Γ_L of the right and left crack, respectively.

Dimensional analysis dictates that any relevant quantity, such as the total dissipated energy, has to depend on the following set of dimensionless groups: h/a_o , h/s , h/H , G_e/Λ , $G_d/J_o^{1/3}G_e$, $G_d\Omega/\mathcal{R}T$, Γ_R/Γ_L , χ , $\mu_o/\mathcal{R}T$, $|\dot{\epsilon}|s^2/D$, τ , $G_e a_o/\Gamma_L$, $\Gamma_L a_o/\eta D$. Here, H is the thickness of the hydrogel substrate, whereas $\tau = |\dot{\epsilon}|t$ is a dimensionless measure of time.

For the computational study, we set the values of part of these dimensionless groups as reported in Table 1. The first three are geometrical ratios, while the following three are related to the elastic moduli of the brittle layer and the hydrogel. We recall from [11] that crack propagation under compression (tension) requires the ratio $3G_d/4J_o^{1/3}G_e$ between the moduli of the hydrogel and the brittle layer to be higher (lower) than 1/2. In compression, for instance, this condition allows the solvent pressure within the cracks to overcome the compressive stresses due to the remotely applied strain. Thus, we set $G_d/J_o^{1/3}G_e = 0.38$, $G_d\Omega/\mathcal{R}T = 6 \times 10^{-5}$ to study cracking in tension, and $G_d/J_o^{1/3}G_e = 3.82$, $G_d\Omega/\mathcal{R}T = 4 \times 10^{-4}$ for the simulations of cracking in compression. Given χ , $G_d\Omega/\mathcal{R}T$ and $\mu_o/\mathcal{R}T$, the initial swelling ratio J_o is computed from Eq. (36). Eventually, by allowing the remaining parameters to vary, we

Table 1: Values of the dimensionless groups used in the numerical simulations.

Parameter	Value
h/a_o	10
h/s	5/3
h/H	0.04
G_e/Λ	0.02
Γ_R/Γ_L	0.9
χ	0.46
$\mu_o/\mathcal{R}T$	0
$G_e a_o/\Gamma_L$	6.7
$\Gamma_L a_o/\eta D$	2.5

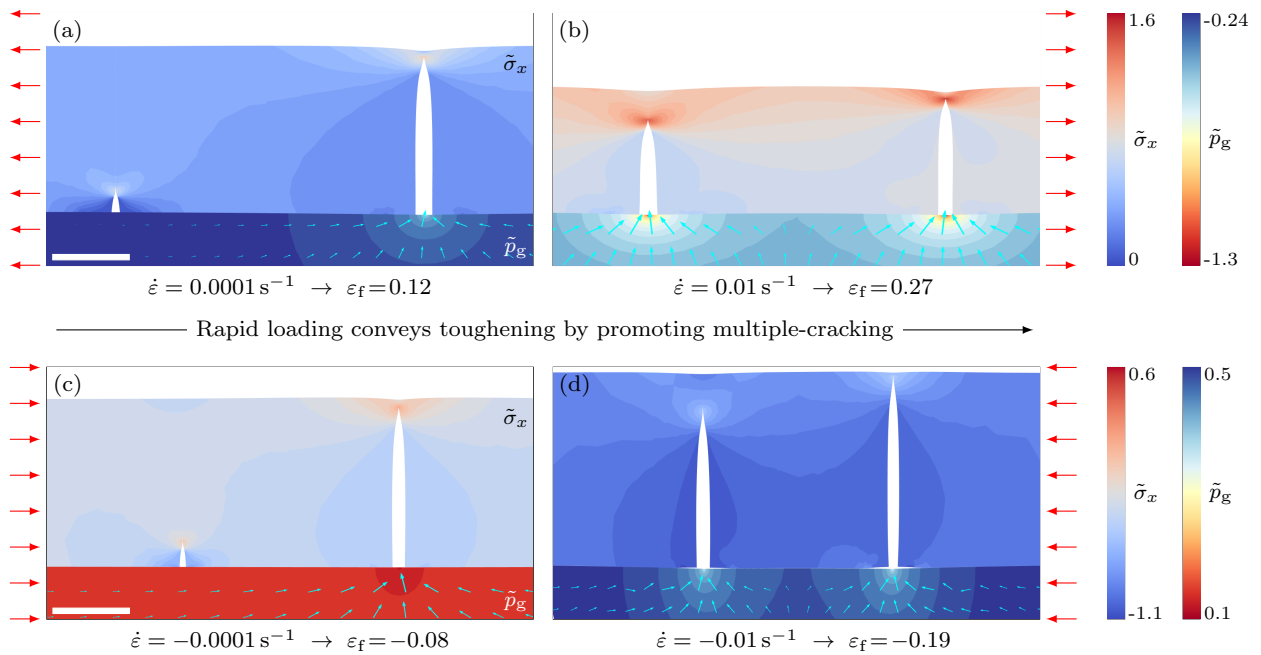


Fig. 2: Snapshots of the system at failure as obtained from numerical simulations, for tensile (a),(b) and compressive (c),(d) strains. The transition from localized (a),(c) to distributed (b),(d) fracture corresponds to increasing values of the dimensionless group $\Pi = |\dot{\epsilon}|s^2/D$, here obtained by varying the strain rate. Contours represent the longitudinal stress $\tilde{\sigma}_x = \mathbf{SF}^T \mathbf{e}_1 \cdot \mathbf{e}_1 / JG_e$ in the brittle layer and the solvent pressure $\tilde{p}_g = \mu J_o^{1/3} / (\Omega G_d)$ within the hydrogel, while ϵ_f is the value of the applied strain at failure. The scale bar is $5 \mu\text{m}$, whereas the arrows in the hydrogel represent the solvent flux.

regard a dimensionless, physical quantity as a function of $\Pi = |\dot{\epsilon}|s^2/D$ and τ .

We now focus on the significance of the dimensionless group of Π upon the fracture behavior of the system. In a previous study [11], we have demonstrated that decreased diffusivity conveys toughening by promoting multiple-cracking. Here, in light of dimensional analysis, we deduce that the transition from localized to distributed fracture is actually controlled by the dimensionless group Π . The results in Fig. 2, where we report snapshots of the system at failure, confirm that such a transition is associated to an *increase* in the value of Π , both in tension and compression. Further evidence is provided in Figs. 3(a),(d), where the relative length difference $\Delta\tilde{a} = (a_R - a_L)/a_o$ between the cracks sharply grows for $\Pi = 2 \times 10^{-7}$, as rapid, single crack propagation occurs. Therefore, multiple-cracking may be obtained by either an increase in strain rate or separation between the cracks, or by a decrease in diffusivity of the solvent within the hydrogel.

The just described behavior may be rationalized as follows. In a brittle solid, the mechanism of crack tip shielding is responsible for localized, dynamic fracture. Any offset between the crack tips implies a progressive decrease (increase) in the energy release rate of the

lagging (leading) crack [12]. In the presence of the hydrogel, crack advance always requires solvent transport and is thereby controlled by its diffusivity. Hence, continued loading that is rapid with respect to the kinetics of solvent transport can favour distributed cracking by sustaining the driving force of both fractures.

Multiple-cracking results in an enhancement of the macroscopic toughness of the system. To quantify such an enhancement, we report in Figs. 3(b),(e) the dimensionless mechanical work $\tilde{W}_t = W_t / (G_e h + G_d H)$ performed on the system as computed by time-integration of Eq. (39). Notice that, an increase of two orders of magnitude in the strain rate produces more than a three-fold increase in the work at failure, both in tension and in compression. This trend is motivated by the increase of the dissipation $\tilde{E}_d = E_d / (\Gamma_L + \Gamma_R) a_o$ that accompanies distributed cracking, see Figs. 3(c),(f). Here, E_d collects the time-integrals of the powers dissipated by fracture, Eq. (40), and solvent transport, Eq. (42), as the energy dissipated by viscous flow within the cracks is comparably negligible. Interestingly, we notice that dissipation due to solvent transport mainly contributes to such an increase in \tilde{E}_d . As a consequence, the relative contribution of the work of fracture to \tilde{E}_d decreases in the transition from localized to distributed cracking.

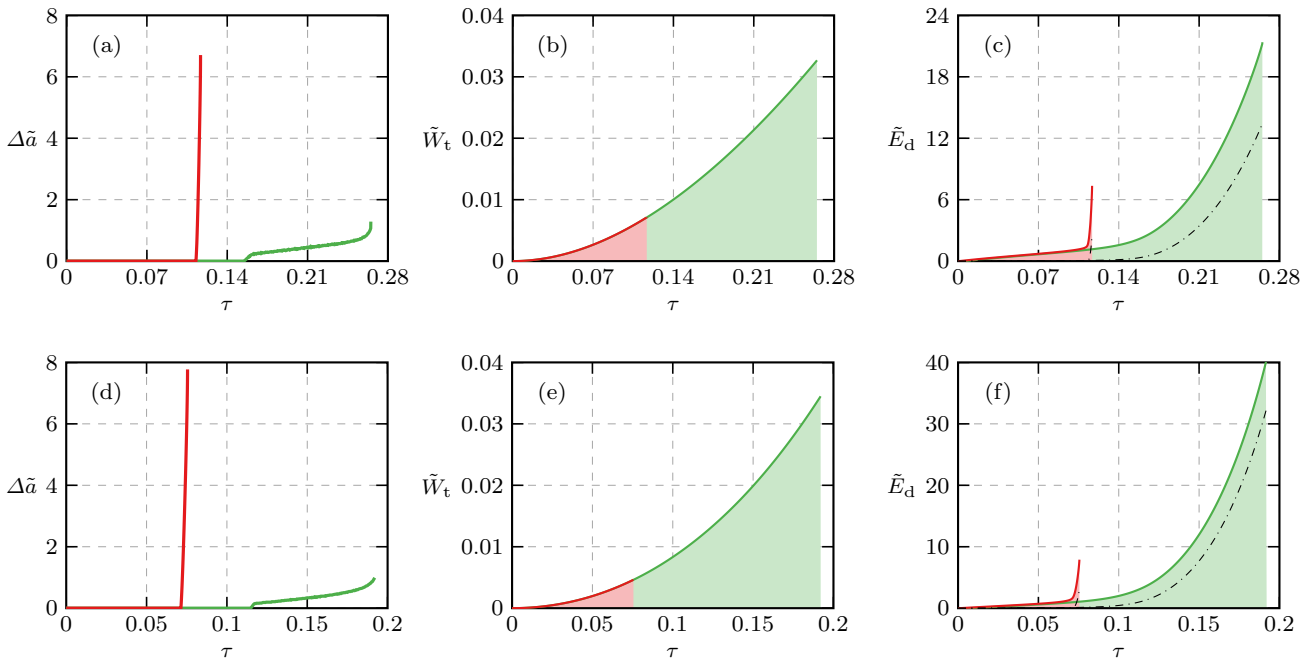


Fig. 3: Dynamics and energetics of crack propagation in tension (a)-(c) and compression (d)-(f), for $|\dot{\epsilon}| = 0.0001 \text{ s}^{-1}$ (red, $\Pi = 2 \times 10^{-7}$) and $|\dot{\epsilon}| = 0.01 \text{ s}^{-1}$ (green, $\Pi = 2 \times 10^{-5}$). The plots show the relative crack length difference (a),(d), the external work performed on the system (b),(e) and the total dissipated energy (c),(f) as a function of time until failure. The dash-dotted line in (c),(f) represents the dissipated energy associated to solvent transport.

4 Conclusions

Motivated by recent experimental results on the fracture of epithelial cell monolayers adhered to an hydrogel substrate, a model has been developed that allows for the analysis of hydraulically driven cracking of this system. We have shown that such a composite can develop a toughening mechanism that relies on the multiple-cracking of the brittle phase. In particular, we have demonstrated that the transition from localized to distributed cracking is determined by either a decrease in solvent diffusivity or an increase in loading rate. A detailed energy analysis has quantified the dissipative processes associated with multiple-cracking. Future work will investigate upon the possibility of implementing this concept in the engineering of flaw-tolerant, biomimetic materials.

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Compliance with ethical standards The authors declare that they have no conflict of interest.

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