

# The Shape of Dunes in the World's Big Rivers

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## ABSTRACT

Dunes are present in all the world's big rivers and form critical agents of bedload transport, constitute appreciable sources of bed roughness and flow resistance, and generate stratification that is the most common depositional element of ancient alluvium. Yet our current models of dunes are conditioned by the geometry of bedforms observed in small rivers and laboratory experiments, and in which the downstream leeside angle is often assumed to be at the angle-of-repose. Here we show, using high-resolution bathymetry from a range of the world's great rivers, that dunes are instead characterized predominantly by low-angle leeside slopes ( $<10^\circ$ ), complex leeside shapes where the steepest portion is near the base of the leeside slope, a mean wavelength:height ratio greater than 100, and a height that is often only 10% of the local flow depth. This radically different shape of dunes in the world's big rivers demands that we incorporate such geometries into predictions of flow resistance and water levels, rethink the scaling relationship of dunes when reconstructing alluvial palaeoflow depths, and calls for a fundamental reappraisal of the character, and origin, of low-angle cross-stratification within ancient alluvial sediments.

## Introduction

Dunes are a ubiquitous morphological element in all rivers that possess bed material grain sizes ranging from sands to gravels<sup>1</sup>, and through their topographic steering of flow are a major source of turbulence within rivers<sup>2</sup>. Sediment transport associated with dunes occurs through dune migration<sup>1,3-5</sup> and by sediment suspension linked to large-scale, dune-related, turbulence. In addition, larger alluvial barforms are created by dune migration and amalgamation, to form areas of hydraulic<sup>1,6</sup>, sedimentary<sup>7,8</sup> and ecological<sup>9,10</sup> heterogeneity within a river, which exert a major control on the location of erosion and deposition and the habitat functioning of river beds. As such, dunes exert a major influence on a range of riverine processes, from grain transport to large-scale channel planform change<sup>3,11-13</sup>.

Our understanding of the fluid dynamics and sediment transport characteristics of alluvial dunes has been guided largely by the study of small dunes in both the laboratory and field<sup>14-17</sup>, with only a few studies having examined flow over dunes in big rivers where dunes with leesides less than the angle-of-repose are present<sup>18-21</sup>, and where multiple scales of bedform interact to create complex dune shapes<sup>6,12,22,23</sup>. Research has also shown that dunes with more complex shaped leeside slopes

possess a different flow dynamics to dunes with high-angle, simple leesides<sup>1,19,21,24</sup>. Specifically, low-angle dunes (defined herein as dunes with a leeside angle less than  $10^\circ$ ), do not possess a zone of permanent flow separation, and dunes with leeside angles less than  $4^\circ$  have been argued to not exhibit flow separation at all<sup>21,24-28</sup>, which consequently causes lower energy losses arising from turbulent eddy shedding in the shear layer between the recirculating flow in the dune leeside and overlying free flow<sup>1</sup>. Furthermore, a scaling relationship between formative flow depth and dune height is often assumed when predicting dune dimensions in modern channels, and reconstructing dune size and flow depth in paleohydraulic reconstructions of ancient riverine sediments<sup>8,16,29-31</sup>. However, recent work<sup>32</sup> has re-evaluated such dune scaling relationships by compiling data from both laboratory and field datasets ( $\sim 50$ ) and concluded that there is a change in dune morphology from an asymmetric to a more symmetric shape and from high to lower angle leesides in shallow ( $< 2.5$  m) and deep flows, respectively. This has been attributed to a likely change in the dominant processes controlling dune formation as dunes become larger, and thus different scaling relationships have been suggested for shallow and deep flows<sup>32</sup>.

However, we presently lack a detailed quantification of the morphology of dunes within large alluvial channels in order to assess exactly what shape of dunes are most common in the world's biggest rivers, and thereby assess the potential importance of dune shape in predicting the behavior of modern rivers and reconstructing the paleohydraulics of ancient fluvial channels. Here, we present and analyze a unique dataset that permits quantification of the shape of dunes in six of the world's major rivers - the Amazon, Mekong, Mississippi, Missouri, Paraná and Waal rivers. This analysis reveals the dominance of low-angle dunes with a complex leeside shape, and highlights that current models of dunes in modern and ancient sediments must better recognize and incorporate the fundamental geometry of these ubiquitous morphological elements.

## Methods and Field Data

Field data from six of the world's major rivers, the Amazon, Mekong, Mississippi, Missouri, Paraná and Waal rivers, were acquired using a multi-beam echosounder (MBES). During data acquisition, a MBES is attached to a moving vessel and multiple (up to 512) acoustic beams are transmitted through the water column to the river bed, thus forming a beam swath as the boat traverses the river. The travel time of the signal from the MBES transmitter to the riverbed and back to the receiver is used to calculate the water depth given a simultaneous measurement of the acoustic velocity in water. The position of the vessel is resolved via a Differential Global Positioning System (DGPS) and an inertial motion unit to correct for pitch, roll and heave, thus yielding bathymetric measurements of centimetric resolution in the x,y, and z components. The MBES surveys reported herein (see Supplementary Figure 1) range in their spatial extent between  $0.1 \text{ km}^2$  (Missouri River) -  $6 \text{ km}^2$  (Amazon River) and survey acquisition time ranged from one day (Missouri River) to three days (Amazon River) depending on survey extent and field conditions. A bedform analysis method for bathymetric information (BAMBI) was developed and applied to the MBES data and quantified the shape of dunes in each river (see Supplementary Methods). Shape descriptors of each dune include dune height, wavelength, average leeside angle, maximum slope angle on the leeside, and the location of the maximum slope, as well as flow depth at each dune. From the MBES data, bedforms are measured across the width of the entire survey area at spanwise steps equal to the MBES grid resolution (0.5 m in all cases), and so in this way one dune will be measured across its entire width. In addition to MBES data, dune shapes from data acquired by a single echosounder system in the Huang He (Yellow) River measured using the BAMBI method and dune data measured by hand from single beam echo sounder surveys of the Jamuna (Brahmaputra) River<sup>18</sup> are presented (Table S1 and Supplementary Figures 2 and 3) as additional data for comparison to dune leeside angles quantified from MBES data.

## Dune Leeside Angle and Shape

Histograms of mean leeside angle possess a peak at  $c. 10^\circ$  (peaks range  $10.2-16.1^\circ$ ; Figure 1a-f), an average standard deviation of  $5.72^\circ$ , and are skewed (about  $1.4^\circ$  on average) towards lower leeside values, with 48 to 90% of the dunes in each river possessing leeside slopes less than  $15^\circ$  (see Table S1). Single echosounder lines (Supplementary Figures 2 and 3) also reveal a similar relation in the Jamuna River<sup>18</sup> ( $n = 770$ ), where dune leeside angles were on average  $10.2^\circ$ , and in the Huang He River where dunes have a mean leeside angle of  $c. 2.0^\circ$  ( $n = 97$ ). The histograms of maximum leeside angle show peaks around  $20^\circ$  (Figure 1h-m), with the histogram shapes having a larger standard deviation about the mean, ranging from  $5.5$  to  $9.9^\circ$ , and with 31% of leeside angles, on average, being between  $20$  and  $30^\circ$  (see Table S1).

Plotting this unique dataset for mean and maximum leeside angle in big rivers in one histogram shows a good fit to a gamma relationship rather than a normal fit (Figure 1g), confirming previous research that a positively skewed probability density function is the best representation of dune morphologic data<sup>33</sup>. The average mean and maximum leeside angles are  $13.4^\circ$  and  $20.5^\circ$ , respectively. The composite histogram of mean leeside angle reveals that 75.4% of all dunes measured herein possess leeside angles less than  $15^\circ$ . For the composite histogram of maximum leeside angle, a peak is present at  $20.5^\circ$ , with maximum leeside angles ranging from  $10 - 30^\circ$ , and with 25.2% of all leesides being between  $20-30^\circ$  (refer to shaded area in Figure 1). These higher values are more representative of traditional angle-of-repose leeside dune slopes, although it is important to highlight that this value of maximum angle only represents a singular maximum slope on the entire leeside, whereas the mean angle represents the average of all slopes on the leeside.

The overlaps between the histograms of mean and maximum leeside angle suggest that the singular high slope values reported in the maximum leeside histogram are not representative of the entire leeside slope. Thus, the position of the maximum leeside angle along the leeside slope is critical, since these steeper slopes will influence the flow dynamics, and especially the production of flow separation, in the dune leeside that is instrumental to flow resistance and energy loss associated with the dune. The present data uniquely allow the position of the maximum leeside slope to be quantified, and is expressed herein as the height of the maximum leeside slope,  $h$ , with respect to the total dune height,  $H$ , from the base of the leeslope (Figure 2a). This data (Figure 2b) shows that the position of the maximum leeside slope is dominantly at 0.3-0.4  $h/H$  (i.e. in the bottom half of the leeside slope) and the distribution is slightly shifted towards lower values, such that the maximum leeside slope is more commonly located  $<0.5 h/H$  (Figure 2b). These results thus demonstrate that even if the leeside is gently sloping at a mean of  $10^\circ$ , a maximum slope of  $20^\circ$  could be present on the dune leeside but would most likely be located towards the bottom half of the leeside. Importantly, the occurrence of higher angle slopes towards the base of the leeside will be far less influential in creating significant flow separation than if they were present at the top of the leeside slope.

### Dune Size and Potential for Flow Separation

Dune height ( $H$ ) plotted against flow depth ( $Y$ ) for each river (Figure 3) shows that in flow depths less than *c.* 5 meters,  $H=0.33Y$  represents the upper limit of dune height, but for all flow depths 82 % of all dunes fall below the  $H=0.10Y$  relation (see Table S2). In flow depths greater than 30 meters, 96% of dunes have heights at, or below, 5 meters ( $<0.167Y$ ). While dunes with heights up to 10 meters do exist in deep flows, such as those in the Amazon River, smaller dunes ( $H<0.10Y$ ) are much more common in such deep channels. This fact challenges the often made assumption that bigger rivers must be characterized by larger dunes. In addition, the wavelength:height ratio of dunes (Supplementary Figure 4) shows a wide range (mean values for individual rivers range from 69-170), with a mean and standard deviation for all rivers of 133 and 315 respectively.

The size of the flow separation zone in the dune leeside may be considered a function of dune height in relation to flow depth (that determines flow velocity at the crest), leeside slope angle and additionally the location of the maximum leeside slope. Plotting mean dune leeside angle against the submerged dune height ( $H/Y$ ; Figure 4) for maximum leeside angles located in the top and bottom half of the dune height (Figs 4a and 4b respectively) allows consideration of the potential for flow separation associated with dunes in the world's big rivers. In addition, Figure 4 uses past experimental data to highlight: i) dunes where permanent flow separation is absent (leeside angles below  $10^\circ$ <sup>21,24-28</sup>), ii) the onset of permanent flow separation, which is dependent on  $H/Y$  and occurs over a range of leeside angles (defined here by a linear interpolation between three experimental test cases<sup>27</sup>), and iii) where fully developed flow separation is present and associated with dunes that possess leeside angles greater than  $24^\circ$ <sup>27</sup>. The majority (93.8 %) of dunes with maximum leeside angles between  $11-18^\circ$  fall below the experimentally derived line where the onset of permanent flow separation has been observed, and only a very low percentage of dunes ( $<1\%$ ) exhibit permanent flow separation (Fig. 4). For dunes with leeside slopes less than  $10^\circ$ , where there is likely no permanent flow separation, the maximum slopes are more common in the lower part of the dune leeside (44%) than in dunes with maximum slopes located in the upper part of the leeside (36%).

This unique dataset thus illustrates that the overwhelming majority of dunes in the world's big rivers have low-angle leesides (mean *c.*  $10^\circ$ ) that are significantly less than the angle-of-repose, possess heights ( $H<0.1Y$ ) far less than commonly assumed with respect to the flow depth, and that even the steeper segments of their leesides occur predominantly towards the bottom of the leeside slope. These morphological characteristics, and their influence on fluid flow, have profound implications for the models of flow required for the most common bedform in the world's large rivers, how flow resistance is predicted and modelled in such channels and how the deposits of such dunes are recognized in ancient alluvial successions.

### Discussion

Although low-angle dunes with complex leeside shapes have been documented previously in the Brahmaputra<sup>18</sup>, Fraser<sup>20</sup> and Amazon<sup>34,35</sup> rivers, and their flow dynamics has received limited study using physical and numerical models<sup>21,25-28</sup>, the present results provide the most comprehensive analysis yet accomplished detailing the morphology of dunes in some of the world's biggest rivers. Our findings reveal the dominance of low-angle dunes and complex dune shapes, with 75% of dunes possessing leeside angles  $<14.9^\circ$ . These results demonstrate the ubiquity of such dunes and suggest that it is essential to account for their morphology when both modelling modern rivers and interpreting their deposits in ancient alluvial successions. Three implications arise from these contentions.

First, low-angle dunes will generate less turbulence than classic angle-of-repose dunes<sup>19,27</sup>, thereby lessening flow resistance caused by dune form roughness<sup>11,36-38</sup>. Parameterization of such roughness and the nature of flow separation<sup>37,38</sup> associated with low-angle dunes should thus be included in fluid dynamic models of alluvial channels<sup>39</sup>, and a composite PDF, such as that presented herein (Figure 1g), provides a desirable quantification in the absence of site-specific data in order to better represent such roughness. The present data also builds on previous work<sup>24</sup> that suggests dune leeside shape is complex, but further quantifies leeside shape by showing that the steepest sections of the leeside are predominantly nearer the leeside base, and not

near the top of the lee face. This again alludes to the lesser role of flow separation, and linked flow resistance, over such leesides. The processes that lead to complex leeside shapes likely revolve around bedform superimposition and amalgamation<sup>12,22,23</sup>, the possible influence of sediment in suspension<sup>40</sup>, together with the modifications to dune morphology associated with transitional dunes<sup>41,42</sup>, all of which may be greatly influenced by spatio-temporal changes in flow during flood hydrographs and the effects of bedform hysteresis<sup>42-46</sup>. Nevertheless, the dominance of dunes with these shapes in large rivers demonstrates their morphology must be reflected in models that seek to predict flow and sediment transport<sup>39</sup>, as well as the effects of such dunes on larger scale bar formation and channel development<sup>13</sup>.

Secondly, in the ancient alluvial record, dune cross-stratification has often been used to reconstruct flow depths<sup>8,30</sup>, and thus help constrain parameters such as channel size and flow discharge<sup>29,31,47</sup>, with the relationship between dune height and flow depth being pivotal in such paleohydraulic reconstructions. The present extensive dataset illustrates that, rather than assuming a relationship between flow depth and dune height of  $H \cong 0.25 - 0.33Y$  as in much past work<sup>47</sup>, it is better to adopt a value of  $H \cong 0.1Y$ . This value, together with a factor accounting for the preservation of the dune<sup>8,23,35,48</sup>, should be adopted to yield more realistic estimates of mean flow depths. This contention thus suggests that many past predictions of alluvial paleoflow depth based on dune height may have been underestimates, and highlights the need to obtain other independent estimates of flow depth where possible, such as from the thickness of channel fill sequences<sup>49</sup> or the height of larger-scale barform-generated stratification<sup>50</sup>.

Lastly, the dominance of low-angle dune leesides in the world's large rivers suggests that the recognition, in both outcrop and core, of such dunes in ancient alluvial successions may require that far more attention be devoted to low-angle stratification. Our data illustrate that low leeside angles are very common, with dips of only a few degrees often being present (Figs 1, 4), and thus low-angle stratification, which may appear essentially flat, especially in core, may require greater consideration in its interpretation. Such low-angle surfaces in alluvial successions may be simply the product of low-angle dunes, rather than conditions representative of upper-stage plane bed conditions<sup>41,51</sup>. Where dunes are large, with leesides many meters or tens of meters long, such low-angle stratification may be extremely difficult to recognize in outcrop, and demands careful tracing of individual laminae, and the subtle erosional surfaces between superimposed low-angle dunes. It is also apparent that complex dune leesides, and the presence of multiple scales of dunes, are commonplace in the world's large rivers, and suggests that the key to establishing the scale of a paleoflow and alluvial channel size may lie in interpretations of the smaller, cross-stratified cosets and the erosional surfaces between them<sup>35</sup>. Our work demonstrates that it is essential to recognize the presence, scale and dominance of low-angle complex dunes within the majority of alluvial channels, if we are to better account for their influence on the dynamics of contemporary river channels, and their recognition in ancient alluvial sequences.

## Supplementary Methods

Recently, several methods to automate the detection and measurement of bedform morphology have been proposed using geostatistical and signal-processing techniques<sup>52,53</sup>. These methods are often unable to account for complexities in bedform morphology, such as leeside shape, and the data outputs are typically statistical values that represent mathematical fits to the raw data rather than measurements of the raw data. In addition, most methods only focus on analyzing bedforms taken from a limited number of profile lines and, whilst a few methods can analyze the entire bathymetric bedform field, most of these methods are computationally expensive. Thus, there exists a need for a bedform analysis method that utilizes the raw bathymetric data, treats the bedforms as having a complex morphology, outputs values that represent such complexity, and is computationally efficient and robust. Such a method will be invaluable in quantifying bedform shape from high-resolution bathymetric datasets and allow the user to gain better knowledge of spatially variable bedforms. In the research reported herein, a Bedform Analysis Method for Bathymetric Information (BAMBI) was developed to automatically measure the geometric characteristics of dunes in big rivers using multi-beam echosounder data acquired for several large rivers. The BAMBI can also be used to measure dunes from single echosounder lines, but additional steps must be made so that the lines are in a matrix format as the BAMBI begins by defining each data point as being related to the eight other surrounding points in a 3x3 window. BAMBI works at the resolution of the data and in the present analysis increased data output from a few hundred measurements to over two hundred and fifty thousand data points, whilst also decreasing data measurement time to a few hours of code run time. Thus, the BAMBI allowed for a highly resolved and spatially extensive analysis herein of six of the world's big rivers to yield a unique new quantification.

In BAMBI (see Figure S5 for flow chart of methodology), the inputs required are an ASCII file of river bathymetry gathered via multi-beam echosounder, a general downstream estimate of flow direction in azimuthal coordinates of the river, and a flow looking angle (the deviation around the flow direction that defines what is considered a downstream-facing slope; set at default as 40°). In the case that MBES xyz data is not available and single echosounder lines must be used, the lines must be used to construct an artificial matrix. Here the lines, with their georeferenced x,y, locations, must be spaced equally in the x and y directions and stacked in a matrix by groups of three. In this way, the matrix will have three columns of NaN, followed by three columns of the echosounder line repeated, and three more columns of NaN. In addition, all echosounder lines must be

aligned with the flow direction. In the case that echosounder lines are not perfectly straight, the user must decide the best way to interpolate the data onto a straight line. All lines can be placed in the same matrix, as long as packages of three NaN columns straddle each package of three repeated echosounder lines.

The output of the analysis method is a text file of 9 columns: X coordinate (latitude), Y coordinate (longitude), dune height, dune mean leeside angle, dune maximum leeside angle, leeside slope direction, dune wavelength, dune flow depth (taken at the crest), and the fractional height of the maximum slope on the leeside for each dune measured across the river width at steps of the data resolution (herein 0.5 meters). To begin, the raw bathymetric data is rotated so that the grid is aligned with the flow direction oriented to  $0^\circ$ , or in other words, the grid is rotated to  $\theta = -\text{flow direction} = 0$ . Now, the grid can be analyzed by column, which coincides with individual profile lines in the flow direction. The first step in the analysis method is to create slope and aspect grids from the rotated raw bathymetric depth data by using a 3x3 floating window [a,b,c; d,e,f; g,h,i]. This computes slope and aspect for each e cell as the window moves through the grid (cellsize equal in x and y) in the following way, where x and y are in a 2D matrix, and z is the third dimension:

$$[dz/dx] = ((c + 2f + i) - (a + 2d + g)) / (8 * x_{cellsize}) \quad (1a)$$

$$[dz/dy] = ((g + 2h + i) - (a + 2b + c)) / (8 * y_{cellsize}) \quad (1b)$$

$$rise\_run = \sqrt{[dz/dx]^2 + [dz/dy]^2} \quad (1c)$$

$$slope\_degrees = ATAN(rise\_run) * 57.29578 \quad (1d)$$

$$aspect = 57.29578 * ATAN2([dz/dy], -[dz/dx]) \quad (1e)$$

$$\begin{aligned} &\text{if} && aspect < 0, cell = 90.0 - aspect \\ &\text{else if} && aspect > 90.0, cell = 360.0 - aspect + 90.0 \\ &\text{else} && cell = 90.0 - aspect \end{aligned} \quad (1f)$$

Once the slope and aspect grids are computed, a leeside cell is defined as a cell with aspect direction in the range of the flow direction  $\pm$  the flow looking angle. All other cells are defined as stoss cells. Thus, a crest location is where a cell changes from stoss to lee side cell and a trough is where a cell changes from a lee to a stoss side cell. Dune height is then computed as the difference between the crest and the following trough cell depth. The dune mean leeside angle is computed as the average of all consecutive lee cell values in the dune leeside, whilst the maximum leeside angle is taken as the singular, maximum lee cell value in the dune leeside. The fractional height of the maximum leeside angle is then computed as the cell height of the maximum lee cell divided by the entire leeside height (dune height) of the dune. At this point, information is computed for dunes of all scales (i.e. superimposed and larger formative dunes), and thus a bedform threshold is applied that is the mean plus the standard deviation of all dune heights computed within the MBES survey. This is conducted under the assumption that smaller scale bedforms are more common in the river and these values shift the bedform height distribution to be peaked at lower values. Once this threshold is found, all dunes that have heights less than the threshold are saved separately as 'small' dunes. These bedforms commonly represent small, superimposed dunes. The remaining dunes are then assumed to be the larger formative dunes in the river. Once the formative scale dunes have been defined, the dune wavelength is computed as the distance between the troughs that bracket the formative dunes. This is also applied for the separate grid of smaller scale dunes within BAMBI.

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## Author contributions statement

J.C. and J.B. conceived the study and identified the potential datasets to be analyzed. J.C. developed the BAMBI code from initial conceptual ideas of J.B., and conducted the analysis and data plotting. All authors provided bathymetric data. J.C., J.B. and T.vD. wrote the initial manuscript that was then reviewed and edited by all authors.

## Additional information

To include, in this order: **Accession codes** (where applicable); **Competing financial interests** (mandatory statement).

The corresponding author is responsible for submitting a [competing financial interests statement](#) on behalf of all authors of the paper. This statement must be included in the submitted article file.

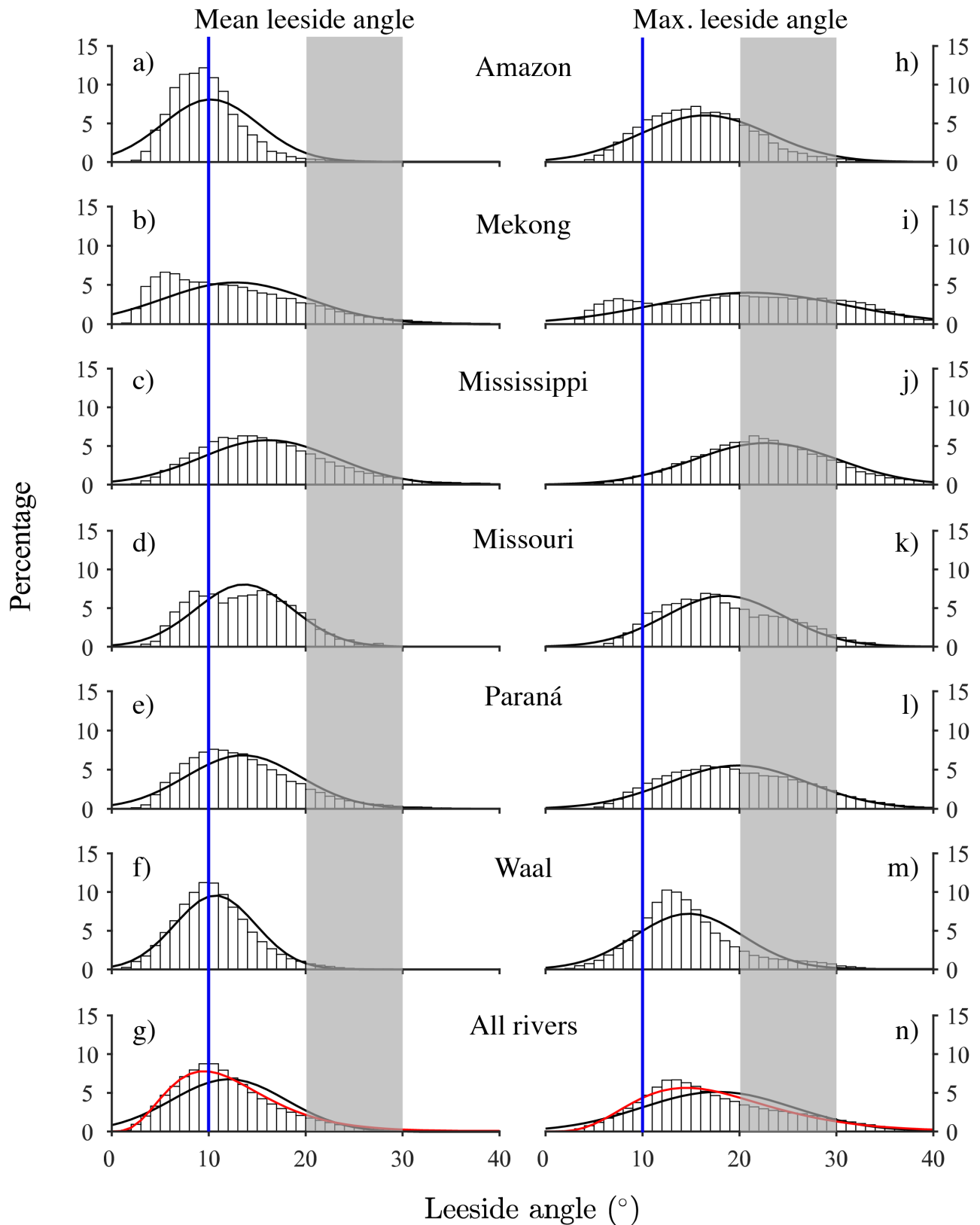
		N total	Mean	Standard Deviation	Variance	Skewness	Kurtosis	P90	P95	Less than 15° (%)	Between 20 & 30° (%)
<b>Amazon</b>	Mean Lee	15244	10.20	4.94	24.37	3.52	22.25	14.69	17.10	90.84	
	Max Lee	15244	16.45	6.63	43.90	1.91	8.45	23.42	26.60		20.70
<b>Mekong</b>	Mean Lee	53648	12.82	7.51	56.46	1.17	2.46	22.79	26.60	66.49	
	Max Lee	53648	21.06	9.91	98.20	0.33	0.04	33.54	36.29		33.35
<b>Mississippi</b>	Mean Lee	26934	16.10	6.91	47.81	1.00	2.06	24.92	28.52	48.74	
	Max Lee	26934	22.76	7.38	54.45	0.62	1.32	31.74	35.29		48.98
<b>Missouri</b>	Mean Lee	4530	13.65	4.96	24.62	0.33	-0.30	20.20	21.84	59.80	
	Max Lee	4530	18.43	6.08	36.95	0.38	-0.47	27.04	29.06		33.66
<b>Paraná</b>	Mean Lee	39917	13.53	5.84	34.10	1.08	2.40	21.09	24.22	65.58	
	Max Lee	39917	19.90	7.19	51.73	0.49	0.21	29.52	32.39		37.03
<b>Waal</b>	Mean Lee	124836	10.69	4.17	17.41	1.26	7.10	15.85	17.97	86.86	
	Max Lee	124836	14.77	5.55	30.82	1.29	4.53	22.25	26.06		13.12
<b>Average</b>	Mean Lee	–	12.83	5.72	34.13	1.39	6.00	19.92	22.71	69.72	
	Max Lee	–	18.89	7.12	52.68	0.84	2.35	27.92	30.95		31.14
<b>All compiled data</b>	Mean Lee	265109	12.12	5.89	34.66	1.48	4.71	19.65	22.96	75.43	
	Max Lee	265109	17.79	7.78	60.60	0.95	1.54	28.68	32.08		25.24
<b>Jamuna</b>	Mean Lee	770	10.20	16.56	–	–	–	–	–	–	–
	Max Lee	–	–	–	–	–	–	–	–	–	–
<b>Huang He</b>	Mean Lee	97	2.02	1.48	–	–	–	–	–	–	–
	Max Lee	97	4.03	3.00	–	–	–	–	–	–	–

**Table S1.** Statistics for mean and maximum leesides in each river and all rivers compiled

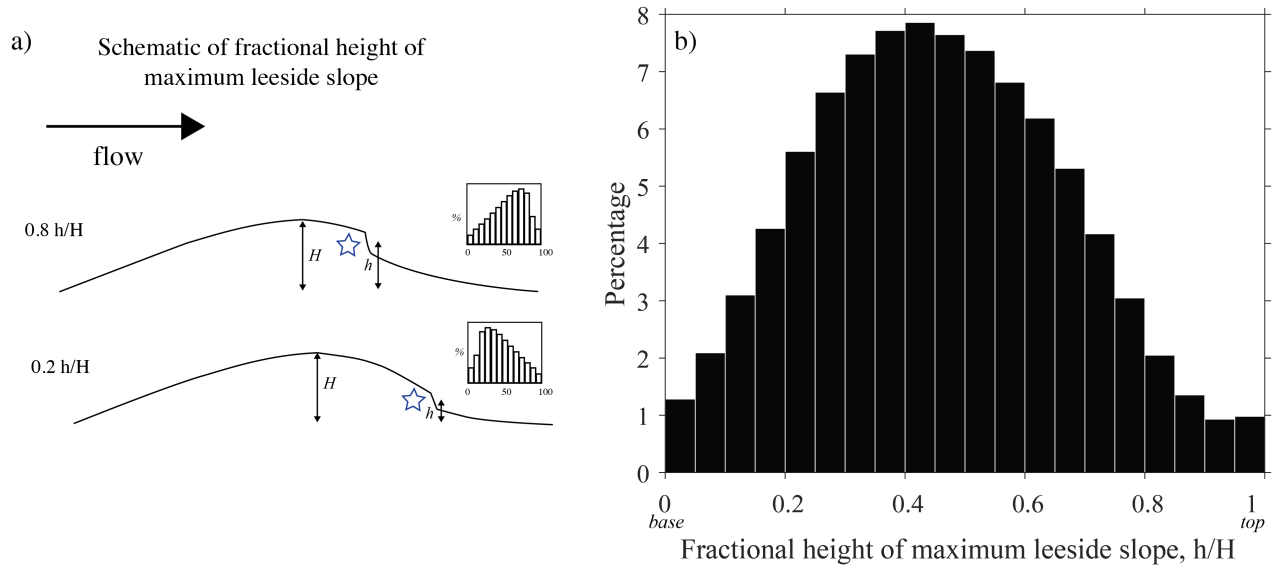
	N total	Dune height < 0.1Y (%)
<b>Amazon</b>	15244	98.58
<b>Mekong</b>	53648	88.83
<b>Mississippi</b>	26934	91.52
<b>Missouri</b>	4530	39.85
<b>Paraná</b>	39917	63.69
<b>Waal</b>	124836	84.27
<b>Average</b>	44185	77.79
<b>All compiled data</b>	140273	82.89

**Table S2.** Percentage of dunes with heights that are less than 1/10 flow depth

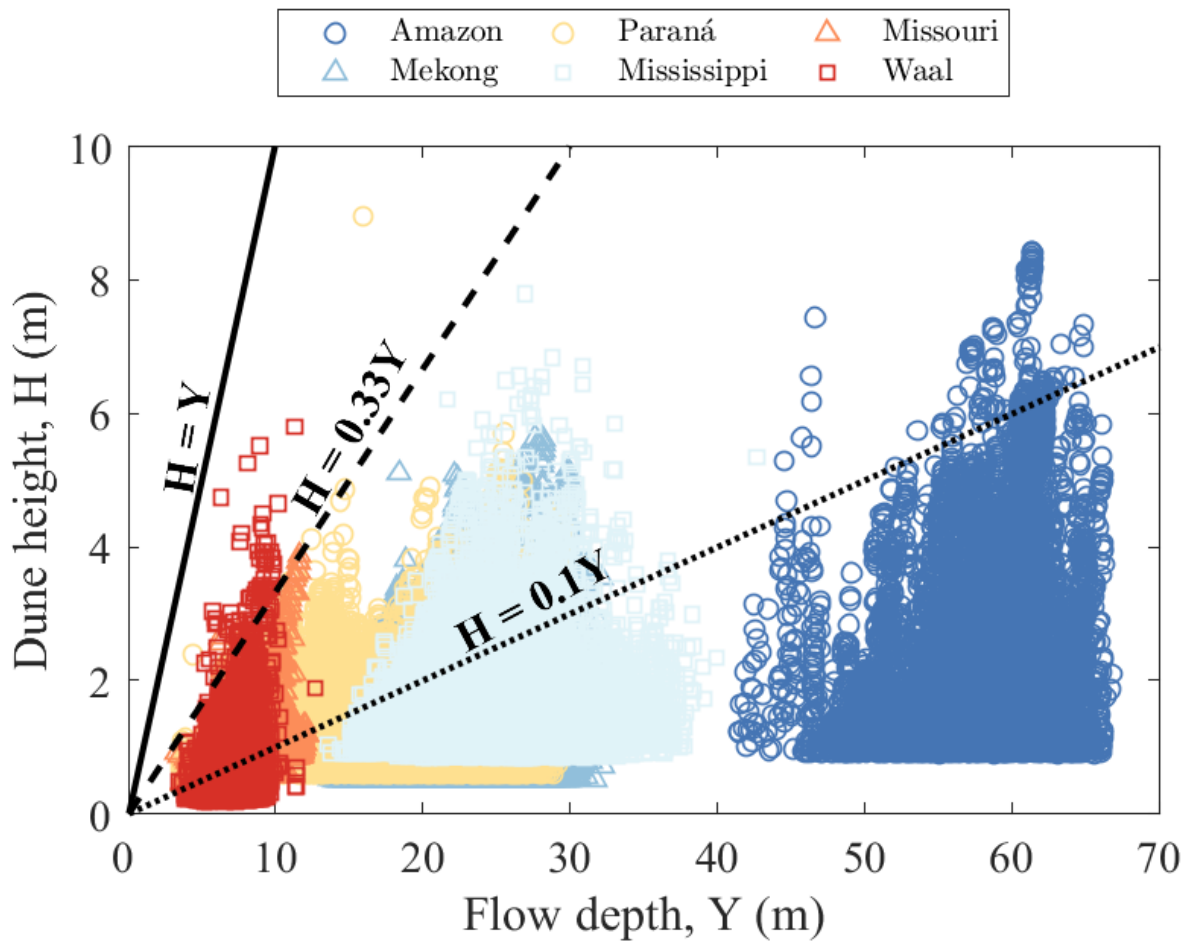




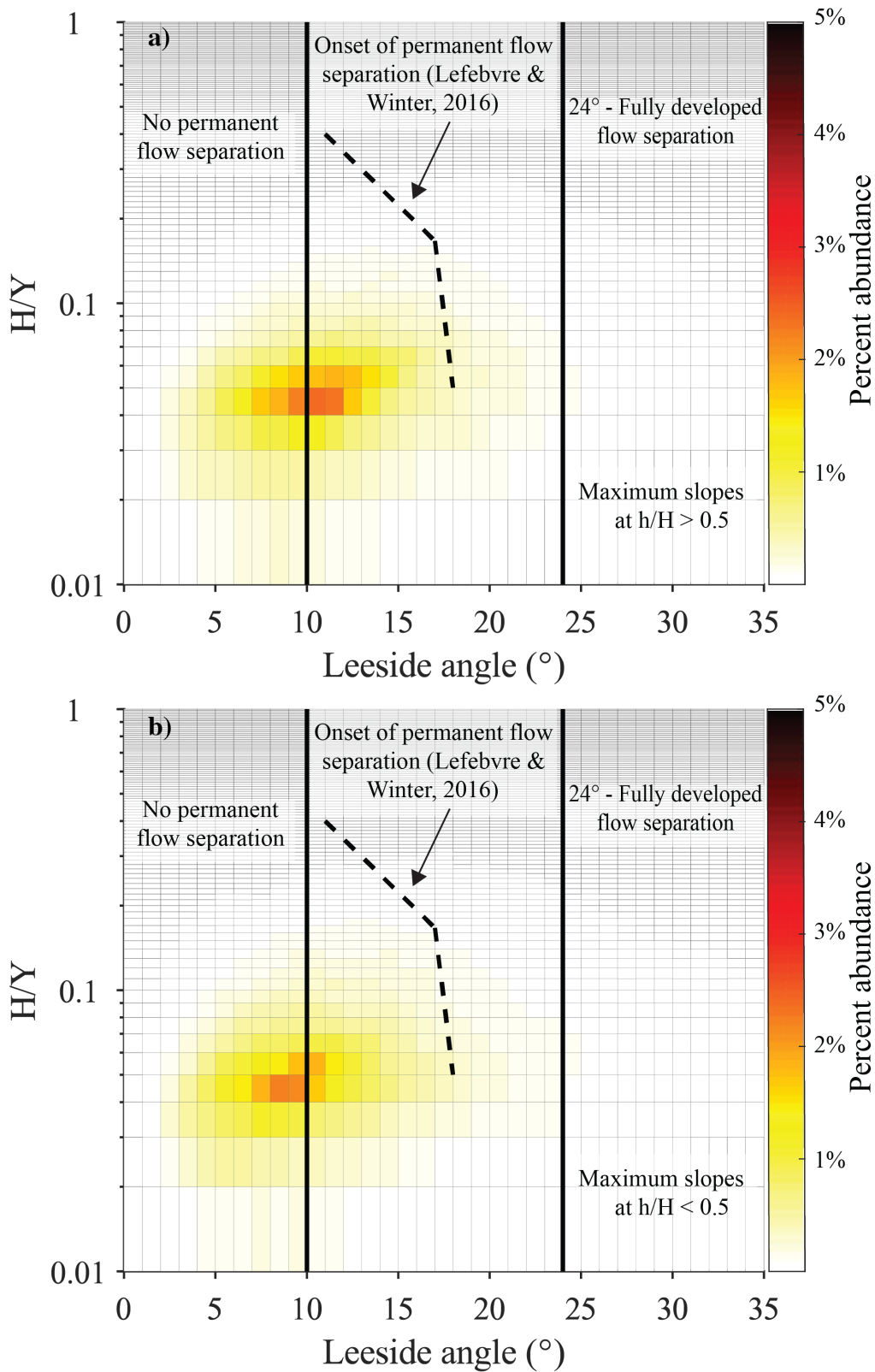
**Figure 1.** Probability density function (PDF) for mean and maximum dune leeside angles in each river and all rivers combined. Black lines represent normal distribution fits and the red line represents a gamma distribution. The blue line marks leeside angles at  $10^\circ$  and the shaded area highlights leeside angles from  $20^\circ$ - $30^\circ$ .



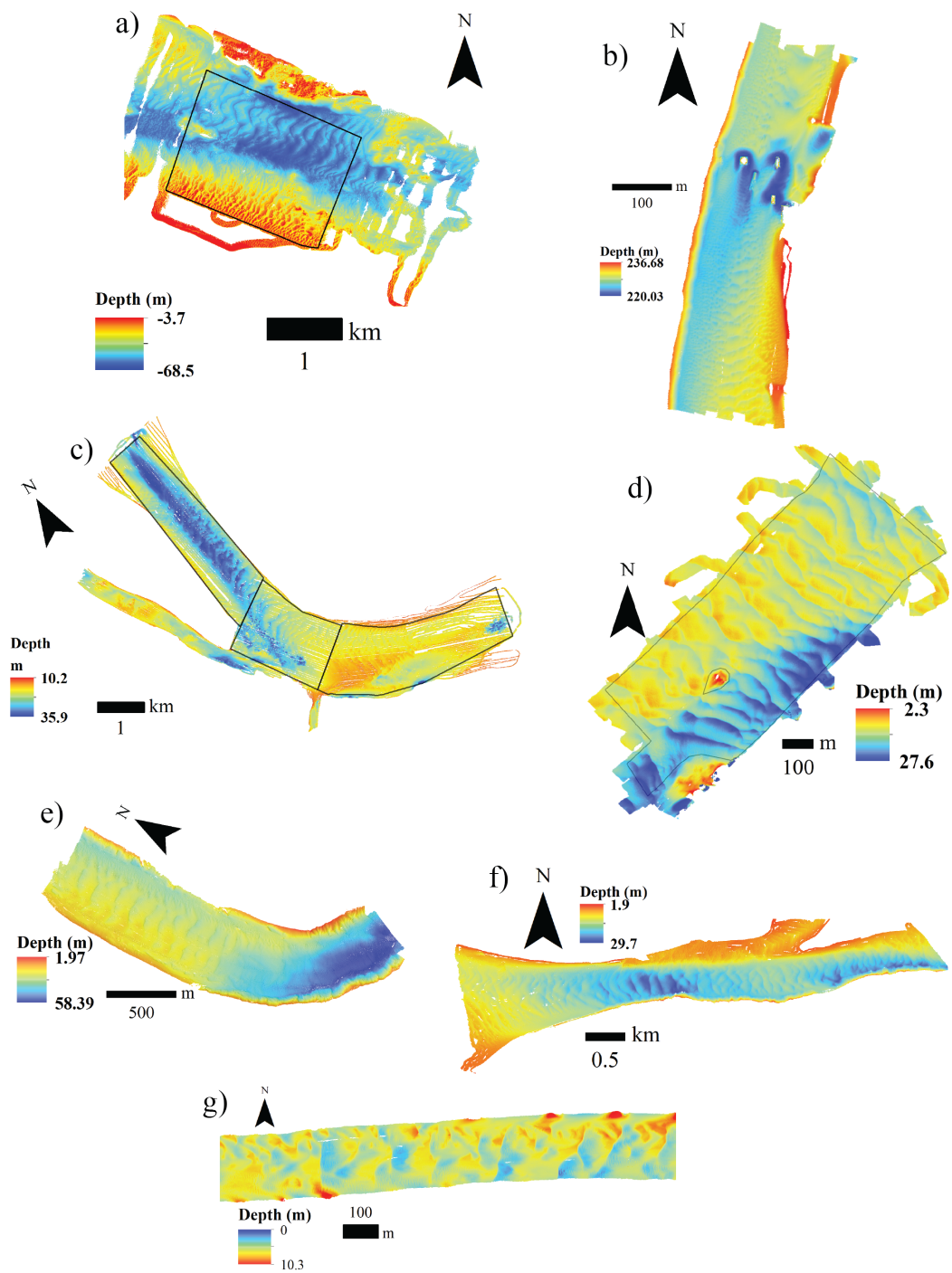
**Figure 2.** a) Schematic showing the location of a maximum slope at 0.2 and 0.8 H for a dune profile. b) PDF of the fractional height of the maximum slope angle on the dune leeside for all rivers.



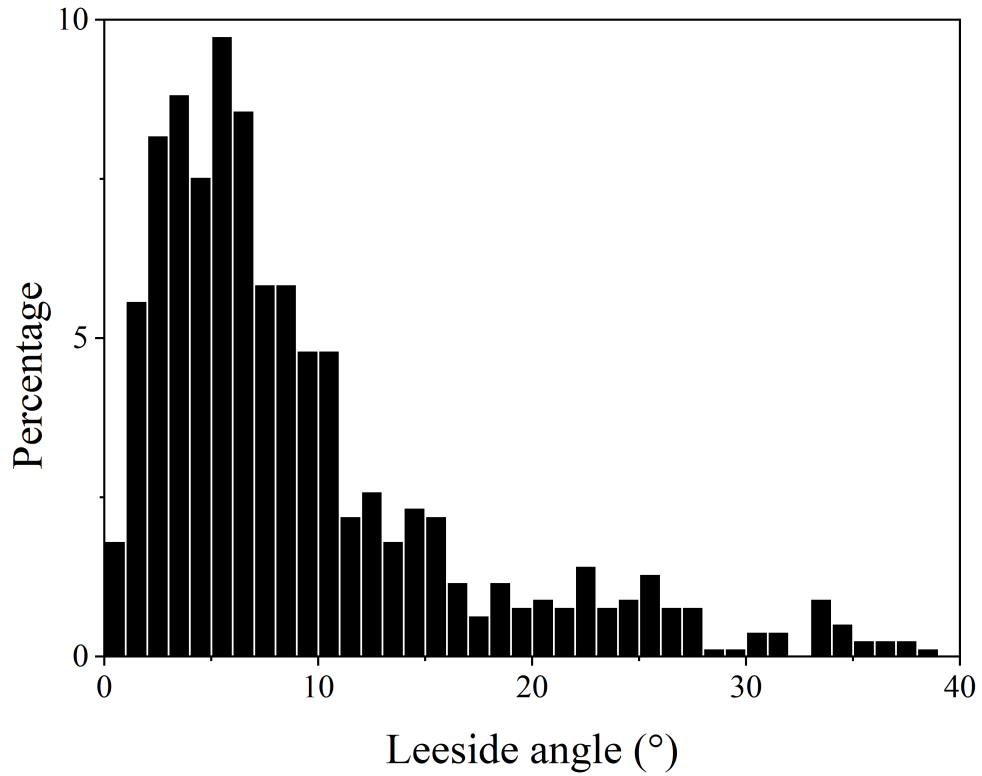
**Figure 3.** Flow depth vs dune height for dunes in all rivers.



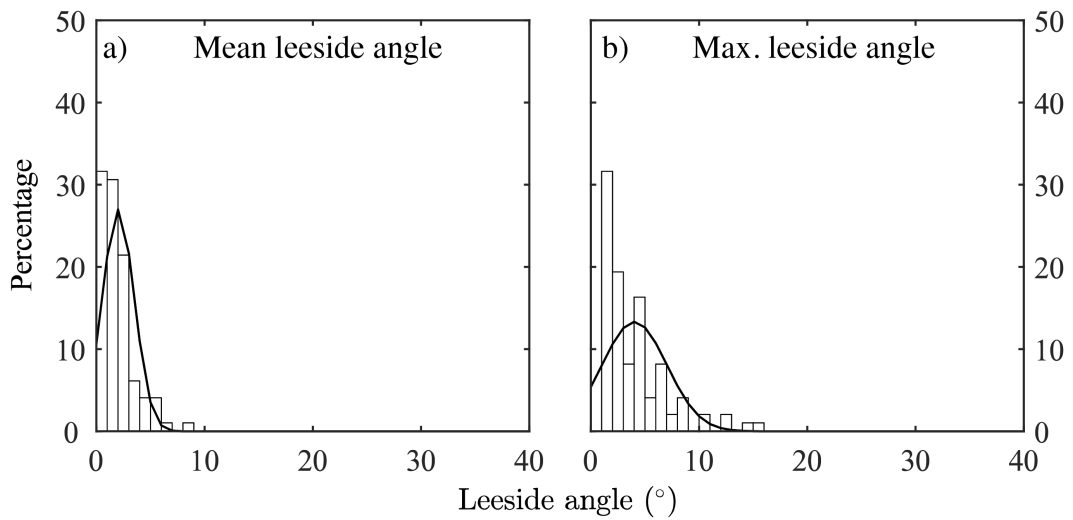
**Figure 4.** Hot spot graph (2D histogram) showing the potential for flow separation represented as a function of the submerged dune height ( $H/Y$ ), leeside angle, and fractional height of the leeside maximum slope, with zones of no permanent flow separation, the onset of flow separation and fully developed flow separation<sup>27</sup>. a) Maximum leesides located on the top half of the dune leeside and b) in the bottom half of the dune leeside. 2D bin units are 0.01  $H/Y$  and  $1^{\circ}$ .



**Figure S1.** Multi-beam echosounder (MBES) maps of rivers analysed in this study from six rivers: a) Amazon, Brazil; b) Mekong, Cambodia; c) Mississippi, USA; d) Missouri, USA; e) Paraná near Paso de la Patria, Argentina; f) Paraná near Aguas Corrientes, Argentina; g) Waal, Netherlands.

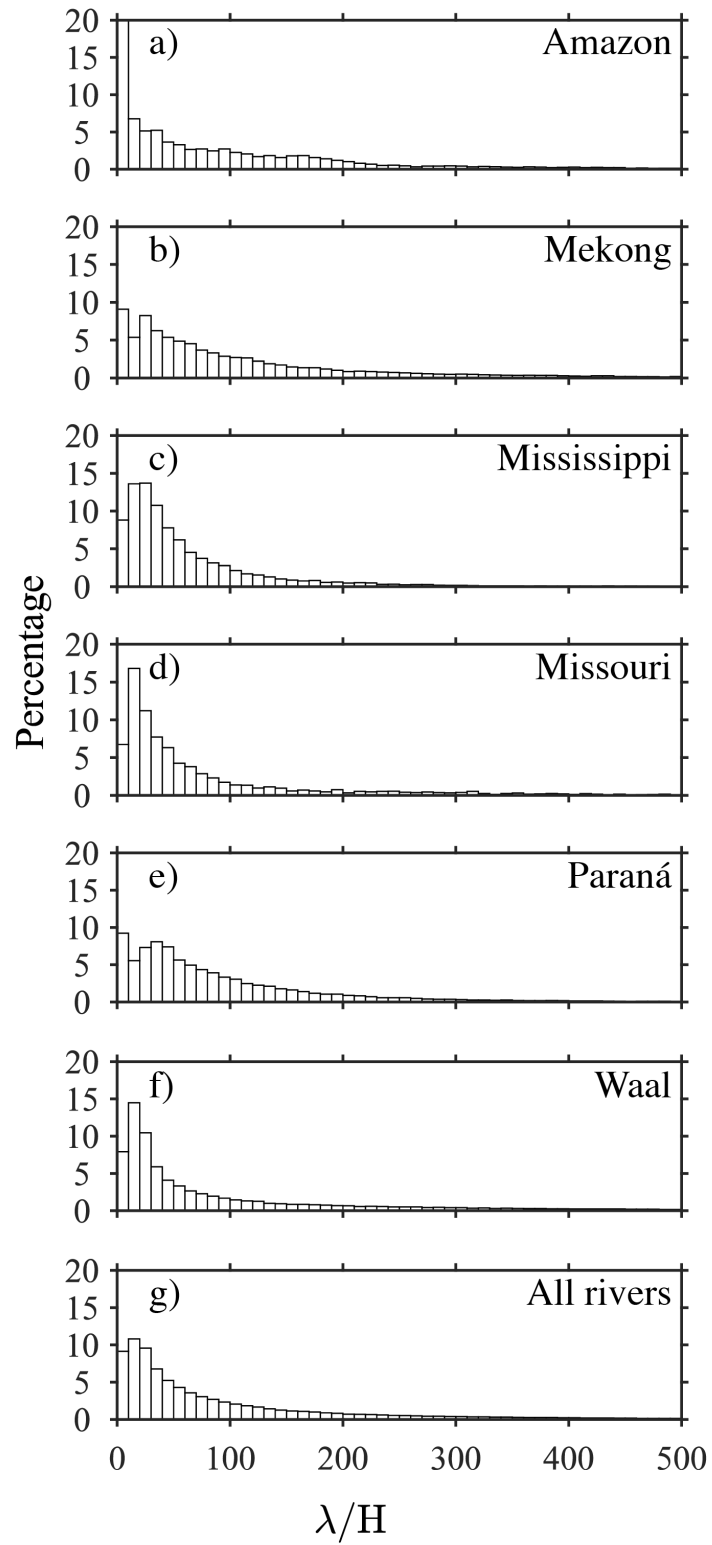


**Figure S2.** Distribution of mean dune leeside angles in the Jamuna (Brahmaputra) River (data from<sup>18</sup>).

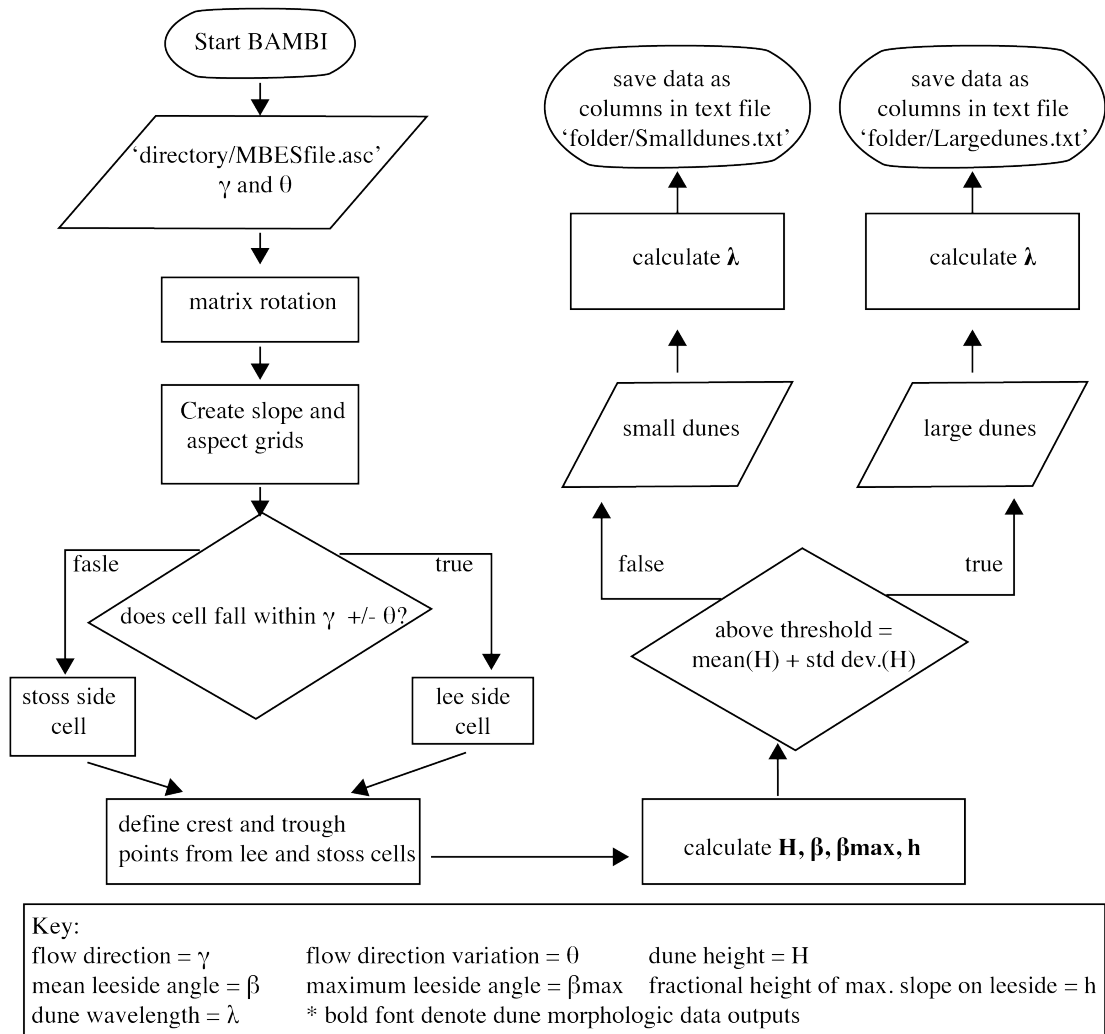


**Figure S3.** Distribution of mean and maximum dune leeside angles in the Huang He (Yellow) River. Leeside measurements were acquired using the BAMBI method from single echosounder lines.





**Figure S4.** Distribution of dune aspect ratio ( $\lambda/H$ ) for all rivers.



**Figure S5.** Flow chart illustrating the BAMBI methodology.