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ASSESSING SOIL COMPACTION FOLLOWING A WINTER TIMBER HARVEST IN THE WESTERN UPPER PENINSULA OF MICHIGAN

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ASSESSING SOIL COMPACTION FOLLOWING A WINTER TIMBER HARVEST
IN THE WESTERN UPPER PENINSULA OF MICHIGAN

By

Rafia Rahman

A THESIS

Submitted in partial fulfillment of the requirements for the degree of

MASTER OF SCIENCE

In Forest Ecology and Management

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College of Forest Resources and Environmental Science

Thesis Advisor: *Matthew C. Kelly*

Committee Member: *Evan S. Kane*

Committee Member: *Zhen Liu*

College Dean: *Andrew J. Storer*

Table of Contents

Acknowledgments.....	v
Abstract.....	vi
1 Introduction and Literature Review	1
1.1 Soil Compaction and Timber Harvesting.....	1
1.2 Study Goals and Objectives.....	9
2 Methods.....	10
2.1 Study Area.....	10
2.2 Harvest System	13
2.3 Study Design.....	13
2.3.1 Machine Traffic	13
2.3.2 Slash Volume.....	17
2.3.3 Percent Rock Content	19
2.3.4 Snow Depth.....	19
2.4 Field Work.....	20
2.5 Lab Procedures.....	24
2.6 Calculations.....	25
2.7 Data Analysis.....	26
3 Results.....	27
3.1 Summary Statistics.....	27
3.2 Effects of Overstory Treatment	28
3.3 Effect of 6-Wheeled vs 8-Wheeled Machines.....	29
3.4 Mixed Effects Model Results.....	30
3.4.1 Effect of Traffic Intensity on Bulk Density.....	30
3.4.2 Effect of Rock Content on Bulk Density	32
3.5 Effects of Snow Depth.....	32
4 Discussion	36
4.1 Effects of Traffic Intensity	36
4.2 Effects of Slash Volume.....	38
4.3 Effects of Percent Rock Content	40
4.4 Winter Harvesting BMPs.....	40
4.5 Limitations and Future Research	41
5 Conclusion	43
6. References	45

7 Appendices.....53

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Abstract

Harvesting during winter is encouraged as a best management practice to protect soil during logging operations. The western Upper Peninsula of Michigan typically experiences early and persistent snowfall, which insulates the forest floor and prevents soils from freezing. The objective of this study is to assess the effects of slash volume, snow depth, overstory treatment, and machine traffic intensity on soil bulk density following a winter harvest of a northern hardwood forest on cobbly silt-loam soils. The harvest was conducted at the Ford Forest in Alberta, Michigan using cut-to-length harvest systems (i.e. harvester and forwarder) during which the soil remained unfrozen. Four levels of machine traffic (high, medium, low, none) and two levels of overstory treatment (clear-cut and partial cut) were considered within a factorial experimental design. Samples were extracted using coring cylinders and separated into three depths (0-5, 5-10, 10-20 cm) prior to drying, sifting and weighing. Results indicate that bulk density did not differ between the no traffic treatment and low traffic treatment at the 0-5 cm depth. However, soil bulk density for the no-traffic treatment was significantly lower than soil bulk density for the medium and high traffic treatments at the 0-5 cm depth. There was a significant effect for traffic in all depths, fine and full soil, except for the 5-10 fine and full soil (which had a p-value of .06). No significant effects of slash volume or snow depth were detected but there was significant effect of percent rock at each depth.

1 Introduction and Literature Review

1.1 Soil Compaction and Timber Harvesting

Soils provide many important functions within a forest ecosystem. They are a source of essential nutrients not only for individual trees but also for the overall forest ecosystem (Dominati et al. 2010). They also provide anchorage and available water necessary to support tree growth. However, soil properties, including soil structure, can be altered by anthropogenic and natural disturbances such as erosion, timber harvesting, prescribed burning, or wildfire (Elliot et al. 1998).

Disturbance from logging can have significant impacts on soils. In recent decades, mechanized harvest systems have become popular because of their improved productivity relative to hand felling systems and the benefits for worker safety (Cambi et al. 2015). Harvest machines, including harvesters, fellerbunchers, skidders, and forwarders, are commonly used to fell, transport and process timber for various purposes (Simmons, 1951; Akay and Sessions, 2001; Greene et al. 2013). Mechanized harvests can impact soil due to the high ground pressures exerted by these modern logging machines (McDonald et al. 1995; McNabb et al. 2001). As axle load capacities increase, machines are becoming capable of supporting greater weight (Håkansson and Reeder, 1994).

A specific concern associated with mechanized harvesting is soil compaction. According to Coder (2000), the definition of soil compaction is the translocation and resorting of textural components in the soil (sand, silt, and clay particles), destruction of soil aggregates, and collapse of aeration pores. Changes in bulk density is commonly used to measure soil compaction. In general, bulk density (g/cm^3) increases as pore space decreases

(Figure 1). Finer texture soils, such as silt and clay, generally have more pore space and thus have lower bulk density than sandy soils (Source: DeJong-Hughes 2018).

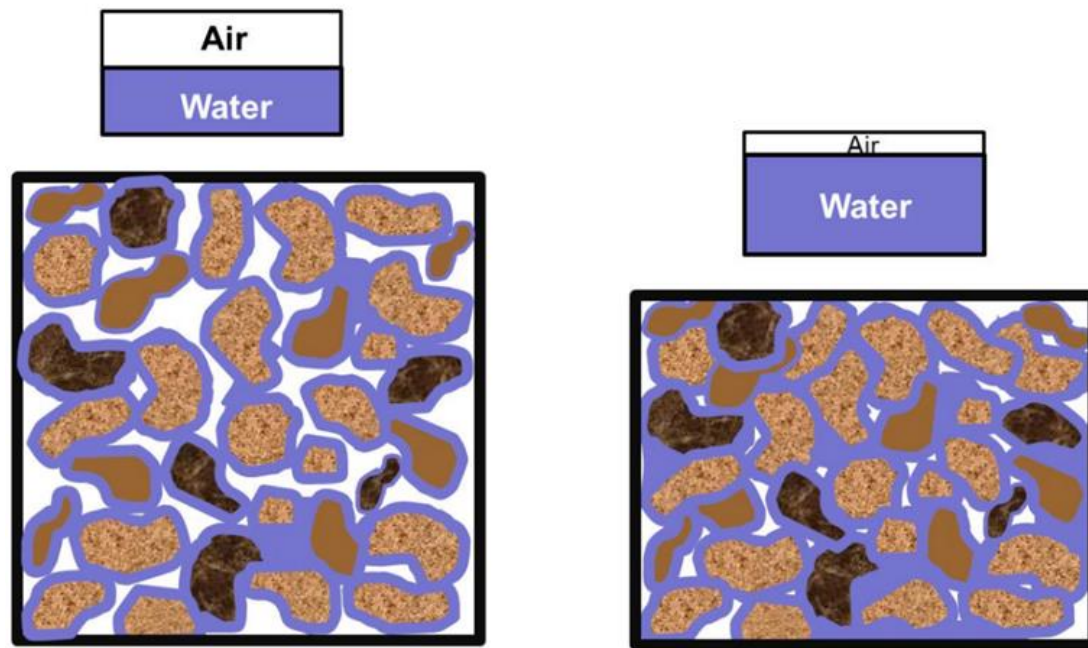


Figure 1. Physical effects on soil due to compaction (DeJong-Hughes, 2018)

Compaction decreases air and water availability to plant roots and microscopic organisms as well (Bodelier et al. 1996; Startsev and McNabb, 2000; Frey et al. 2009). Soil compaction changes soil physical properties and structure, decreases pore space and saturated hydraulic conductivity (Jansson and Johansson, 1998; Grace et al. 2006), and affects site quality by reducing the rate of water penetration and aeration of soil, and can increase resistance to root penetration (Greacen and Sands, 1980; Taylor & Brar 1991; Quesnel and Curran, 2000; Grigal 2000; Zhao et al. 2010) and can eventually restrict plant growth (Kozlowski, 1999; Meyer et al. 2014). Recovering adequate pore space, water availability, and rich organic matter content after compaction can take long periods of time, ranging from an estimated seventy to one hundred forty years depending on variables such as climatic conditions, type

of soil and degree of compaction (Greacen & Sands, 1980; Froehlich et al. 1985; Webb et al. 1986). Additionally, harvesting disturbances can affect tree regeneration success by damaging tree roots, decreasing root respiration, and limiting the active rooting zone as well as root growth and development (Hatchell et al. 1970; Martin, 1988).

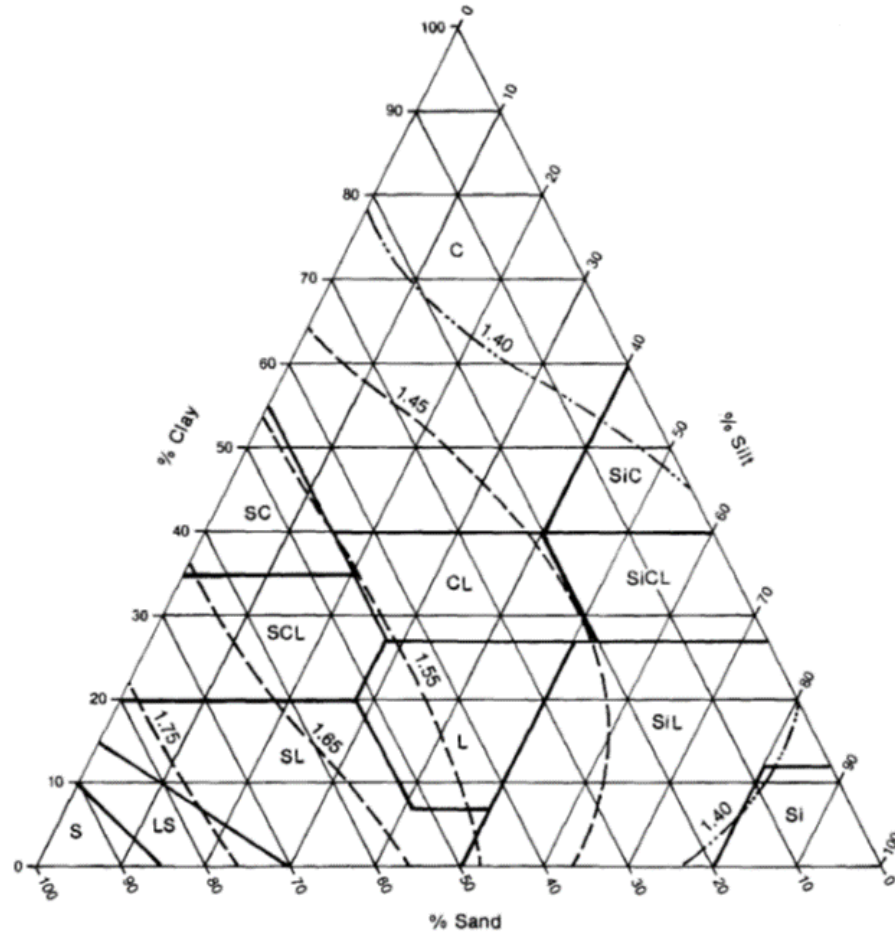


Figure 2. Growth-limiting bulk density (g/cm^3) textural triangle (source: Daddow and Warrington, 1983)

The degree to which soil is compacted depends on numerous factors such as machine traffic intensity, slope steepness, site characteristics, harvesting machinery type, designing or planning of skid roads, and the caution and expertise of machine operators (Reisinger et al. 1992; Laffan et al. 2001; Eliasson and Wa sterlund 2007; Demir et al. 2007; Najafi et al. 2009; Solgi and Najafi 2014; Naghdi and Solgi 2014; Cambi et al. 2015). Additionally, soil deformation is linked to soil moisture, initial bulk density, soil organic matter, and ground elevation (Ballard, 2000; Jamshidi et al. 2008). Generally, soils with low bulk density are more susceptible to compaction (Hillel, 1998; Williamson and Neilsen, 2000; Powers et al. 2005). Soils which have bulk densities $\geq 1.4 \text{ Mg m}^{-3}$ are not that much affected by compaction. Although tree growth can be reduced due to compaction on clayey soils, Powers et al (2005) found compaction benefited tree growth in sandy soils due to increased water and nutrient availability.

Machine traffic intensity (the number of machine passes on a skid trail due to tree harvesting) is a key factor in soil compaction as deformations generally increase with the increasing number of passes and may eventually lead to significant disturbance of soil (Mosaddeghi et al. 2000; Solgi and Najafi 2014).

The relationship is nonlinear between soil bulk density and traffic intensity (McNabb et al. 1997; Najafi, 2010), such that the first few passes are generally responsible for most surface compaction, but bulk density may increase with increasing traffic over the site according to the number of passes and soil depth (Hatchell et al. 1970; Brais and Camire', 1998; Williamson and Neilsen, 2000; McNabb et al. 2001). Traffic intensity over a given skid trail can be measured using GPS technology (McMahon, 1997; Carter et al. 1999; McDonald et al. 2002). GPS units can be attached to each machine to track machine

movement. Those data can then be analyzed to determine the number of passes over a given skid trail within ArcMap so that the affected areas can be identified (Zenner et al. 2007).

In temperate forests, harvesting in winter is typically encouraged as a best management practice to protect soils, particularly those composed mainly of finer texture silt or clay soils. Thus summer logging is generally not recommended on sensitive or poorly drained soils (Smith and Wass, 1976; Krag et al. 1986). When harvesting forested wetlands, harvesting in the winter under frozen conditions is necessary to prevent negative impacts to these sensitive areas (Zasada et al. 1987).

Similarly, placing slash (i.e. logging residue in the form of tree tops and limbs) on skid trails is encouraged to reduce soil disturbance, including compaction, erosion and surface runoff (Sawyers et al. 2012; Wade et al. 2012; Vinson et al. 2017). Slash can also play an important role for improving site quality by providing an organic layer for natural tree regeneration (Eisenbies et al. 2005), and reducing compaction caused by heavy forestry machines (Parkhurst, 2018). For erosion control, slash application is recommended (Virginia Department of Forestry [VDOP] 2011; Wade et al. 2012; Vinson et al. 2017). Eliasson and Wästerlund (2007) found that topsoils of strip roads in which slash was established did not incur any damage from compaction. On the other hand, McDonald and Seixas (1997) found that slash did not reduce compaction on sandy soil after the first pass of a rubber-tired forwarder.

Differences in silvicultural techniques applied during harvesting can produce different levels of slash due to differences in harvest intensity, particularly in terms of the amount

of trees cut per acre (or volume removed per acre). The type of silviculture treatment being applied can also affect machine traffic intensity.

Bigelow et al. (2018) applied three different selection methods in longleaf pine forest on coarse-textured soils including single-tree, group, and group with reserved trees. The authors found that according to the single-tree selection system, a greater area was affected by single machine passes than higher numbers of passes, on the other hand under group and group with reserves selection system more area was affected by high traffic areas.

Malo and Messier (2011) studied the effect of two type of machine tracks primary (multiple trip) and secondary (only one trip) followed by a silvicultural system (selection cutting) to evaluate sugar maple (*Acer saccharum* Marsh.) fine root growth and reported that heavy machinery has an effect on physiological structure, growth and development of sugar maple one year after the silvicultural operation (selection logging) was completed. It was found from the data that the control area was less affected than both primary and secondary tracks for the fine root growth of sugar maple.

Stone (2002) conducted an experiment that examined the effects of winter logging on soil disturbance and regeneration success on clay soils of four aspen-dominated stands in Western Upper Michigan. The results showed that a large skidder was responsible for deep rutting on 20% of sites that received a thinning that removed $7.8 \text{ m}^2 \text{ ha}^{-1}$ ($34 \text{ ft}^2 \text{ ac}^{-1}$) of basal area, and on 38% of clearcut sites. The authors also found that 45% of clearcuts did not have aspen regeneration after the first growing season and 82% had less than the recommended minimum of $15,000 \text{ suckers ha}^{-1}$ ($6,000 \text{ ac}^{-1}$).

Bates et al. (1993) carried out a study that looked at harvesting effects on quaking aspen regeneration in northern Minnesota and found that regeneration of aspen is affected by

equipment traffic and harvest season. In that study, regeneration vigor associated with variables such as stem density, stem height growth, and crown closure, all of which were greater following winter harvesting. The authors also reported that aspen regeneration was reduced significantly following the summer harvesting and with increased traffic in the harvest sites. The results from this study suggest that comparatively fine-textured and poorly drained soils are more prone to regeneration problems for aspen once harvested initially in summer but the most vigorous regeneration happens following winter harvesting.

Zenner et al. (2007) also investigated soil disturbance due to ground-based logging operations within a quaking aspen stand. Different levels of traffic intensity were applied to measure effects of machine traffic on aspen regeneration, growth, recovery on this site as well as resistance capacity to penetration within the top 15 cm of soil for three years after clearcutting. The result showed that within the 0-5 cm depth, soil can recover from disturbance three years after the harvest, but partial recovery was found within the top 10cm depth during four or less machine passes and recovery was very limited for 10-15 cm soil depth within a three-year period. Skidding traffic intensity significantly reduced height, density of aspen sucker, growth, dbh, and basal diameter compared with control areas but resistance to penetration was not significantly different.

Naghdi et al. (2018) found that machine traffic has an effect on soil pore space and bulk density. They sampled skid trails immediately after a skidding operation and again one year later to evaluate recovery of soil physical properties. The authors measured soil bulk density across three levels of traffic intensity and two levels of slope steepness. Data showed that bulk density and microporosity were greater due to the use of harvest

machinery whereas microporosity and total porosity were less for top ten cm of soil depth compared with the areas that were not harvested. The compacted soil did not show any significant recovery after one year. Rather, further decrease in microporosity was reported. Williamson and Neilson (2000) studied soil compaction and how the soil profile can be disturbed in a skid trail due to the operation of heavy ground-based logging machines. Six forest areas (dry and wet forests) were selected to evaluate. The authors reported that compaction restricts root growth and reduces forest productivity. It was observed that machine forces displaced topsoils rather than causing compaction in situ on the wettest soils logged.

Parkhurst et al. (2018) conducted a study within a pine stand and observed that the heavier skidder was responsible for higher bulk density, reduced macroporosity, and more visible ruts than the lighter dozer and the amount of disturbance to a given site may increase with the increased machine size. They also found that providing slash cover had limited effect on changes in bulk density and porosity than using the forest floor for overland skidding. In addition, they found that mechanical resistance data contradicted the machine size finding because the effects from the heavy skidder and light dozer were similar in size in the surface depth category.

Zasada et al. (1987) showed that winter logging is suitable because accessing floodplains is easier during the winter season while logging, as well as transport, but during summer season these areas are not accessible when rivers and poorly drained areas are no longer frozen. They also observed that tree regeneration can be protected from physical damage by logging with a good snowpack as the upper layer of the snowpack was disturbed and mixed with logging debris, the lower part of the snowpack was compacted but not mixed.

1.2 Study Goals and Objectives

The western upper peninsula of Michigan typically experiences early and persistent snowfall, which insulates the forest floor and prevents soils from freezing. This study was conducted to assess post-harvest soil compaction following a winter harvest of northern hardwoods on cobbly silt-loam soils. The harvest included both clearcuts and various partial cuts (e.g. shelterwood, singletree-selection). The cover type was northern hardwoods, with a very large component of sugar maple (*Acer saccharum* Marsh.). The objective of the study was to assess the effects of machine traffic, slash volume, snow depth, and percent rock content on soil bulk density following operation of a cut-to-length harvest system (i.e. harvester and forwarder) during which the soil remained unfrozen.

2 Methods

2.1 Study Area

This study was conducted following a winter timber harvest at Michigan Technological University's Ford Forest, located in Alberta, Michigan during the months of February and March of 2017. This site consists primarily of northern hardwoods, dominated by sugar maple (*Acer saccharum* Marsh), with some yellow birch (*Betula alleghaniensis*), basswood (*Tilia Americana*), red maple (*Acer rubrum*), balsam fir (*Abies balsamea*), black cherry (*Prunus serotina*), ironwood (*Ostrya virginiana*), and american elm (*Ulmus Americana*).

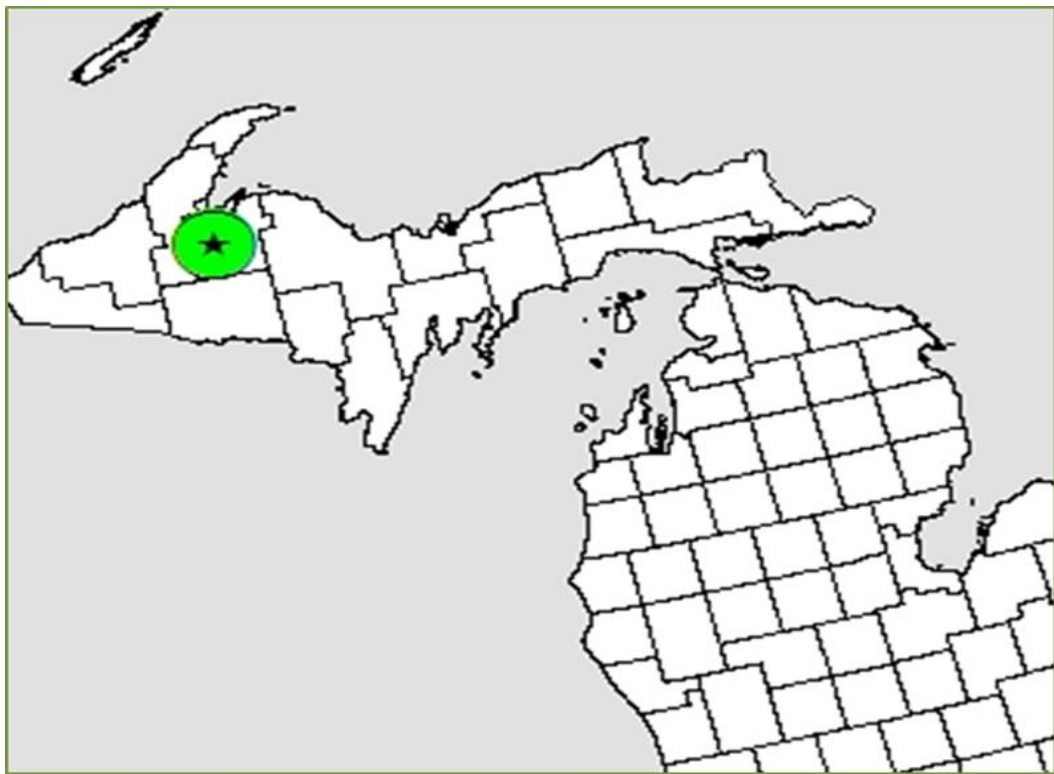


Figure 3. Study site located in Alberta, MI at Michigan Technological University's Ford Forest.

The harvest occurred as part of the Northern Hardwood–Silvicultural Experiment for Enhancing Diversity (NH-SEED), which included both clearcuts and various partial cuts (e.g. shelterwood, singletree-selection).

The site consists mainly of the Champion soil series (taxonomic class: coarse-loamy, mixed, superactive, frigid Oxyaquic Fragiorthods), with relatively small areas of Tacoosh, Witbeck, and Michigamme soils series (Figure 4). The champion series is characterized by well-drained to moderately well-drained cobbly silt loam soils. According to the Natural Resources Conservation Service, gravel content ranges from 0 to 10% for A, E, and B horizons; and from 5 to 35% in the 2B and 2C horizons whereas cobble and stone content range from 0 to 35% for A, E, and B horizons and from 0 to 15% in the 2B and 2C horizons. The Michigamme series consists of moderately deep, well-drained soils that are formed by igneous or metamorphic bedrock. In this soil series, the upper part of the solum is moderately permeable but slow or very slow in the lower part.

According to the National Oceanic and Atmospheric Administration (NOAA), during winter, average minimum temperature is about 7.1°F, and the average maximum temperature is 23.7°F. Weather data for this study site during the harvest period, which started Feb 6, 2017, and ended March 26, 2017, varied on a daily basis. The average snowfall was 0.75 inch per day within the period. Snow depth data was also collected for each day during the harvest where the average snow depth was about 11 inch. The range of snow depth was recorded from 1 to 27 inch and the maximum snow depths were found at the beginning of the harvest time and these data were collected also before the machine passes and became lower during the last days in March. The average data were found for maximum and minimum temperatures of about 31.7°F and 13.5°F.

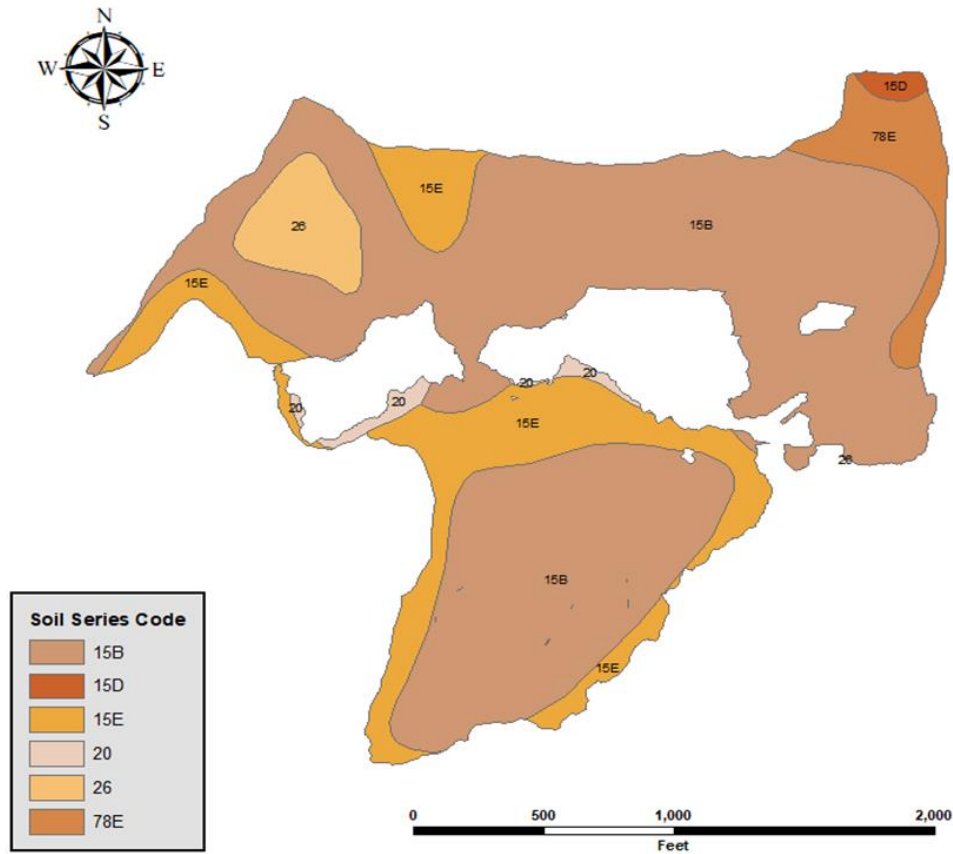


Figure 4. Soil series map for Study area (Source: WSS, NCRS-USDA), where 15B= Champion cobbly silt loam with 1 to 8% slope, 15D = Champion cobbly silt loam with 8 to 15% slopes, 15E = Champion cobbly silt loam with the slope range of 15 to 35%, 20 = Carbondale and Tacoos muck with 0 to 1% slopes, 26 = Witbeck muck with 0 to 2% slopes, 78E = Champion-Michigamme cobbly silt loams with 15 to 35 % slopes

2.2 Harvest System

The harvest was conducted using two cut-to-length harvest systems, each comprising a harvester and a forwarder. The two harvesters were different, one was a 6-wheeled PONSEE Bear and the other was an 8-wheeled PONSEE Ergo. The harvester fells trees and processes them into logs and the forwarder transports the logs from the harvest area to the road or landing, where they are picked up by a log truck and brought to a mill.



Figure 5. **A** showing a forwarder as part of a cut to length system and **B** showing a harvester (PONSEE bear)

2.3 Study Design

Soil samples were collected from forest, Alberta, MI and later analyzed to measure the effects of various factors on soil bulk density. Those factors include machine traffic, slash volume, rock content, and snow depth, and are explained in greater detail below.

2.3.1 Machine Traffic

GPS units were used to collect waypoints every 3 seconds for each harvest machine during the entire harvest. Those GPS data were then used within an ArcGIS to analyze the number of passes over a given skid trail. Six sample plots were established for each level of machine traffic (3) within each type of overstory treatment (2) resulting in 18 total plots.

Each plot was defined as a section of skid trail 20 m in length. Machine traffic was defined in terms of number of machine passes and grouped into three categories:

- High traffic (≥ 8 passes)
- Medium Traffic (4 – 7 passes)
- Low traffic (1 – 3 machine passes)

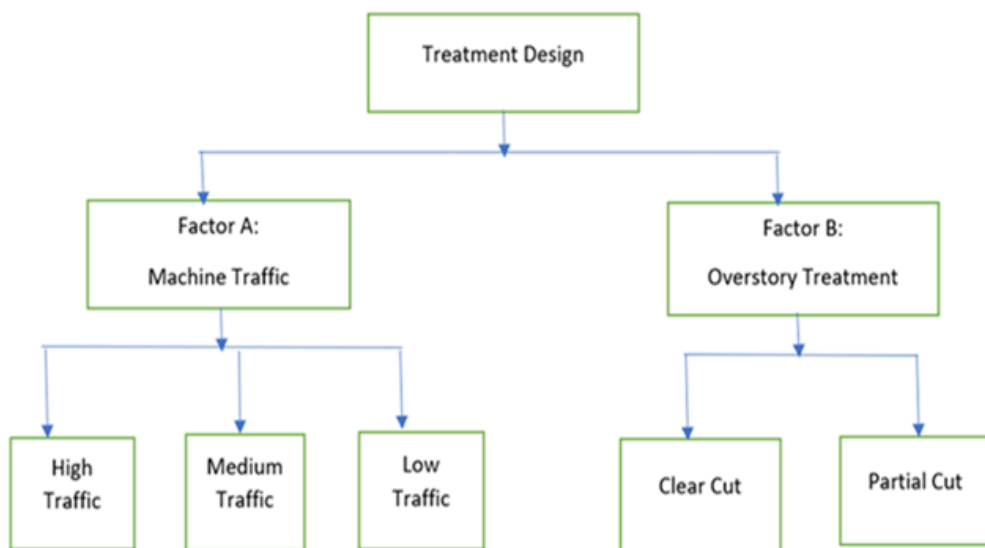


Figure 6. Treatment design of this research where factor A represents three levels of machine traffic and factor B represents overstory treatment with clearcut and partial cut

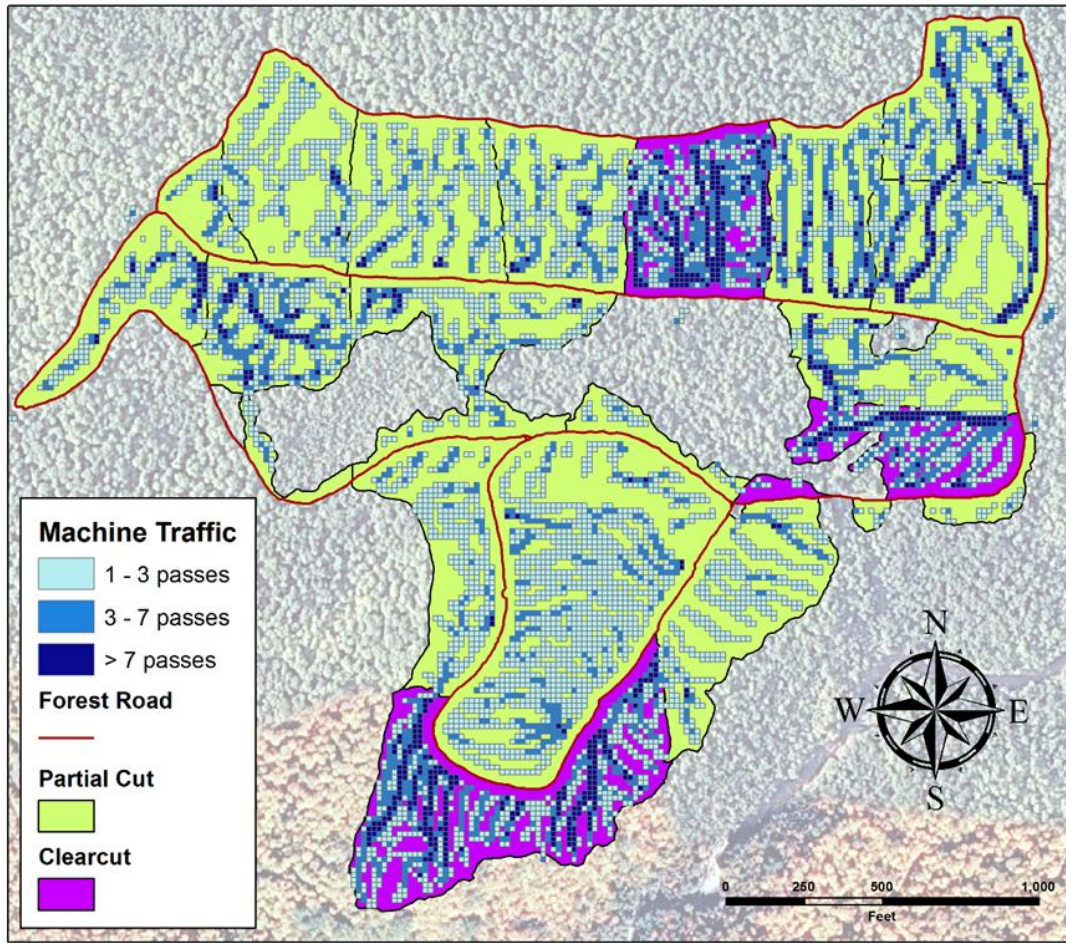


Figure 7. Showing all skid trails and the different levels of traffic (high, medium, low)

Sample plots were stratified equally into one of two overstory treatments - partial cut and clearcut. Stratifying the sampling by overstory treatment was meant to account for potential differences in slash volume. All segments of skid trails were identified and partitioned into 20-meter segments. Next, three segments were selected randomly from the total population of skid trail segments for each combination of machine traffic level and overstory treatment. The random selection was done using a random number generator within MS Excel.

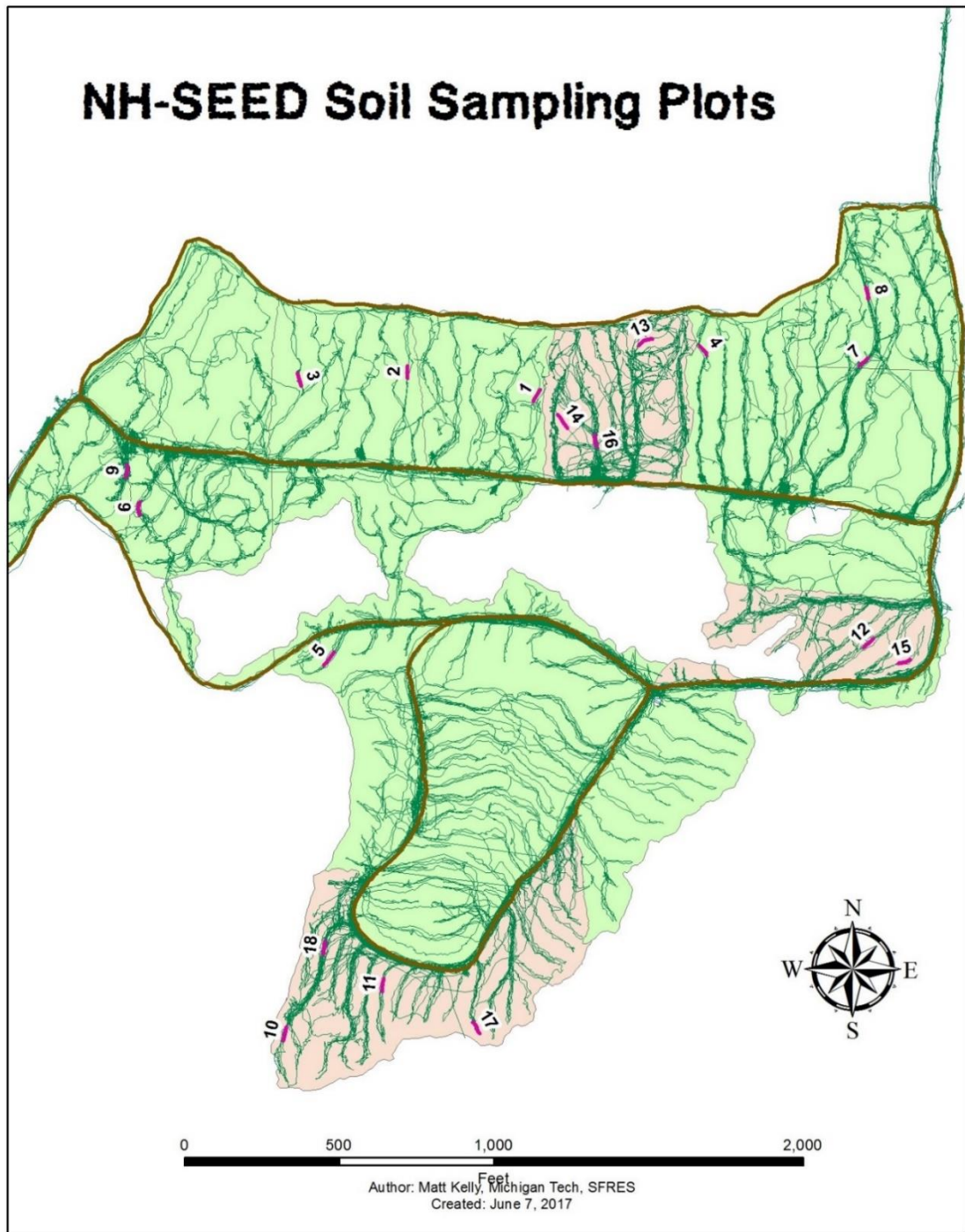


Figure 8. Map showing the location of the study site with the sample plots.

Within each plot, 6 sample points were located along each side of the skid trail, within the tire tracks, for a total of 12 points per plot. Points were spaced two meters apart. Additionally, 31 samples were collected randomly from locations within the harvest area where machines did not travel. These areas were identified within ArcGIS as areas where no machines traveled, according to the GPS data. Thus, these samples represent a “no traffic” treatment level.

2.3.2 Slash Volume

Slash is defined as woody debris from unutilized tree limbs and tops that were either intentionally placed on the skid trail or happened to fall on the skid trail during the harvest operation. Slash volume was measured by first visually estimating a packing ratio of woody material within a three-dimensional space over a square meter area surrounding the sample point. To estimate the volume of the three-dimensional space over a given point, a square meter quadrat was used to establish length and width, while the height of the highest piece of woody material within the quadrat was used to estimate the total volume of the space.

Packing ratios were visually estimated with the help of a field guide. The field guide included images of six different levels of slash volume for which volumes and packing ratios were fully measured. The field guide was developed prior to sampling. At each of the six points chosen to create the field guide, height of the highest piece of slash within the square-meter quadrat was measured. Next, all slash within the quadrat was cut, removed, and weighed using a luggage scale. Thus, for each of the six representative plots, the density of slash was measured in units of m^3/m^2 .

Next, this density was compared to the density of sugar maple wood with 23 percent moisture content (MC), which is roughly 706.5 kg/m³ (Simpson and TenWolde, 1999). This MC represented the mean MC of all wood samples measured in the field during the development phase of the field guide using a handheld moisture content meter. Therefore, the packing ratio was the ratio of the measured slash density to 706.5 kg/m³.

The images and measured packing ratios found in field guide were used to help visually estimate packing ratio for each sample point. This estimated packing ratio was then applied to the three-dimensional space above square meter, as determined by the height of the highest piece of woody debris, to calculate slash volume in terms of m³/m².



A



B

Figure 9. Estimating the packing ratio using a square meter quadrat and packing ratio field guide was developed by calculating packing ratio as volume of slash / volume of 3-dimensional space to use as a reference later for each sample point

2.3.3 Percent Rock Content

Rock has density of 2.65 g/cm³ (NRCS, USDA). It was reported that rock fragment content negatively influences fine soil bulk density (Stewart et al. 1970; Torri et al. 1994).

Therefore, percent rock content was measured for this study to identify potential effects of rock content on soil bulk density in different depth of soil (0-5 cm, 5-10 cm, 10-20 cm).

Additional Data related to rockiness were collected during field sampling which includes number of attempts at each sample point, depth to rock or root obstruction for each failed attempt, number and percent cover of surface rocks within a square meter plot around the sample point.

2.3.4 Snow Depth

Daily snow depth data collected in the village of Alberta, MI and reported to NOAA were used to assess impacts of snow depth on soil bulk density. The snow depth on the day that a skid trail was first traversed, according to the GPS data, was used for all samples in a given plot. Snow depth was generally greatest at the start of the harvest, but decreased substantially at various point throughout the harvest due to periods of warm temperatures (Appendix 16)



Figure 10. Representation of snow depth and the underlying unfrozen soil during one of the harvest days

2.4 Field Work

At each sample point, soil was extracted using a slide hammer and a 20 cm x 5 cm core sampler. The sample was divided into three depths using liners that fit within the cylinder. Soils within each depth were placed into plastic bags labeled with the plot and point number, and the soil depth (0-5 cm, 5 - 10 cm, 10 - 20 cm).



A



B



C



D



E

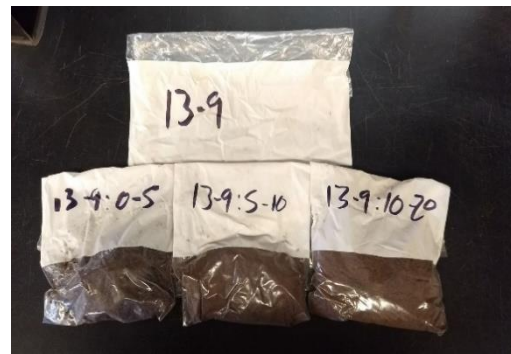
Figure 11. A B showing soil samples were extracting using a slide hammer and a 20 cm corer. Samples were separated into different depths (0-5, 5-10, 10-20 cm) and C, D and E showing the skid trail, 12 sample points taken at 2 meters intervals along each side of the wheel tracks /ruts

2.5 Lab Procedures

Bulk density (g/cm^3) was measured for depths 0-5 cm, 5-10 cm, and 10-20 cm for all samples. Soil samples were kept in a refrigerator in separate plastic bags maintaining a specific temperature after collecting the samples. An aluminum tray was used to weigh full soil samples with different depth and the measurement units were in grams.



A



B



C



D

Fig 12. A and B (collected samples from research site with three subgroups according to depth 0-5 cm, 5-10 cm, and 10-20 cm), C (samples in the oven to remove the moisture content), D (scale for measuring the weight of soil for each depth)

After weighing the full soil with moisture content, the specific temperature in the oven was maintained to remove the soil moisture content and that was 175-degree Fahrenheit and all the data were recorded. Then wooden rolling pin and spoon were used to grind the soil and using a sieve, the rocks were extracted from the sieve for different depth of soil samples. After this, rocks and fine soil were separated to weigh again and record the data. The weigh was taken for both rock and soil. Once drying, sifting, weighing were done all data were recorded again for bulk density calculation. The sieve size grade (#10) was used in lab to separate fine soils from rocks and larger particles.

2.6 Calculations

Calculations were performed after collecting lab data to determine soil bulk density for fine sediment and the full soil sample. In addition, calculations were conducted to determine rock volume, percent rock content, and slash volume.

Volume calculations for cylinder liners:

- 10-20 cm liner: $h=9.65$ cm, $r= 2.413$ cm , $\pi r^2 h = 176.56$ cm³
- 0-5 and 5-10 cm liners: $h = 5.08$ cm, $r = 2.286$ cm, $\pi r^2 h = 83.39$ cm³

The volume of Soil (cm³):

- Volume of Cylinder – Volume of Rock (ml)

The volume of Rock (cm³):

- $0.2376+0.3962*\text{weight of Rock (Premer, 2016)}$

Percentage of Rock Volume (%):

- $\text{Volume of rock} / (\text{Volume of Soil} + \text{Volume of Rock})$

Fine Soil Bulk Density (g/cm³):

- $\text{Fine Soil Weight (g)} / \text{Volume of Soil (cm}^3)$

Soil Bulk Density (g/cm^3):

- Weight of Dry Soil (g)/Volume of Cylinder (cm^3)

Slash Volume (kg/m^3):

- $1\text{m} \times 1\text{m} \times \text{Height of slash(m)} \times (\text{Packing Ratio}/100)$

2.7 Data Analysis

Data were analyzed using a mixed-effects model where the dependent variable (y) was soil bulk density, and independent fixed variables included machine traffic, slash volume, and overstory treatment, while percent rock content was included as a random variable. This model was fit for each depth of soil, and for total and fine soils. SAS version 9.4 was used to run the model. A separate regression analysis was run to estimate the effects of snow depth on bulk density.

Descriptive statistics were calculated using Microsoft excel to summarize the results. Additionally, one-way analysis of variance tests (ANOVA) was used to compare slash volume between partial and overstory treatments and to compare soil bulk density between 6 and 8-wheeled harvesters.

3 Results

The primary objective of this research was to assess the effects of machine traffic, slash volume, percent rock content, overstory treatment and snow depth on soil bulk density. Data were collected from a total of 247 sample points across 18 plots (i.e. sections of skid trail) and 31 points that received no machine traffic.

3.1 Summary Statistics

According to Table 1, the mean of fine soil bulk density was greater (1.50 g/cm^3) in 5-10 cm depth than 0-5 cm (1.20 g/cm^3) and 10-20 cm (1.44 g/cm^3). Bulk densities for the full soil sample (including rock and cobble) were 1.12 g/cm^3 , 1.36 g/cm^3 and 1.28 g/cm^3 in 0-5 cm, 5-10 cm, and 10-20 cm soil depth, across all levels of machine traffic.

Variables related to rockiness such as attempts and average depth of failed attempts in each sample point, number of surface rocks, percent rock cover, and percent rock content in the soil were also measured in this study (Table 1). The upper layer of soil (0-5 cm depth), showed less rock content than soils at greater depths. The average percentage of rock volume in 0-5 cm was 6% compared with 10% in 5-10 cm and 10-20 cm soil depths. The range of percent surface rock cover varied from 0 to 26. The results also showed that the mean number of surface rocks was 1.13 with a range of 0 to 15. A number of sample points required multiple attempts to drive the cylinder in the ground to collect a soil sample due to the presence of rocks or other obstructions in the soil. The number of attempts and average depth of failed attempts were counted for each sample point. The range of number of attempts varied from 1 to 13, with an average of 1.95 attempts per sample point. The

depth at which a failed attempt was abandoned ranged from 1 cm to 19 cm, with an average of 11.15 cm.

Table 1. Descriptive Statistics for each variable showing the mean value

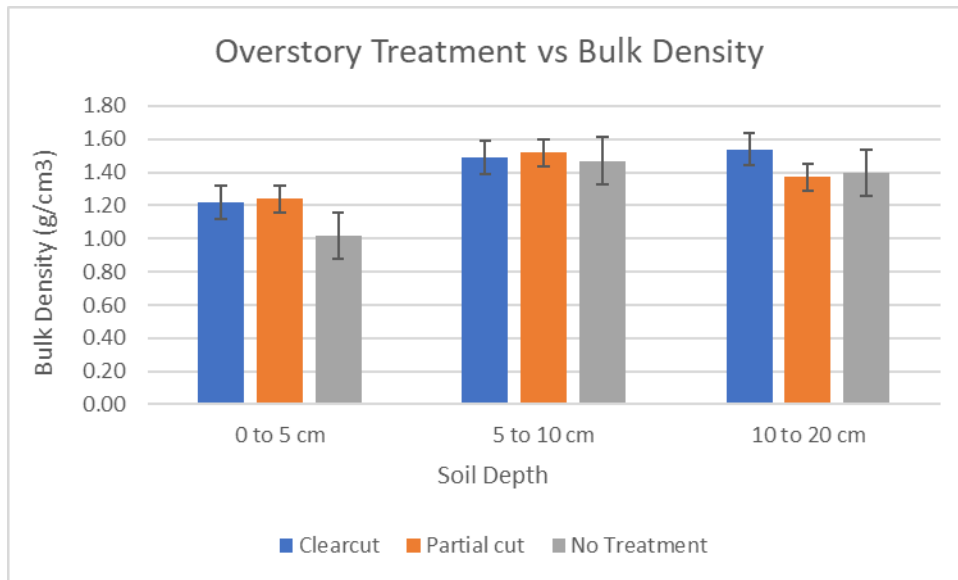
Variable	Depth	Mean	Standard Deviation	Minimum	Maximum
Full Soil Bulk Density (g/cm ³)	0-5 cm	1.12	0.21	0.47	1.75
	5-10 cm	1.36	0.24	0.75	2.09
	10-20 cm	1.28	0.21	0.40	1.81
Fine Soil Bulk Density (g/cm ³)	0-5 cm	1.20	0.27	0.5	2.26
	5-10 cm	1.50	0.34	0.8	2.47
	10-20 cm	1.44	0.33	0.4	2.49
Percentage of Rock volume	0-5 cm	0.06	0.06	0.00	0.37
	5-10 cm	0.10	0.09	-0.01	0.52
	10-20 cm	0.10	0.09	0.00	0.42
Attempts		1.95	1.69	1	13
Avg. Depth of Failed Attempts		11.15	5.20	1	19
# of surface rocks		1.13	2.07	0	15
% rock cover		1.20	3.31	0	26
Average Snow Depth (inch)		10.50	5.19	1	19
Average slash volume (kg/m ²)		0.0098	0.00	0.0	0.15

3.2 Effects of Overstory Treatments

Results showed no significant difference between mean bulk density of soils under the two overstory treatments (clearcut and partial cut) on bulk density (Figure 13). The mean bulk densities were 1.22 g/cm³ and 1.24 g/cm³ for clearcut and partial cut harvest system in the 0-5 cm depth. It was 1.49 g/cm³ and 1.52 g/cm³ in 5-10 cm for clearcut and partial cut respectively. Only clearcut treatment plot showing a slightly higher mean bulk density (1.54 g/cm³) than partial cut (1.37 g/cm³) in 10-20 cm depth and interestingly no treatment samples showing slightly higher bulk density than partial cut. Data were also collected from no treatment area where the mean bulk densities were 1.02 g/cm³, 1.47 g/cm³ and 1.40 g/cm³ in 0-5, 5-10 and 10-20 cm soil depth.

Mean slash volumes were compared between the two silvicultural techniques used in this study (clearcut and partial cut) and no significant difference was detected (Appendix 17).

Figure 13. Showing the effect of overstory treatment on bulk density at three different soil depth

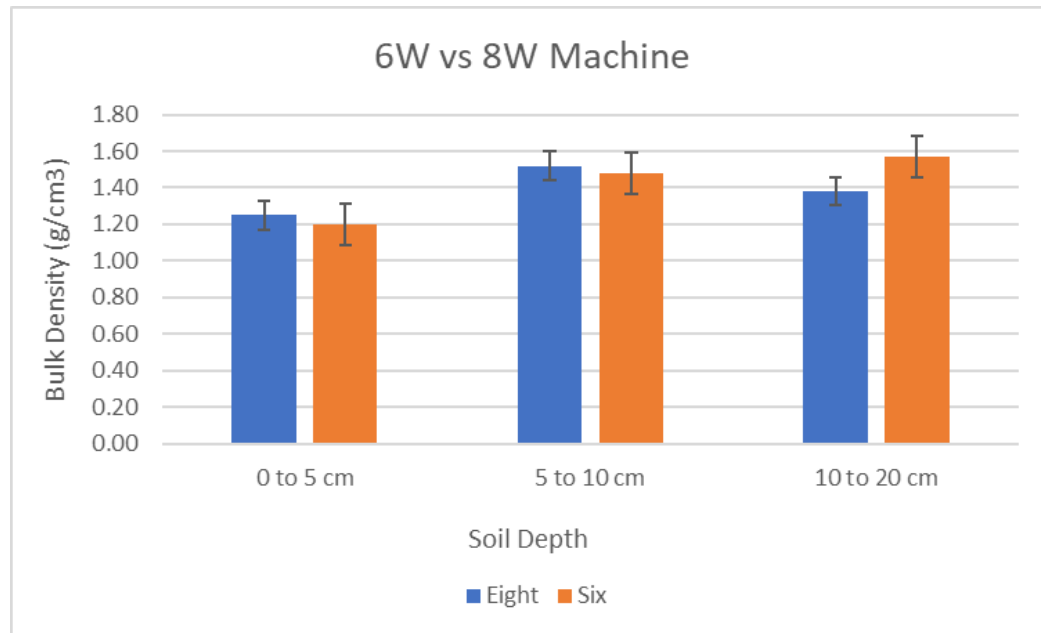


3.3 Effect of 6-Wheeled vs 8-Wheeled Machines

Both a six-wheeled harvester and eight-wheeled harvester were used during the harvest. The mean bulk densities for skid trails used by six-wheeled machine averaged over all levels of machine traffic were 1.20 g/cm³, 1.48 g/cm³, and 1.57 g/cm³ for 0-5 cm, 5-10 and 10-20 cm soil depths, respectively. The mean bulk densities for skid trails used by eight-wheeled machine averaged over all levels of machine traffic were 1.25 g/cm³, 1.52 g/cm³, and 1.38 g/cm³ for 0-5 cm, 5-10, and 10-20 cm soil depths, respectively (Figure 14). One- way ANOVA analysis was conducted to test for differences in bulk density between the two machine types at each soil depth. The results showed that there was no significant effect was found on bulk density for 0-5 and 5-10 soil depth but at 10-20 cm

depth there is significant difference due to six and eight-wheeled machines (Appendices 7-9).

Figure 14. Comparison of soil bulk densities for skid trails used by 8- and 6-wheeled harvesters



3.4 Mixed Effects Model Results

Mixed effects models were run for both full and fine soils, and at each depth (0-5, 5-10 and 10-20 cm). Results show a significant effect of machine traffic and rock content for all models at the $\alpha = 0.05$ level except for the 5-10 full soil – the p-value for traffic for that model was 0.07 (Appendices 1-6).

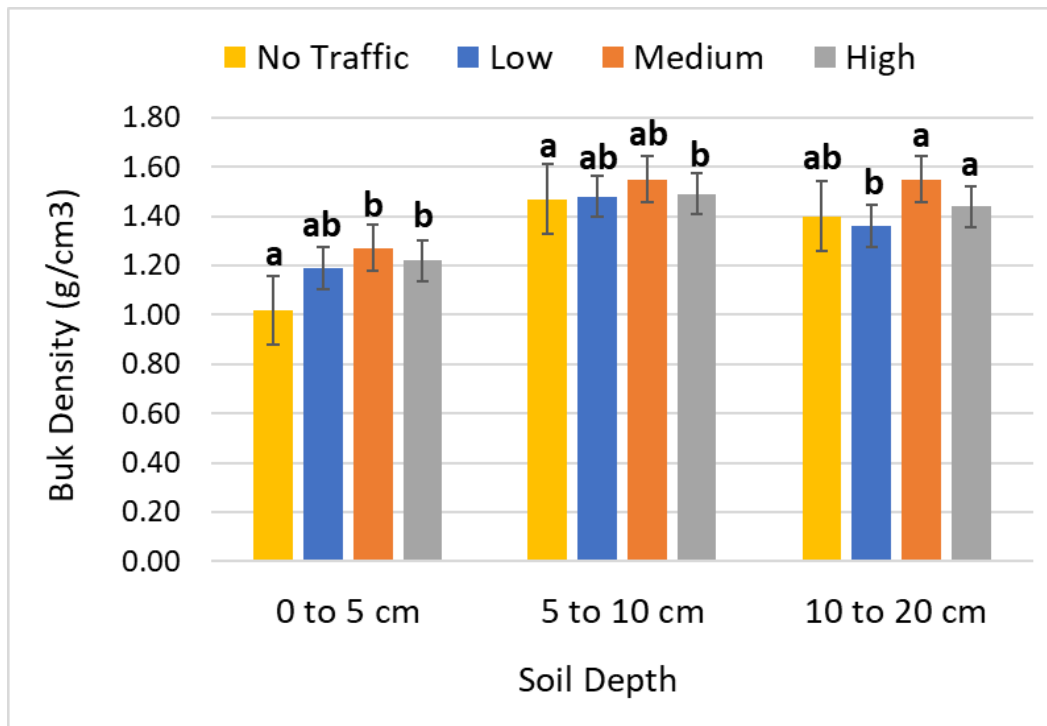
3.4.1. Effect of Traffic Intensity on Bulk Density

The mean bulk densities were greater at the 5-10 cm depth compared to 0-5 cm where the means were 1.48 g/cm³, 1.55 g/cm³, 1.49 g/cm³ and 1.48 g/cm³ for low, medium, high and no traffic respectively. There was no significant difference between low and no traffic. Again, medium traffic intensity also showing the highest bulk density at 5-10 cm soil depth. At the 10-20 cm depth, the

no traffic treatment was not significantly different than the low and high traffic treatment area but it was significantly different than the medium traffic treatments for 10-20 cm depth.

Mixed effects models were run in SAS to understand effects of various on bulk density for each depth of soil. Within SAS, PROC MIXED was used to fit a mixed model that included machine traffic, overstory treatment and slash volume as fixed effects and percent rock content as a random effect. Given that machine traffic was a significant factor in all but two model (5-10 fine and full soil). Bonferroni method was used to determine differences between pairs of machine traffic levels. For 0-5 cm depth, both fine soil and full soil resulted in significant differences in mean bulk density density between no traffic and both medium and high levels of machine traffic. In the 5-10 cm depth, differences in bulk density among traffic levels for full and fine soil were not significantly different at the $\alpha = .05$ level, though just barely (P-value = 0.06 for both fine and full soils at 5-10 cm). On the other hand, there was a difference between high and low and low and medium traffic in the 10-20 cm depth.

Figure 15. Relationship between bulk density and traffic intensity in three different depth (0-5 cm, 5-10 cm and 10-20 cm)



3.4.2 Effect of Rock Content on Bulk Density

To evaluate the effect of rock content on bulk density, an analysis was run in SAS using a mixed effects model where percent rock content was included as a random effect variable. The results show that rock content was a significant positive factor for predicting bulk density in this study. The effect of percent rock content was significant for 0-5 cm, 5-10 cm and 10-20 cm soil depth for both full and fine soil (Appendices 1-6).

3.5 Effects of Snow Depth

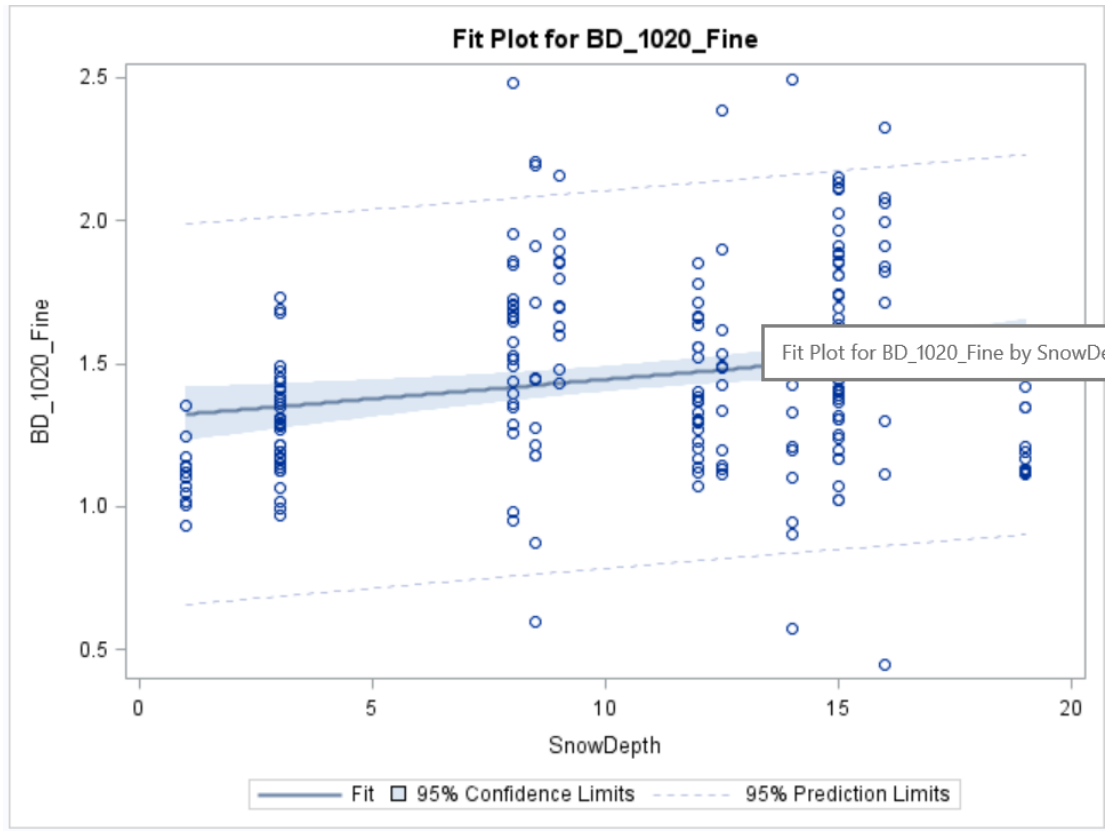
A simple linear regression was used to relate bulk density to snow depth in SAS using Proc GLM method. The results showed no significant relationship for the 0-5 and 5-10 cm depth for both full and fine soils also at 10-20 cm depth for full soil, but there was a significant

effect at the 10-20 depth for fine soil. However, the effect was positive because bulk density increased as snow depth increased.

10-20 Fine:

Parameter	Estimate	Standard Error	t Value	Pr > t
Intercept	1.309040637	0.05149421	25.42	<.0001
SnowDepth	0.013554175	0.00439900	3.08	0.0023

R-Square	Coeff Var	Root MSE	BD_1020_Fine Mean
0.042479	23.05119	0.334556	1.451359

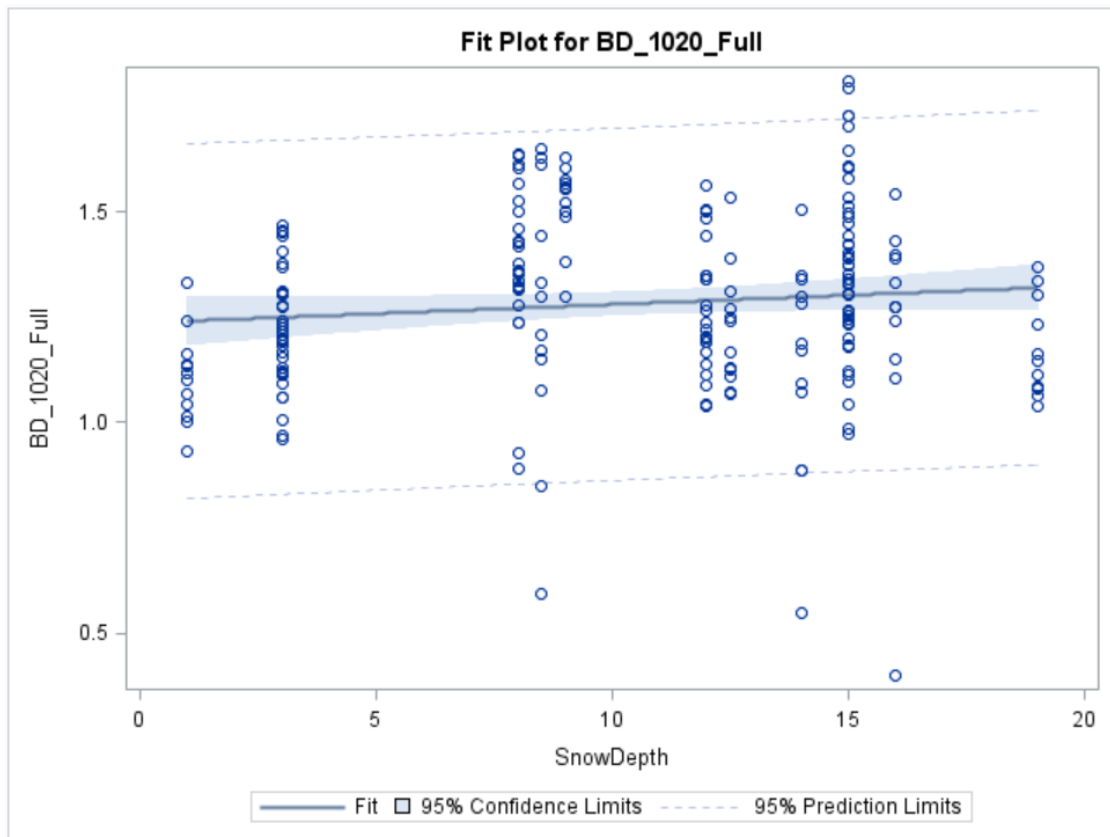


10-20 Full:

Parameter	Estimate	Standard Error	t Value	Pr > t
Intercept	1.236833685	0.03257732	37.97	<.0001
SnowDepth	0.004387303	0.00278299	1.58	0.1164

R-Square Coeff Var Root MSE BD_1020_Full Mean

0.011480 16.49804 0.211653 1.282900



4 Discussion

4.1 Effects of Traffic Intensity

According to the results, mean bulk density within skid trails that experienced low machine traffic levels (1-3 passes) was not significantly greater than the mean bulk density for areas that experienced no traffic at the 0-5 cm depth. However, compared to the no traffic level, bulk density at the medium traffic level (5-7 passes) was 24% greater, and 17% greater for the high traffic level (>8 passes) for the full soil samples (including rock content) which were significant. This result suggests that compaction was significant in the upper layer of the soil once traffic exceeded 3 machine passes. At the 5-10 cm depth, significant differences in bulk density occurred between none and high level machine traffic, suggesting that compaction occurs after 7 machine passes at that depth for both full and fine soils. These results correspond with similar findings on the effects of machine traffic on soil bulk density, which are well-documented.

Jourgholami et al. (2014) observed that most of the changes in bulk density and total porosity happened after fewer than five passes, but significant changes of increases in penetration resistance occurred even after ten passes. On the other hand, Jansson and Johansson (1998) found at 40 to 50 cm depth of a silt loam soil, bulk density becomes higher with the increasing intensity of traffic (4-8 passes) and this happened for both a wheeled machine and a tracked machine. The tracked machine, in contrast, caused compaction at 5 cm depth. The maximum in comparison compaction (42%) occurred at 10 cm depth following eight passes with the tracked machine, whereas with the wheeled machine maximum relative compaction (37%) occurred at 15 cm depth after six passes.

Agherkakli et al. (2010) proved that post-logging soil bulk densities were greatly higher than pre-logging bulk densities. They used two level of slopes (SC1, < 20% and SC2, > 20%) and three levels of traffic intensity (one, five and nine traffics) for their study and observed the increment of bulk density in terms of percentage in SC1 was 3%, 6% and 8% at the one, five and nine traffic frequency, respectively. In SC1 and SC2, the percentage of change in bulk density after the first traffic was 17.6% and 21%, respectively. After first few machines passes the majority of compaction occurs, it becomes less in later on (Han et al., 2006; Wallbrink et al., 2002). Rab and Dignan (2002) reported that about 3% more topsoil disturbance was related to 'wet season' logging.

In general, the effect of traffic intensity on soil bulk density decreases with increasing soil depth (Koolen et al., 1992) and with increasing number of passes, which is reflected in the results of this study. Williamson and Neilsen (2000) conducted a study of six clay to gravelly sandy soils and found that the uppermost (10 cm) portion of soil experienced 62% of soil compaction after a single machine pass, with little increase after following traffic. McNabb et al. (2001) showed that after three machine passes, the increasing rate of bulk densities were 10%, 7% and 4% at five, ten, and twenty cm soil depths respectively on a medium-textured soil. Other authors also recorded similar decreasing patterns at depths down to 30 cm (Han et al., 2009; Williamson and Neilsen, 2000). In the current study, bulk density increased significantly after three machine passes in the 0-5 cm depth and after 7 passes for the 5-10 cm depth.

According to the growth limiting bulk density textural triangle (Figure 2) (Daddow and Warrington, 1983), bulk density for a silt-loam soil occurs between 1.4 and 1.47 g/cm³. In this study, we found that mean bulk densities at the 0-5 cm soil depth were not greater than

1.3 g/cm³, which is lower than the threshold for root growth restriction. However, mean bulk density was highest for medium traffic intensity at 5-10 cm (1.55 g/cm³) and 10-20 cm (1.55 g/cm³) soil depth which could limit tree growth.

4.2 Effects of Slash Volume

There was no significant effect of slash volume on bulk density, according to the data collected in this study. However, McDonald and Seixas (1997) conducted a study where two levels of traffic, three slash densities and two soil moisture contents were measured to quantify soil compaction. They found soil compaction did not reduce after one forwarder pass on dry, loamy sand soils due to slash, but it was noticed for additional passes, where slash did provide some protection. Results from that study indicated that slash cover is mostly beneficial on wet soils. However, another previous study was conducted to identify the effect of machine passes, soil moisture, and slash on penetration resistance in a fine loamy to loam soil using a cut-to-length harvest system (Han et al. 2006). The authors found that slash does not have any significant effects with an increasing number of machine passes and suggested that moist soil may require a high amount of slash to protect it from long term negative impacts of soil compaction. Slash may also it possibly help to reduce ruts as well (Han et al. 2006). Similarly, no effect of slash volume on bulk density was detected for the current study at 0-5, 5-10 and 10-20 cm soil depth.

Hutchings et al. (2002) reported that soil compaction occurs with normal harvesting operations. In that study, they suggested creating slash mat rather than working on bare soil in a clay loam soil in order to decrease compaction. Another report showed that compaction was reduced by 12.9% at a 10 cm soil depth and by 4.5% at 20 cm in a silty clay soil after generating a 10 cm thick slash mat on strip roads (Eliasson and Wästerlund,

2007). In another study, Han et al. (2009) investigated soil compaction on an Andisol soil in a mixed coniferous forest using a cut-to-length and whole-tree harvesting system. Avoiding the negative effect on soil compaction, they suggested leaving an amount of 7–40 kg/m² of slash on the ground. Labelle and Jaeger (2012) also recommended leaving as a minimum of 15–20 kg/m² of slash over highly vulnerable soils and concluded that, although slash mats lose a small amount of capability to distribute the applied loads with increasing machine passes, they are still useful at high traffic frequencies, for example, 12 forwarder cycles. Leaving slash on the ground is hence a useful practice to reduce soil compaction, However, Eliasson and Wästerlund (2007) did not find any major decrease of rut depth after one, two and five machine passes on top of a 10-20 cm thick slash mat in a silty clay forest soil in Sweden.

Akay et al. (2007) suggest that woody material other than slash, such as chip and sawdust also help to decrease soil compaction. It was not suggested to remove slash cover completely if soil needs protection from post-harvesting erosion (Rice and Datzman, 1981; Edeso et al., 1999). Parkhurst et al. (2018) reported that providing slash cover had limited effect on changes in bulk density and porosity than using the forest floor for overland skidding. In our study, though clearcut and partial cut were applied as two overstory treatments to notice if there is any significant effect of slash volume on soil compaction, we did not find any significant effect of slash on soil bulk density. As we know that slash continues to breakdown over time, it can assume that slash will add more organic matter to the ground of this research site and help to regenerate trees also add benefits to some habitat of micro-organism community as well.

4.3 Effects of Percent Rock Content

Houston and Walsh (1993) investigated the differences in rock correction methods designed for compaction of clayey soils in laboratory. They observed very significant differences in maximum dry density using scalp-and-replace procedures compared with the rock correction equations when soil fines are clay. Rücknagel et al. (2013) reported fine earth (A soil which can be passed through a 2-millimeter sieve without grinding its primary particles) in gravelly soils is less vulnerable to compaction. They also observed that a maximum gravel content of around 25% by volume, fine earth bulk density remained nearly constant although the total bulk density of the soil gradually increased.

4.4 Winter Harvesting BMPs

The uniqueness of this study is that, although harvesting is generally preferred and recommended in northern hardwood stands in the Western UP, there has been little research on the effects of harvesting in the winter on soil compaction in this region. However, in light of the findings that medium and high levels of machine traffic resulted in higher bulk densities in this study, winter harvests can still impact soils. It is possible that winter harvesting resulted in less impacts on soils (compaction, rutting, disturbance) than summer harvesting. However, we do not have data with which to compare the effects of season, as we did not collect data of summer harvesting from our study site, or a similar site. Zasada et al. (1987) showed that winter logging is may be preferred to summer because of easier access to different surfaces of floodplains as river and poorly drained areas become frozen. They also observed that tree regeneration can be protected from physical injury by logging with a good snowpack.

Stone (2002) conducted an experiment that examines the effects of winter logging on soil disturbance and regeneration in Western Upper Michigan and reported that drier soil conditions can minimize soil compaction and rutting. Stone (2002) also suggested that plowing snow from skid trails might be a solution that will permit the soil to freeze and improve compaction and rutting and the time of plowing and cost also could be economically advantageous to save equipment maintenance and fuel costs. That might not be practical as the forest floor has many obstacles, such as stumps, rocks and uneven terrain that would make plowing skid trails difficult (unlike plowing roads which are flat and generally free of any stumps or other obstructions). Not only that, removing snow from the skid trail can also cause disturbance to soil nutrients during plowing as the uppermost soil layer becomes disturbed with the blade of the snowplow.

4.5 Limitations and Future Research

Though we did not find any effect of snow depth on bulk density at 0-5 cm and 5-10 cm soil depth but our data showed that there is significant effect at 10-20. It was expected that greater snow depth would protect soils, leading to lower bulk density. However, this study did not control for snow depth, and thus snow depth for the randomly selected plots seemed to cluster around 15 inches, with little variability. In addition, soil moisture content was measured periodically from non-skid trail areas during the harvest, resulting in a range of roughly 35 to 50% moisture content, however soil moisture content was not measured from sampling plots at the time those segments of skid trail were traversed by the logging machines. For this reason, moisture content data were not included in this study. However, previous research has shown that soil moisture content can be a significant factor affecting soil compaction during harvest operations. Finally, although the higher bulk densities

found in the 5-10 cm appear to exceed the threshold at which root growth could be limited, future research is needed to further determine if the compaction observed in these skid trails has any significant effect on tree growth. Thus, it is recommended that future research look at measuring the growth rate of trees from both high and low traffic areas of this study site.

5 Conclusion

This study assessed the effects of percent rock content, slash volume, traffic intensity, overstory treatment and snow depth on bulk density in Ford Forest, Alberta, Michigan.

Four levels of traffic intensities (none, low, medium, high) and two levels of overstory treatments (partial and clearcut) were used to assess the effects where the dependent variable was bulk density, fixed variables were slash volume, traffic intensity and random variable was percent rock content. Separate linear regressions were also run to calculate the effect of snow depth on bulk density at each depth (0-5, 5-10, 10-20 cm).

For 0-5 cm depth, mean soil bulk density for both medium and high levels of machine traffic were significantly greater than the mean bulk density of soils from areas that experienced no machine traffic. However, no significant difference was detected between low traffic and no traffic. Thus, at the 0-5 cm depth, more than three passes can cause increased compaction, however this compaction may not be enough to limit root growth. There was a difference between high-low and low-medium traffic in 10-20 cm depth, suggesting that passes over 7 can result in higher compaction at this depth. The percent rock content has a positive significant effect on bulk density, but no effect was detected for slash volume and snow depth, except at the 10-20 cm depth where snow depth seems to have some effect.

From this study the suggestion for foresters and loggers is, 1) though winter harvesting is generally preferred in order to protect soils, managers still need to be aware of potential impacts to soil for main skid trails that receive higher levels of traffic, 2) although no effect of slash volume on mitigating compaction was detected, it is still recommended to place slash on skid trails during harvest operation due to the benefits of slash reported from

previous studies, and 3) more research is needed for effects of snow as we noticed counterintuitive result at 10-20 cm but not at 0-5 and 5-10 cm depth. At 10-20 cm depth, data showed a significant positive relationship between snow depth and bulk density only for fine soil.

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7 Appendices

Appendix 1. 0-5 fine soil

Type 3 Tests of Fixed Effects				
Effect	Num DF	Den DF	F Value	Pr > F
Plot(Traffic)	15	226	2.92	0.0003
Traffic	3	226	4.97	0.0023
SlashVol	1	226	0.01	0.9430

Solution for Random Effects					
Effect	Estimate	Std Err Pred	DF	t Value	Pr > t
RC_05	3.1506	0.2294	226	13.73	<.0001

Appendix 2. 0-5 full soil

Type 3 Tests of Fixed Effects				
Effect	Num DF	Den DF	F Value	Pr > F
Plot(Traffic)	15	226	3.16	<.0001
Traffic	3	226	5.06	0.0021
SlashVol	1	226	0.01	0.9325

Solution for Random Effects					
Effect	Estimate	Std Err Pred	DF	t Value	Pr > t
RC_05	1.3805	0.2109	226	6.55	<.0001

Appendix 3. 5-10 fine soil

Type 3 Tests of Fixed Effects				
Effect	Num DF	Den DF	F Value	Pr > F
Plot(Traffic)	15	217	3.83	<.0001
Traffic	3	217	2.46	0.0637
SlashVol	1	217	0.13	0.7186

Solution for Random Effects					
Effect	Estimate	Std Err Pred	DF	t Value	Pr > t
RC_510	3.1551	0.2061	217	15.31	<.0001

Appendix 4. 5-10 full soil

Type 3 Tests of Fixed Effects				
Effect	Num DF	Den DF	F Value	Pr > F
Plot(Traffic)	15	226	3.16	<.0001
Traffic	3	226	5.06	0.0021
SlashVol	1	226	0.01	0.9325

Solution for Random Effects					
Effect	Estimate	Std Err Pred	DF	t Value	Pr > t
RC_05	1.3805	0.2109	226	6.55	<.0001

Appendix 5. 10-20 fine soil

Type 3 Tests of Fixed Effects				
Effect	Num DF	Den DF	F Value	Pr > F
Plot(Traffic)	15	225	5.15	<.0001
Traffic	3	225	6.20	0.0005
SlashVol	1	225	0.62	0.4333

Solution for Random Effects					
Effect	Estimate	Std Err Pred	DF	t Value	Pr > t
RC_1020	3.2428	0.1615	225	20.08	<.0001

Appendix 6. 10-20 full soil

Type 3 Tests of Fixed Effects				
Effect	Num DF	Den DF	F Value	Pr > F
Plot(Traffic)	15	226	6.09	<.0001
Traffic	3	226	5.42	0.0013
SlashVol	1	226	0.65	0.4205

Solution for Random Effects					
Effect	Estimate	Std Err Pred	DF	t Value	Pr > t
RC_1020	1.1855	0.1399	226	8.47	<.0001

Appendix 7. Relation of eight and six wheeled machine on bulk density in 0-5 cm soil depth

Anova: Single Factor						
SUMMARY						
<i>Groups</i>	<i>Count</i>	<i>Sum</i>	<i>Average</i>	<i>Variance</i>		
8W	132	164.8235	1.248663	0.050932		
6W	84	100.6058	1.197689	0.109928		
ANOVA						
<i>Source of Variation</i>	<i>SS</i>	<i>df</i>	<i>MS</i>	<i>F</i>	<i>P-value</i>	<i>F crit</i>
Between Groups	0.133385	1	0.133385	1.807043	0.180287	3.88528
Within Groups	15.79614	214	0.073814			
Total	15.92952	215				

Appendix 8. Relation of eight and six wheeled machine on bulk density in 5-10 cm soil depth

Anova: Single Factor						
SUMMARY						
<i>Groups</i>	<i>Count</i>	<i>Sum</i>	<i>Average</i>	<i>Variance</i>		
8W	125	189.8607	1.518885	0.082283		
6W	82	121.7242	1.484441	0.14674		
ANOVA						
<i>Source of Variation</i>	<i>SS</i>	<i>df</i>	<i>MS</i>	<i>F</i>	<i>P-value</i>	<i>F crit</i>
Between Groups	0.058747	1	0.058747	0.545209	0.461126	3.88722
Within Groups	22.08907	205	0.107752			
Total	22.14782	206				

Appendix 9. Relation of eight and six wheeled machine on bulk density in 10-20 cm soil depth

Anova: Single Factor						
SUMMARY						
<i>Groups</i>	<i>Count</i>	<i>Sum</i>	<i>Average</i>	<i>Variance</i>		
8W	132	182.0239	1.378969	0.091216		
6W	84	131.4698	1.565116	0.135989		
ANOVA						
<i>Source of Variation</i>	<i>SS</i>	<i>df</i>	<i>MS</i>	<i>F</i>	<i>P-value</i>	<i>F crit</i>
Between Groups	1.778741	1	1.778741	16.38169	7.24E-05	3.88528
Within Groups	23.23634	214	0.108581			
Total	25.01508	215				

Appendix 10. Comparison among different level of traffic intensities in Bonferroni at 0-5 cm depth for fine soil

Differences of Least Squares Means									
Effect	Traffic	Traffic	Estimate	Standard Error	DF	t Value	Pr > t	Adjustment	Adj P
Traffic	High	Low	0.05811	0.03255	226	1.79	0.0755	Bonferroni	0.4533
Traffic	High	Medium	0.002439	0.03228	226	0.08	0.9398	Bonferroni	1.0000
Traffic	High	None	0.1485	0.04313	226	3.44	0.0007	Bonferroni	0.0041
Traffic	Low	Medium	-0.05567	0.03190	226	-1.75	0.0823	Bonferroni	0.4940
Traffic	Low	None	0.09042	0.04181	226	2.16	0.0316	Bonferroni	0.1897
Traffic	Medium	None	0.1461	0.04256	226	3.43	0.0007	Bonferroni	0.0043

Appendix 11. Comparison among different level of traffic intensities in Bonferroni at 0-5 cm depth for full soil

Differences of Least Squares Means									
Effect	Traffic	Traffic	Estimate	Standard Error	DF	t Value	Pr > t	Adjustment	Adj P
Traffic	High	Low	0.05122	0.03018	226	1.70	0.0910	Bonferroni	0.5460
Traffic	High	Medium	0.01131	0.02993	226	0.38	0.7060	Bonferroni	1.0000
Traffic	High	None	0.1459	0.03999	226	3.65	0.0003	Bonferroni	0.0020
Traffic	Low	Medium	-0.03991	0.02958	226	-1.35	0.1785	Bonferroni	1.0000
Traffic	Low	None	0.09468	0.03876	226	2.44	0.0153	Bonferroni	0.0920
Traffic	Medium	None	0.1346	0.03945	226	3.41	0.0008	Bonferroni	0.0046

Appendix 12. Comparison among different level of traffic intensities in Bonferroni at 5-10 cm depth for fine soil

Differences of Least Squares Means									
Effect	Traffic	Traffic	Estimate	Standard Error	DF	t Value	Pr > t	Adjustment	Adj P
Traffic	High	Low	0.07611	0.03785	217	2.01	0.0456	Bonferroni	0.2734
Traffic	High	Medium	0.02510	0.03785	217	0.66	0.5079	Bonferroni	1.0000
Traffic	High	None	0.1147	0.04960	217	2.31	0.0217	Bonferroni	0.1302
Traffic	Low	Medium	-0.05101	0.03627	217	-1.41	0.1610	Bonferroni	0.9661
Traffic	Low	None	0.03857	0.04652	217	0.83	0.4080	Bonferroni	1.0000
Traffic	Medium	None	0.08959	0.04718	217	1.90	0.0589	Bonferroni	0.3534

Appendix 13. Comparison among different level of traffic intensities in Bonferroni at 5-10 cm depth for full soil

Differences of Least Squares Means									
Effect	Traffic	Traffic	Estimate	Standard Error	DF	t Value	Pr > t 	Adjustment	Adj P
Traffic	High	Low	0.06346	0.03299	223	1.92	0.0557	Bonferroni	0.3340
Traffic	High	Medium	0.02758	0.03261	223	0.85	0.3987	Bonferroni	1.0000
Traffic	High	None	0.1057	0.04334	223	2.44	0.0155	Bonferroni	0.0932
Traffic	Low	Medium	-0.03588	0.03217	223	-1.12	0.2660	Bonferroni	1.0000
Traffic	Low	None	0.04222	0.04159	223	1.02	0.3111	Bonferroni	1.0000
Traffic	Medium	None	0.07810	0.04193	223	1.86	0.0638	Bonferroni	0.3831

Appendix 14. Comparison among different level of traffic intensities in Bonferroni at 10-20 cm depth for fine soil

Differences of Least Squares Means									
Effect	Traffic	Traffic	Estimate	Standard Error	DF	t Value	Pr > t 	Adjustment	Adj P
Traffic	High	Low	0.08914	0.02990	225	2.98	0.0032	Bonferroni	0.0191
Traffic	High	Medium	-0.02667	0.02976	225	-0.90	0.3711	Bonferroni	1.0000
Traffic	High	None	0.07189	0.03993	225	1.80	0.0731	Bonferroni	0.4387
Traffic	Low	Medium	-0.1158	0.02948	225	-3.93	0.0001	Bonferroni	0.0007
Traffic	Low	None	-0.01724	0.03849	225	-0.45	0.6546	Bonferroni	1.0000
Traffic	Medium	None	0.09857	0.03894	225	2.53	0.0121	Bonferroni	0.0723

Appendix 15. Comparison among different level of traffic intensities in Bonferroni at 10-20 cm depth for full soil

Differences of Least Squares Means									
Effect	Traffic	Traffic	Estimate	Standard Error	DF	t Value	Pr > t	Adjustment	Adj P
Traffic	High	Low	0.07930	0.02711	226	2.93	0.0038	Bonferroni	0.0228
Traffic	High	Medium	-0.02033	0.02696	226	-0.75	0.4516	Bonferroni	1.0000
Traffic	High	None	0.05194	0.03591	226	1.45	0.1494	Bonferroni	0.8966
Traffic	Low	Medium	-0.09963	0.02671	226	-3.73	0.0002	Bonferroni	0.0015
Traffic	Low	None	-0.02736	0.03457	226	-0.79	0.4295	Bonferroni	1.0000
Traffic	Medium	None	0.07227	0.03486	226	2.07	0.0393	Bonferroni	0.2358

Appendix 16. Weather data of the research the site between February 2, 2017 to March 26, 2017

Date	Snow	Snow Depth	Temperature MAX	Temperature MIN
2/6/2017	1.2	19	18	11
2/7/2017	2.1	20	22	13
2/8/2017	9.6	27	24	6
2/9/2017	1.2	28	10	-4
2/10/2017	0.4	27	16	-4
2/11/2017	0	26	33	14
2/12/2017	0.4	25	33	21
2/13/2017	0	24	28	7
2/14/2017	0	22	45	20
2/15/2017	0.1	22	35	14
2/16/2017	0	21	18	-1
2/17/2017	0	21	29	10
2/18/2017	0	18	55	29
2/19/2017	0	16	55	25
2/20/2017	0	13	51	29
2/21/2017	0	11	49	38
2/22/2017	0	9	56	35
2/23/2017	2.3	10	49	26
2/24/2017	0	10	32	19
2/25/2017	9.2	16	19	13
2/26/2017	1.2	16	20	9
2/27/2017	2.3	17	28	-1
2/28/2017	0.7	15	40	13
3/2/2017	1.4	15	35	-1
3/3/2017	0.1	15	23	-6
3/4/2017	0	14	18	-8
3/5/2017	0	13	34	11
3/6/2017	0	8	41	34
3/7/2017	0	3	50	27
3/8/2017	0.2	3	42	15
3/9/2017	2.2	4	19	14
3/10/2017	0	3	23	0
3/11/2017	0	3	8	0
3/12/2017	0	3	15	0
3/13/2017	0	3	18	2
3/14/2017	0	3	19	-6
3/15/2017	0	3	28	1

3/16/2017	0	3	28	2
3/17/2017	0	2	43	25
3/18/2017	1.3	2	33	30
3/19/2017	0	1	32	23
3/20/2017	0	1	40	24
3/21/2017	0	1	48	25
3/22/2017	0	1	26	2
3/23/2017	0	1	35	10
3/24/2017	0	1	32	26
3/25/2017	0	1	35	30
3/26/2017	0	0	33	28

Appendix 17. Comparison between mean slash volumes of clearcut and partial cut

Anova: Single Factor						
SUMMARY						
<i>Groups</i>	<i>Count</i>	<i>Sum</i>	<i>Average</i>	<i>Variance</i>		
Partial cut	109	1.61502	0.014817	0.009358		
Clearcut	109	3.81525	0.035002	0.036597		
ANOVA						
<i>Source of Variation</i>	<i>SS</i>	<i>df</i>	<i>MS</i>	<i>F</i>	<i>P-value</i>	<i>F crit</i>
Between Groups	0.022206	1	0.022206	0.966456	0.326665	3.88487
Within Groups	4.963079	216	0.022977			
Total	4.985286	217				