

Distributed vs spot temperature measurements in dynamic rating of overhead power lines

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Abstract

The increase of global energy demand and new ways of electricity production are two of the main challenges for the power sector. The electric market has to address the addition of new and renewable sources of energy to the energy mix and to be able to integrate them into the grid, while maintaining the principles of robustness, security and reliability [1]. All of these changes point to the creation of smart grids, in which advanced generation, information and communication technologies are needed.

An accurate knowledge of the electric grid state is crucial for operating the line as efficiently as possible and one of the most important grid parameters to be measured and controlled is the temperature of the overhead conductors due to their relation with the maximum allowable sag of the line and its thermal limit (annealing).

This paper presents the results of real-time monitoring of an overhead power line using a distributed temperature sensing system (DTS) and compares these results with spot temperature measurements in order to estimate the loss of accuracy of having less thermal information. This comparison has been carried out in a 30 km long distributed temperature sensing system with fiber optic inside a LA-455 conductor and 6 weather stations placed along the line. An area of influence is defined for each weather station corresponding to the orography of the surroundings. The spot temperatures are obtained from the DTS in the nearest point from the weather stations assuming these six locations to be the ones where the spot temperature measurement equipment would be located.

The main conclusion is that, in the case of study, spot measurements are enough to obtain a good approximation of the average temperature of the line conductor.

Keywords: distributed temperature sensing system (DTS), power line, dynamic rating, spot temperature

1. Introduction

2 The increase of global energy demand and new ways of electricity production are two of
3 the main challenges for the power sector. The electric market has to address the addition of

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4 new and renewable sources of energy to the energy mix and to be able to include them into
5 the grid, while maintaining the principles of robustness, security and reliability. All of these
6 changes point to the creation of smart grids, in which advanced generation, information and
7 communication technologies are needed [2, 3].

8 An accurate knowledge of the electric grid state is crucial for operating the line as
9 efficiently as possible and one of the most important grid parameters to be measured and
10 controlled is the temperature of the overhead conductors due to their relation with the
11 maximum allowable sag of the line and its thermal limit[4].

12 This paper presents the results of real-time monitoring of an overhead power line using
13 a distributed temperature sensing system (DTS) [5, 6] and compares these results with spot
14 temperature measurements in order to estimate the loss of accuracy of having less thermal
15 information.

16 **2. Materials and methods**

17 The system of the study is a 220 kV line placed in the north-east of Spain with a LA-455
18 conductor and seasonal static rates (790 A spring, 730 A summer, 760 A autumn and 870 A
19 winter) with a length of approximately 30 km. The line has 6 weather stations distributed
20 uniformly along the line as can be seen in Figure 1. Ambient temperature, humidity, wind
21 and solar radiation data are provided every 5 minutes for all the positions.

22 Additionally, this line has a Distributed Temperature Sensor (DTS) that monitors ap-
23 proximately 10,200 points along the line with a resolution of 2 meters. The values of conduc-
24 tor temperature are provided approximately every 10 minutes. For the operation, the line
25 has been divided into 23 sections. A section is understood as the set of consecutive spans
26 with the same direction. Furthermore, 6 areas of influence are selected for each weather
27 station corresponding to the orography of the surroundings.



Figure 1: Weather stations placed in the line

28 From 10 September 2013 to 31 March 2014 environmental conditions and conductor
29 temperature measurements were recorded and all the information was then analyzed in

30 several ways in order to obtain a better knowledge of the accuracy of the measurements.
 31 The idea was to estimate the loss of accuracy when just spot temperature measurements can
 32 be recorded, in this case one measurement close to each weather station, instead of having
 33 all the distributed thermal information.

34 To do so, the average, maximum and minimum temperatures obtained in each area of
 35 influence by the DTS were stored with 10 minutes resolution. At the same time, the closest
 36 DTS measurement to the weather stations were also stored.

37 **3. Results**

38 Once the type of monitoring system used in this study was explained, the main results
 39 are presented. This section is divided in the results of the spot temperature measurements
 40 and the distributed ones and then a comparison between both is made.

41 *3.1. Spot temperature measurements, T_c*

42 The spot temperatures are obtained from the DTS in the nearest point from the weather
 43 stations assuming these six locations to be the ones where the spot temperature measurement
 44 equipment would be located.

45 *3.2. Distribution temperature measurements, T_{max} , T_{min} , T_{av}*

46 The distributed temperature measurements are divided in the areas of influence of the
 47 6 weather stations and the average, T_{av} , the minimum, T_{min} , and the maximum, T_{max} ,
 48 temperatures recorded in every area are presented.

49 The maximum temperature difference detected between the maximum and the minimum
 50 temperature measurements in an area of influence was 24.8°C.

51 If this data is split in the different areas of influence, the maximum and minimum dif-
 52 ferences are summarized in Table 1.

Table 1: Maximum and minimum temperature differences

Area	Max. diff.	T_{max}	T_{min}	T_{av}	Min. diff.	T_{max}	T_{min}	T_{av}
1	24.8	30.6	5.8	15.5	5.3	23	17.7	20.2
2	16.7	24.6	7.9	15.9	4.4	27.7	23.3	25.6
3	17.8	22.6	4.8	12.4	4.2	11.4	7.2	9.3
4	20.1	21.4	1.3	8.9	4.1	18	13.9	15.7
5	19.3	34.4	15.1	24.3	4.8	9	4.2	6.6
6	19.5	19.5	0	14.6	4.4	8.1	3.7	5.8

53 It can be noticed that the minimum difference is between 4 and 5°C and the maximum
 54 between 17 and 25°C. Another interesting result is that this difference increases as the
 55 ambient temperature decreases as can be seen in Figure 2. This is an important aspect in
 56 the study of the critical values as the differences are reduced when the ambient temperature
 57 increases.

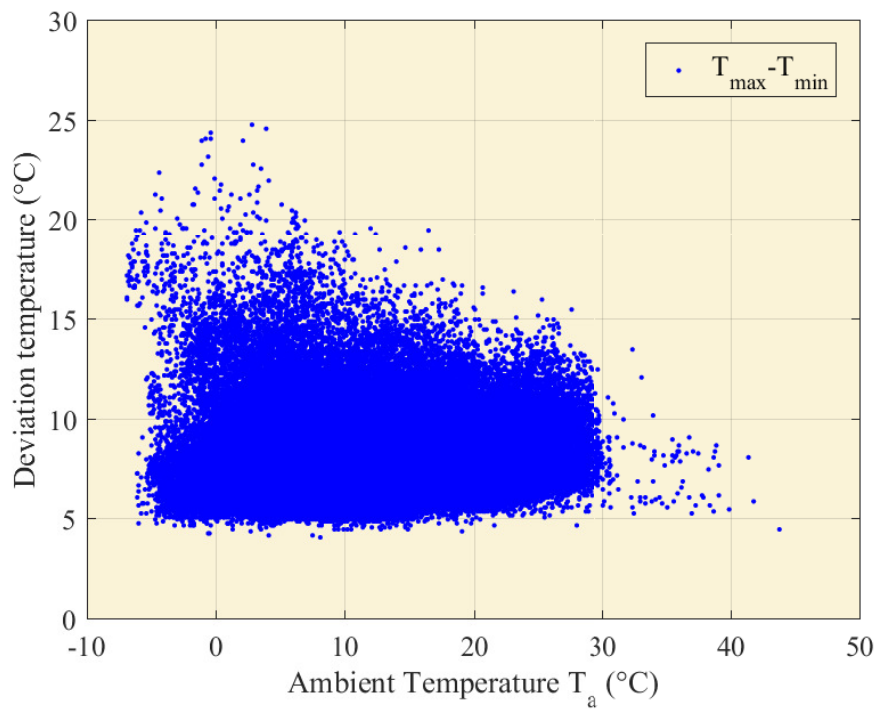


Figure 2: Temperature difference vs ambient temperature

58 However, the most critical parameter in the decrease of the difference between the max-
59 imum and minimum temperature measured in an area of influence is the wind speed. As
60 it increases, the distributed temperature tends to be more homogeneous as can be seen in
61 Figure 3 and it is predicted in the literature [7, 8].

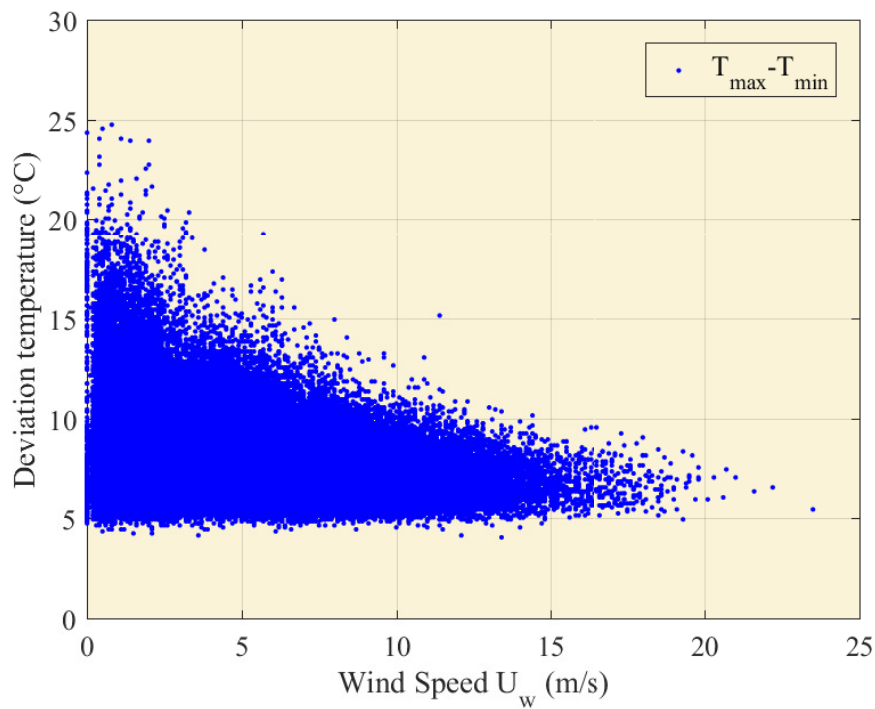


Figure 3: Temperature difference vs wind speed

62 *3.3. Distributed vs spot temperature measurements*

63 The first thing to be noted is that the average of the distributed temperature and the spot
 64 temperature measured nearby the weather station are very similar, with the main difference
 65 in the smoothness of the temperature profile and with variations lower than $\pm 5^\circ\text{C}$ in more
 66 than 99 of the cases as can be seen in figures 4 and 5.

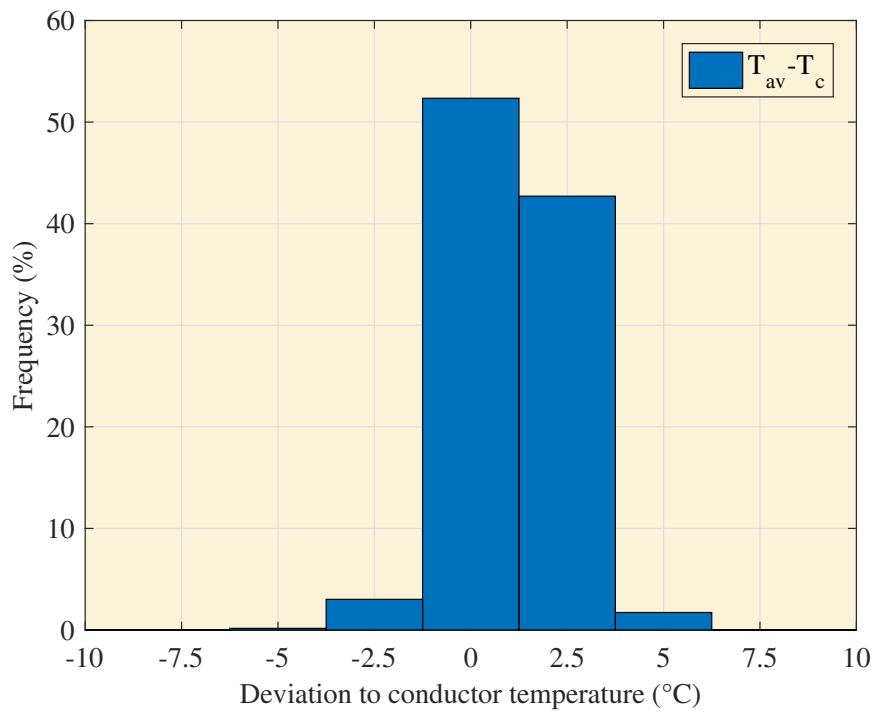


Figure 4: Temperature difference frequency ($T_{av} - T_c$)

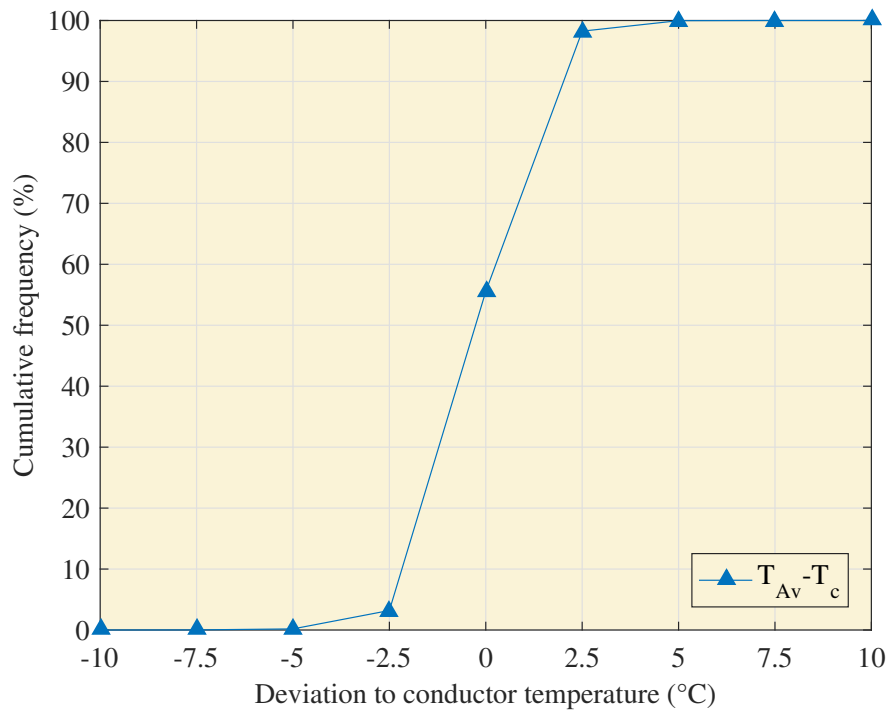


Figure 5: Temperature difference accumulated frequency ($T_{av} - T_c$)

67 As a matter of example a specific day is represented in figure 6 with the values of the
 68 spot temperature, the average, minimum and maximum distributed temperatures for the
 69 corresponding area of influence. Furthermore, solar radiation, ambient temperature and
 70 current are also represented.

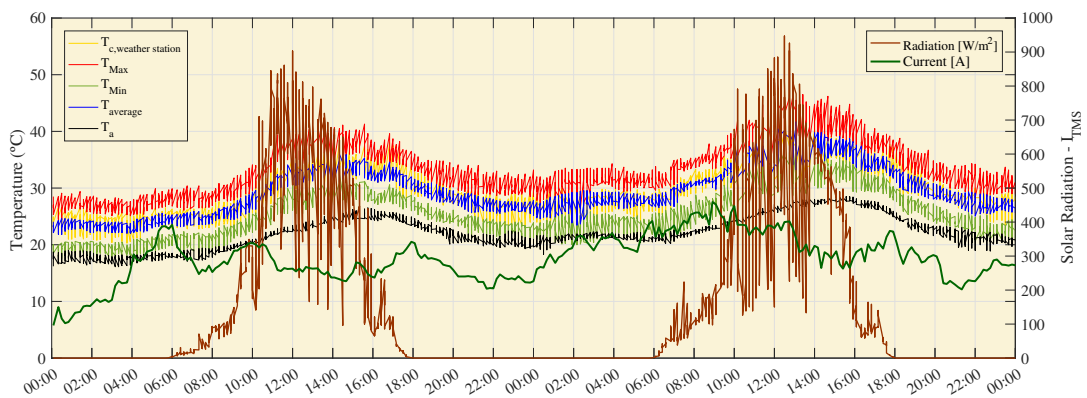


Figure 6: Main line and weather parameters for a specific day

71 Even in the cases with the highest conductor temperatures the differences between the
 72 spot and average temperature are inside $\pm 5^\circ\text{C}$. This is an important conclusion in favor of

73 the discrete temperature measurements to be extrapolated as the average vane temperature
74 to calculate sag elongations.

75 Table 2 shows the average of the standard deviation of T_c , T_{av} , T_{max} and T_{min} for
76 the 6 areas of influence, i .e, in every recorded sample the standard deviation between the
77 values of the measures of the six areas of influence is calculated and then the average of the
78 standard deviation for all the recorded samples is summarized.

Table 2: Average of the standard deviation between areas of influence

Temperature measurement	Standard deviation
T_c (spot temperature)	1.6
T_{av} (average temperature of the area of influence)	1.2
T_{max} (average temperature of the area of influence)	1.7
T_{min} (average temperature of the area of influence)	1.2

79 In order to continue evaluating the effect of measuring the distributed temperature and
80 the spot temperature, the average of the distributed temperature measured for the total
81 length of the line is compared with the average of the temperature measured in the 6
82 spot zones, close to the weather stations. The result is that for the more than 17.000
83 measurements, the difference between making the average of all the distributed temperatures
84 and the average just for the 6 spot measurements is less than 3°C , with a difference average of
85 0.1 and a standard deviation of 0.5. Figures 7 and 8 represent the frequency and accumulated
86 frequency of the difference between the two averages.

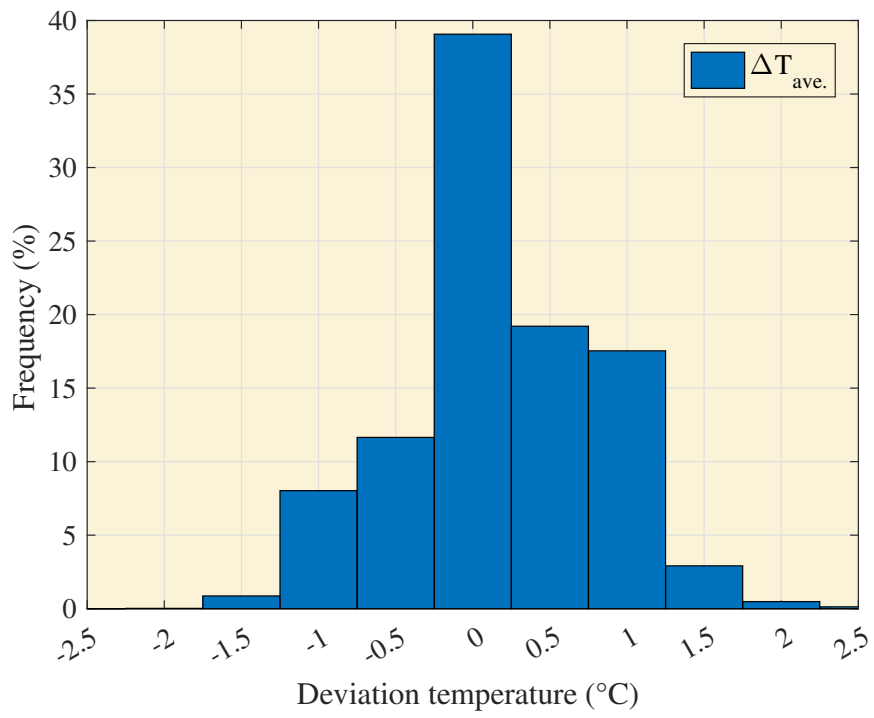


Figure 7: Temperature difference frequency ($\overline{T_{av}} - \overline{T_c}$)

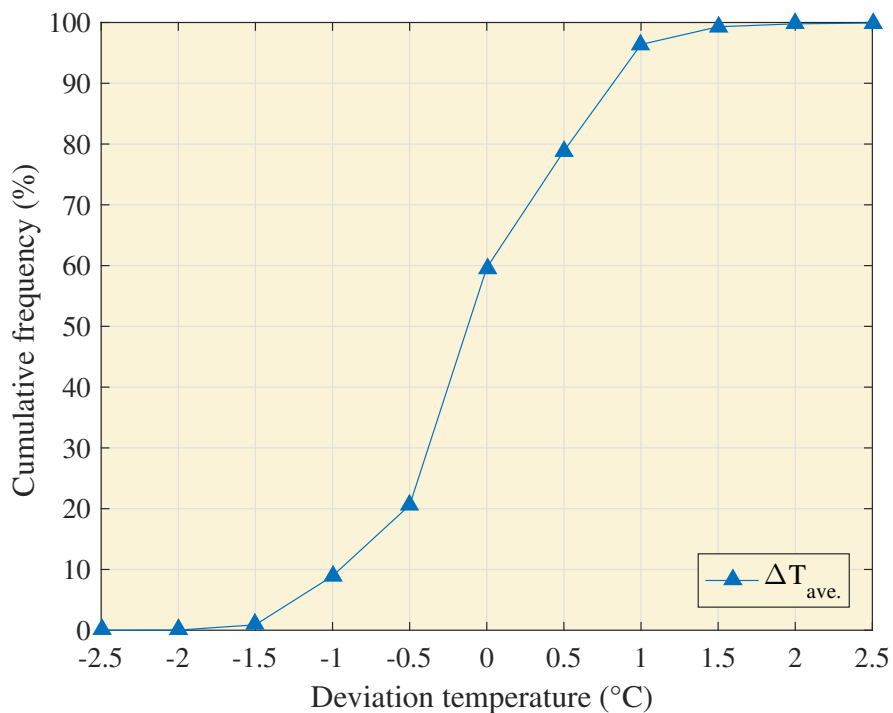


Figure 8: Temperature difference accumulated frequency ($\overline{T_{av}} - \overline{T_c}$)

87 4. Conclusions

88 30 km of a high voltage power line were monitored with a distributed temperature
 89 sensing system (DTS) and six weather stations placed along the line from 10 September
 90 2013 to 31 March 2014. These data were recorded every 10 minutes and the conductor
 91 temperature measured every 2 meters.

92 The data analysis was focused on the differences between using spot or distributed tem-
 93 perature measurements in dynamic rating operation of overhead power lines. Distributed
 94 temperature sensors are very expensive to implement and needs to stop the line operation
 95 for a considerable period of time. Spot temperature sensors are cheaper and faster to im-
 96 plement but with the uncertainty of where to place them to have a representative value of
 97 the temperature of the conductor.

98 This paper shows that, in the case studied, spot measurements are enough to obtain
 99 a good approximation of the temperature of the line conductor. The line was not heavily
 100 loaded during the time of the study and no temperatures above 50°C were reached. Further
 101 analysis should be done to check a broader range of load and weather conditions in order to
 102 be used in dynamic rating operation.

103 References

- 104 [1] A. Arroyo, P. Castro, M. Manana, R. Domingo, A. Laso, Co2 footprint reduction and efficiency increase
 105 using the dynamic rate in overhead power lines connected to wind farms, Applied Thermal Engineering

- 106 130 (2018) 1156 – 1162. doi:<https://doi.org/10.1016/j.applthermaleng.2017.11.095>.
107 URL <http://www.sciencedirect.com/science/article/pii/S135943111733497X>
- 108 [2] E. Carlini, G. Giannuzzi, C. Pisani, A. Vaccaro, D. Villacci, Experimental deployment of a self-organizing
109 sensors network for dynamic thermal rating assessment of overhead lines, *Electric Power Systems Re-*
110 *search* 157 (2018) 59 – 69. doi:<https://doi.org/10.1016/j.epsr.2017.12.007>.
111 URL <http://www.sciencedirect.com/science/article/pii/S0378779617304789>
- 112 [3] E. Carlini, C. Pisani, A. Vaccaro, D. Villacci, A reliable computing framework for dy-
113 namic line rating of overhead lines, *Electric Power Systems Research* 132 (2016) 1 – 8.
114 doi:<https://doi.org/10.1016/j.epsr.2015.11.004>.
115 URL <http://www.sciencedirect.com/science/article/pii/S0378779615003302>
- 116 [4] D. L. Alvarez, F. F. da Silva, E. E. Mombello, C. L. Bak, J. A. Rosero, D. L. Iason, An approach
117 to dynamic line rating state estimation at thermal steady state using direct and indirect measure-
118 ments, *Electric Power Systems Research* 163 (2018) 599 – 611, *advances in HV Transmission Systems*.
119 doi:<https://doi.org/10.1016/j.epsr.2017.11.015>.
120 URL <http://www.sciencedirect.com/science/article/pii/S0378779617304595>
- 121 [5] A. Ukil, H. Braendle, P. Krippner, Distributed temperature sensing: Review of technology and applica-
122 tions, *IEEE Sensors Journal* 12 (5) (2012) 885–892. doi:10.1109/JSEN.2011.2162060.
- 123 [6] K. Morozovska, P. Hilber, Study of the monitoring systems for dynamic line rating, *Energy Procedia*
124 105 (2017) 2557 – 2562, 8th International Conference on Applied Energy, ICAE2016, 8-11 October 2016,
125 Beijing, China. doi:<https://doi.org/10.1016/j.egypro.2017.03.735>.
126 URL <http://www.sciencedirect.com/science/article/pii/S1876610217307981>
- 127 [7] A. Arroyo, P. Castro, R. Martinez, M. Manana, A. Madrazo, R. Lecuna, A. Gonzalez, Comparison
128 between IEEE and CIGRE thermal behaviour standards and measured temperature on a 132-kV overhead
129 power line, *Energies* 8 (12) (2015) 13660–13671. doi:10.3390/en81212391.
130 URL <http://www.mdpi.com/1996-1073/8/12/12391>
- 131 [8] P. Castro, A. Arroyo, R. Martinez, M. Manana, R. Domingo, A. Laso, R. Lecuna, Study of dif-
132 ferent mathematical approaches in determining the dynamic rating of overhead power lines and a
133 comparison with real time monitoring data, *Applied Thermal Engineering* 111 (2017) 95 – 102.
134 doi:<https://doi.org/10.1016/j.applthermaleng.2016.09.081>.
135 URL <http://www.sciencedirect.com/science/article/pii/S1359431116316891>