

# Analysis of Magnetization effects for HTS conductors for HEP magnets

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CORC Samples:  
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Advanced  
Conductor  
Technologies and  
University of  
Colorado  
Twisted Strand:  
University of  
Houston



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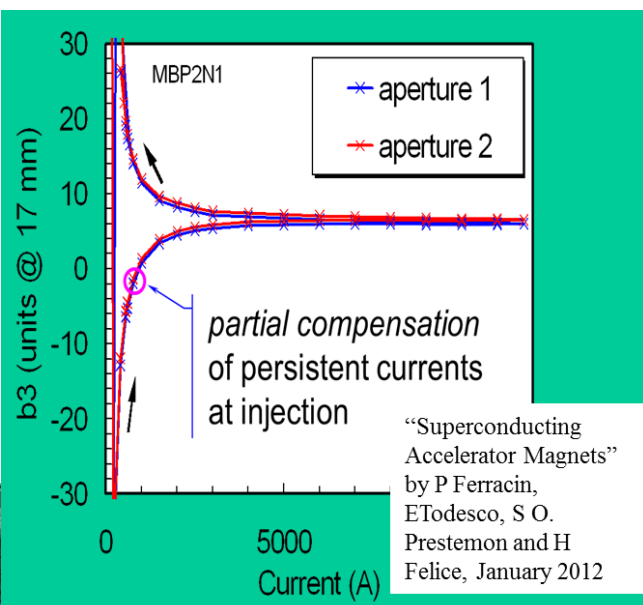
# Outline of talk

- Motivation - accelerator quality
- Comparison of accelerator and b3
- Magnetization of Tape vs Cable
- Magnetization of various cable types
- Coupling -- Magnetization -- loss?
- Decay and its implications

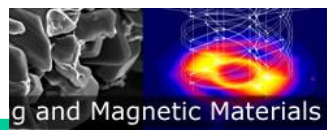
# Why the focus on Magnetization? - its b3 and its change for accelerator magnets

Strand type	NbTi <sup>(1)</sup>	Nb <sub>3</sub> Sn <sup>(2)</sup>	Bi:2212 <sup>(3)</sup>	YBCO	YBCO
Cable type	Rutherford	Rutherford	Rutherford	TSTC	CORC™
Cable packing factor, $\lambda_c$	0.88	0.855	0.87 <sup>(4)</sup>	0.56	0.58
Strand filling factor, $\lambda_s$	0.385	0.455	0.26	0.01 <sup>(5)</sup>	0.01 <sup>(5)</sup>
Layer CCD, $J_{c,inj}$ , kA/mm <sup>2</sup>	20.4	-	1.75	88 <sup>(6)</sup>	88 <sup>(6)</sup>
Eng. CCD <sup>(7)</sup> , $J_{e,inj}$ , kA/mm <sup>2</sup>	7.85	-	0.455	0.88	0.88
Fil. (strand) size, $d_{eff}$ , $\mu\text{m}$	7	61	278	4000 <sup>(8)</sup>	4000 <sup>(10)</sup>
$J_{cable,inj}$ kA/mm <sup>2</sup>	6.91	13.0	0.396	0.493	0.510
$J_{cable,coll}$ kA/mm <sup>2</sup>	0.704	0.855	0.348	0.244	0.232
$B_{b,coll}$ , T	8	15	20	20	20
$b_3$ , units <sup>(11)</sup>	3	41	19	330 <sup>(12)</sup>	330 <sup>(12)</sup>
$b_{3*}$ , units <sup>(13)</sup>			37	99	99

This is based on an estimation from Tape

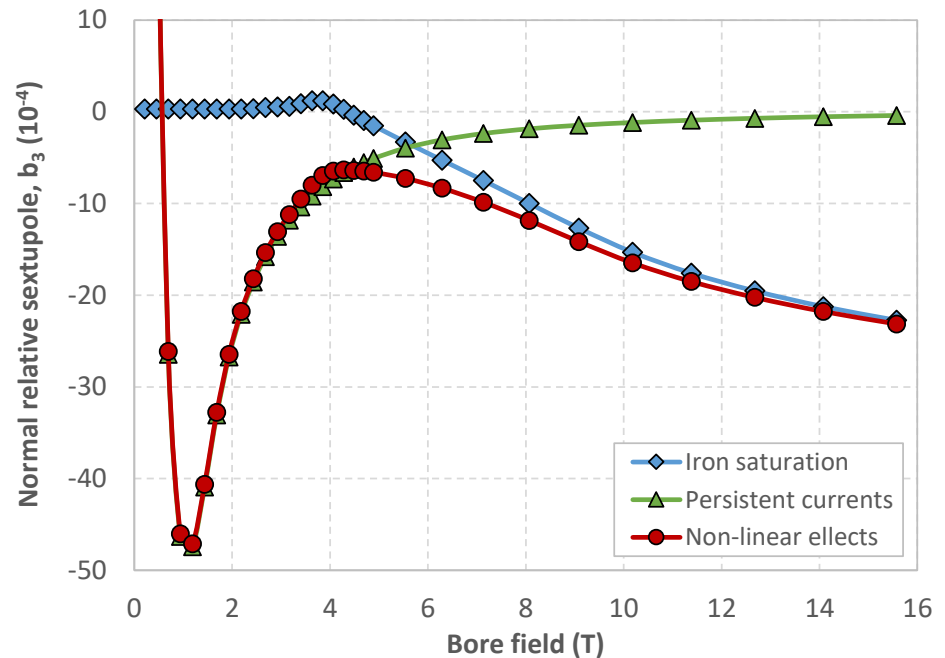
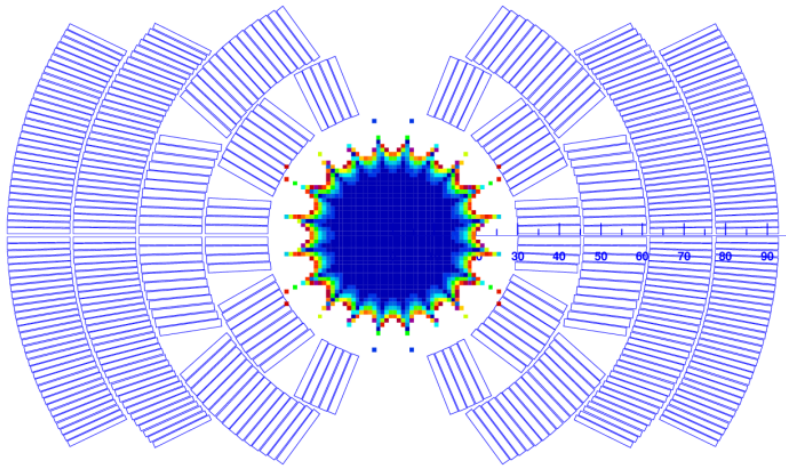


Sample	B, T	orientation	-M <sub>0</sub> , kA/m	-M <sub>20min</sub> , kA/m	$\Delta M_{20min}/M_0$ , %	$\Delta b_3$ , %
Bi:2212						
	1 T	⊥ axis	15	12	20	20
	12 T	⊥ axis	2.7	1.5	42	42
YBCO						
	1 T	B//c	991	906	9	9
	1 T	45°	933	811	14	14
	12 T	B//c	280	187	33	33
	12 T	45°	229	200	13	13



# Cos theta coil MDP

## Nb<sub>3</sub>Sn RRP Conductor



A Zlobin, “15 T dipole design concept, magnetic design and quench protection”, Presentation at the US MDP workshop Jan 2017

# Canted cos theta Dipole

## NbTi Strand

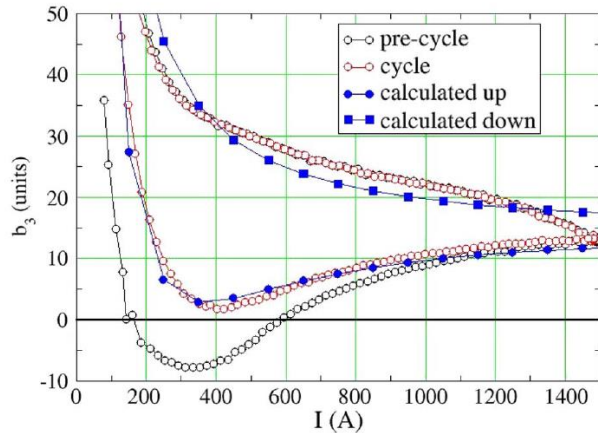


Fig. 11. Combined geometric and magnetization sextupole up to 1500 A.

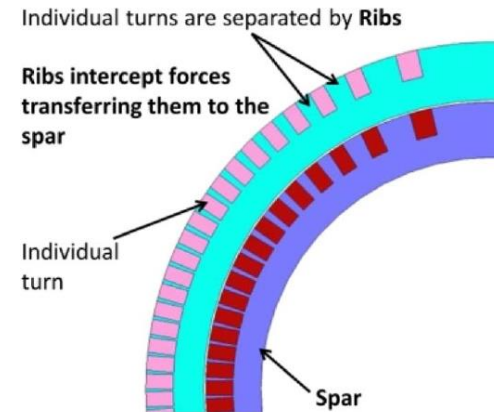
TABLE I  
CCT1 MAGNETIC PARAMETERS

Symbol	Units	Value
Strand diameter (SSC outer)	mm	0.65
Strands per cable		8
Bare cable	mm	2.72x1.07
Insulated cable	mm	3.02x1.37
Cable keystone angle	Deg.	0
Channel size	mm	3.02x1.59
Clear bore dia.	mm	50.8
Number of layers		2
Layer1/2 radial spar thickness	mm	3.07
Between layers radial insulation	mm	0.25
Layer1/2 canted angle	Deg.	15
Layer 1/2 No. of turns		78/72
Layer 1/2 single turn length	mm	499/604
Mandrels length	mm	841.1
Axial pitch length	mm	7.60
Minimum rib thickness (mid-plane)	mm	0.38
Maximum rib thickness (pole)	mm	6.02

IEEE TRANSACTIONS ON APPLIED SUPERCONDUCTIVITY, VOL. 25, NO. 3, JUNE 2015

## Test Results of CCT1—A 2.4 T Canted-Cosine-Theta Dipole Magnet

S. Caspi, L. N. Brouwer, T. Lipton, A. Hafalia Jr, S. Prestemon, D. R. Dietderich, H. Felice, X. Wang, E. Rochepault, A. Godeke, S. Gourlay, and M. Marchevsky





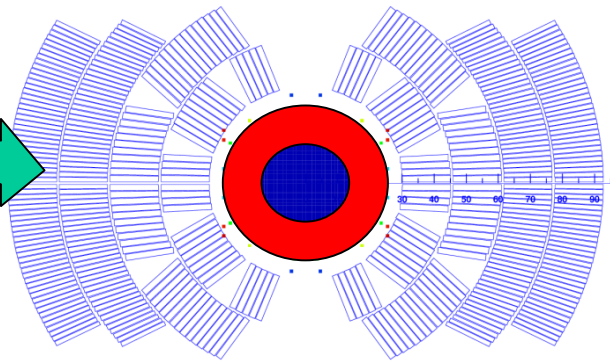
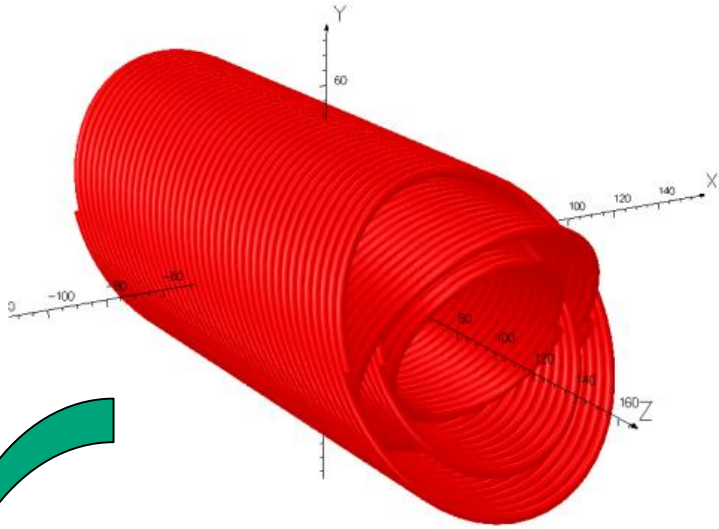
# Canted Cos Theta dipole 2

X Wang of LBNL proposes to make a 4 layer canted cos dipole using YBCO cable

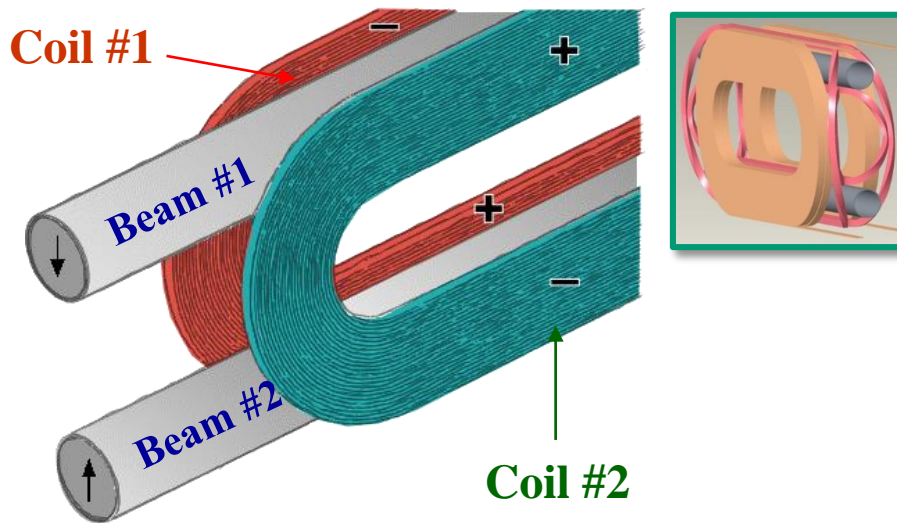
- As part of LBNL-OSU collaboration, Nb<sub>3</sub>Sn magnetization measurements and Bi:2212 magnetization data have been provided for error field calculations in other magnet designs
- This collaboration is expanded to include YBCO conductor and cable magnetization for magnets, and collaboration on error field determination

X. Wang, “REBCO accelerator magnet development: status and plans”, Presented at the USMDP NAPA, Jan 2017

- If we consider for a moment the simplest case of an HTS insert in a background Nb<sub>3</sub>Sn magnet, then at injection, it may be reasonable to approximate field on CCT as a “uniform 1 T”
- Initial error estimates using biot savart (and a doublet approach) suggest significant b<sub>3</sub> for CCT wound with YBCO cables, as expected extrapolating from CCT1 > 25 unit

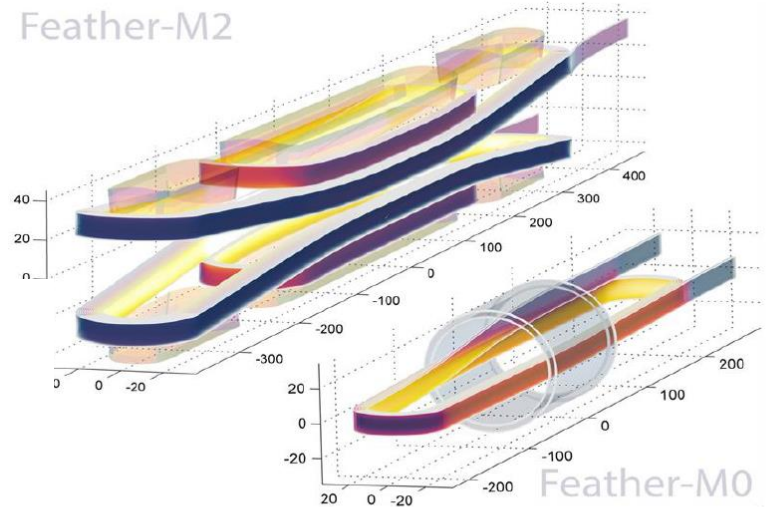


# A number of other designs and possibilities



Ramesh Gupta, "Hybrid Configuration and BNL Activities", USMDP, 2017

## Accelerator Quality HTS Dipole Magnet Demonstrator Designs for the EuCARD-2, 5 Tesla 40 mm Clear Aperture Magnet



1. Aligned block development HTS magnets, (bottom right) Feather-M0 rich detection development coil, (top left) Feather-M2 the EuCARD-2 five a standalone approaching accelerator field quality insert magnet.

G. A. Kirby, J. van Nugteren, A. Ballarino, L. Bottura, N. Chouika, S. Clement, V. Datskov, L. Fajardo, J. Fleiter, R. Gauthier, L. Gentini, L. Lambert, M. Lopes, J.C. Perez, G. de Rijk, A. Rijllart, L. Rossi, H. ten Kate, (CERN), M. Durante, P. Fazilleau, C. Lorin (CEA), E. Härö, A. Stenvall, (TUT), S. Caspi, M. Marchevsky, (LBNL), W. Goldacker, A. Kario, (KIT)

# What does the magnetization of HTS, esp YBCO, look like?

For round strands – Nb<sub>3</sub>Sn, Bi2212, the simple rules are

1. For  $B$  perpendicular,  $B \gg B_p$

Full field penetration

$$\Delta M = \frac{4}{3\pi} d_{eff} J_c$$

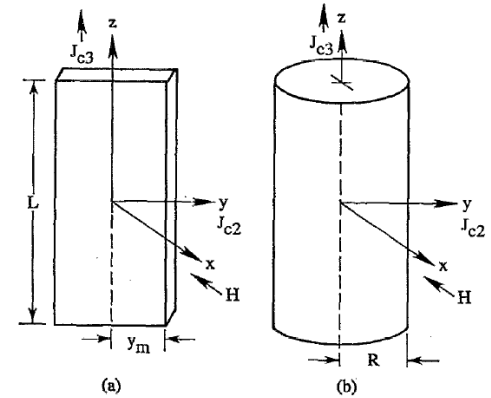
$$B_p = \mu_0 0.8 J_c d_{eff}$$

cylinders

$$\Delta M = a J_c$$

$$B_p = \mu_0 J_c a$$

slabs



2. For  $B$  Perpendicular,  $B \ll B_p$

No or nearly no penetration

$$M = -2H$$

cylinders

$$M = -H$$

slabs

Only true if  $B \parallel$  to thin edge



# What does the magnetization of HTS, esp YBCO, look like?

For flat strands with  $B \perp$  tape

1. For  $B$  perpendicular,  $B \gg B_p$

$$\Delta M = aJ_c$$

$a$  is half width

slabs

But,  $B_p$  for  $B \perp$  slab much lower than  $B_p$  for cylinder or slab with  $B //$  slab

$$H_p \approx J_c \left( \frac{t}{\pi} \right) \left( \ln \frac{w}{t} + 1 \right)$$

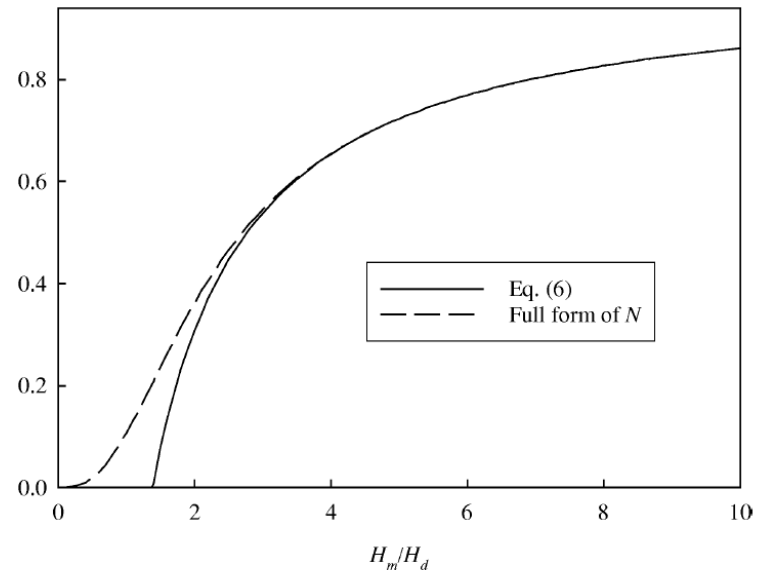
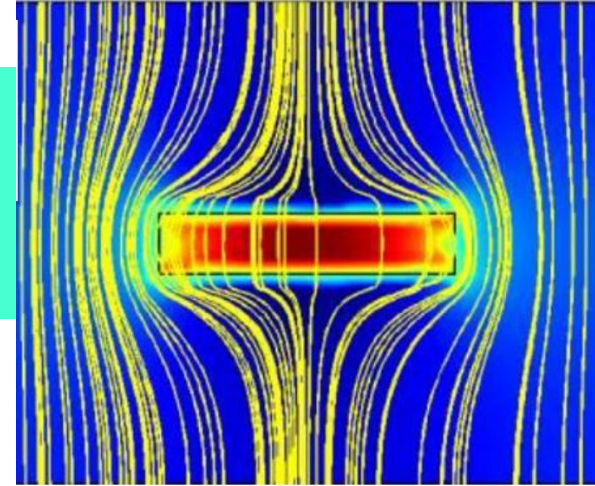
2. For  $B$  perpendicular,  $B \ll B_p$

$M = -\infty$  As the width becomes infinite

3. For  $B$  perpendicular,  $B \approx B_p$

$$\Delta M = NaJ_c \quad N = 2 \left( \frac{H_d}{H_m} \right) \text{Ln} \left( \cosh \frac{H_m}{H_d} \right) - \tanh \left( \frac{H_m}{H_d} \right) \approx \left( 1 - \frac{1.4}{(H_m/H_d)} \right)$$

$H_m$  is the applied field and  $H_d = 0.4J_c t$



# What does the magnetization of HTS, esp YBCO, look like?

4. For B perpendicular

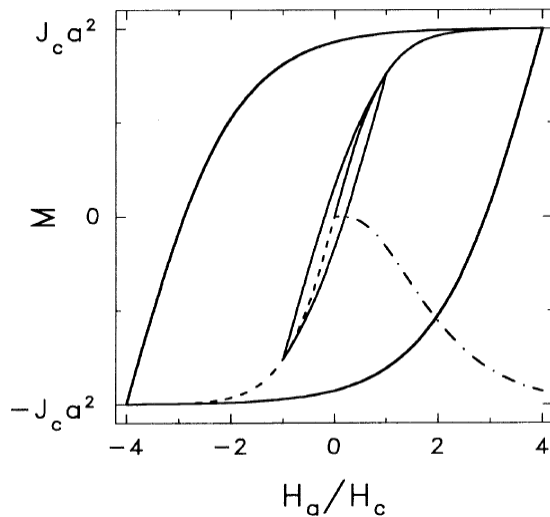
$$M = \pi a^2 H_a (1 - H_a^2 / 3H_c^2)$$

$$H_a \ll H_c$$

$$M_{\uparrow\downarrow} = \pm J_c a^2 \left[ \tanh \frac{H_0}{H_c} + 2 \tanh \frac{H_a \mp H_0}{2H_c} \right]$$

$$M = J_c a^2 [1 - 2 \exp(-2H_a/H_c)] \quad H_a \gg H_c$$

$$M_{\uparrow\downarrow} = M/L = J_c t a^2 = J_{cs} a^2$$



$a$  is half width of tape

$H_a$  is applied field

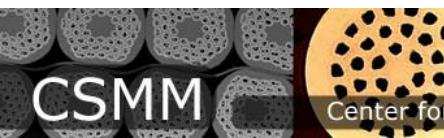
$H_c = J_c / \pi$ , where  $J$  is sheet current A/m

$J_{cs} = \text{usual } J_c * t$

$H_0 = H_{max}$

$M_{\uparrow\downarrow}$  is moment per unit length

$$M = m/Lta$$



**Type-II-superconductor strip with current  
in a perpendicular magnetic field**

Ernst Helmut Brandt and Mikhail Indenbom\*

# So, let's try some numbers for Tape

Conductor spec

t	2 microns	0.000002	m
w	4 mm	0.004	m
Jc		2.5E+11	A/m <sup>2</sup>
lc		2000	A

4 K, 200 A 77 K

If the sample was very thick --

$$B_p = \mu_0 J_c a \approx 1000 \text{ T (4 K) or } 100 \text{ T 77 K}$$

But for real YBCO which is quite thin ...

$$H_p \approx 0.4 J_c t \left[ \ln \left( \frac{d}{t} \right) + 1 \right]$$

Bp YBCO		1.520280467	T	4 K
		0.152028047	T	77 K

For flat strands with  $B \perp$  tape,  $B \gg B_p$   $M = (a/2)J_c =$

	Film norm	Film norm	tape norm
	A/m	kA/m	kA/m
del M=	500000000	500000	10000

12.56	Tesla	4 K
1.256	Tesla	77 K

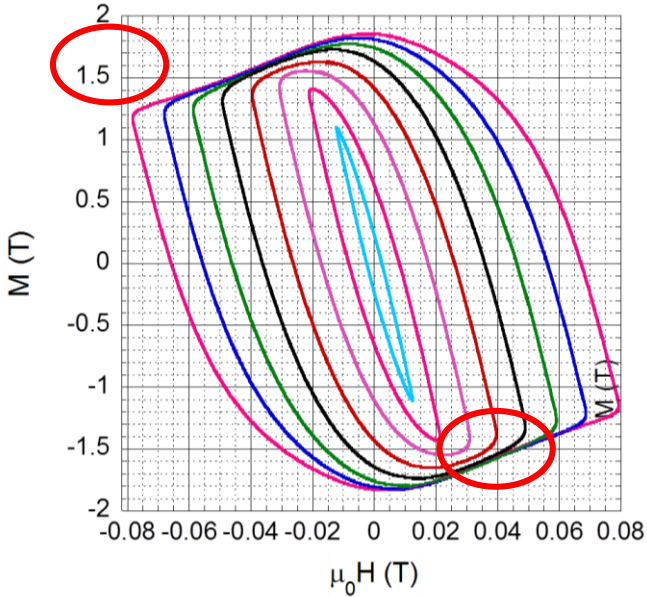
4 K, 1000 kA/m 77 K



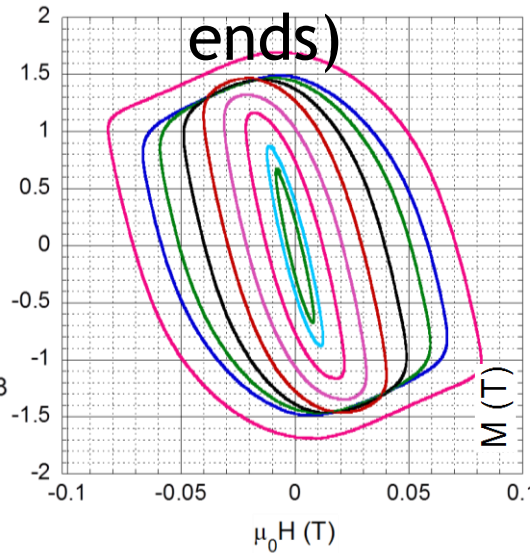
# Measured Loss in Striated and Twisted YBCO

## University of Houston tape samples

Un-Striated

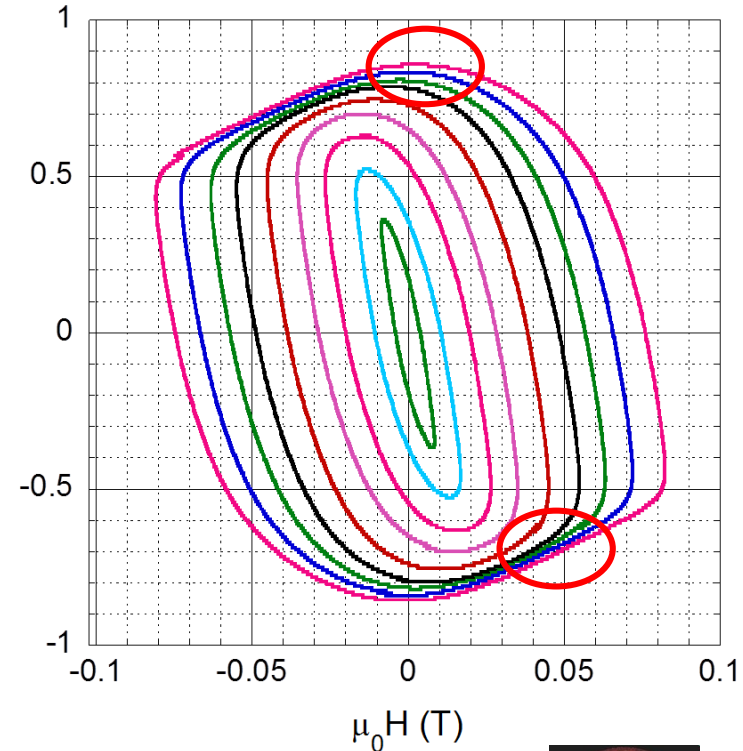


Striated  
(soldered  
ends)



Striated and  
Twisted

77 K data



width = 12 mm  
length = 16.1 cm  
Thickness = 70  $\mu\text{m}$

Unstriated,  $B_p = 0.04$  T,  $M = 1.5$  T

Striated,  $B_p = 0.04$  T,  $M = 0.8$  T

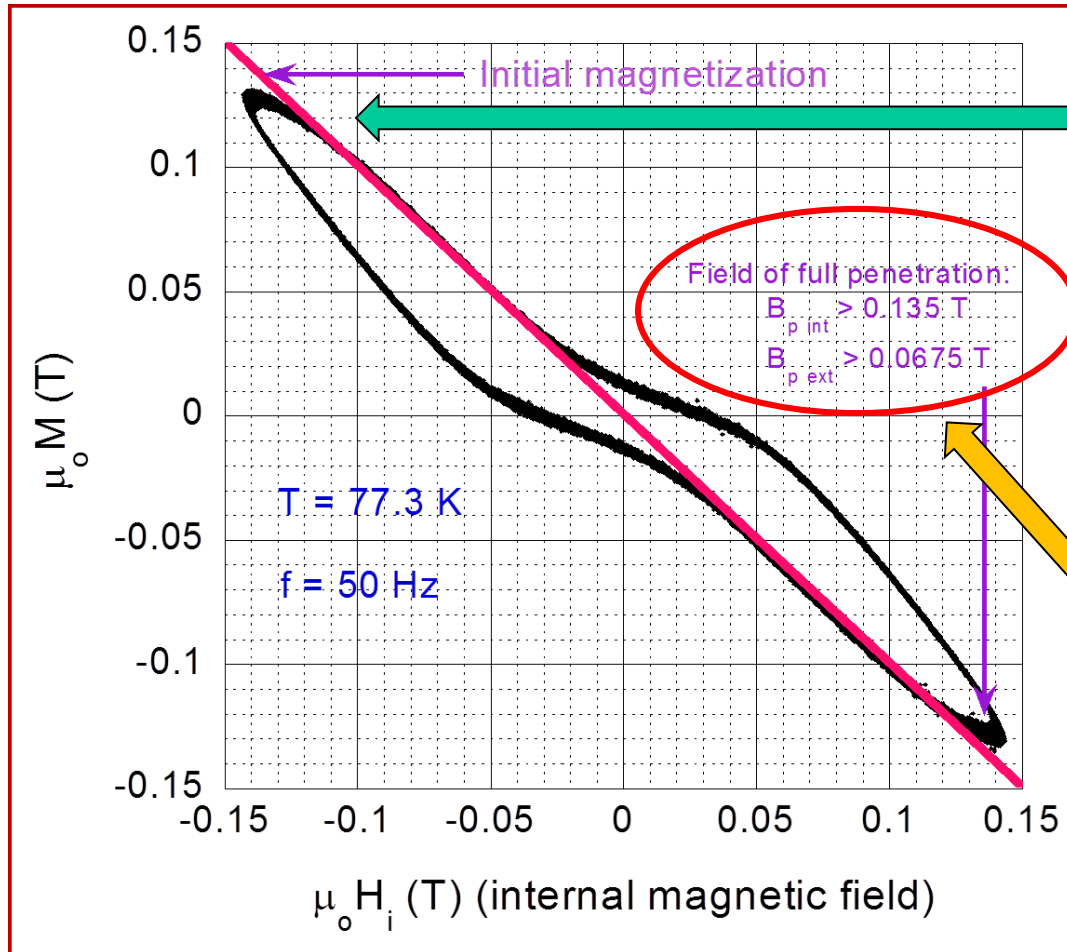


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# Magnetization Measurements on CORC at 77 K



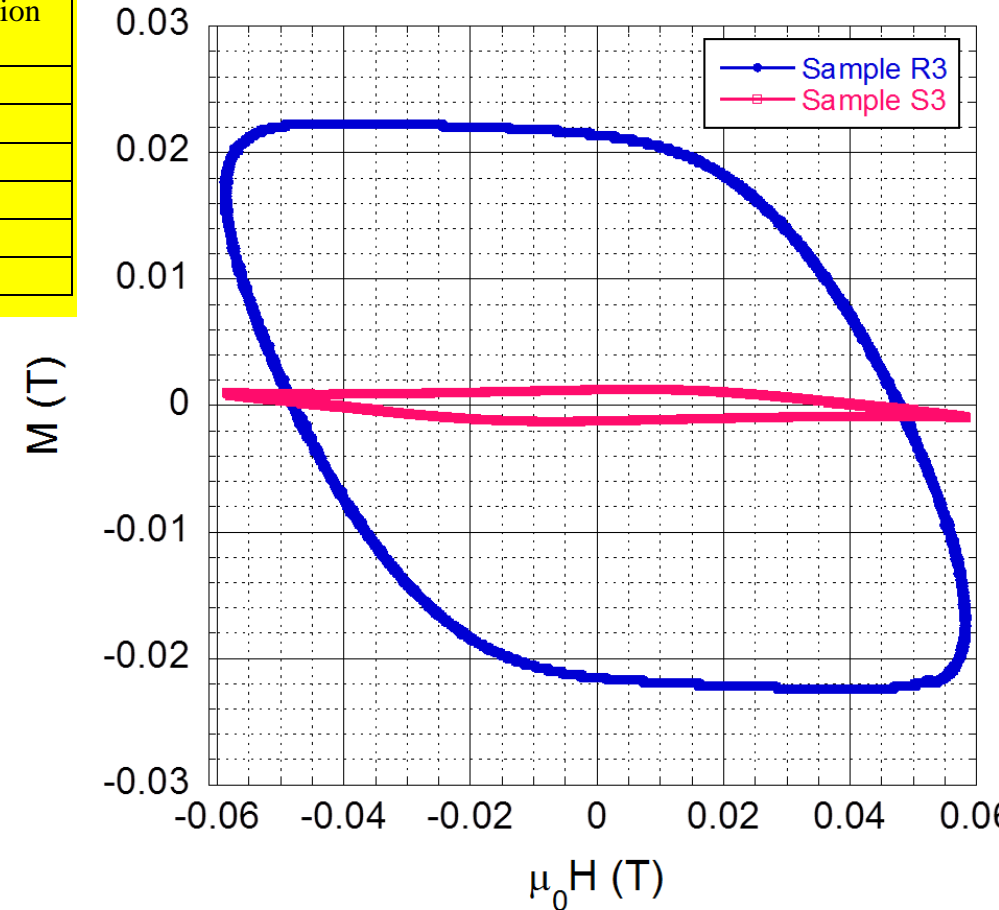
- Saturation magnetization reduced as compared to tape
- This is due to normalizing to volume of cable rather than tape (**factor of 3.3**), (**factor 3**) = 10
- But note the error field in dipoles is due to moment, not magnetization
- Apparent  $B_p$  the same as tape
- But local  $B_p$  doubled
- local fields complicated

# Striated measurement results of CORC at 77 K

Sample	# of tapes	$I_c$ (A)	ID (mm)	OD (mm)	Length (cm)	Striation
R1	2 x 3 = 6	607.9	4.96	6.17	11.7	None
S1	2 x 3 = 6	348.5	4.95	6.07	12.2	5
R2	3 x 3 = 9	904.2	4.93	6.37	11.7	none
S2	3 x 3 = 9	534.9	4.94	6.38	11.8	5
R3	4 x 3 = 12	1227.5	5.02	6.85	11.7	none
S3	4 x 3 = 12	749.4	4.97	6.78	11.9	5

Striations do significantly reduce loss

Some factor from striation, some from  $I_c$  loss



# New UoT Studies

Nijhuis and K. Yagotyntsev,  
The University of Twente

- While new OSU machine is being installed, made measurements at UoT
- Measured TWST, CORC, and Roebel cables at 4 K
- AC loss (10-60 mHz, 0.4 T), M-H (0-1.4 T, 10 mHz)
- Extracting: hysteretic, coupling, Magnetization at injection, and field penetration



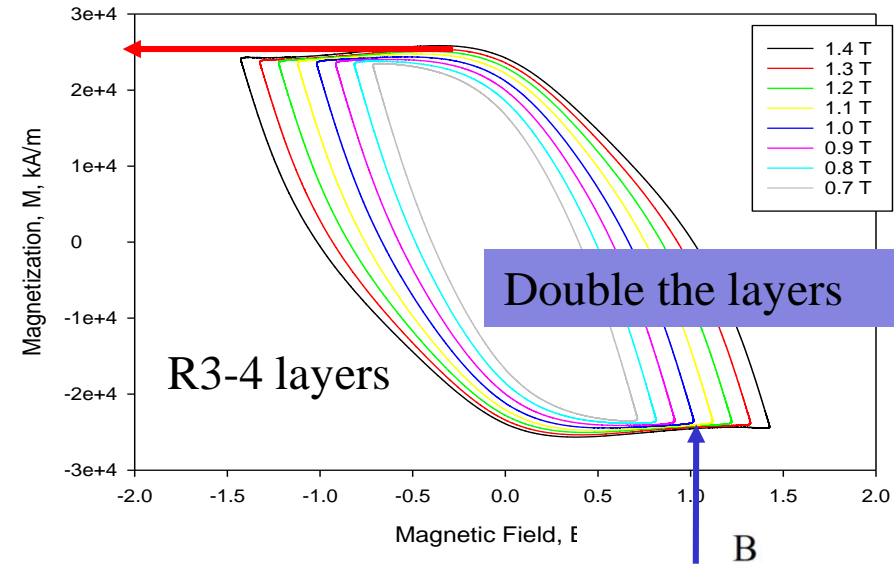
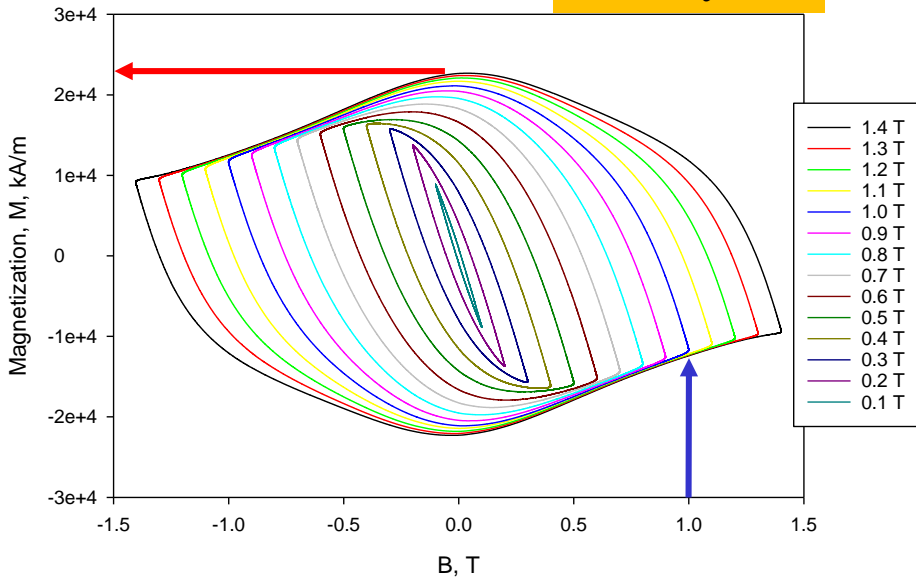
# CORC M-H Effect of layer number

Normalized to tape volume, 4 K result

Sample	Tapes	$I_c$ (A)	ID (mm)	OD (mm)	Length (cm)	Striations
R1	2 x 3 = 6	608	4.96	6.17	11.7	none
S1	2 x 3 = 6	349	4.95	6.07	12.2	5
R2	3 x 3 = 9	904	4.93	6.37	11.7	none
S2	3 x 3 = 9	535	4.94	6.38	11.8	5
R3	4 x 3 = 12	1228	5.02	6.85	11.7	none
S3	4 x 3 = 12	750	4.97	6.78	11.9	5

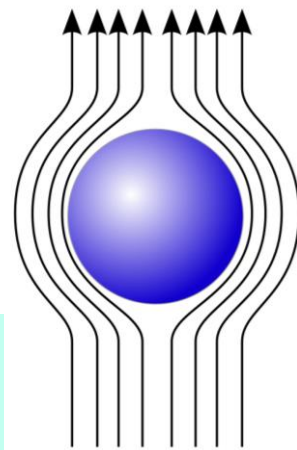
R1-2 layers

Few layers



	Film norm	Film norm	tape norm
	A/m	kA/m	kA/m
del M=	500000000	500000	10000

This is close to what we might expect for simple tape, but that is maybe fortuitous, as field lines are complicated



$M_{max} \approx 2M_{tape}$  when tape volume normalized, not influenced by layer #  
 $B_p$  similar to tape and not influenced by tape #



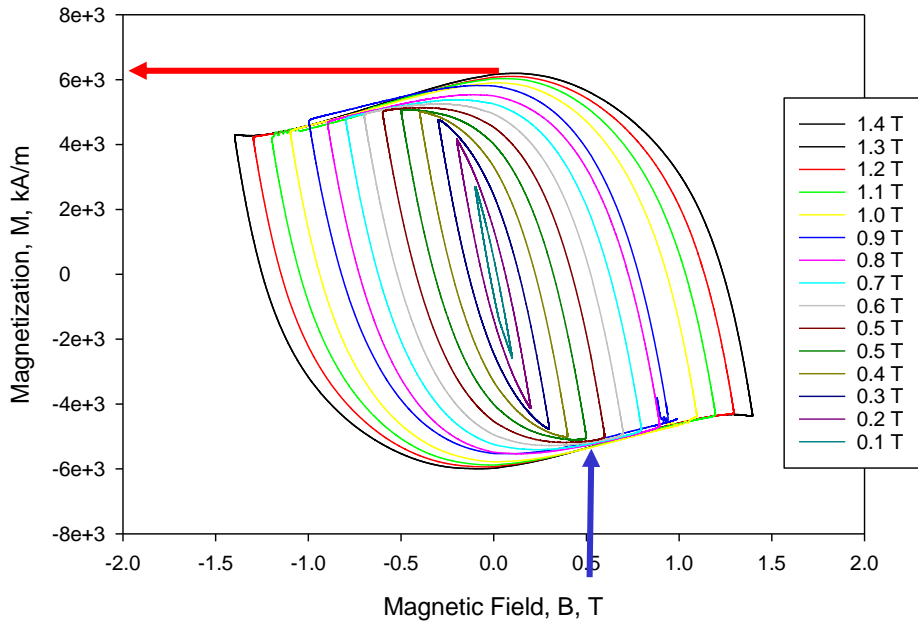
# CORC M-H Effect of striation

Normalized to tape volume, 4 K result

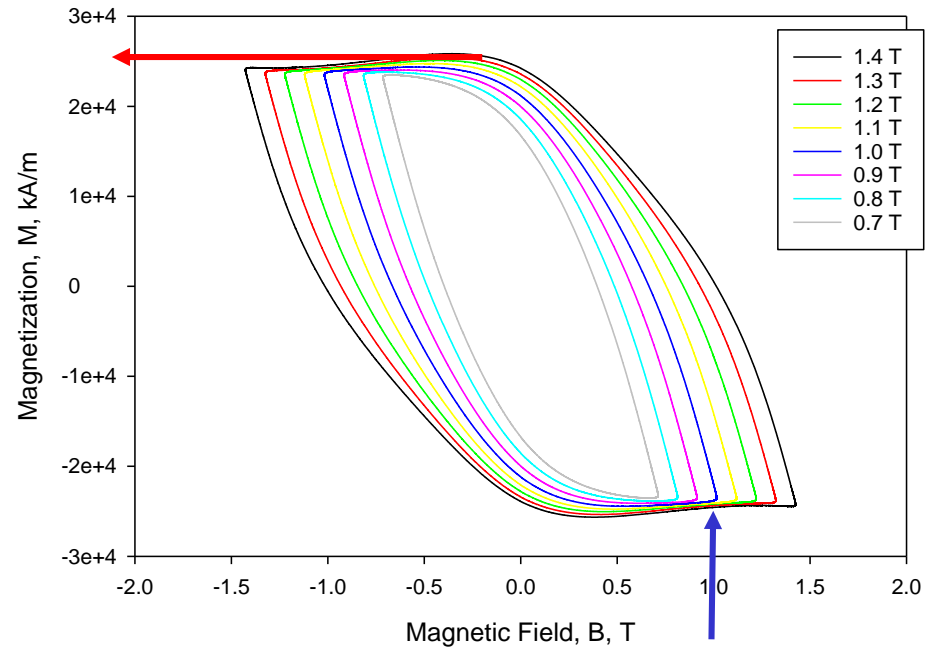
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S2	3 x 3 = 9	535	4.94	6.38	11.8	5
R3	4 x 3 = 12	1228	5.02	6.85	11.7	none
S3	4 x 3 = 12	750	4.97	6.78	11.9	5

S3-4 layer-striped

6 x 5 = 30



R3-4 layers



- Striping by 5 reduces  $M_{max}$  by 4
- $B_p$  appears to be reduced by 1/2

Let's further explore this:

Loss (Q) below  $B_p$  goes as  $B^3$ , above as  $B$

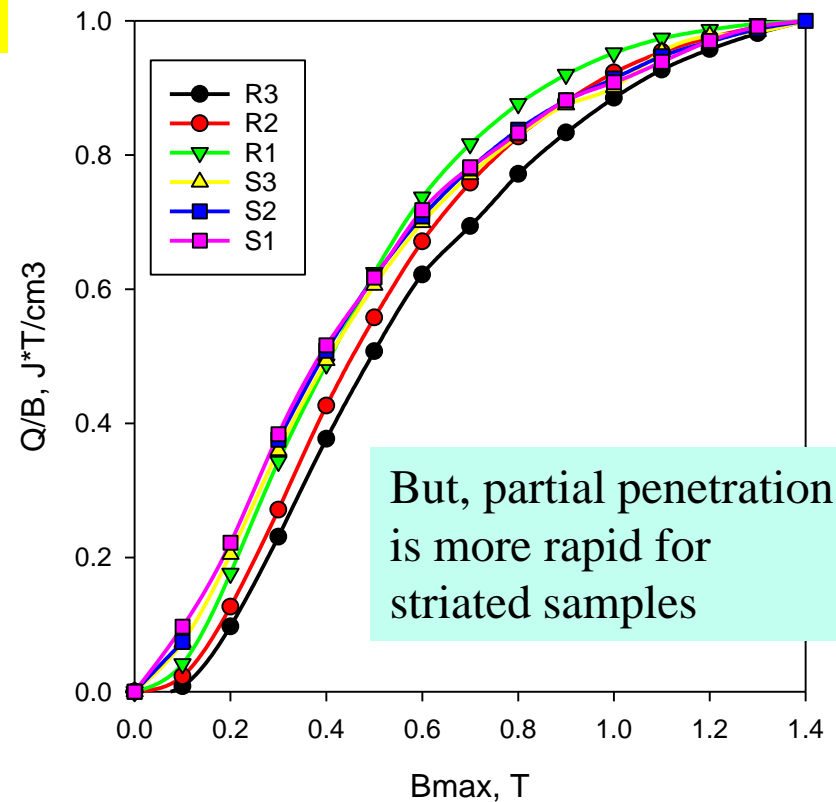
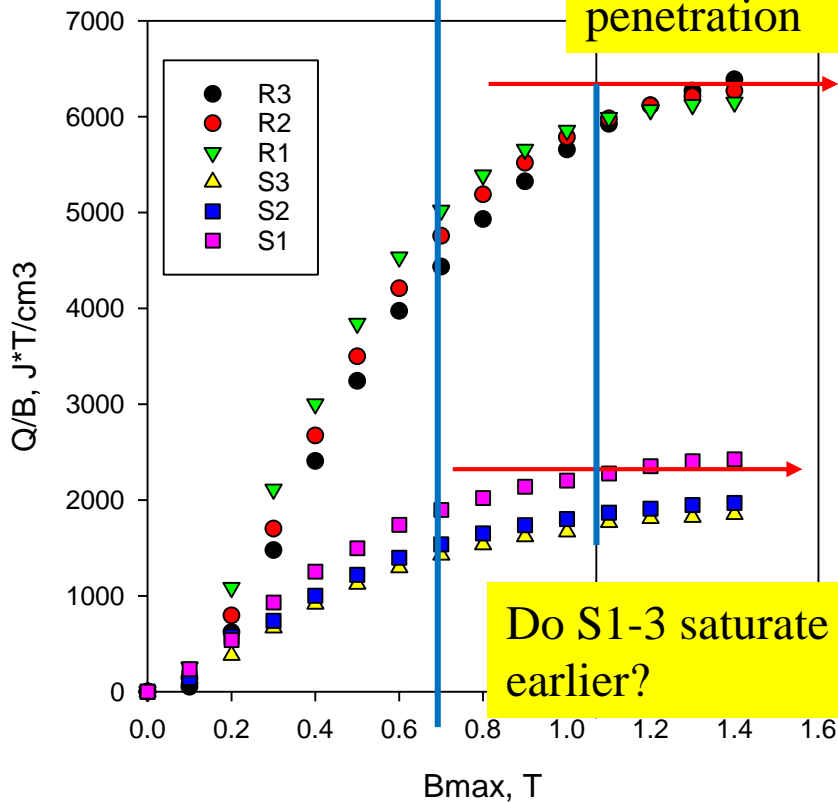
# Field Penetration into cables

## - CORC Cables

Saturation "effective width" different by x 3

Approaching full penetration

Full penetration happens at same place

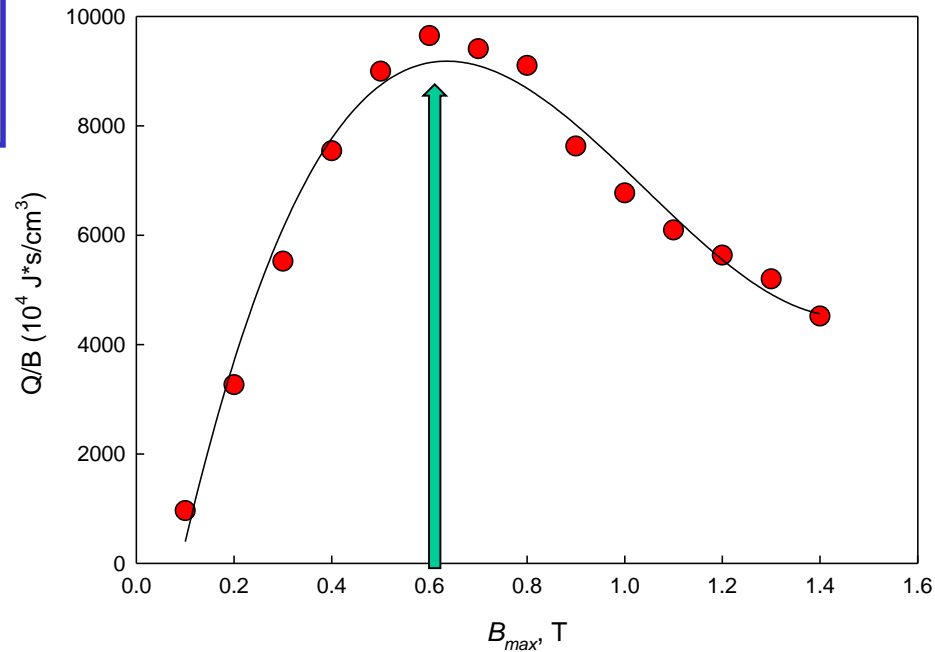
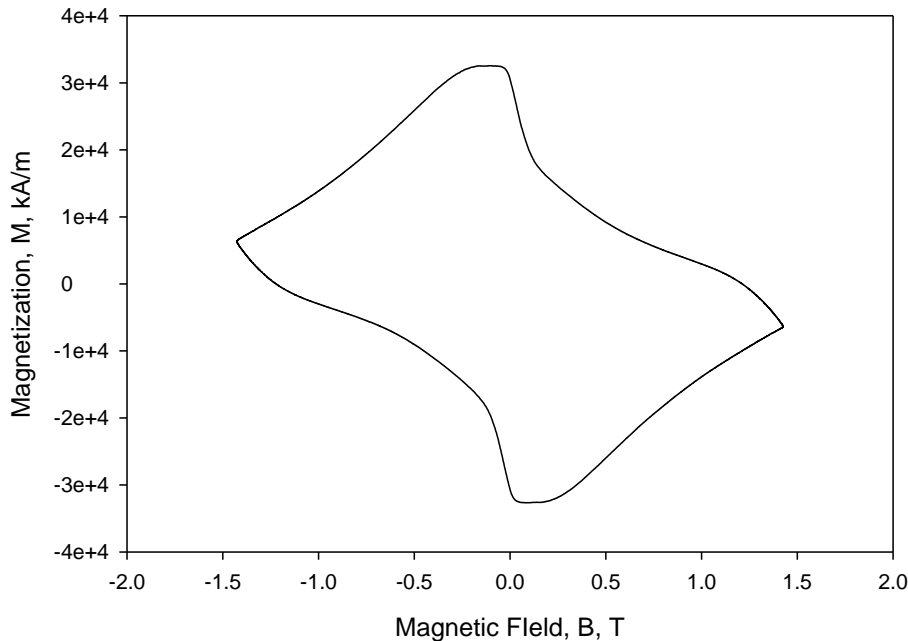


So, true  $B_p$  not really changed by striation, but apparent value is

# Roebel M-H

Normalized to tape volume, 4 K result

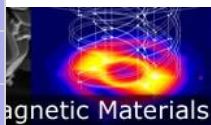
width = 13 mm  
 thickness = 0.5 mm  
 twist pitch = 12.5 cm  
 Made of 9 tapes, each 5 mm wide  
 Cable  $I_c(77.3K, \text{self field}) = 922.5 \text{ A}$



- Loss peaks at field penetration

M similar to other cables, shape mod

	Film norm	Film norm	tape norm
	A/m	kA/m	kA/m
del M=	500000000	500000	10000



Department of Materials Science and Engineering



# M-H, TSTC

4 mm wide SuNAM Tape 150  $\mu\text{m}$  SS

$I_c = 200$  A, 77 K, SF

Conductor Length = 200 mm, Twist Pitch = 200 mm

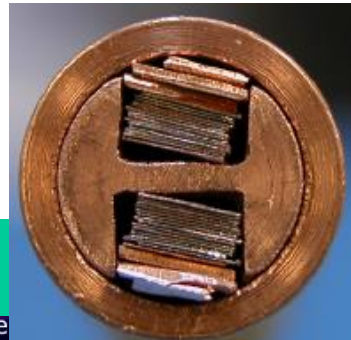
- TSTC-1: stacked tapes twisted between Cu strips, with retaining Cu and in plexiglass Tube



- TSTC-2: Tapes stacked Horizontally in a single helical groove in an OFHC Cu rod with sheath (05 " OD)
- TSTC-3: Tapes stacked vertically in a single helical groove in OFHC Cu with sheath
- TSTC-4: Tapes stacked in two vertical grooves in an OFHC Cu rod with a Cu sheath



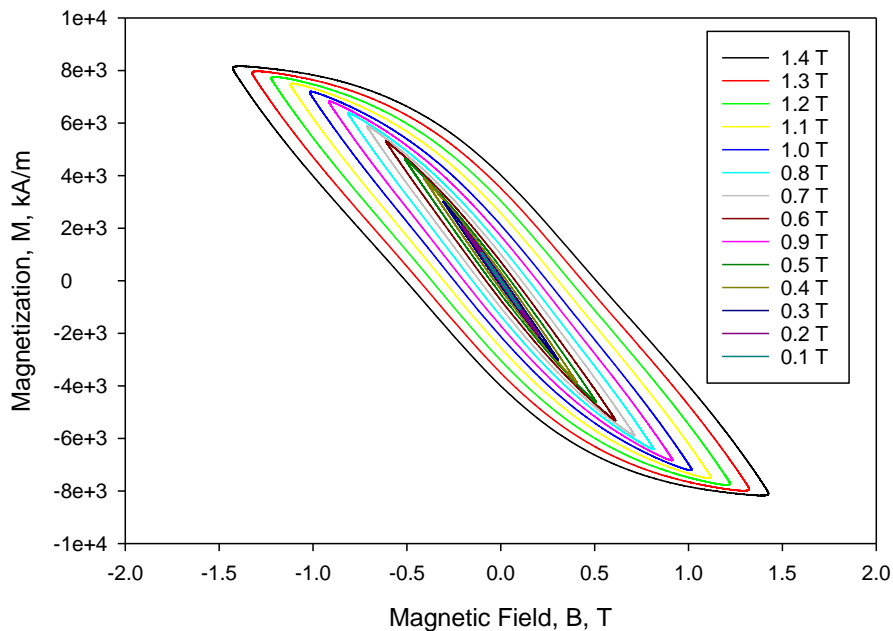
No soldering, packing only





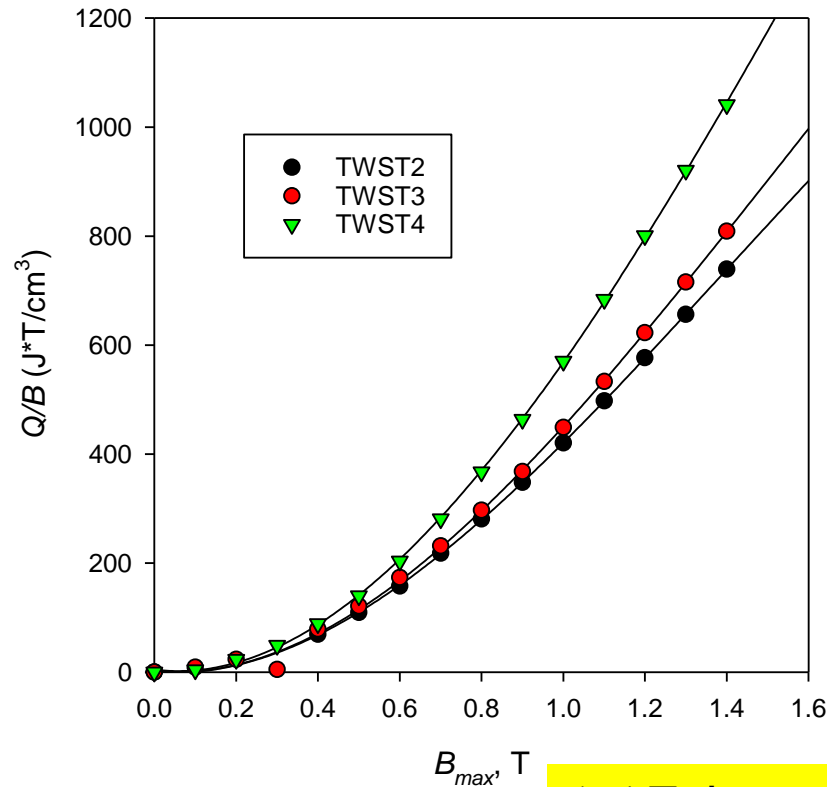
# TWST-4 M-H and $B_p$

Normalized to tape volume, 4 K result



$M_{max}$  should be  $\approx 3.14/2 = 1.2 \times 10^4$  kA/m

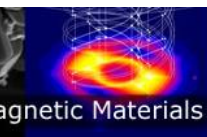
Above penetration,  $Q/B$  should be fixed, with y-intercept  $w \cdot l_c$



Below penetration,  $Q$  goes as  $B^3$ , above, as  $B$

1.4 T does not penetrate the sample

	Film norm	Film norm	tape norm
	A/m	kA/m	kA/m
del M=	500000000	500000	10000



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# Results

- $M \approx x 2M_{tape}$  for CORC
- $M$  similar to tape but shape mod Roebel
- $M \approx M_{tape}$  (maybe  $2/3.14 M_{tape}$ ) for TWST
- $M_{max} \approx 10000-20000$  kA/m for  $B_{\perp}$  tape, Roebel cable, and any orientation CORC and TWST
- $B_p$  similar to individual tape for CORC, Roebel, and TWST
- Striping tapes in CORC reduces  $M$  and  $B_{p-app}$

# Discussion

- CORC cables initial slope suggest flux exclusion from whole cable at low fields → an initial magnetization slope which is 3 x higher (this may be injection region)
- Striation of the CORC cables removes this effect, and flux exclusion volume drops below full cable volume between  $B_{p-app}$  and  $B_{p-true}$
- Flux exclusion for TWST and Roebel are like cable volume rather than tape, but here tape and cable volume similar

Cable	1 T Minj, kA/m
CORC	-12,000
CORC striated	-5000
Roebel	-20000
TWST	-8000

Strand type	NbTi <sup>(1)</sup>	Nb <sub>3</sub> Sn <sup>(2)</sup>	Bi:2212 <sup>(3)</sup>	YBCO	YBCO
Cable type	Rutherford	Rutherford	Rutherford	TSTC	CORC™
Cable packing factor, $\lambda_c$	0.88	0.855	0.87 <sup>(4)</sup>	0.56	0.58
Strand filling factor, $\lambda_s$	0.385	0.455	0.26	0.01 <sup>(5)</sup>	0.01 <sup>(5)</sup>
Layer CCD, $J_{c,inj}$ , kA/mm <sup>2</sup>	20.4	-	1.75	88 <sup>(6)</sup>	88 <sup>(6)</sup>
Eng. CCD <sup>(7)</sup> , $J_{e,inj}$ , kA/mm <sup>2</sup>	7.85	-	0.455	0.88	0.88
Fil. (strand) size, $d_{eff}$ , $\mu$ m	7	61	278	4000 <sup>(8)</sup>	4000 <sup>(10)</sup>
$J_{cable,inj}$ kA/mm <sup>2</sup>	6.91	13.0	0.396	0.493	0.510
$J_{cable,coll}$ kA/mm <sup>2</sup>	0.704	0.855	0.348	0.244	0.232
$B_{b,coll}$ , T	8	15	20	20	20
$b_3$ , units <sup>(11)</sup>	3	41	19	330 <sup>(12)</sup>	330 <sup>(12)</sup>
$b_{3*}$ , units <sup>(13)</sup>			37	99	99

77 K Ic	4 K Ic	Jc (A/m <sup>2</sup> )	M
200	2000	2.5 x 10 <sup>11</sup>	10000
80	800	10 <sup>11</sup>	4000
70	700	0.88 x 10 <sup>11</sup>	3250

- So, for the tape, while the  $M$  goes up, it goes up as  $I_c$ , so less cables, and field errors are same
- But, cable vs tape differences matter – all within factor of two

# Next Steps

- Further Measurements of the most recent cables, expanded up to  $\pm 3$  T at 4 K
- LBNL-OSU collaboration (X. Wang) with YBCO data detailed field error estimations canted cos and other magnets
- Explore  $M$  modification with current injection
- Consider more closely effects of creep on error fields
- Loss is of interest?

# Magnetization - but loss?

- For the LHC NbTi dipoles ramping at about 7 mT/s AC loss is only a small contributor to cryogenic load
- Could be larger for YBCO cables.
- For a YBCO cable carrying a current of 10 kA at 20 T the loss at 7 mT/s is estimated to be 200 mW/m
- For an HTS insert of, say, 70 turns the winding dissipation would be 14 W/m -- more than double the LHC ring's 4.5 K/1.8 K refrigeration capacity
- This is a handle-able problem, but not of no interest

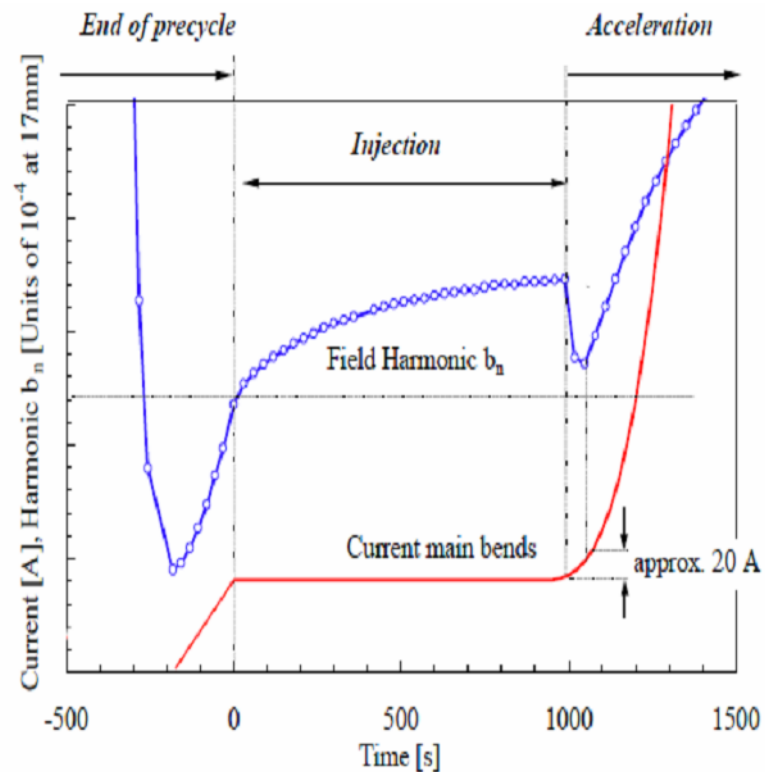
10 kA cable		Measured CORC cable	
T/s	t, sec	Q/m	mW/m
0.007	2285.7143	9142.857	0.000109
Q, J/m <sup>3</sup>	A m <sup>2</sup>	Q/m	mW/m
10000000	0.0000785	785	0.085859

So, 1/3 of simple estimate, but still substantial



# Drift in accelerator Magnets

- Just as important as the absolute value of  $b_3$  is any *change with time* during the injection porch
- It is possible to compensate for error fields with corrector coils, but the presence of *drift* makes this much more difficult
- At right is shown the drift of the error fields as a function of time from zero to 1000 seconds for LHC magnets, followed by a snap-back once the energy ramp begins



Keep both  $b_3$  and its drift below 1 unit for Nb<sub>3</sub>Sn based magnets. This is possible

Sample	$B$ , T	orientation	$-M_0$ , kA/m	$-M_{20min}$ , kA/m	$M_{20min}/M_0$	$\Delta M$ , kA/m	% $b_3$
Bi:2212	1 T	$\perp$	15	12	0.80	3.0	20
	12 T	$\perp$	2.7	1.5	0.58	1.1	42
YBCO							
	1 T	$\perp$	991	906	0.91	90	10
	1 T	45°	933	811	0.86	120	14
	12 T	$\perp$	280	187	0.67	93	33
	12 T	45°	229	200	0.87	29	13



# Loss Appendix



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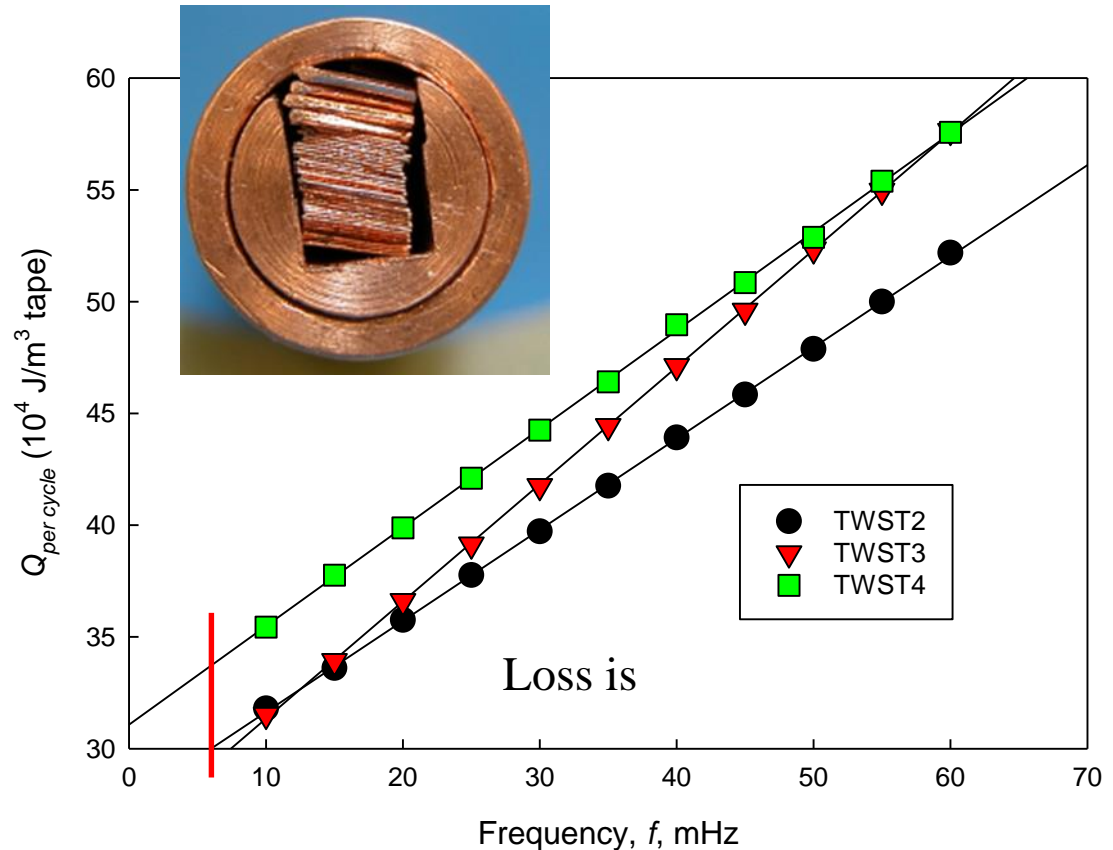


# TSTC-Hysteretic and Coupling Loss

- 30 tapes, 200 A/77 K SF -> 6 kA at 4 K, 20 T
- At accelerator-relevant frequencies, non-negligible coupling loss.
- Ballpark of coupling currents for Nb<sub>3</sub>Sn magnets (3 x)
- Hyst loss about 3 x, but not fully penetrated
- (not current normalized)

	Hyst	Slope	rho
	10 <sup>4</sup> J/cm <sup>2</sup>	J*s/cm <sup>3</sup>	n-ohm-cm
cable			
TWST2	27.6	408	95
TWST3	26.1	524	74
TWST4	31.1	441	87

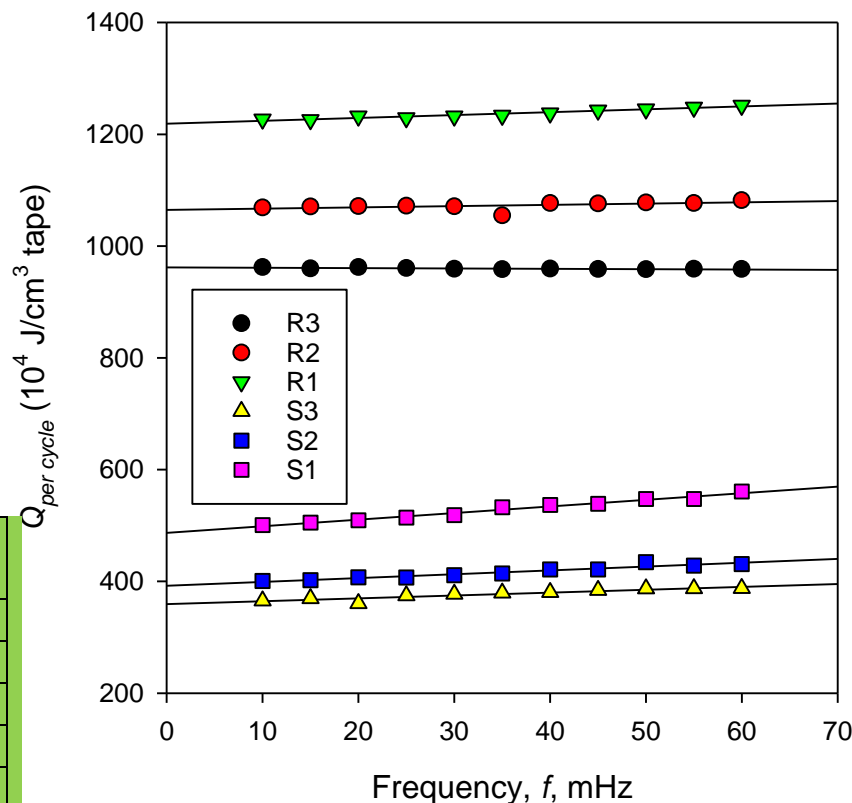
Resistivity about 1 order above Cu at Lhe temp



Pressure of abrasion related to the twist of the tapes making for low contact resistance

# CORC Hysteretic and Coupling Loss

- Early Experimental cables for striped/not striped
- More flux penetration here
- Coupling loss values show high interstrand resistance - not infinite, but in milli-100s milliohms
- **Note 1:** Loss per tape volume greater for fewer layers- relevant for injection
- **Note 2:** Striped Tape CORC loss suppressed by about x 3 (not quite 5)



Sample	Tapes	$I_c$ (A)	ID (mm)	OD (mm)	Length (cm)	Striations
R1	2 x 3 = 6	608	4.96	6.17	11.7	none
S1	2 x 3 = 6	349	4.95	6.07	12.2	5
R2	3 x 3 = 9	904	4.93	6.37	11.7	none
S2	3 x 3 = 9	535	4.94	6.38	11.8	5
R3	4 x 3 = 12	1228	5.02	6.85	11.7	none
S3	4 x 3 = 12	750	4.97	6.78	11.9	5

# Roebel Hysteretic and Coupling Loss

- More flux penetration here given geomtry
- Coupling loss values show high interstrand resistance - not infinite, but in milli-100s milliohms

width = 13 mm  
thickness = 0.5 mm  
twist pitch = 12.5 cm  
Made of 9 tapes, each 5 mm wide  
Cable  $I_c(77.3K, \text{ self field}) = 922.5 \text{ A}$

