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# The Effect of pH and Pulsed Ultraviolet Light Emitting Diode Duty Cycles on the First Order Rate Constant and Byproduct Profile of the Advanced Oxidation of Tartrazine

Brandon M. Stewart

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**THE EFFECT OF pH AND PULSED ULTRAVIOLET LIGHT EMITTING  
DIODE DUTY CYCLES ON THE FIRST ORDER RATE CONSTANT AND  
BYPRODUCT PROFILE OF THE ADVANCED OXIDATION OF TARTRAZINE**

THESIS

Brandon M. Stewart, 1st Lt, USAF

AFIT ENV-MS-16-M-186

**DEPARTMENT OF THE AIR FORCE  
AIR UNIVERSITY**

***AIR FORCE INSTITUTE OF TECHNOLOGY***

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**Wright-Patterson Air Force Base, Ohio**

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THESIS

Presented to the Faculty

Department of Systems Engineering and Management

Graduate School of Engineering and Management

Air Force Institute of Technology

Air University

Air Education and Training Command

In Partial Fulfillment of the Requirements for the  
Degree of Master of Science in General Engineering Management

Brandon M. Stewart, BS

1st Lt, USAF

March 2016

**DISTRIBUTION STATEMENT A.**  
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Member

### **Abstract**

Water treatment capability is required for military operations, production of drinking water, and industrial wastewater treatment. The Advanced Oxidation Process (AOP) is one of many viable steps for treating water; however, it is important to understand the byproducts of the treatment process to avoid creating other constituents more severe than the first. Tartrazine (TAR) was oxidized with pulsed Ultra-Violet (UV) Light Emitting Diodes (LEDs) in combination with hydrogen peroxide (H<sub>2</sub>O<sub>2</sub>) in an AOP at the laboratory scale.

The relative concentration of TAR was reduced from 1 to between 1 – 0.75 over pH values between 6 and 9, and at Duty Cycles (DCs) ranging from 0% to 100%. The first order rate constant for TAR removal was statistically and positively correlated with DC, was statistically and negatively correlated with pH, and was typically greatest at pH 6. DC and pH were variables in a regression model of the first order rate constant with adjusted R<sup>2</sup> of 0.85.

Chromatographic contrast angle determinations revealed that the byproduct profile was most significantly influenced by pH 7 under both positive and negative ionization, by the 70% DC for the positive ionization, and 50% DC for the negative ionization. DC and pH were variables in regression models to predict positive and negative Chromatographic Contrast Angle (CCA) with adjusted R<sup>2</sup> of 0.76, and 0.68, respectively.

Chemical byproduct analysis indicated that OH addition, H abstraction, and electron transfer without molecule transfer were among the plausible reaction

mechanisms for TAR degradation. Of six metabolites identified, two potentially novel metabolites demonstrated that TAR was likely cleaved. These metabolites were (1-(2-hydroxy-4-sulfonatophenyl)-5-oxo-4,5-dihydro-1H-pyrazol-4-yl)diazene-1-ide and (E)-4-(hydroxydiazene)-5-oxo-1-(4-sulfonatophenyl)-4,5-dihydro-1H-pyrazole-3-carboxylate. Two other potentially novel metabolites were identified: (E)-4-((2-hydroxy-4-sulfonatophenyl)diazene)-5-oxo-1-(4-sulfonatophenyl)-4,5-dihydro-1H-pyrazole-3-carboxylate, and (E)-4-((1-(4-sulfonatophenyl)-4,5-dihydro-1H-pyrazol-4-yl)diazene)benzenesulfonate. There were several potential isomers for each metabolite identified.

This research is the first to determine the optimal pH for UV LED-driven oxidation of TAR, the first to use CCA to evaluate byproduct profiles, and the first to identify novel TAR-related byproducts from UV LED-based AOP. This study is the first to develop regression models for the prediction of TAR removal and the byproduct profile given pH and DC; given the assumption that all other operating conditions are analogous to those of this study.

*To my Wife, Son, and Daughter. To paraphrase Voyager: My attachment to my family is not something that can be described as a mere emotion. My family is part of my identity. Without them, I would be incomplete.*



## **Acknowledgments**

First, I would like to thank Dr. Willie Harper, Jr., my thesis advisor, for his guidance and support in the completion of my thesis research. Second, I would like to thank committee members Dr. Michael Miller and Lt Col David Kempisty for their technical expertise. I would also like to thank Dr. Daniel Felker and Dr. Edward White, for their instruction and assistance with challenging research questions and analysis. Lastly, I would like to thank Dr. Catherine Almquist of Miami (OH) University, Mr. Nathaniel Godby, Ms. Sarah Fyda, Ms. Lana Amer, Ms. Kandace Bailey, Capt Kelsey Duckworth, Maj. Michael Spencer, Maj. Robert Scott, Capt. Patrick Mudimbi, and Capt. Drew Gallucci, whose previous work, concurrent work, and invaluable training have directly contributed to the successful completion of my study.

Brandon M. Stewart

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## **Glossary of Acronyms and Abbreviations**

AFIT – Air Force Institute of Technology

ANOVA – Analysis of the Variance

AOP – Advanced Oxidation Process

BEAR – Base Expeditionary Airfield Resources

BOD – Biological Oxygen Demand

CBRN – Chemical, Biological, Radiological, Nuclear

CCA – Chromatographic Contrast Angle

CSTR – Continuous Stirred-Tank Reactor

DC – Duty Cycle

DOC – Dissolved Organic Carbon

DOD – Department of Defense

DV – Dummy Variable

EPA – Environmental Protection Agency

HPLC – High Performance Liquid Chromatography

IUPAC – International Union of Pure and Applied Chemistry

LED – Light Emitting Diode

LS Means – Least Squares Means

MS – Mass Spectroscopy

NOM – Natural Organic Matter

PFR – Plug Flow Reactor

ROWPU – Reverse Osmosis Water Purification Unit

SSE – Sum Squares Error

SSR – Sum Squares Regression

TS – Test Statistic

US – United States

USAF – United States Air Force

UV – Ultraviolet

VIF – Variance Inflation Factor

VUV – Vacuum Ultraviolet

WPAFB – Wright Patterson Air Force Base

$\text{COO}^-$  – Carboxylic Acid Group (Deprotonated)

CN – Cyanide

$\text{HO}\cdot$  – Hydroxyl Radical

NaOH – Sodium Hydroxide

Sulf – Sulfonic Acid Group

$2\dot{\text{O}}_2^-$  – Super Anoxide Radical

Tar – Tartrazine

TCS – Triclosan

UV-Vis – Ultraviolet, Visible Spectrum

-

# **PULSED ULTRAVIOLET LIGHT EMITTING DIODES FOR ADVANCED OXIDATION OF TARTRAZINE**

## **I: Introduction**

### **1.1 Chapter Overview**

This chapter discusses the problem, background, research, and investigative questions for the application of Ultraviolet (UV) Light Emitting Diodes (LEDs) in water treatment processes. Additionally, it articulates the scope, assumptions, and limitations of the research. This section also provides a description of the methodology used to conduct the experiments, and highlights the remaining sections of this thesis.

### **1.2 General Issue**

The purpose of this thesis is to increase knowledge of the utilization of UV LEDs for use in water treatment through an Advanced Oxidation Process (AOP). Specifically, this research effort attempts to identify optimal operating parameters such as pH and DC for the AOP of Tartrazine (TAR), to categorize reaction mechanisms, and to suggest possible byproduct structures.

Understanding options to treat water is of particular importance in the military environment (*Quadrennial Defense Review*, 2014). The Air Force needs water treatment capabilities to answer the threat of chemical weapons attack, accidental industrial chemical release, or other military operations resulting in environmental contamination (Duckworth et al., 2014; Mudimbi, 2015; Scott, 2015; Spencer, 2014). There are several types of AOP reactions; this thesis will focus on UV-hydrogen peroxide (UV/H<sub>2</sub>O<sub>2</sub>) process. When UV light comes in contact with H<sub>2</sub>O<sub>2</sub>, it produces two hydroxyl radicals

(HO·) (Andreozzi, et al., 1999; Legrini, et al., 1993; Tayade, et al., 2009; S. H. Vilhunen & Sillanpää, 2009). These hydroxyl radicals are more powerful oxidants than chlorine or ozone and react quickly and efficiently with contaminants (Munter, 2001). There is discussion of how pH affects the AOP (Andreozzi et al., 1999; Vescovi, Coleman, & Amal, 2010) and the extent of these effects is not fully understood. Additionally, operating conditions for AOP vary substantially based on the constituent in question. Andreozzi (1999) demonstrated that the H<sub>2</sub>O<sub>2</sub> photolysis of benzene, toluene, and other organic compounds was pH dependent and that degradation increased with higher pH. Imoberdorf (2011) did not observe significant effects in degradation of natural organic matter when adjusting pH between 5 and 9. Conversely, another study found UV radiation alone degrades TAR relatively quickly at a pH of 6 (dos Santos, et al., 2014). The AOP reaction often does not completely mineralize compounds (i.e. the end products are not solely CO<sub>2</sub> and H<sub>2</sub>O). It is important to fully identify the byproducts of the reaction in the context of water treatment because the byproducts (also called intermediate oxidation products) may be more harmful or toxic than the original compound (Munter, 2001).

Using LEDs for conducting AOP reactions comes with multiple benefits. LEDs are superior to traditional mercury lamps in several respects. LEDs require very little energy, are cost-comparative, produce significantly less heat, efficiently produce light, are more compact, more robust, require no warm up time (instant on/off), run on direct current, which allows for operation with batteries or solar panels, are not manufactured with mercury, which carries many negative health implications, and have longer lifetimes (Autin et al., 2013; *Crystal IS*, 2013). While LEDs are a rapidly improving technology,

their potential is not fully realized. Downsides to LEDs include: extreme sensitivity to negative current or electrical shorts, potential corrosion of the metal casings, and emitting a single wavelength; as opposed to mercury lamps, which are polychromatic.

### **1.3 Problem Statement**

The EPA and the Air Force Institute of Technology (AFIT) are investigating the use of LEDs due to the interest in treatment methods and improving the health of deployed service members. UV LEDs are still in the developmental stage; however, the method has proven to be a viable and efficient means for driving the AOP (Duckworth et al., 2014; Mudimbi, 2015; Scott, 2015; Spencer, 2014). Notwithstanding, thorough research and investigative questions are required to advance the understanding of treatment methods, system components, and operating conditions.

### **1.4 Research Objectives/Questions/Hypotheses**

This research effort addresses two main questions: 1.) What operating conditions promote the most effective use of UV LEDs for degradation of TAR? 2.) What reactions occur and how are they characterized? In order to conduct this study, the following investigative questions and respective hypotheses were formulated:

1. How does pH affect the reaction? Considering the conclusions of (Farhataziz, AB, Ross, & Ross, 1977; Imoberdorf & Mohseni, 2011; Legrini et al., 1993), there is no consensus on the effect pH has on the AOP reactions, particularly of the UV/H<sub>2</sub>O<sub>2</sub> AOP. To adequately answer this question, the removal of TAR must be

quantified at a variety of pH levels and DCs. The hypothesis for this research question is that pH plays a significant role in the degradation of TAR.

2. What byproducts are generated in the AOP of TAR? Is the byproduct profile influenced by pH? The hypothesis for this research question is that pH does affect the byproduct profile.
3. Which reaction mechanisms play a role in the AOP of TAR? According to Benjamin (2013), Hydroxyl radicals can decompose a compound in three different ways: Hydrogen Abstraction, Electron Abstraction, or OH addition. Based on the composition of TAR, the most likely method is electron transfer or OH addition. Given this hypothesis, the byproducts of the reaction must be identified.

## **1.5 Methodology**

To answer the investigative questions, experiments were conducted – hereafter referred to as the AOP Experiments. The AOP Experiment involved manipulating both pH and DCs. DC indicates the amount of time the LEDs are on. For example, the 100% DC refers to the LEDs remaining on continuously. The 30% DC means the lights are on for 30% of the time and off for 70% of the time. This experiment was conducted at AFIT.

Two kinds of control experiments exist for the AOP Experiment. The first control did not incorporate  $H_2O_2$  in the solution mixture; thus preventing the AOP, resulting in negligible TAR reduction unless there is some effect due to pH adjustor, UV radiation, or some interaction of the two. The second control experiment operated at the 0% DC to see if pH adjustor and  $H_2O_2$  interact without UV radiation. The baseline for this experiment



is 100% DC at pH 7. The solution flows from the source solution beaker into the reactor, and then into the Ultraviolet-Visible Spectrum (UV-Vis) spectrophotometer. The spectrophotometer measures absorbance, which is used to calculate concentration and the first order rate constant of the AOP.

The effluent from each experiment was collected, filtered, and processed by High Performance Liquid Chromatography (HPLC). Both positive and negative ionization readings were collected, resulting in chromatograms and mass spectroscopy (MS) plots for each experiment. Chromatographic Contrast Angles (CCAs) were calculated from the chromatograms and were used to analyze the effect of pH on the byproduct profile. The chromatograms and the MS plots were used in chemical analysis to identify potential byproduct structures and reaction mechanisms associated with those structures.

The statistical methods used in this study included one-way Analysis of Variance (ANOVA), Tukey Analysis, and Linear Regression Analysis. The software used to conduct this analysis was JMP Pro® versions 11 and 12.

## **1.6 Assumptions/Limitations**

The limitations of this research are as follows:

1. The LEDs used are small and operate at low power. The assumption is that as technology improves, and as the number of manufacturing vendors increases, LEDs will become more versatile, more powerful, and less expensive.

2. The LEDs for this research were supplied by a single manufacturer (Sensor Electronic Technology, Inc.), due to the limited number of UV LED vendors. In addition to LED limitations, only non-toxic chemicals are allowed in the laboratory due to safety

and disposal requirements. Because of this limitation, TAR was selected as a “witness dye.”

3. This research is a laboratory study; the kinetic and hydraulic characteristics observed during this research may or may not be observed at a larger scale.

## **II. Literature Review**

### **2.1 Chapter Overview**

This section elucidates the relevant literature and background to UV LED applications in AOP processes. Specifically, it develops the key issues of operating conditions and byproducts generated when UV LEDs are used in the UV/H<sub>2</sub>O<sub>2</sub> AOP. These areas include UV light and usage, Advanced Oxidation Processes, and AOP byproduct analysis; to include Chromatographic Contrast Angle (CCA) analysis and Mass Spectroscopy analysis.

### **2.2 Background**

Whether accidental or malicious, water contamination is a threat to public safety and health. The United States Military must safeguard clean water against Chemical, Biological, Radiological, or Nuclear (CBRN) contamination, because water is a fundamental, precious resource (*Quadrennial Defense Review*, 2014). Industrial accidents, in which chemicals are released, create adverse human and environmental health effects, requiring expensive medical treatment and remediation (Barrett, 2014; Fitzsimmons, 2014). The EPA sponsors this research in an effort to find safe and viable methods to decontaminate water.

### **2.3 UV Light and LED Usage**

The UV spectrum spans between 100 and 400 nm. This is further categorized into Vacuum (100-200 nm), C (200-280 nm), B (280-315 nm), and A (315-400 nm) (*Crystal IS*, 2013). It is well established that UV light can degrade molecular structures, as well as

inactivate microorganisms by damaging RNA and or DNA (Andreozzi et al., 1999; Cassan, Mercier, Castex, & Rambaud, 2006; dos Santos et al., 2014; Munter, 2001). UV light is traditionally produced with low-pressure mercury lamps (Bettles, Schujman, Smart, Liu, & Schowalter, 2007; Würtele, Kolbe, Lipsz, & Külberg, 2011), but these lamps have several drawbacks, particularly with respect to AOP, to include: high energy consumption, high heat emission, short lifespan, instability, and disposal issues with respect to mercury as an environmental contaminant (Autin et al., 2013).

LEDs have many properties and characteristics that make them superior to mercury lamps (Autin et al., 2013; *Crystal IS*, 2013, US EPA, 2000; Vilhunen & Sillanpää, 2009). These properties include: LEDs do not contain mercury, and therefore do not pose the associated health risks (OSHA, 2012; US EPA, 2000, US EPA, 2013); LEDs are expected to become more effective and less expensive with time according to Haitz's Law (Autin et al., 2013; Lenk & Lenk, 2011); LEDs require no warm up time, which saves energy and increases the bulb lifecycle by incorporating pulsing DCs (Autin et al., 2013; Tran, et al., 2014); LEDs generate significantly less heat and are more robust than traditional lamps (Bettles et al., 2007).

## **2.4 Advanced Oxidation of Tartrazine**

### ***2.4.1 Advanced Oxidation Processes (AOP)***

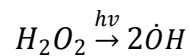
The AOP creates hydroxyl radicals ( $\text{HO}\cdot$ ), which hold a single, unpaired electron in an orbital (Benjamin & Lawler, 2013), and which quickly oxidize compounds (Andreozzi et al., 1999), to include disinfection byproducts (DBP) (Chin & Bérubé, 2005; Toor & Mohseni, 2007).  $\text{HO}\cdot$  radicals are short lived but are very powerful oxidizing

agents – twice as potent as chlorine and 1.3 times more so than ozone (Legrini et al., 1993; Munter, 2001).

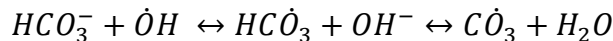
There are two general categories of AOP: photochemical and non-photochemical, which refers to whether or not a UV light source is required for the reaction. Within the non-photochemical category, there are four AOP varieties: combining Ozone with 1.) high pH; 2.) H<sub>2</sub>O<sub>2</sub>; 3.) some other catalyst (Cortes, et al., 1998; Munter, 2001; Paillard, et al., 1988); and 4.) Fenton’s reaction using H<sub>2</sub>O<sub>2</sub> and Fe<sup>+2</sup> (Fenton, 1884).

The photochemical category includes combining UV radiation with: 1) H<sub>2</sub>O<sub>2</sub>, see Equation 1; 2) Ozone and H<sub>2</sub>O<sub>2</sub>; 3) TiO<sub>2</sub>; and other titanium or molybdenum composite materials (Andreozzi et al., 1999; Liu et al., 2015; Munter, 2001; Schröder & Meesters, 2005; Varshney & Kanel, 2016). This research focuses on the UV/H<sub>2</sub>O<sub>2</sub> AOP as a continuation of that conducted by Duckworth (2014), Spencer (2014), Scott (2015), and Mudimbi (2015) using H<sub>2</sub>O<sub>2</sub> to degrade a “witness dye”. There are a few noteworthy formulas due to their potential role in the AOP reaction:

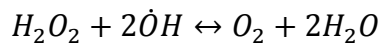
**Equation 1: Photochemical AOP UV/H<sub>2</sub>O<sub>2</sub>**



**Equation 2: Atmospheric Acidification/Hydroxyl Radical Sink**



**Equation 3: Peroxide/Hydroxyl Radical Sink**



These formulas are significant because they indicate potential sinks for radicals, just through interaction of hydroxyl radicals and peroxide, as well as the acidification of water due to exposure to atmospheric CO<sub>2</sub>. Equation 2 plays a large role in this study

because  $\text{H}_2\text{CO}_3$   $\text{pK}_{\text{a}1}$  and  $\text{pK}_{\text{a}2}$  are 6.35 and 10.33 (Benjamin, 2014), respectively – the pH of the solutions in this experiment was between 6 and 10, making  $\text{HCO}_3^-$  the most prevalent form of carbonic acid in the solution (at pH less than 6.35 it is not the most prevalent form, but is close to the same concentration as  $\text{H}_2\text{CO}_3$ ); log concentration of  $\text{HCO}_3^-$  was calculated with VMINTEQ and increases linearly from approximately -5 to -1 between pH = 6.35 and 10.33 (Gustafsson, 2012).  $\text{HO}_2^-$  forms in acid/base equilibrium with  $\text{H}_2\text{O}_2$ , see Equation 3. However, this attribute has much less influence because the  $\text{pK}_{\text{a}}$  for that reaction is 11.6 (Buxton, Greenstock, Helman, & Ross, 1988; Legrini et al., 1993) and the pH was less for all experiments of this study.

The “witness dye,” as coined by Scott (2015), is used in place of toxic contaminants due to the limitations of lab safety requirements and the ease of disposal of the witness dye. Degradation of the witness dye is characterized by absorbance, which is measured by a UV-Vis Spectrophotometer. The decrease in absorbance over time demonstrates that the AOP reaction occurs and degrades the dyes. Duckworth (2014) leveraged DCs of 10%, 50%, 70%, and 100% for the  $\text{H}_2\text{O}_2/\text{UV}$  AOP to degrade methylene blue and observed the log of the degradation rate constant increased linearly with increase in DC. Spencer (2014) developed a stainless steel reactor for use in both AOP and disinfection processes and measured the output angle for UV radiation in water to be between 43 and 46 degrees. Scott (2015) incorporated brilliant blue and methylene blue in the AOP experiment and observed degradation rate constant results consistent with Duckworth (2014). Scott (2015) also demonstrated that fouling of the UV LED lens is greater with methylene blue than that of brilliant blue due to the cationic nature of methylene blue interacting with the LED surface. Mudimbi (2015) observed slight

fouling of the LED lens with use of TAR compared to methylene blue, and increased correlation of results with the computer model of the Continuous Stirred-Tank Reactor (CSTR) reactor by incorporating a magnetic stir bar. This greatly reduced the amount of variation between the measured concentration and the models predicted concentration. Mudimbi (2015) also established the AOP conditions in the CSTR reactor could provide up to 23% removal of TAR during 100% DC.

Whether acidic or basic conditions are favorable to the AOP is inconsistent in the literature. Duckworth (2014), Mudimbi (2015), and Scott (2015) did not discuss is what effect, if any, pH of their solutions had on the AOP reaction. This is of interest due to the fact that pH is commonly addressed in AOP literature and does not have the same effect on one contaminant as it does another. In addition, the pH condition may also affect the reaction mechanism of degradation. Measurements taken in the lab demonstrate the pH of the supplied distilled, de-ionized (DI) water was not consistent from one day to the next and could have significantly affected their data. Each contaminant is unique and, thus, the AOP operating procedures could be different from one contaminant to the next. Andreozzi (1999) confirmed that acidity decreased  $\text{HO}\cdot$  production for organic compounds such as toluene, benzene, chlorobenzene, tri/tetra-chloroethylene, and butanol. However, Alpert (2010), showed that higher alkalinity scavenges  $\text{HO}\cdot$  in the UV/ $\text{H}_2\text{O}_2$  AOP of methylene blue, and that this scavenging effect was strongest in the presence of dissolved organic carbon (DOC) between concentrations of 0 to 2 mg/L. Jinhui (2012) demonstrated that pH was not as important for degradation of organic matter as exposure time or light intensity; conversely, Jyothi (2014) established that pH had great effect on phenol and ZnO. Legrini (1993) found that the production of  $\text{HO}\cdot$  from

H<sub>2</sub>O<sub>2</sub> was pH dependent and increased with more alkaline solutions. As previously discussed, the operating conditions of this research are such that this phenomenon does not have an effect. Tayade (2009) showed optimum operation for degradation of Methylene Blue dye at pH 9. Vescovi (2010) examined dioxane, and determined that AOP was optimal at neutral pH.

TAR has three Na<sup>+</sup> ions that may separate from the structure due to interaction with water, which means that in evaluation of the Mass Spectroscopy, masses of 534, 511, 488, and 465 can indicate TAR because the mass weight of Na<sup>+</sup> is 23. TAR can be considered acidic: both the sulfonic acid groups' pKa are 2, and the azo group pKa is 10.86 (Gómez, Arancibia, Rojas, & Nagles, 2012). Therefore, in this study's experimental conditions, it is expected that the H in the azo group does not dissociate. In addition, sulfonic acid grouped with a benzene ring (hereafter referred to the Sulfonic Acid Group) is a common product in both the manufacture and degradation of TAR.

This thesis effort is similar to the work conducted by dos Santos (2014), which examined the effect of pH and UV radiation on TAR, found optimal removal of TAR at pH 6, and identified byproducts of this reaction. However, the work done by dos Santos (2014) is distinct from this research effort: dos Santos (2014) used UV light alone, and not AOP, to degrade TAR. In addition, operating conditions were substantially different from those of this study: light intensity was 10 times greater and initial concentration of TAR was 5 times less.

#### ***2.4.2 AOP Reaction Mechanisms***

There are three main mechanisms by which HO· radicals degrade a compound. They are: Hydrogen Abstraction, OH Addition, or Electron Transfer (Benjamin &



Lawler, 2013; Legrini et al., 1993; Vilhunen & Sillanpää, 2009). Hydrogen Abstraction occurs at saturated organic compounds (i.e. no double bonds). The chemical makeup of TAR is depicted in Figure 1 with a potential Hydrogen Abstraction opportunity highlighted. Legrini (1993) investigated hydroxyl radical production in the H<sub>2</sub>O<sub>2</sub>/UV, Ozone/UV, Ozone/H<sub>2</sub>O<sub>2</sub>/UV, TiO<sub>2</sub>/UV, and vacuum ultraviolet (VUV) AOPs of organic substrates and observed the primary reaction mechanism of hydroxyl radicals to be hydrogen abstraction, which generates radical chain reactions in the presence of dissolved oxygen. Wang (2014) investigated UV radiation on humic acid and observed formation of hydroxyl radicals and suggested that hydrogen abstraction contributed to the formation of acidic functional groups and that OH addition contributed to the split of the carbon chain. Durme, Dewulf, & Sysmans, (2007) studied the mineralization of toluene using non-thermal plasma (DC positive corona discharge) and found formation of hydroxyl radicals, and products to suggest hydrogen abstraction occurred at carbon rings.

OH Addition, also known as electrophilic addition (Aleboyeh, Aleboyeh, & Moussa, 2003; Legrini et al., 1993), occurs at unsaturated bonds (Benjamin & Lawler, 2013), or in the presence of natural organic matter (NOM), can occur at double bonds (Matilainen & Sillanpää, 2010). There are 9 hydrogen atoms in TAR; each represents an opportunity for OH addition, both at the benzene rings and at the N-H bond in the azo group (Figure 2). Legrini (1993) also suggested OH addition as a viable mechanism for the AOPs of organic substrates, particularly for chlorinated phenols. Gonzalez, Oliveros, Wörner, & Braun (2004) explored VUV photolysis in the reduction of aromatic hydrocarbons and found evidence to suggest electrophilic addition of OH was a main facilitator of the degradation of the substrate. Gao, Ji, Li, & An (2014) explored the

hydroxyl radical reduction of triclosan (TCS) and proposed 12 OH addition opportunity locations, as triclosan is a chlorinated phenoxyphenol containing a benzene ring, a phenolic ring, and three chlorine substituents.

The third mechanism for mineralization is electron transfer. This could occur at any location, but perhaps the most apparent indicator would be the loss of either sulfonic acid or the deprotonated carboxylic acid ( $\text{COO}^-$ ) groups. There may be interaction with any of these structures and other constituents in the water after any of the reaction mechanisms have occurred. Gao (2014) observed one electron transfer route in the investigation of TCS in secondary reaction progressions. Gonzalez (2004) evaluated organic compounds, corresponding radicals, and  $\text{NO}^\bullet$  radicals and observed electron transfer from  $\text{NO}^\bullet$  to  $\text{NO}^-$  yielding  $\text{N}_2\text{O}$ . Jyothi (2014) evaluated AOPs utilizing oscillation in photo and sono signals to produce radicals for the degradation of phenol and ZnO and observed electron transfer and that the transfer was pH dependent.

Under similar AOP conditions, the mineralization progresses more quickly for brilliant blue than for TAR (Mudimbi, 2015; Scott, 2015), likely due to the fact that there are many more available double bonds than TAR. Due to the structure of TAR, it is expected that OH addition or electron transfer is the most likely mode for the mineralization of TAR.

Analysis of the byproduct profile for the AOP of TAR has not been conducted previously; however, other studies of the degradation of TAR have observed the following byproduct structures. Maslowska (1996) studied the voltammetric reduction of TAR and observed addition of 2 hydrogens at both nitrogen locations in the azo group. Weisz (2014) showed that TAR is not a pure substance: Pk 5 and Pk7 (manufactured

isomers) form as well as the main structure of TAR, see Figure 3 and following discussion. The structures are distinguished by the number of sulfonic acid groups that form. dos Santos (2014) showed an addition of 2 hydrogen atoms as well, but indicated their locations were in place of two removed  $\text{Na}^+$  due to ionization. dos Santos (2014) also showed fissure of the double nitrogen bond in the azo group, followed by loss of the  $\text{COO}^-$  group in subsequent byproduct formations.

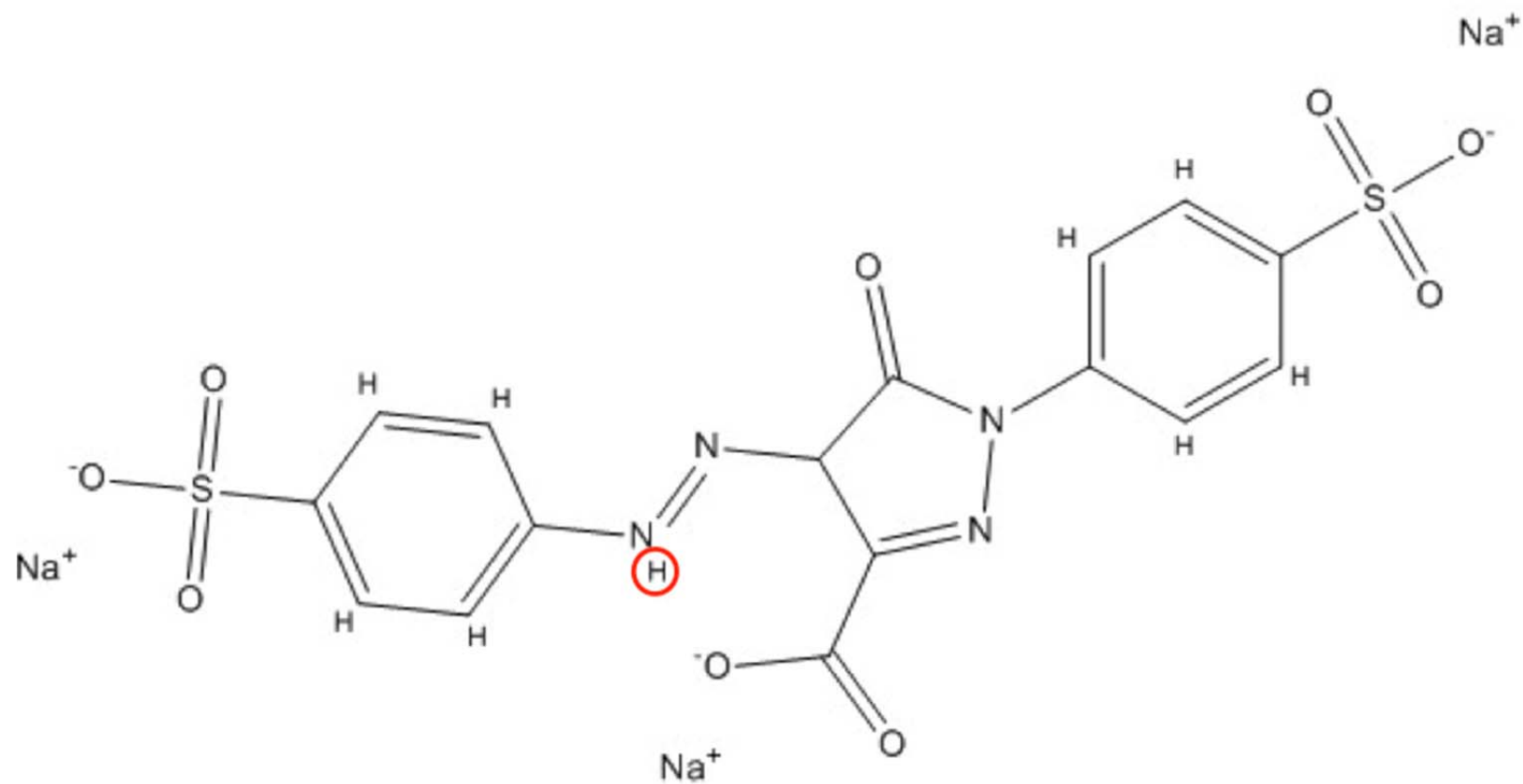


Figure 1: Tartrazine (H Abstraction Location)

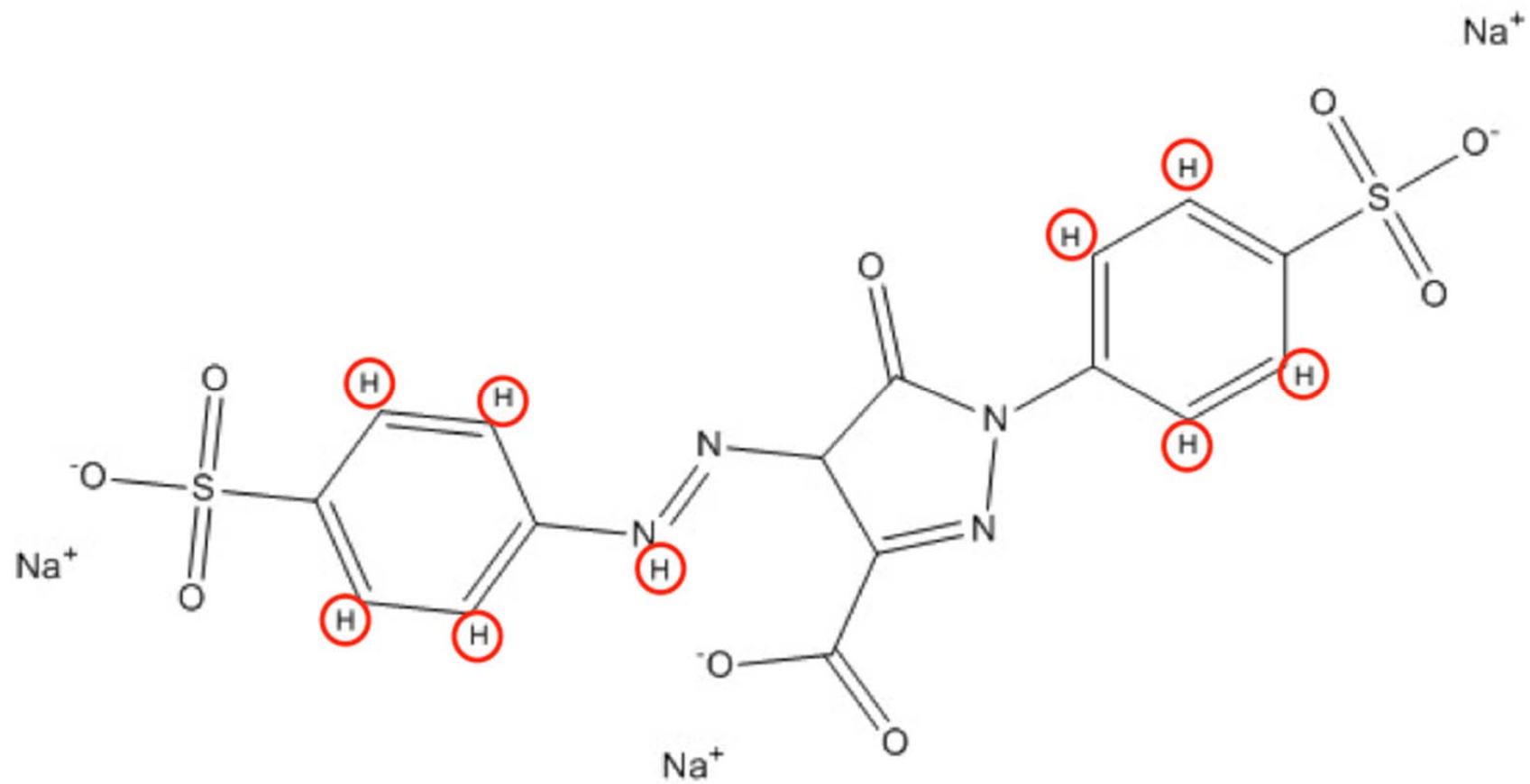


Figure 2: Tartrazine (OH Addition Locations)

## 2.5 Spectral Chromatographic Contrast Angle

One method of comparing byproduct profiles without identifying the structures is in the calculation of CCAs (Wan, Vidavsky, & Gross, 2002). The CCA is denoted by  $\theta$ , and is a vector in multi-dimensional space. High angles (up to 90 degrees) indicate differing byproduct profiles, while low angles indicate strong similarity. This is the most reliable comparison method for library searches for compound identification (Wan et al., 2002). Theta is calculated by Equation 4, where a and b are the two spectra under comparison and i is the number of points in each data set; i also indicates the number of dimensions of space in which the vector exists.

### Equation 4: Chromatographic Contrast Angle Calculation

$$\cos\theta = \frac{\sum_i a_i b_i}{\sqrt{\sum_i a_i^2 \sum_i b_i^2}}$$

This method has been widely used in a variety of applications. Li (2001) used this method in HPLC analysis of fatty acids, specifically for photodiode array detector produced spectra. The produced spectra were compared with the spectra library for spectrum matching. The method of using contrast angles was also used to analyze sample purity, and used to indicate photometric error, or solution imprecision. Kushnir (2005) showed that contrast angle calculation is useful for LC-MS for identification of compounds, particularly if two or more mass transitions are used. In this case, calculation complexity can be greatly reduced. In addition, Zhang (2011) used spectral contrast angles to analyze peptide modification trends, and recommended the method as statistically acceptable to compare protein/ligand structures. However, the “self-angles”

for the protein/ligands used were much greater (up to 35 degrees in some cases) than those used by Wan (2002).

## **2.6 Tartrazine and Chromatography**

TAR is defined as  $C_{16}H_9N_4Na_3O_9S_2$ , has a molecular weight of 534.4, and is commonly recognized as is represented in Figure 1 (Weisz et al., 2014). However, TAR is a manufactured product and it is not a pure substance. Other isomers of the molecule are depicted in Figure 3, (Weisz et al., 2014).

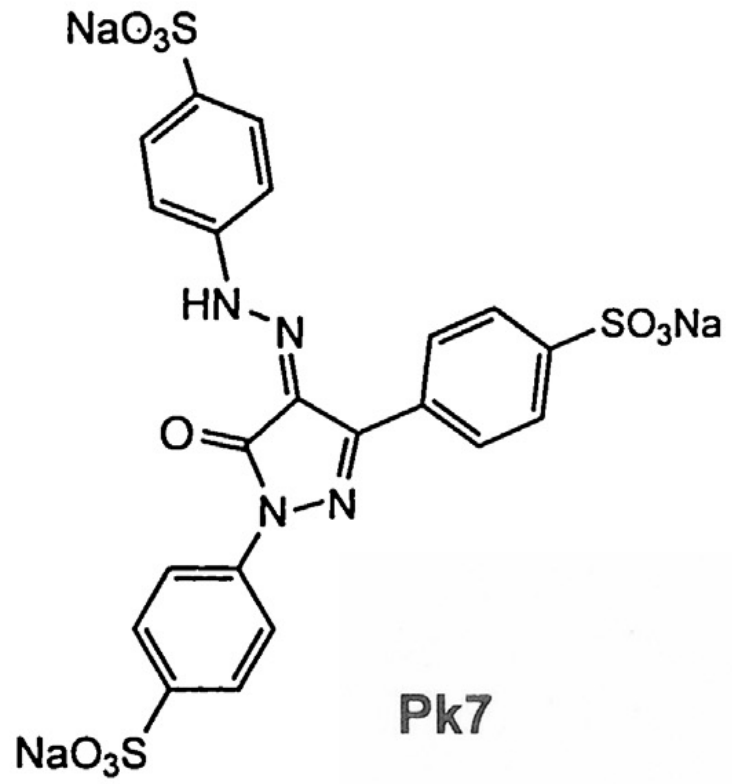
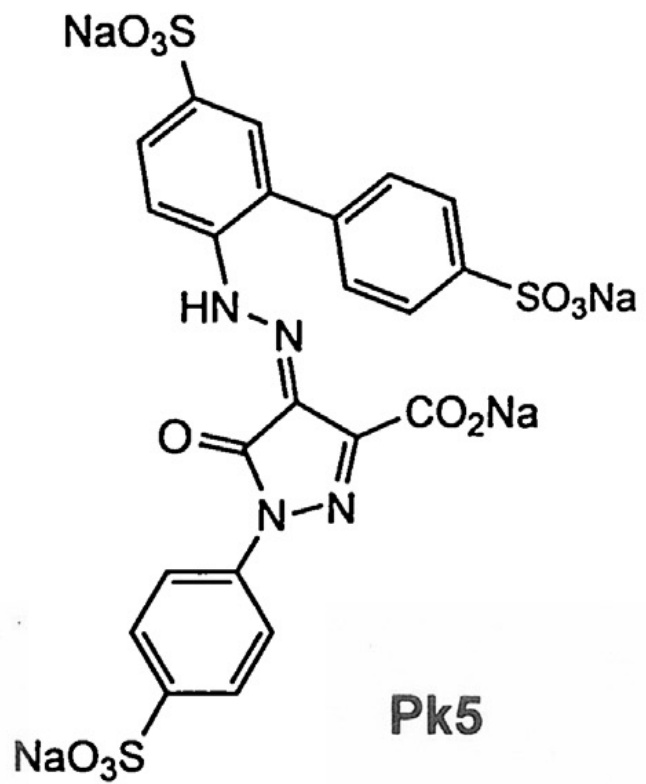


Figure 3: Tartrazine Manufacturing Isomers



These manufactured isomers, Pk5 and Pk7, are different from the main structure of TAR due to an extra sulfonic acid group, either forming off a benzene ring or forming in place of the COO<sup>-</sup> location. Their molecular weights are 713.5 and 646.5, respectively. According to Weisz (2014), Pk5 is detected by UV-Vis, with peaks at 258 and 428.1 nm, whereas Pk7 is characterized by peaks at 276.9 and 404.1 nm.

Other studies have been conducted on decomposition products of TAR. In the UV decomposition of TAR study, several noteworthy products emerged: fully ionized TAR with the addition of 2 Hydrogen atoms, the fissure of the double nitrogen bond of the azo group, and secondary products losing the COO<sup>-</sup> group (dos Santos et al., 2014).

Maslowska (1996) observed both TAR plus 2 hydrogen atoms (although, proposed a different structure than dos Santos (2014)), as well as a “reduction of [the] azo group... result[ing] in the formation of a hydrazine compound” in evaluating the voltammetric reduction of TAR.

## **2.7 Objectives**

The purpose of this study is to evaluate degradation of TAR using operating conditions such as DC and pH to characterize ideal operation procedures and to identify reaction mechanisms that occur in the H<sub>2</sub>O<sub>2</sub>/UV LED AOP of TAR. The objectives of this work are:

- Determine the effects of pH and DC on the removal of TAR
- Determine the effect of pH and DC on the byproduct profile
- Propose chemical structures of measured byproducts

### III. Methodology

#### 3.1 Materials and Equipment

Materials and equipment between the AOP Experiment are varied and will be discussed individually in the following subsections. However, operating parameters are as follows. Water was conveyed through PharMed® BPT tubing (inner diameter of 0.8 millimeters, Valley Forge, PA) via a digital pump – Easy-Load II Masterflex, model 77200-50 (Cole Parmer, Vernon Hills, IL ) at rate of 0.7 mL/minute.

DC programs for both reactors' LEDs were controlled by Data Acquisition System Laboratory (DASYLab, version 12, Stamford, CT). Power was delivered to the circuit board by the driver box measurement computing device (USB-2408-2AO, Norton, MA), and the circuit board delivered 20 mA to each LED (Duckworth et al., 2014; Spencer, 2014). The luminous flux and optical power output of bulbs were measured through Labsphere® integrating sphere (Labsphere ® North Sutton, NH), which was calibrated with a Deuterium Lamp (S/N 667329).

To ensure LEDs are functioning properly (correct voltage and DC waveform) at each experiment without deconstructing the reactor, each LED signal was measured by oscilloscope (OWON PDS5022T, Zhangzhou, China). Kimtech Kimwipes ® (Kimberly-Clark, Roswell, GA) were used to clean the cuvette and the pH meter diode.

Finally, in order to ensure complete mixing of the solutions within the reactors, both reactors contained a magnetic stir bar and were placed on a Corning Stirrer Table; model PC-210, S/N 220197028704 (Corning, Inc. Corning, NY).

### ***3.1.1 AOP Experiment***

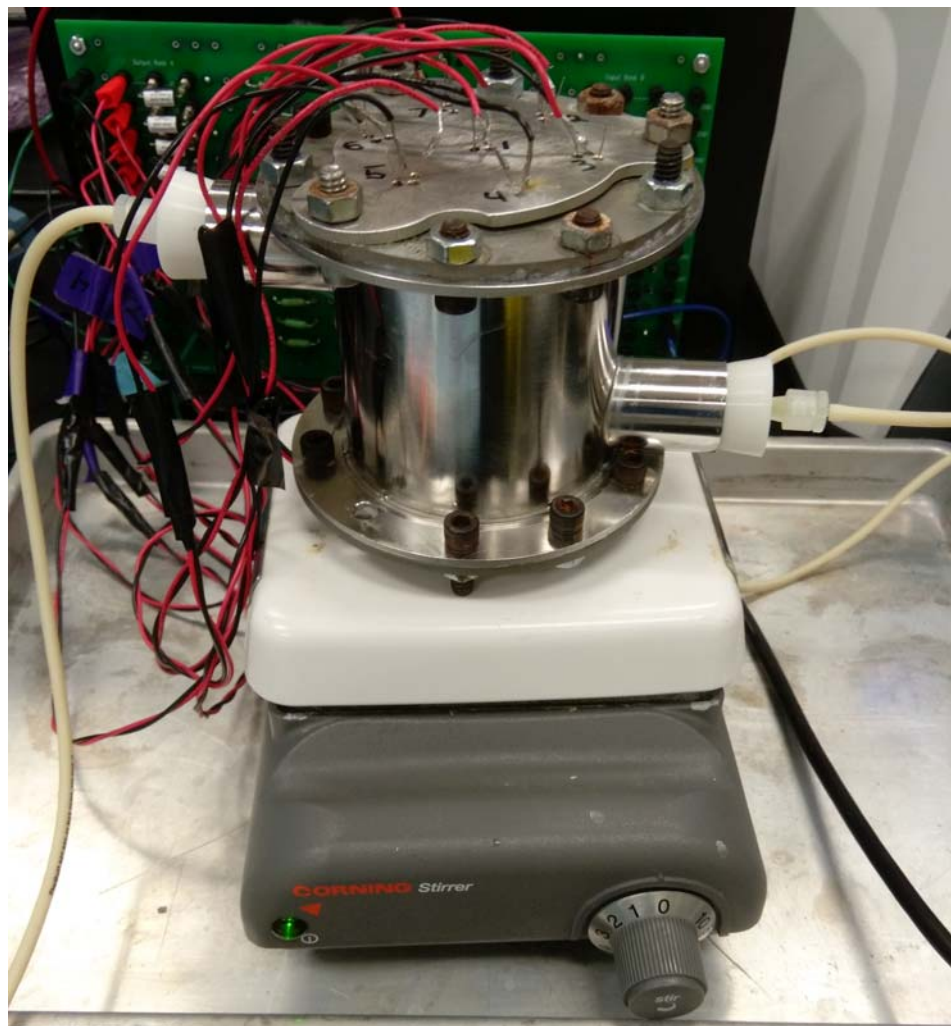
In order to answer the first research question, two Independent Variables (IVs) of pH and DC were adjusted with the anticipation of observing significant differences between the respective first order rate constants ( $k_s$ ). The pH was adjusted to levels of 6, 7, 8, or 9; the DCs were adjusted from 0%, 5%, 10%, 20%, 30%, 50%, 70%, and 100%: the total number of planned experiments was 36. The order in which the experiments were executed was randomized to prevent introducing a learning curve into the data. Intentional repeat experiments were scheduled to be conducted when degradation behavior was not anticipated or when errors were made in the preparation stages. A total of 6 additional experiments were conducted: an accidental repeat pH 8 at 70% DC, an error in pH adjustment led to an experiment operated at pH 5 at 70% DC, a repeat of pH 9 at 50% DC was conducted because the first iteration did not use a mix table, an experiment operated at pH 7 and 50% DC was operated at 1.5 mL/min instead of 0.7 mL/min, and unexpected results led to the repeat of experiment conditions pH 6 at 70% DC and pH 8 at 100% DC.

The solution for each AOP experiment consisted of Hydrogen Peroxide (30% in water, Fisher Scientific, Pittsburgh, PA), TAR (Acid Yellow 23, CAS: 1934-21-0, Sigma-Aldrich Co, St. Louis, MO), reverse osmosis, purified, deionized water (DI Water, AFIT ENV Lab), and stock solutions of NaOH (1.0, 0.1, or 0.01 M, AFIT ENV Lab) or as required for pH adjustment. It is important to note that the pH level of the DI water was not consistent throughout the experiment and ranged from 4.1 to 7.4. This variation is not caused due to the pH meter, which was calibrated before each use; it is likely due to a malfunction in the storage or production of the DI water.

The exact amounts for the solution, measuring and mixing procedures are detailed as follows. Mass was measured using a Mettler Type AT 261 Delta Range SNR L43911 mass scale (Hightstown, NJ). It is important to note that the mass scale was not perfectly balanced and the fisheye was not centered. The amount desired for TAR was 0.02672 g, which equates to 0.05 mmol/L. The mean measurement for TAR was .026728 g with a standard deviation of 1.97e-5 g. The preferred amount of H<sub>2</sub>O<sub>2</sub> was 2.87953 g (30% in water) (Mudimbi, 2015), which is approximately 25 mmol/L. The mean measurement for H<sub>2</sub>O<sub>2</sub> was 2.878817 g with a standard deviation of 2.599e-3 g. H<sub>2</sub>O<sub>2</sub> is volatile and the precision of the conveying implement was low. This explains why the standard deviation for H<sub>2</sub>O<sub>2</sub> mass measurement was much higher than that of TAR. 1000 mL of DI water was measured with volumetric flasks  $\pm$  0.6 mL.

Upon completion of mass measurement, TAR was added to the DI water, followed by the H<sub>2</sub>O<sub>2</sub>. The solution was mixed for 10 – 15 minutes and a pH reading was made. A determination was then made for how much NaOH was required and at what concentration. This was measured and added to the solution, mixed, and a new pH reading was made using SevenMulti pH Meter, S/N 1229425365 (Mettler-Toledo Group, Schwerzenbach, Switzerland), see Appendix A for calibration procedures. This process was repeated until arriving on the desired pH level as described in the experiment schedule, see Appendix B. In the event of overshooting the desired pH, a future scheduled experiment was conducted instead. Upon complete mixing of the solution at the desired pH, the solution was poured into the reactor. The reactor was designed and constructed by Duckworth (2014) and Spencer (2014), and houses seven 245 nm UV LEDs from Sensor Electronic Technology, Inc. (Columbia, SC). The reactor was

constructed of 316 stainless steel; inflow and outflow ports were 1 inch in diameter, see Figure 4.



**Figure 4: AOP Reactor**

This reactor contained a half-inch stir bar to meet the assumptions of a CSTR. After the reactor is full and placed on the mix table, calibration curve mixtures were prepared.

The calibration curve mixtures were comprised of 0% solution, 25%, 50%, 75%, and 100%. For 0% solution, 10 mL of DI water was all that is required. For 25% solution calibration, 7.5 mL of DI water was combined with 2.5 mL of the solution. For 50% solution calibration, 5 mL of DI water was combined with 5 mL of solution. For 75%, 2.5 mL of DI water was combined with 7.5 mL of the solution. For 100%, 10 mL of solution was required.

The outflow of the CSTR was connected to a continual flow, quartz cuvette for use in Agilent Technologies Cary 60 UV-Vis Spectrophotometer (Santa Clara, CA). See entire setup in Figure 5.

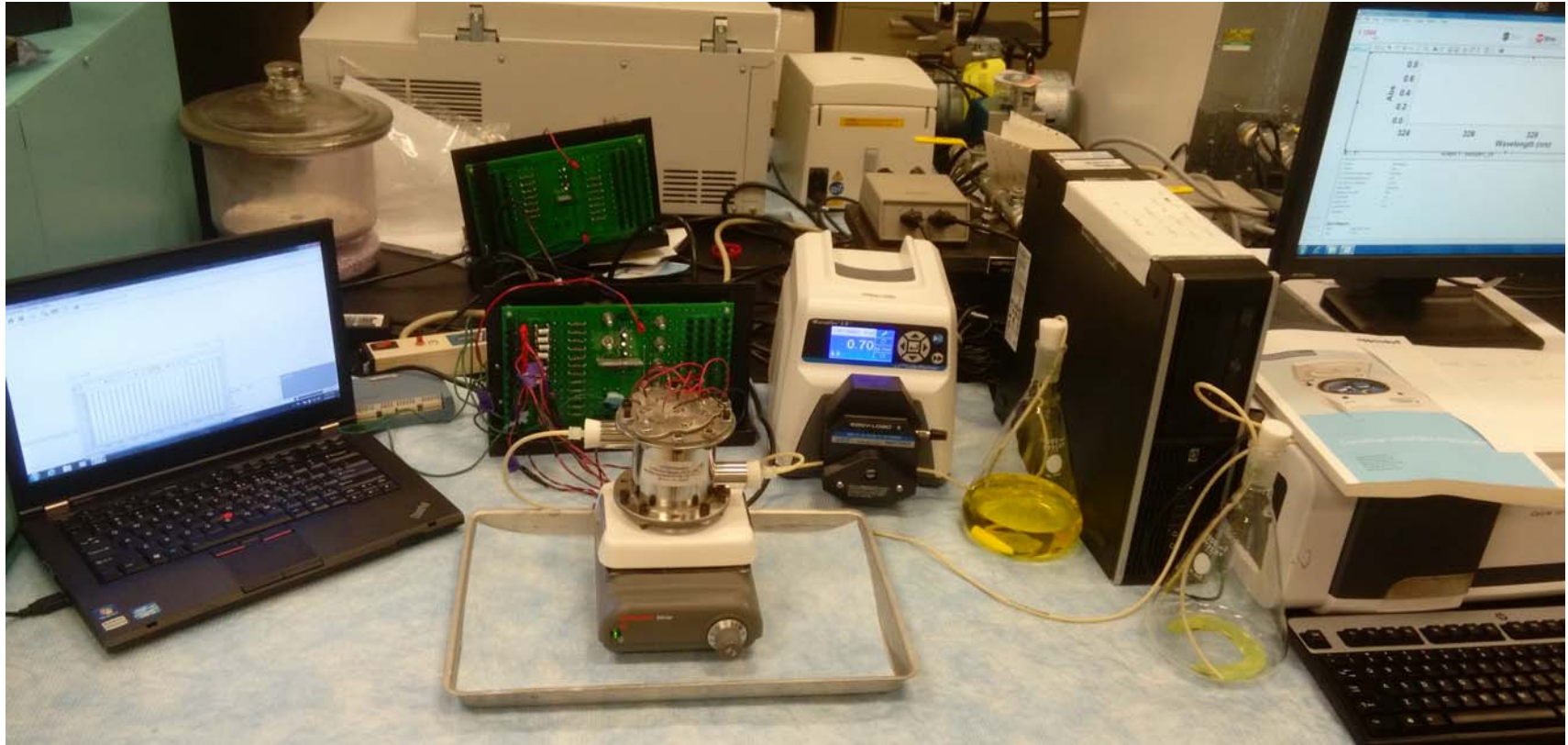


Figure 5: AOP Experimental Setup



The Cary 60 Scan program was set up to measure absorbance every five minutes for five hours between 425 and 435 nm; the absorbance peak for TAR is 430 nm. Five hours was selected as the experiment operating time due to previous research operating conditions (Mudimbi, 2015; Scott, 2015). It should be noted, that the full residence time for this reactor at flow rate of 0.7 mL/min is 500 minutes; however, steady state removal was achieved prior to the 300 minutes of operation. After the experiment concluded, calibration curve mixtures were individually loaded into the cuvette through a syringe and the absorbance was measured through Cary 60 Rapid Result function at 430 nm. These values were entered into the excel program which calculated the calibration curve equation and R<sup>2</sup>. The data collected by Cary 60 was added to this spreadsheet and the model was created using solver to find k<sub>s</sub> (min<sup>-1</sup>) see Equation 5, where C<sub>F</sub> is the final concentration, C<sub>I</sub> is the initial concentration, τ is residence time in the reactor, and t is the retention time (see data and charts in Appendix C and D, respectively). To calculate the adjusted first order rate constant (k<sub>s,adj</sub>), k<sub>s</sub> is divided by the duty cycle (DC), see Equation 6.

**Equation 5: CSTR Equation**

$$\frac{C_F}{C_I} = \left( \frac{1}{1 + \tau k_s} \right) (1 + \tau k_s e^{-\left(\frac{1}{\tau} + k\right)t})$$

**Equation 6: Adjusted First Order Rate Constant**

$$k_{s,adj} = \frac{k_s}{DC}$$

In the effort to answer the second research question, the byproducts of this AOP were examined. Using the chromatography of untreated TAR as a baseline and

foundation for the analysis method, effluent streams from the AOP Experiment were compared to that of the baseline. Using the information from Benjamin & Lawler (2013) and dos Santos et al. (2014), potential degradation mechanisms were selected that might explain the observed changes in the chromatography. Special attention was paid to the byproducts in experiments in which the pH of the solution increases.

Thirty minutes prior to the completion of each experiment, the outflow from the cuvette was transferred to a different storage beaker. The pH of this effluent was measured, and approximately 10 mL was taken for use in byproduct analysis. The 10 mL of effluent was filtered through a 0.2  $\mu\text{m}$  hydrophilic syringe filter (Minisart from Sartorius Stedim Biotech, Goettingen Germany). This was stored in the dark at 2 degrees Celsius until analysis by High Performance Liquid Chromatography (HPLC).

### ***3.1.2 Byproduct Analysis***

#### **3.1.2.1 Chromatographic Contrast Angle Analysis**

The first step to determine how byproducts were formed was to calculate CCAs for each experiment effluent chromatography. The byproducts were analyzed using HPLC, both a positive ionization and a negative ionization analysis was conducted (see method files in Appendix H and I, respectively). The HPLC was an Agilent Technology 1260 Infinity combined with 6130 Quadrupole LC/MS (Agilent Technologies, Santa Clara, CA). The method included use of a SUPELCO Analytical column (Ascentis<sup>®</sup> Express C18, Cat#53829-U, 15 cm x 4.6mm, 2.7  $\mu\text{m}$ ) and a particle fragmentor, with acetonitrile as the mobile phase. Using Equation 4, the CCA was calculated between the 0% DC experiments and the H<sub>2</sub>O<sub>2</sub> Control experiments within each pH level. In addition, the CCAs were calculated between each experiment and the 0% DC of the respective pH

level. Wan (2002) individually measured the same analyte 28 times to calculate a “self-spectral angle”. In theory, if two vectors are identical, their CCA should equal zero. However, in application, the readings are not so precise. Wan's (2002) calculations for the self-spectral angle contrast yielded  $2.7^\circ \pm 1.6^\circ$ , and  $2.2^\circ \pm 1.0^\circ$  for analytes a and b. This study did not include the calculation of a self-spectral angle because of the large number of experiments to analyze. Therefore, for the purpose of this study any CCAs calculated less than  $5^\circ$  will be considered for similarity. Each data set for the analytes of this study included over 120 points; therefore, this study's CCAs are calculated in 120-dimensional space and cannot be graphically represented on traditional Cartesian axes.

#### 3.1.2.2 Mass Spectroscopy Analysis

Analysis of the MS spectra suggested byproduct structures. See Positive and Negative Chromatograms, and MS plots in Appendix J and K, respectively. Factors that were considered were mass to charge ratios (kinetic energy) reported by the MS, but also the fact that in this method, a doubly charged particle with a mass of 26 will be indistinguishable from a single-charge particle with a mass of 13. This study's AOP experiments were conducted over several months, and the byproducts of each experiment were stored at 2 degrees C until completion of all AOP experiments, so that each experiment's effluent could be processed by the HPLC on the same day. However, due to the randomization of the experiment order, any effect time could have on byproduct profiles (whether long term reactions continued or if steady state was reached upon completion of the experiment) should not be statistically significant with respect to any DC or pH regression analysis.

### **3.2 H<sub>2</sub>O<sub>2</sub> Control AOP Experiment (0% DC)**

There may be interaction with the dye and the pH adjustors. In order to form a baseline, a complete solution was mixed at each pH level and transferred through the CSTR reactor but the UV LEDs were not powered. The  $k_s$  was expected to be close to or equal to zero. Effluent samples from each of these experiments were stored in the refrigerator to be evaluated via HPLC along with the other experiment effluents.

### **3.3 UV Control AOP Experiment (100% no H<sub>2</sub>O<sub>2</sub>)**

In order to ensure that there is no interaction between the pH adjustor and the UV radiation, a solution was mixed without H<sub>2</sub>O<sub>2</sub> and transferred through the CSTR reactor while running the 100% DC. The  $k_s$  was expected to be close to or equal to zero. Effluent samples from each of these experiments were also collected and stored for evaluation with the byproducts in the HPLC.

### **3.4 Statistical Methods**

The purpose of this section is to outline the statistical methods used for data analysis for this research effort. This section provides computer program information and execution procedures for Analysis of Variance (ANOVA), Tukey, and Linear Regression analyses. These analyses were conducted to predict the first order rate constant, as well as chromatographic contrast angles. These were the “response” variables, and are denoted by  $Y_1$  or  $Y_2$ . Predictor variables, such as pH, DC, operator of the experiment, spin table speeds, date of the experiment, etc. were used in analysis and are denoted by  $X_1, \dots, X_i$ . P-values were considered statistically significant if they were less than 0.05 (95% confidence).

In order to gain a better understanding of statistical significance of the levels within pH and DC, dummy variables (DVs) can be incorporated into models. DVs are binary; pH levels are represented by three dummy variables, for example, pH 6, pH 7, and pH 8 (this assumes that pH 9 is the baseline). DC levels are represented by seven DVs, for example, DC 5, 10, 20, 30, 50, 70, and 100 (which assumes DC 0 is the baseline). All regression models in this study include DVs.

#### ***3.4.1 Analysis of Variance***

One-way Analysis of Variance (ANOVA) analyses were conducted for each response variable. This uses the F-Test and is statistically significant when the p-value is less than 0.05. Each ANOVA test incorporated pH and DCs as predictors. The ANOVA report is generated in JMP® by the “Fit Y by X” analytical tool. Then, “Means and ANOVA” option is chosen for the plot which reports the means, standard deviation error, and upper/lower 95% for each category within each X variable. The “Prob > F” displays the p-value of the test. The F-test only shows that one of the categories within pH or DC is significant; it does not specify which pH level or DC is significant. To better clarify statistical distinctions, Tukey analyses was performed.

#### ***3.4.2 Tukey Analysis***

Tukey Analysis was conducted for each response variable. This uses the Q-Test and is statistically significant at  $\alpha = 0.05$ . Each Tukey analysis incorporated pH and DCs as predictors. The report is generated in JMP® by the “Fit Model” tool. Then under each variable, “LS Means Plots” and “LS Means Tukey HSD” options are selected. These display the LS Means plot, which shows means and error bars; and the Tukey table, which shows statistically significant comparisons in red. This also displays a table where

each level (i.e. pH levels 6 through 9 or DC levels between 5% and 100%) is categorized by letter groups (see Appendix). These letters connect levels which are not statistically different; therefore, levels not connected by the same letter are significantly different. While the Tukey analysis provides insight to what levels are distinct, it doesn't provide the whole picture. To better understand what levels are significant predictors, regression analysis must be conducted.

### ***3.4.3 Linear Regression Analysis***

#### **3.4.3.1 Effect Tests**

Linear regression is an iterative process. Evaluating ANOVA and Tukey analyses gives an idea of what might be significant, but another tool in selecting viable predictor variables is to use a Stepwise fit. The stopping rule is p-value threshold (set to 0.25 to enter and to leave), and the direction is mixed. Every conceivable predictor variable is loaded and compared against one another. After the rules are established, the model computes and shows all variables ranked by the p-value for that particular arrangement of variables. However, these are suggested variables and their respective p-values will change with any change in the model, in addition, may not uphold required assumptions, or meet reasonable p-values. Ideally, all significant predictor variables have p-value of less than 0.05. Having too many predictor variables can also have a negative effect on the validity of the model. For this reason, the adjusted  $R^2$  will be the preferred value used in this research effort for amount of understood variance. The adjusted  $R^2$  carries a penalty for increasing the number of variables, as well as for variables of low added benefit. After each model is generated, four columns must be added to the data table: the residuals

of the model, the studentized residuals of the model, Cook's D Influence, and the residuals of the model squared, each to be discussed in coming sections.

#### 3.4.3.2 Required Assumptions in Regression Modelling

There are three assumptions that must be upheld in order to produce a valid regression model. They are normally distributed residuals, constant variance, and independence. Each of these assumptions requires a test.

Whether the residuals are normally distributed is evaluated with the Shapiro-Wilks Test (W-Test). A distribution is created for the residuals of the model. Then, a "continuous, normal fit" tool is selected and under the "fitted normal" dropdown menu, the "goodness of fit test" is selected, which reports the Shapiro-Wilks test. The assumption of normality is upheld with p-values of greater than 0.05.

The assumption of constant variance is tested by the Breusch-Pagan test. This requires an additional model to be generated with all the same X variables as the original model, only the Y variable is the residuals of the model squared. This creates a Sum of Squares Regression (SSR) model. The only value of interest reported by this SSR model is located under the Analysis of Variance heading; the value for the model-sum of squares is required for the calculation of the Breusch-Pagan test statistic (TS). In addition, three values required for the Breusch-Pagan test are found in the original model. The values are: N (located after "observations or sum wghts"), degrees of freedom (located under the ANOVA heading; the value for model-DF), and the Sum of Squares Error (SSE) (located under the ANOVA heading; the value for error-sum of squares). These values are incorporated into the following excel equations for the TS (Equation 7) and p-value (Equation 8). The final step in testing for constant variance is the  $\chi$ -distribution in

excel, coded “Chidist(TS, degrees of freedom)”. The resulting p-value is compared with  $\alpha$ , and if the p-value is greater than 0.05, then the assumption of constant variance is upheld.

**Equation 7: Breusch-Pagan Test Statistic**

$$TS = \frac{\frac{SSR}{2}}{\left(\frac{SSE}{N}\right)^2}$$

**Equation 8: Breusch-Pagan P-Value**

$$p - value = \chi(TS, DF)$$

Finally, the assumption of independence is tested with the Durbin-Watson test. This is found in the original model report, under “Row Diagnostics” then “Durbin-Watson Test”. This displays the TS, but not the p-value. This is corrected by selecting the drop down for Durbin-Watson, and selecting “significance p-value”. If the p-value is greater than 0.05, then the assumption of independence is upheld.

If any of these tests are not upheld, the model may still be valid. However, outlier detection must be conducted (to make the case that a robust deviation has occurred). If any cohorts exist, they should be identified and incorporated to the model. The residual by predicted plot must also appear to have no trend. If none of these steps resolve the issue, other variable combinations must be considered, and the assumptions tests must be conducted again.

3.4.3.3 Outlier and Influence Detection and Processing

Outliers and overly influential points are mainly detected by two respective tools. The first is a histogram of the studentized residuals. The desired outcome is that no points fall outside  $\pm 3$  standard deviations. The second tool is an overlay plot of Cook’s D



Influence. In this plot, it is important that no points rank higher than 0.5. Any points that are identified by these tools can be evaluated – if any explanation can be offered as to why these points in particular can be grouped together (for example, all conducted on the same day, or during some condition that did not apply to the rest), a cohort variable may be created. Overly influential points may cause issues with the assumptions tests, but if all the assumption tests pass, then the points may still be included. If not, there may be a reasonable case to have the points excluded from the model due to the fact they were overly influential.

#### 3.4.3.4 Model Formation

Once a model is formulated in which all the tests pass and a reasonable adjusted  $R^2$  is achieved, the model may be evaluated for functionality. Variance Inflation Factor (VIF) scores must be less than 2 for all parameters. All models in this study are linear, and the equation for the model is generated in the original model report under “Parameter Estimates”. The base formula for linear regression is shown in Equation 9, where  $Y$  is the model’s predicted value,  $e$  is the intercept,  $X_i$  are the predictor variables, and  $\beta_i$  are the respective predictor variable coefficients.

#### **Equation 9: Linear Regression Model**

$$Y = e + \sum_{i=1}^n \beta_i X_i$$

#### 3.4.3.5 Error Analysis

Once the formula is entered into a column in the data sheet, a new column is generated to calculate the model’s Average Predictive Error (APE), which is defined by

the absolute value of the true response value minus the model's predicted value divided by the true response value, see Equation 10.

**Equation 10: Regression Model APE Score**

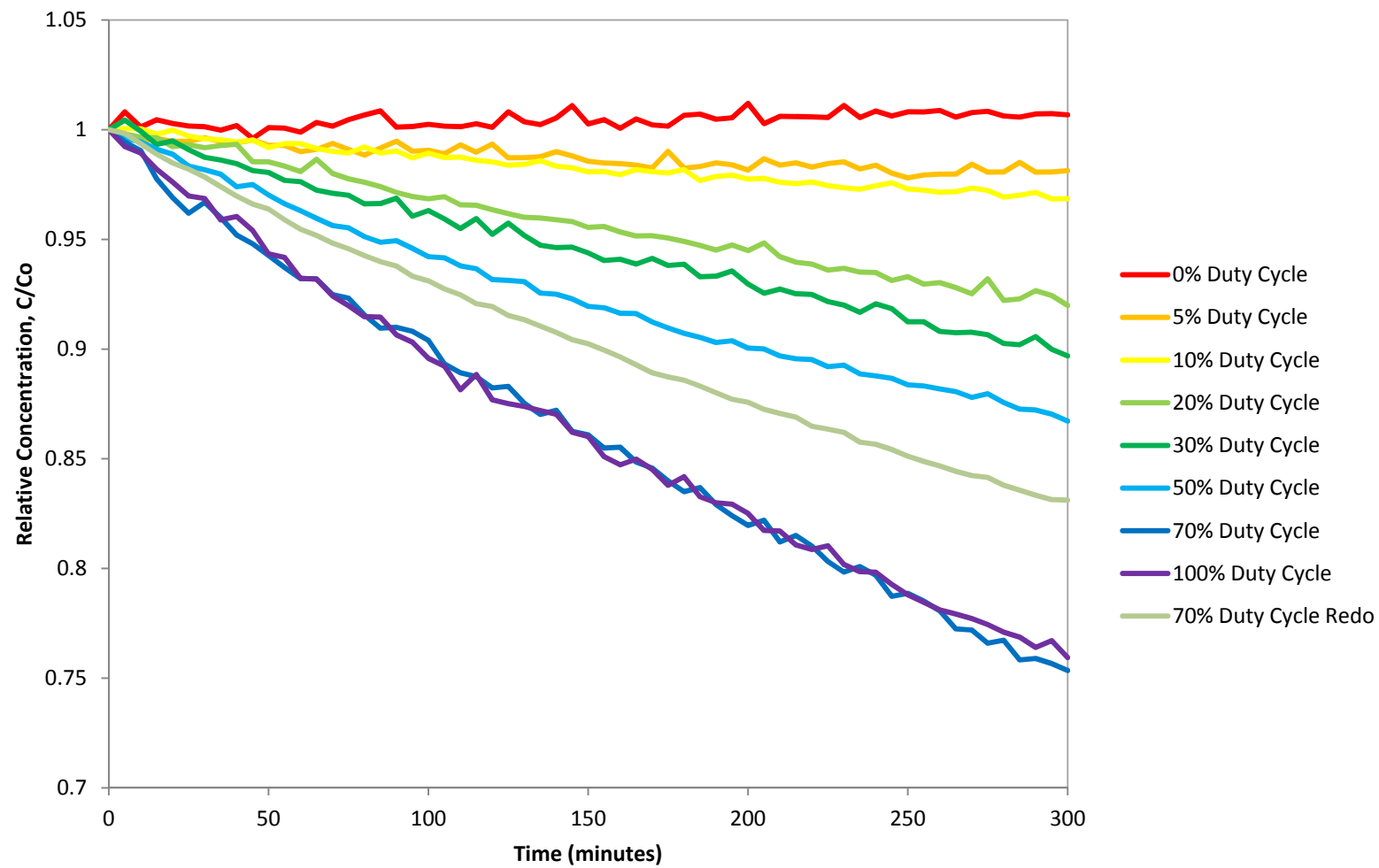
$$APE (\%) = \frac{|Y_{true} - Y_{predicted}|}{Y_{true}} * 100\%$$

Finally, these values are used to create a histogram of all the APEs. This research report will state each regression model's respective mean APE, the median APE, the maximum APE, and the amount of the deviation from the true value generated by that specific maximum error.

## IV. Results and Discussion

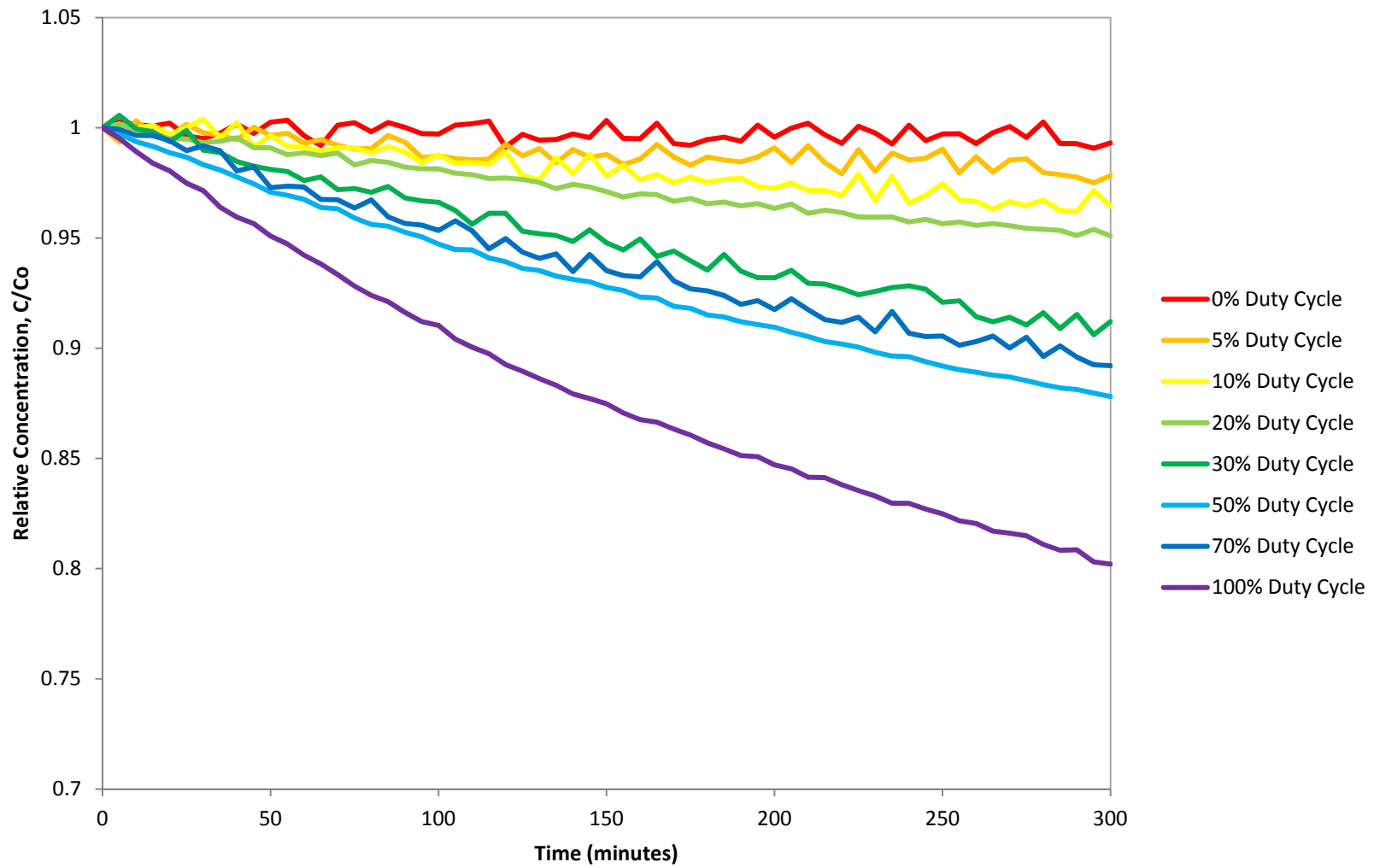
### 4.1 The Effect of pH and Duty Cycle on the Relative Concentration of Tartrazine

Figure 6 shows the effect of DC on the relative concentration of TAR at pH 6. The x-axis shows the time of the experiment; the y-axis shows the relative concentration ( $C/C_0$ ). Over the course of 300 minutes, the relative concentration of TAR decreased to 0.98, 0.97, 0.91, 0.90, 0.87, 0.75 - 0.83, and 0.76 for DCs of 5%, 10%, 20%, 30%, 50%, 70%, 70% repeat experiment, and 100% respectively. Noteworthy results include the first iteration of the 70% DC, for which the  $C/C_0$  was approximately 0.75 -- the greatest level of removal observed in this study, and an improvement of 2% removal compared to the optimal removal observed by Mudimbi (2015) at 100% DC. However, Mudimbi (2015) did not record the pH of this solution. The pH 6 at 70% DC condition was repeated approximately two months later, and only achieved relative  $C/C_0$  reduction of approximately 0.83. This may be attributed to the decrease in output capability of the LEDs due to operating time. The second highest concentration reduction was for the 100% DC, approximately 0.76. A possible explanation for the decreased performance at the 100% DC may have been due to different operators between the three experiments. However, this explanation was not found to be a significant predictive factor for the first order rate constant. The rest of the data set results were as expected, with the first order rate constant gradually increasing with increasing DC level. These results mean that operating the experiment at pH 6 can increase the proficiency of the AOP of TAR. Additionally, optimal TAR removal may be accomplished with greater efficiency than the 100% DC.



**Figure 6: The Effect of Duty Cycle on the Removal of Tartrazine at pH 6**

Figure 7 shows the effect of DC on the relative concentration of TAR at pH 7. The x-axis shows the time of the experiment; the y-axis shows the relative concentration ( $C/C_0$ ). The magnitudes of the relative concentration of TAR were recorded as follows: 0.98, 0.96, 0.95, 0.91, 0.88, 0.89, 0.80 for DCs of 5%, 10%, 20%, 30%, 50%, 70%, and 100%, respectively. These first order rate constants appeared as expected, gradually increasing between 0% and 100% DCs, with one exception. The reduction in relative concentration for the 50% DC (0.88) narrowly exceeded the reduction for that of the 70% DC (0.89). This was not due to the degradation of the LEDs over time, because the 50% was conducted a month after the 70%. This will be discussed further for the pH 8 and 9 sections. Also, the 100% DC (20% removal) substantially outperformed the 50% DC (12% removal). This data set demonstrated that at pH 7, the removal of TAR generally follows AOP/dye reduction trends previously observed by Duckworth (2014), Mudimbi (2015) and Scott (2015).



**Figure 7: The Effect of Duty Cycle on the Removal of Tartrazine at pH 7**

Figure 8 shows the effect of DC on the relative concentration of TAR at pH 8. The x-axis shows the time of the experiment; the y-axis shows the relative concentration ( $C/C_0$ ). The observed concentration of TAR after 300 minutes was 1.00, 0.99, 0.97, 0.96, 0.84, 0.87 - 0.91, 0.90-0.90 for DC levels of 5%, 10%, 20%, 30%, 50%, 70%, 70% duplicate, 100%, and 100% duplicate, respectively. In this operating condition, the greatest removal was observed during the 50% DC (16% removal), the second greatest removal was observed during one of the 70% DC iterations (13% removal), and the third greatest removal was observed for both the 100% DC iterations (10% removal). This inversion of the relationship between removal and the DC was not expected. It is likely the abundance of  $\text{OH}^-$  and the bicarbonate (see Equation 2) in the solution may have a scavenging effect on the hydroxyl radicals (Alpert et al., 2010). This may also indicate an interaction between this scavenging effect and the higher DCs. This data showed that at higher pH levels the first order rate constant is negatively correlated with higher DC, resulting in diminished TAR removal.

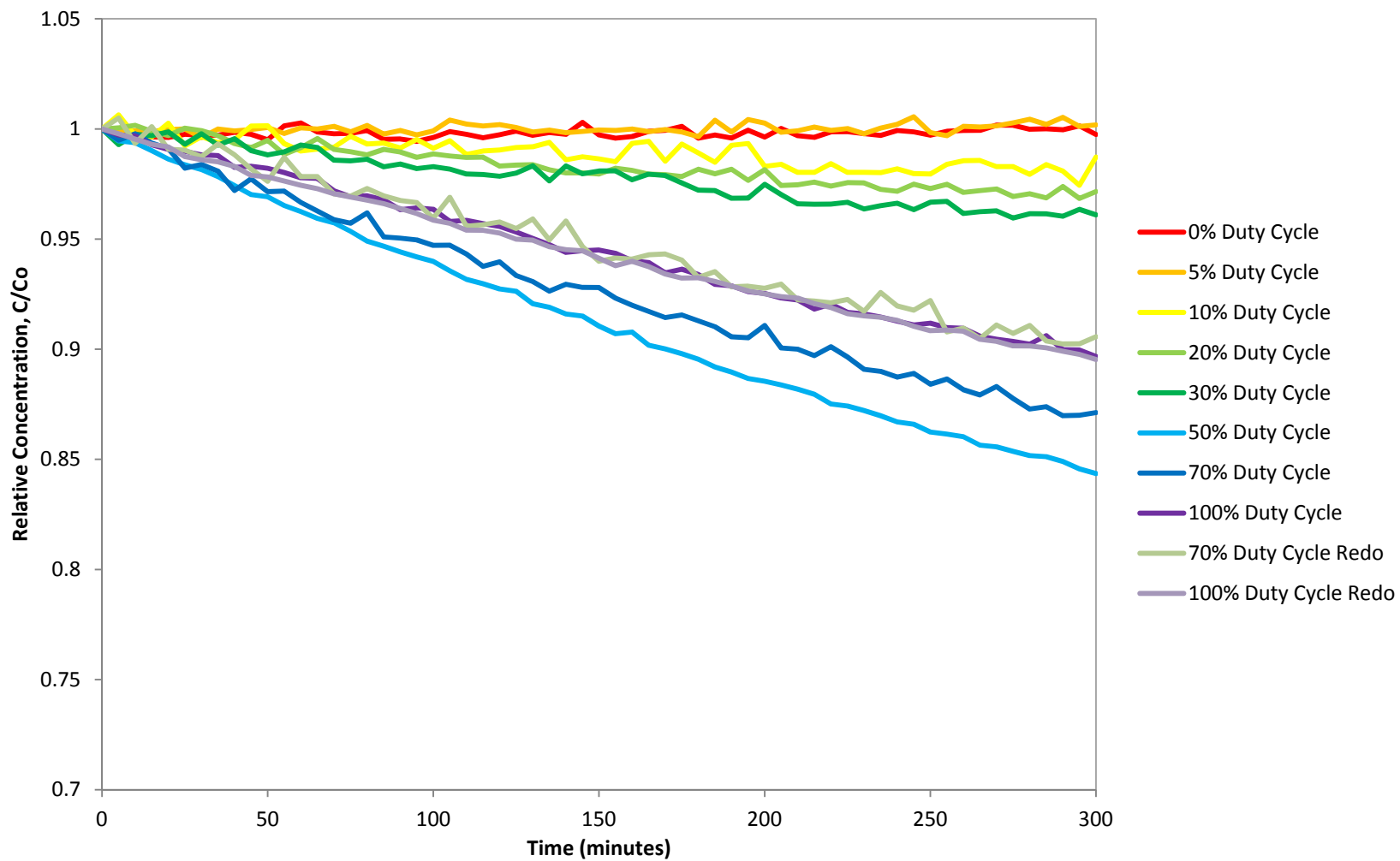
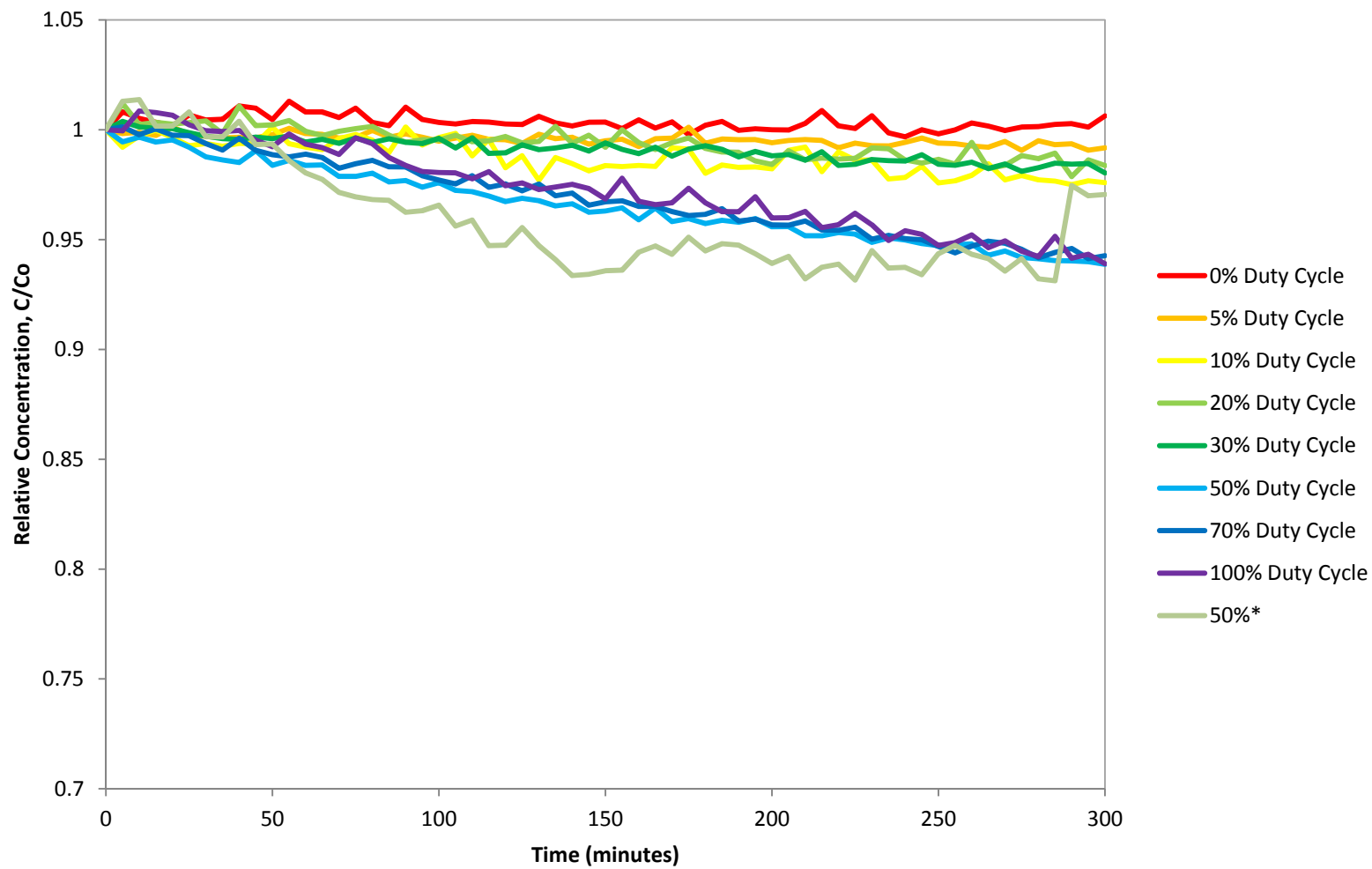


Figure 8: The Effect of Duty Cycle on the Removal of Tartrazine at pH 8



Figure 9 shows the effect of DC on the relative concentration of TAR at pH 9. The x-axis shows the time of the experiment; the y-axis shows the relative concentration ( $C/C_0$ ). The relative concentrations of TAR at the end of 300 minutes were recorded as follows: 0.99, 0.98, 0.98, 0.98, 0.94 - 0.97, 0.94, and 0.94 for DC levels of 5%, 10%, 20%, 30%, 50%, 50% experiment repeat, 70%, and 100%, respectively. Under this operating condition, the removal of TAR was similar for all DC levels. The top three TAR removal conditions were 50%, 70%, and 100% (the magnitude of each of these three concentrations was within  $C/C_0$  of .005); however, the same inversion observed during pH 8 experiments occurred, with the greatest removal of TAR occurring at the 50% DC (only 6% removal). Because this inversion behavior was observed for all experiment conditions except pH 6, the most likely explanation is that bicarbonate (the dominant carbonate species at pH values  $>6.35$ ) interacts with hydroxyl radicals resulting in less TAR removal. This is supported by the negative correlative relationship between bicarbonate concentration and TAR removal between pH 8 and pH 9 conditions observed in this study. For the pH 9 experiments, however, the differences in the first order rate constants between these levels were much less than for the pH 8 experiments. This data set showed further diminishment of performance of the AOP. Within the pH 9 condition, improvement between DCs was negative or marginal with DC increases. As with the pH 8 experiments, the positive correlative relationship between DC and first order rate constant does not apply. This additional decrease in performance relative to the pH 8 experiments supports the indication of a scavenging effect due to the increase in the concentration of  $\text{OH}^\cdot$ .



**Figure 9: The Effect of Duty Cycle on the Removal of Tartrazine at pH 9**

## 4.2 Statistical Analysis of First Order Rate Constants

Figure 10 shows the one-way ANOVA of  $k_s$  by nominal pH. The x-axis shows the pH of the experiment and the y-axis shows the first order rate constant. The ANOVA triangles indicate the specific pH level mean response, and the upper and lower 95% values, while the line through the entire plot shows the mean response for all data points. Mean response for the all points was  $3.91E-4 \text{ min}^{-1}$ , and the mean response within the pH levels were:  $6.22E-4 \text{ min}^{-1}$ ,  $4.18E-4 \text{ min}^{-1}$ ,  $3.54E-4 \text{ min}^{-1}$ ,  $1.74E-4 \text{ min}^{-1}$  for pH 6, 7, 8, and 9, respectively. The mean values of pH 6 and 7 outperformed the overall mean, while pH 8 and 9 did not exceed the overall mean. The data points at pH 9 were clustered, and became more widespread at lower pH levels. This is due to the fact that at pH 9, significantly less removal was observed. The reported p-value was 0.0471, which denotes the high confidence that pH is a statistically significant predictor of the first order rate constant.

Figure 11 shows one-way ANOVA of  $k_s$  by DC. The x-axis shows the DC of the experiment and the y-axis shows the first order rate constant. The ANOVA triangles indicate the specific DC level mean response, and the upper and lower 95% values, while the line through the entire plot shows the mean response for all data points. Mean response for the all points was  $3.91E-4 \text{ min}^{-1}$ , and the mean response within the DC levels were:  $5.4E-5 \text{ min}^{-1}$ ,  $1.22E-4 \text{ min}^{-1}$ ,  $1.95E-4 \text{ min}^{-1}$ ,  $2.85E-4 \text{ min}^{-1}$ ,  $4.88E-4 \text{ min}^{-1}$ ,  $6.51E-4 \text{ min}^{-1}$ , and  $6.89E-4 \text{ min}^{-1}$  for DCs 5%, 10%, 20%, 30%, 50%, 70%, and 100%, respectively. The mean values for DC levels 50%, 70%, and 100% exceeded the overall mean, while the DC levels 5%, 10%, 20%, and 30% did not exceed the overall mean. The

points were closely positioned in the lower DCs, and more spread out at higher DCs. The pH had much greater influence on the first order rate constant at higher DCs. The p-value was 0.0017, which indicates high level of confidence of statistical significance of DC as a predictor variable for the first order rate constant. This finding was consistent with other research findings with respect to degradation of dye using AOP (Duckworth, 2014; Mudimbi, 2015; Scott, 2015).

Tukey analysis (Appendix E) showed a statistically significant (with 95% confidence) distinction between pH groups as described as follows. Levels 6 and 7 were connected by group A, and Levels 7, 8, and 9 were connected by group B. Levels not connected by the same letter are significantly different. This means that responses between pH 6 and 7 were not significantly different, but pH 6 responses were significantly different from those of pH 8 and 9. Tukey analysis of the first order rate constant by DC (Appendix E) showed distinction between DC groups as follows. DC Levels 100%, 70%, and 50% were connected by group A; DC Levels 70%, 50%, and 30% are connected by group B; DC Levels 50%, 30%, 20%, and 10% were connected by group C; lastly, DC Levels 30%, 20%, 10%, and 5% were connected by group D. This means the 100% DC was significantly different than DCs of 30% and below, the 70% DC was significantly different than DCs of 20% and below, and that the 50% DC was significantly different than the 5% DC. This result is consistent with other AOP research conducted by Duckworth (2014), Mudimbi (2015), and Scott (2015).

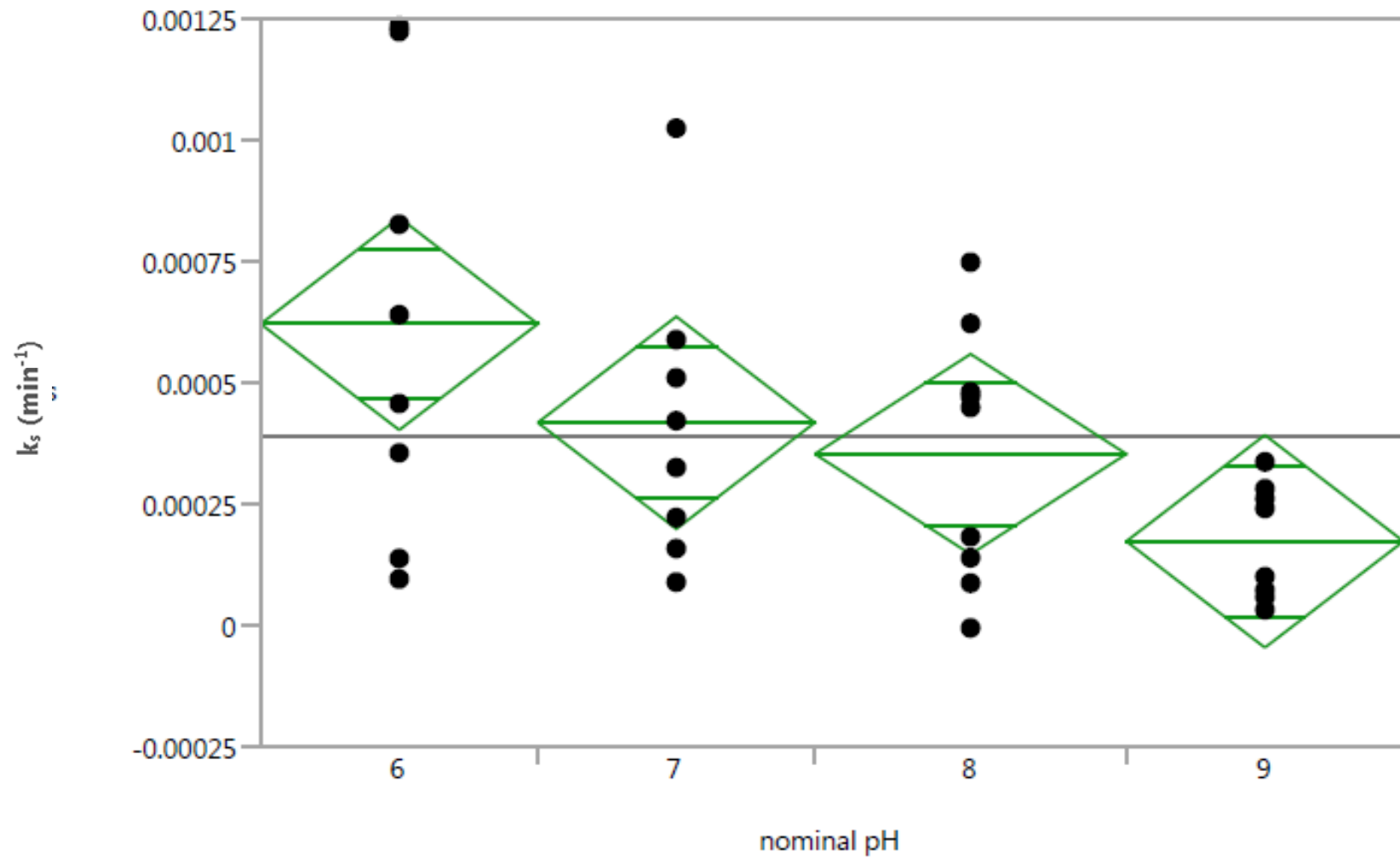


Figure 10: AOP ANOVA of  $k_s$  by nominal pH; p-value = 0.0471 means there is a statistically significant distinction between at least two pH groups. Each point represents one experiment. Within each pH category, experiments operated at DCs between 5% and 100% are represented.

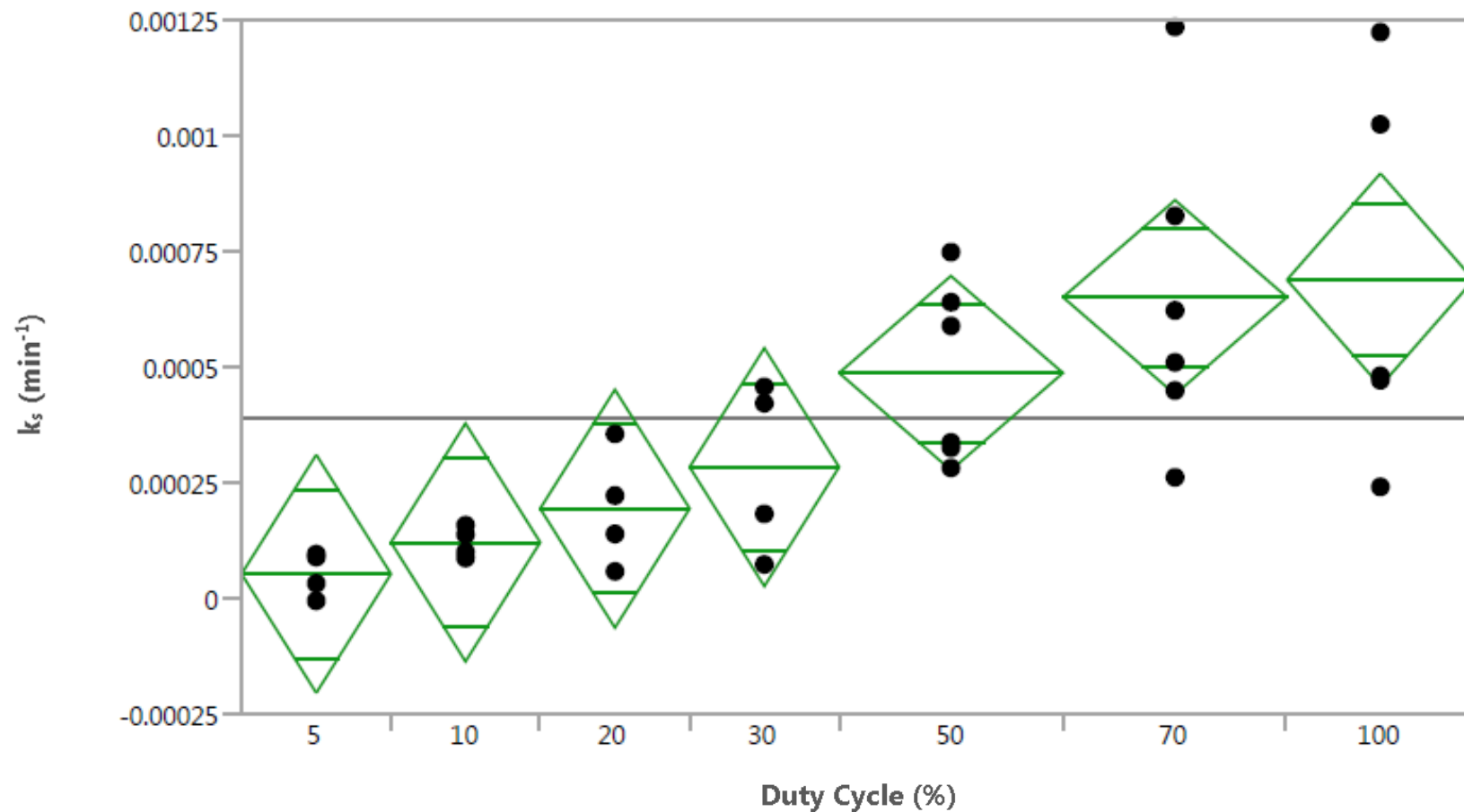


Figure 11: AOP ANOVA of  $k_s$  by Duty Cycle;  $p$ -value = 0.0017 means there is a statistically significant distinction between at least two DC groups. Each point represents one experiment. Within each DC category, experiments operated at nominal pH levels between 6 and 9 are represented.

Figure 12 shows the one-way ANOVA of  $k_{s,adj}$  ( $k_s/DC$ ) by nominal pH. The adjusted first order rate constant is the first order rate constant divided by the DC; thus, the  $k_{s,adj}(DC=100\%) = k_s(DC=100\%)$ . The x-axis shows the pH of the experiment and the y-axis shows the adjusted first order rate constant. The ANOVA triangles indicate the specific pH level mean response, and the upper and lower 95% values, while the line through the entire plot shows the mean response for all data points. Mean response for the all points was  $9.64E-4 \text{ min}^{-1}$ , and the mean responses within the pH levels were:  $1.511E-3 \text{ min}^{-1}$ ,  $1.19E-3 \text{ min}^{-1}$ ,  $6.79E-4 \text{ min}^{-1}$ ,  $5.13E-4 \text{ min}^{-1}$  for pH 6, 7, 8, and 9, respectively. The mean values of pH 6 and 7 surpassed the overall mean, while pH 8 and 9 were below the overall mean. The reported p-value was  $<0.0001$ , which denotes the high confidence that pH is a statistically significant predictor of the adjusted first order rate constant.

Figure 13 shows the one-way ANOVA of  $k_{s,adj}$  by DC. The x-axis shows the DC of the experiment and the y-axis shows the adjusted first order rate constant. The ANOVA triangles indicate the specific DC level mean response, and the upper and lower 95% values, while the line through the entire plot shows the mean response for all data points. The mean response for the all points was  $9.64E-4 \text{ min}^{-1}$ , and the mean responses within the DC levels were:  $1.088E-3 \text{ min}^{-1}$ ,  $1.223E-3 \text{ min}^{-1}$ ,  $9.75E-4 \text{ min}^{-1}$ ,  $9.49E-4 \text{ min}^{-1}$ ,  $9.75E-4 \text{ min}^{-1}$ ,  $9.30E-4 \text{ min}^{-1}$ , and  $6.89E-4 \text{ min}^{-1}$  for DC levels of 5%, 10%, 20%, 30%, 50%, 70%, and 100%, respectively. The mean values of DCs 5%, 10%, 20%, and 50% exceeded the overall mean, while DCs 30%, 70%, and 100% did not exceed the overall mean. The mean value for the 10% DC was the greatest out of each of the DCs, similar to the first order rate constant. This is a unique deviation, as Mudimbi (2015) and Scott

(2015) observed greatest values for the adjusted first order rate constant in the 5% DC. However, the trend of the entire study agrees with that observed by Mudimbi (2015) and Scott (2015). While the greatest values for this study were also from the 5% DC, the mean of the 10% group was greatest. The result was influenced by the pH 8 experiment at 5% DC, which did not produce a positive  $k_s$  (slightly negative). Theoretically, the  $k_s$  for this point should be 0, because there was no TAR removal observed. The Tukey analysis' of the adjusted first order rate constant by DC reported a p-value of 0.8827, which exhibits insufficient evidence to suggest that DC is a statistically significant predictor of the adjusted first order rate constant.

Tukey analysis of  $k_{s,adj}$  by pH and DC (Appendix E) shows a statistically significant (with 95% confidence) distinction between pH groups as described as follows. Levels 6 and 7 were connected by group A, Levels 7, and 8 were connected by group B, and Levels 8 and 9 were connected by group C. Tukey analysis shows that levels not connected by the same letter are significantly different. This means that responses for pH 6 and 7 were not significantly different, but pH 6 responses were significantly different from those of pH 8 and 9. Tukey analysis of the adjusted first order rate constant by DC (Appendix E) showed no distinction between DC groups, as all DC levels are connected by the same letter.



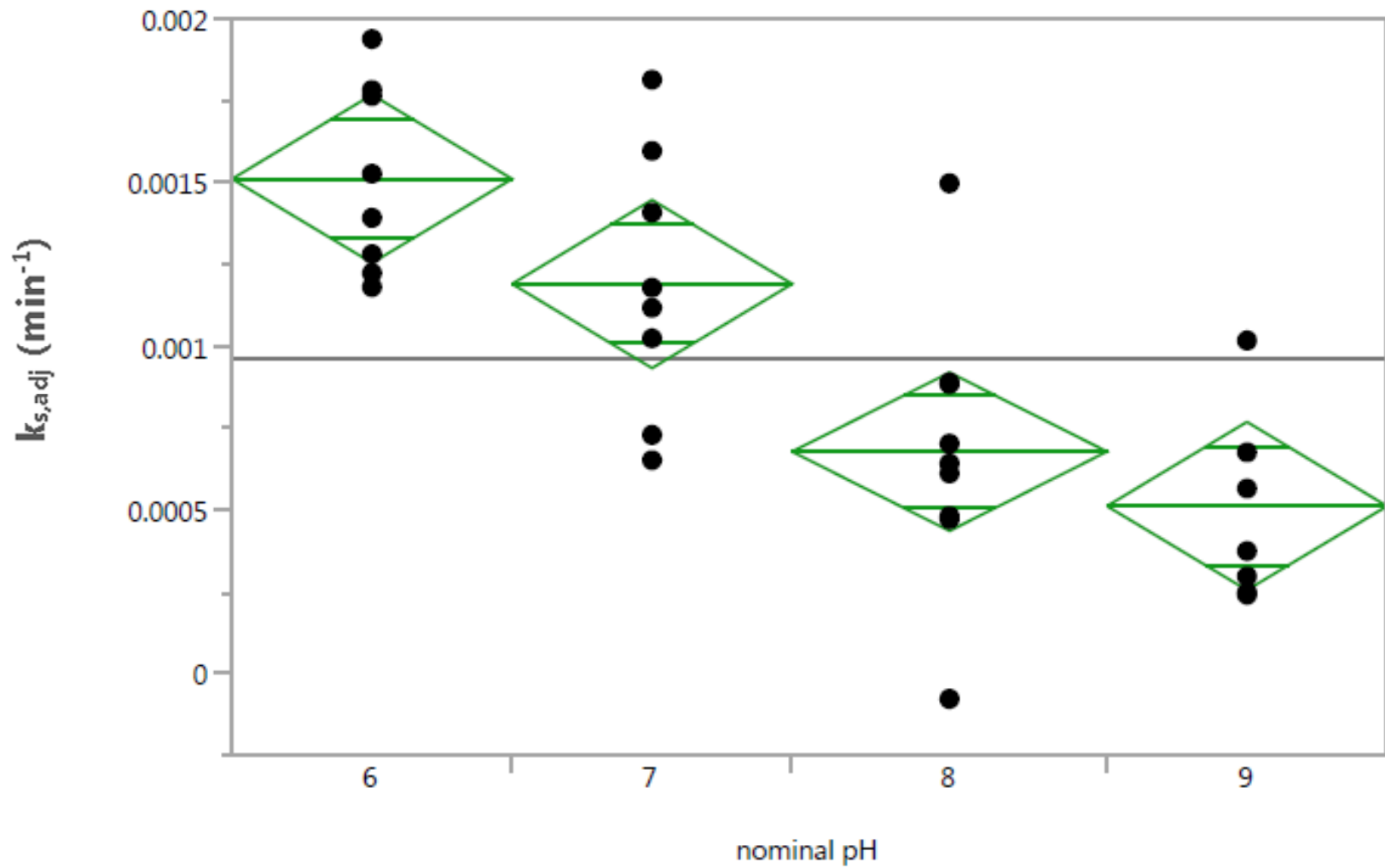


Figure 12: ANOVA of AOP  $k_{s,adj}$  by Nominal pH; p-value < 0.0001 means there is a statistically significant distinction between at least two pH groups. Each point represents one experiment. Within each pH category, experiments operated at DCs between 5% and 100% are represented.

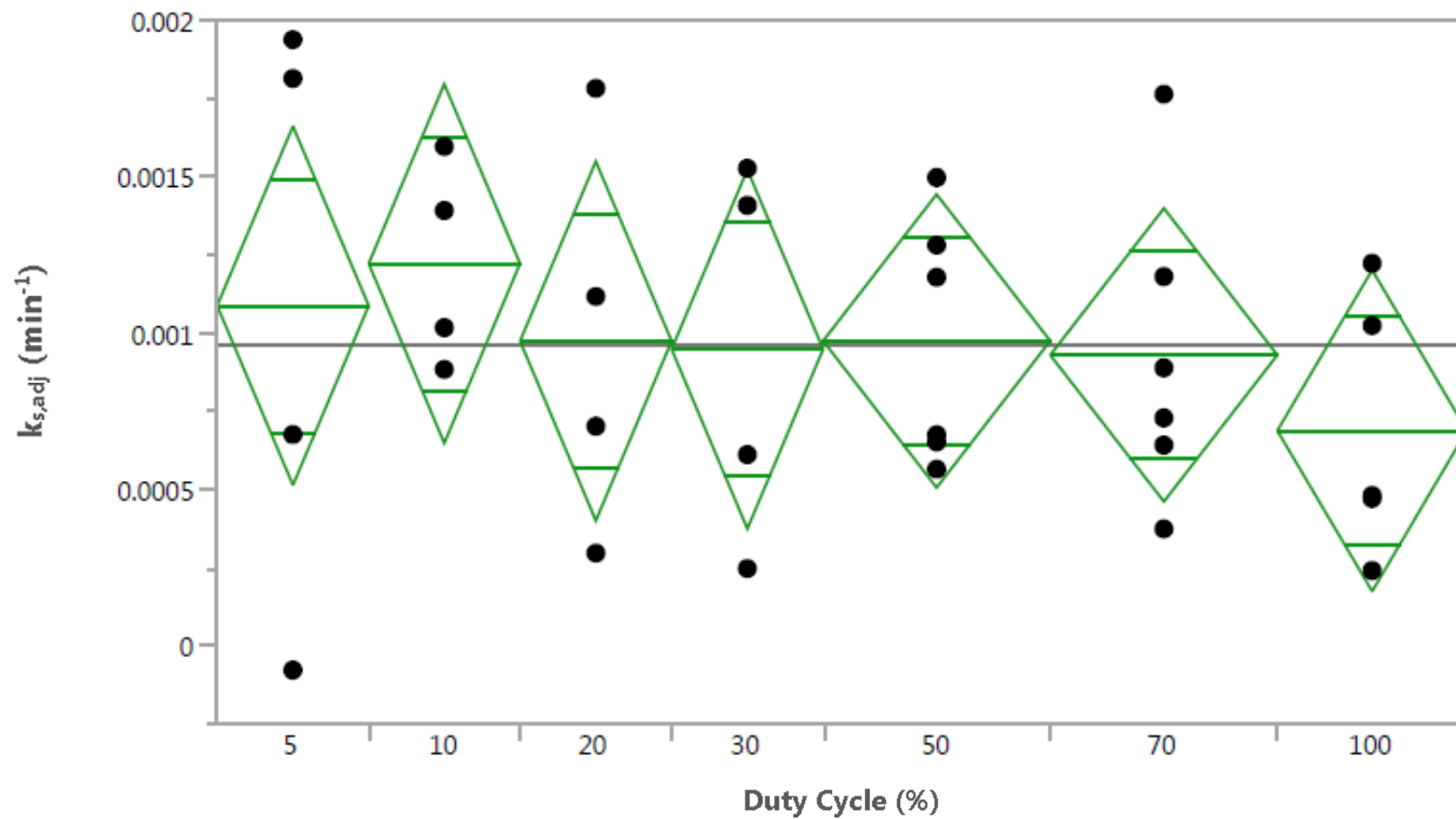


Figure 13: ANOVA of AOP  $k_{s,adj}$  by Nominal Duty Cycle; p-value = 0.8827 means there is insufficient evidence to suggest a statistically significant distinction between at least two DC groups. Each point represents one experiment. Within each DC category, experiments operated at nominal pH levels between 6 and 9 are represented. This result is anticipated due to the definition of the adjusted first order rate constant.

Using the above information, a linear regression analysis was conducted using primary dependent variables pH and DC to predict  $k_s$  only, as  $k_{s,adj}$  can be calculated given  $k_s$  and DC. Points that were excluded from the model were H<sub>2</sub>O<sub>2</sub> control and the 0% DC experiments, but their purpose was not to predict removal, but rather to establish that the UV radiation alone could not account for significant removal of TAR, or that adding hydrogen peroxide to the solution at a given pH level could not account for significant removal of TAR. The other exclusion was the experiment dated 29 May 15. This point was excluded because the pH of the solution for the experiment fell outside the operating procedures set for this study, which caused unacceptable amount of influence as detected by the statistical parameter Cook's D. The resulting model upheld the three assumptions for linear regression models: independence (Durbin Watson Test), normally distributed residuals (Shapiro-Wilks Test), and constant variance (Breusch-Pagan Test). The adjusted R<sup>2</sup> for this model was .85, all Variance Inflation Factor (VIF) scores fell below 2.0, no significant outliers or overly influential points were detected (by studentized residuals, and Cooks D influence overlay plots), with one exception. This was the point for the experiment dated 30 July 15, with operating conditions of pH 7 and 100% DC. This point was overly influential, but did not cause failure of any of the three assumptions tests, and the model incorporated a term specifically to deal this this singular point. The model's mean predictive error was 7.93E-5 min<sup>-1</sup> with standard deviation of 6.34E-5 min<sup>-1</sup>. The Median error was 6.43E-5 min<sup>-1</sup>. The maximum error was 2.20E-4 min<sup>-1</sup>.

The high APE scores for this model resulted from the fact that the model does not incorporate terms to specifically deal with pH 9 at duty cycles less than 30%, and at pH 8 at low duty cycles. These terms, however, do not represent operating conditions of interest due to the low first order rate constants. See the regression model (Equation 11) and assumption tests in Appendix F. Figure 14 shows the comparison between the true apparent first order rate constant and the AOP Regression models predicted value. The x-axis shows the experiment number and the y-axis shows the first order rate constant. Figure 15 shows the relationship between the true (observed) first order rate constant (x-axis) and that predicted by the regression model (y-axis). The plot shows a linear trend about tightly clustered points, which is indicative of the strong adjusted  $R^2$  for the model.

**Equation 11: AOP Regression Model**

$$\begin{aligned}
 Y_{AOP} = & (7.8989E - 5) - 0.00017(pH9) + 8.9044E - 5(pH7) + 0.0002688(pH6) \\
 & + 0.0001608(DC 30) + 0.0003848(DC 50) + 0.0004662(DC 70) \\
 & + 0.0006139(DC 100) \\
 & + 0.0004428(pH6 - 0.24242)(DC 70 - 0.18182) \\
 & + 0.0006832(pH6 - 0.24242)(DC 100 - 0.15152) \\
 & + 0.0005658(pH7 - 0.24242)(DC 100 - 0.15152)
 \end{aligned}$$

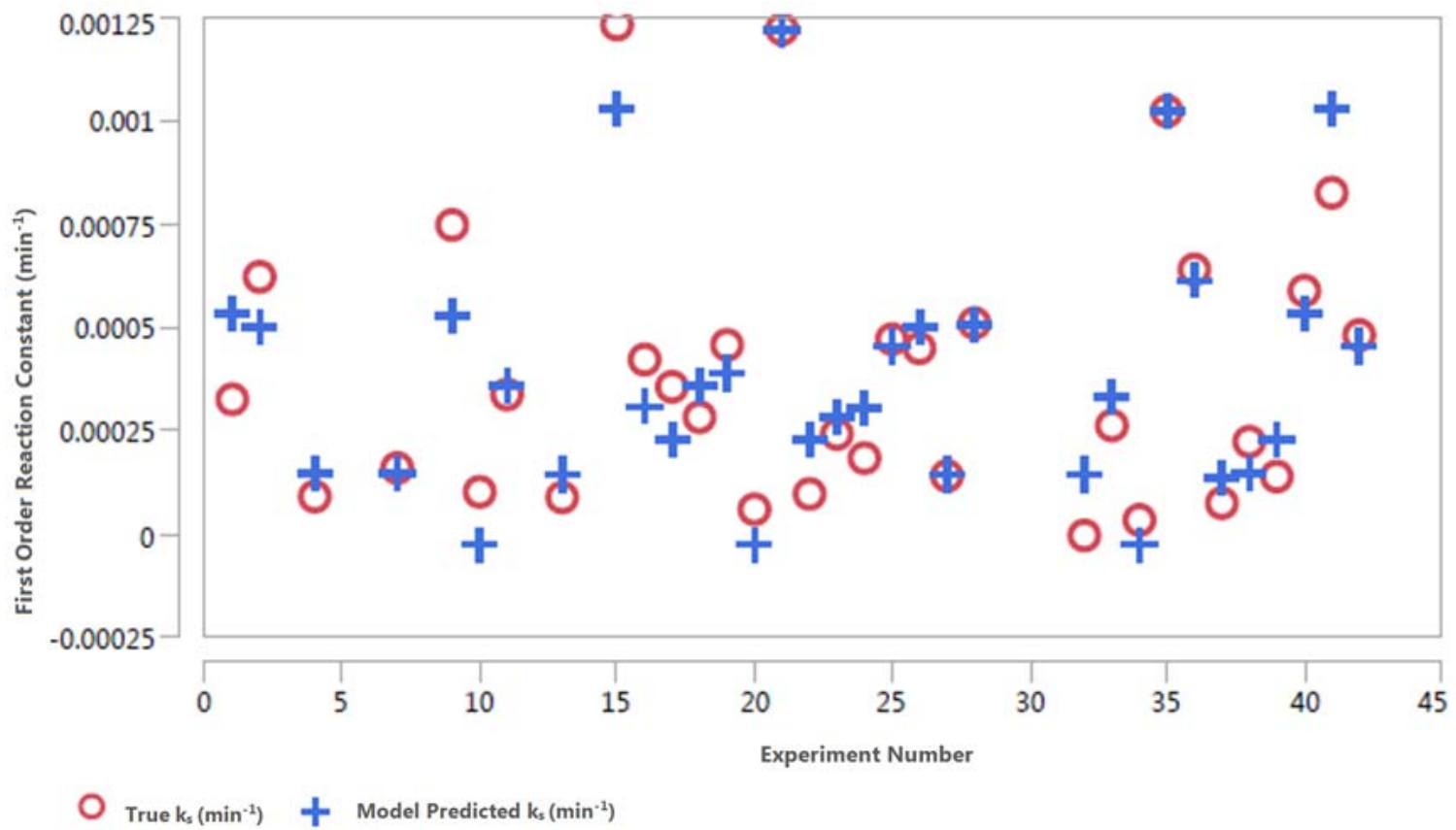


Figure 14: AOP Regression Model Predicted vs. Actual Response

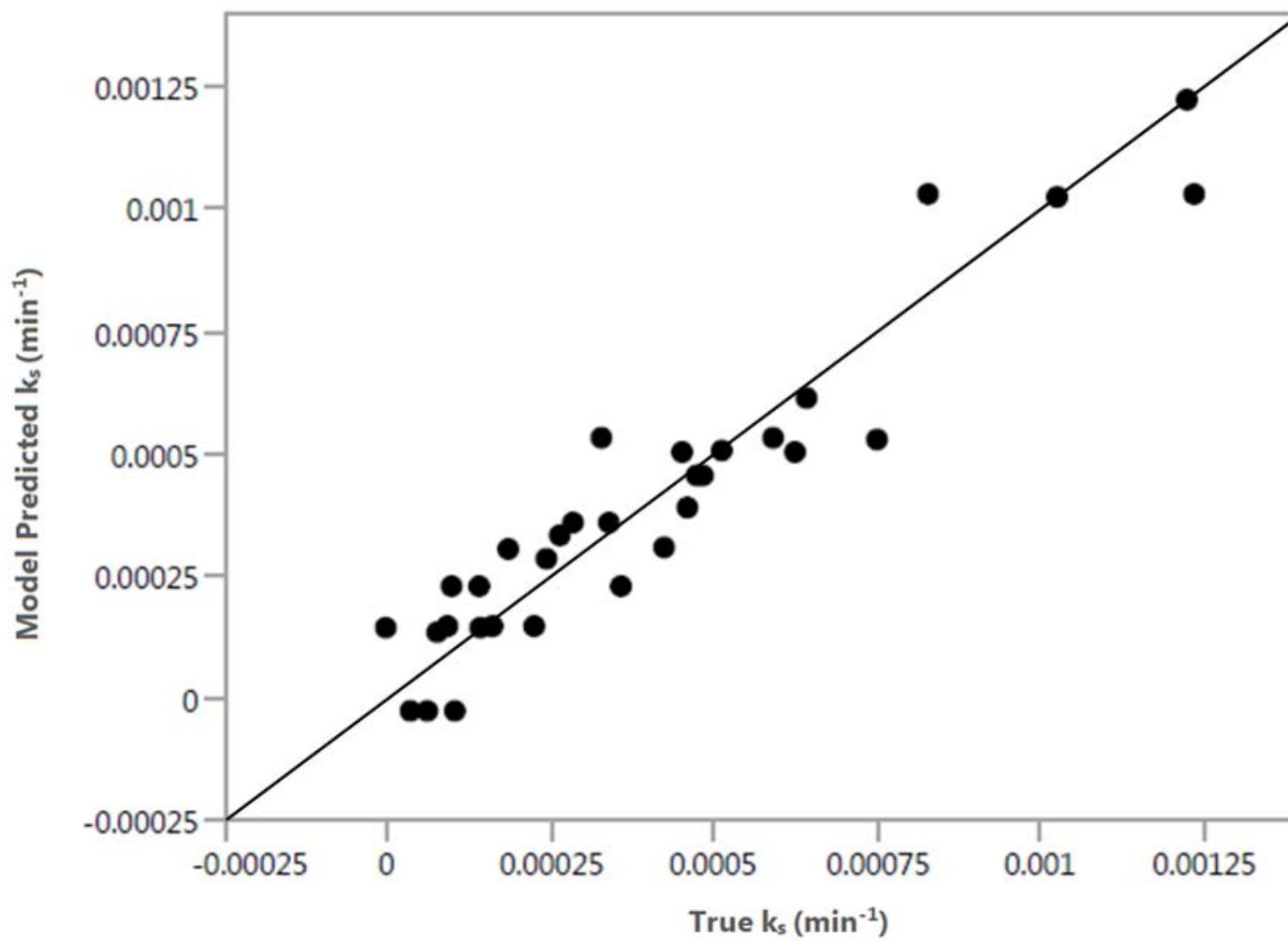


Figure 15: True vs Predicted First Order Rate Constant

### 4.3 The Effect of pH and Duty Cycle on the AOP Byproduct Profile

#### 4.3.1 Chromatographic Contrast Angle Analysis

The purpose of this section is to determine the impact of pH and/or DC on the AOP byproduct profile. To establish the relationships between the pH levels, CCAs were calculated between the 0% DC experiments among the different pH levels (all 6 unique pairings). Since each experiment had two chromatographs (from positive and negative ionization), a total of 12 calculations were made (Figure 16, Figure 17). In similar fashion, CCAs were calculated between H<sub>2</sub>O<sub>2</sub> control experiments for both the positive and the negative runs (Figure 18, Figure 19). Comparisons made with pH 7 tended to produce larger CCAs, see summaries in Appendix L.

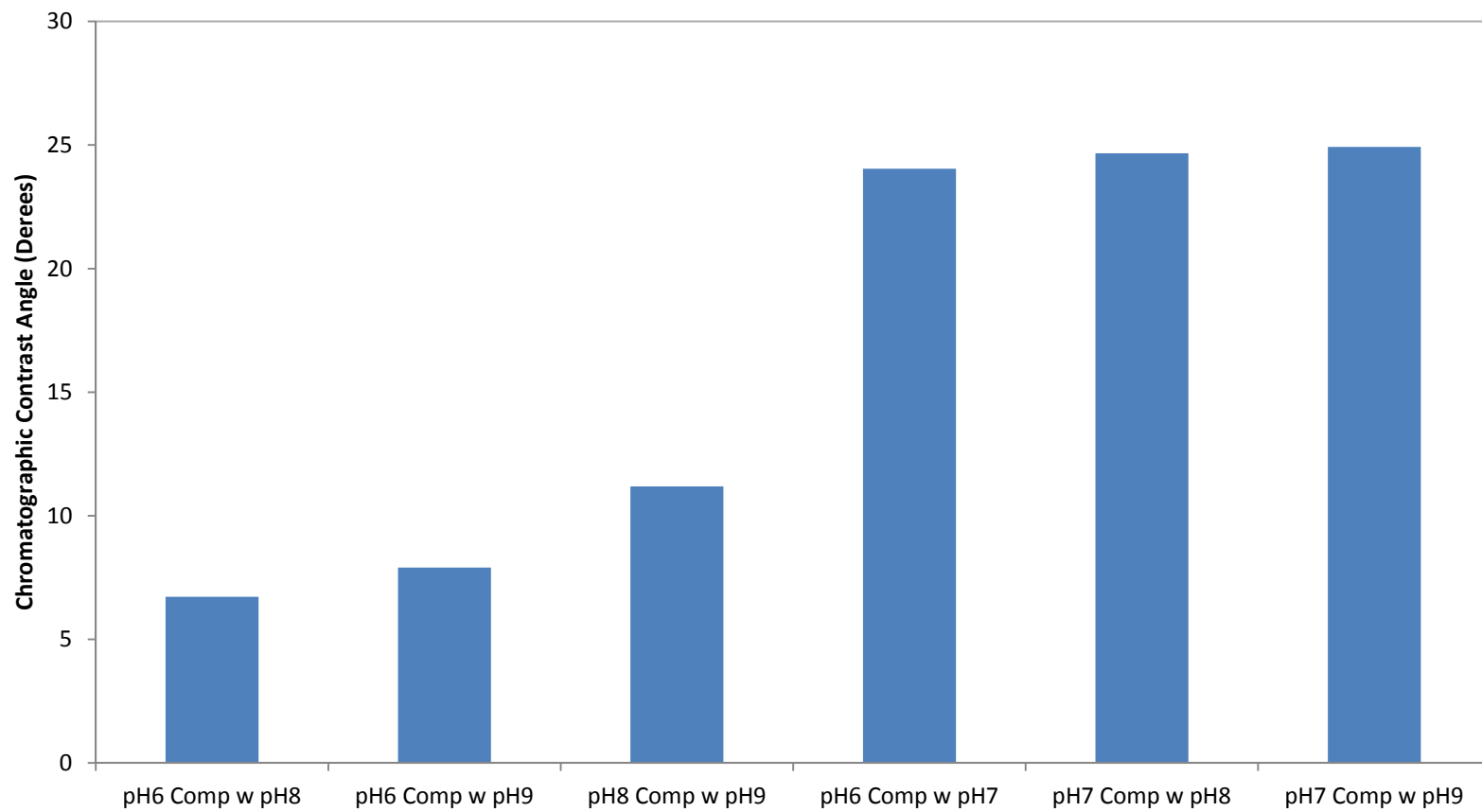
##### 4.3.1.1 The Effect of pH on Chromatographic Contrast Angles

Figure 16 shows the effect of pH on the 0% DC CCAs under positive ionization. The x-axis shows the pH labels for the 2 chromatographs being compared, and the y-axis shows the values of the CCAs. The CCA value for the pH 7/9 comparison was 24.9°, the highest value observed in this study. The second and third highest values were 24.7°, and 24.0° from the pH 7/8 and pH 6/7 comparisons respectively. These data mean that the byproduct profile observed at pH 7 was most different from those observed at pH 6, 8, and 9 at 0% DC under positive ionization. Smaller values were observed at comparisons pH 6/8 (6.7°), pH 6/9 (7.9°), and pH 8/9 (11.2°).

The chromatographs of the positive run appear to have three main peaks; hereafter referred to as peaks 1-3 from left to right. In comparison pH 6/8, there are no shifts, the magnitudes of the first two peaks are nearly identical, and the third peak is slightly

smaller in the pH 8 chromatogram. This explains why the CCA was low for this comparison. Similar, slight deviations and no shifts were observed for the other low CCA comparisons. However, the larger CCA comparisons contained greater deviations. The pH 6/7 comparison peak 2 greatly increased from pH 6 to pH 7. Also, slight increases in peaks 1 and 3 were observed. The comparison of pH 7/8 also produced large distinction, due to the magnitude of the pH 7 chromatograms peak 2, but no shifts were observed. Similarly, the peak 2 of the chromatogram of pH 9 was dwarfed by comparison to pH 7. This suggests that without UV radiation, pH 7 influences the byproduct profile more so than the other pH conditions.

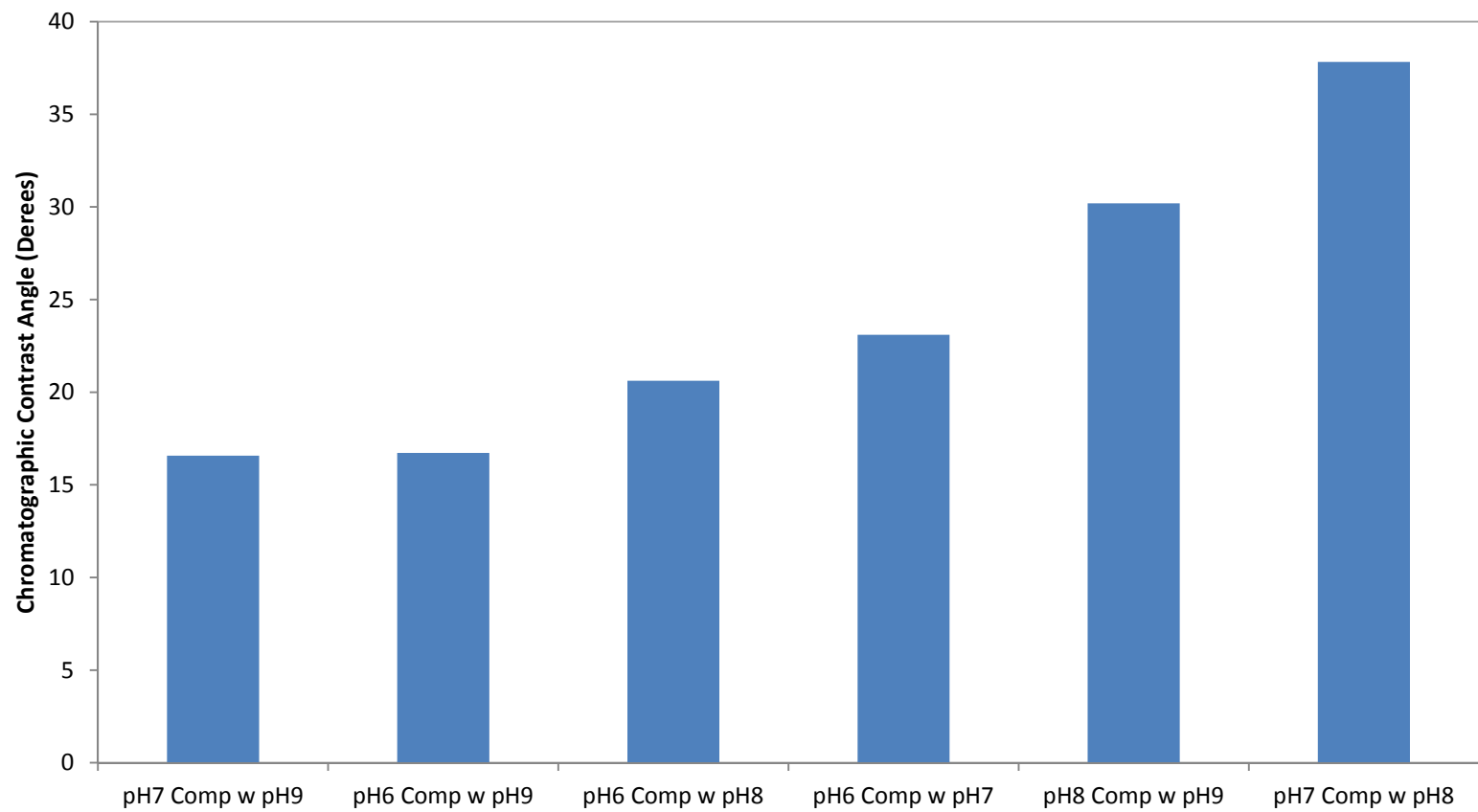




**Figure 16: The Effect of pH on Chromatographic Contrast Angles for 0% DC under Positive Ionization**

Figure 17 shows the effect of pH on the 0% DC CCAs under negative ionization. The x-axis shows the pH labels for the 2 chromatograms being compared, and the y-axis shows the values of the CCAs. The CCA value for the pH 7/8 comparison was 37.8°, the highest value observed in this study. The second and third highest values were 30.2°, and 23.1° from the pH 8/9 and pH 6/7 comparisons respectively. The smaller angles produced were 20.6° (pH 6/8), 16.7° (pH 6/9), and 16.6° (pH 7/9). The similarities between chromatograms were less than that of the positive ionization condition.

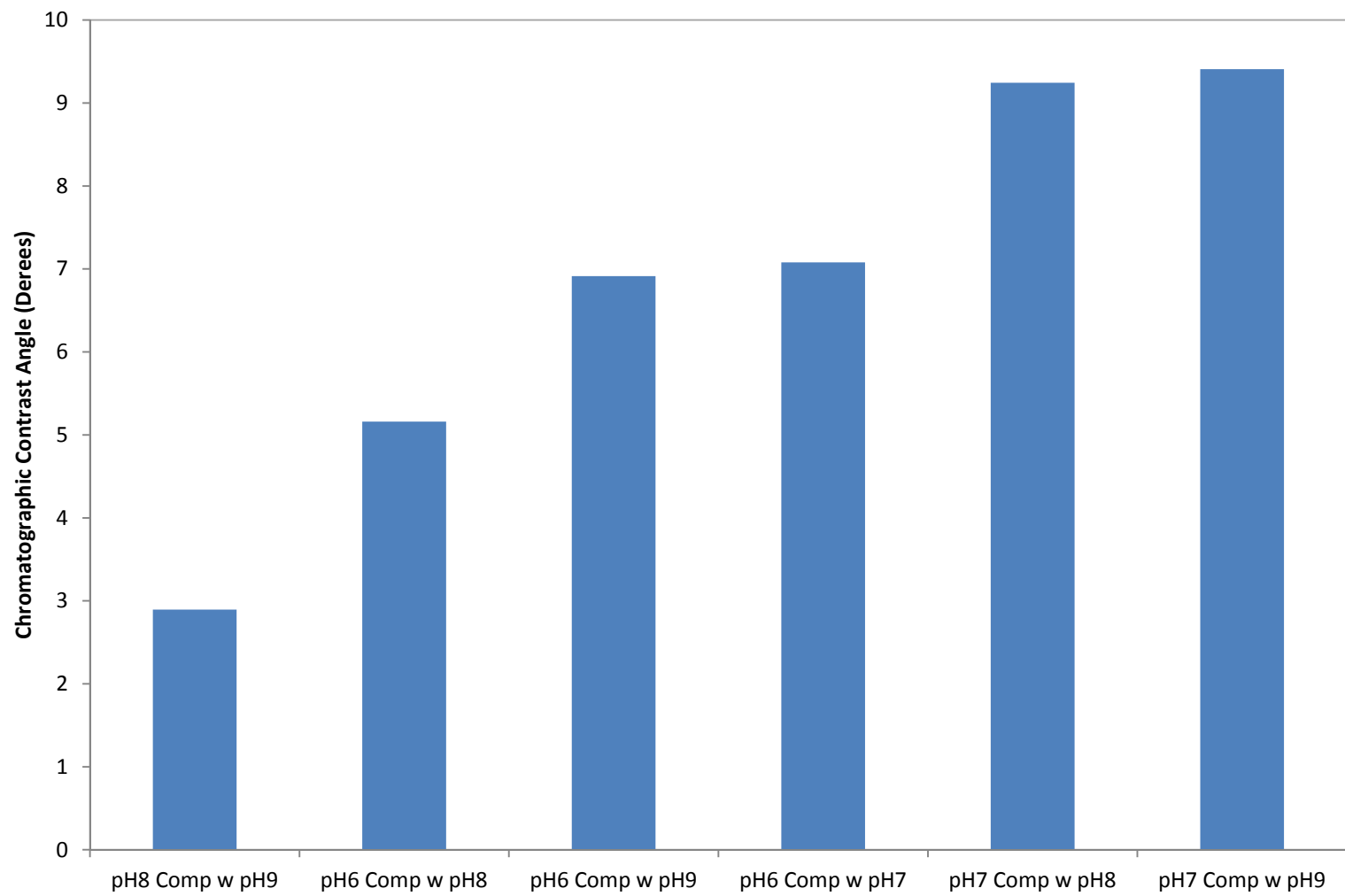
The associated chromatographs did not follow the pattern observed for the positive ionization byproduct profile. The largest peak 1 was evenly matched for pH 7 and pH 9; pH 7 had the largest peak 2; and pH 8 had the largest peak 3. Noticeable shifts occurred in peak 1 between pH 6/9, 7/8, and 8/9. This suggests that pH impacts the byproduct profile under negative ionization in the presence of H<sub>2</sub>O<sub>2</sub> without UV radiation.



**Figure 17: The Effect of pH on Chromatographic Contrast Angles for 0% DC under Negative Ionization**

Figure 18 shows the effect of pH on the H<sub>2</sub>O<sub>2</sub> control CCAs under positive ionization. The x-axis shows the pH labels for the 2 chromatograms being compared, and the y-axis shows the values of the CCAs. This chart is similar to Figure 16 in that the largest CCA values were created in comparisons made with pH 7, and the order of comparisons from largest to smallest was similar. The values in this chart were different from Figure 16 with respect to the magnitude of the (positive) CCAs of the H<sub>2</sub>O<sub>2</sub> control experiments, which were much less than that of the 0% DC (positive) CCAs. The CCA value for the pH 7/9 comparison was 9.4°, the highest value observed in this study. The second and third highest values were 9.2°, and 7.1° from the pH 7/8 and pH 6/7 comparisons respectively. These data mean that the byproduct profile observed at pH 7 was most different from those observed at pH 6, 8, and 9. Smaller values were observed at comparisons pH 8/9 (2.9°), pH 6/8 (5.2°), and pH 6/9 (6.9°).

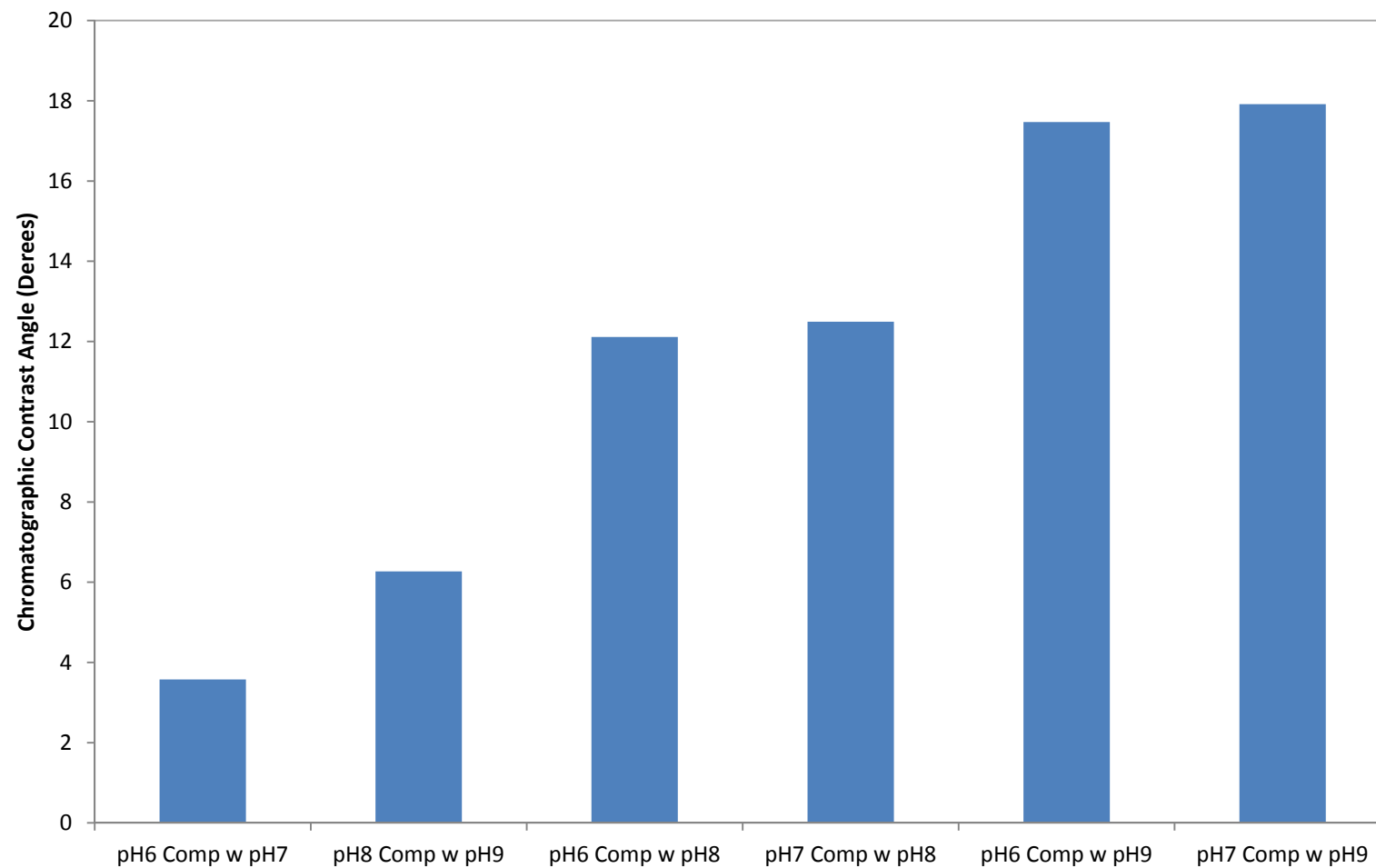
In contrast from the 0% DC chromatograms, in which only pH 7 had a substantial peak 2, the H<sub>2</sub>O<sub>2</sub> control chromatograms of pH 7 are the only ones which do not have a peak 2. The only other main difference between the pH conditions is slight changes in magnitudes of the three peaks. No considerable shifts were observed. This is why the CCAs are considerably lower for this figure.



**Figure 18: The Effect of pH on Chromatographic Contrast Angles for H<sub>2</sub>O<sub>2</sub> Controls under Positive Ionization**

Figure 19 shows the effect of pH on the H<sub>2</sub>O<sub>2</sub> control CCAs under negative ionization. The x-axis shows the pH labels for the 2 chromatograms being compared, and the y-axis shows the values of the CCAs. The CCA value for the pH 7/9 comparison was 17.9°, the highest value observed in this study. The second and third highest values were 17.5°, and 12.5° from the pH 6/9 and pH 7/8 comparisons respectively. Smaller values were observed at comparisons pH 6/7 (3.6°), pH 8/9 (6.3°), and pH 6/8 (12.1°).

The associated chromatograms were very similar. The trend was a large peak 1, and miniscule peaks 2 and 3. Slight peak 1 shifts were observed for pH comparisons 6/8, 6/9, 7/8, and 7/9. Other than these reasons, the CCA's were driven by distinctions in the magnitudes of the respective pH comparisons peaks 1. This means that without peroxide and under UV radiation, peak 1 is most affected by pH.



**Figure 19: The Effect of pH on Chromatographic Contrast Angles for H<sub>2</sub>O<sub>2</sub> Controls under Negative Ionization**

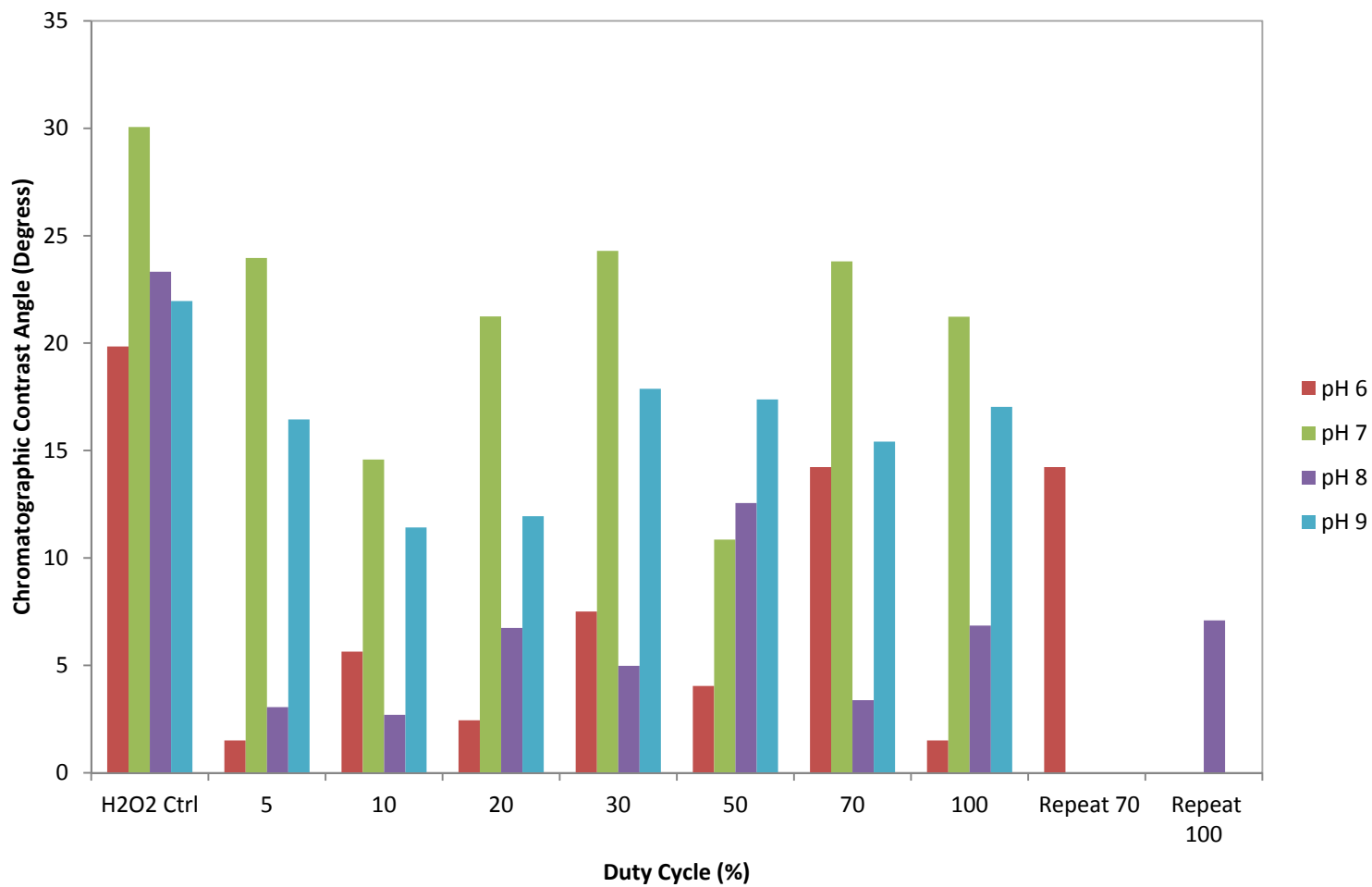
#### 4.3.1.2 The Effect of Duty Cycle on Chromatographic Contrast Angles

Finally, the CCAs were calculated for every experiment relative to the 0% DC of the corresponding pH level for both the positive and negative run (Figure 20, Figure 21).

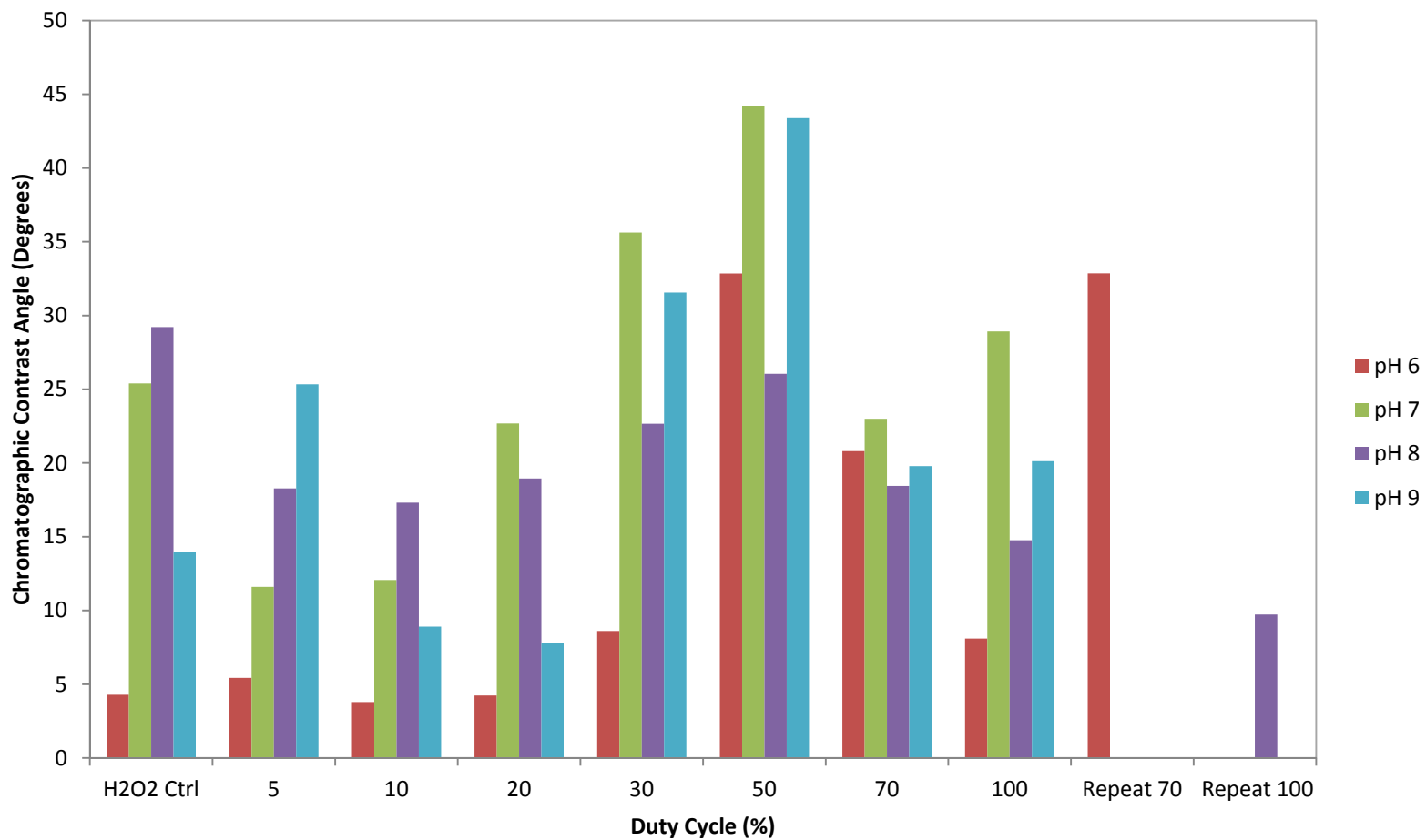
Figure 20 shows the effect of DCs on CCA for the positive ionization. The x-axis shows the DC and the y-axis shows the contrast angle in degrees. There were few CCAs under 5°, all of which were at pH 6, for DCs 5%, 20%, and 100%. The CCAs did not correlate directly to TAR removal, otherwise a larger CCA would have been observed between pH 6 DCs 0% and 100%. Also, pH 7 was associated with high CCA values within each DC category, ranging from 10° to 30°.

Figure 21 shows the effect of DC on the CCA in the negative ionization condition. The x-axis shows the DC and the y-axis shows the contrast angle in degrees. There were only three comparisons in which the CCA was less than 5°: (all at pH 6) H<sub>2</sub>O<sub>2</sub> Ctrl, 10%, and 20% DC. This reiterates the point that the CCA did not directly relate to the removal of TAR. The condition pH 7 consistently created relatively large CCAs (ranging from 11° to 44°), but wasn't always the greatest angle within a DC category. These exceptions were pH 8 during the H<sub>2</sub>O<sub>2</sub> control comparison, as well as pH 9 during the 5% DC.





**Figure 20: The Effect of Duty Cycle on Chromatographic Contrast Angles under Positive Ionization. Each chromatogram was compared to the 0% DC chromatogram of the respective pH level.**



**Figure 21: The Effect of Duty Cycle on Contrast Angles under Negative Ionization. Each chromatogram was compared to the 0% DC chromatogram of the respective pH level.**

#### 4.3.1.3 Statistical Evaluation of the effect of pH and Duty Cycle on CCA

In consideration of both positive and negative CCAs, pH level 7 was associated with larger CCAs. In addition, DCs 30%, 50%, and 70% appeared to create larger CCAs for the negative run. One-Way ANOVA and Tukey analyses were conducted for both positive and negative CCAs. See summary statistics, ANOVA, LS Means diagrams (positive and negative), and Tukey (positive and negative) reports in Appendix M.

Figure 22 shows the one-way ANOVA of the positive CCA by DC. The x-axis shows the DC, and the y axis shows the positive CCA in degrees. The triangles depict the mean, upper 95%, and lower 95% for each DC category. The line through the middle of the figure shows the mean of all responses in the data set, which is 11.5°. The means for each DC are 11.2°, 8.6°, 10.6°, 13.7°, 11.2°, 14.2°, and 10.7° for DCs 5%, 10%, 20%, 30%, 50%, 70%, and 100%, respectively. The p-value was 0.9519, which demonstrates insufficient evidence to suggest that DC alone cannot be used as a statistically significant predictor variable for the positive CCA.

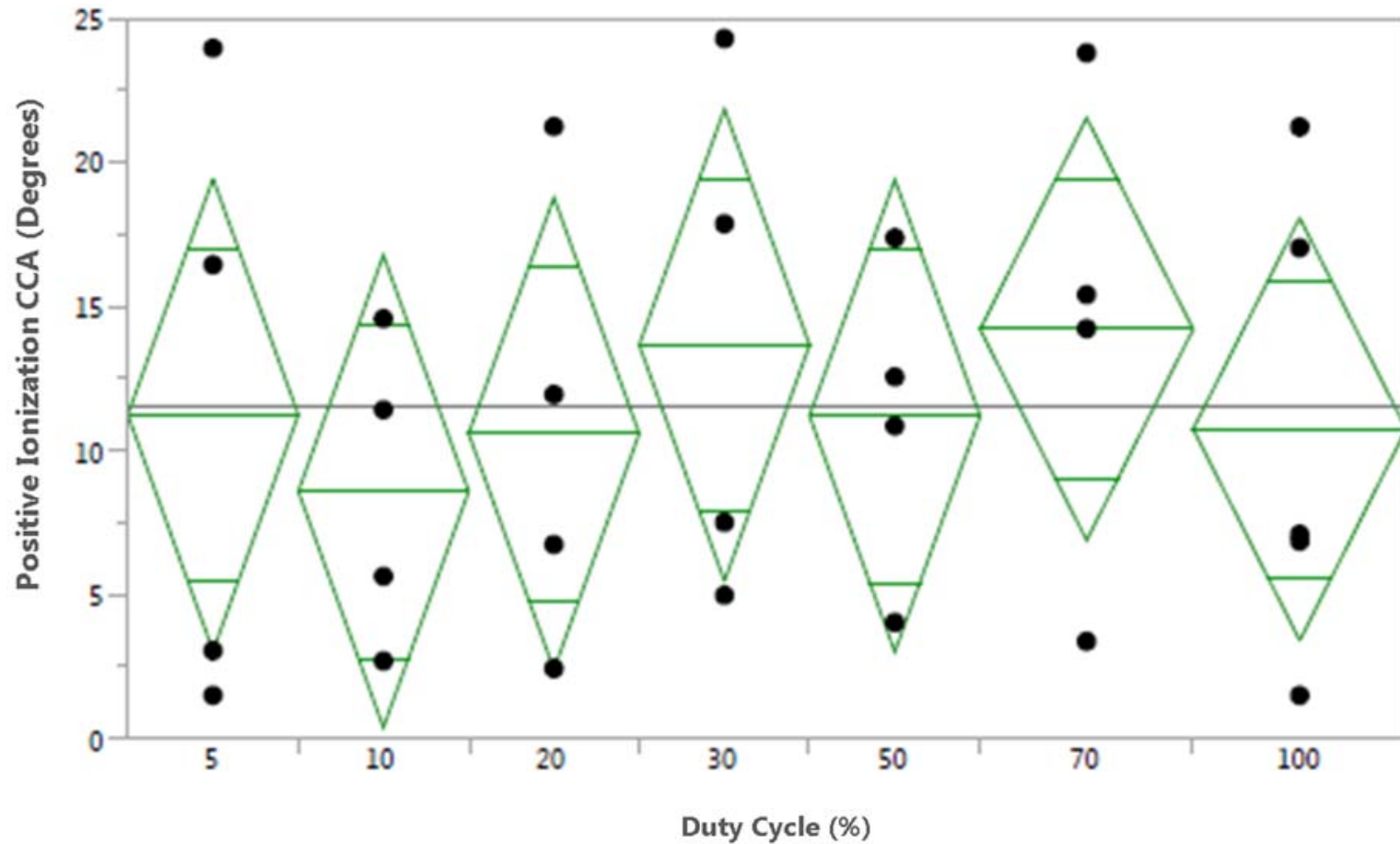


Figure 22: ANOVA of Positive Ionization CCA by Duty Cycle; p-value = 0.9519 indicates insufficient evidence to suggest that DC is a statistically significant predictor of the Positive Ionization CCA. Each point represents one experiment. Within each DC category, experiments operated at nominal pH levels between 6 and 9 are represented.

Figure 23 shows the one-way ANOVA of the positive CCA by pH level. The x-axis shows the nominal pH, and the y axis shows the positive CCA in degrees. The triangles depict the mean, upper 95%, and lower 95% for each pH category. The line through the middle of the figure shows the mean of all responses in the data set (which is 11.5°). The means for the pH levels are 6.4°, 20.0°, 5.9°, and 15.4° for pH levels 6, 7, 8, and 9, respectively. The pH 9 was tightly clustered, which may be attributable to the fact that pH 9 produced the least amount of variance with respect to the first order rate constant, and thus, would have less effect on changing the byproduct profile. The p-value was less than 0.0001, which demonstrated that pH is a statistically significant predictor variable for the positive CCA.

Tukey analysis (Appendix M) of the positive CCA by pH (p-value = 0.00004), DC (p-value = .00075), and the interaction of pH and DC (p-value = .00097) produced strong indication that pH and DCs together were strong predictors of CCA. DCs were grouped into the following letter categories: 70% and 30% were group A, 100%, 5%, and 50% were group B, 5%, 50%, and 20% were group C, and 10% was group D. Levels not connected by the same letter are significantly different. Each of the pH levels were grouped into separate letter groups. This means that several DCs were unique, and that each pH level was statistically distinct.

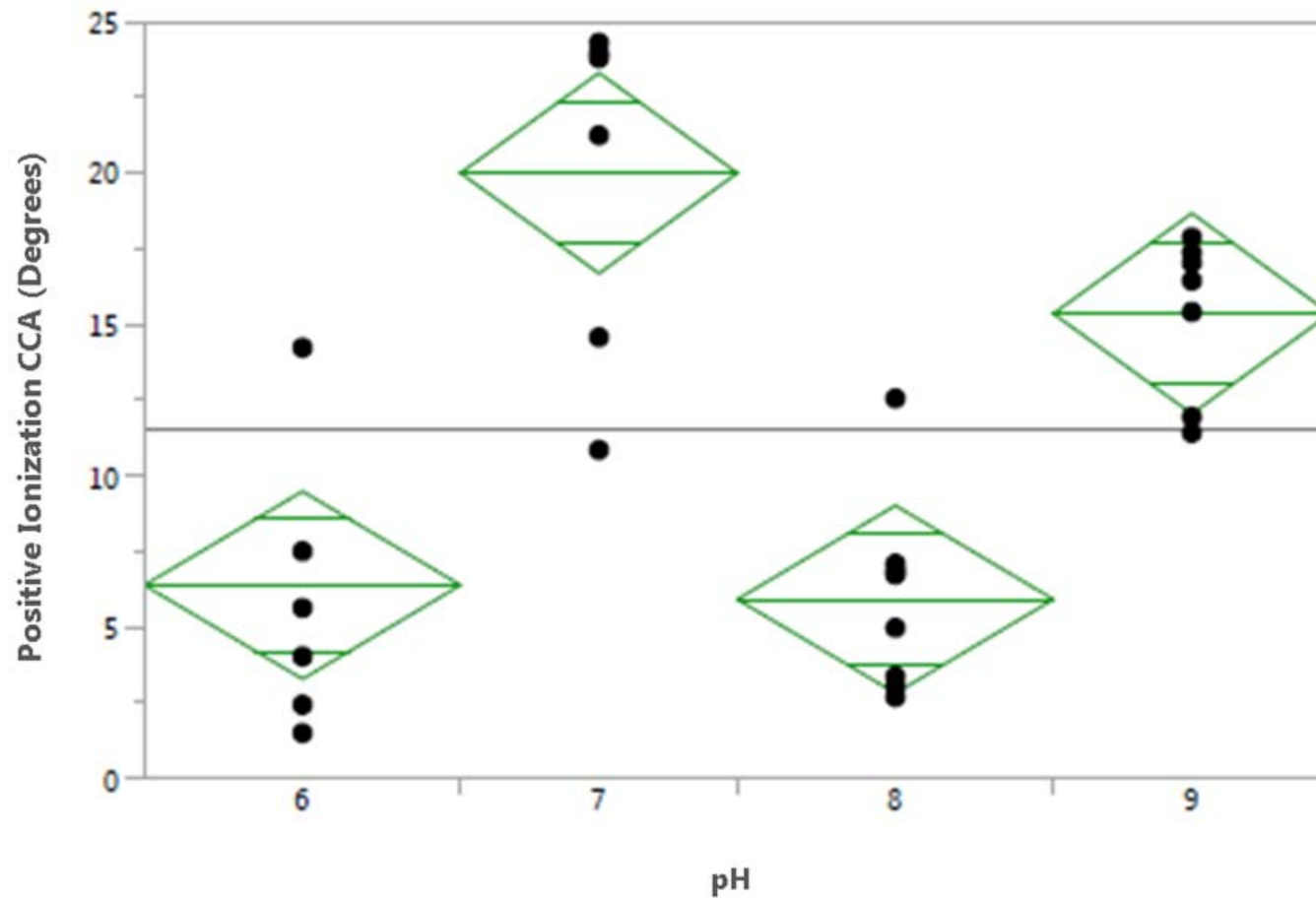


Figure 23: ANOVA of Positive Ionization CCA by pH; p-value = 0.0001 indicates there is a statistically significant distinction between at least two pH groups. Each point represents one experiment. Within each pH category, experiments operated at DCs between 5% and 100% are represented.

Figure 24 shows the one-way ANOVA of the negative CCA by DC. The x-axis shows the DC, and the y axis shows the negative CCA in degrees. The triangles depict the mean, upper 95%, and lower 95% for each DC category. The line through the middle of the figure shows the mean of all responses in the data set (which is 19.9°). The means for the DCs were 15.2°, 10.5°, 13.4°, 24.6°, 36.6°, 23.0°, and 16.3° for DC levels 5%, 10%, 20%, 30%, 50%, 70%, and 100%, respectively. The p-value was 0.0035, which demonstrated that DC is a statistically significant predictor variable for the negative CCA.

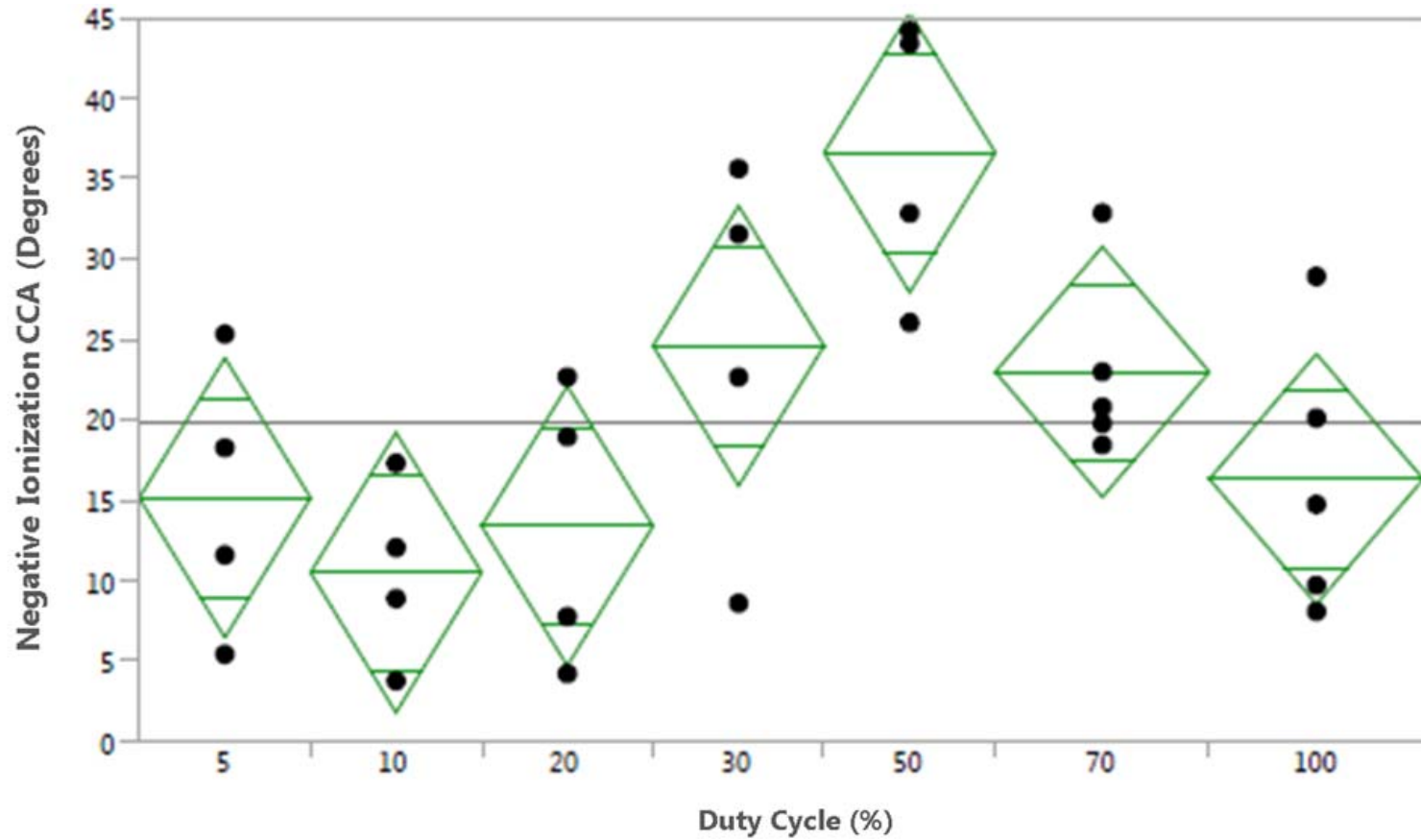


Figure 24: ANOVA of Negative Ionization CCA by Duty Cycle; p-value =0.0035 indicates statistically significant distinction between at least two DC groups. Each point represents one experiment. Within each DC category, experiments operated at pH levels between 6 and 9 are represented.



Figure 25 shows the one-way ANOVA of the negative CCA by pH level. The x-axis shows the nominal pH, and the y axis shows the negative CCA in degrees. The triangles depict the mean, upper 95%, and lower 95% for each pH category. The line through the middle of the figure shows the mean of all responses in the data set (which is 19.9°). The means for the pH levels were 14.6°, 25.4°, 18.3°, and 22.4° for pH levels 6, 7, 8, and 9, respectively. The p-value was 0.2544, which demonstrates the insufficient evidence to suggest that pH alone is a statistically significant predictor variable for the negative CCA.

The Tukey analysis of the negative CCA (Appendix M) by pH (p-value = .04282) and DC (p-value = .00105) produced significant evidence that pH and DC together were strong predictors. The DC groups were A: 50%, 30%, and 70%, and B: 30%, 70%, 100%, 5%, 20%, and 10%. This means that 50% is significantly different than 100%, 5%, 20%, and 10%, but the 30% and 70% could belong to either group. The pH groups were A: 7, 9, and 8, and B: 9, 8, and 6. This means that pH 7 and 6 were statistically different, but pH 8 and 9 could belong to either group.

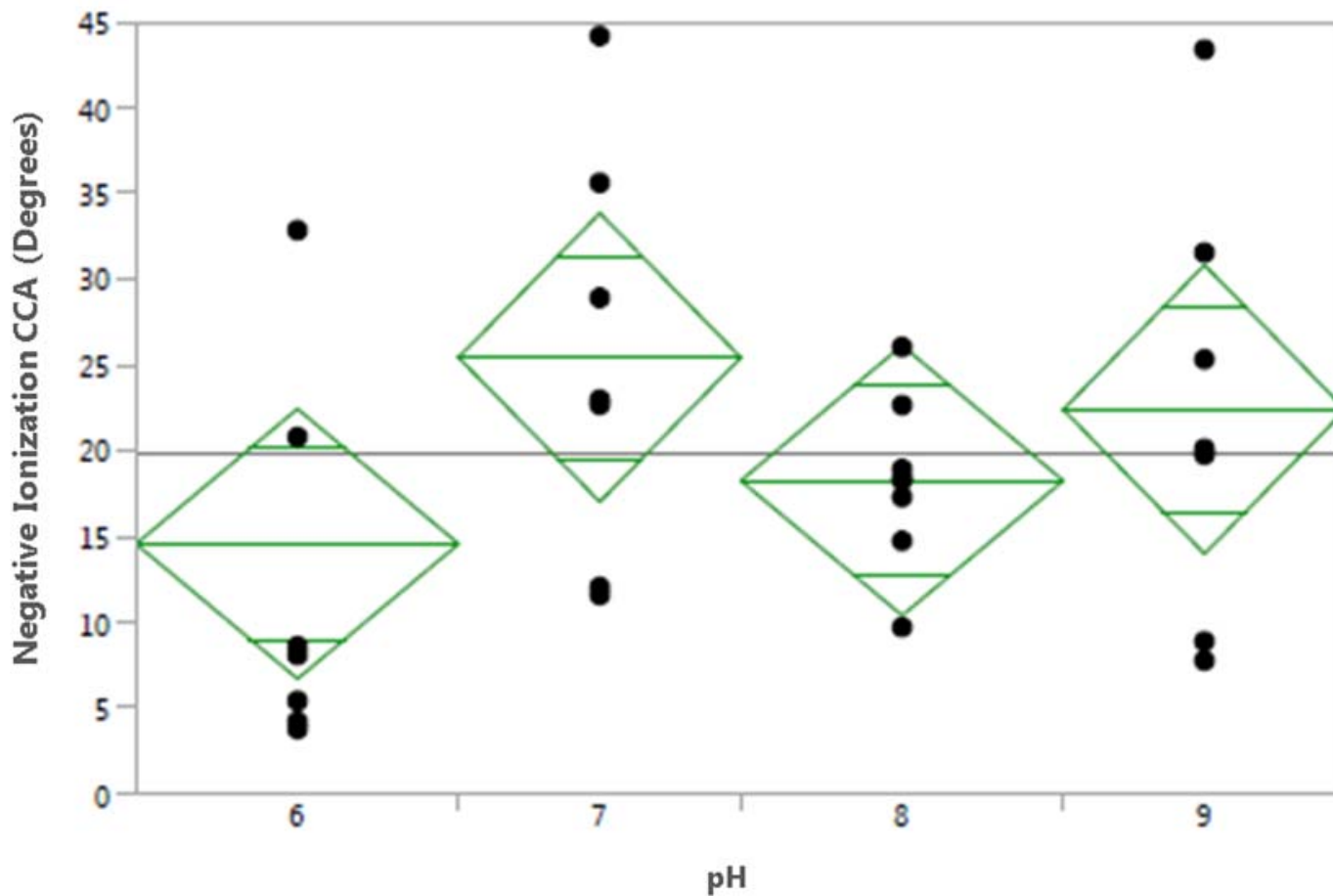


Figure 25: ANOVA of Negative Ionization CCA by pH; p-value = 0.2544 indicates insufficient evidence to suggest that pH is a statistically significant predictor of the Negative Ionization CCA. Each point represents one experiment. Within each pH category, experiments conducted at DCs between 5% and 100% are represented.

#### 4.3.1.4 Regression Analysis of Positive and Negative Ionization CCAs

A linear regression model was constructed with pH (nominal), DC (nominal), and interaction terms. The model upheld the three assumptions for linear regression models: independence (Durbin Watson Test), normally distributed residuals (Shapiro-Wilks Test), and constant variance (Breusch-Pagan Test). The significant predictor variables were pH 6, pH 7, pH 8, DC 70, and DC 70 \* pH 6. The adjusted R<sup>2</sup> for this model was .76, all VIF scores fell below 2.0, no significant outliers or overly influential points were detected (by studentized residuals, and Cooks D influence overlay plots), and the model's mean predictive error was 2.51° with standard deviation of 2.02°. The maximum error was 9.07°. See model (Equation 12) and assumption tests in Appendix N. Figure 26 shows the relationship between the true (observed) positive ionization chromatographic contrast angle (x-axis) and that predicted by the regression model (y-axis). The plot shows a linear trend, but it is apparent the model predicted the same value for several different conditions. This is due to the fact that the model incorporated dummy variables which did not cover many operating conditions such as pH 9 and most duty cycles.

##### **Equation 12: Positive Ionization CCA Regression Model**

$$Y_{(+)\text{CCA}} = (14.84291) - 9.853601(\text{pH}6) - 9.429323(\text{pH}8) + 3.1633158(\text{DC } 70) \\ + 4.637696(\text{pH}7) + 9.9500619(\text{pH}6 - 0.26667)(\text{DC } 70 - 0.16667)$$

The resulting negative run model upheld the three assumptions for linear regression models: independence (Durbin-Watson Test), normally distributed residuals (Shapiro-Wilks Test), and constant variance (Breusch-Pagan Test). The significant predictor variables were pH 6, pH 8, DC 30, DC 50, DC 70, and DC 70 \* pH 6. The adjusted R<sup>2</sup> for the model was .68, all VIF scores fell below 2.0, no significant outliers or

overly influential points were detected (by studentized residuals, and Cooks D influence overlay plots), and the model's mean predictive error was 4.50° with standard deviation of 3.11°. The maximum error was 10.90°. See model (Equation 13) and assumption tests in Appendix O. Figure 26 shows the relationship between the true (observed) negative ionization chromatographic contrast angle (x-axis) and that predicted by the regression model (y-axis). This model incorporated more duty cycle conditions, resulting in a stronger linear trend than that of the positive CCA.

**Equation 13: Negative Ionization CCA Regression Model**

$$\begin{aligned}
 Y_{(-)CCA} = & (17.87982) - 10.64895(pH6) - 5.000822(pH8) + 10.593667(DC\ 30) \\
 & + 22.596346(DC\ 50) + 8.3034399(DC\ 70) \\
 & + 18.489657(pH6 - 0.26667)(DC\ 70 - 0.16667)
 \end{aligned}$$

As expected, the randomization of the experiment order prevented bias of time: no significant effects were observed in the regression analysis that could be attributable to the date on which the experiment was run. This is true for both the positive and negative ionization conditions.

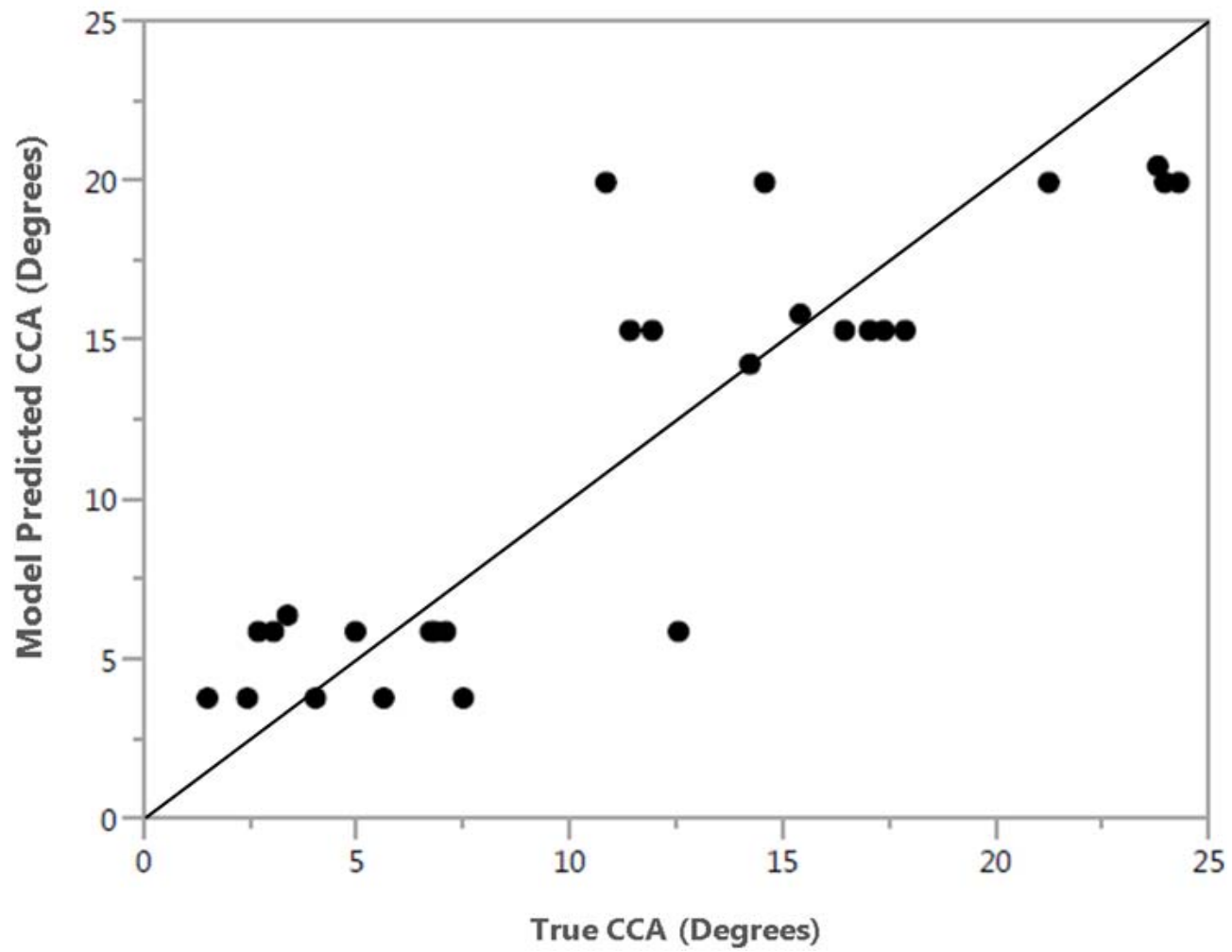


Figure 26: True vs Predicted Positive CCA

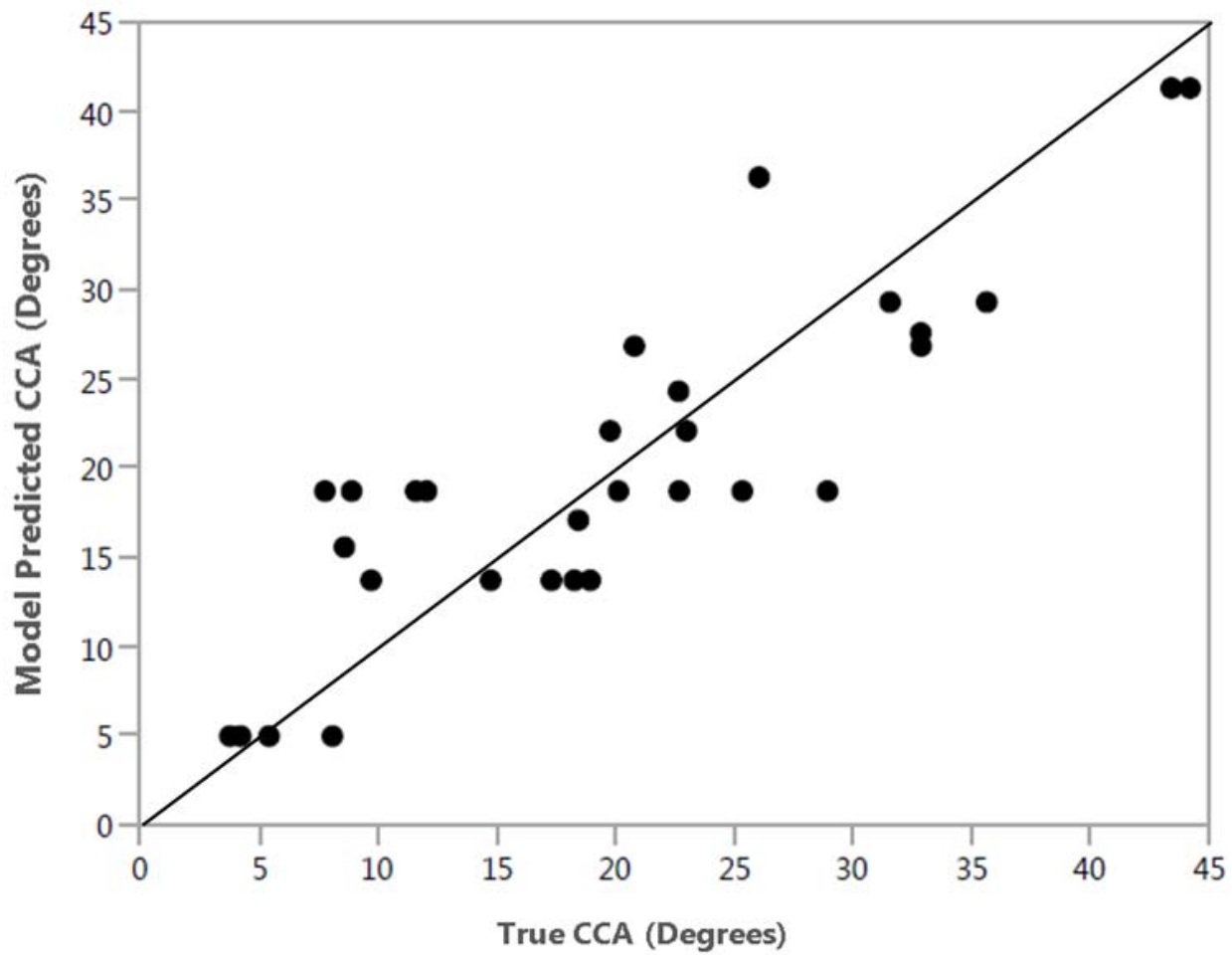


Figure 27: True vs Predicted Negative CCA

### 4.3.2 Mass Spectroscopy Analysis

Mass Spectroscopy analysis of the AOP byproducts suggests several isomers within each proposed structure. In chromatographs of all experimental conditions, three main peaks emerged for both ionization HPLC settings. These peaks are characterized in Table 1.

**Table 1: Proposed Byproduct Structures Naming Convention**

Retention Time	Proposed Structure	Ionization	Product Name
2.846	Tartrazine (abbrev TAR)	Negative	A
3.303	TAR + OH	Negative	B
3.909	TAR – O – COO + (CN)**	Negative	C
3.126	TAR + 2H	Positive	D
3.612	TAR – sulfonic acid (sulf) – COO + OH + (CN)**	Positive	E
3.938	TAR – sulf + O + (CN)**	Positive	F

\*\*CN from mobile phase and not from AOP reactions

There are several isomers for each proposed structure. TAR (Product A) may retain between zero and three Na<sup>+</sup> ions, thereby changing the charge of the main structure between neutral and -3, and reducing the mass of the main structure by 22.99 for every Na<sup>+</sup> lost. This phenomenon will be present in each remaining proposed structure, where the number of Na<sup>+</sup> is not constant; however, the main structures are not be affected. See each structure's mass with the variation in ionization in Table 2. It is likely that this ionization is due to the interaction of TAR with water and not due to the AOP.

**Table 2: Each Product's Potential Mass Due to Ionization**

Mass	A	B	C	D	E	F
- 0Na	534.36	551.37	474.35	536.38	328.22	371.22
- 1Na	511.32	528.38	451.36	513.39	305.23	348.23
- 2Na	488.38	505.39	428.37	490.40	282.24	325.24
- 3Na	465.39	482.40	405.38	467.41	-	-

Product B (Tar + OH) has 9 isomers, at each H location within the TAR structure as previously discussed. Product C is only a reduction of TAR and does not have any proposed isomers. The CN may take multiple locations (most likely at the local positive end of the main TAR structure left by the removal of O), but as the CN is due to the mobile phase, its location is trivial (this is also applicable for Products E and F). Product D likely has few simple isomers. The H's potentially bond at the local negative regions left by ionization, or at the azo group. The formation order for Product E is unclear. The OH addition may occur before or after the loss of the sulfonic acid group or COO<sup>-</sup> group. However, the OH locations will follow the same trends as discussed for Product B. Finally, Product F formation order is also unclear. Possible locations for the addition of oxygen are at such a location that hydrogen abstraction can occur, followed by OH addition.

### ***4.3.3 Byproduct and Mechanisms Associated with UV LED AOP of Tartrazine***

#### **4.3.3.1 Product A: Ionized Tartrazine**

Product A is the base case of TAR, which may be partially ionized in solution. It is not clear whether the 9<sup>th</sup> hydrogen atom is bonded to the nitrogen in the azo group, or bonded to the stand-alone oxygen opposite the COO<sup>-</sup> group. For the purposes of this study, it will be assumed that TAR's 9<sup>th</sup> Hydrogen atom is bonded to the N in the azo group, denoted by IUPAC name (E)-5-oxo-1-(4-sulfonatophenyl)-4-((4-sulfonatophenyl)diazenyl)-4,5-dihydro-1H-pyrazole-3-carboxylate.



#### 4.3.3.2 Product B: Tartrazine + OH

The most likely mechanism to account for the structure of Product B is OH addition. See Figure 28 with the caveat that the OH can join the main TAR structure at any of the locations detailed in Figure 2. These locations were determined using information from Benjamin (2013); however, the specific structures have not been previously proposed in the literature review of this study. The IUPAC names for the shown possible isomers in Figure 28 are:

- (E)-4-((2-hydroxy-4-sulfonatophenyl)diazenyl)-5-oxo-1-(4-sulfonatophenyl)-4,5-dihydro-1H-pyrazole-3-carboxylate
- (E)-4-(2-hydroxy-2-(4-sulfonatophenyl)-2 $\lambda^4$ -diazenyl)-5-oxo-1-(4-sulfonatophenyl)-4,5-dihydro-1H-pyrazole-3-carboxylate

#### 4.3.3.3 Product C: Tartrazine – O – COO Group

Product C is most likely caused by electron transfer, suggested by the fact that the main structure only loses atoms other than hydrogen. The presence of CN is attributable to the mobile phase. The loss of the COO<sup>-</sup> group may not be attributable to the AOP reaction, but to UV radiation alone. This structure is similar to that of dos Santos (2014), who observed the loss of the COO<sup>-</sup> group in subsequent reactions but did not also observe a loss of O. The IUPAC name for the proposed structure is (E)-4-((1-(4-sulfonatophenyl)-4,5-dihydro-1H-pyrazol-4-yl)diazenyl)benzenesulfonate.

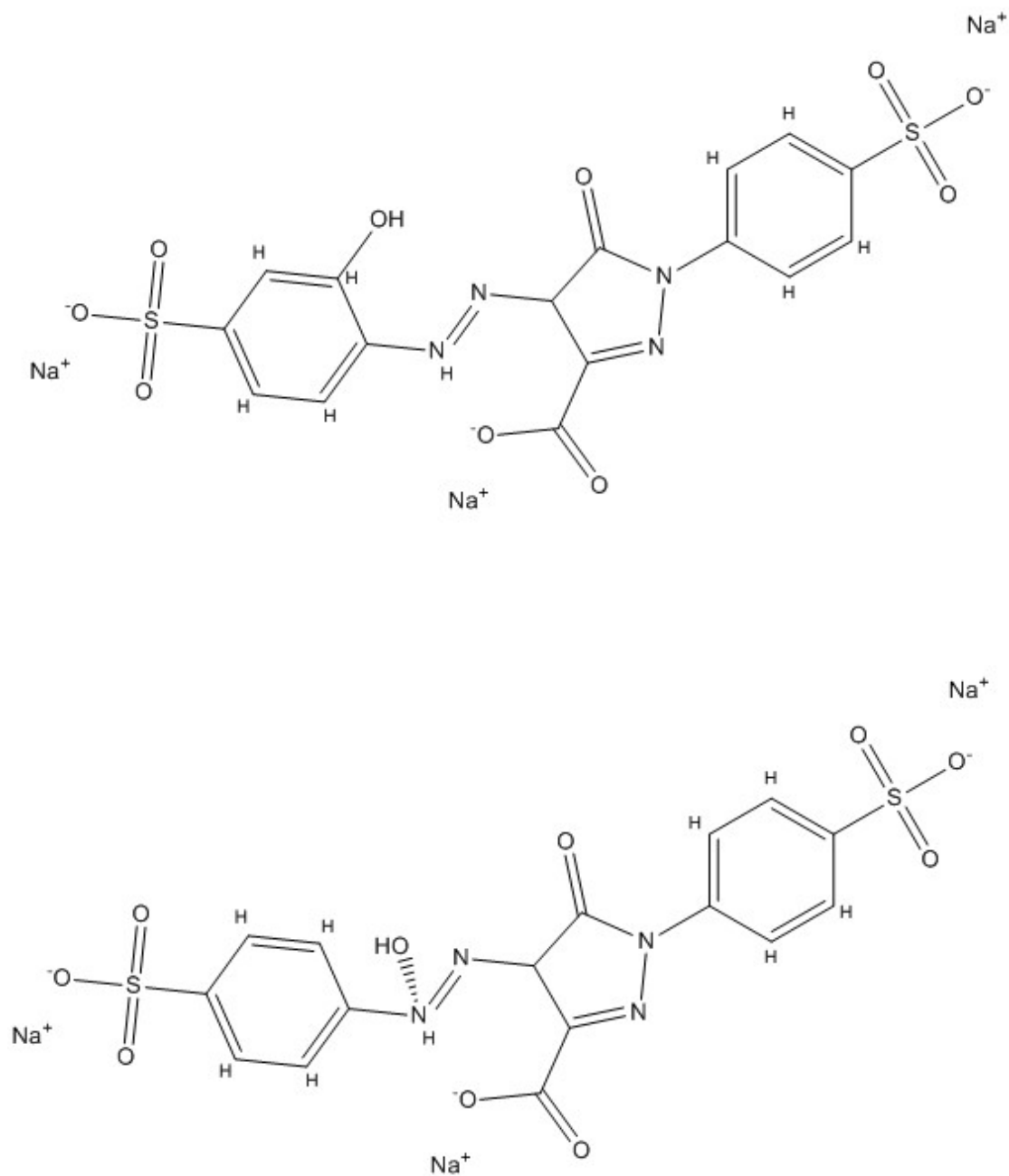


Figure 28: Tartrazine + OH Potential Isomers

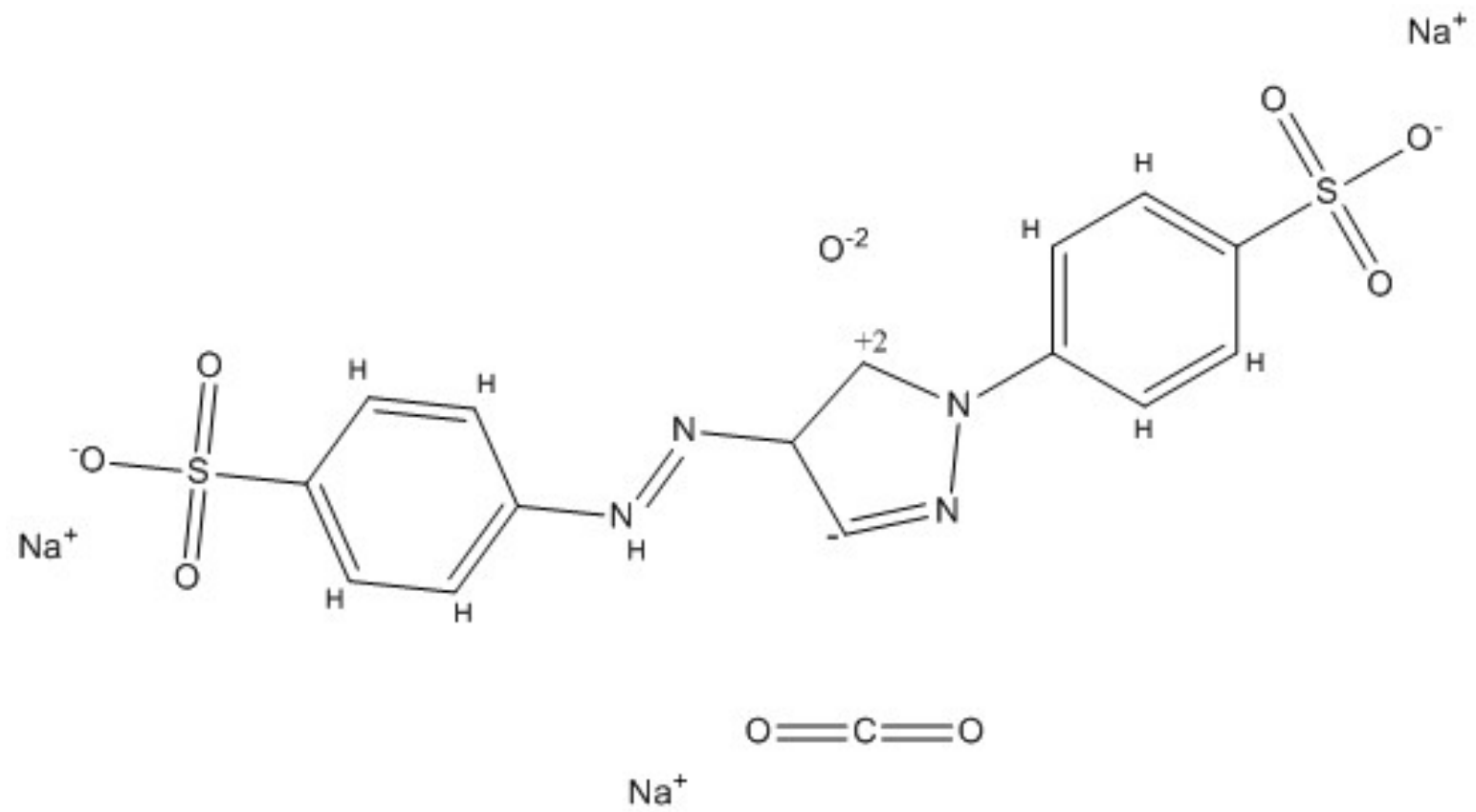


Figure 29: Tartrazine – O – COO + (CN) Potential Isomers

#### 4.3.3.4 Product D: Tartrazine + 2H

The net result of Product D is an increase from 9 to 11 hydrogen atoms. This could be interaction with the free H's in the water as depicted in Figure 30, or two OH additions and a loss of two oxygen atoms. Due to the fact that the sulfonic acid groups have pKa of 2, the third isomer within Figure 30 seems unlikely. In addition, dos Santos (2014) proposed the same structure as the first isomer within Figure 31.

It should also be noted, that a fourth isomer is possible as presented by Maslowska (1996). That isomer instead presents hydrogen bonds with both Nitrogen atoms within the azo group, and with the single oxygen opposite the COO<sup>-</sup> group depicted in Figure 31.

The IUPAC names for each of the four possible isomers for Product D are listed below:

- (E)-4-(3-carboxy-5-oxo-4-((4-sulfophenyl)diazenyl)-4,5-dihydro-1H-pyrazol-1-yl)benzenesulfonate
- (E)-4-((3-carboxy-5-oxo-1-(4-sulfophenyl)-4,5-dihydro-1H-pyrazol-4-yl)diazenyl)benzenesulfonate
- (E)-5-oxo-1-(4-sulfophenyl)-4-((4-sulfophenyl)diazenyl)-4,5-dihydro-1H-pyrazole-3-carboxylate
- (E)-5-hydroxy-1-(4-sulfonatophenyl)-4-((4-sulfonatophenyl)diazenyl)-4,5-dihydro-1H-pyrazole-3-carboxylate

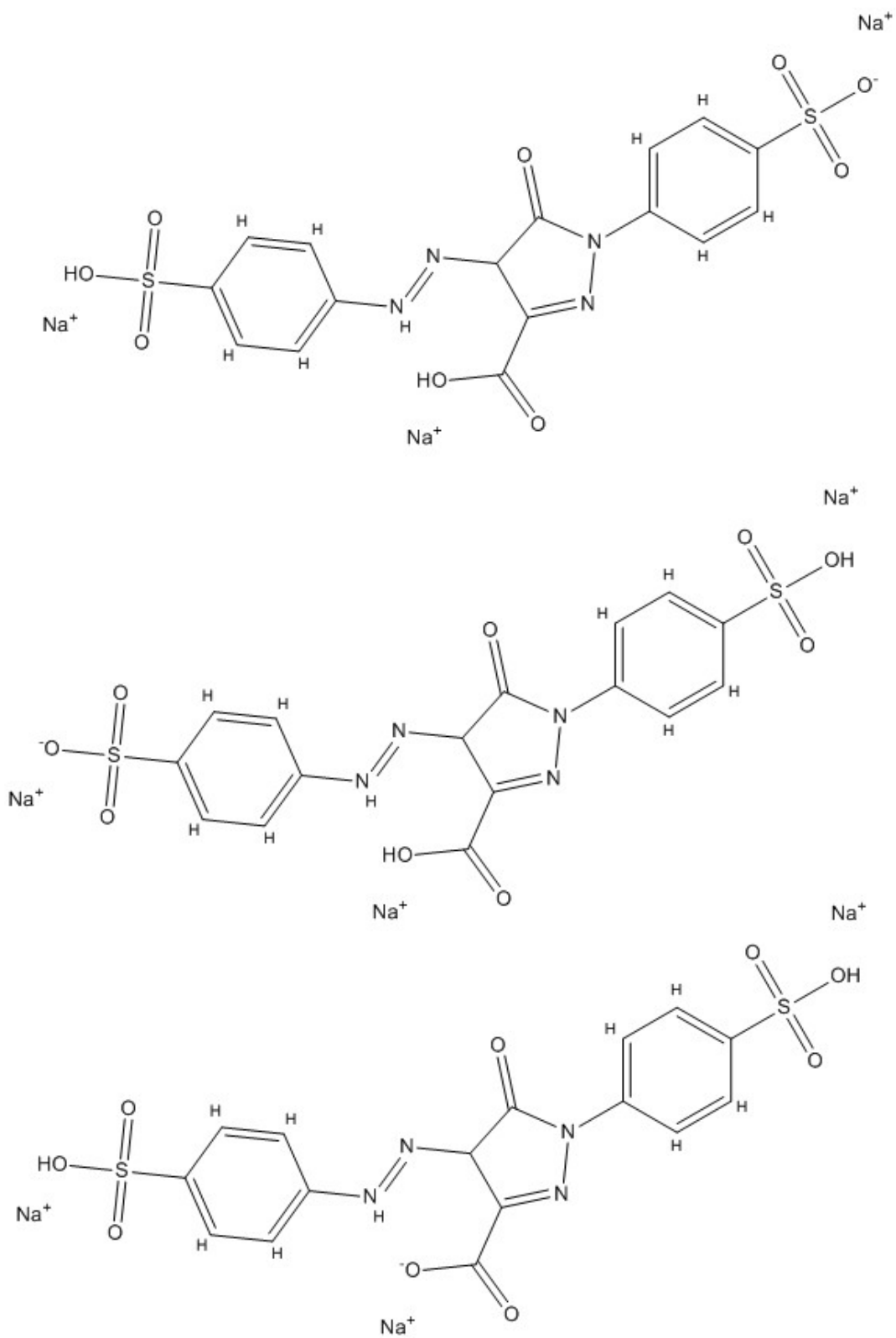


Figure 30: Tartrazine + 2H Potential Isomers

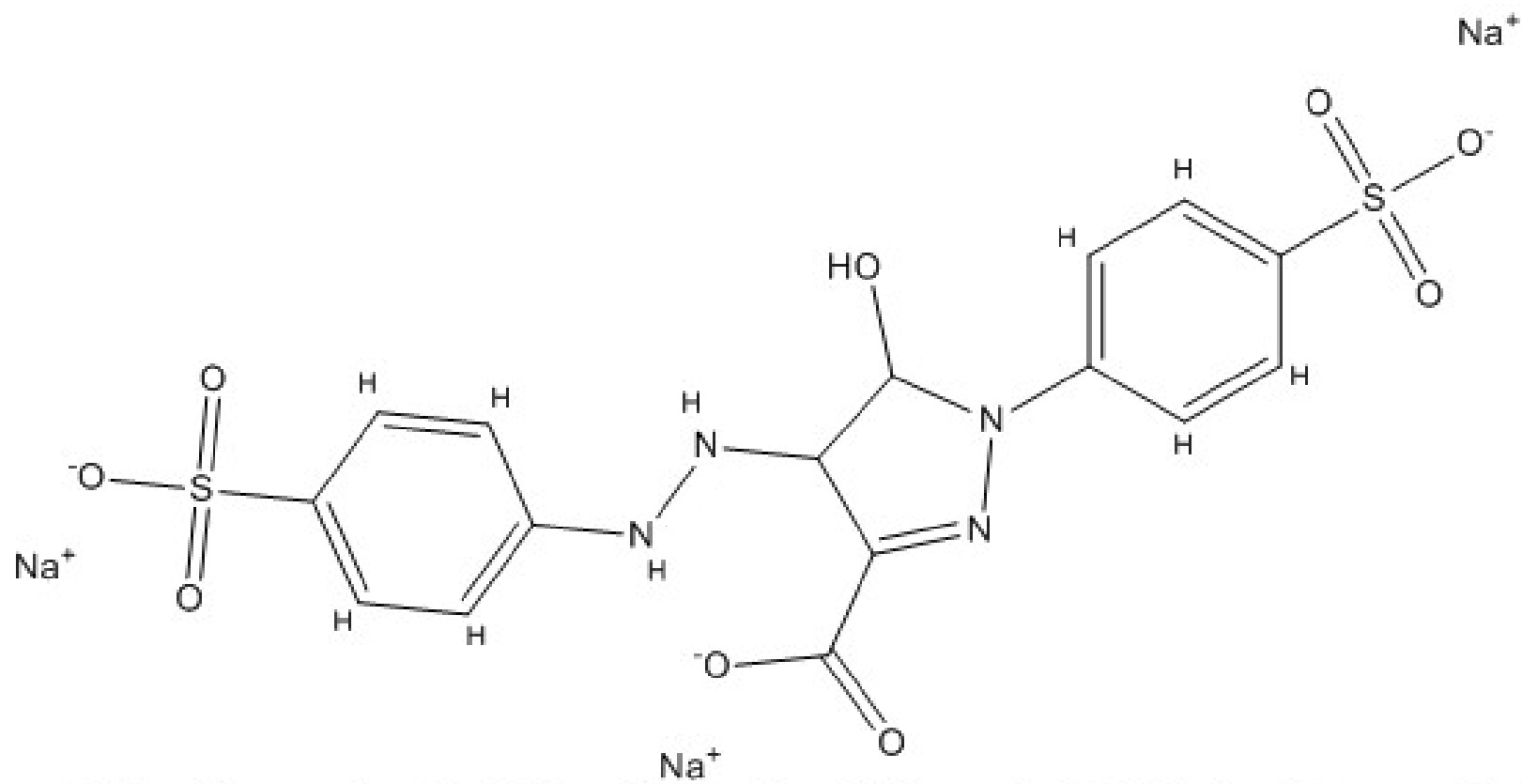


Figure 31: Tartrazine + 2H Most Likely Isomer

#### 4.3.3.5 Product E: Tartrazine – Sulfonic Acid Group – COO Group + OH

The reaction mechanisms for Product E are likely twofold: OH addition and Electron transfer, see Figure 32. The OH Addition is indicated by the increase of OH. The Electron Transfer is indicated by the loss of the sulfonic acid group and the COO<sup>-</sup> group. There are intermediate groups within this proposed structure. TAR – sulfonic acid group could be one of two structures, denoted by IUPAC names:

- (3-carboxylato-5-oxo-1-(4-sulfonatophenyl)-4,5-dihydro-1H-pyrazol-4-yl)diazen-1-ide
- (E)-3-carboxylato-5-oxo-4-((4-sulfonatophenyl)diazenyl)-4,5-dihydropyrazol-1-ide

The sulfonic acid group is expressed as 4-methylbenzenesulfonate. The order of the reaction mechanisms is undetermined. The IUPAC names for Product E's proposed isomers are:

- (1-(2-hydroxy-4-sulfonatophenyl)-5-oxo-4,5-dihydro-1H-pyrazol-4-yl)diazen-1-ide
- (Z)-4-(4-(hydroxydiazenyl)-5-oxo-4,5-dihydro-1H-pyrazol-1-yl)benzenesulfonate
- monosodium mono((E)-4-((3-hydroxy-4-sulfonatophenyl)diazenyl)-5-oxo-4,5-dihydropyrazol-1-ide)
- (Z)-4-(2-hydroxy-2-(4-sulfonatophenyl)-2H-diazenyl)-5-oxo-4,5-dihydropyrazol-1-ide

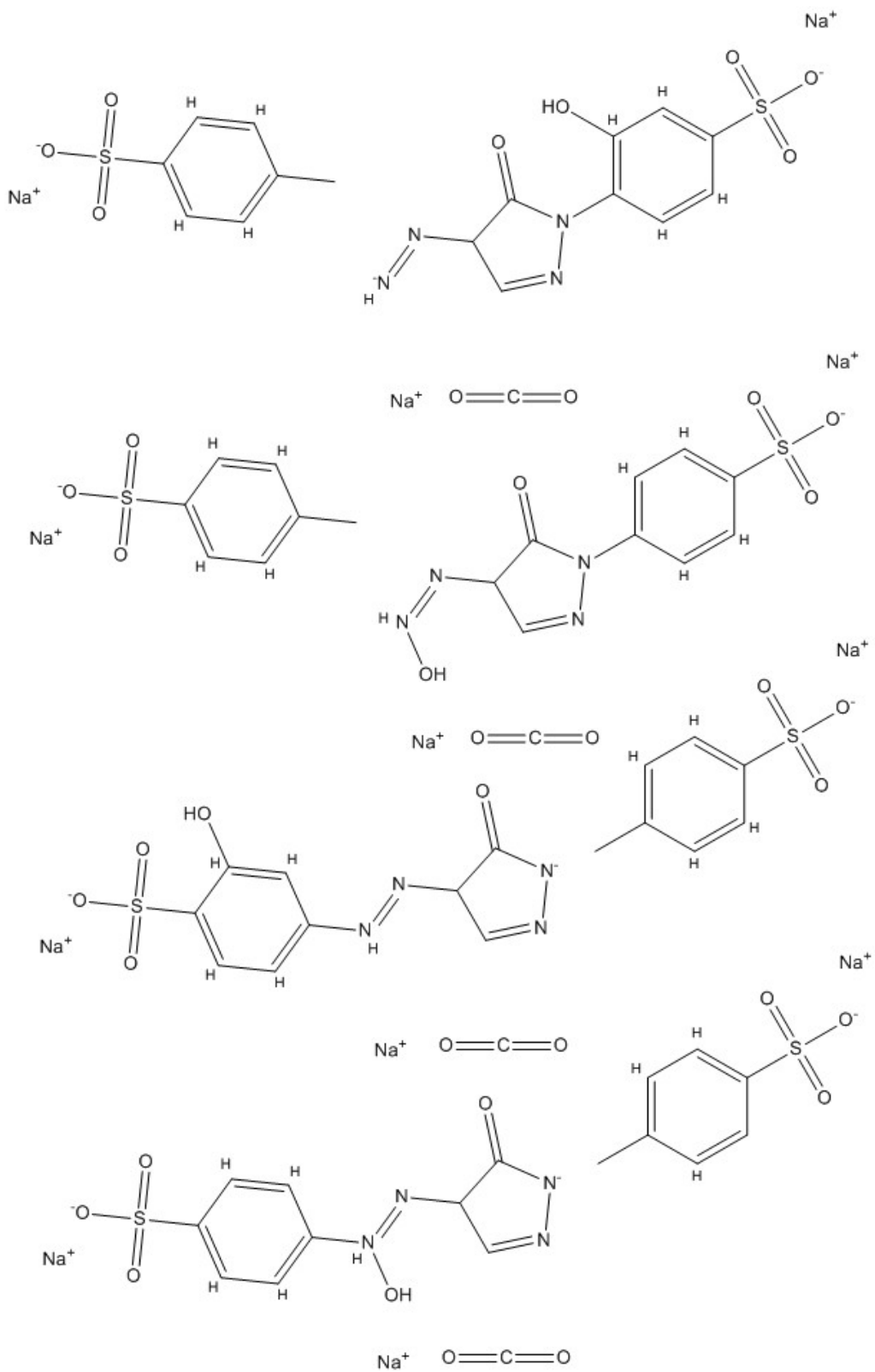


Figure 32: Tartrazine – Sulfonic Acid –  $\text{COO} + \text{OH} + (\text{CN})$  Potential Isomers



#### 4.3.3.6 Product F: Tartrazine – Sulfonic Acid Group + O

The reaction mechanism for Product F is one of two possibilities. First, the main structure of TAR (before or after loss of the sulfonic acid group) could pick up an oxygen atom from the water or from other possible reactions. If there had been a gain of two oxygen atoms, this could suggest a super anoxide radical ( $2\dot{O}_2^-$ ) was created in the reactor, and propagation of the radical would be possible (Benjamin & Lawler, 2013). The results of the AOP experiment are consistent with the explanation that super anoxide radicals are not created in these conditions; otherwise a greater decrease in concentration of TAR would be expected. Second, and more likely, there could be a hydrogen abstraction followed by an OH addition, the net result of which would only be an increase by one oxygen atom, see Figure 33. The location of CN from the mobile phase was not determined. Product F's proposed IUPAC name is (E)-4-(hydroxydiazenyl)-5-oxo-1-(4-sulfonatophenyl)-4,5-dihydro-1H-pyrazole-3-carboxylate.

#### ***4.3.4 Byproduct Structure Summary***

In summary, six products were consistently observed regardless of pH or DC of the experiments. Of these products, there were several proposed structures and respective isomers. To summarize and to simplify, the first isomer of each structure is included in Table 3; the structures mass calculations are shown in Appendix P.

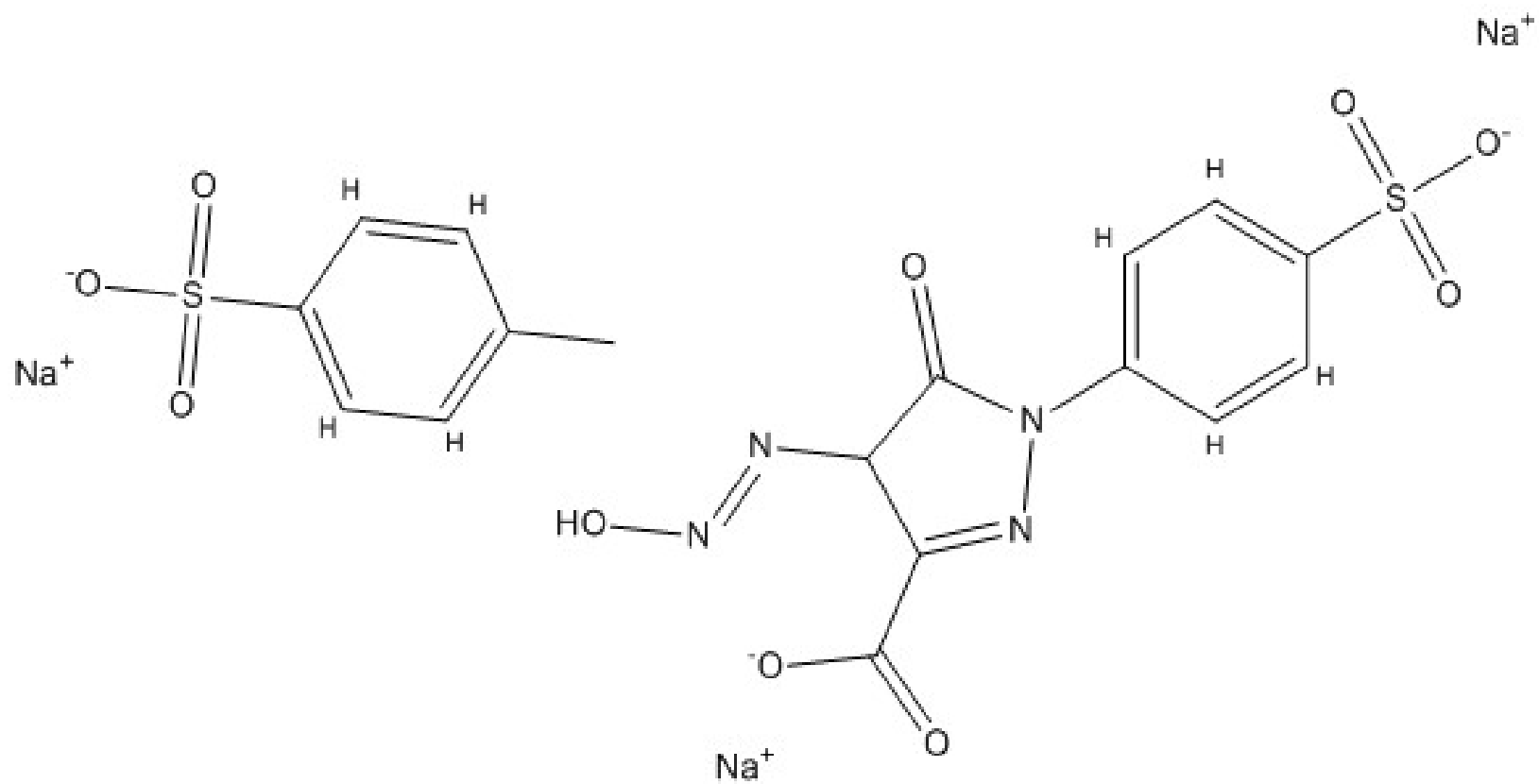
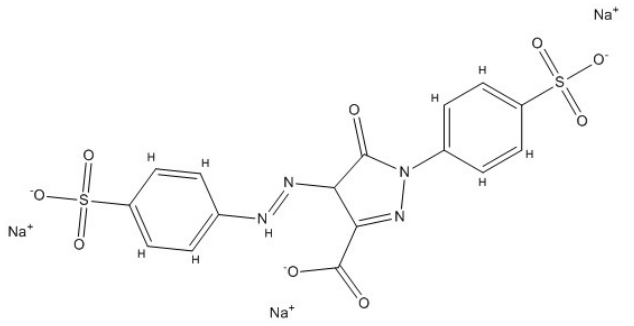
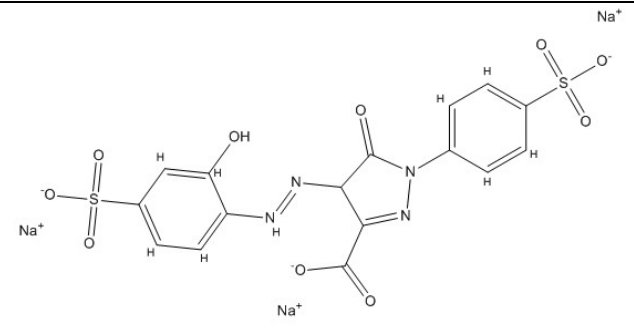
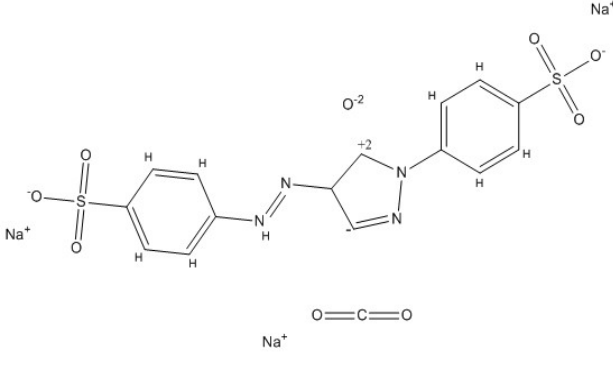
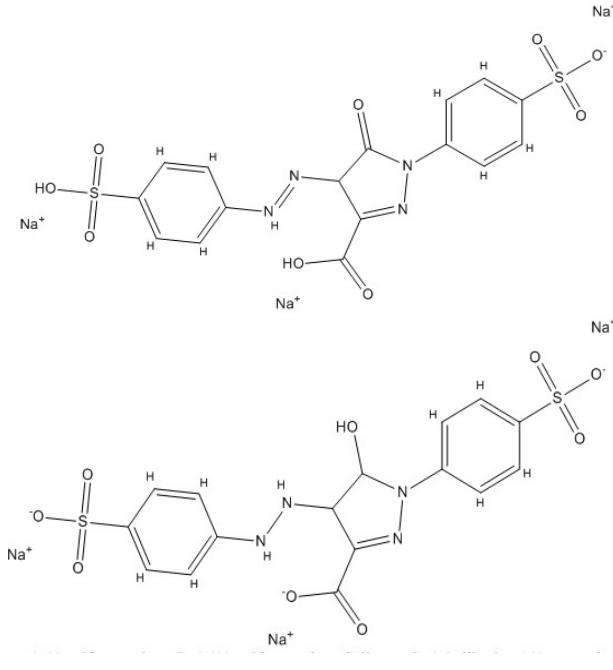
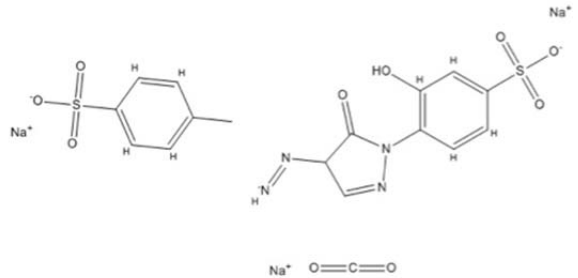
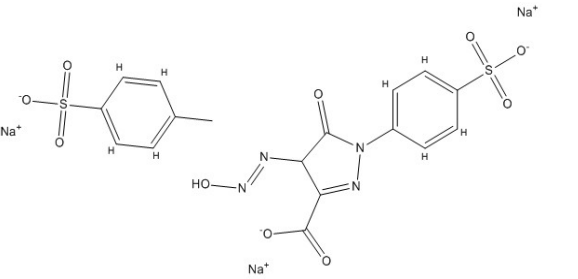
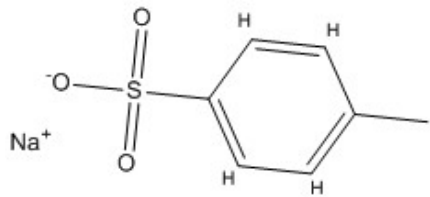


Figure 33: Tartrazine – Sulfonic Acid + O + (CN) Potential Isomer Structure

**Table 3: Proposed Structures by Mass, IUPAC Name. Reaction Mechanisms denoted by H, E, or O for Hydrogen Abstraction, Electron Transfer, or OH addition, respectively.**

Product (Mass) Reaction Mechanism	Structure	IUPAC Name	Reported by Others
A (534.36, 511.37, 488.38, 465.39) <b>None</b>		(E)-5-oxo-1-(4-sulfonatophenyl)-4-((4-sulfonatophenyl)diazenyl)-4,5-dihydro-1H-pyrazole-3-carboxylate	(Al-Dawery 2013; dos Santos et al., 2014; Maslowska & Janiak, 1996; Weisz et al., 2014)
B (551.37 528.38 505.39 482.40) <b>O</b>		(E)-4-((2-hydroxy-4-sulfonatophenyl)diazenyl)-5-oxo-1-(4-sulfonatophenyl)-4,5-dihydro-1H-pyrazole-3-carboxylate	No

<p>C (474.35 451.36 428.37 405.38)</p> <p><b>E</b></p>		<p>(E)-4-((1-(4-sulfonatophenyl)-4,5-dihydro-1H-pyrazol-4-yl)diazenyl)benzenesulfonate</p>	<p>No</p>
<p>D (536.38 513.39 490.40 467.41)</p> <p><b>E</b></p>		<p>(E)-4-(3-carboxy-5-oxo-4-((4-sulfonatophenyl)diazenyl)-4,5-dihydro-1H-pyrazol-1-yl)benzenesulfonate</p> <p>or</p> <p>(E)-5-hydroxy-1-(4-sulfonatophenyl)-4-((4-sulfonatophenyl)diazenyl)-4,5-dihydro-1H-pyrazole-3-carboxylate</p>	<p>(dos Santos et al., 2014)</p> <p>(Maslowska &amp; Janiak, 1996)</p>

<p>E (328.22 305.23 282.24) OH Add <b>E</b></p>		<p>(1-(2-hydroxy-4-sulfonatophenyl)-5-oxo-4,5-dihydro-1H-pyrazol-4-yl)diazene-1-ide</p>	<p>No</p>
<p>F (371.22 348.23 325.24) <b>H, E, O</b></p>		<p>(E)-4-(hydroxydiazenyl)-5-oxo-1-(4-sulfonatophenyl)-4,5-dihydro-1H-pyrazole-3-carboxylate</p>	<p>No</p>
<p>Sulfonic Acid Group (179.14 156.15) <b>E</b></p>		<p>4-methylbenzenesulfonate</p>	<p>(Weisz et al., 2014)</p>

#### **4.4 Investigative Questions Answered**

The first investigative question asked how pH affects the AOP of TAR and the associated hypothesis was that pH was significant. This hypothesis was supported by the data and analysis. The pH of the solution significantly affected the first order rate constant; this study observed a negative correlative relationship. Optimal TAR removal reported by Mudimbi (2015) was about 22%. This study observed optimal removal of 25%, with corresponding  $k_s$  of  $1.2346E-03 \text{ min}^{-1}$ .

The second investigative question of this research was what byproducts are generated and does pH influence the byproduct profile? The AOP of TAR produces several byproducts, each with a variety of possible structures, masses, and charge. Possible products are described in Table 3. The pH of the solution significantly influenced the CCAs in this study.

The third investigative question of the research was what reaction mechanisms occur in the AOP of TAR? The observations made in this study suggest that primary mechanisms of the AOP of TAR are OH Addition and Electron Transfer; but observations were also made that also indicate Hydrogen Abstraction.

#### **4.5 Summary**

In summary, this section developed the results and analysis conducted on the AOP Experiment, and the associated byproduct analysis. The pH of the solution significantly affected the first order rate constant. The byproduct profile of TAR remained consistent throughout the experiment, but the magnitudes of the peaks (amounts of each byproduct) varied greatly as detected by the CCA analysis, particularly at pH 7

and DC levels between 30% and 70%. The main reaction mechanisms of the AOP of TAR are likely OH Addition and Electron Transfer.

## V. Conclusions and Recommendations

### 5.1 Chapter Overview

This chapter presents the outcomes of this study, discusses the significance of the findings and provides recommendations for further research in this field. The operating conditions for the UV/H<sub>2</sub>O<sub>2</sub> AOP of TAR are discussed. The suggested byproducts from this reaction are characterized and potential reaction mechanisms identified.

### 5.2 Conclusions of Research

The conclusions of this study are as follows:

- The relative concentration of TAR was reduced from 1 to between 1 – 0.75 over the pH and DC values investigated in this effort. The first order rate constant for TAR removal was statistically and positively correlated with DC, statistically and negatively correlated with pH, and typically greatest at pH6. DC and pH were used as predictor variables in a regression model of the first order rate constant with adjusted R<sup>2</sup> of 0.85.
- Chromatographic contrast angle determinations revealed that the byproduct profile was most significantly influenced by pH and duty cycle. CCA under positive ionization is predicted by significant factors of pH 6, pH 7, pH 8, and 70% DC. The CCA under negative ionization is predicted by pH 6, pH 8, 30% DC, 50% DC, 70% DC. These factors were used as variables in regression models to predict positive and negative CCA with adjusted R<sup>2</sup> of 0.76, and 0.68, respectively.



- Chemical byproduct analysis indicated that OH addition (Products B, E, and F), electron transfer without molecule transfer (Products C, D, E, and F), and possibly H abstraction (Product F) were among the plausible reaction mechanisms for TAR degradation.
- Four potentially novel metabolites were identified, two of which demonstrate that TAR was likely cleaved. These metabolites were (1-(2-hydroxy-4-sulfonatophenyl)-5-oxo-4,5-dihydro-1H-pyrazol-4-yl)diazene-1-ide and (E)-4-(hydroxydiazanyl)-5-oxo-1-(4-sulfonatophenyl)-4,5-dihydro-1H-pyrazole-3-carboxylate (Products E and F, respectively). The other novel metabolites proposed by this study are: (E)-4-((2-hydroxy-4-sulfonatophenyl)diazanyl)-5-oxo-1-(4-sulfonatophenyl)-4,5-dihydro-1H-pyrazole-3-carboxylate, and (E)-4-((1-(4-sulfonatophenyl)-4,5-dihydro-1H-pyrazol-4-yl)diazanyl)benzenesulfonate (Products B and C, respectively).

### 5.3 Significance of Research

This research explained what effect pH has on the apparent first order rate constant for the LED driven UV/H<sub>2</sub>O<sub>2</sub> AOP of TAR. This research also demonstrated pH can be used in conjunction with DC as a predictor for the first order rate constant as well as the positive and negative CCAs of the chromatograms of the byproducts. This capability was not previously available and no regression models existed. Additionally, this research offered suggestion of byproduct structures and identified possible AOP reaction mechanisms.

These are significant findings, because understanding AOP ideal operating conditions, mechanisms, and products can help the USAF in treatment of military wastewater, preserving the local environment, and safeguarding military members in chemical attack situations.

Byproducts are just as important to understand as the original substance because they may be toxic as well. It is not acceptable to conduct an AOP on CBRN contaminants and expect complete mineralization. Understanding the AOP reaction mechanisms leads to better understanding of the how byproducts are formed which may help in predicting AOP outcomes for contaminants for which laboratory testing has not been conducted or data may not be available.

The creation of linear regression models for reactor performance and byproduct profile has not been accomplished in other studies on TAR. These models are practically applicable to future research as follows. The AOP regression model provides a baseline against which future researchers can compare additional independent variable (other than pH or DC) testing in the AOP of TAR without having to conduct the conditions represented in this study again. The byproduct profile models are also useful as future research on byproduct formation can save time and effort by using the model as a baseline.

#### **5.4 Recommendations for Future Research**

Future research in this field should consider a variety of topics, to include: evaluation of more acidic pH levels, implementation of more powerful LEDs which will provide greater understanding of the UV dose effects, executing AOPs on other

contaminants (perhaps mild chemical or nerve agents), construction of large scale reactor capable of handling greater flow rates, and creating exact mass characterization using time of flight MS. Future TAR byproduct research should include measurement by UV-Vis at peaks 258, 277, and 404 to detect and substantiate manufacturing isomers Pk5 and Pk7. Future research could also incorporate hydroxyl radical sensors to quantify concentrations of the radicals during the reaction. Future research should also attempt to construct predictive models for byproducts depending on the constituent.

## **5.5 Summary**

To conclude, wastewater treatment is vital to the success of USAF operations. Incorporating UV LEDs into these treatment methods can be beneficial with further study and design. This study observed that the LED UV/H<sub>2</sub>O<sub>2</sub> AOP of TAR is significantly affected by the pH of the solution. The first order rate constant can be reasonably predicted by DC and pH levels. Operating conditions can be manipulated to maximize  $k_s$  (DCs 70-100%) or to maximize  $k_{s,adj}$  (DCs of 5-10%), at pH 6. Evaluation of the AOP reaction byproducts suggested reaction mechanisms of OH Addition and Electron Transfer.

# PULSED ULTRAVIOLET LIGHT EMITTING DIODES FOR ADVANCED OXIDATION OF TARTRAZINE

## Appendix A: pH Meter Calibration Procedures

- a. Turn Meter On
- b. Take meter out of solution
- c. Place meter over waste beaker and rinse w/distilled water (including inside the tip)
- d. Wipe down
- e. Place meter in "4" solution (pink) – make sure tip is not touching glass
- f. Press "cal", wait until  $\surd$  (A), remove, repeat step c and d
- g. Place in "7" solution (yellow) repeat step f
- h. Place in "10" solution (blue) repeat step f
- i. Once the meter reads  $\surd$  (A), hit "end", hit "save"
- j. Place meter in "7" (yellow) soln, hit "read". Wait for  $\surd$  (A) and ensure  $\sim=7$ . Rinse and Dry.
- k. Take reading of your solution. Rinse and dry.
- l. VERIFY pH machine reading with strip (machine is most accurate, but looking at ones place only)
- m. If disagreement between math and machine, hit "cal" one more time. Take notes.
- n. When you believe the reading is correct, return meter to original solution. Power off.

## Appendix B: AOP Experiment Schedule

Data Point	Duty Cycle (%)	pH	H <sub>2</sub> O <sub>2</sub> Ctrl	Date Completed
1	70	8	N	9-Jul-15
2	0	7	N	7-Mar-15
3	5	7	N	13-Mar-15
4	0	9	N	16-Mar-15
5	100	9	Y	8-Apr-15
6	10	7	N	9-Apr-15
7	100	8	Y	16-Apr-15
8	50	8	N	23-Apr-15
9	10	9	N	30-Apr-15
10	50	9	N	7-May-15
11	0	6	N	14-May-15
12	10	8	N	27-May-15
13	70	6	N	1-Jun-15
14	20	6	N	9-Jun-15
15	30	6	N	17-Jun-15
16	100	6	N	26-Jun-15
17	30	7	N	3-Jun-15
18	20	9	N	22-Jun-15
19	5	6	N	29-Jun-15
20	30	8	N	2-Jul-15
21	70	7	N	13-Jul-15
22	100	9	N	1-Jul-15
23	100	8	N	6-Jul-15
24	20	8	N	10-Jul-15
25	100	7	Y	14-Jul-15
26	0	8	N	15-Jul-15
27	100	6	Y	17-Jul-15
28	70	9	N	23-Jul-15
29	5	8	N	21-Jul-15
30	100	7	N	30-Jul-15
31	20	7	N	6-Aug-15
32	50	7	N	11-Aug-15
33	10	6	N	7-Aug-15
34	5	9	N	28-Jul-15
35	30	9	N	5-Aug-15
36	50	6	N	4-Aug-15
37	100	8	N	13-Aug-15
38	70	6	N	12-Aug-15









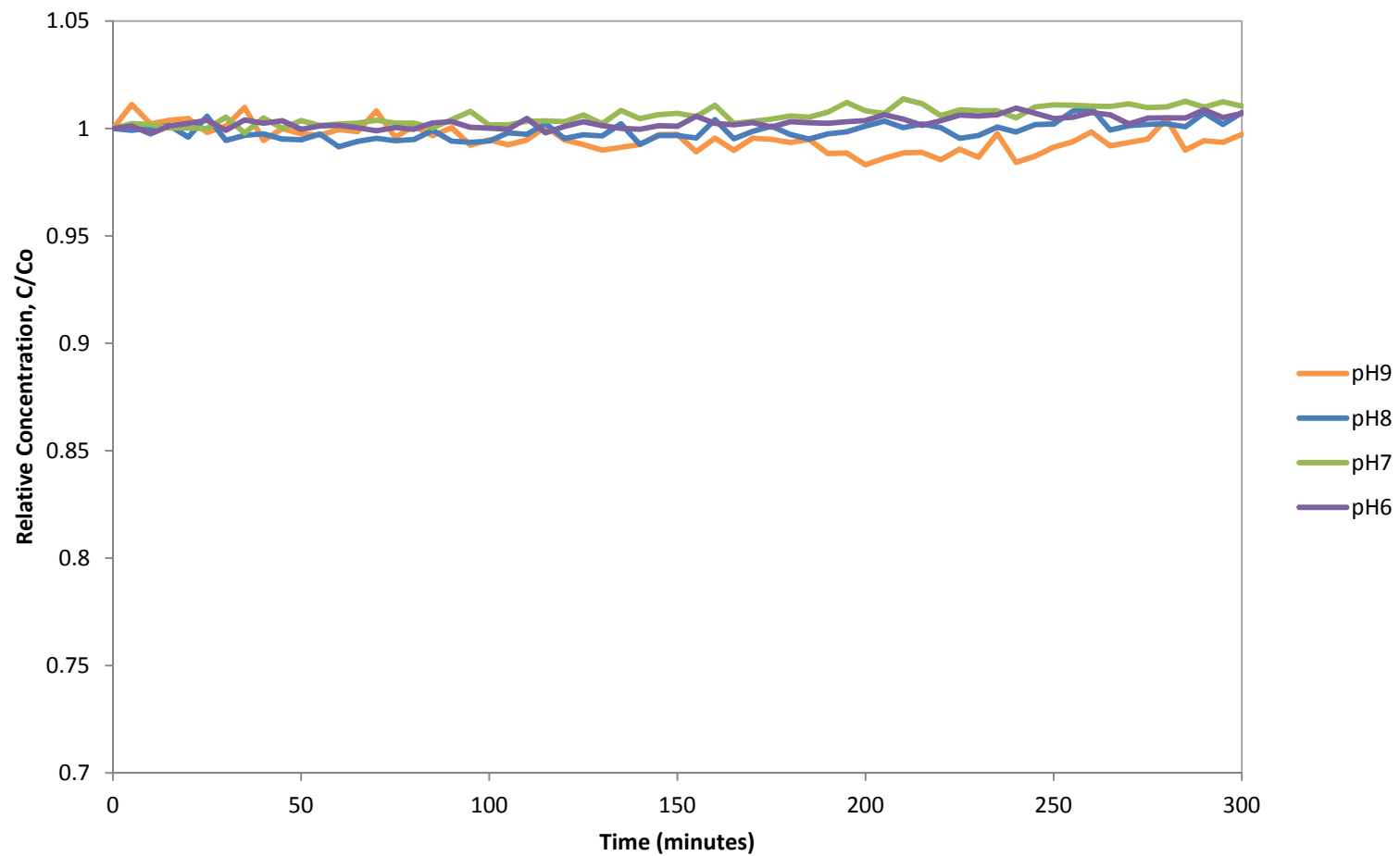




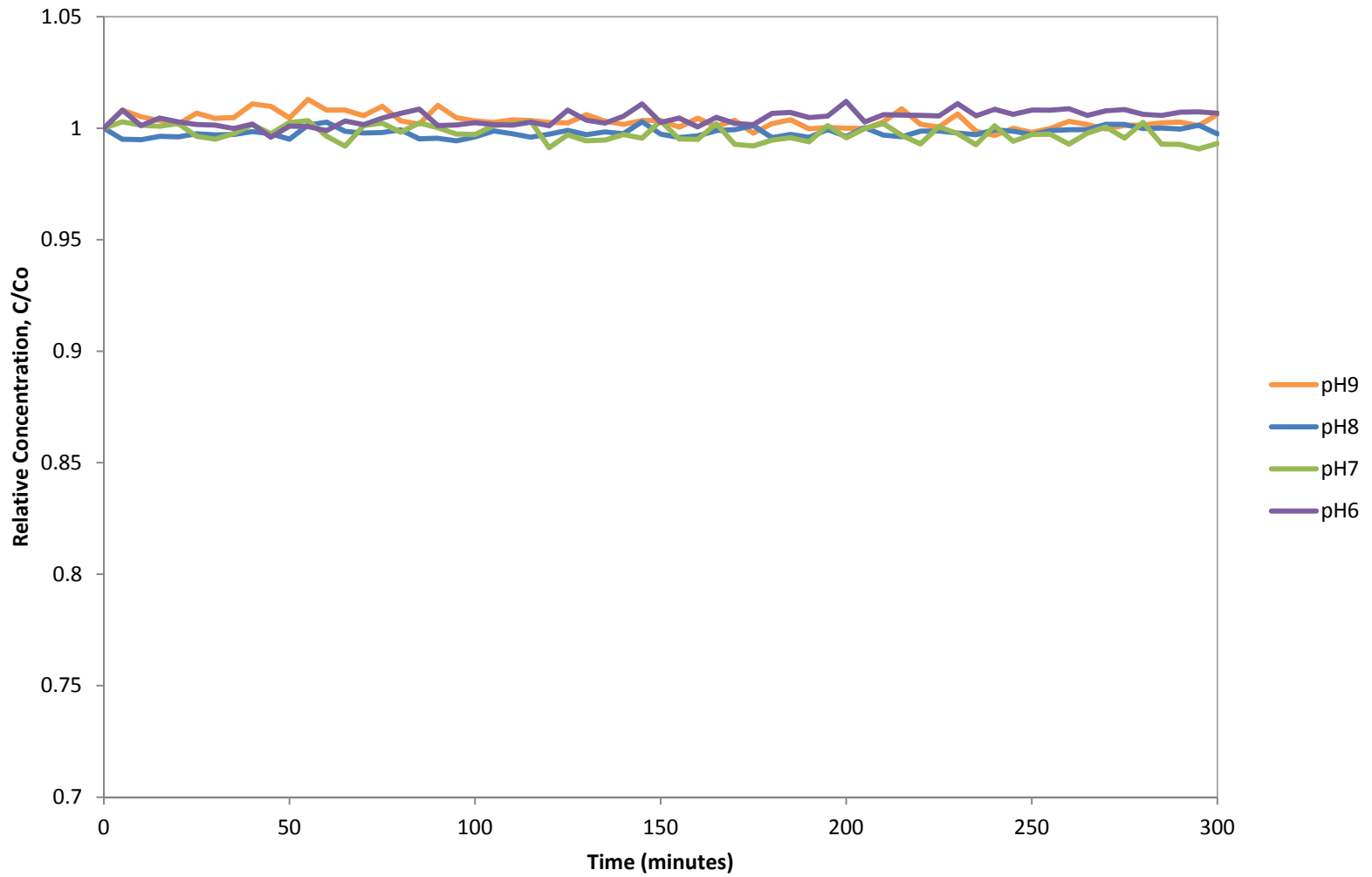
15-Jun-15		9-Jul-15		12-Aug-15		13-Aug-15	
pH9 50		pH8 70		pH6 70		pH8 100	
2.8300E-04	5.6600E-04	4.5001E-04	6.4288E-04	8.2701E-04	1.1814E-03	0.000481987	4.8199E-04
0.9950	0.9899	0.9915	0.9831	0.9995	0.9990	0.9988	0.9977
C/Co	Model	C/Co	Model	C/Co	Model	C/Co	Model
1	1	1	1	1	1	1	1
0.994477902	0.998593308	1.004943956	0.997764068	0.998282809	0.995894796	0.997813881	0.997605403
0.996676647	0.997203101	0.993460191	0.995556183	0.993596411	0.991848723	0.995402067	0.995241222
0.994427577	0.995829187	1.001026193	0.993375995	0.988843975	0.987860928	0.993018866	0.992907072
0.995406017	0.994471373	0.990786588	0.991223155	0.98484553	0.983930573	0.991842235	0.990602569
0.992027601	0.993129472	0.990366077	0.989097321	0.982016246	0.980056829	0.987444385	0.988327339
0.987673831	0.991803298	0.987422259	0.986998153	0.978447546	0.976238882	0.986019029	0.986081008
0.986264787	0.990492665	0.993180886	0.984925318	0.974036397	0.972475928	0.985068163	0.983863211
0.985105792	0.989197391	0.988282502	0.982878485	0.969708438	0.968767174	0.98299217	0.981673584
0.990509363	0.987917297	0.981823828	0.980857328	0.966128415	0.965111841	0.978922535	0.979511769
0.983842915	0.986652205	0.976228504	0.978861525	0.963837407	0.961509158	0.97822842	0.977377414
0.98606528	0.985401939	0.987093813	0.976890757	0.958973303	0.957958367	0.976337925	0.97527017
0.983771914	0.984166325	0.978360987	0.974944711	0.954602291	0.954458721	0.97443389	0.973189692
0.983929065	0.982945192	0.978355924	0.973023076	0.951779397	0.951009483	0.972872795	0.97113564
0.978758384	0.981738369	0.970507164	0.971125547	0.948329879	0.947609927	0.970562802	0.969107679
0.978758599	0.980545689	0.96945174	0.969251821	0.945722363	0.944259337	0.969090269	0.967105477
0.980225147	0.979366986	0.972925283	0.967401599	0.94260617	0.940957008	0.967639719	0.965128707
0.976254526	0.978202097	0.969646575	0.965574587	0.939832384	0.937702246	0.966101934	0.963177046
0.976872073	0.97705086	0.967500167	0.963770493	0.937874701	0.934944364	0.963880572	0.961250175
0.973860653	0.975913114	0.966616676	0.96198903	0.933226311	0.931332687	0.961604356	0.959347779
0.975945179	0.974788702	0.959438504	0.960229914	0.931048541	0.928216551	0.958583988	0.957469547
0.972364814	0.973677467	0.968962638	0.958492864	0.927374563	0.925145299	0.957136858	0.955615173
0.97178905	0.972579255	0.955836643	0.956777604	0.924749781	0.922118284	0.954013272	0.953784353
0.969837984	0.971493913	0.956532549	0.955083861	0.920716131	0.91913487	0.954004828	0.951976788
0.967354228	0.970421129	0.957792935	0.953411365	0.919395387	0.916194428	0.952742497	0.950192183
0.968805987	0.969361238	0.954811716	0.951759848	0.915331353	0.91329634	0.949908394	0.948430246
0.967727326	0.968313608	0.959128125	0.950129049	0.913370082	0.910439995	0.949481778	0.946690689
0.965350969	0.967278257	0.949609399	0.948518706	0.91050649	0.907624792	0.946524219	0.944973228
0.966268459	0.966255038	0.958185828	0.946928564	0.907598499	0.904850138	0.945235648	0.943277582
0.962459296	0.965243811	0.946582493	0.945358369	0.904315027	0.90211545	0.944711886	0.941603474
0.963001032	0.964244435	0.939914713	0.943807871	0.902432325	0.899420152	0.941312916	0.939950631
0.9644347	0.963256771	0.941386506	0.942276823	0.899552501	0.896763676	0.937960844	0.938318783
0.95907327	0.962280681	0.940893836	0.94076498	0.896432216	0.894145464	0.939913591	0.936707662
0.964366355	0.96131603	0.942850704	0.939272102	0.892825565	0.891564963	0.937517689	0.935117005
0.958202086	0.960362685	0.943190314	0.937797951	0.88917345	0.889021632	0.934137213	0.933546553
0.959568485	0.959420511	0.940456522	0.936342292	0.887321326	0.886514934	0.932272399	0.93199605
0.957285888	0.95848938	0.932615358	0.934904893	0.88584827	0.884044341	0.932419304	0.93046524
0.958776414	0.95756916	0.935182164	0.933485525	0.883140185	0.881609335	0.930781581	0.928953875
0.957907886	0.956659725	0.928329446	0.932083962	0.880076127	0.879209402	0.928666228	0.927461707
0.959585428	0.955760948	0.928606392	0.93069998	0.877125587	0.876844037	0.926446262	0.925988493
0.955853225	0.954872703	0.927682853	0.929333336	0.875762407	0.874512742	0.925153643	0.924533992
0.955901612	0.953994869	0.929537872	0.927983882	0.872542954	0.872215026	0.923907084	0.923097966
0.951710306	0.953127321	0.922418047	0.926651332	0.870689876	0.869950407	0.92322581	0.92168018
0.951707506	0.952269941	0.921867491	0.925335498	0.869003742	0.867718406	0.920628289	0.920280403
0.953174054	0.951422609	0.921074858	0.924036171	0.864820078	0.865518554	0.918911846	0.918898406
0.95252097	0.950585206	0.922569323	0.922753142	0.863533026	0.863350389	0.916142297	0.917533963
0.948779722	0.949757618	0.917174243	0.921486208	0.862016749	0.861213453	0.915104196	0.916186851
0.950764458	0.948939728	0.925744917	0.920235166	0.857611093	0.859107298	0.914515671	0.91485685
0.949783577	0.948131423	0.919669928	0.918999818	0.856583032	0.857031478	0.913104063	0.913543743
0.948173087	0.947332591	0.917728136	0.917779966	0.854248466	0.854985559	0.910394601	0.912247316
0.947218409	0.94654312	0.922089946	0.916575416	0.85117925	0.852969108	0.908385326	0.910967355
0.947611125	0.945762902	0.90782912	0.915385976	0.848794848	0.850981702	0.908653593	0.909703652
0.947988297	0.944991827	0.909591957	0.914211457	0.846726112	0.849022922	0.908172332	0.908456001
0.942846692	0.944229788	0.904832825	0.913051671	0.844283633	0.847092356	0.90451389	0.907224198
0.944808957	0.94347668	0.910984689	0.911906434	0.842329257	0.845189597	0.903535527	0.906008041
0.941809598	0.942732398	0.907139947	0.910775563	0.841507156	0.843314245	0.901473701	0.904807332
0.941291912	0.941996838	0.910741116	0.909658877	0.837992217	0.841465905	0.90146742	0.903621874
0.940402636	0.941269899	0.903715429	0.9085562	0.835732209	0.839644188	0.900637428	0.902451474
0.940325246	0.940551478	0.902390653	0.907467354	0.833351115	0.837848711	0.899086243	0.90129594
0.939913308	0.939841477	0.90243732	0.906392168	0.831403915	0.836079095	0.89762704	0.900155084
0.938775492	0.939139797	0.905675864	0.905330469	0.831095479	0.834334969	0.895323118	0.899028719

## Appendix D: AOP Experiment Charts by Duty Cycle

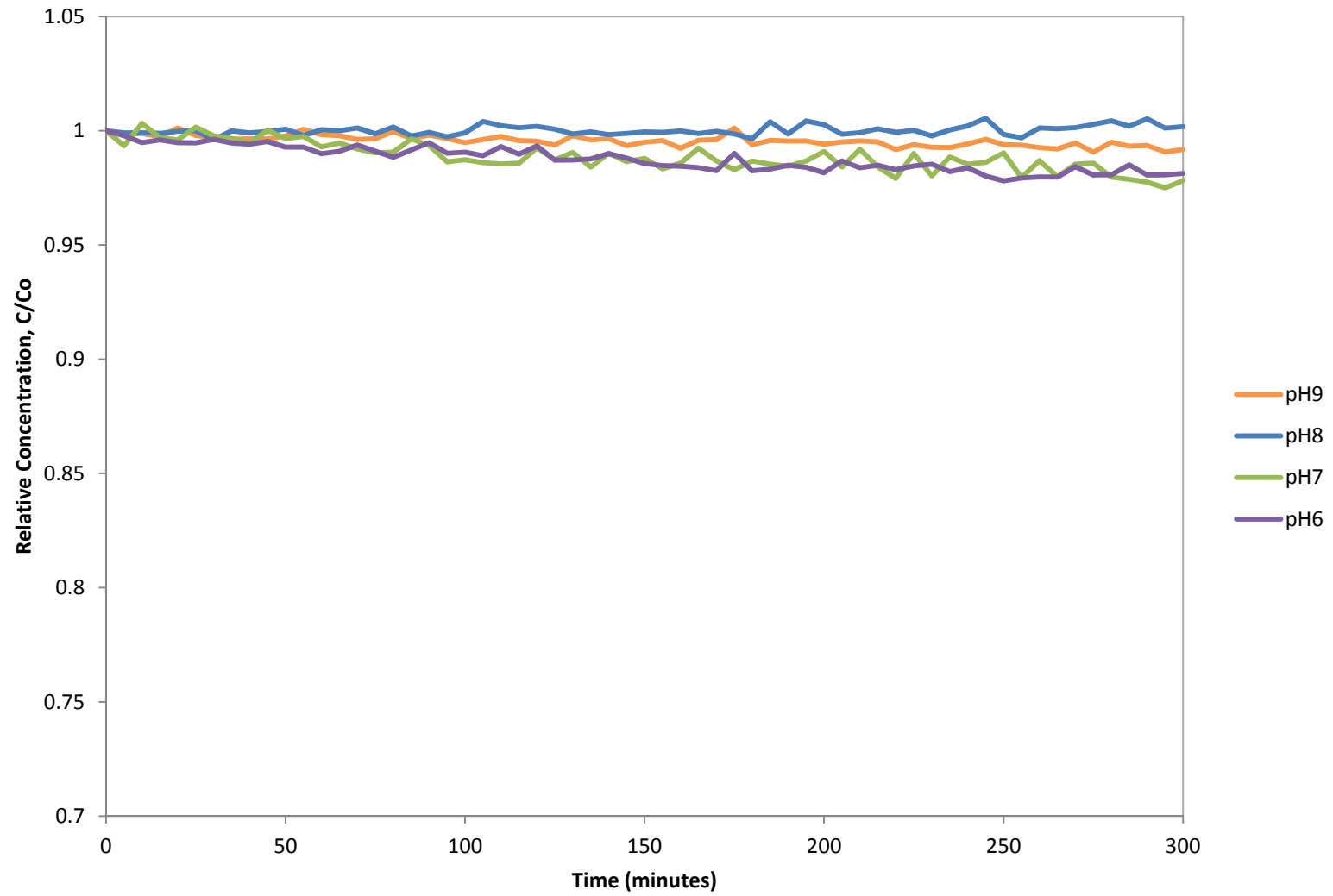
### 100% Duty Cycle: H<sub>2</sub>O<sub>2</sub> Ctrl



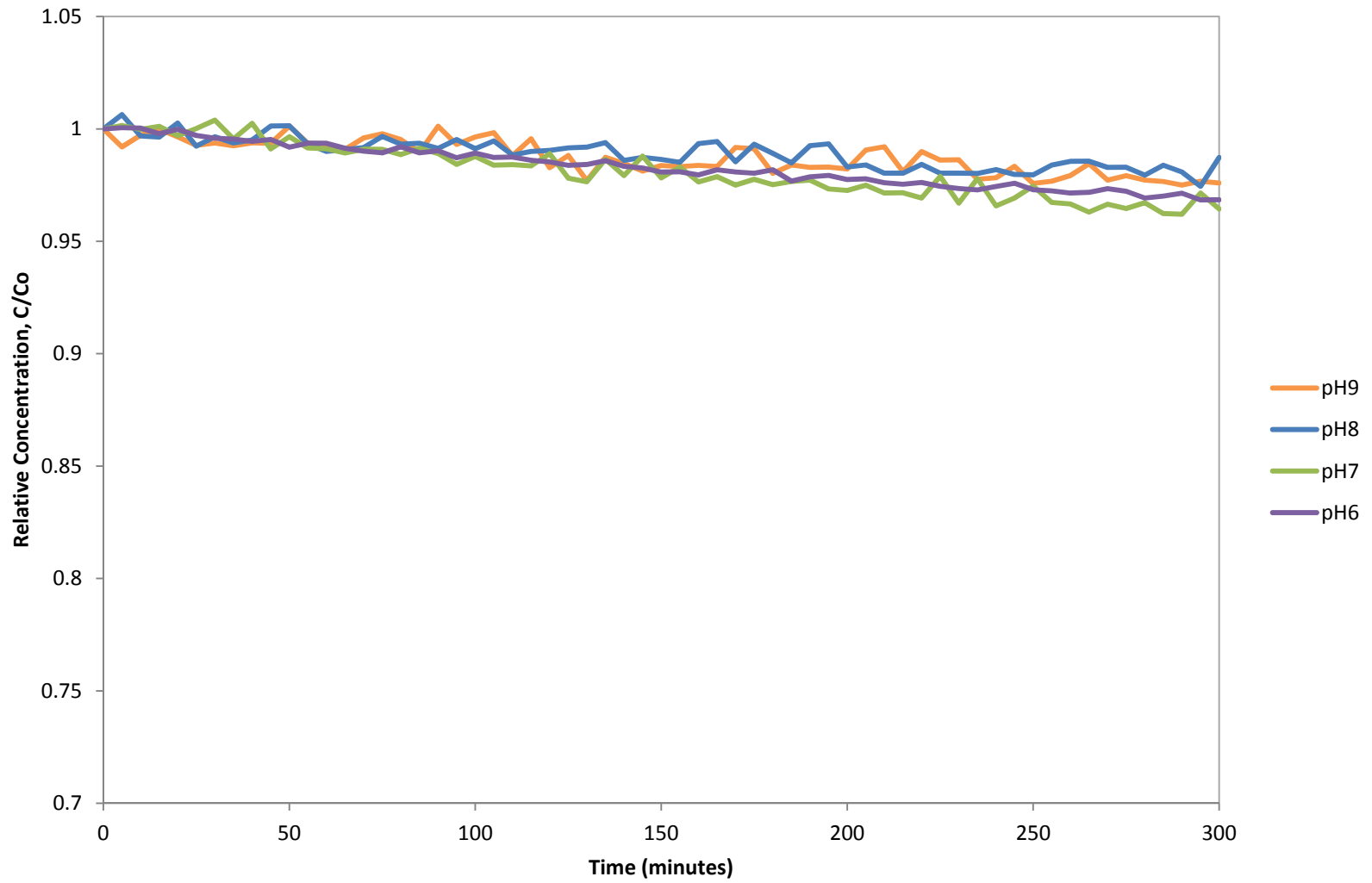
## 0% Duty Cycle



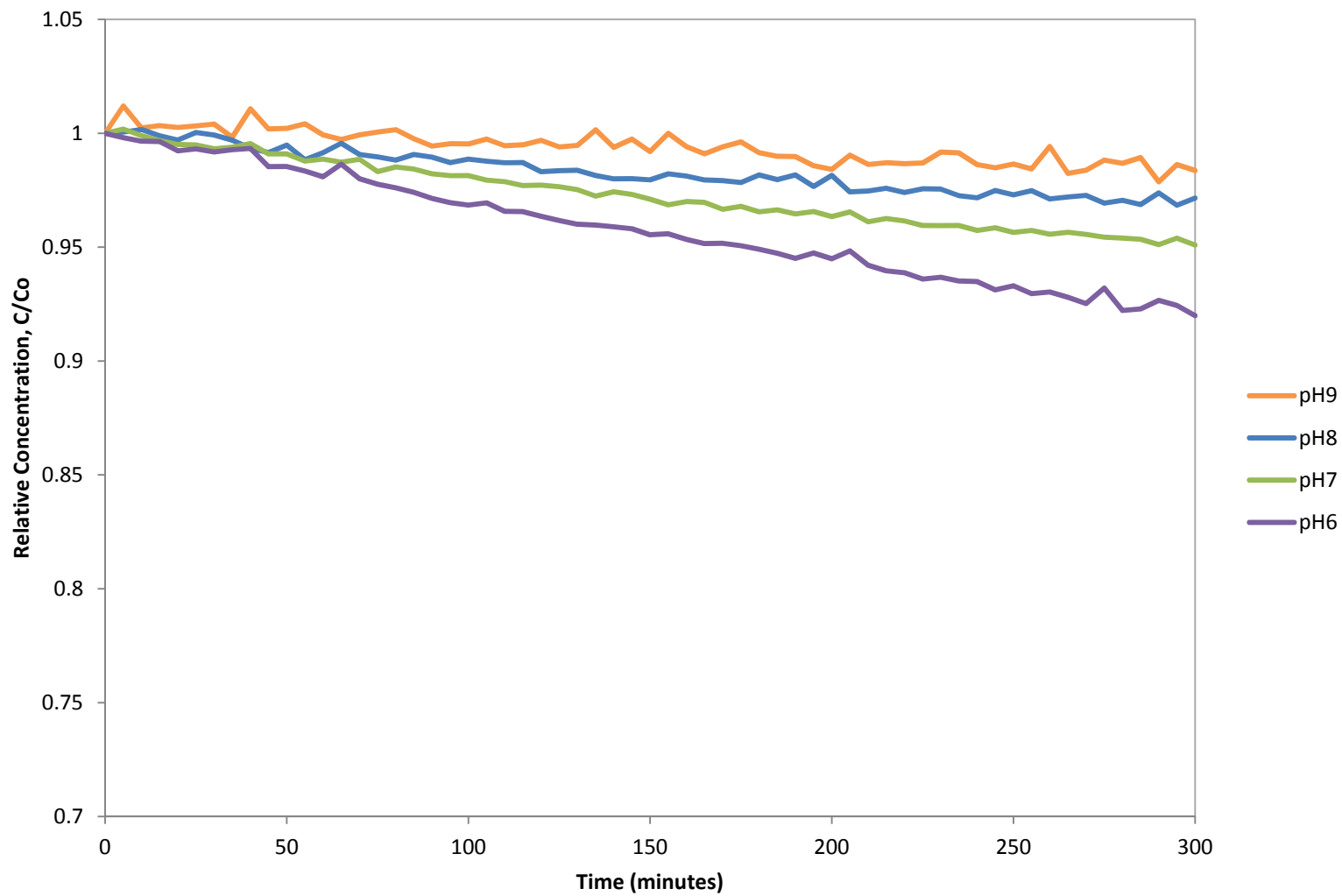
## 5% Duty Cycle



## 10% Duty Cycle

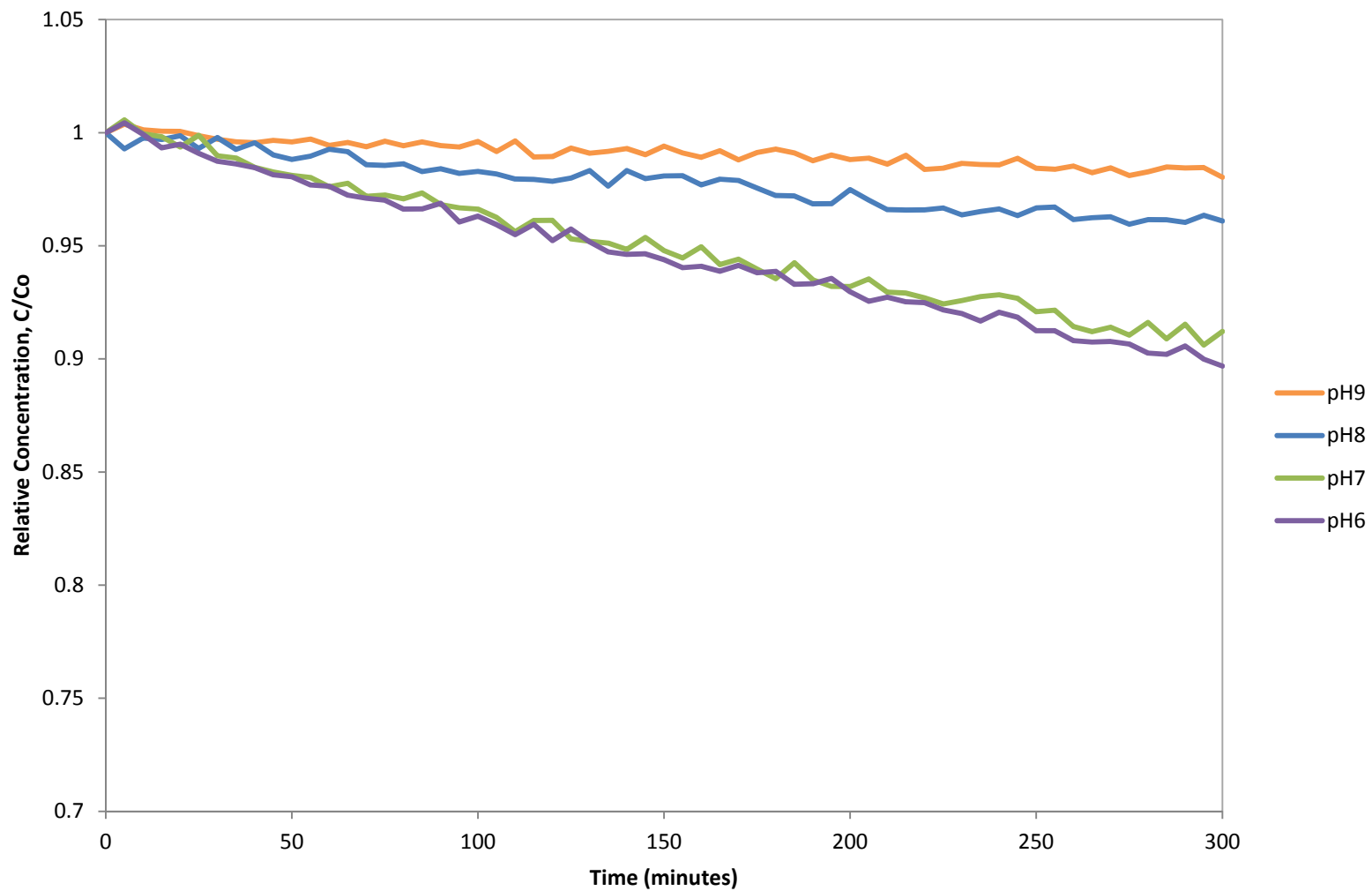


## 20% Duty Cycle

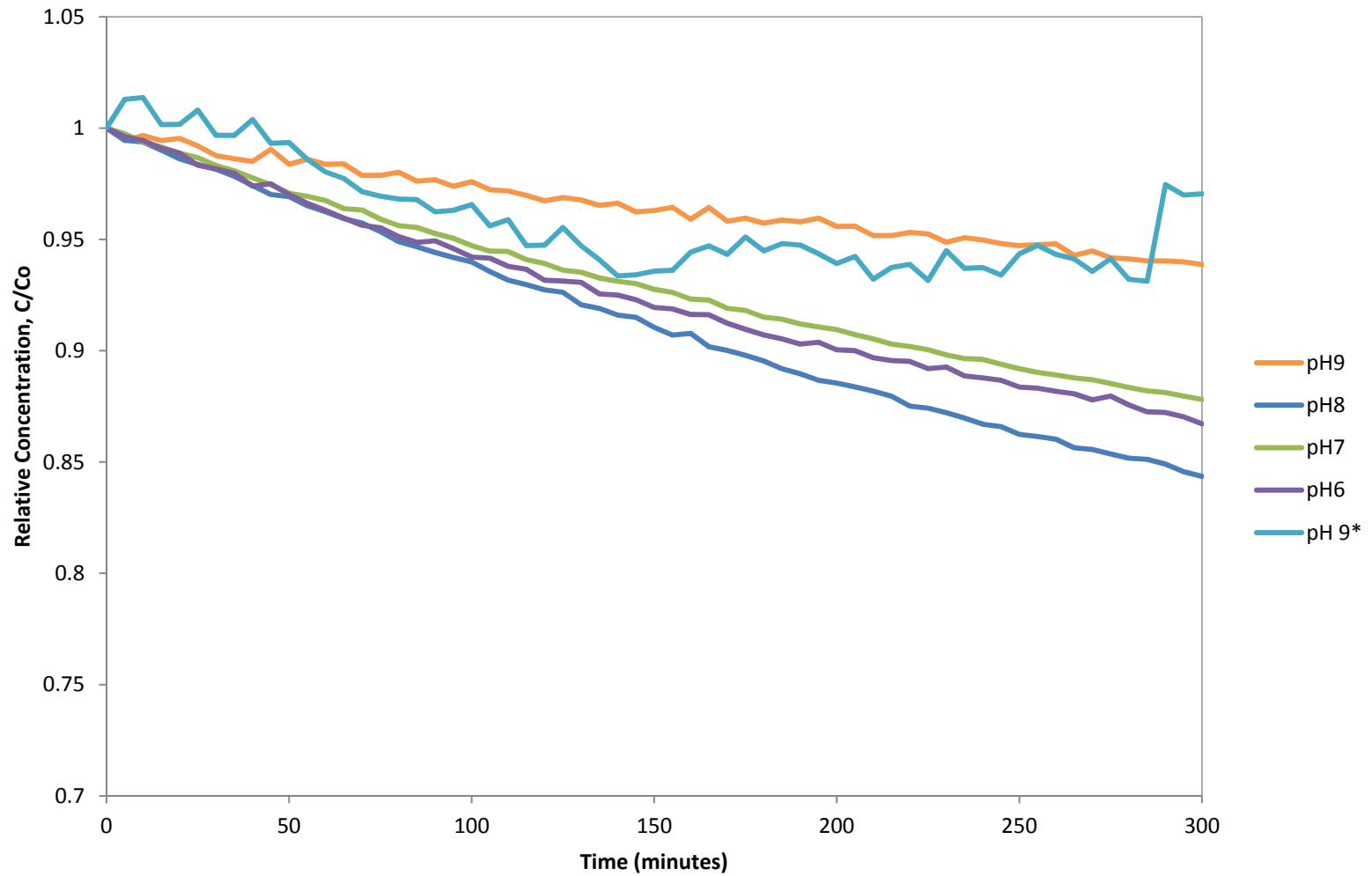




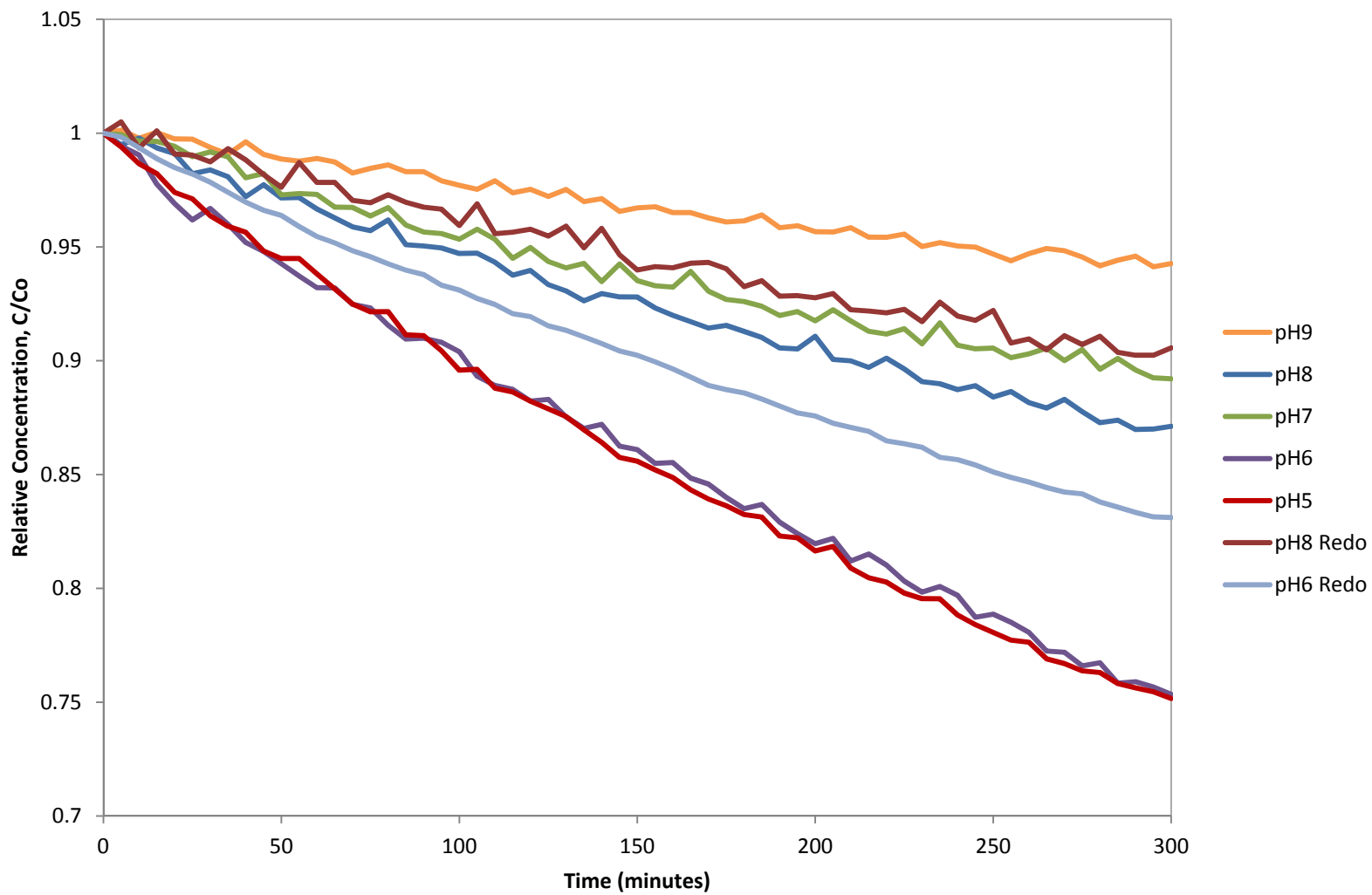
### 30% Duty Cycle



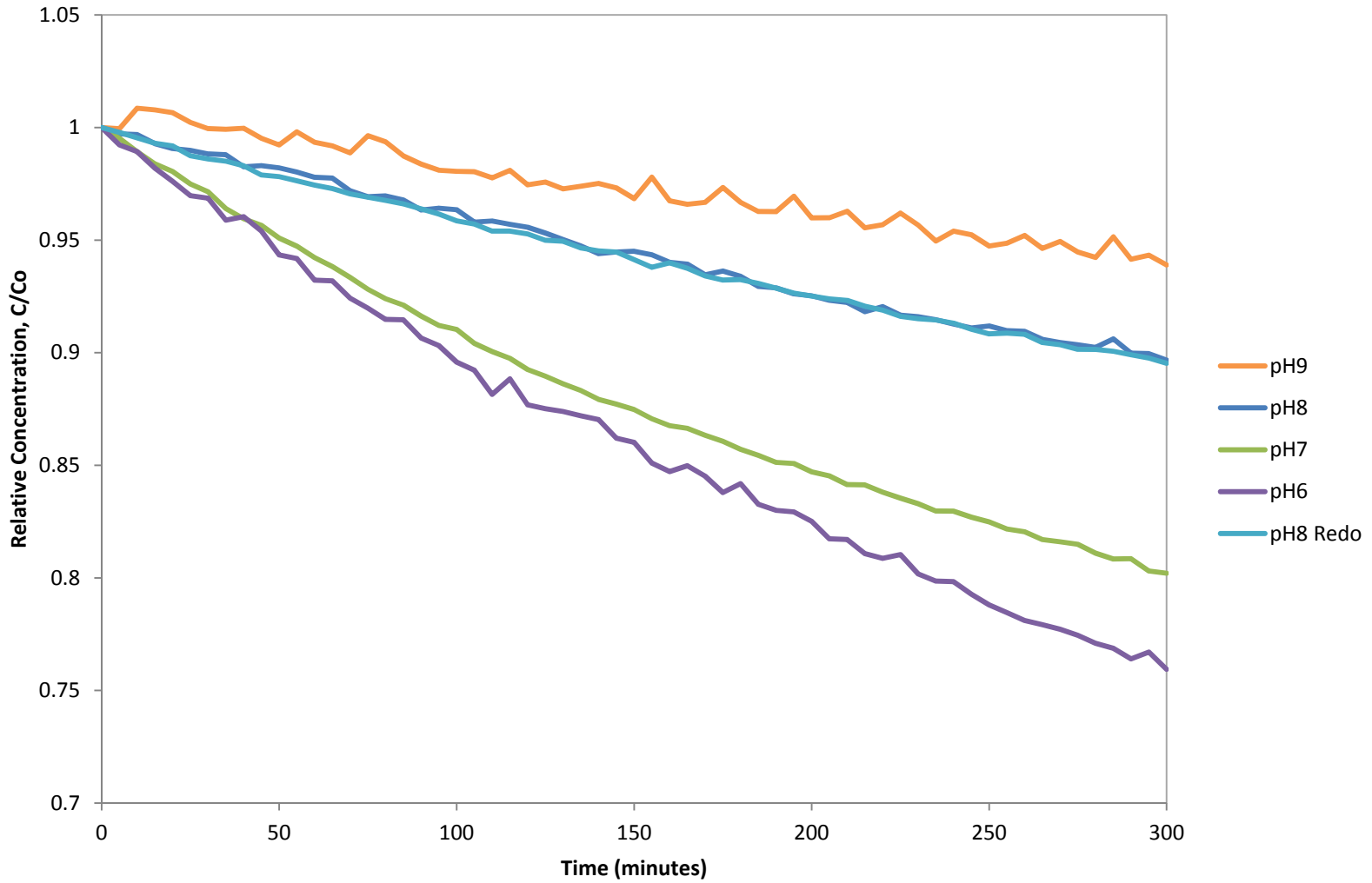
## 50% Duty Cycle



## 70% Duty Cycle



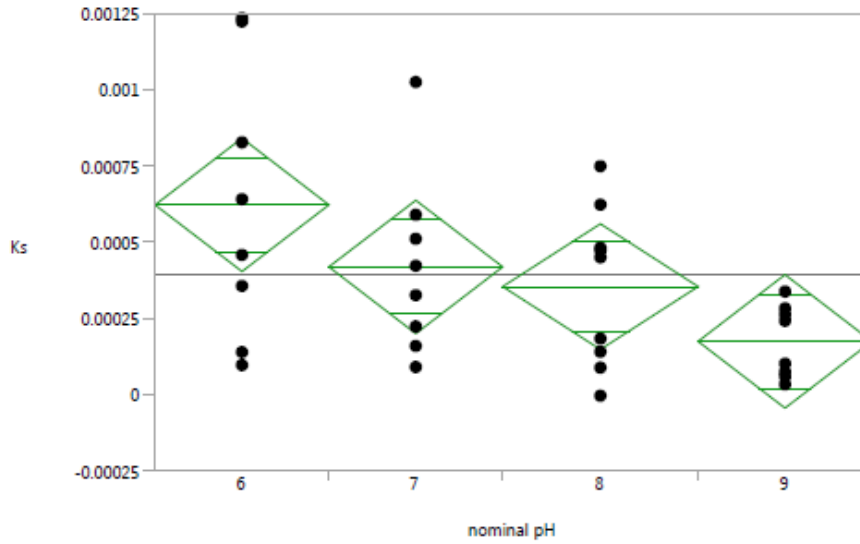
# 100% Duty Cycle



## Appendix E: AOP ANOVA and Tukey Analyses

### Fit Group

#### Oneway Analysis of Ks By nominal pH



Excluded Rows 9

#### Oneway Anova

##### Summary of Fit

Rsquare	0.236317
Adj Rsquare	0.157315
Root Mean Square Error	0.000302
Mean of Response	0.000391
Observations (or Sum Wgts)	33

##### Analysis of Variance

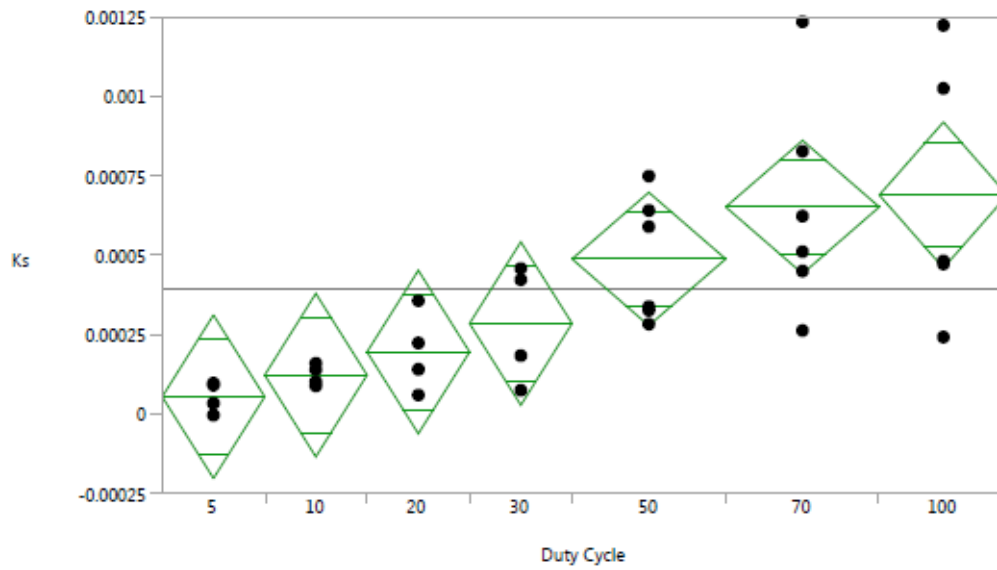
Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F
nominal pH	3	8.20585e-7	2.7353e-7	2.9913	0.0471*
Error	29	2.65181e-6	9.1442e-8		
C. Total	32	3.47239e-6			

##### Means for Oneway Anova

Level	Number	Mean	Std Error	Lower 95%	Upper 95%
6	8	0.000622	0.00011	0.0004	0.00084
7	8	0.000418	0.00011	0.0002	0.00064
8	9	0.000354	0.00010	0.00015	0.00056
9	8	0.000174	0.00011	-4.4e-5	0.00039

Std Error uses a pooled estimate of error variance

### Oneway Analysis of Ks By Duty Cycle



Excluded Rows 9

### Oneway Anova

#### Summary of Fit

Rsquare	0.532025
Adj Rsquare	0.424031
Root Mean Square Error	0.00025
Mean of Response	0.000391
Observations (or Sum Wgts)	33

#### Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F
Duty Cycle	6	1.8474e-6	3.079e-7	4.9264	0.0017*
Error	26	1.62499e-6	6.25e-8		
C. Total	32	3.47239e-6			

#### Means for Oneway Anova

Level	Number	Mean	Std Error	Lower 95%	Upper 95%
5	4	0.000054	0.00012	-0.0002	0.00031
10	4	0.000122	0.00012	-0.0001	0.00038
20	4	0.000195	0.00012	-0.0001	0.00045
30	4	0.000285	0.00012	2.78e-5	0.00054
50	6	0.000488	0.00010	0.00028	0.00070
70	6	0.000651	0.00010	0.00044	0.00086
100	5	0.000689	0.00011	0.00046	0.00092

Std Error uses a pooled estimate of error variance

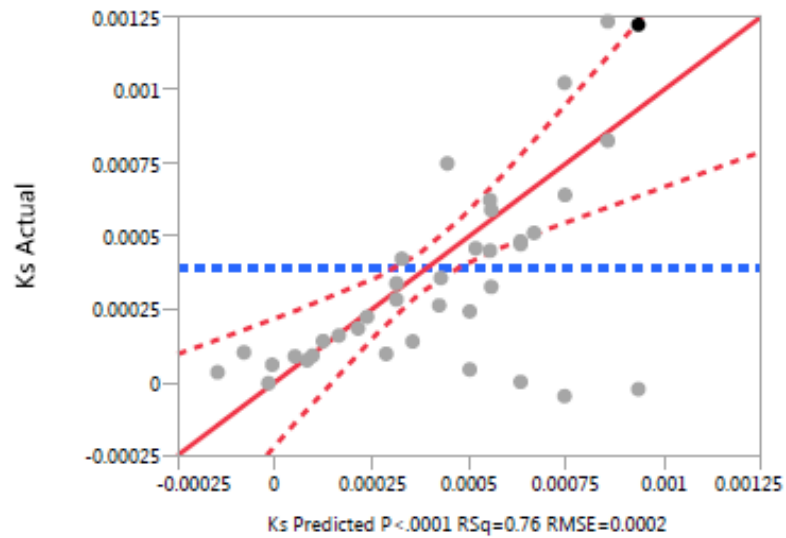
## Response Ks

### Whole Model

### Effect Summary

Source	LogWorth	PValue
Duty Cycle	4.234	0.00006
nominal pH	2.963	0.00109

### Actual by Predicted Plot



### Summary of Fit

RSquare	0.764249
RSquare Adj	0.671999
Root Mean Square Error	0.000189
Mean of Response	0.000391
Observations (or Sum Wgts)	33

### Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	9	2.65377e-6	2.9486e-7	8.2845
Error	23	8.18619e-7	3.5592e-8	Prob > F
C. Total	32	3.47239e-6		<.0001*

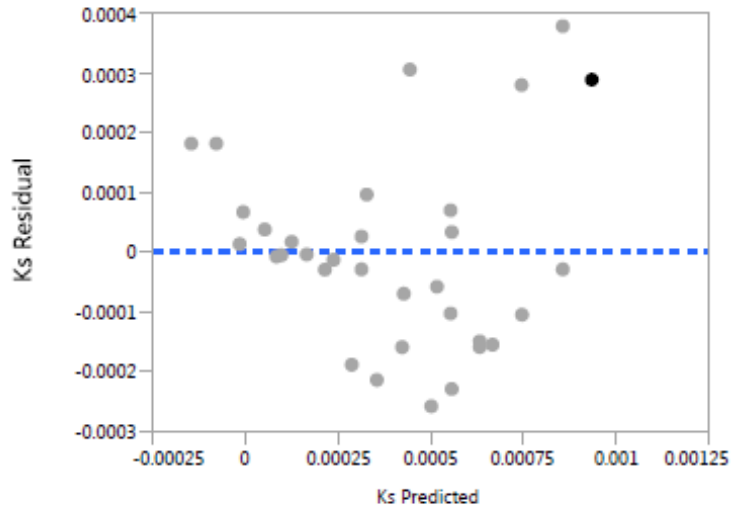
### Effect Tests

Source	Nparm	DF	Sum of Squares	F Ratio	Prob > F
nominal pH	3	3	8.06372e-7	7.5520	0.0011*
Duty Cycle	6	6	1.83319e-6	8.5842	<.0001*

**Response Ks**

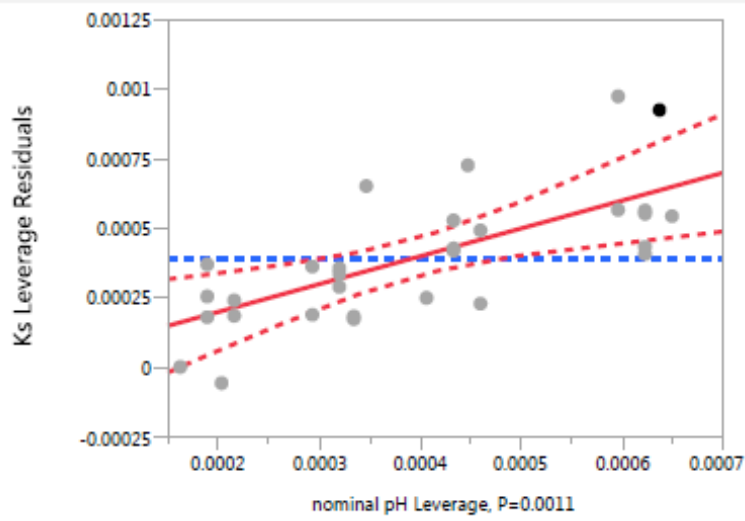
**Whole Model**

**Residual by Predicted Plot**



**nominal pH**

**Leverage Plot**



**Least Squares Means Table**

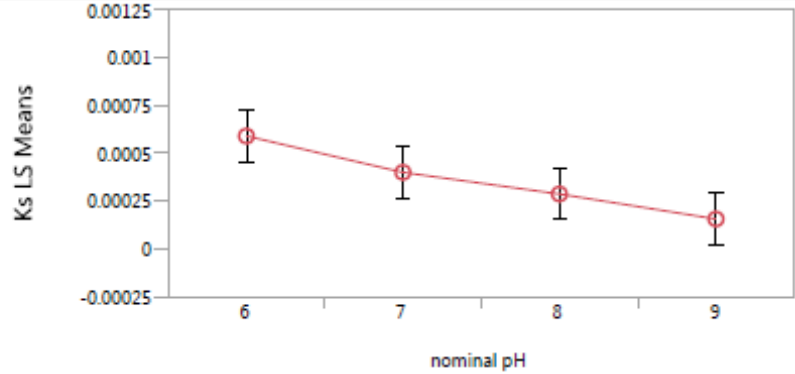
Level	Least Sq Mean	Std Error	Mean
6	0.00058861	0.00006734	0.000622
7	0.00039879	0.00006734	0.000418
8	0.00028569	0.00006389	0.000354
9	0.00015480	0.00006734	0.000174



**Response Ks**

**nominal pH**

**LS Means Plot**



**LSMeans Differences Tukey HSD**

$\alpha = 0.050$   $Q = 2.76731$

	LSMean[j]			
Mean[i]-Mean[j]	6	7	8	9
Std Err Dif				
Lower CL Dif				
Upper CL Dif				
6	0	0.00019	0.0003	0.00043
	0	0.0001	9.21e-5	0.0001
	0	-0.0001	4.8e-5	0.00017
	0	0.00045	0.00056	0.0007
7	-0.0002	0	0.00011	0.00024
	0.0001	0	9.31e-5	9.43e-5
	-0.0005	0	-0.0001	-1.7e-5
	7.4e-5	0	0.00037	0.00051
8	-0.0003	-0.0001	0	0.00013
	9.21e-5	9.31e-5	0	9.31e-5
	-0.0006	-0.0004	0	-0.0001
	-4.8e-5	0.00014	0	0.00039
9	-0.0004	-0.0002	-0.0001	0
	0.0001	9.43e-5	9.31e-5	0
	-0.0007	-0.0005	-0.0004	0
	-0.0002	1.7e-5	0.00013	0

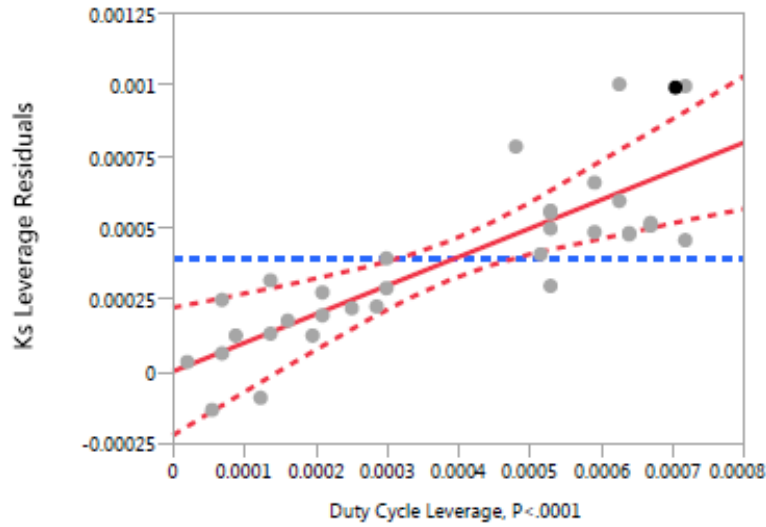
Level		Least Sq Mean
6	A	0.00058861
7	A B	0.00039879
8	B	0.00028569
9	B	0.00015480

Levels not connected by same letter are significantly different.

**Response Ks**

**Duty Cycle**

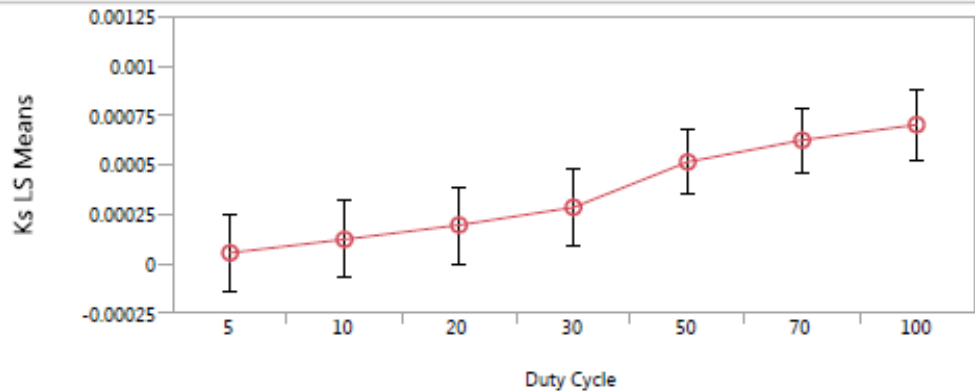
**Leverage Plot**



**Least Squares Means Table**

Level	Least Sq Mean	Std Error	Mean
5	0.00005441	0.00009433	0.000054
10	0.00012229	0.00009433	0.000122
20	0.00019506	0.00009433	0.000195
30	0.00028475	0.00009433	0.000285
50	0.00051448	0.00007783	0.000488
70	0.00062462	0.00007783	0.000651
100	0.00070319	0.00008511	0.000689

**LS Means Plot**



**LSMeans Differences Tukey HSD**

$\alpha = 0.050$   $Q = 3.22319$

Response Ks

Duty Cycle

LSMeans Differences Tukey HSD

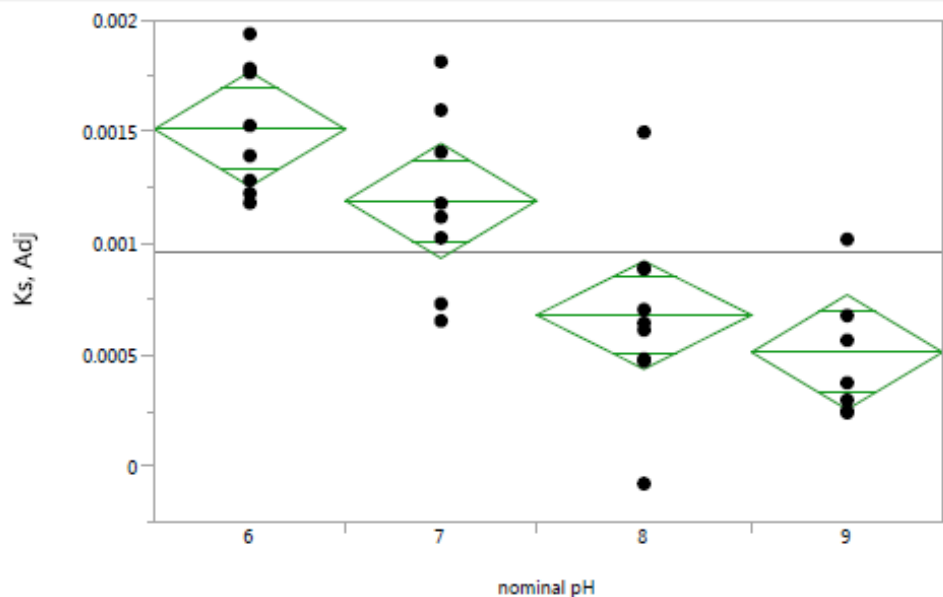
		LSMean[j]						
Mean[i]-Mean[j]		5	10	20	30	50	70	100
Std Err Dif								
Lower CL Dif								
Upper CL Dif								
LSMean[i]	5	0	-0.0001	-0.0001	-0.0002	-0.0005	-0.0006	-0.0006
		0	0.00013	0.00013	0.00013	0.00012	0.00012	0.00013
		0	-0.0005	-0.0006	-0.0007	-0.0009	-0.001	-0.0011
		0	0.00036	0.00029	0.0002	-0.0001	-0.0002	-0.0002
	10	6.79e-5	0	-0.0001	-0.0002	-0.0004	-0.0005	-0.0006
		0.00013	0	0.00013	0.00013	0.00012	0.00012	0.00013
		-0.0004	0	-0.0005	-0.0006	-0.0008	-0.0009	-0.001
		0.0005	0	0.00036	0.00027	1.98e-6	-0.0001	-0.0002
	20	0.00014	7.28e-5	0	-0.0001	-0.0003	-0.0004	-0.0005
		0.00013	0.00013	0	0.00013	0.00012	0.00012	0.00013
		-0.0003	-0.0004	0	-0.0005	-0.0007	-0.0008	-0.0009
		0.00057	0.0005	0	0.00034	7.48e-5	-3.5e-5	-0.0001
	30	0.00023	0.00016	0.00009	0	-0.0002	-0.0003	-0.0004
		0.00013	0.00013	0.00013	0	0.00012	0.00012	0.00013
		-0.0002	-0.0003	-0.0003	0	-0.0006	-0.0007	-0.0008
		0.00066	0.00059	0.00052	0	0.00016	5.43e-5	-8.9e-6
	50	0.00046	0.00039	0.00032	0.00023	0	-0.0001	-0.0002
		0.00012	0.00012	0.00012	0.00012	0	0.00011	0.00012
		6.59e-5	-2e-6	-0.0001	-0.0002	0	-0.0005	-0.0006
		0.00085	0.00079	0.00071	0.00062	0	0.00025	0.00019
	70	0.00057	0.0005	0.00043	0.00034	0.00011	0	-0.0001
		0.00012	0.00012	0.00012	0.00012	0.00011	0	0.00011
		0.00018	0.00011	3.54e-5	-0.0001	-0.0002	0	-0.0004
		0.00096	0.0009	0.00082	0.00073	0.00047	0	0.00029
	100	0.00065	0.00058	0.00051	0.00042	0.00019	7.86e-5	0
		0.00013	0.00013	0.00013	0.00013	0.00012	0.00011	0
		0.00024	0.00017	0.0001	8.92e-6	-0.0002	-0.0003	0
		0.00106	0.00099	0.00092	0.00083	0.00056	0.00045	0

Level	Least Sq Mean
100 A	0.00070319
70 A B	0.00062462
50 A B C	0.00051448
30 B C D	0.00028475
20 C D	0.00019506
10 C D	0.00012229
5 D	0.00005441

Levels not connected by same letter are significantly different.

**Fit Group**

**Oneway Analysis of Ks, Adj By nominal pH**



Excluded Rows 9

**Oneway Anova**

**Summary of Fit**

Rsquare	0.586179
Adj Rsquare	0.54337
Root Mean Square Error	0.000355
Mean of Response	0.000964
Observations (or Sum Wgts)	33

**Analysis of Variance**

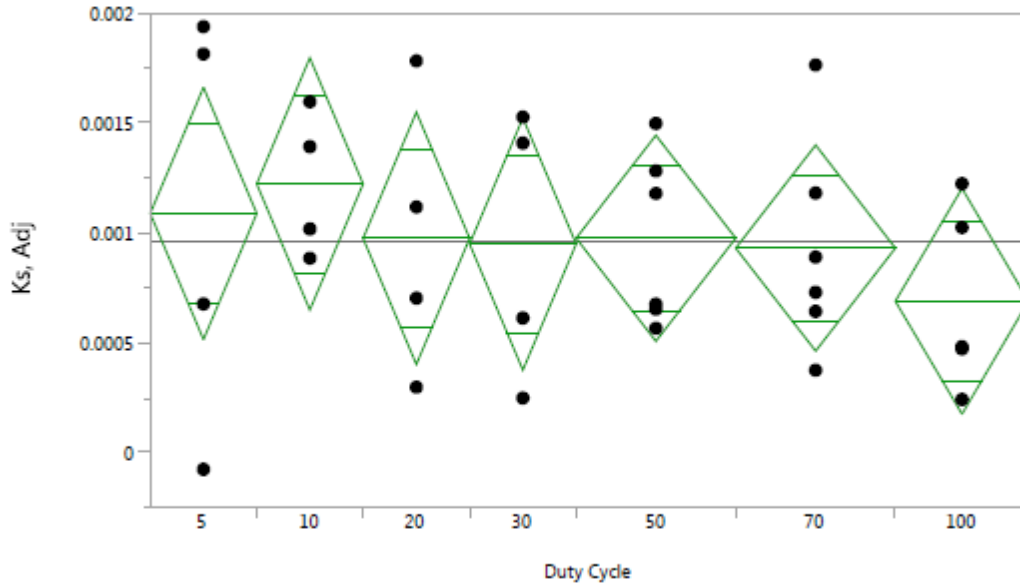
Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F
nominal pH	3	5.1671e-6	1.7224e-6	13.6929	<.0001*
Error	29	3.64778e-6	1.2579e-7		
C. Total	32	8.81488e-6			

**Means for Oneway Anova**

Level	Number	Mean	Std Error	Lower 95%	Upper 95%
6	8	0.001511	0.00013	0.00125	0.00177
7	8	0.001190	0.00013	0.00093	0.00145
8	9	0.000679	0.00012	0.00044	0.00092
9	8	0.000513	0.00013	0.00026	0.00077

Std Error uses a pooled estimate of error variance

### Oneway Analysis of Ks, Adj By Duty Cycle



Excluded Rows 9

### Oneway Anova

#### Summary of Fit

Rsquare	0.081336
Adj Rsquare	-0.13066
Root Mean Square Error	0.000558
Mean of Response	0.000964
Observations (or Sum Wgts)	33

#### Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F
Duty Cycle	6	7.16966e-7	1.1949e-7	0.3837	0.8827
Error	26	8.09791e-6	3.1146e-7		
C. Total	32	8.81488e-6			

#### Means for Oneway Anova

Level	Number	Mean	Std Error	Lower 95%	Upper 95%
5	4	0.001088	0.00028	0.00051	0.00166
10	4	0.001223	0.00028	0.00065	0.00180
20	4	0.000975	0.00028	0.00040	0.00155
30	4	0.000949	0.00028	0.00038	0.00152
50	6	0.000975	0.00023	0.00051	0.00144
70	6	0.000930	0.00023	0.00046	0.00140
100	5	0.000689	0.00025	0.00018	0.00120

Std Error uses a pooled estimate of error variance

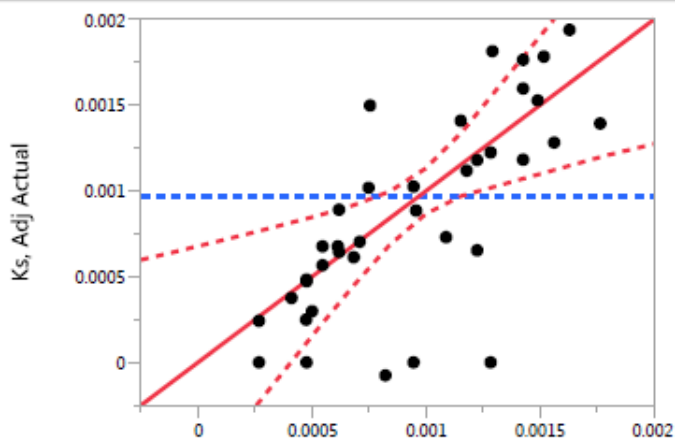
**Response Ks, Adj**

**Whole Model**

**Effect Summary**

Source	LogWorth	PValue
nominal pH	4.410	0.00004
Duty Cycle	0.230	0.58932

**Actual by Predicted Plot**



Ks, Adj Predicted P=0.001 RSq=0.66 RMSE=0.0004

**Summary of Fit**

RSquare	0.656642
RSquare Adj	0.522285
Root Mean Square Error	0.000363
Mean of Response	0.000964
Observations (or Sum Wgts)	33

**Analysis of Variance**

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	9	5.78022e-6	6.4314e-7	4.8873
Error	23	3.02666e-6	1.3159e-7	Prob > F
C. Total	32	8.81488e-6		0.0010*

**Lack Of Fit**

Source	DF	Sum of Squares	Mean Square	F Ratio
Lack Of Fit	18	2.68198e-6	1.49e-7	2.1614
Pure Error	5	3.44676e-7	6.8935e-8	Prob > F
Total Error	23	3.02666e-6		0.2012

Max RSq  
0.9609

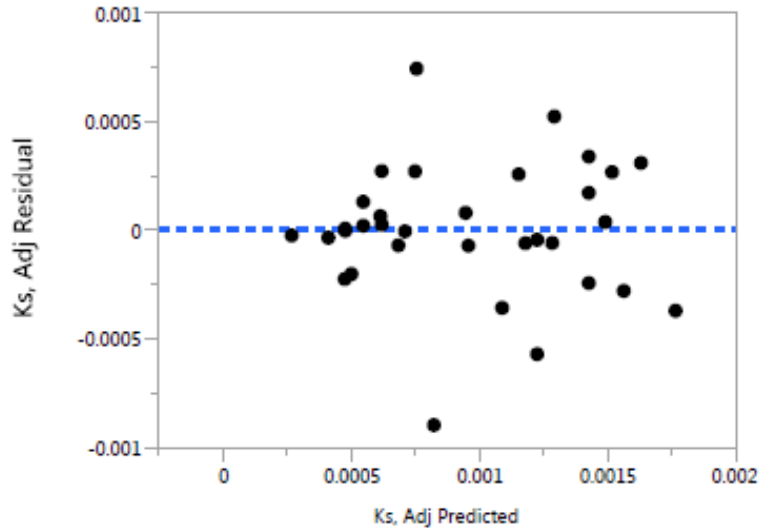
**Effect Tests**

Source	Nparm	DF	Sum of Squares	F Ratio	Prob > F
nominal pH	3	3	5.07126e-6	12.8457	<.0001*
Duty Cycle	6	6	6.21125e-7	0.7867	0.5893

Response Ks, Adj

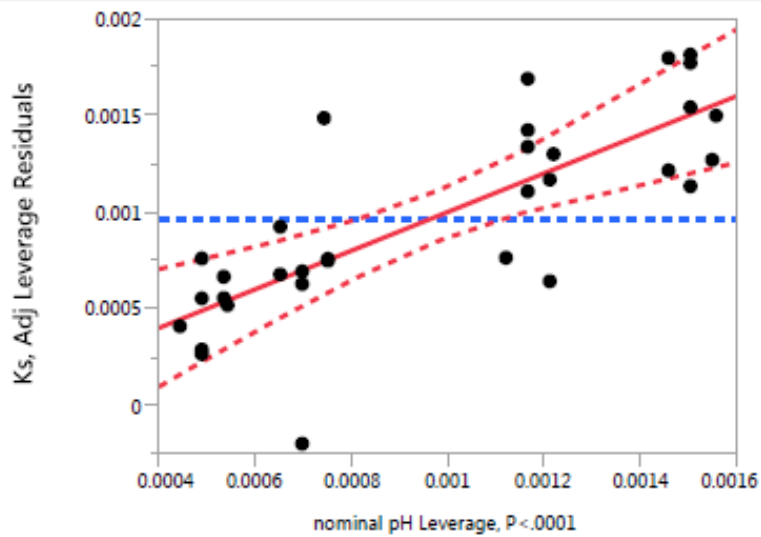
Whole Model

Residual by Predicted Plot



nominal pH

Leverage Plot



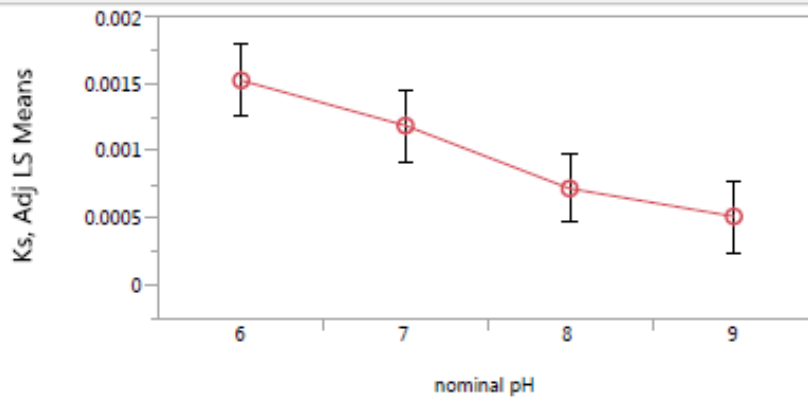
Least Squares Means Table

Level	Least Sq Mean	Std Error	Mean
6	0.00152352	0.00012948	0.001511
7	0.00118562	0.00012949	0.001190
8	0.00071648	0.00012286	0.000679
9	0.00050797	0.00012949	0.000513

**Response Ks, Adj**

nominal pH

**LS Means Plot**



**LSMeans Differences Tukey HSD**

$\alpha = 0.050$   $Q = 2.76731$

		LSMean[j]			
Mean[i]-Mean[j]		6	7	8	9
Std Err Dif					
Lower CL Dif					
Upper CL Dif					
6		0	0.00034	0.00081	0.00102
		0	0.00018	0.00018	0.00018
		0	-0.0002	0.00032	0.00051
		0	0.00085	0.0013	0.00152
7		-0.0003	0	0.00047	0.00068
		0.00018	0	0.00018	0.00018
		-0.0008	0	-2.6e-5	0.00018
		0.00017	0	0.00096	0.00118
8		-0.0008	-0.0005	0	0.00021
		0.00018	0.00018	0	0.00018
		-0.0013	-0.001	0	-0.0003
		-0.0003	2.6e-5	0	0.0007
9		-0.001	-0.0007	-0.0002	0
		0.00018	0.00018	0.00018	0
		-0.0015	-0.0012	-0.0007	0
		-0.0005	-0.0002	0.00029	0

Level		Least Sq Mean
6	A	0.00152352
7	A B	0.00118562
8	B C	0.00071648
9	C	0.00050797

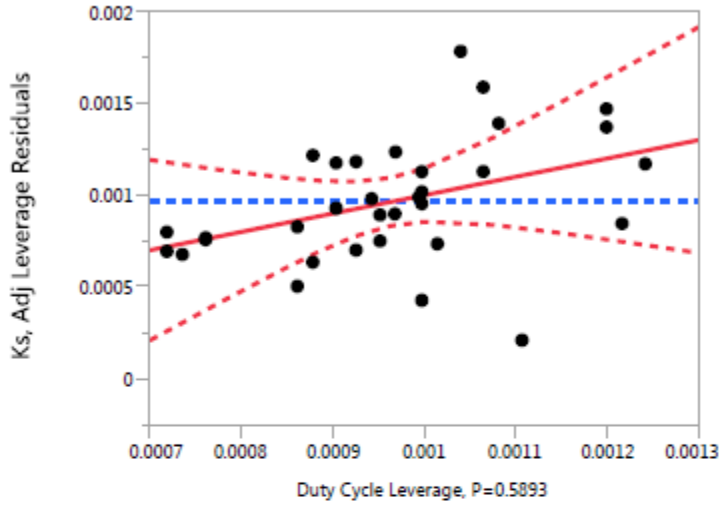
Levels not connected by same letter are significantly different.



Response Ks, Adj

Duty Cycle

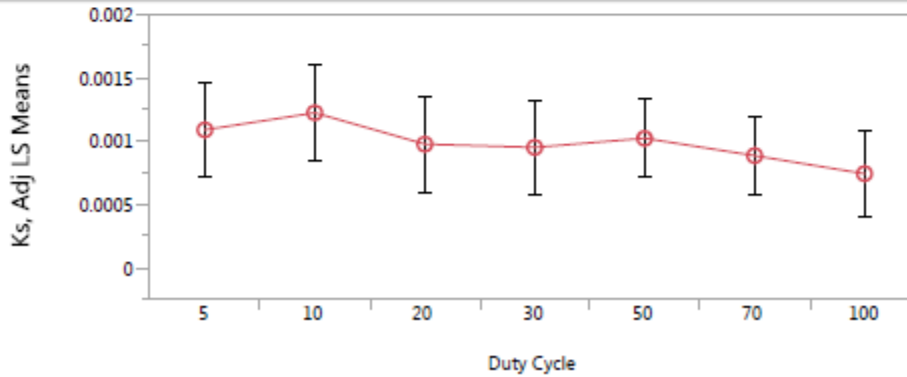
Leverage Plot



Least Squares Means Table

Level	Least Sq Mean	Std Error	Mean
5	0.00108814	0.00018138	0.001088
10	0.00122288	0.00018138	0.001223
20	0.00097531	0.00018138	0.000975
30	0.00094917	0.00018138	0.000949
50	0.00102103	0.00014966	0.000975
70	0.00088496	0.00014966	0.000930
100	0.00074230	0.00016366	0.000689

LS Means Plot



LSMeans Differences Tukey HSD

$\alpha = 0.050$   $Q = 3.22319$

Response Ks, Adj

Duty Cycle

LSMeans Differences Tukey HSD

		LSMean[j]						
Mean[i]-Mean[j]		5	10	20	30	50	70	100
Std Err Dif								
Lower CL Dif								
Upper CL Dif								
LSMean[i]	5	0	-0.0001	0.00011	0.00014	6.71e-5	0.0002	0.00035
		0	0.00026	0.00026	0.00026	0.00024	0.00024	0.00024
		0	-0.001	-0.0007	-0.0007	-0.0007	-0.0006	-0.0004
		0	0.00069	0.00094	0.00097	0.00083	0.00096	0.00113
	10	0.00013	0	0.00025	0.00027	0.0002	0.00034	0.00048
		0.00026	0	0.00026	0.00026	0.00024	0.00024	0.00024
		-0.0007	0	-0.0006	-0.0006	-0.0006	-0.0004	-0.0003
		0.00096	0	0.00107	0.0011	0.00096	0.0011	0.00127
	20	-0.0001	-0.0002	0	2.61e-5	-4.6e-5	0.00009	0.00023
		0.00026	0.00026	0	0.00026	0.00024	0.00024	0.00024
		-0.0009	-0.0011	0	-0.0008	-0.0008	-0.0007	-0.0006
		0.00071	0.00058	0	0.00085	0.00071	0.00085	0.00102
	30	-0.0001	-0.0003	-2.6e-5	0	-0.0001	6.42e-5	0.00021
		0.00026	0.00026	0.00026	0	0.00024	0.00024	0.00024
		-0.001	-0.0011	-0.0009	0	-0.0008	-0.0007	-0.0006
		0.00069	0.00055	0.0008	0	0.00069	0.00082	0.00099
	50	-0.0001	-0.0002	4.57e-5	7.19e-5	0	0.00014	0.00028
		0.00024	0.00024	0.00024	0.00024	0	0.00021	0.00022
		-0.0008	-0.001	-0.0007	-0.0007	0	-0.0006	-0.0004
		0.00069	0.00056	0.0008	0.00083	0	0.00083	0.001
	70	-0.0002	-0.0003	-0.0001	-0.0001	-0.0001	0	0.00014
		0.00024	0.00024	0.00024	0.00024	0.00021	0	0.00022
		-0.001	-0.0011	-0.0008	-0.0008	-0.0008	0	-0.0006
		0.00055	0.00042	0.00067	0.00069	0.00055	0	0.00085
	100	-0.0003	-0.0005	-0.0002	-0.0002	-0.0003	-0.0001	0
		0.00024	0.00024	0.00024	0.00024	0.00022	0.00022	0
		-0.0011	-0.0013	-0.001	-0.001	-0.001	-0.0009	0
		0.00044	0.00031	0.00055	0.00058	0.00044	0.00057	0

Level	Least Sq Mean
10	A 0.00122288
5	A 0.00108814
50	A 0.00102103
20	A 0.00097531
30	A 0.00094917
70	A 0.00088496
100	A 0.00074230

Levels not connected by same letter are significantly different.

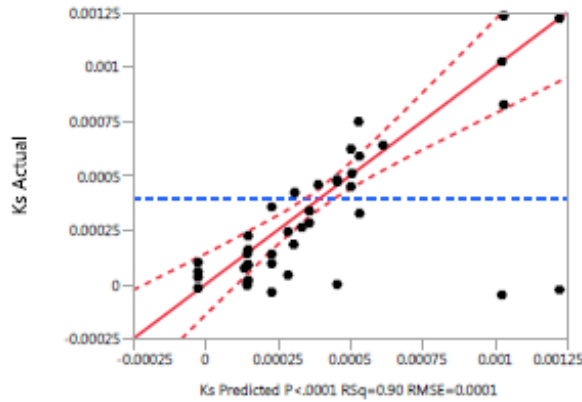
## Appendix F: AOP Regression Report

### Response Ks

#### Effect Summary

Source	LogWorth	PValue
DV DC 100	8.138	0.00000
DV DC 70	6.563	0.00000
DV DC 50	5.380	0.00000
DV pH6	3.578	0.00026
DV pH6*DV DC 100	3.489	0.00032
DV pH7*DV DC 100	2.802	0.00158
DV pH6*DV DC 70	2.681	0.00209
DV pH9	1.905	0.01245
DV DC 30	1.426	0.03747
DV pH7	0.778	0.16680

#### Actual by Predicted Plot



#### Summary of Fit

RSquare	0.899731
RSquare Adj	0.854155
Root Mean Square Error	0.000126
Mean of Response	0.000391
Observations (or Sum Wgts)	33

#### Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	10	3.12422e-6	3.1242e-7	19.7410
Error	22	3.48172e-7	1.5826e-8	<b>Prob &gt; F</b>
C. Total	32	3.47239e-6		<b>&lt;.0001*</b>

#### Parameter Estimates

Term	Estimate	Std Error	t Ratio	Prob> t	Std Beta	VIF
Intercept	7.8989e-5	5.237e-5	1.51	0.1457	0	.
DV pH9	-0.00017	6.244e-5	-2.72	<b>0.0125*</b>	0.355112	1.4702044
DV pH7	8.9044e-5	6.227e-5	1.43	0.1668	0.117639	1.485137
DV pH6	0.0002688	0.000062	4.34	<b>0.0003*</b>	0.161821	1.1717172
DV DC 30	0.0001608	7.263e-5	2.21	<b>0.0375*</b>	0.457516	1.247506
DV DC 50	0.0003848	6.342e-5	6.07	<b>&lt;.0001*</b>	0.554353	1.2731293
DV DC 70	0.0004662	0.000064	7.28	<b>&lt;.0001*</b>	0.678575	1.2353928
DV DC 100	0.0006139	6.789e-5	9.04	<b>&lt;.0001*</b>	-0.22452	1.4929043
(DV pH6-0.24242)*(DV DC 70-0.18182)	0.0004428	0.000127	3.49	<b>0.0021*</b>	0.307121	1.1433804

## Response Ks

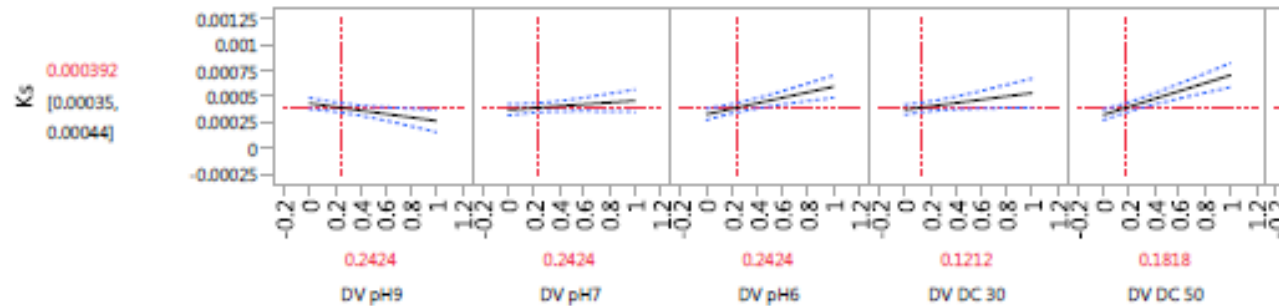
### Parameter Estimates

Term	Estimate	Std Error	t Ratio	Prob> t	Std Beta	VIF
(DV pH6-0.24242)*(DV DC 100-0.15152)	0.0006832	0.000161	4.25	0.0003*	0.245932	1.0910389
(DV pH7-0.24242)*(DV DC 100-0.15152)	0.0005658	0.000157	3.60	0.0016*	0.254353	1.0930907

### Sorted Parameter Estimates

Term	Estimate	Std Error	t Ratio	Prob> t
DV DC 100	0.0006139	6.789e-5	9.04	<.0001*
DV DC 70	0.0004662	0.000064	7.28	<.0001*
DV DC 50	0.0003848	6.342e-5	6.07	<.0001*
DV pH6	0.0002688	0.000062	4.34	0.0003*
(DV pH6-0.24242)*(DV DC 100-0.15152)	0.0006832	0.000161	4.25	0.0003*
(DV pH7-0.24242)*(DV DC 100-0.15152)	0.0005658	0.000157	3.60	0.0016*
(DV pH6-0.24242)*(DV DC 70-0.18182)	0.0004428	0.000127	3.49	0.0021*
DV pH9	-0.00017	6.244e-5	-2.72	0.0125*
DV DC 30	0.0001608	7.263e-5	2.21	0.0375*
DV pH7	8.9044e-5	6.227e-5	1.43	0.1668

### Prediction Profiler



### Durbin-Watson

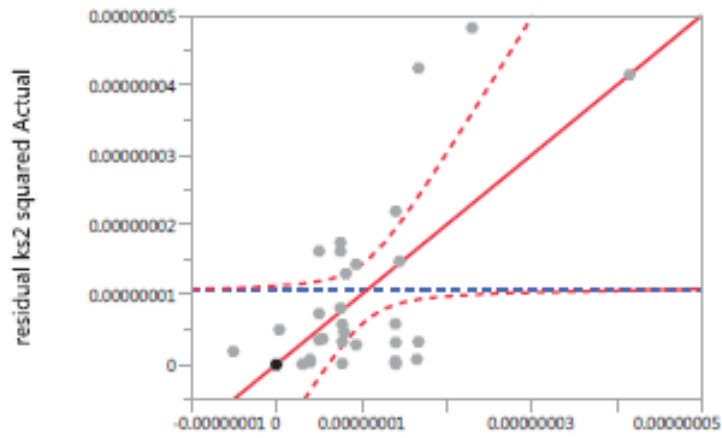
Durbin-Watson	Number of Obs.	AutoCorrelation
1.9169662	33	-0.0205

Response residual ks2 squared

Effect Summary

Source	LogWorth	PValue
DV pH6*DV DC 70	2.490	0.00323
DV pH9	0.881	0.13138
DV DC 50	0.857	0.13889
DV DC 100	0.772	0.16896
DV pH7	0.506	0.31167
DV DC 70	0.362	0.43421 ^
DV pH6*DV DC 100	0.063	0.86575
DV pH7*DV DC 100	0.059	0.87313
DV pH6	0.059	0.87344 ^
DV DC 30	0.023	0.94920

Actual by Predicted Plot



residual ks2 squared Predicted P=0.0456 RSq=0.52 RMSE=1.2e-8

Summary of Fit

RSquare	0.516492
RSquare Adj	0.296716
Root Mean Square Error	1.159e-8
Mean of Response	1.055e-8
Observations (or Sum Wgts)	33

Analysis of Variance

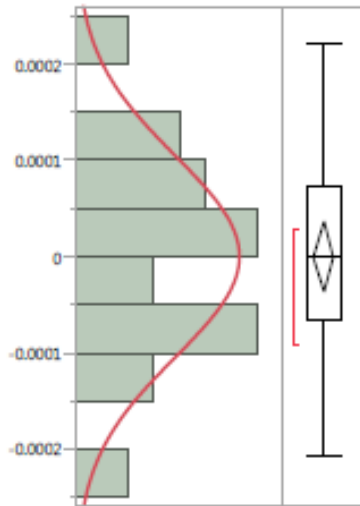
Source	DF	Sum of Squares	Mean Square	F Ratio
Model	10	3.1588e-15	3.159e-16	2.3501
Error	22	2.9571e-15	1.344e-16	Prob > F
C. Total	32	6.1159e-15		0.0456*

Lack Of Fit

Source	DF	Sum of Squares	Mean Square	F Ratio
Lack Of Fit	9	1.6727e-15	1.859e-16	1.8811
Pure Error	13	1.2844e-15	9.88e-17	Prob > F
Total Error	22	2.9571e-15		0.1456
			<b>Max RSq</b>	
				0.7900

**Distributions**

**Residual Ks 2**



Normal(-6e-20,0.0001)

**Quantiles**

100.0%	maximum	0.0002196485
99.5%		0.0002196485
97.5%		0.0002196485
90.0%		0.0001273575
75.0%	quartile	0.000071942
50.0%	median	-2.1684e-19
25.0%	quartile	-0.000065608
10.0%		-0.000141813
2.5%		-0.000206098
0.5%		-0.000206098
0.0%	minimum	-0.000206098

**Summary Statistics**

Mean	-5.91e-20
Std Dev	0.0001043
Std Err Mean	1.8158e-5
Upper 95% Mean	3.6986e-5
Lower 95% Mean	-0.000037
N	33

**Fitted Normal**

**Parameter Estimates**

Type	Parameter	Estimate	Lower 95%	Upper 95%
Location	$\mu$	-5.91e-20	-0.000037	3.6986e-5
Dispersion	$\sigma$	0.0001043	8.3884e-5	0.000138

-2log(Likelihood) = -512.448114486424

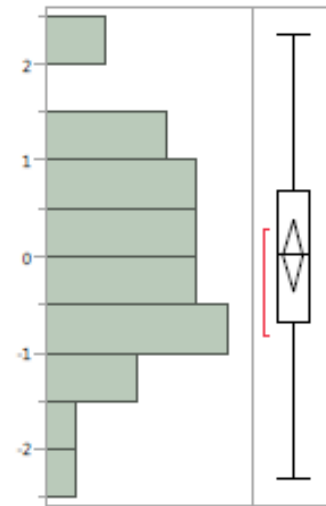
**Goodness-of-Fit Test**

Shapiro-Wilk W Test

W	Prob<W
0.985231	0.9228

Note: Ho = The data is from the Normal distribution. Small p-values reject Ho.

**Studentized Resid Ks 2**



**Quantiles**

100.0%	maximum	2.2909882697
99.5%		2.2909882697
97.5%		2.2909882697
90.0%		1.1484072446
75.0%	quartile	0.6903684223
50.0%	median	0.0211334525
25.0%	quartile	-0.673318889
10.0%		-1.276097008
2.5%		-2.29098827
0.5%		-2.29098827
0.0%	minimum	-2.29098827

**Summary Statistics**

Mean	0.0005882
Std Dev	1.0381169
Std Err Mean	0.1835149
Upper 95% Mean	0.3748693
Lower 95% Mean	-0.373693
N	32

Breusch Pagan Test

Interact Two file in L Drive

N (sample size)  
dof (explained)  
Sum Sqrs Error (SSE)  
Sum Sqrs Regression (SSR)

User Defined
33
10
3.48E-07
3.16E-15

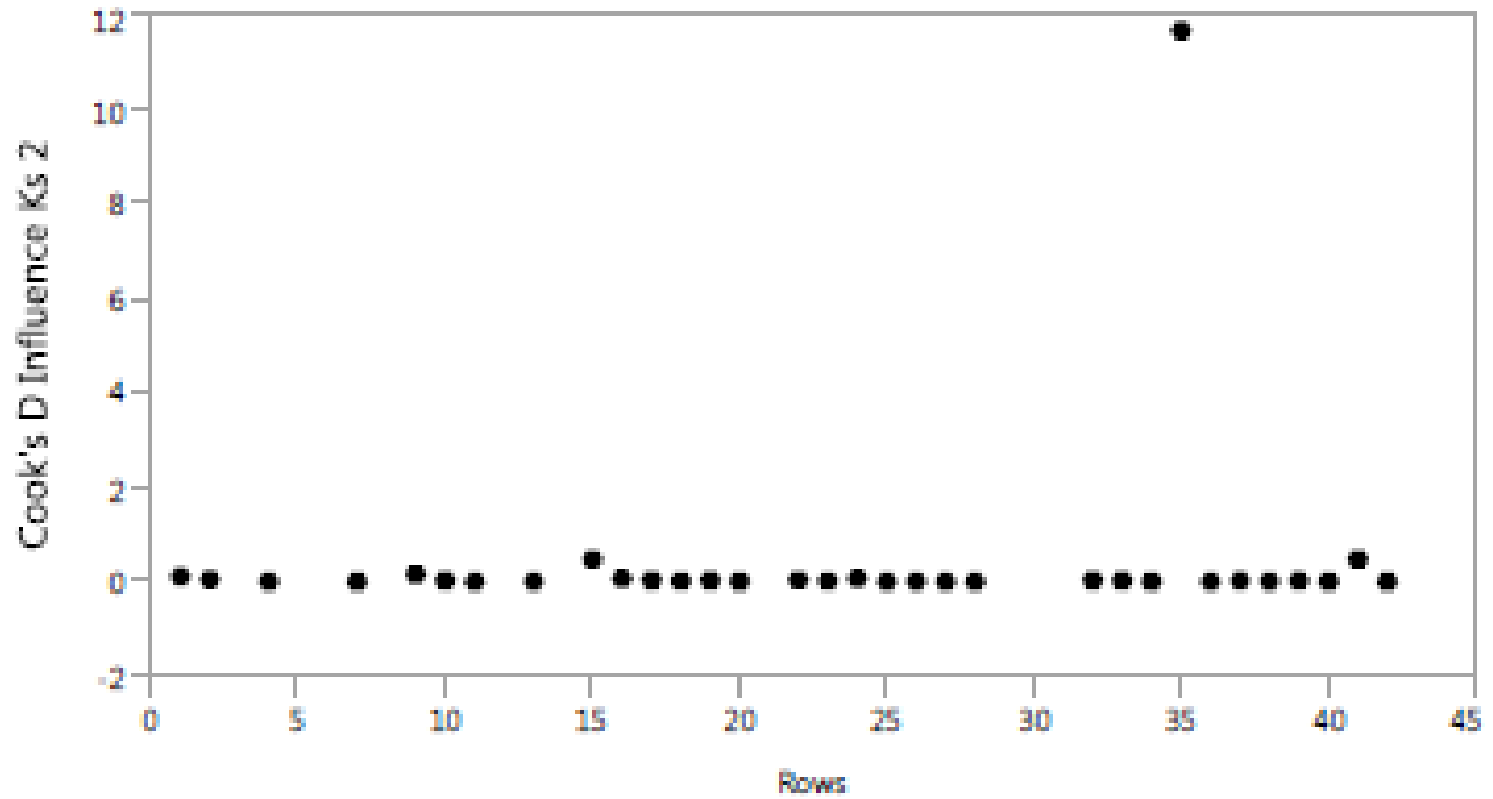
Test Statistic  
P-Value

Computer Calculates
14.18836424
0.164571822

assumption constant variance  
compare w/ $\alpha = 0.05$   
fail to reject upholds assumption of constant variance

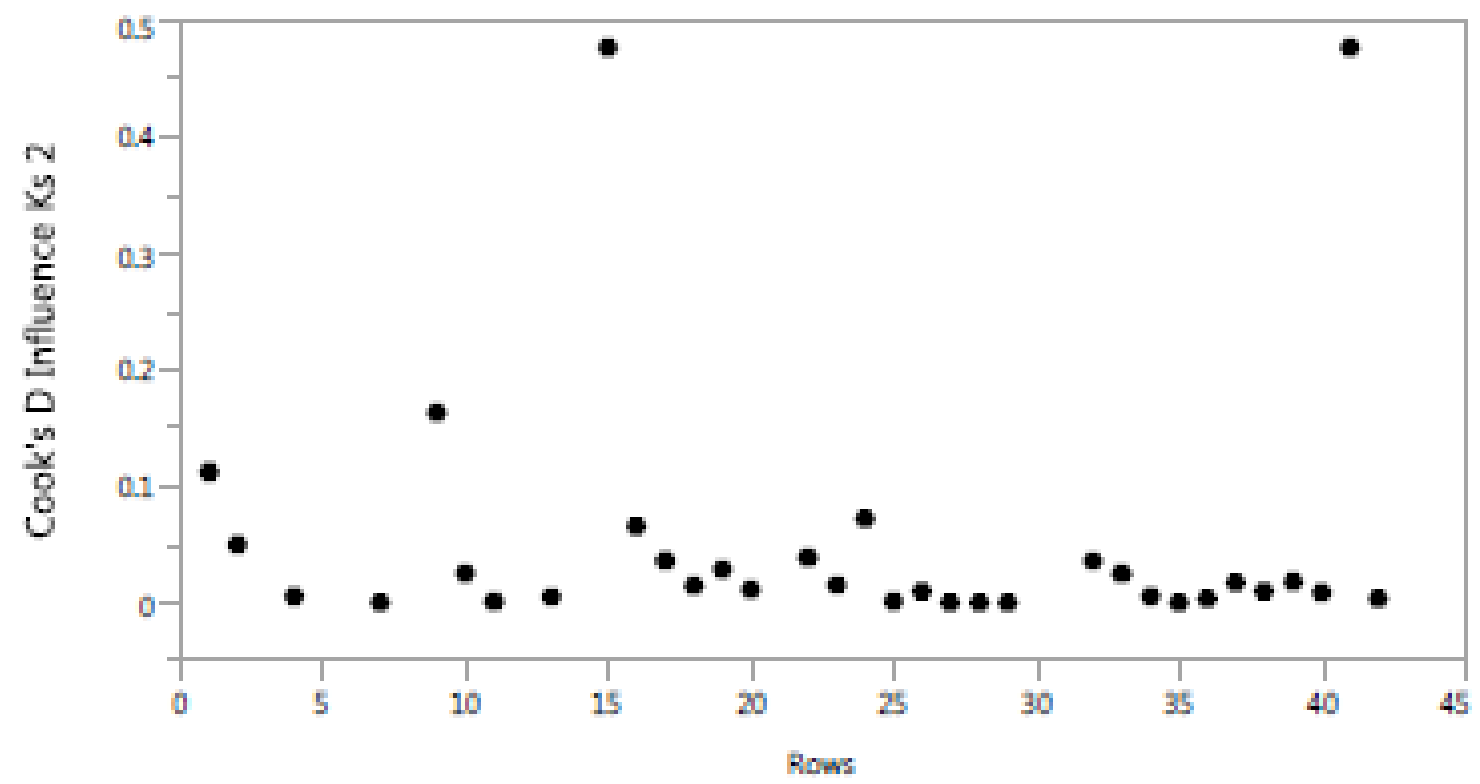
Result - Computer Calculated
GOOD - Constant Variance

### Overlay Plot



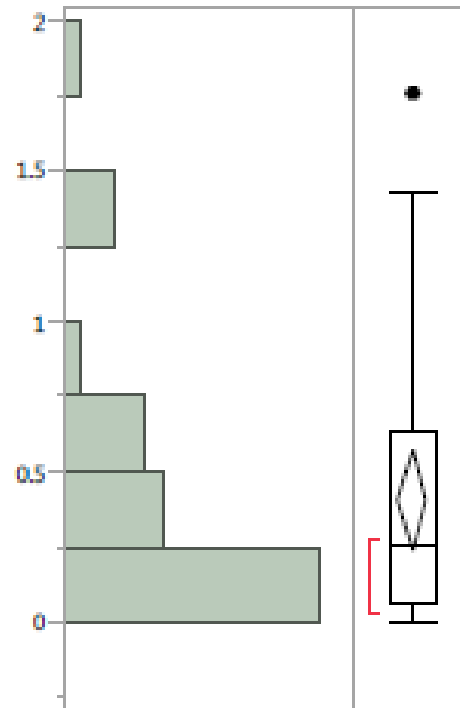


### Overlay Plot



## Distributions

### Model 2 APE Score



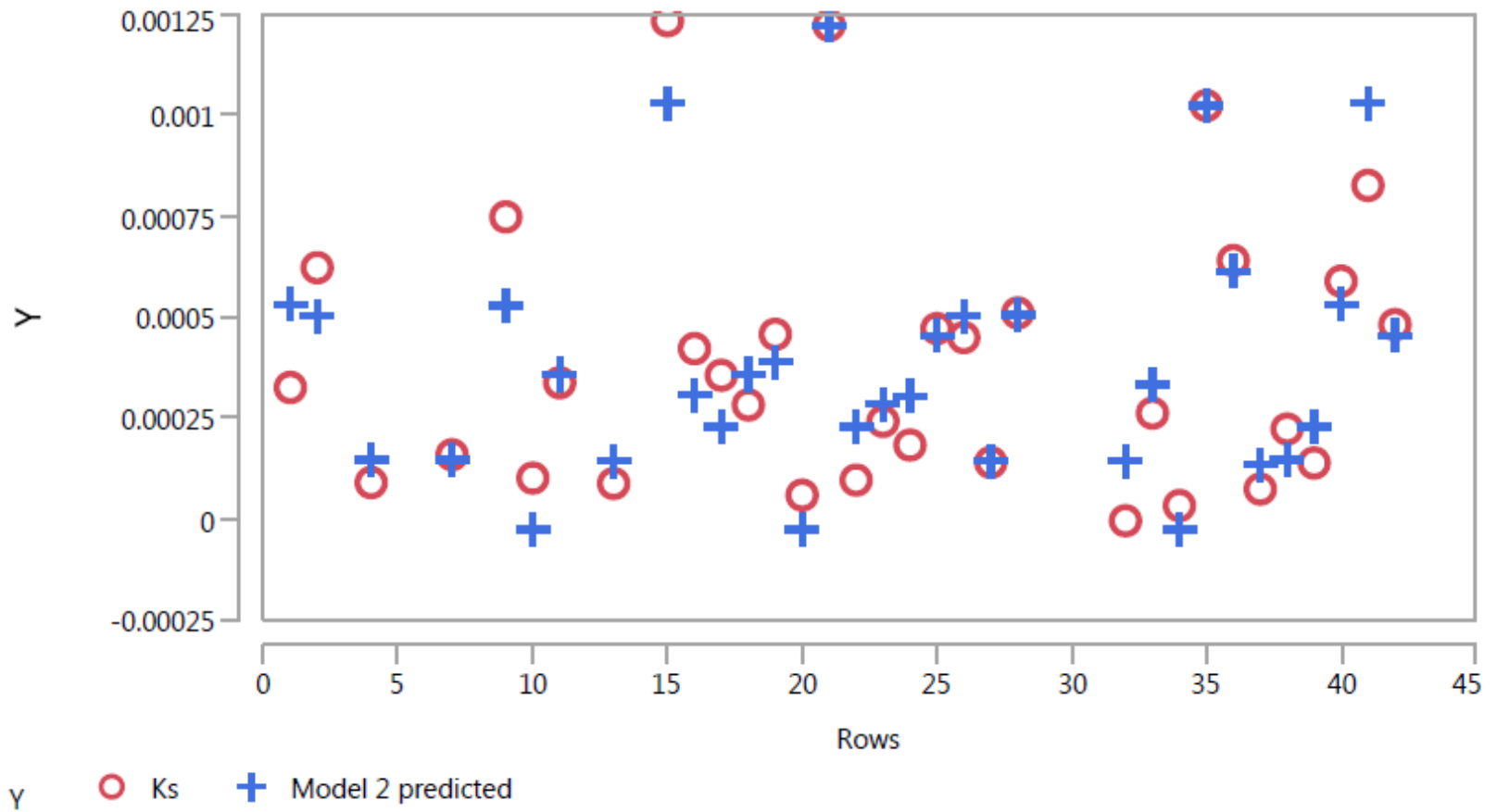
### Quantiles

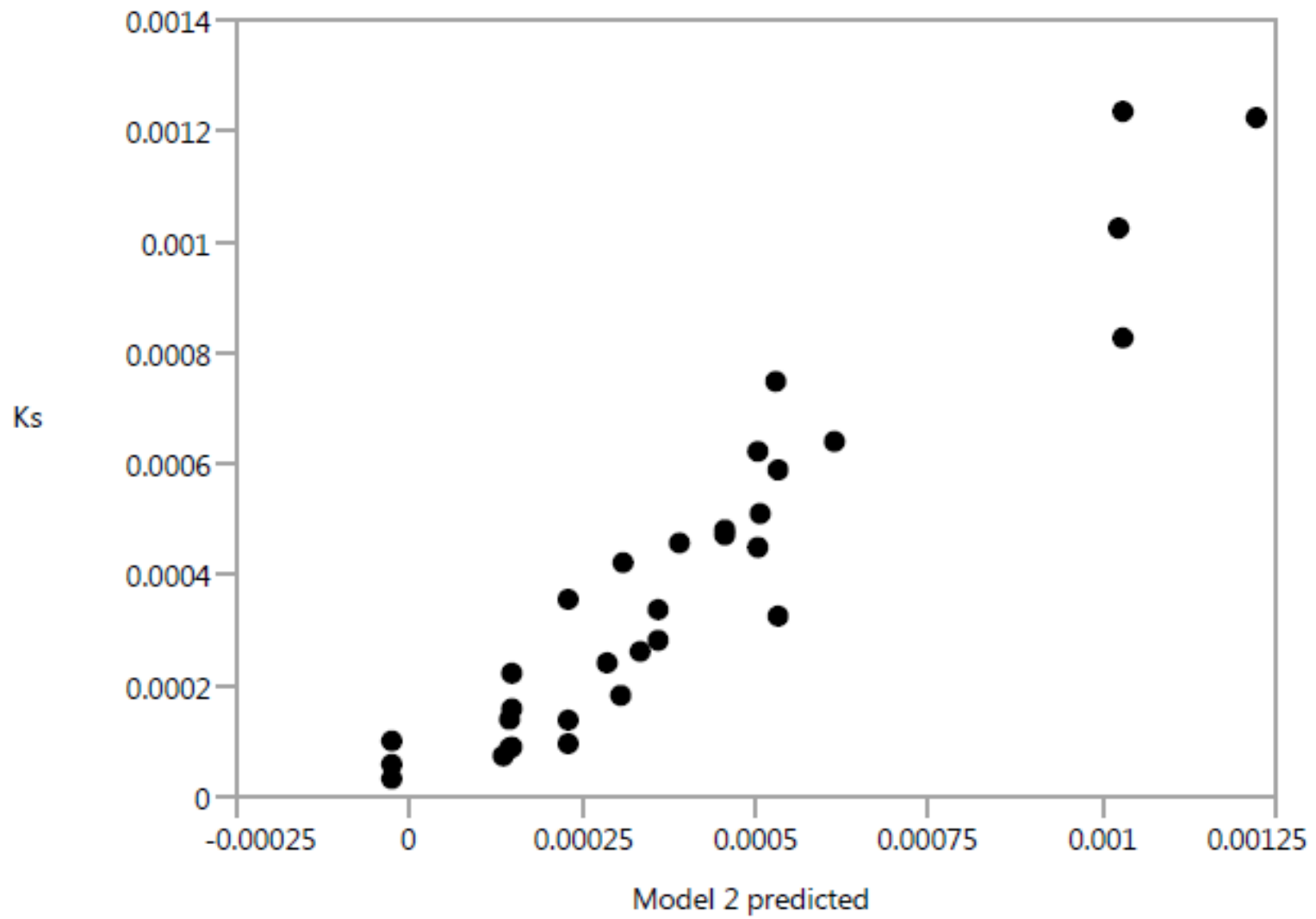
100.0%	maximum	1.7570529777
99.5%		1.7570529777
97.5%		1.7570529777
90.0%		1.3308539669
75.0%	quartile	0.6318708458
50.0%	median	0.2574568695
25.0%	quartile	0.0656837022
10.0%		0.0138784018
2.5%		0.0000221614
0.5%		0.0000221614
0.0%	minimum	0.0000221614

### Summary Statistics

Mean	0.4081583
Std Dev	0.4648379
Std Err Mean	0.0821725
Upper 95% Mean	0.5757503
Lower 95% Mean	0.2405664
N	32

### Overlay Plot



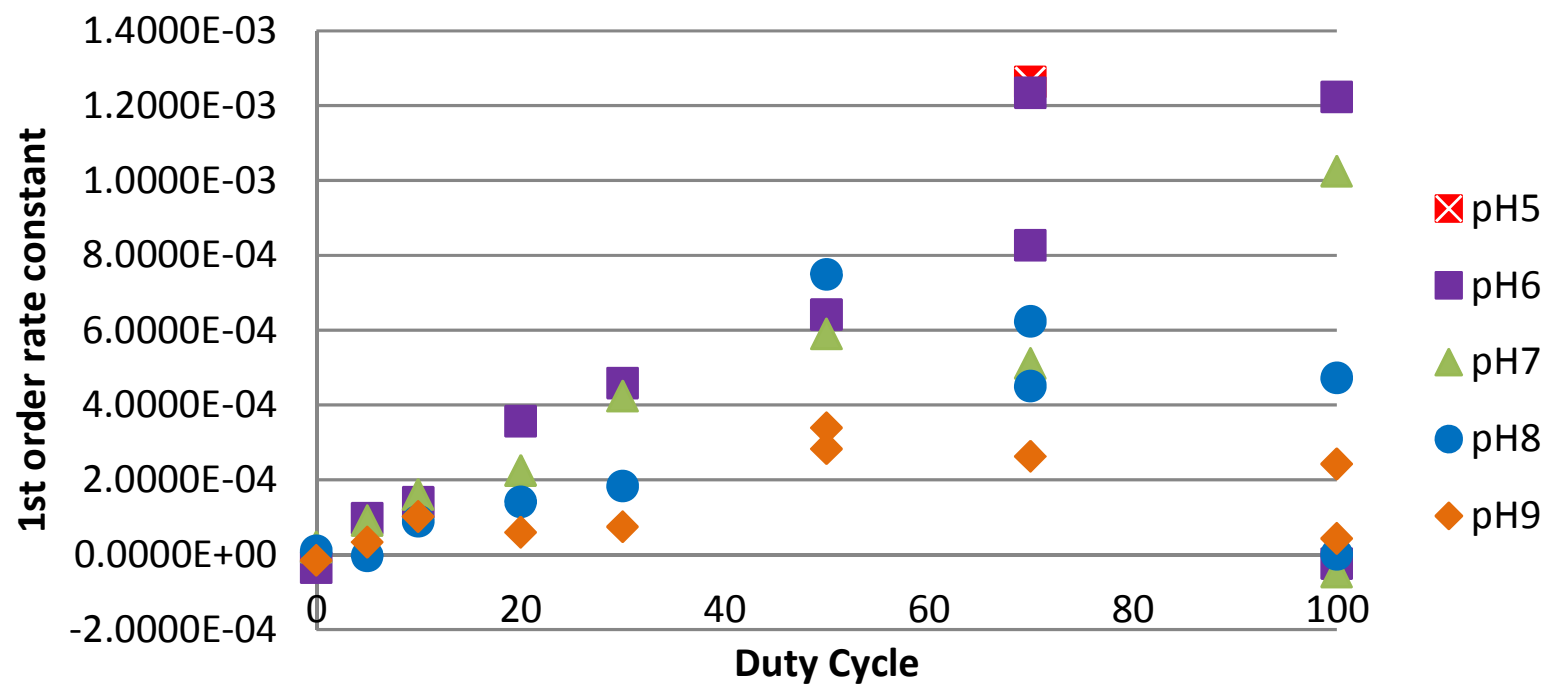


**Appendix G: First Order Reaction Constant (Apparent and Adjusted) Charts**

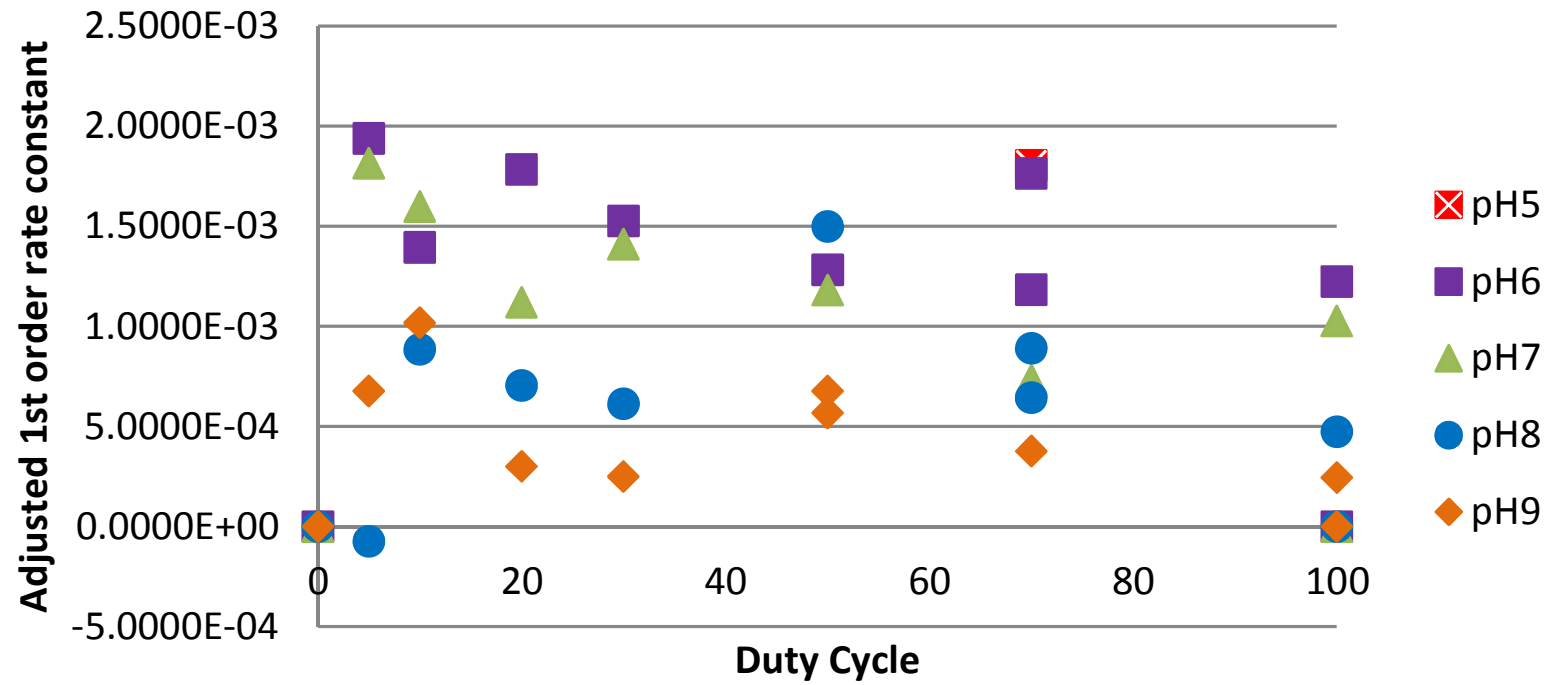
<b>Ks</b>	<b>pH5</b>	<b>pH6</b>	<b>pH7</b>	<b>pH8</b>	<b>pH9</b>
<b>100</b>		-2.4032E-05	-4.7812E-05	9.4125E-07	4.3388E-05
<b>0</b>		-3.5141E-05	1.9741E-05	9.8817E-06	-1.5526E-05
<b>5</b>		9.6902E-05	9.0691E-05	-3.7994E-06	3.3837E-05
<b>10</b>		1.3923E-04	1.5964E-04	8.8471E-05	1.0181E-04
<b>20</b>		3.5649E-04	2.2352E-04	1.4060E-04	5.9627E-05
<b>30</b>		4.5805E-04	4.2257E-04	1.8371E-04	7.4676E-05
<b>50</b>		6.4074E-04	5.8957E-04	7.4882E-04	3.3801E-04
<b>70</b>	1.2624E-03	1.2346E-03	5.1079E-04	6.2298E-04	2.6271E-04
<b>100</b>		1.2235E-03	1.0246E-03	4.7230E-04	2.4222E-04
<b>50</b>					2.8300E-04
<b>70</b>		8.2701E-04		4.5001E-04	
<b>100</b>				4.8199E-04	

<b>Ks, adj</b>	<b>pH5</b>	<b>pH6</b>	<b>pH7</b>	<b>pH8</b>	<b>pH9</b>
<b>100</b>		0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
<b>0</b>		0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
<b>5</b>		1.9380E-03	1.8138E-03	-7.5987E-05	6.7673E-04
<b>10</b>		1.3923E-03	1.5964E-03	8.8471E-04	1.0181E-03
<b>20</b>		1.7825E-03	1.1176E-03	7.0298E-04	2.9814E-04
<b>30</b>		1.5268E-03	1.4086E-03	6.1237E-04	2.4892E-04
<b>50</b>		1.2815E-03	1.1791E-03	1.4976E-03	6.7602E-04
<b>70</b>	1.8034E-03	1.7637E-03	7.2970E-04	8.8997E-04	3.7530E-04
<b>100</b>		1.2235E-03	1.0246E-03	4.7230E-04	2.4222E-04
<b>50</b>					5.6600E-04
<b>70</b>		1.1814E-03		6.4288E-04	
<b>100</b>				4.8199E-04	

## Ks by pH and Duty Cycle



## Ks, Adj by pH and Duty Cycle



## Appendix H: Positive Ionization HPLC Method File

Data File : D:\data\tarr\20150824\_TAR\_STEWART 2015-08-24 09-11-48\tar1000017.D  
Acq. Method: 1500819A\_TAR\_MS.M

The Acq. Method's Instrument Parameters for the Run were :

=====  
Fraction Collector  
=====

Fraction Collector (G1364C)  
=====

Peak Detector Mode: at least one peak detector  
Rinse Needle At Start Of Collection: No  
Rinse Needle Between Collection: No

Fraction Trigger Mode  
Fraction Trigger Mode: Off

Fill Volume  
Fill Volume Mode: As Configured

Peak Detectors  
Peak Detector  
Detector type with serial number Unit Up Slope

-----  
G1315C:DEAA200974 mAU 5.00  
G1321B:DEABW04663 LU 5.00

Down Slope Threshold Upper Threshold Mode

-----  
5.00 5.000 3000.000 Off  
5.00 5.000 3000.000 Off

Stop Time  
Stoptime Mode: As pump/injector

Post Time  
Posttime Mode: Off



Timetable

Instrument Curves

Store Temperature: No

=====

FLD

=====

FLD (G1321B)

=====

Detection Mode: Fluorescence Mode  
Fit spectra range on: Yes  
PMT gain: 10  
Baseline Behaviour Mode: Append  
Peakwidth: > 0.2 min (4 s resp. time) (2.31 Hz)  
Analog Output Source Channel 1: 1  
Analog Output Source Channel 2: 2  
Signal polarity: Positive (+)

Signal A

Excitation  
Use Signal: Yes  
Signal: Signal A  
Wavelength Mode: Wavel. Set  
Excitation Wavelength: 200 nm

Emission  
Use Signal: Yes  
Signal: Signal A  
Wavelength Mode: Wavel. Set  
Emission Wavelength: 410 nm

Multiple Wavelengths  
Multi Wavelength Mode: Multi Emission

Emission Signals

Emission Signal

Use	Signal	Mode	Em. Wavel. nm
-----	--------	------	------------------

-----			
Yes	Signal B	Wavel. Set	500
Yes	Signal C	Wavel. Set	650
Yes	Signal D	Wavel. Set	700

Acquire Spectra

Acquire Spectra Mode: None

Fluorescence Scan Range

Excitation Scan

Scan Excitation WL From: 220 nm  
Scan Excitation WL To: 380 nm  
Scan Excitation WL Step: 5 nm

Emission Scan

Scan Emission WL From: 300 nm  
Scan Emission WL To: 500 nm  
Scan Emission WL Step: 5 nm

Lamp Settings

Lamp on only during run: Yes  
Lamp on required for analysis: No  
Lamp economy mode on: No  
Lamp energy reference mode on: Yes

Analog Output 1

Analog 1 Zero Offset: 5 %  
Analog 1 Attenuation: 100 LU

Analog Output 2

Analog 2 Zero Offset: 5 %  
Analog 2 Attenuation: 100 LU

Stoptime

Stoptime Mode: As pump/injector

Posttime

Posttime Mode: Off

Timetable

=====  
DAD  
=====

DAD (G1315C)  
=====

Peakwidth: >0.10 min (2.0 s response time) (2.5 Hz)  
Slit: 4 nm  
UV Lamp Required: No  
Vis Lamp Required: No

Analog Output 1  
Analog 1 Zero Offset: 5 %  
Analog 1 Attenuation: 1000 mAU

Analog Output 2  
Analog 2 Zero Offset: 5 %  
Analog 2 Attenuation: 1000 mAU

Signals

Signal table

Use Sig. Signal Wavelength Bandwidth Use Ref.  
nm nm

-----  
Yes Signal A 414 200 Yes  
No Signal B  
Yes Signal C 430 5 Yes  
No Signal D  
No Signal E  
No Signal F  
No Signal G  
No Signal H

Ref Wavel. Ref Bandw.  
nm nm

-----

360 100

360 100

Prepare Mode

Margin for negative Absorbance: 100 mAU

Autobalance

Autobalance Prerun: Yes

Autobalance Postrun: No

Spectrum

Spectrum Store: None

Stoptime

Stoptime Mode: As pump/injector

Posttime

Posttime Mode: Off

Timetable

Instrument Curves

Store Board Temperature: No

Store Optical Unit Temperature: No

Store UV Lamp Anode Voltage: No

=====  
Column Comp.  
=====

Column Comp. (G1316A)

=====

Valve Position: Port 1 -> 2

Left Temperature Control

Temperature Control Mode: Not Controlled

Enable Analysis Left Temperature

Enable Analysis Left Temperature On: Yes

Enable Analysis Left Temperature Value: 0.80 °C

Right Temperature Control

Right temperature Control Mode: Temperature Set

Right temperature: 35.00 °C

Enable Analysis Right Temperature

Enable Analysis Right Temperature On: Yes

Enable Analysis Right Temperature Value: 0.80 °C

Stop Time

Stoptime Mode: As pump/injector

Post Time

Posttime Mode: Off

Timetable

Instrument Curves

Store Left Temperature: Yes

Store Right Temperature: No

=====

HiP Sampler

=====

HiP Sampler (G1367E)

=====

Auxiliary

Draw Speed: 100.0 µl/min  
Eject Speed: 100.0 µl/min  
Draw Position Offset: 0.0 mm  
Wait Time After Drawing: 2.0 s  
Sample Flush Out Factor: 5.0  
Vial/Well bottom sensing: No

Injection

Injection Mode: Standard injection  
Injection Volume: 5.00 µL

High throughput

Automaitc Delay Volume Reduction: No

Overlapped Injection

Enable Overlapped Injection: No

Valve Switching

Valve Movements: 0

Valve Switch Time 1

Switch Time 1 Enabled: No

Valve Switch Time 2

Switch Time 2 Enabled: No

Valve Switch Time 3

Switch Time 3 Enabled: No

Valve Switch Time 4

Switch Time 4 Enabled: No

Stop Time

Stoptime Mode: As pump/No limit

Post Time

Posttime Mode: Off

Timetable

Instrument Curves

Store Temperature: No

=====

Valve

=====

Valve (G1170A)

=====

Position Switching Mode:            Use valve position  
Valve position:                            1  
After Run Position Switching Mode:        Do not switch

Stop Time  
Stoptime Mode:                            As pump/injector

Post Time  
Posttime Mode:                            Off

Timetable

Position Description  
Position    Position Description

-----

1	MS
2	FLD
3	DAD
4	Channel 4
5	Channel 5
6	Channel 6
7	Channel 7
8	Channel 8
9	by pass
10	Channel 10
11	Channel 11
12	Channel 12

=====  
Quat. Pump  
=====

Quat. Pump (G1311B)  
=====

Low Pressure Limit: 0.00 bar  
High Pressure Limit: 550.00 bar  
Flow: 0.350 ml/min  
Maximum Flow Gradient: 100.000 ml/min<sup>2</sup>  
Primary Channel: Automatic

Stop Time  
Stoptime Mode: Time set  
Stoptime: 25.00 min

Post Time  
Posttime Mode: Off

Compress  
Compressibility Mode: Compressibility Value Set  
Compressibility: 100 10e-6/bar

Stroke  
Automatic Stroke Calculation: Yes

Timetable

Solvent Composition

Channel Name 1 Used Percent  
%

-----  
A Yes 40.0  
B Yes 50.0  
C Yes 10.0  
D No



Instrument Curves  
Store Pressure: Yes  
Store Flow: Yes  
Store Solvent Ratio A: Yes  
Store Solvent Ratio B: Yes  
Store Solvent Ratio C: Yes  
Store Solvent Ratio D: Yes  
Store Direction of Piston A: No

=====  
Mass Spectrometer Detector  
=====

General Information  
-----

Use MSD : Enabled  
Tune File : atunes.tun  
StopTime : No Limit  
Time Filter : Enabled  
Data Storage : Condensed  
Peakwidth : 0.10 min  
Fast Scan : Disabled  
Fast Scan Data Reconstruction: Disabled  
Polarity Switch Delay : 50 ms  
Ionization Switch Delay : 50 ms

Signals  
-----

[Signal 1]

Not Active

[Signal 2]

Ionization Mode : API-ES  
Polarity : Positive  
Fragmentor Ramp : Disabled  
Percent Cycle Time : 100.00 %

Scan Parameters

Time (min)	Mass Range Low	Mass Range High	Frag-mentor	Gain	Thres-EMV	Step-hold	Step-size
0.00	100.00	700.00	70	1.0	150	0.10	

[Signal 3]

Not Active

[Signal 4]

Not Active

Spray Chamber

-----

[MSZones]

Gas Temp	: 300 C	maximum 350 C
DryingGas	: 10.0 l/min	maximum 13.0 l/min
Neb Pres	: 45 psig	maximum 60 psig
Quad Temp	: 0 C	maximum 0 C

VCap (Positive)	: 3000 V
VCap (Negative)	: 3500 V

[Time Table]

Time Table is empty.

END OF MS ACQUISITION PARAMETERS

=====  
FIA Series  
=====

FIA Series in this Method : Disabled

Time Setting

Time between Injections : 0.15 min

Injection Loop Flush Time : 0.17 min

=====

Column(s)

=====

Column Description : Ascentis Exp C18

Serial# : USMD005296

Product# : 53822-U Batch# :

Diameter : 2.1 mm Length : 50.0 mm

Particle size : 2.7  $\mu$ m Void volume : 60.0 %

Maximum Pressure : 400.0 bar Maximum pH : 9.0

Minimum pH : 2.0

Maximum Temperature: 60.0 °C

Comment :

## Appendix I: Negative Ionization HPLC Method File

### Method Information

Method: D:\METHOD\1500819A\_TAR\_MS.M  
Modified: 8/25/2015 at 1:15:13 PM

### Method Audit Trail

Operator : user  
Date : 8/19/2015 11:13:50 AM  
Change Info: This method was created at 8/19/2015 11:13:50 AM and based on  
method D:\METHOD\1500819\_TAR\_MS.M

Operator : user  
Date : 8/19/2015 11:13:52 AM  
Change Info: Method saved. User comment: ""

Operator : user  
Date : 8/24/2015 9:01:21 AM  
Change Info: Method saved. User comment: ""

### Run Time Checklist

Pre-Run Cmd/Macro: off  
Data Acquisition: on  
Standard Data Analysis: on  
Customized Data Analysis: off  
Save GLP Data: off  
Post-Run Cmd/Macro: off  
Save Method with Data: off

### Injection Source and Location

Injection Source: HipAls

Injection Location: HipAls

=====  
The Acq. Method's Instrument Parameters for the Run were :

Data File : D:\data\tarr\20150820\_TAR\_STEWART 2015-08-20 13-47-13\tar1000035.D  
Acq. Method: 1500819A\_TAR\_MS\_NEG.M

The Acq. Method's Instrument Parameters for the Run were :

=====  
Fraction Collector  
=====

Fraction Collector (G1364C)  
=====

Peak Detector Mode: at least one peak detector

Rinse Needle At Start Of Collection: No

Rinse Needle Between Collection: No

Fraction Trigger Mode

Fraction Trigger Mode: Off

Fill Volume

Fill Volume Mode: As Configured

Peak Detectors

Peak Detector

Detector type with serial number Unit Up Slope

-----  
G1315C:DEAA200974 mAU 5.00

G1321B:DEABW04663 LU 5.00

Down Slope Threshold Upper Threshold Mode

-----  
5.00 5.000 3000.000 Off

5.00 5.000 3000.000 Off

Stop Time  
Stoptime Mode: As pump/injector

Post Time  
Posttime Mode: Off

Timetable

Instrument Curves  
Store Temperature: No

=====

FLD

=====

FLD (G1321B)

=====

Detection Mode: Fluorescence Mode  
Peakwidth: > 0.2 min (4 s resp. time) (2.31 Hz)  
PMT gain: 10  
Baseline Behaviour Mode: Append  
Fit spectra range on: Yes  
Analog Output Source Channel 1: 1  
Analog Output Source Channel 2: 2  
Signal polarity: Positive (+)

Stoptime  
Stoptime Mode: As pump/injector

Posttime  
Posttime Mode: Off

Multiple Wavelengths  
Multi Wavelength Mode: Multi Emission

Emission Signals

Emission Signal

Use Signal	Mode	Em. Wavel. nm
-----		
Yes Signal B Wavel. Set		500
Yes Signal C Wavel. Set		650
Yes Signal D Wavel. Set		700

Acquire Spectra

Acquire Spectra Mode: None

Analog Output 1

Analog 1 Attenuation: 100 LU

Analog 1 Zero Offset: 5 %

Analog Output 2

Analog 2 Attenuation: 100 LU

Analog 2 Zero Offset: 5 %

Lamp Settings

Lamp on only during run: Yes

Lamp on required for analysis: No

Lamp economy mode on: No

Lamp energy reference mode on: Yes

Fluorescence Scan Range

Excitation Scan

Scan Excitation WL From: 220 nm

Scan Excitation WL To: 380 nm

Scan Excitation WL Step: 5 nm

Emission Scan

Scan Emission WL From: 300 nm

Scan Emission WL To: 500 nm

Scan Emission WL Step: 5 nm

Signal A

Excitation

Use Signal: Yes

Signal: Signal A

Wavelength Mode: Wavel. Set

Excitation Wavelength: 200 nm

Emission  
 Use Signal: Yes  
 Signal: Signal A  
 Wavelength Mode: Wavel. Set  
 Emission Wavelength: 410 nm

Timetable

=====  
 DAD  
 =====

DAD (G1315C)  
 =====

Peakwidth: >0.10 min (2.0 s response time) (2.5 Hz)  
 Slit: 4 nm  
 UV Lamp Required: No  
 Vis Lamp Required: No

Analog Output 1  
 Analog 1 Attenuation: 1000 mAU  
 Analog 1 Zero Offset: 5 %

Analog Output 2  
 Analog 2 Attenuation: 1000 mAU  
 Analog 2 Zero Offset: 5 %

Signals

Signal table

Use Sig.	Signal	Wavelength nm	Bandwidth nm	Use Ref.
Yes	Signal A	414	200	Yes
No	Signal B			
Yes	Signal C	430	5	Yes
No	Signal D			
No	Signal E			
No	Signal F			



No Signal G  
No Signal H

Ref Wavel. nm	Ref Bandw. nm
360	100
360	100

Prepare Mode

Margin for negative Absorbance: 100 mAU

Autobalance

Autobalance Prerun: Yes

Autobalance Postrun: No

Spectrum

Spectrum Store: None

Stoptime

Stoptime Mode: As pump/injector

Posttime

Posttime Mode: Off

Timetable

Instrument Curves

Store Board Temperature: No

Store Optical Unit Temperature: No

Store UV Lamp Anode Voltage: No

=====  
Column Comp.  
=====

Column Comp. (G1316A)  
=====

Valve Position: Port 1 -> 2

Left Temperature Control  
Temperature Control Mode: Not Controlled

Enable Analysis Left Temperature  
Enable Analysis Left Temperature On: Yes  
Enable Analysis Left Temperature Value: 0.80 °C

Right Temperature Control  
Right temperature Control Mode: Temperature Set  
Right temperature: 35.00 °C

Enable Analysis Right Temperature  
Enable Analysis Right Temperature On: Yes  
Enable Analysis Right Temperature Value: 0.80 °C

Stop Time  
Stoptime Mode: As pump/injector

Post Time  
Posttime Mode: Off

Timetable

Instrument Curves  
Store Left Temperature: Yes  
Store Right Temperature: No

=====

HiP Sampler

=====

HiP Sampler (G1367E)

=====

Auxiliary

Draw Speed: 100.0 µl/min  
Eject Speed: 100.0 µl/min  
Draw Position Offset: 0.0 mm  
Wait Time After Drawing: 2.0 s  
Sample Flush Out Factor: 5.0  
Vial/Well bottom sensing: No

Injection

Injection Mode: Standard injection  
Injection Volume: 5.00 µL

High throughput

Automatic Delay Volume Reduction: No

Overlapped Injection

Enable Overlapped Injection: No

Valve Switching

Valve Movements: 0

Valve Switch Time 1

Switch Time 1 Enabled: No

Valve Switch Time 2

Switch Time 2 Enabled: No

Valve Switch Time 3

Switch Time 3 Enabled: No

Valve Switch Time 4

Switch Time 4 Enabled: No

Stop Time

Stoptime Mode: As pump/No limit

Post Time

Posttime Mode: Off

Timetable

Instrument Curves

Store Temperature: No

=====  
Valve  
=====

Valve (G1170A)  
=====

Position Switching Mode: Use valve position  
Valve position: 1  
After Run Position Switching Mode: Do not switch

Stop Time  
Stoptime Mode: As pump/injector

Post Time  
Posttime Mode: Off

Timetable

Position Description

Position Position Description

-----

1	MS
2	FLD
3	DAD
4	Channel 4
5	Channel 5
6	Channel 6
7	Channel 7
8	Channel 8
9	by pass
10	Channel 10
11	Channel 11

### Method Information

Method: D:\METHOD\1500819A\_TAR\_MS.M  
Modified: 8/25/2015 at 1:15:13 PM

### Method Audit Trail

Operator : user  
Date : 8/19/2015 11:13:50 AM  
Change Info: This method was created at 8/19/2015 11:13:50 AM and based on  
method D:\METHOD\1500819\_TAR\_MS.M

Operator : user  
Date : 8/19/2015 11:13:52 AM  
Change Info: Method saved. User comment: ""

Operator : user  
Date : 8/24/2015 9:01:21 AM  
Change Info: Method saved. User comment: ""

### Run Time Checklist

Pre-Run Cmd/Macro: off

Data Acquisition: on

Standard Data Analysis: on

Customized Data Analysis: off

Save GLP Data: off

Post-Run Cmd/Macro: off

Save Method with Data: off

### Injection Source and Location

Injection Source: HipAls

D No

Instrument Curves

Store Pressure:	Yes
Store Flow:	Yes
Store Solvent Ratio A:	Yes
Store Solvent Ratio B:	Yes
Store Solvent Ratio C:	Yes
Store Solvent Ratio D:	Yes
Store Direction of Piston A:	No

=====  
Mass Spectrometer Detector  
=====

General Information

-----

Use MSD : Enabled  
Tune File : atunes.tun  
StopTime : No Limit  
Time Filter : Enabled  
Data Storage : Condensed  
Peakwidth : 0.10 min  
Fast Scan : Disabled  
Fast Scan Data Reconstruction: Disabled  
Polarity Switch Delay : 50 ms  
Ionization Switch Delay : 50 ms

Signals

-----

[Signal 1]

Ionization Mode : API-ES  
Polarity : Negative

Fragmentor Ramp : Disabled  
Percent Cycle Time : 100.00 %

Scan Parameters

Time (min)	Mass Range Low	Mass Range High	Frag-mentor	Gain	Thres-EMV	Step-hold	Size
0.00	100.00	550.00	70	1.0	150	0.10	

[Signal 2]

Not Active

[Signal 3]

Not Active

[Signal 4]

Not Active

Spray Chamber

-----

[MSZones]

Gas Temp	: 300 C	maximum 350 C
DryingGas	: 10.0 l/min	maximum 13.0 l/min
Neb Pres	: 45 psig	maximum 60 psig
Quad Temp	: 0 C	maximum 0 C

VCap (Positive) : 3000 V

VCap (Negative) : 3500 V

[Time Table]

Time Table is empty.

END OF MS ACQUISITION PARAMETERS

=====

FIA Series

=====

FIA Series in this Method : Disabled

Time Setting

Time between Injections : 0.15 min

Injection Loop Flush Time : 0.17 min

=====

Column(s)

=====

Column Description : Ascentis Exp C18

Serial# : USMD005296

Product# : 53822-U Batch# :

Diameter : 2.1 mm Length : 50.0 mm

Particle size : 2.7  $\mu$ m Void volume : 60.0 %

Maximum Pressure : 400.0 bar Maximum pH : 9.0

Minimum pH : 2.0

Maximum Temperature: 60.0  $^{\circ}$ C

Comment :

The Data Analysis Parameters of the used Method are :

=====

Integration Events

=====

-----

Non signal specific Integration Events

-----

Event	Value
Tangent Skim Mode	Standard
Baseline Correction	Advanced
Tail Peak Skim Height Ratio	0.000
Front Peak Skim Height Ratio	0.000



Skim Valley Ratio	20.000
Peak to Valley Ratio	500.000

-----  
 Default Integration Event Table "Event"  
 -----

Event	Value	Time
----- ----- -----		
Initial Slope Sensitivity	1.000	Initial
Initial Peak Width	0.020	Initial
Initial Area Reject	1.000	Initial
Initial Height Reject	1.700	Initial
Initial Shoulders	OFF	Initial

-----  
 Detector Default Integration Event Table "Event\_DAD"  
 -----

Event	Value	Time
----- ----- -----		
Initial Slope Sensitivity	5.000	Initial
Initial Peak Width	0.020	Initial
Initial Area Reject	5.000	Initial
Initial Height Reject	1.000	Initial
Initial Shoulders	OFF	Initial

-----  
 Detector Default Integration Event Table "Event\_ADC"  
 -----

Event	Value	Time
----- ----- -----		
Initial Slope Sensitivity	1.000	Initial
Initial Peak Width	0.020	Initial
Initial Area Reject	1.000	Initial
Initial Height Reject	1.700	Initial
Initial Shoulders	OFF	Initial

-----  
 Detector Default Integration Event Table "Event\_FLD"  
 -----

Event	Value	Time
----- ----- -----		
Initial Slope Sensitivity	1.000	Initial
Initial Peak Width	0.020	Initial

Initial Area Reject	1.000	Initial
Initial Height Reject	1.700	Initial
Initial Shoulders	OFF	Initial

-----  
 Detector Default Integration Event Table "Event\_MSD"  
 -----

Event	Value	Time
Initial Slope Sensitivity	10000.000	Initial
Initial Peak Width	0.020	Initial
Initial Area Reject	1000.000	Initial
Initial Height Reject	100.000	Initial
Initial Shoulders	OFF	Initial

-----  
 Signal Specific Integration Event Table "Event\_MSD1SPC"  
 -----

Event	Value	Time
Initial Slope Sensitivity(Full Scan)	1.000	Initial
Initial Peak Width(Full Scan)	0.250	Initial
Initial Slope Sensitivity(Cond. Scan/SIM)	0.100	Initial
Initial Peak Width(Cond. Scan/SIM)	0.050	Initial
Initial Area Reject	0.000	Initial
Initial Height Reject	5.000	Initial
Initial Shoulders	OFF	Initial

-----  
 Detector Default Integration Event Table "Event\_VWD"  
 -----

Event	Value	Time
Initial Slope Sensitivity	1.000	Initial
Initial Peak Width	0.020	Initial
Initial Area Reject	1.000	Initial
Initial Height Reject	1.700	Initial
Initial Shoulders	OFF	Initial

-----  
 Detector Default Integration Event Table "Event\_ECD"  
 -----

Event	Value	Time
-------	-------	------

Initial Slope Sensitivity	1.000	Initial
Initial Peak Width	0.020	Initial
Initial Area Reject	1.000	Initial
Initial Height Reject	1.700	Initial
Initial Shoulders	OFF	Initial

Detector Default Integration Event Table "Event\_MWD"

Event	Value	Time
Initial Slope Sensitivity	1.000	Initial
Initial Peak Width	0.020	Initial
Initial Area Reject	1.000	Initial
Initial Height Reject	1.700	Initial
Initial Shoulders	OFF	Initial

Signal Specific Integration Event Table "Event\_MSD1TIC"

Event	Value	Time
Initial Slope Sensitivity	4255.241	Initial
Initial Peak Width	0.157	Initial
Initial Area Reject	13989.271	Initial
Initial Height Reject	743.464	Initial
Initial Shoulders	OFF	Initial

Apply Method's Manual Integration Events: No

Specify Report

Calculate: Area Percent  
 Use Multiplier & Dilution Factor with ISTDs

Use Sample Data from Data File  
 Destination: Screen  
 Quantitative Results sorted by: Signal

Report Style: Short  
Sample info on each page: No  
Add Chromatogram Output: Yes  
Chromatogram Output: Portrait  
Size in Time direction: 100 % of Page  
Size in Response direction: 40 % of Page  
Uncalibrated Peaks: Report with Calibrated Peaks

=====  
Signal Options  
=====

Include: Axes, Retention Times, Baselines, Tick Marks  
Font: Times New Roman, Size: 8

Ranges: Full  
Multi Chromatograms: Overlaid, Each in full Scale

=====  
Calibration Table  
=====

Calib. Data Modified :

Rel. Reference Window : 5.000 %  
Abs. Reference Window : 0.000 min  
Rel. Non-ref. Window : 5.000 %  
Abs. Non-ref. Window : 0.000 min  
Uncalibrated Peaks : not reported  
Partial Calibration : Yes, identified peaks are recalibrated  
Correct All Ret. Times: No, only for identified peaks

Curve Type : Linear  
Origin : Included  
Weight : Equal

Recalibration Settings:  
Average Response : Average all calibrations  
Average Retention Time: Floating Average New 75%

Calibration Report Options :  
Printout of recalibrations within a sequence:  
Calibration Table after Recalibration

Normal Report after Recalibration  
If the sequence is done with bracketing:  
Results of first cycle (ending previous bracket)

=====

Peak Sum Table

=====

\*\*\*No Entries in table\*\*\*

=====

=====

Sample related custom fields

=====

Custom Field	Type	Mand.	Default Value
--------------	------	-------	---------------

-----

None defined

=====

Compound related custom fields

=====

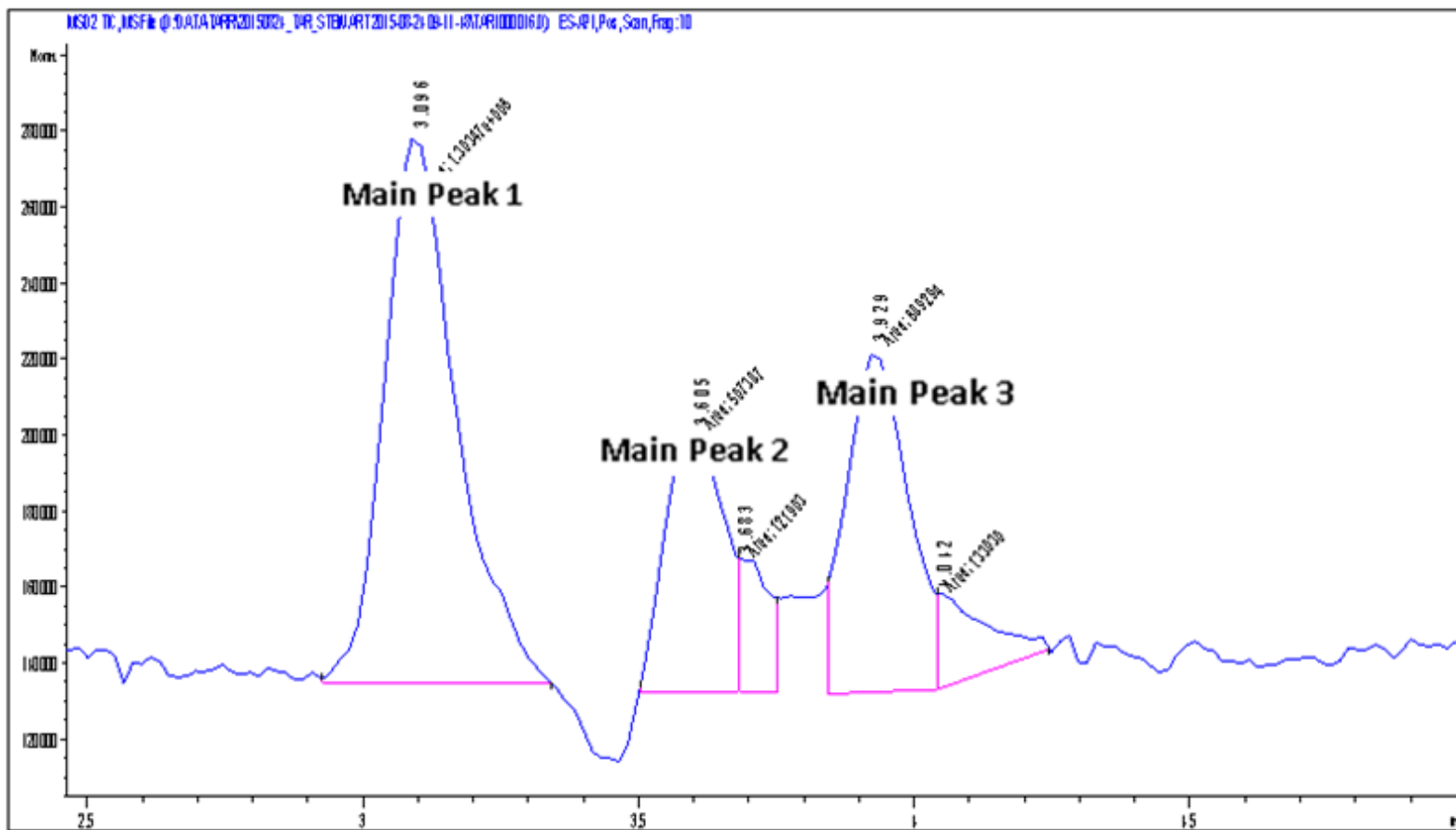
Custom Field	Type	Mand.	Default Value
--------------	------	-------	---------------

-----

None defined

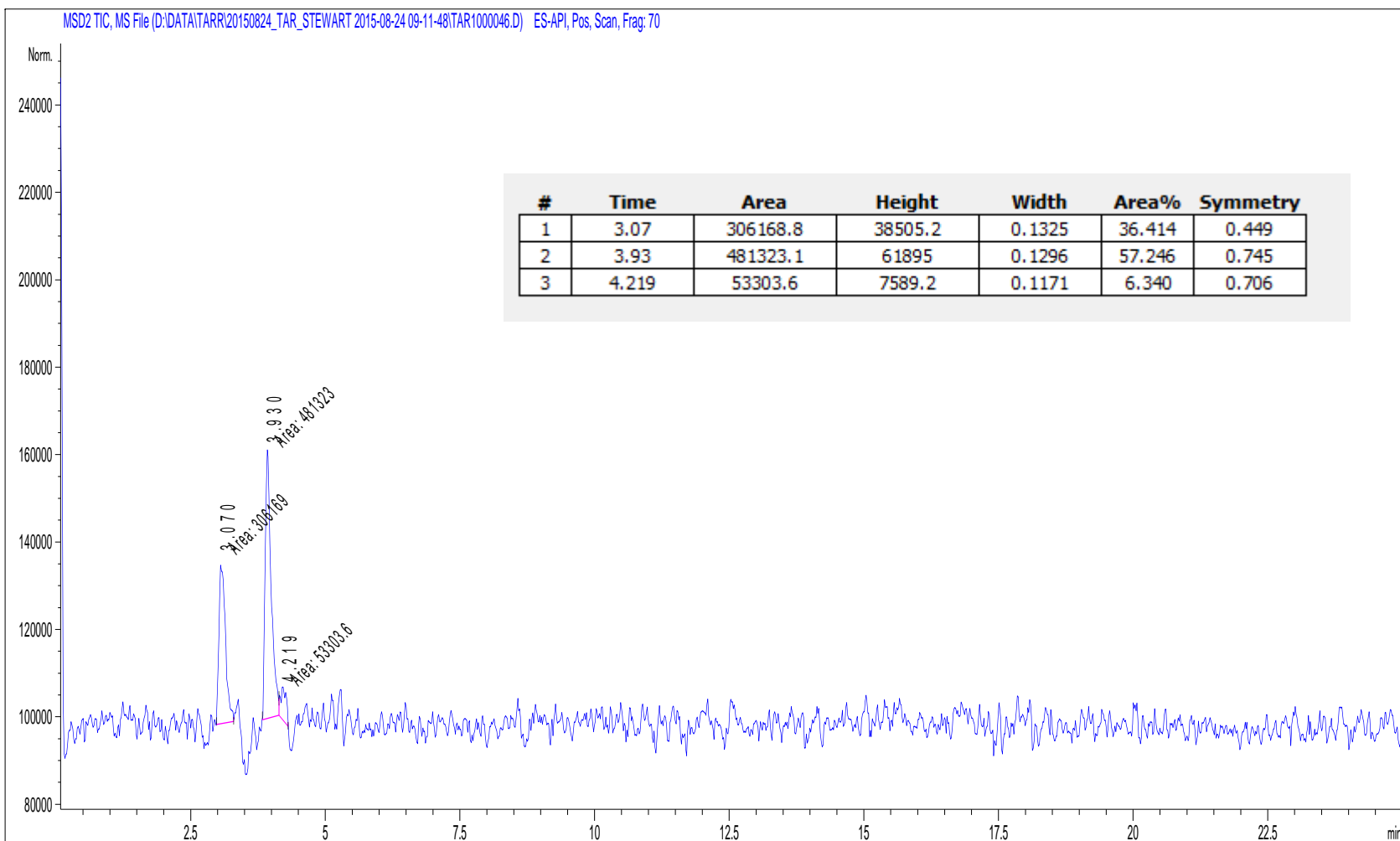
## Appendix J: Positive Ionization HPLC Chromatograms and Mass Spectroscopy

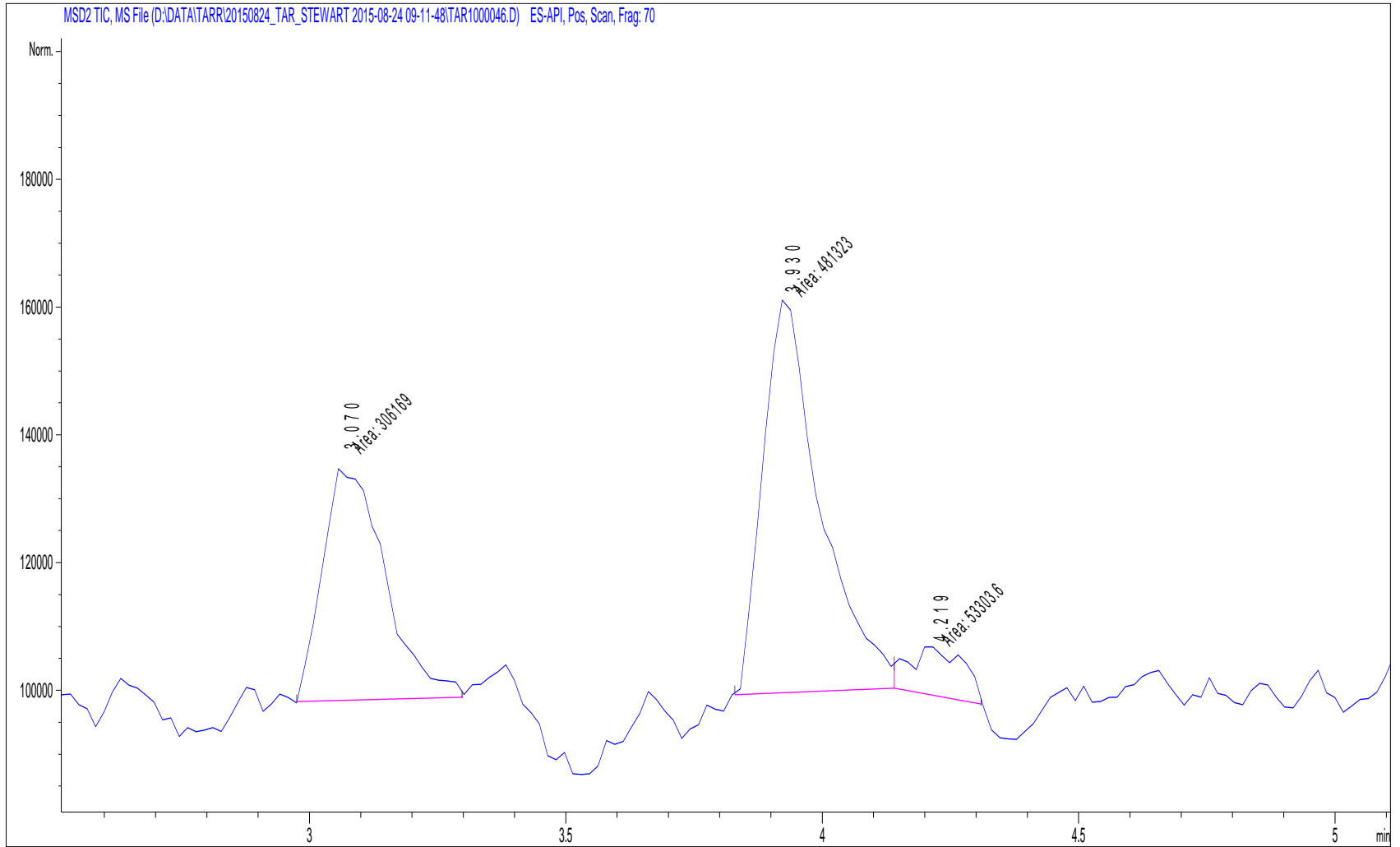
### Example Positive Chromatogram



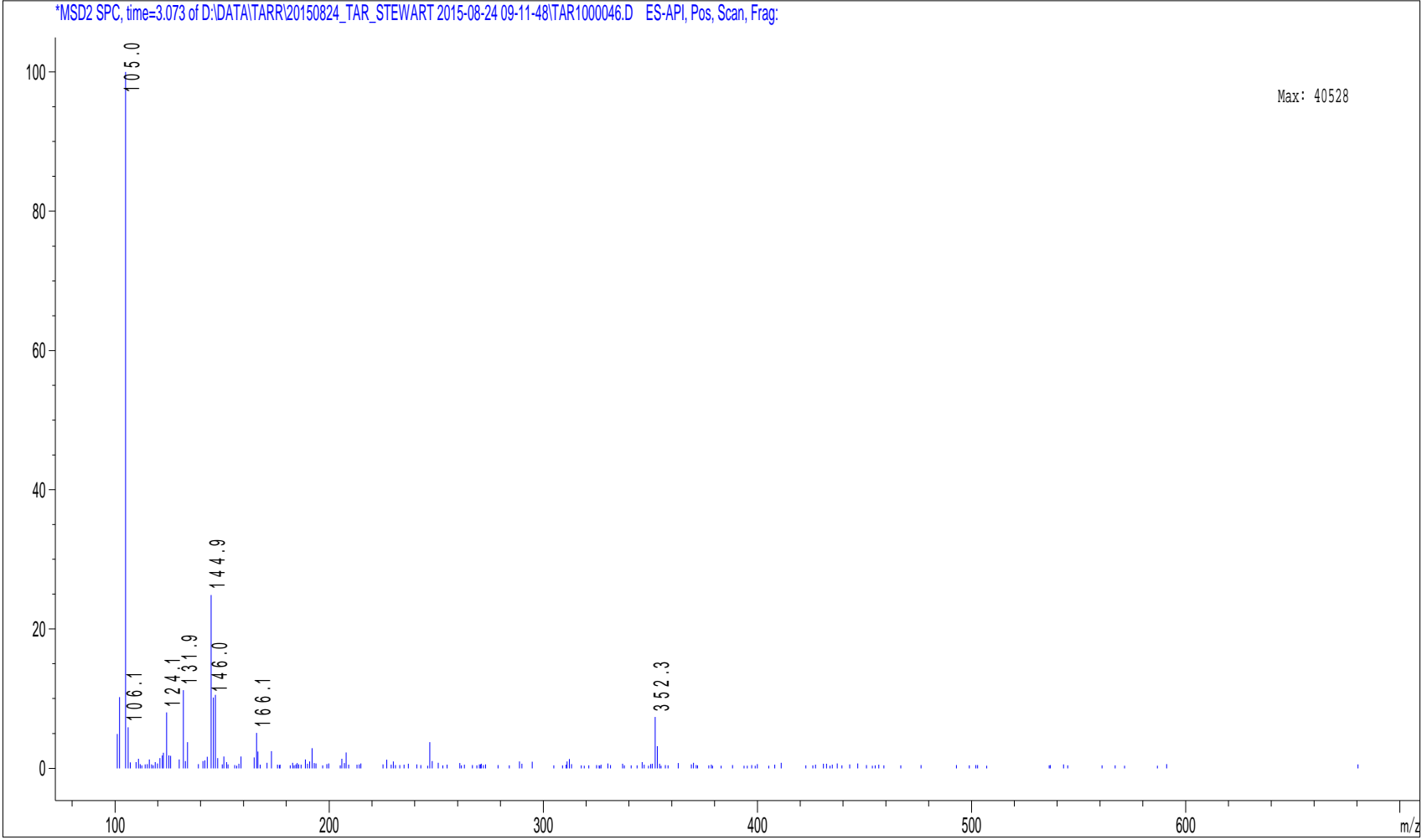
# Baselines, Standards, Misc.

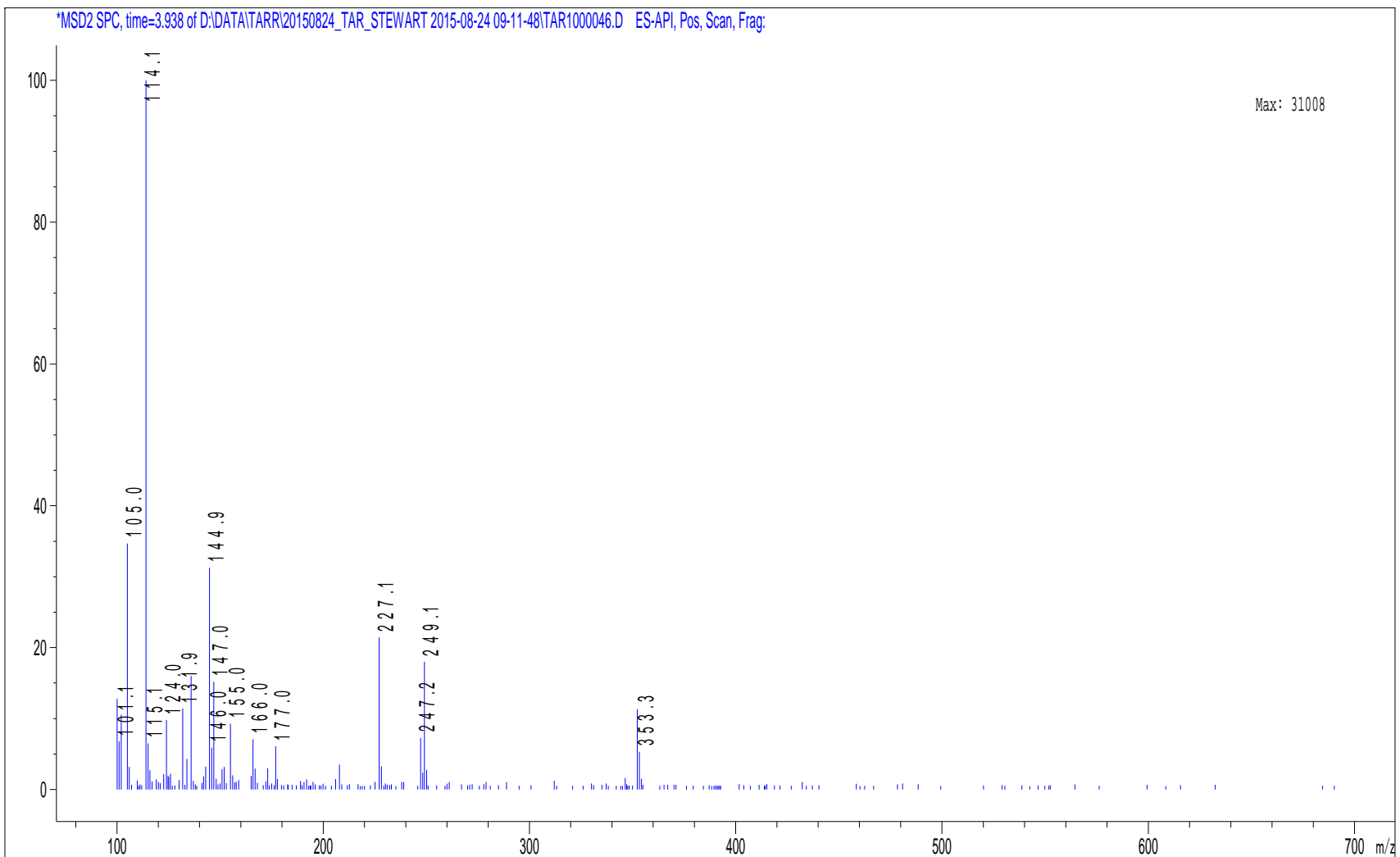
20-Aug-15  
Baseline - DI Water  
P2-A-01

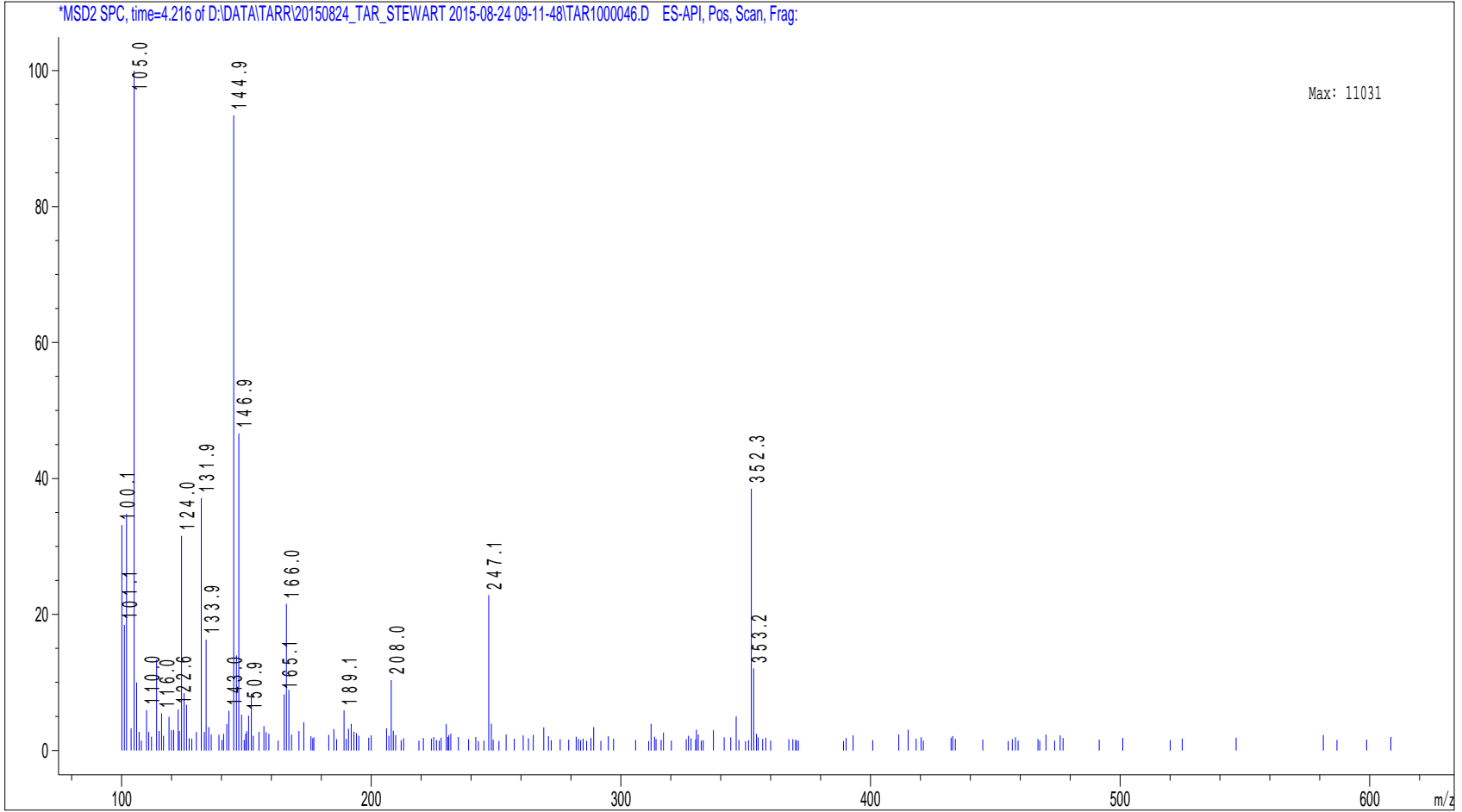




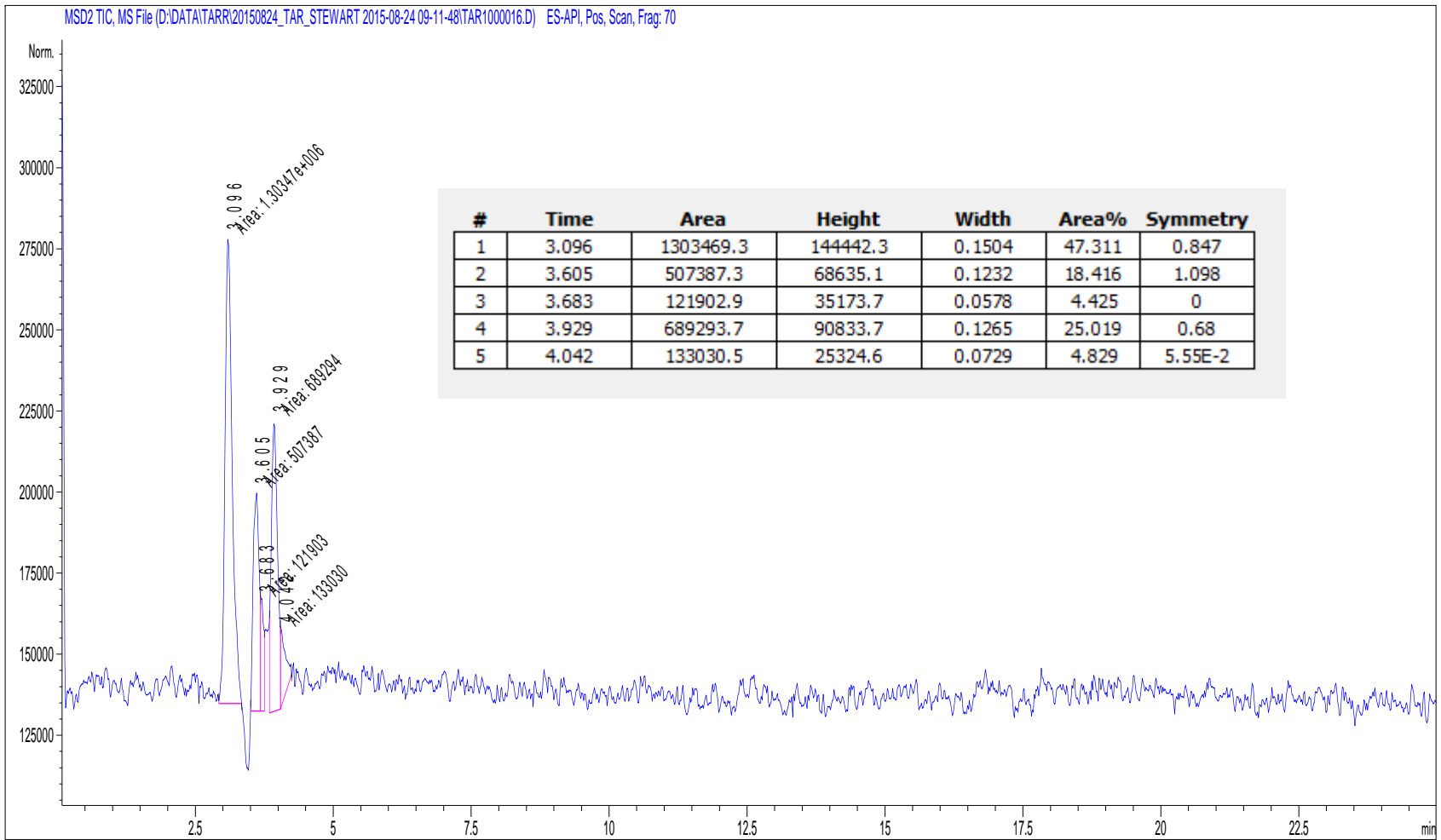


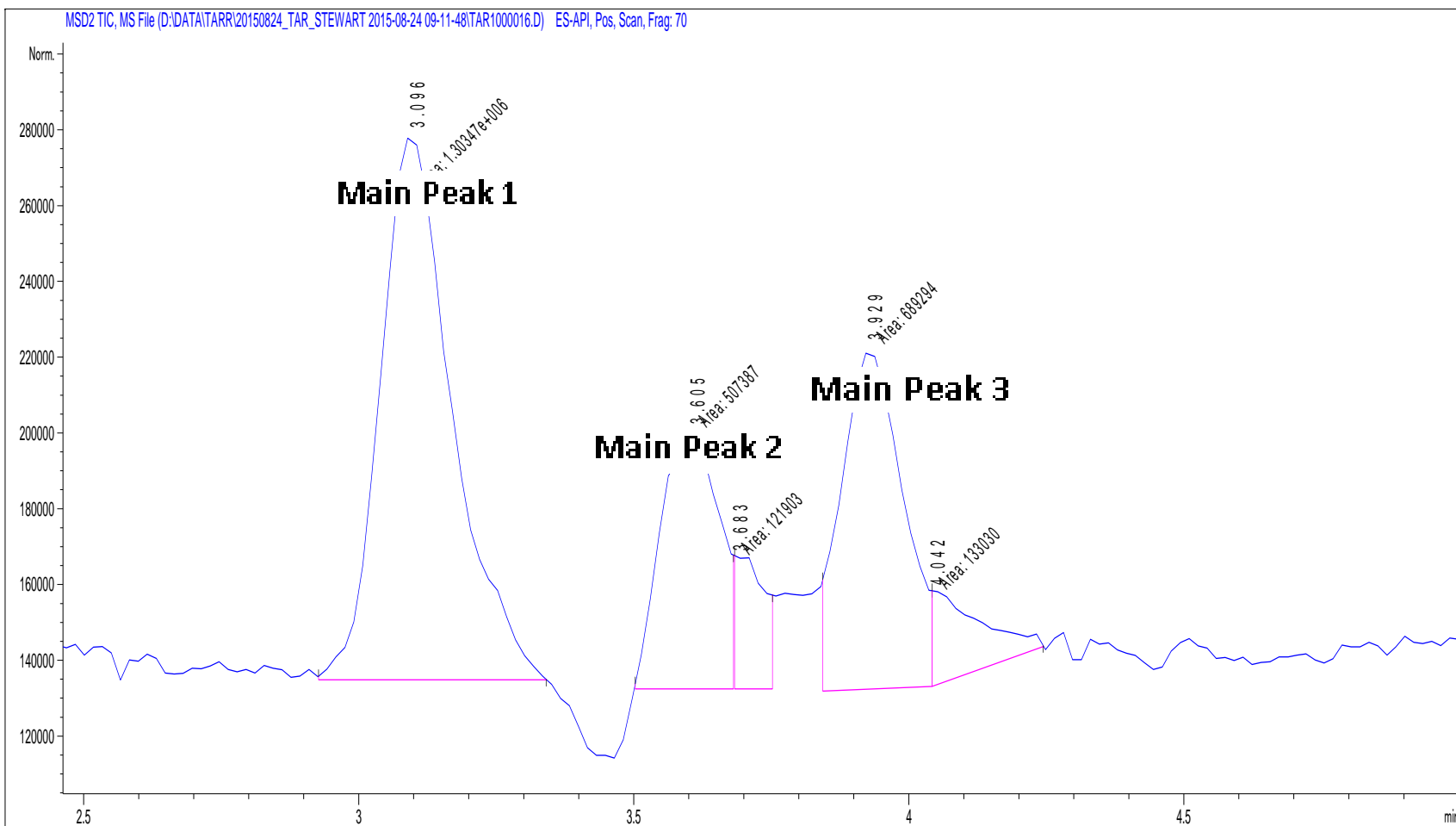




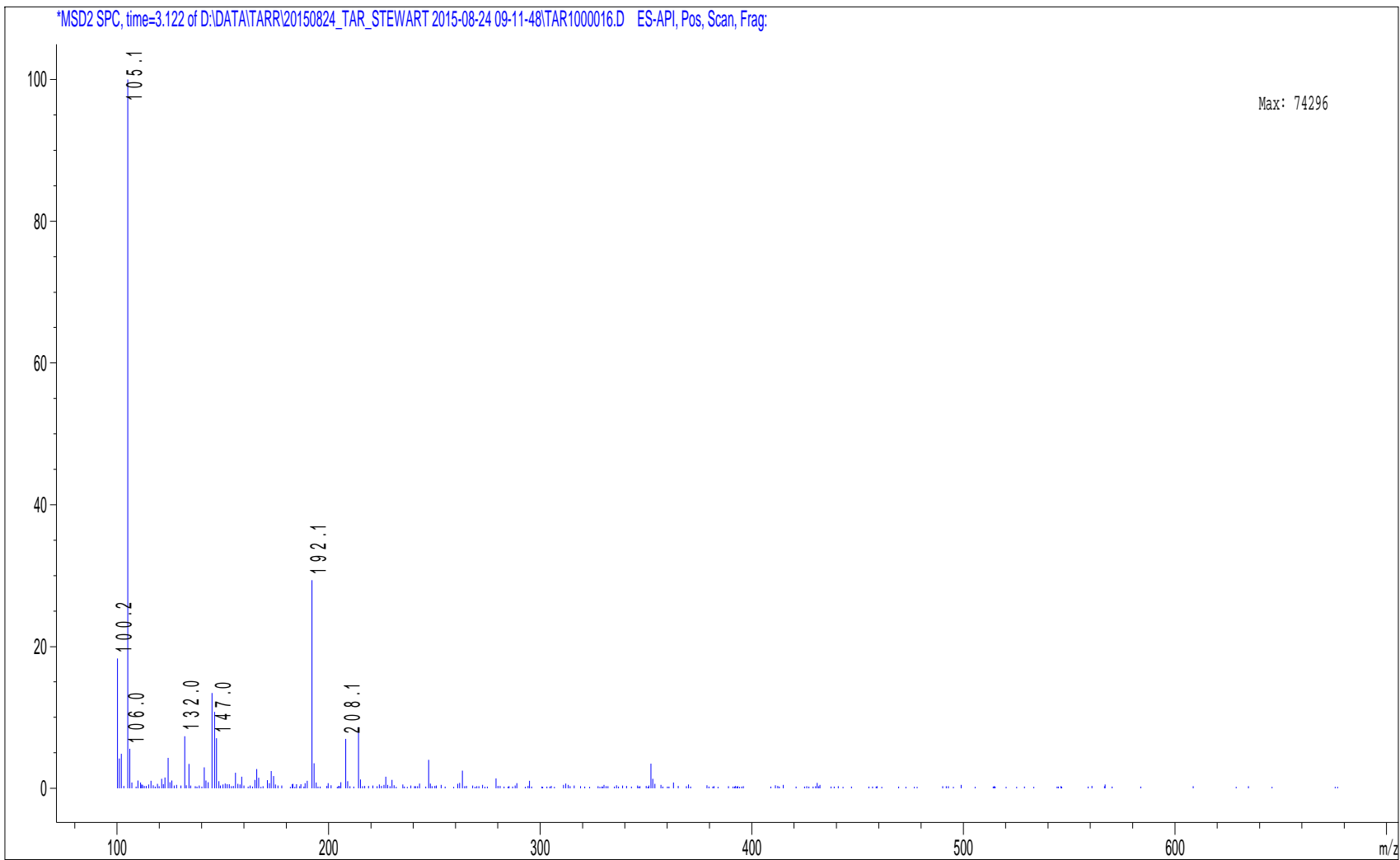


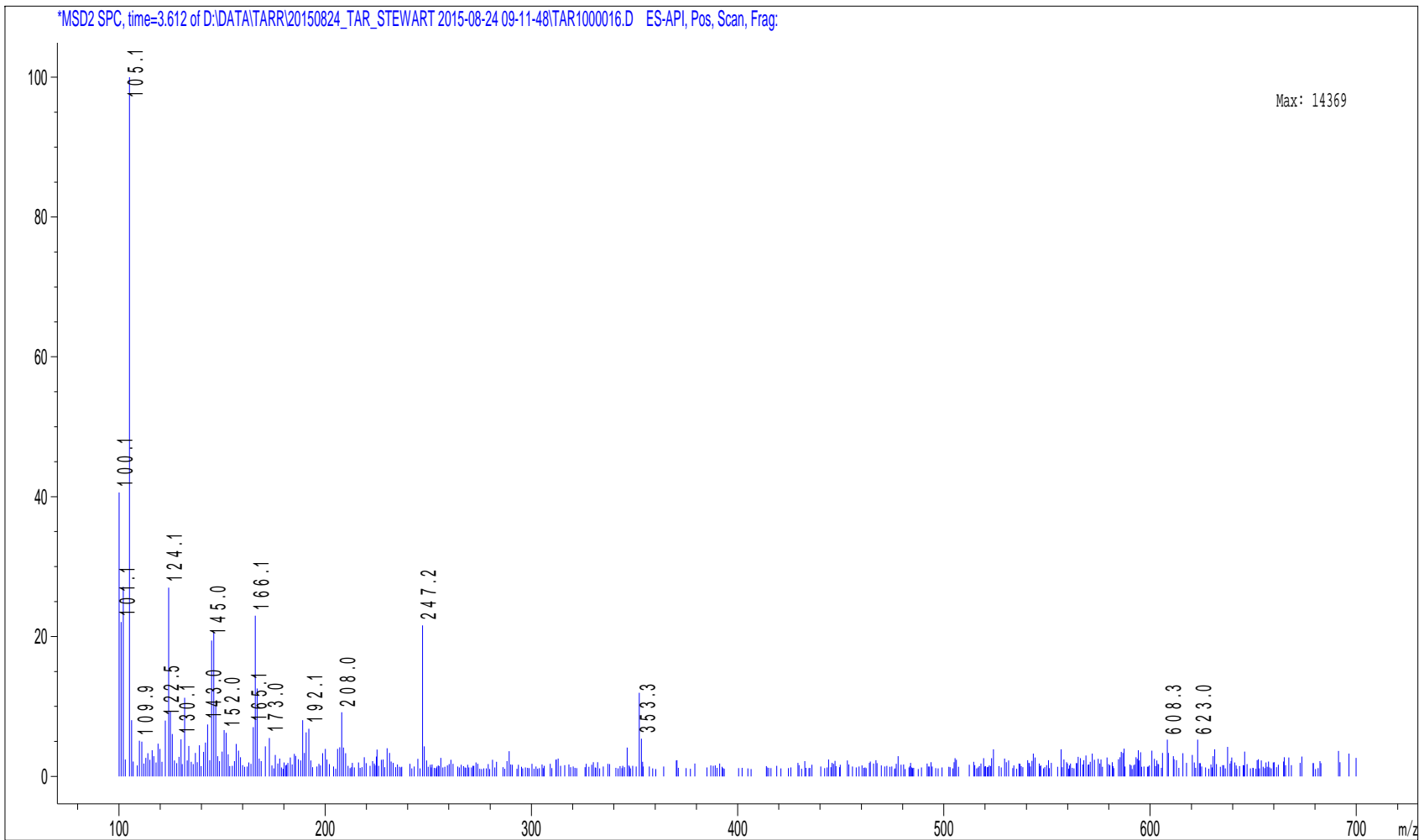
29-May-15  
pH5 - repeat  
P2-B-03

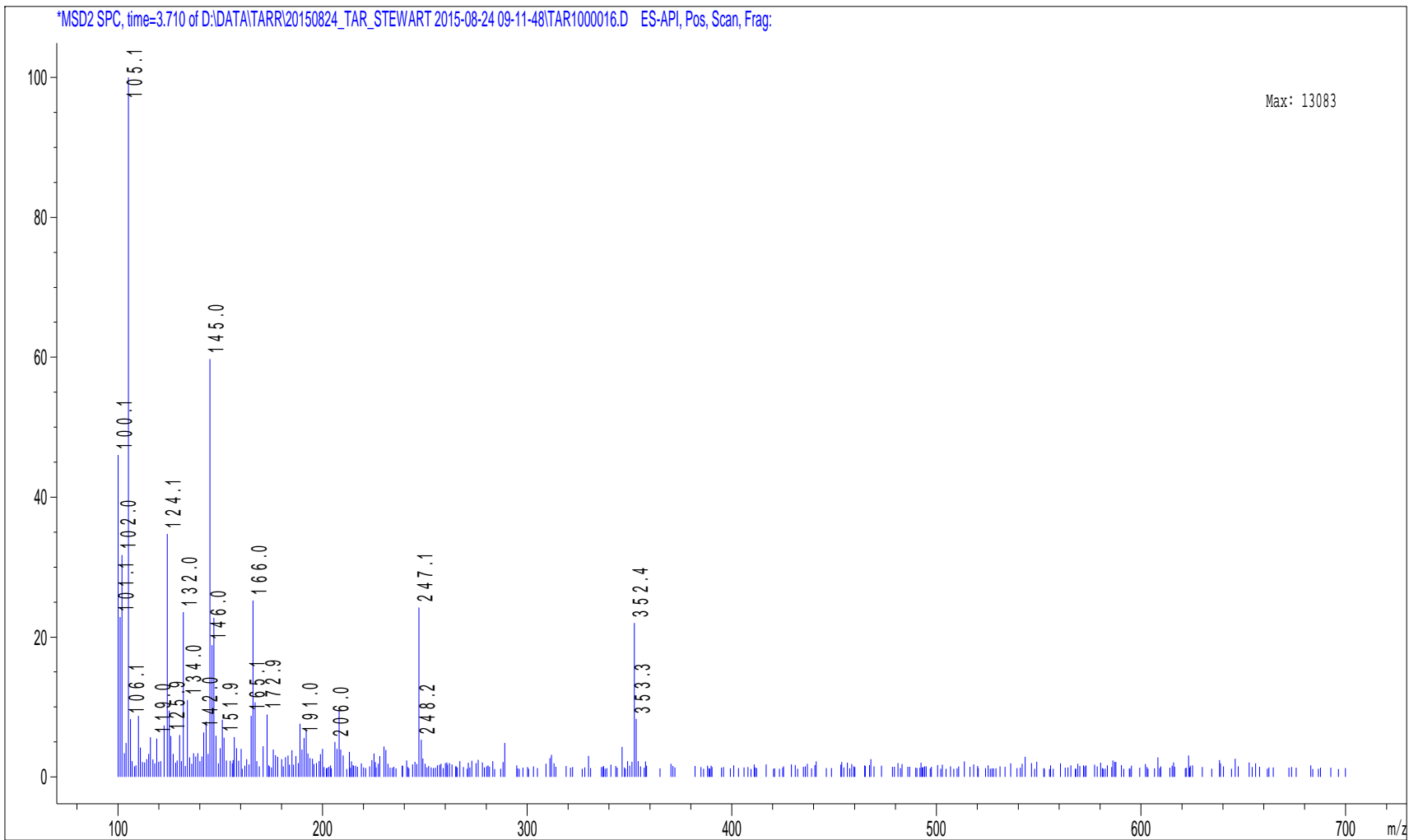




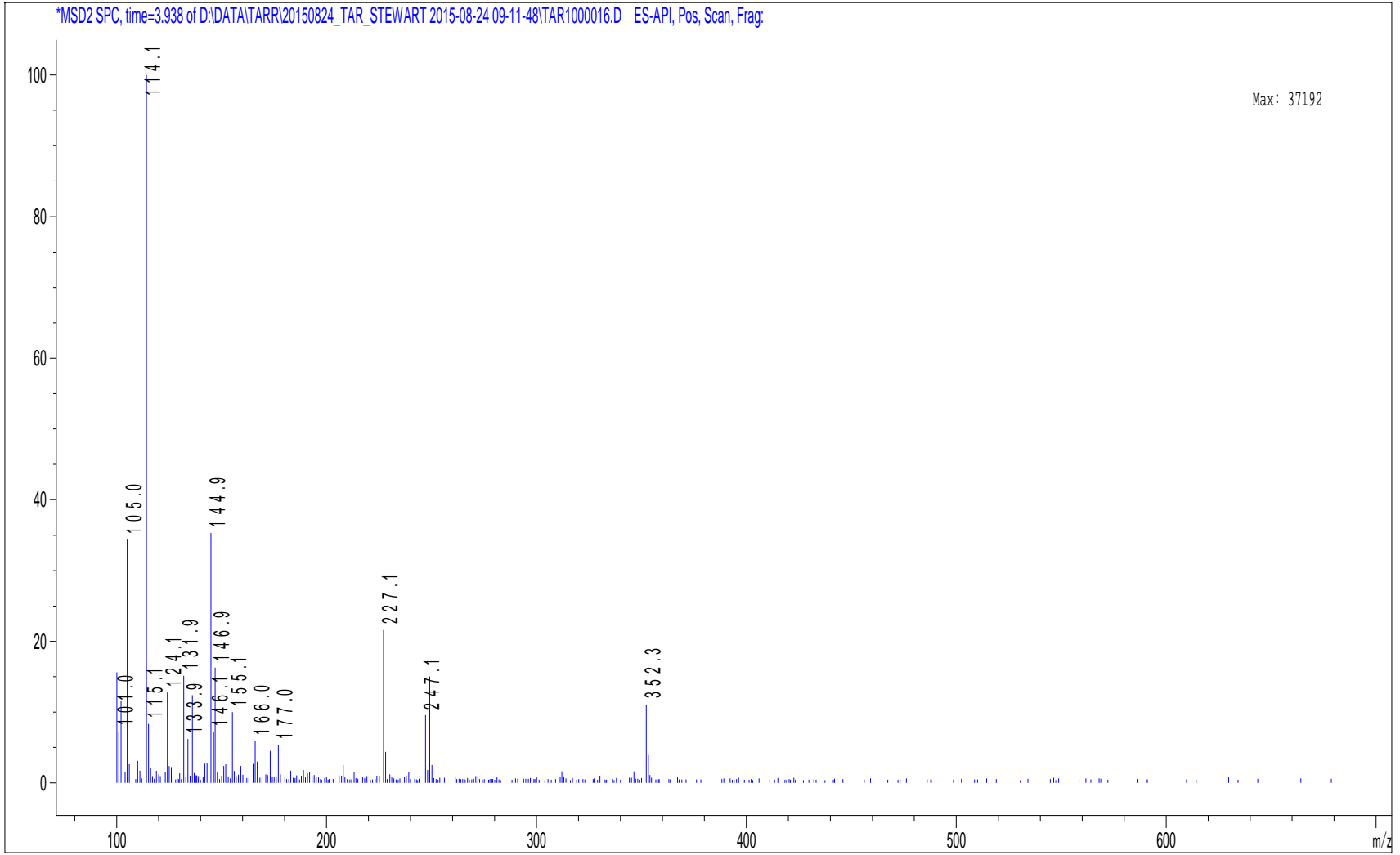
**Main Peak 3**

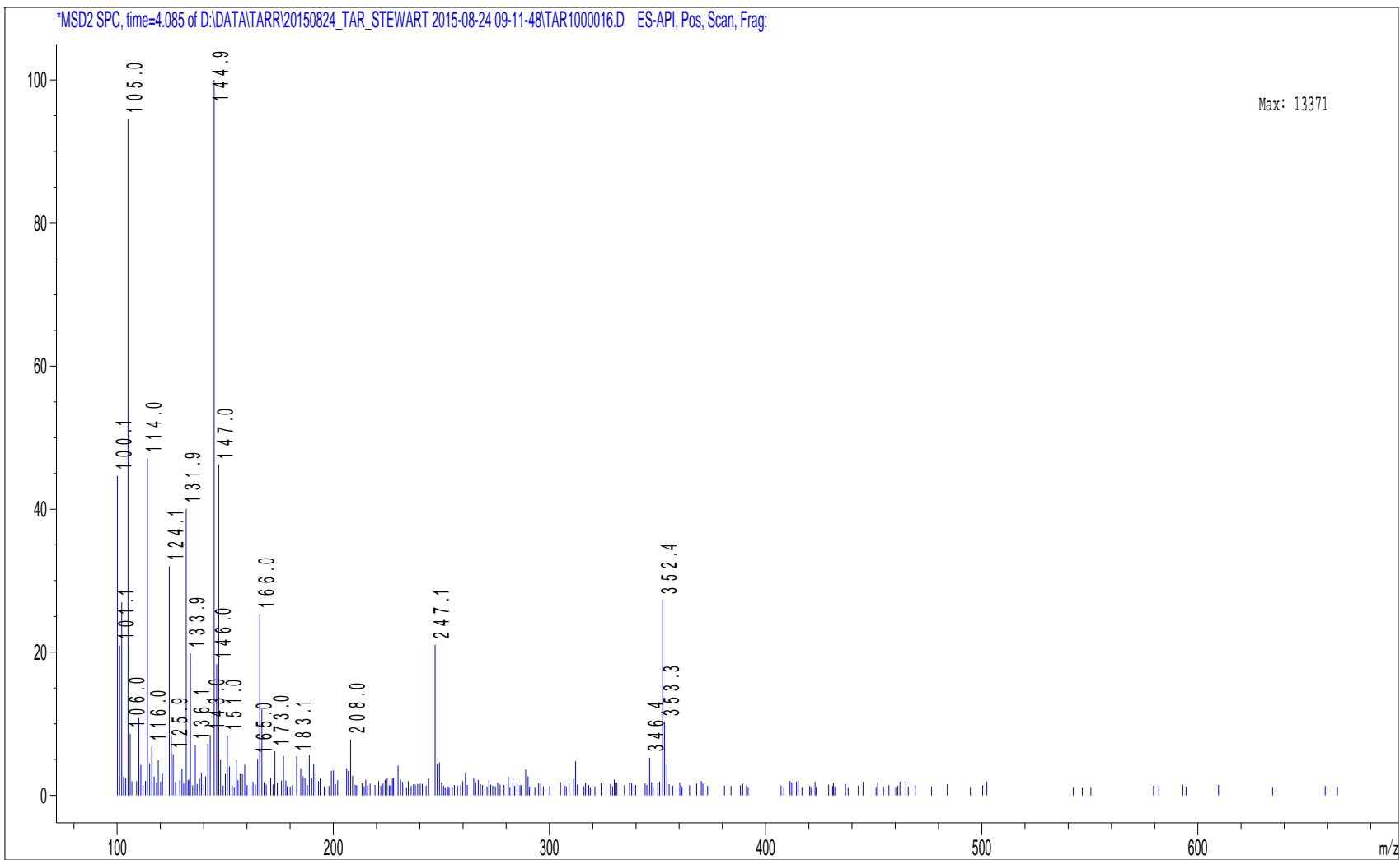




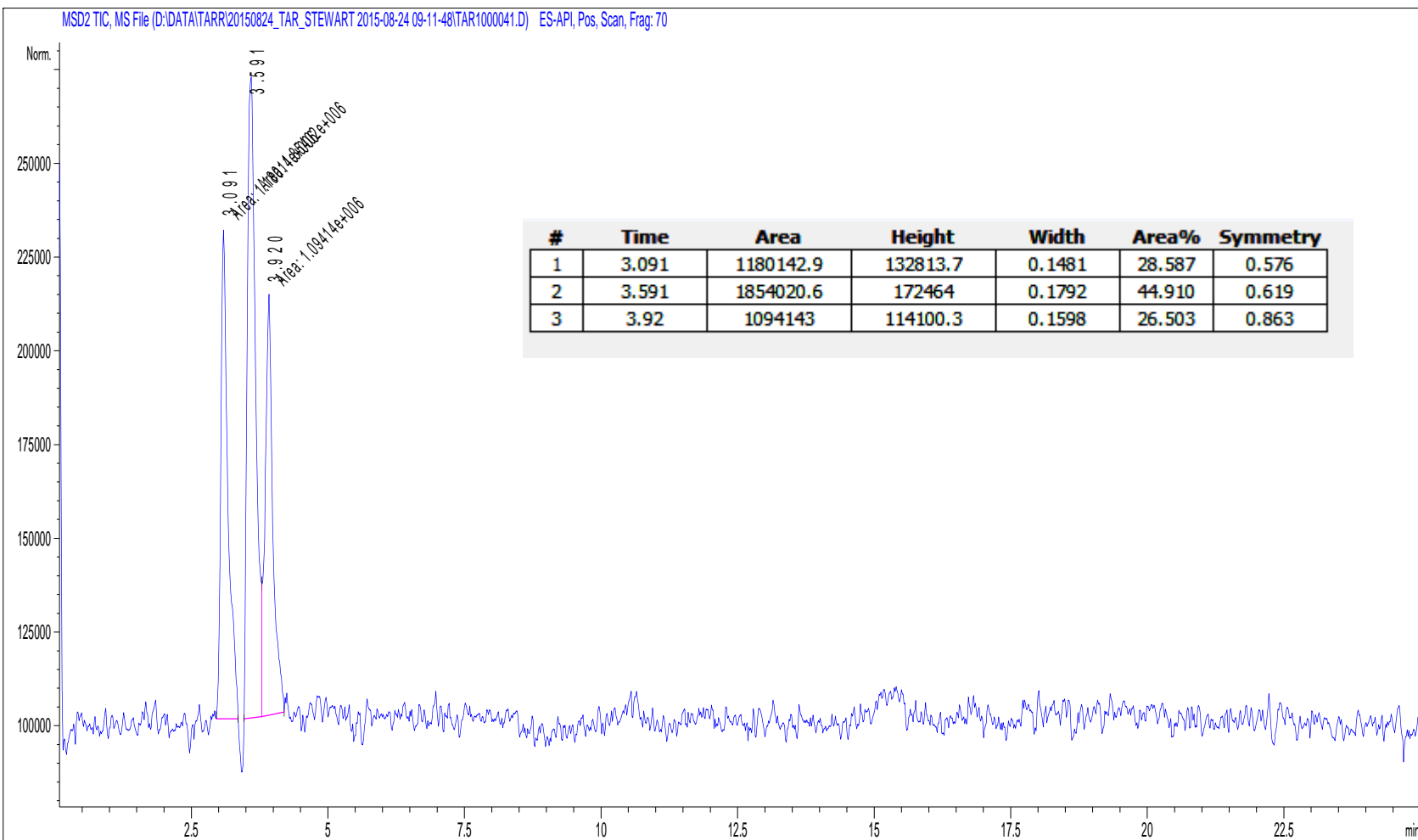


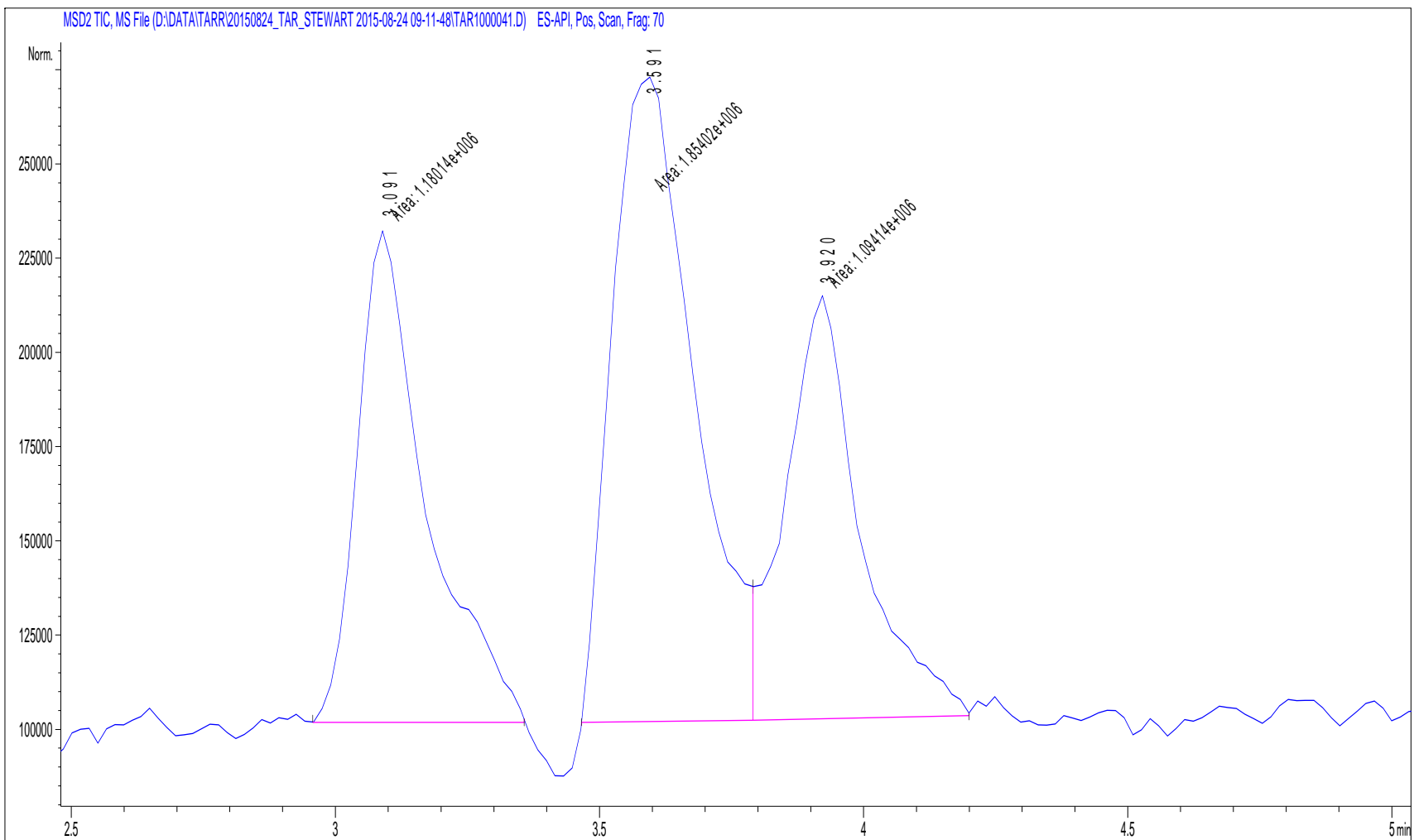


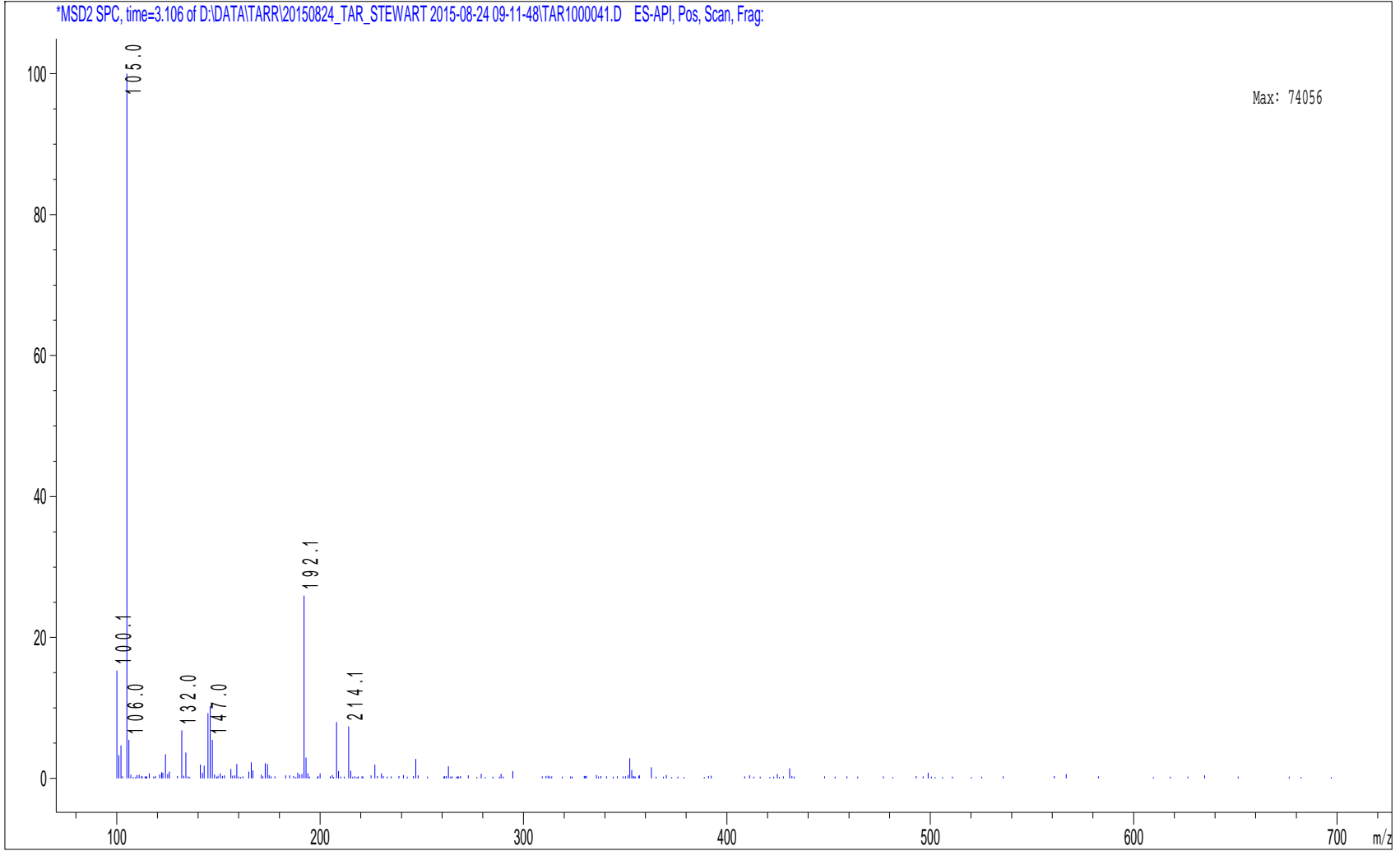


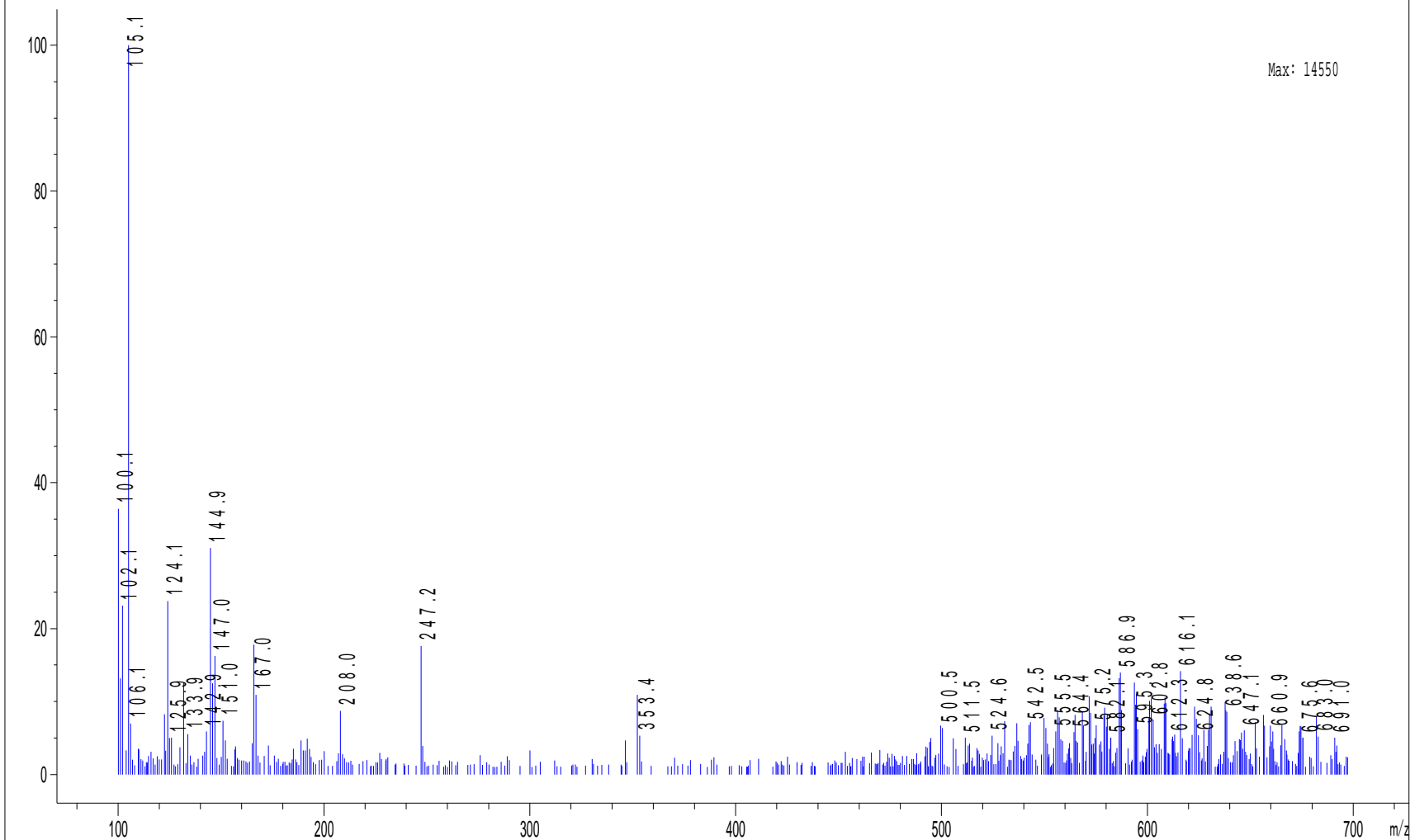


11-Aug-15  
UNTREATED SOLUTION  
P2-E-05

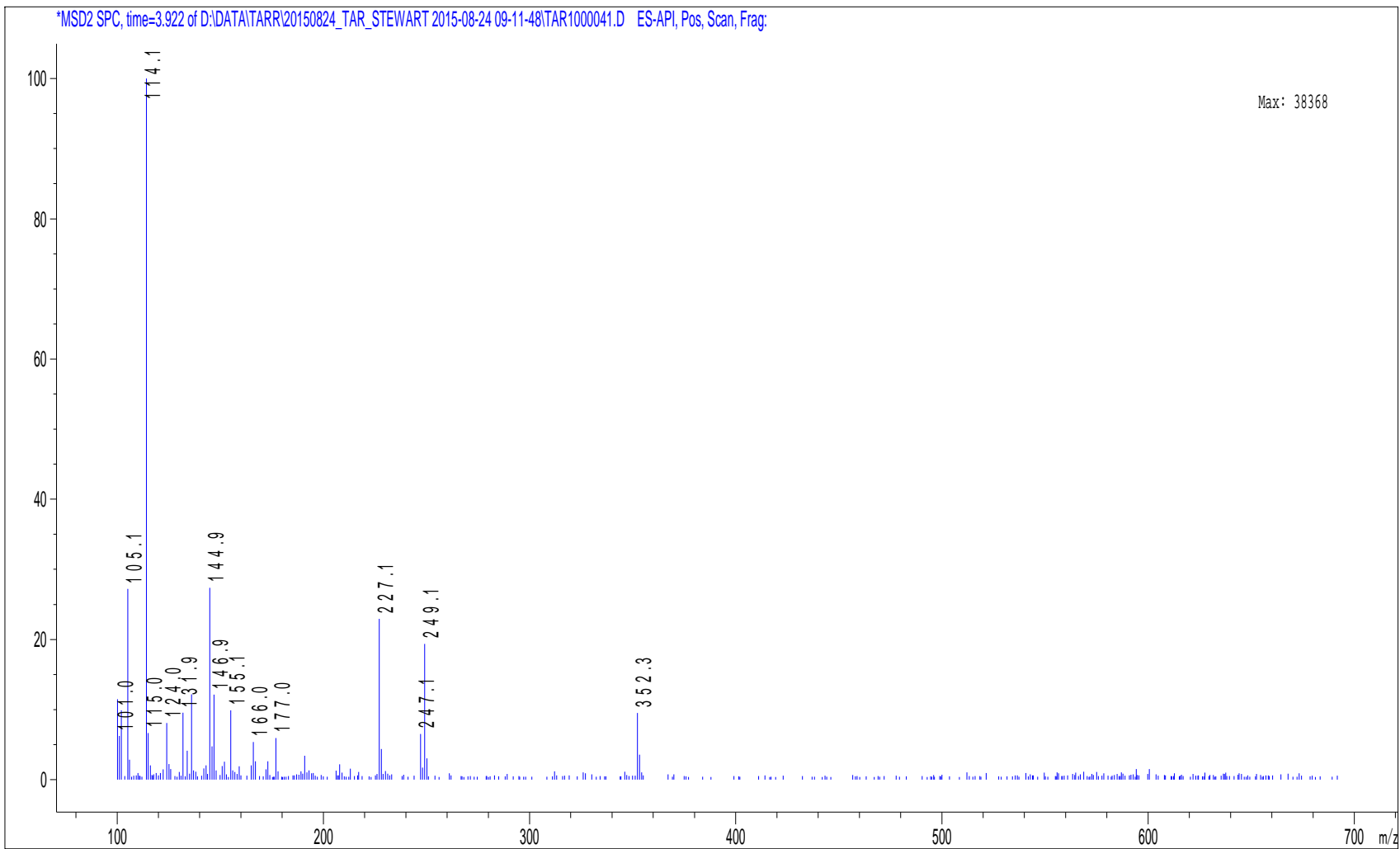








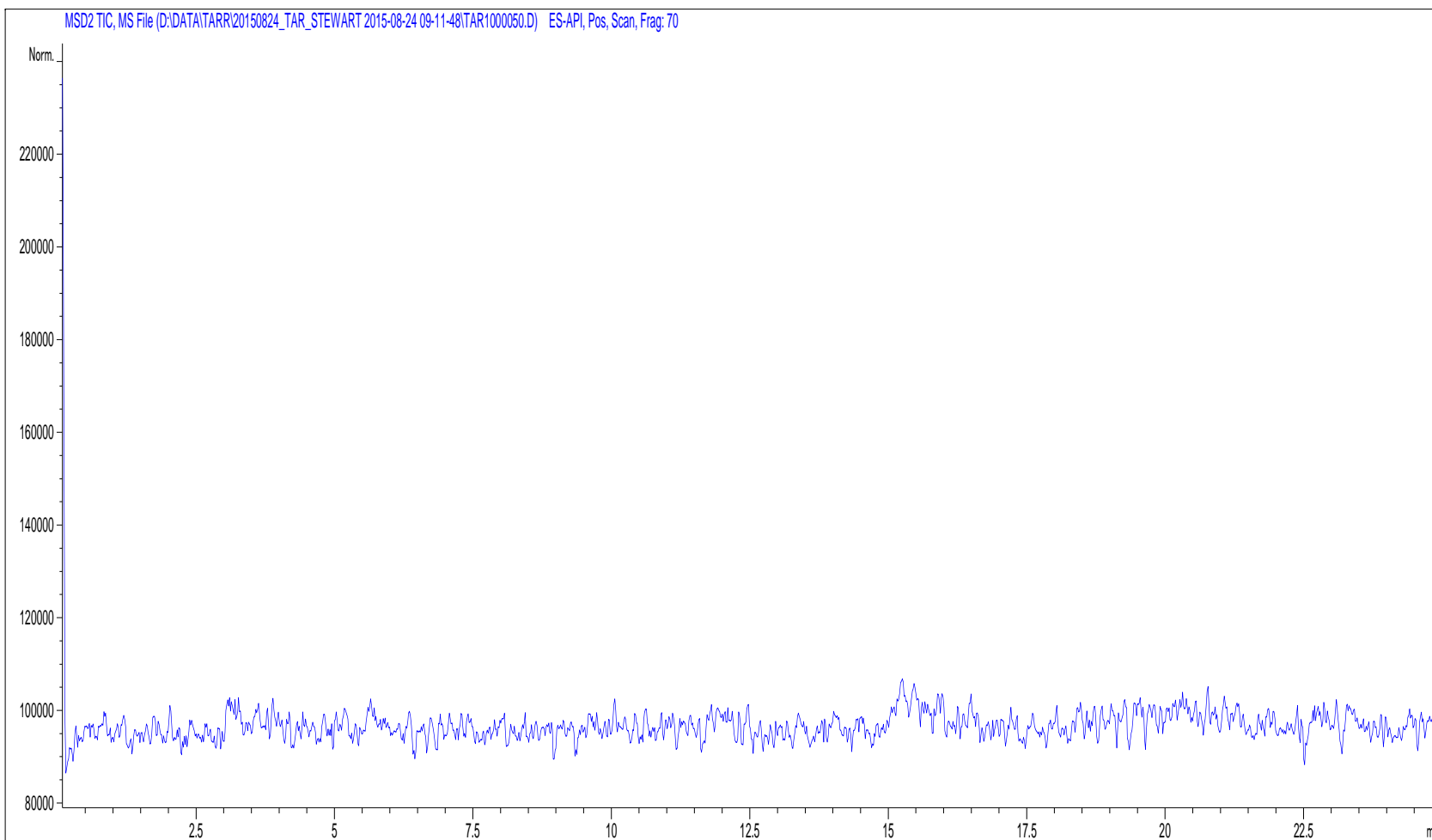
Max: 14550



---

--  
**Standard**  
**P1-A-09**

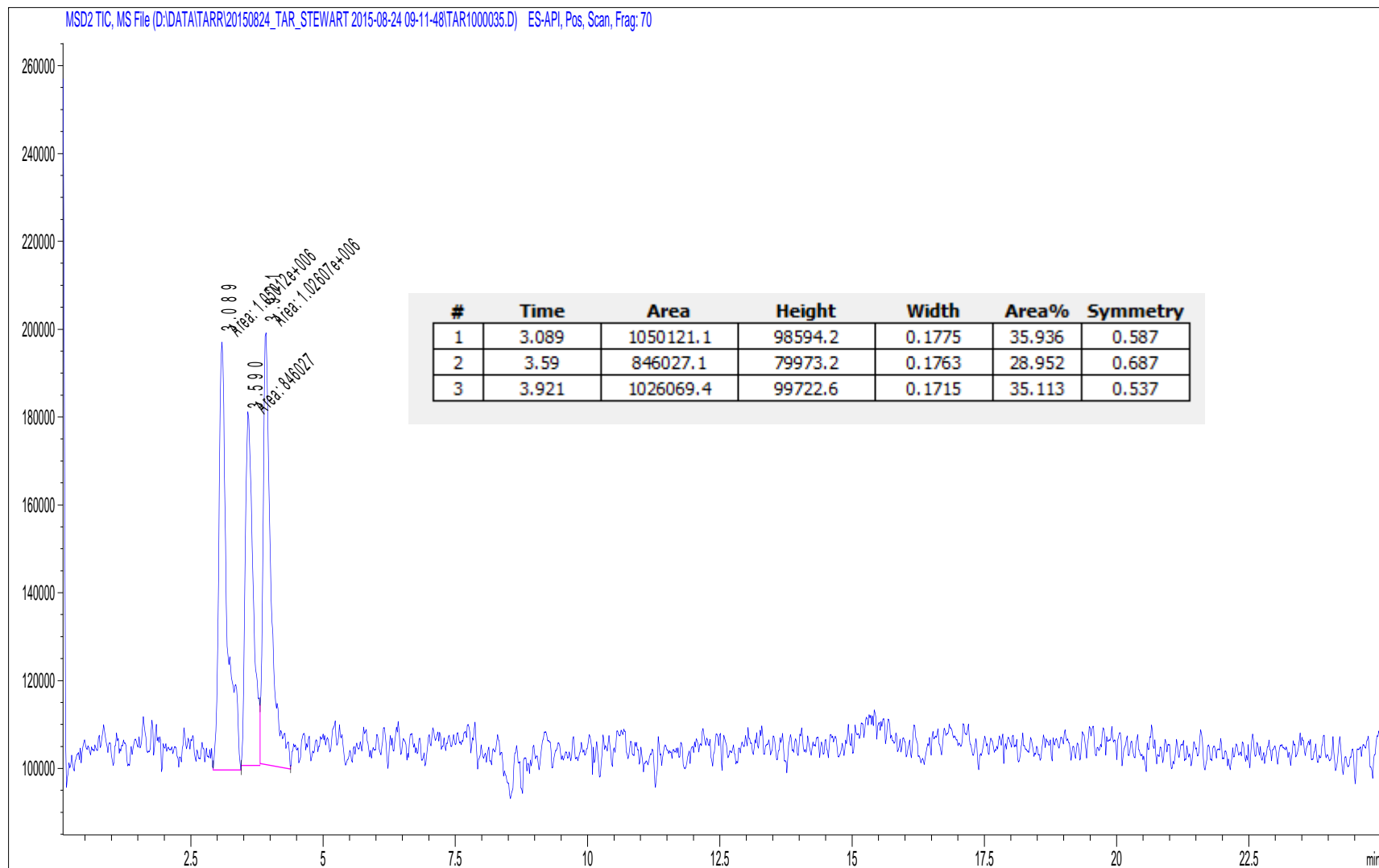
---

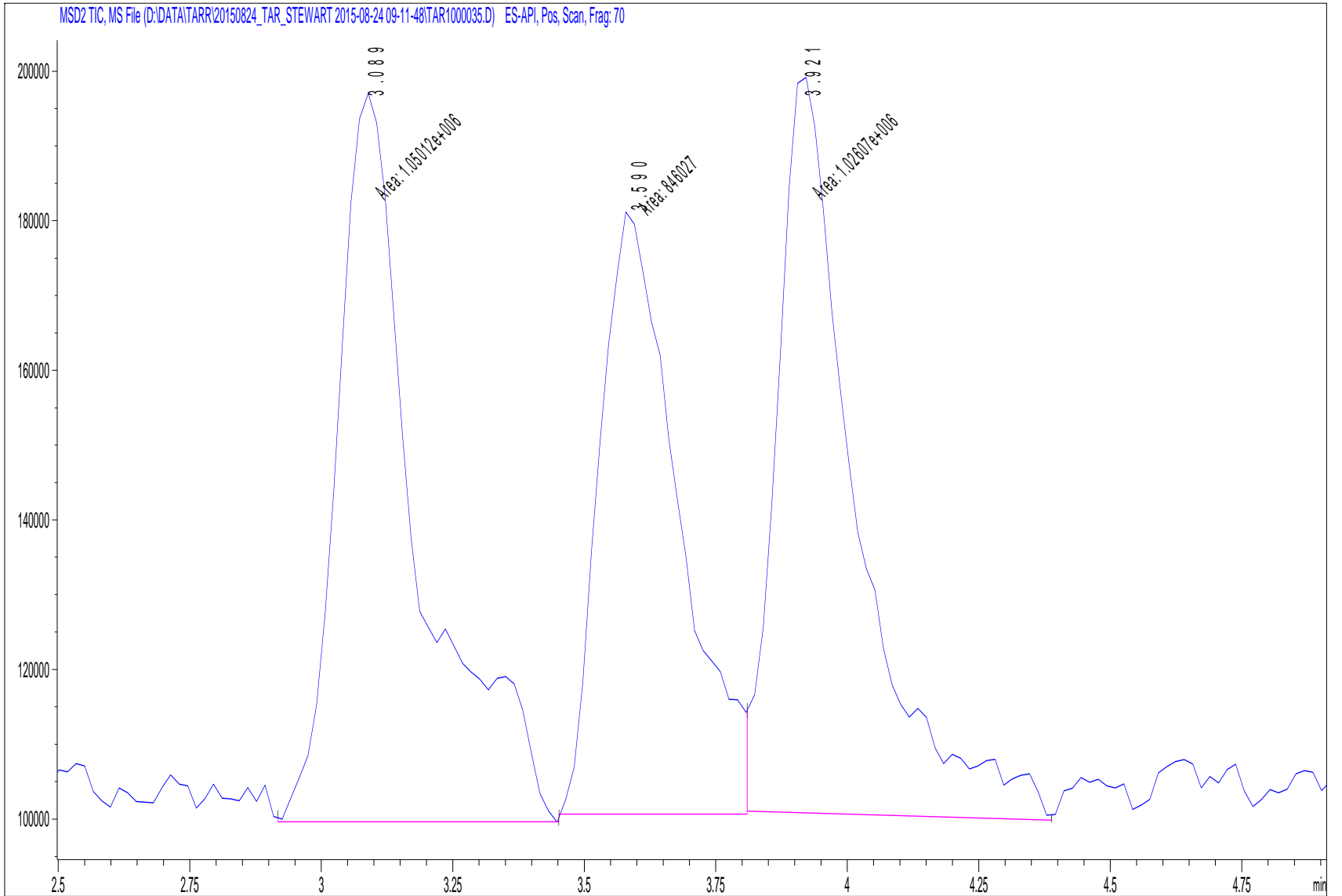


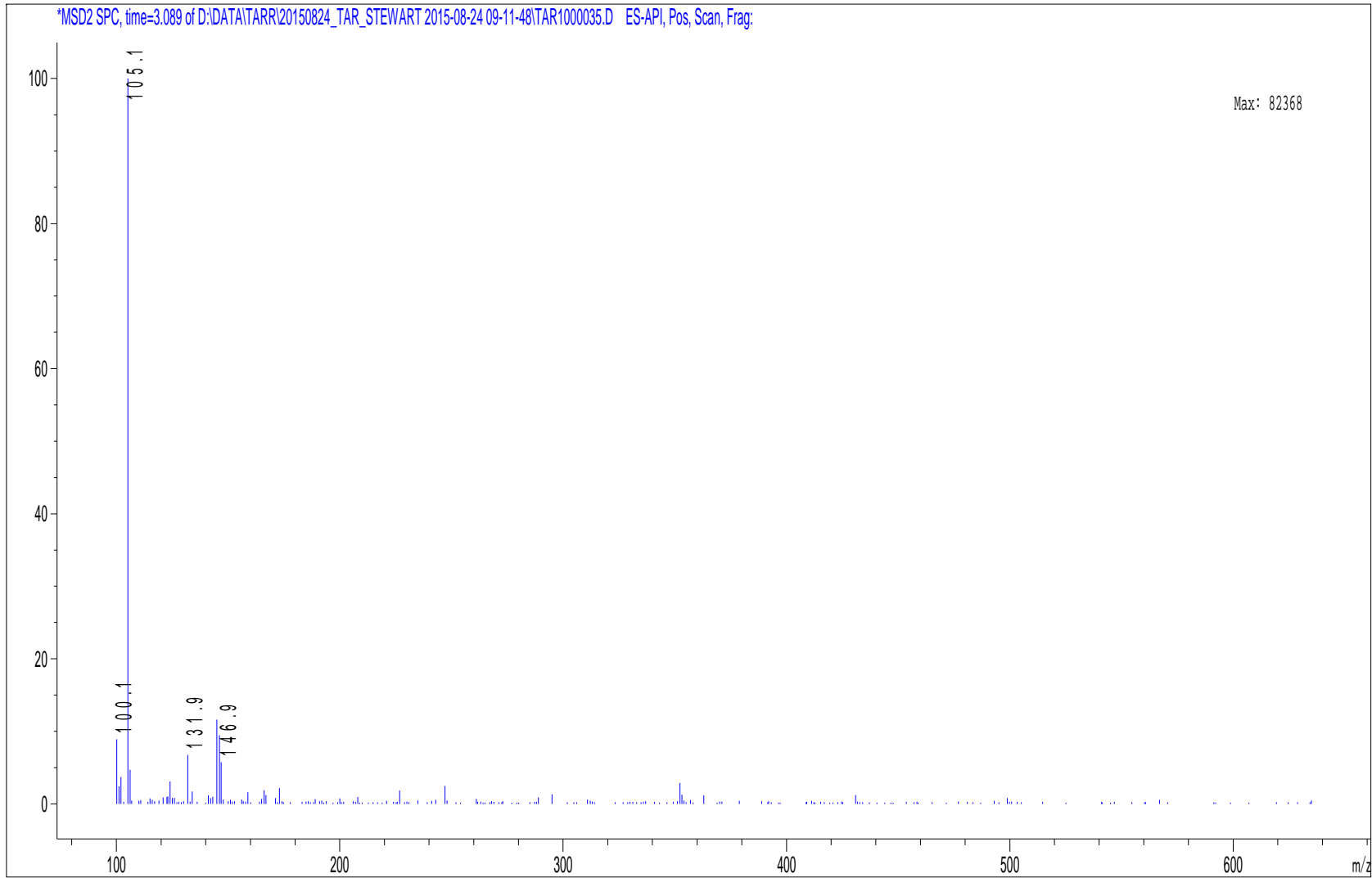


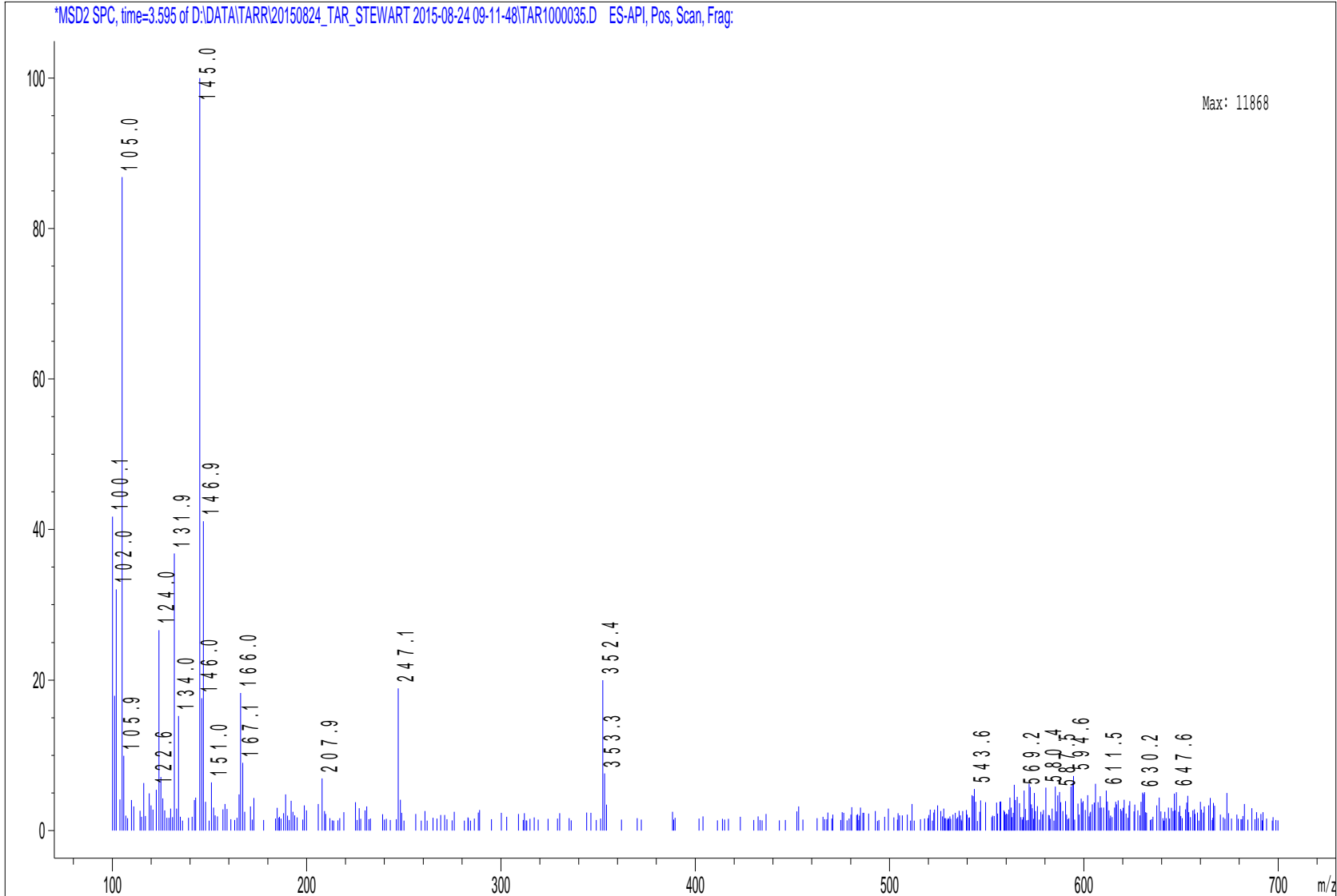
# pH 6

17-Jul-15  
H2O2 Ctrl  
P2-D-02

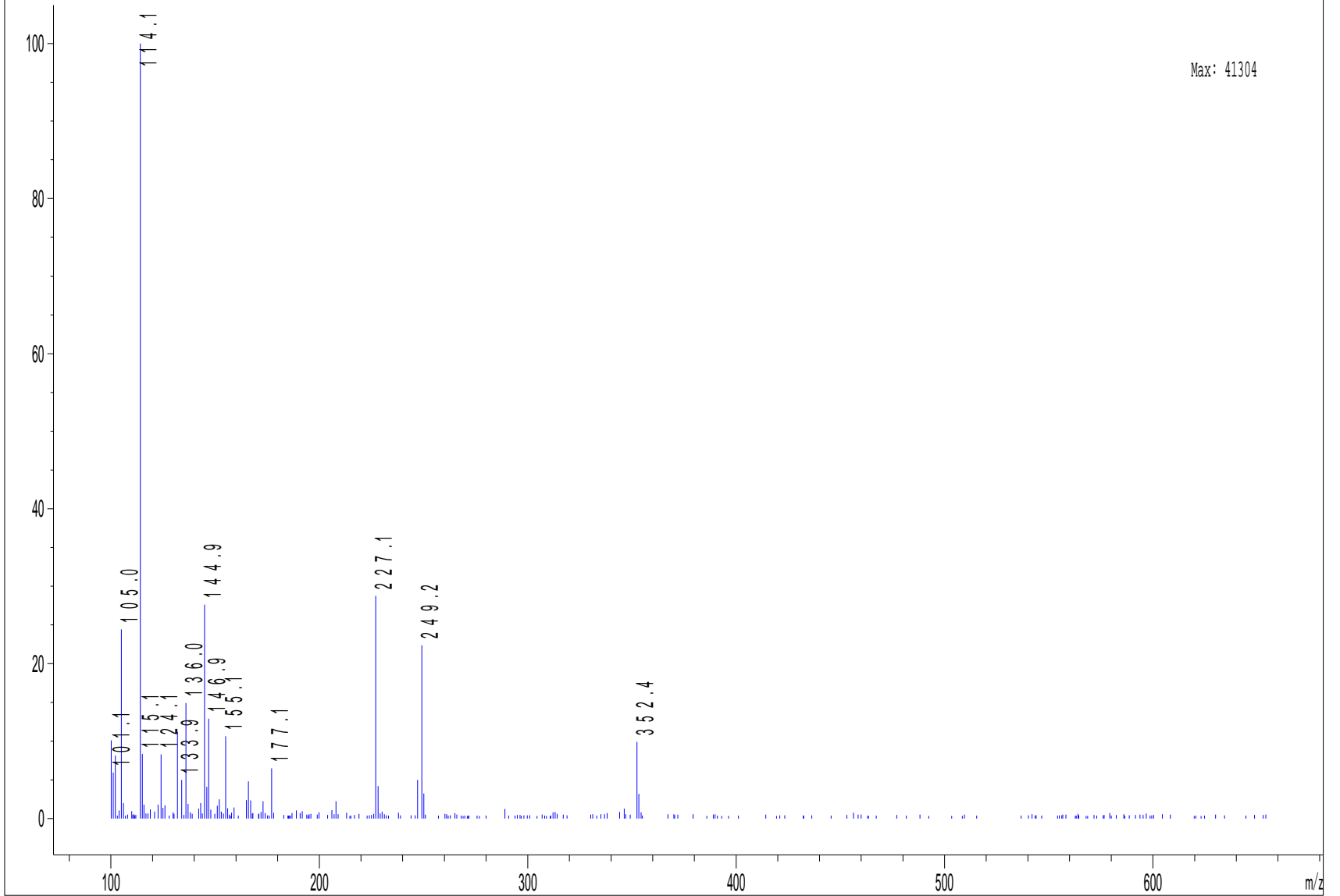








\*MSD2 SPC, time=3.922 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000035.D ES-API, Pos, Scan, Frag:

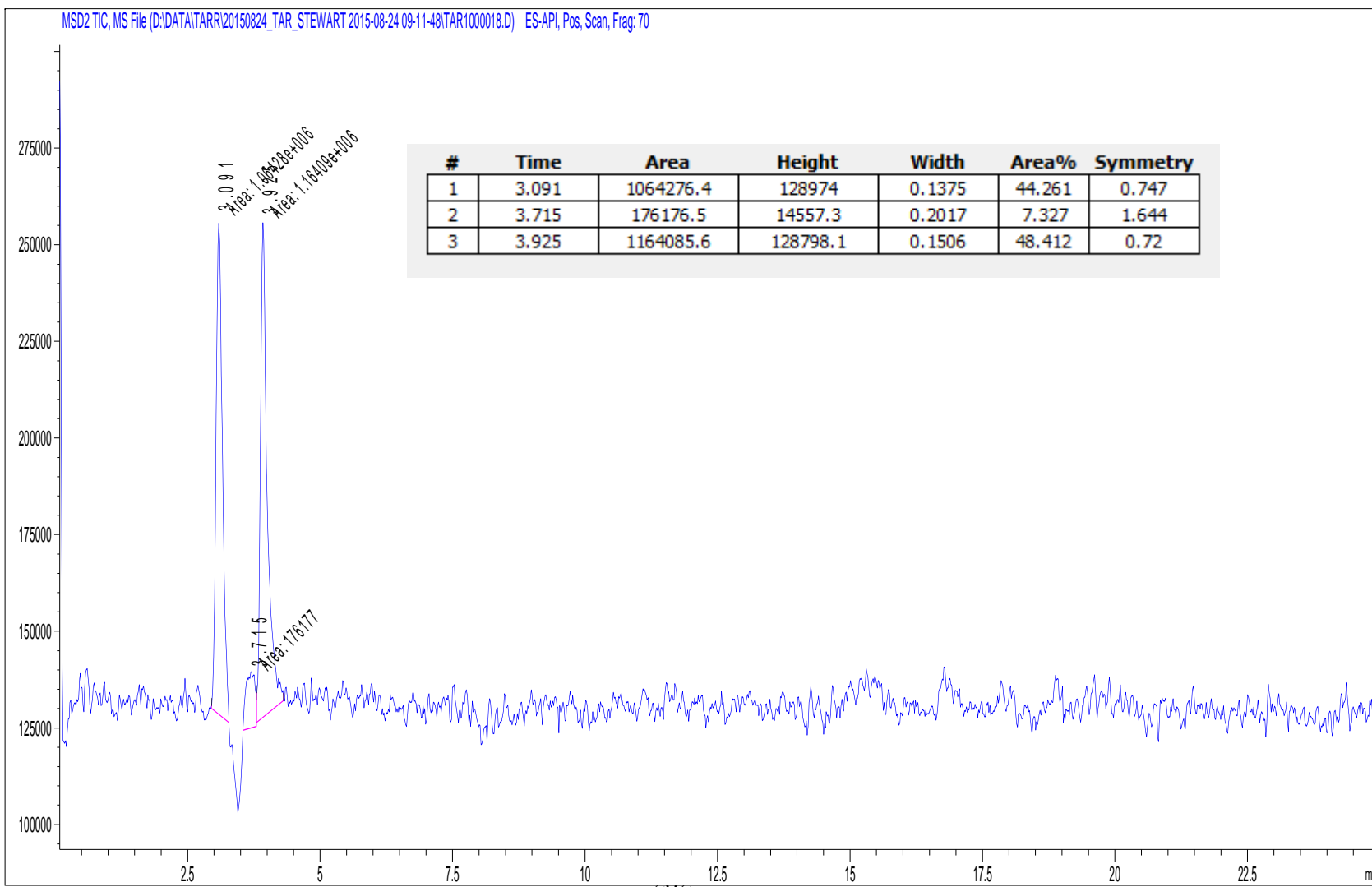


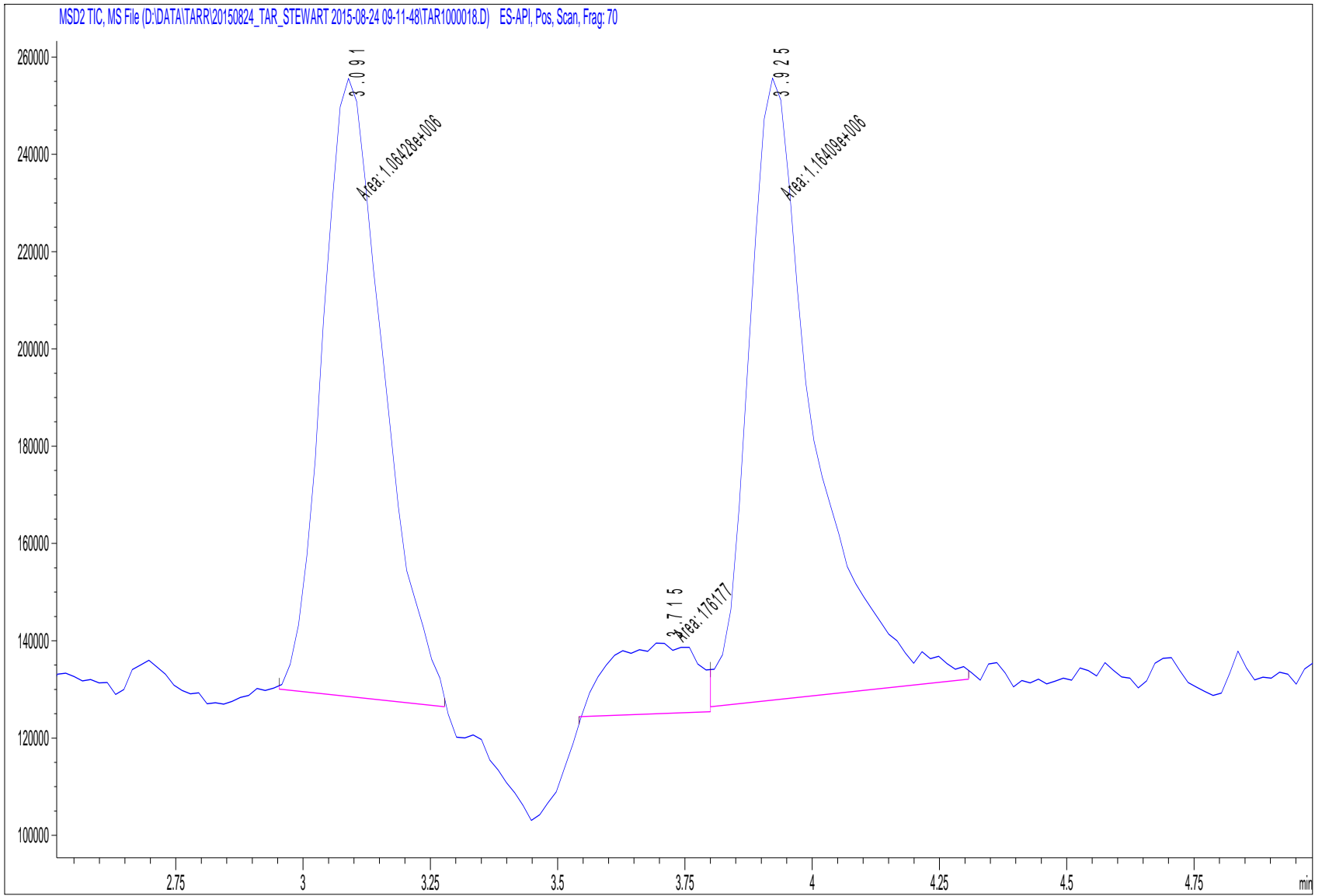
Max: 41304

14-May-15

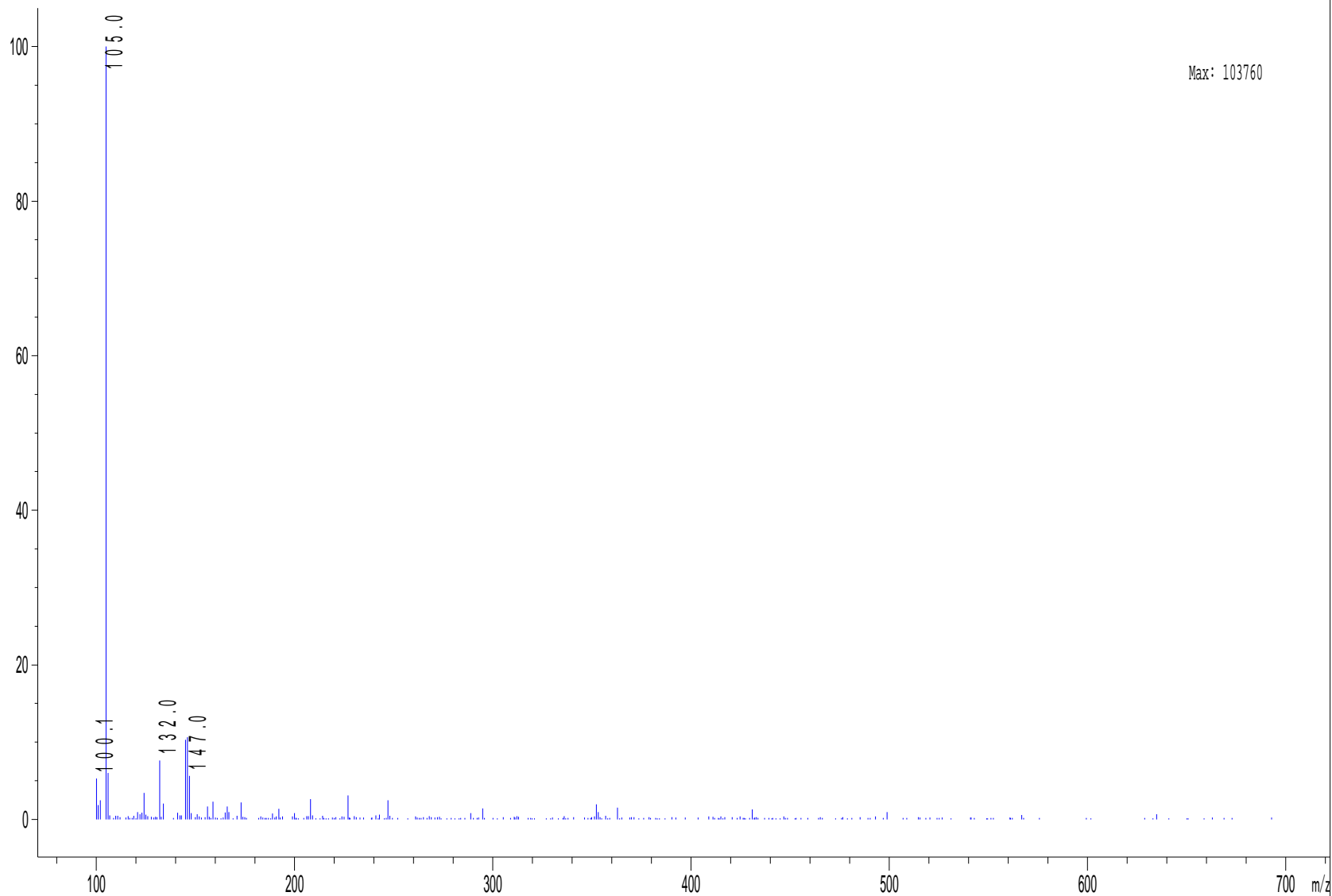
0 DC

P2-B-01



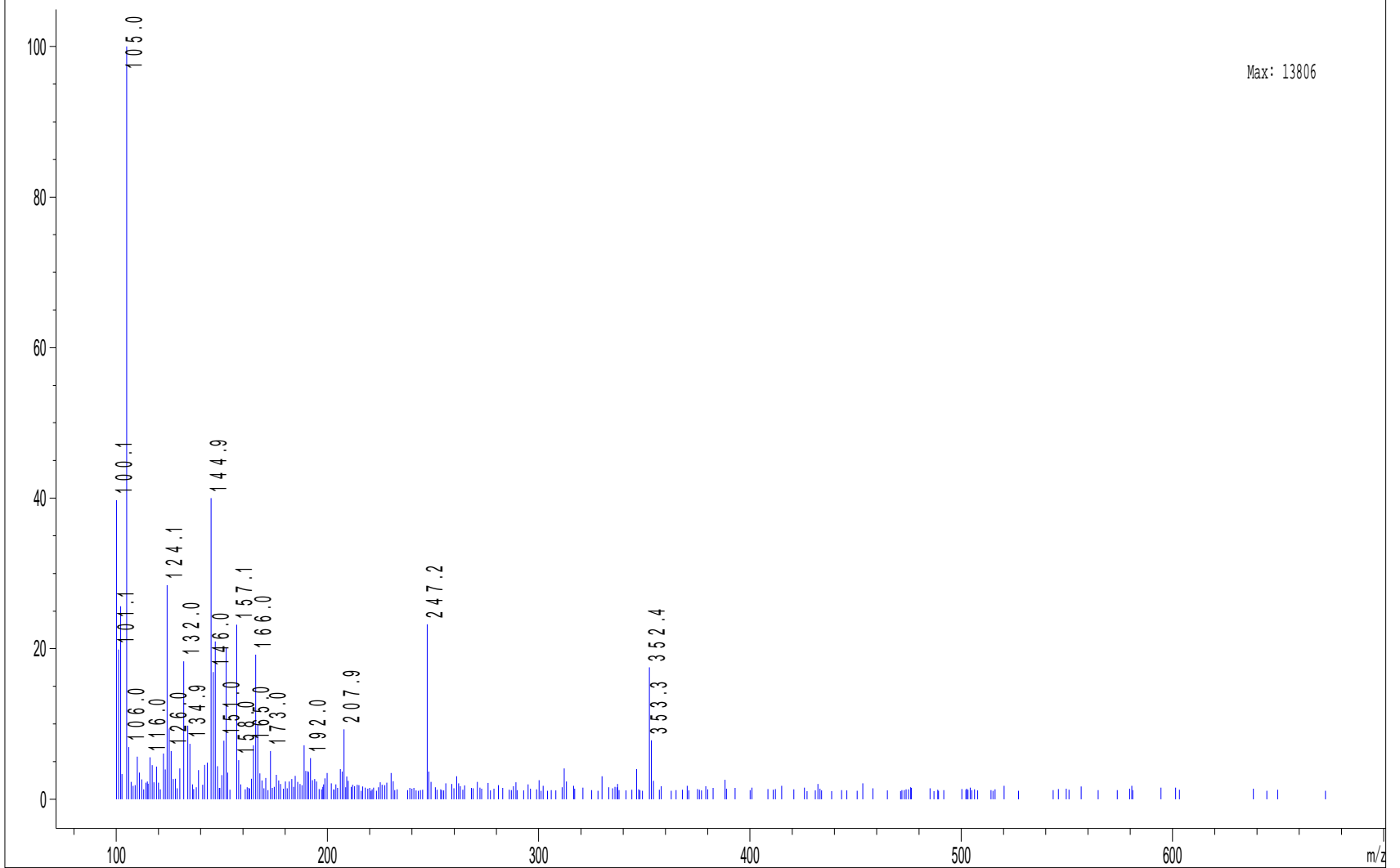


\*MSD2 SPC, time=3.089 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09:11:48\TAR1000018.D ES-API, Pos, Scan, Frag:

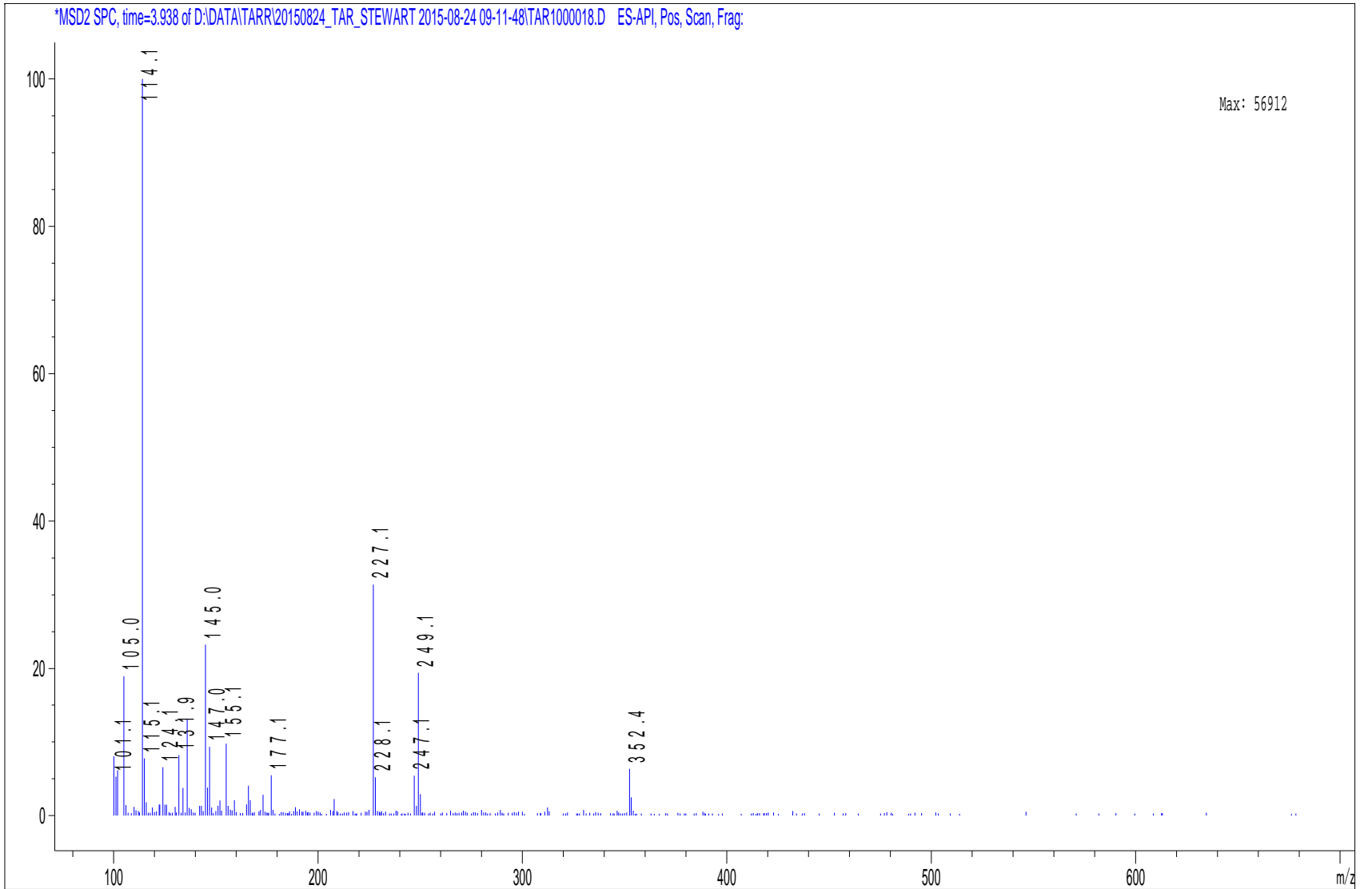




\*MSD2 SPC, time=3.677 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09:11:48\TAR1000018.D ES-API, Pos, Scan, Frag:



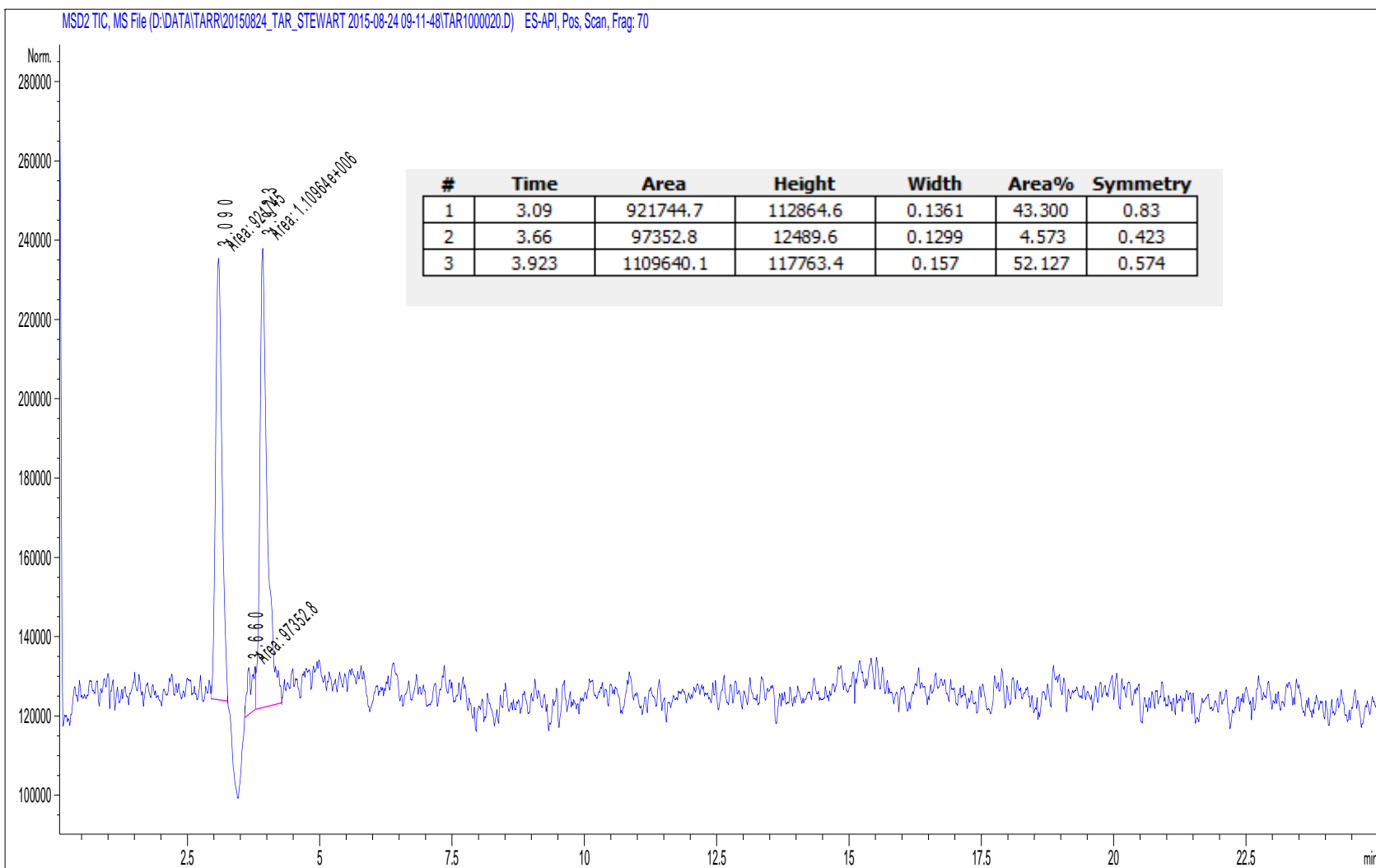
Max: 13806

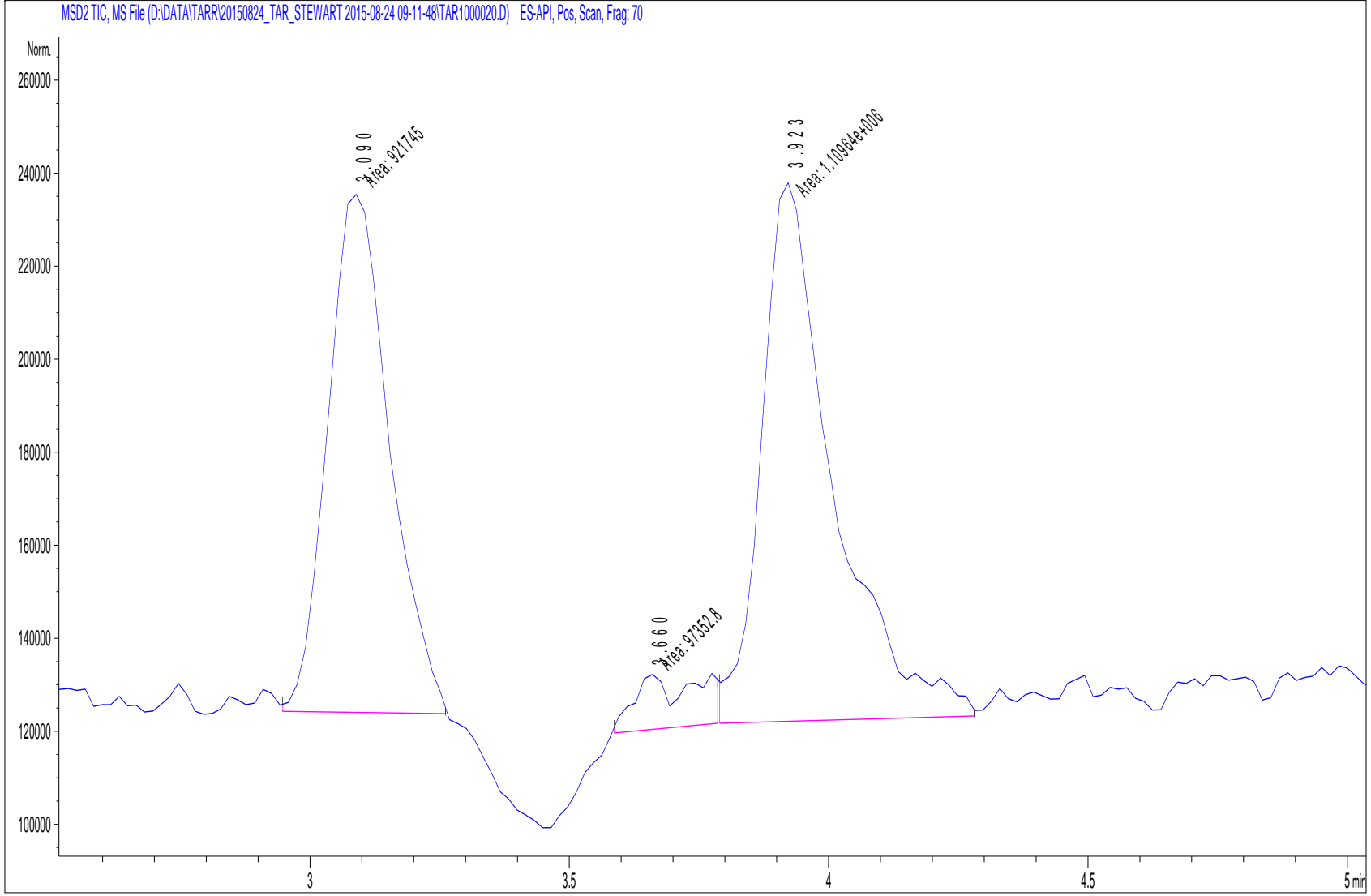


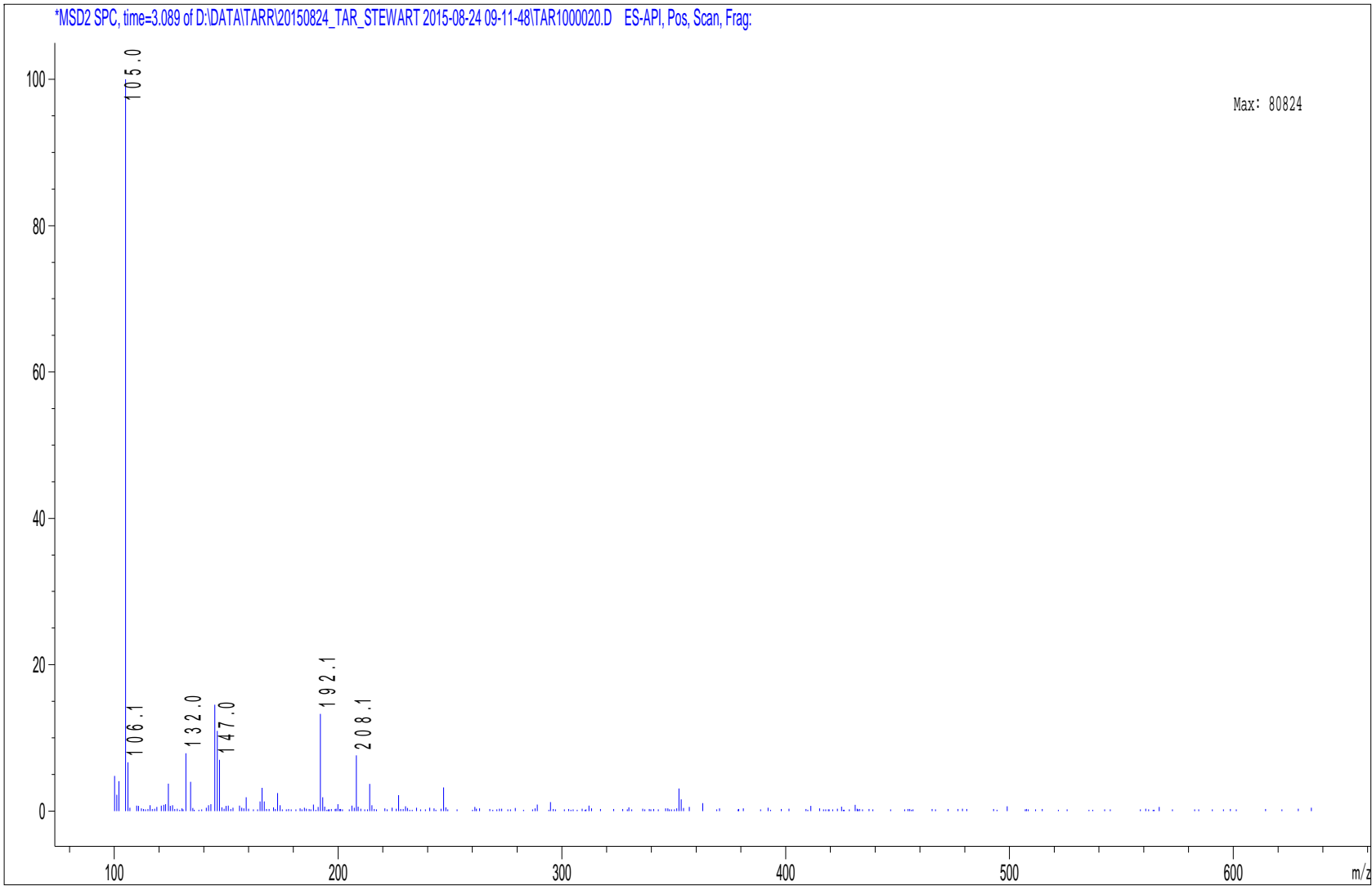
29-Jun-15

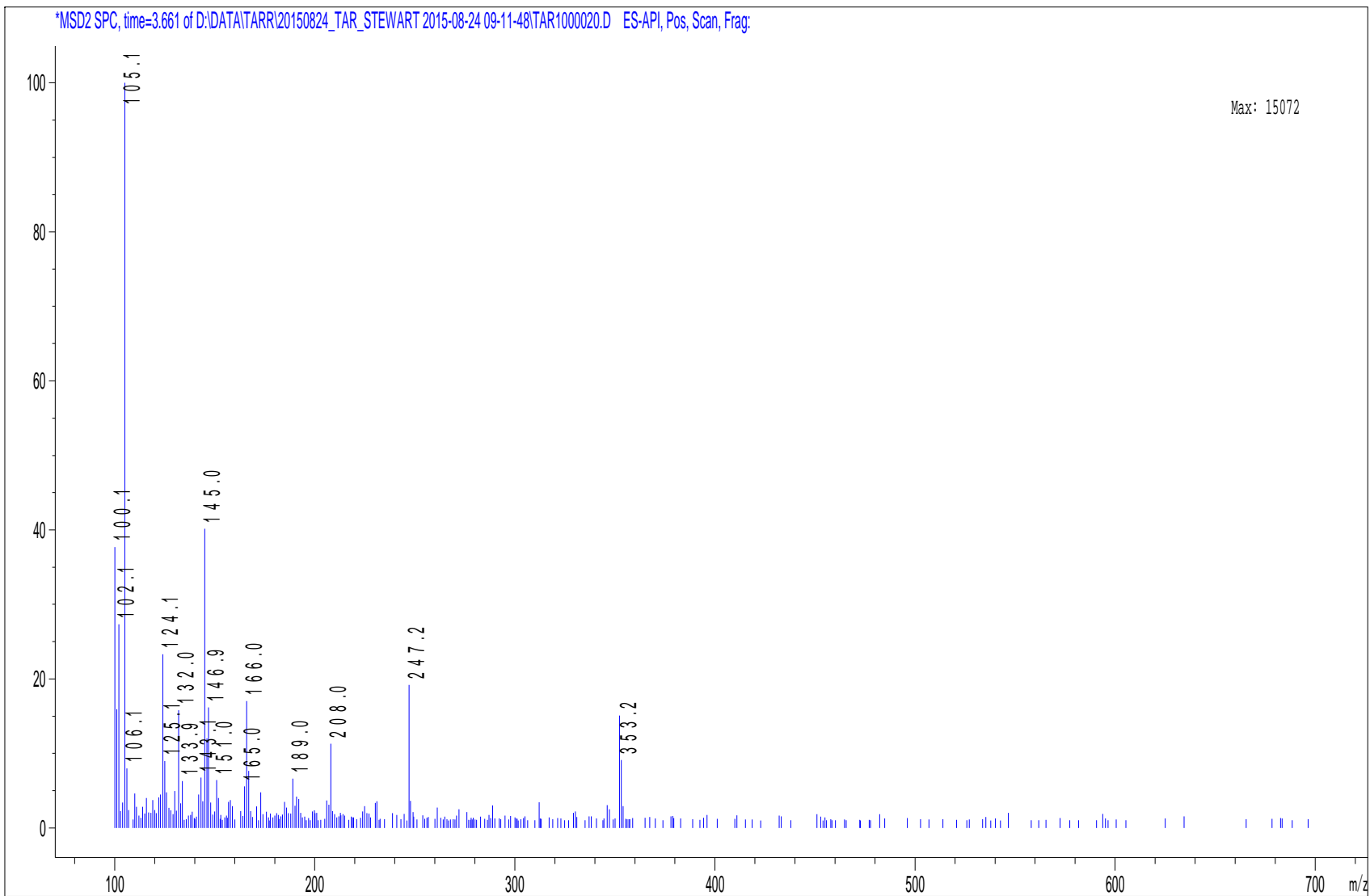
5 DC

P2-C-02

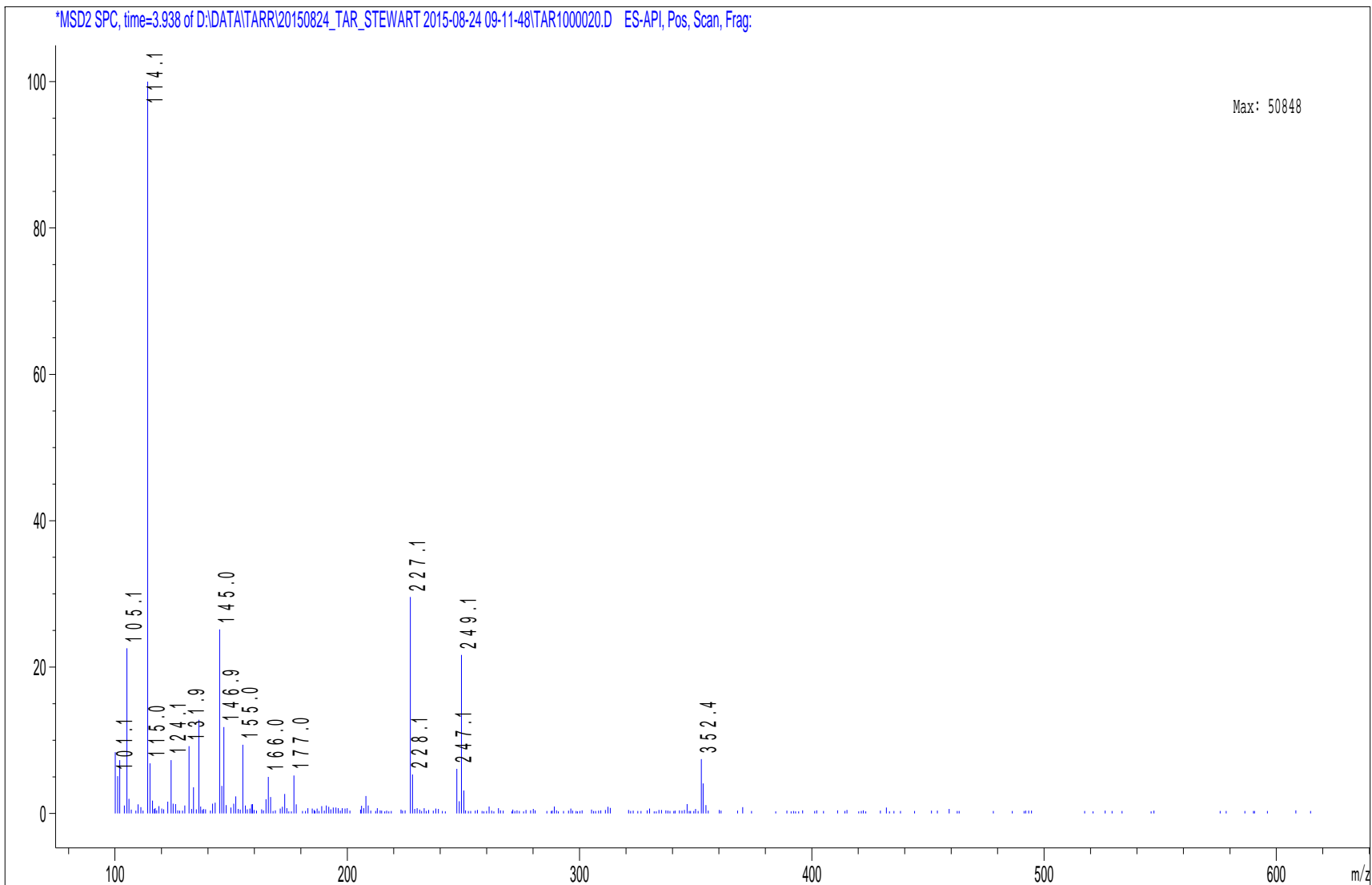








\*MSD2 SPC, time=3.938 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000020.D ES-API, Pos, Scan, Frag:



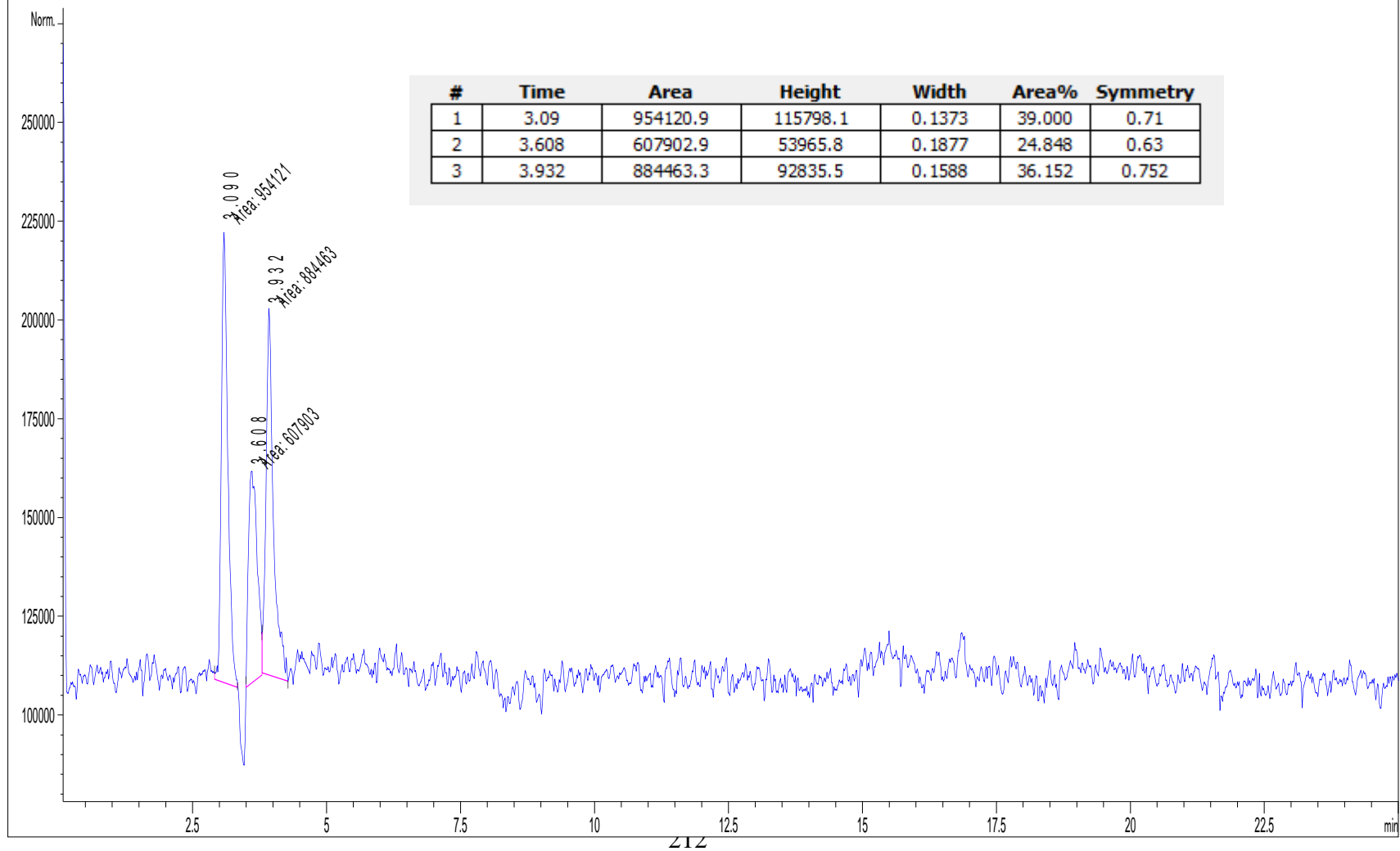
Max: 50848

7-Aug-15

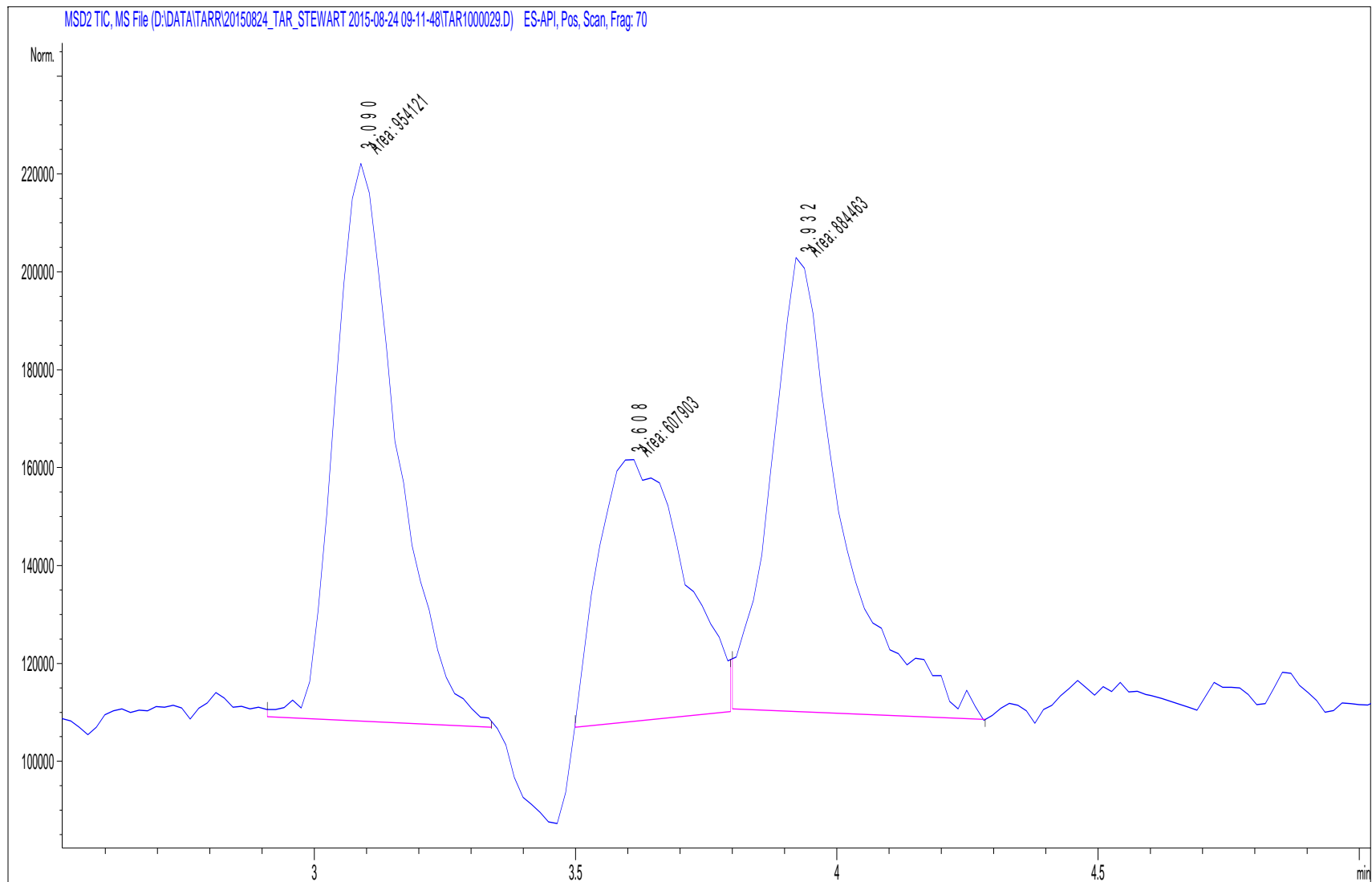
10 DC

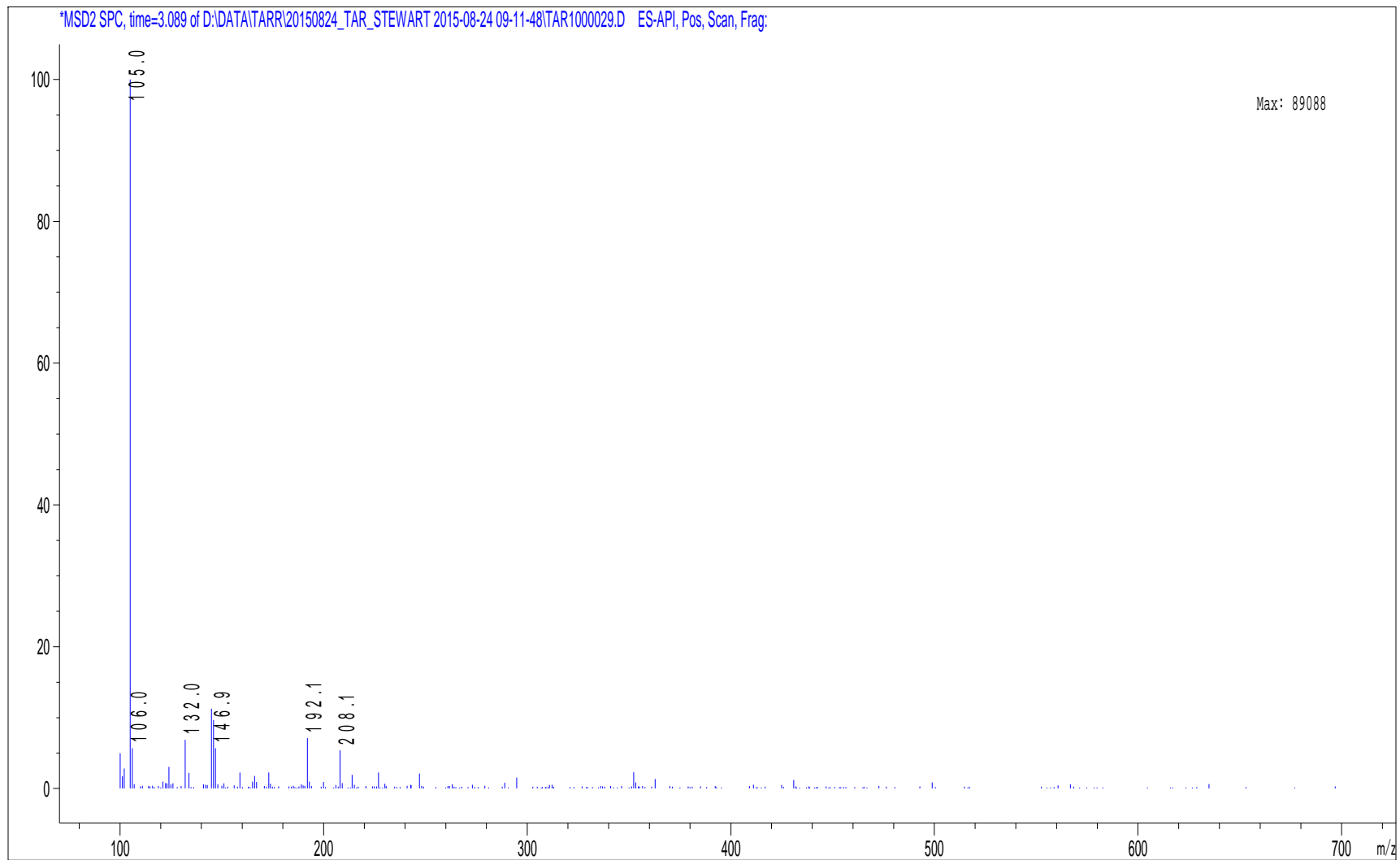
P2-D-08

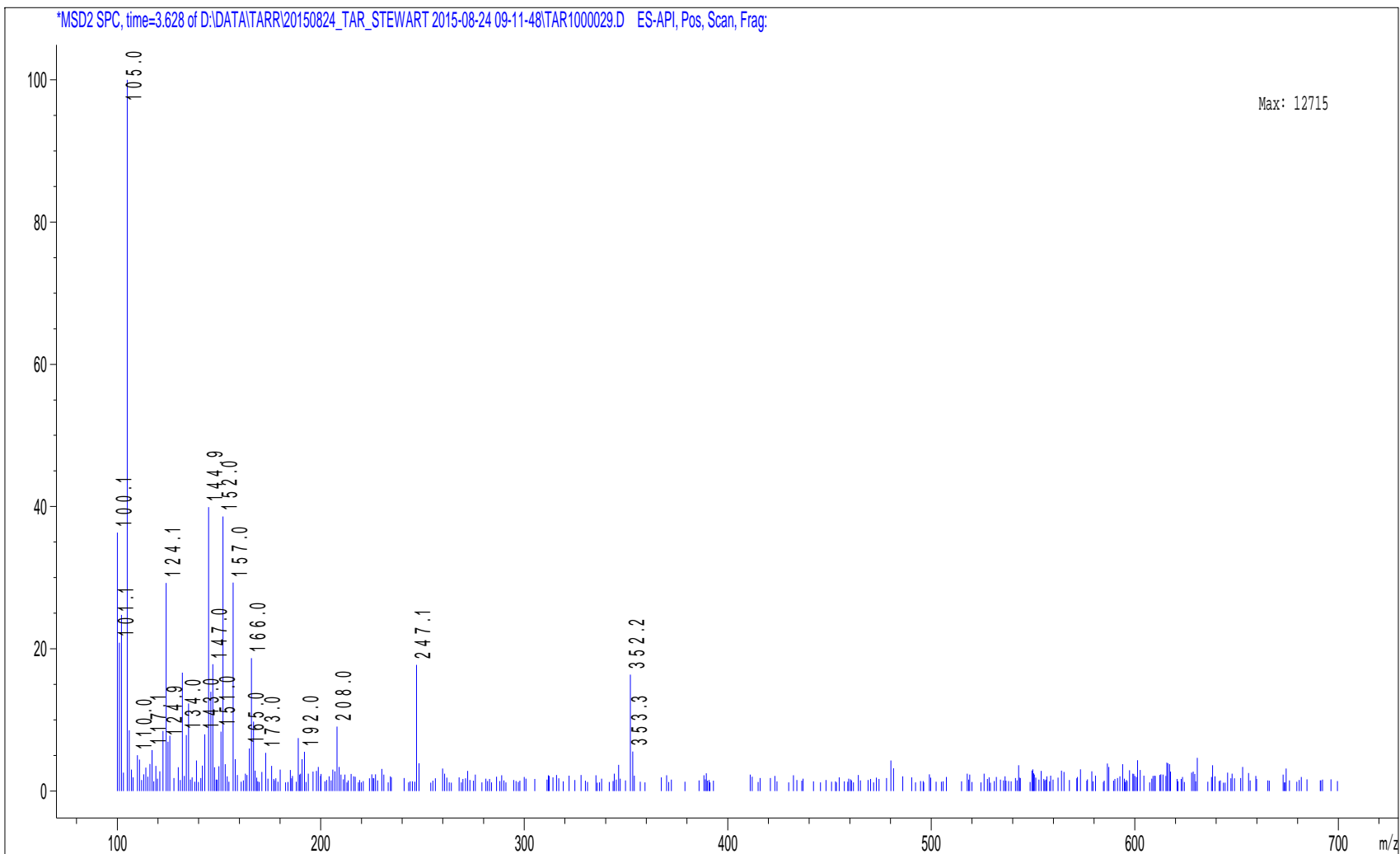
MSD2 TIC, MS File (D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000029.D) ES-API, Pos, Scan, Frag: 70



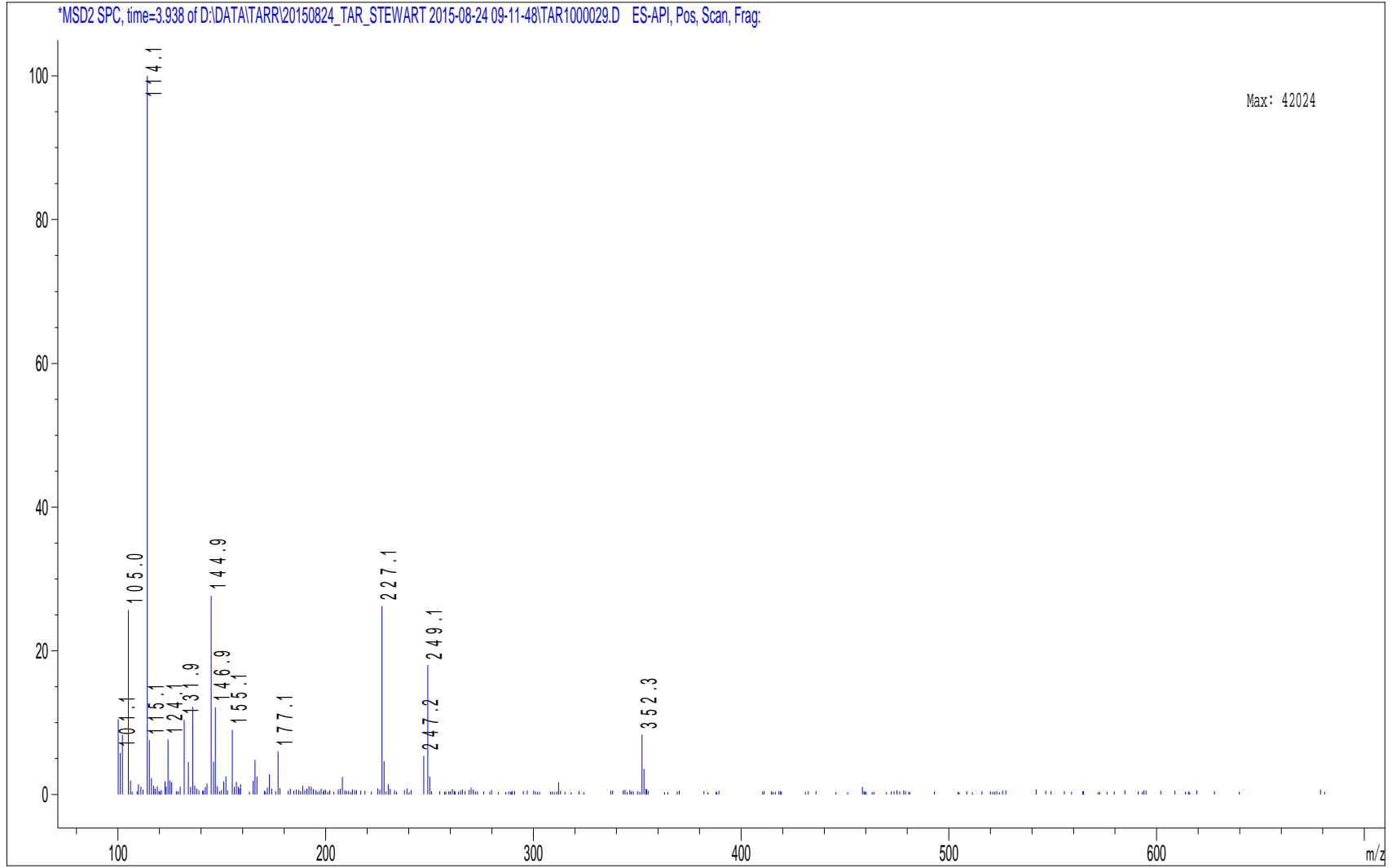








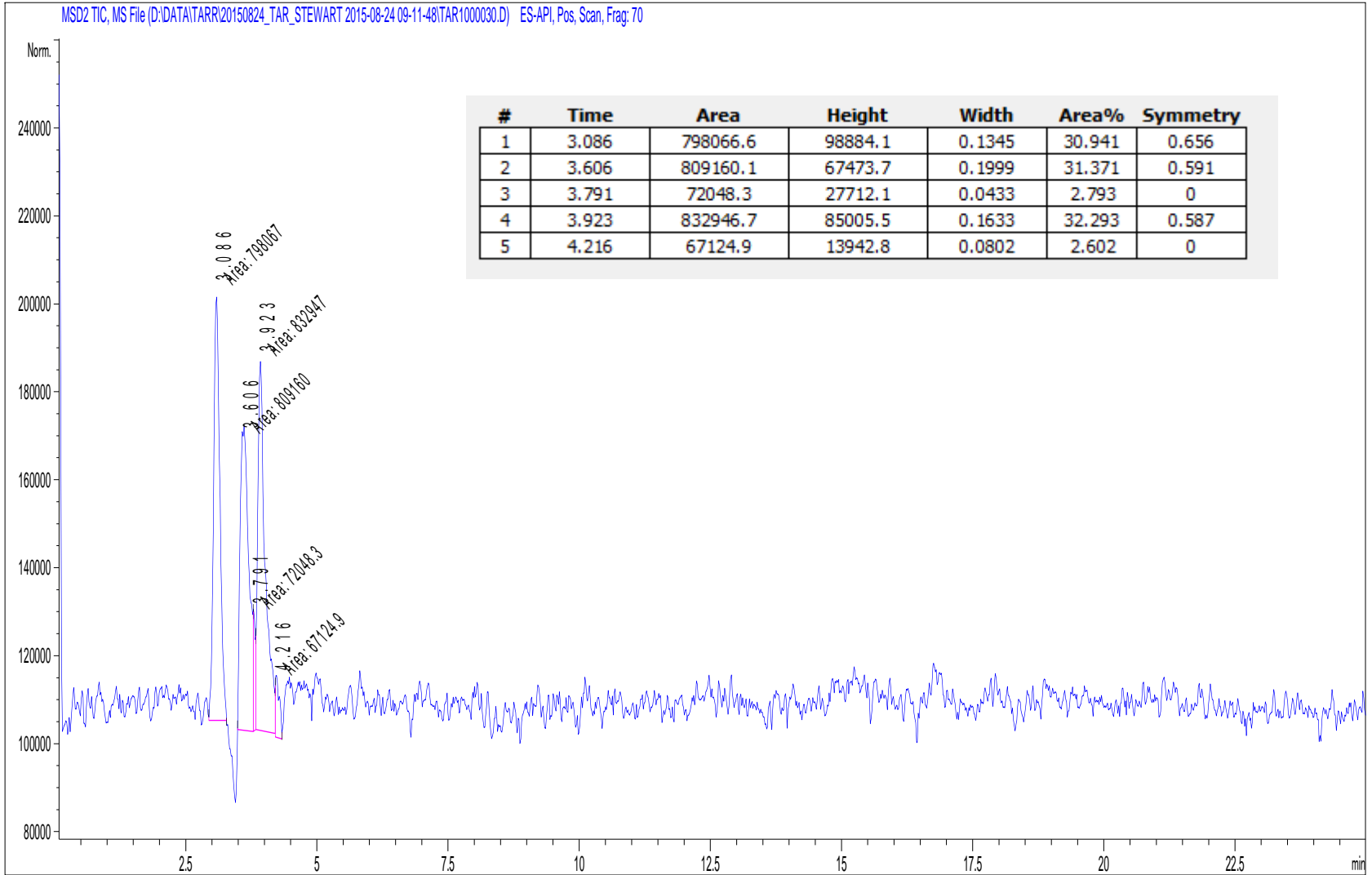
\*MSD2 SPC, time=3.938 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000029.D ES-API, Pos, Scan, Frag:

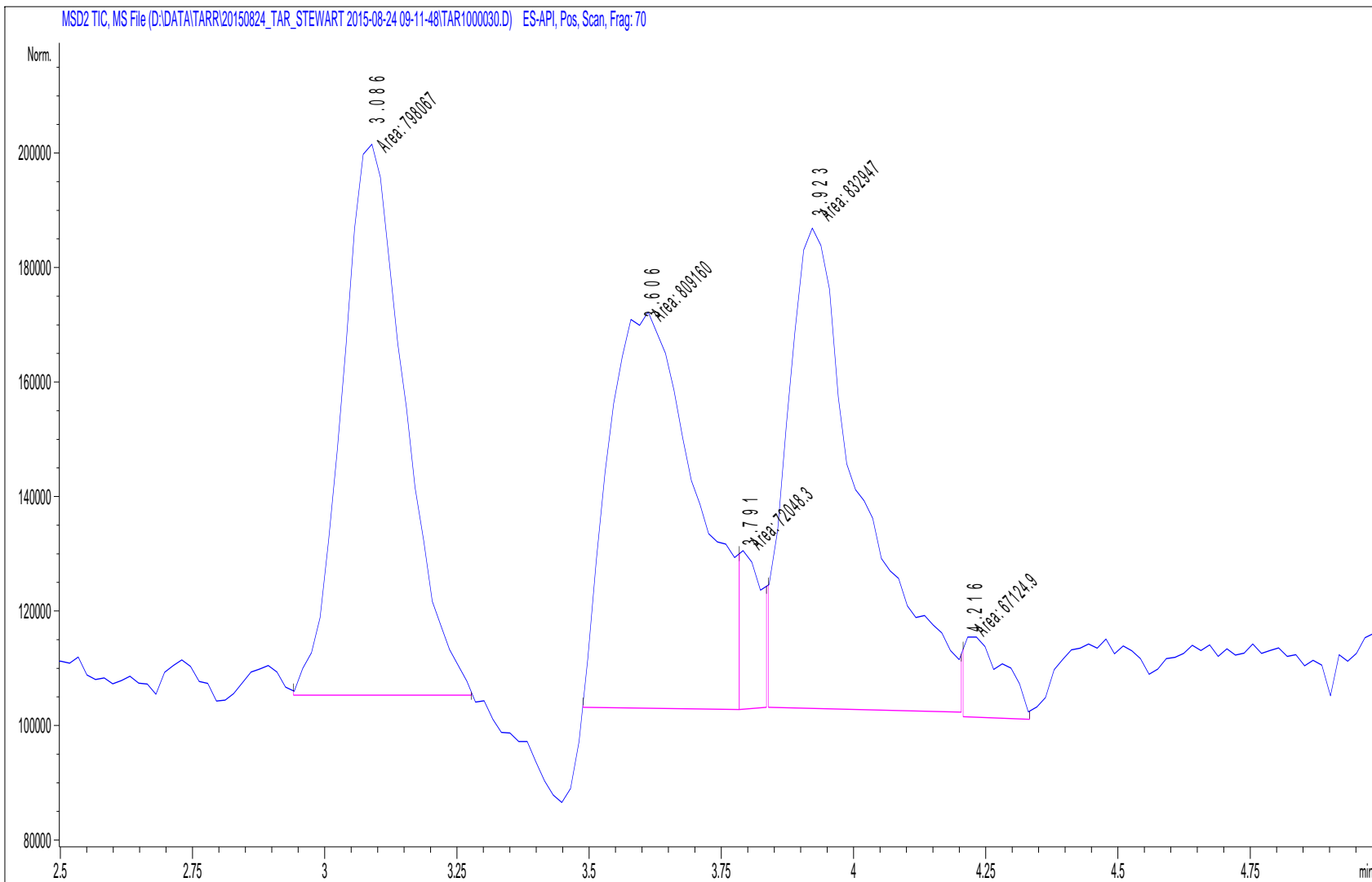


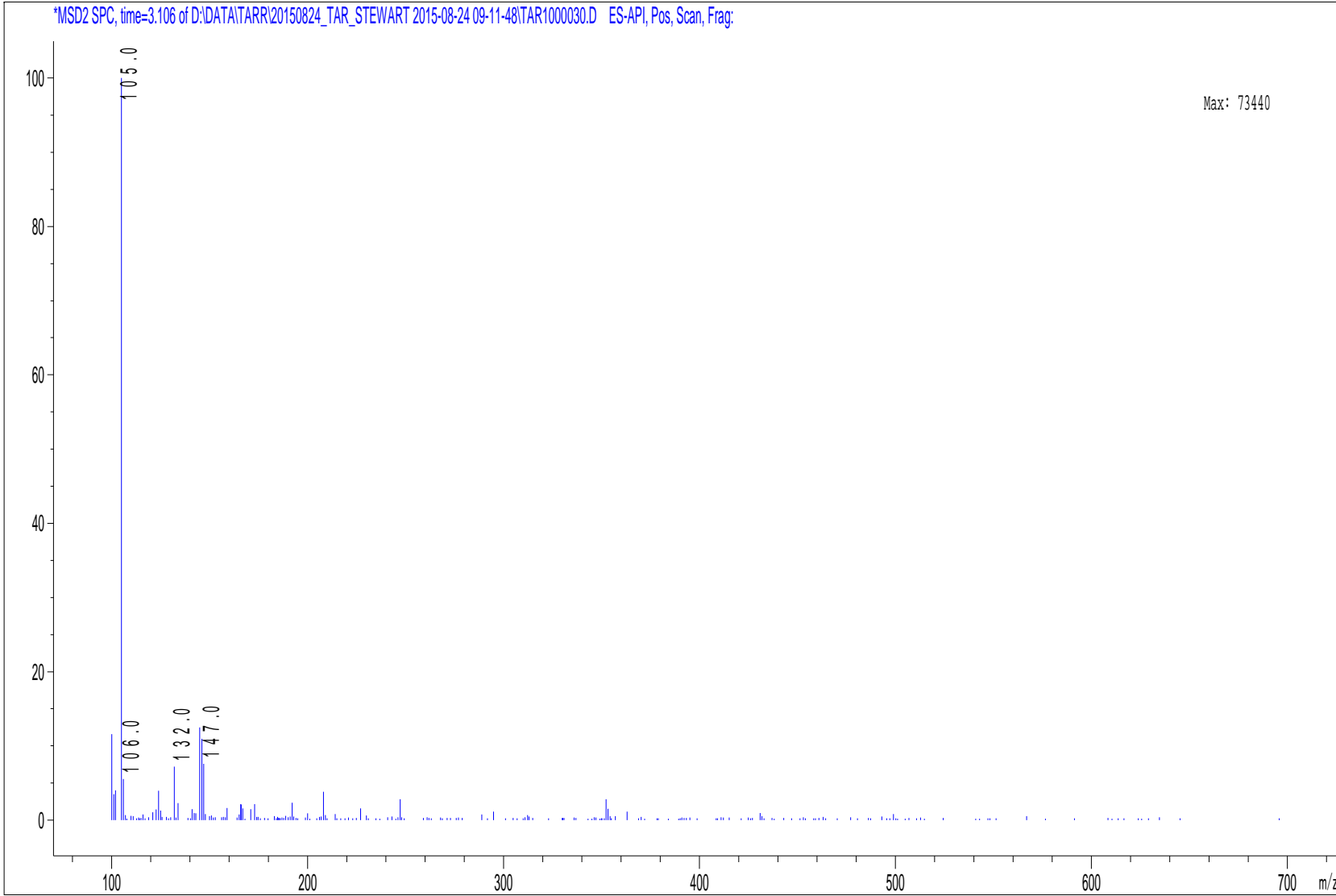
31-Jul-15

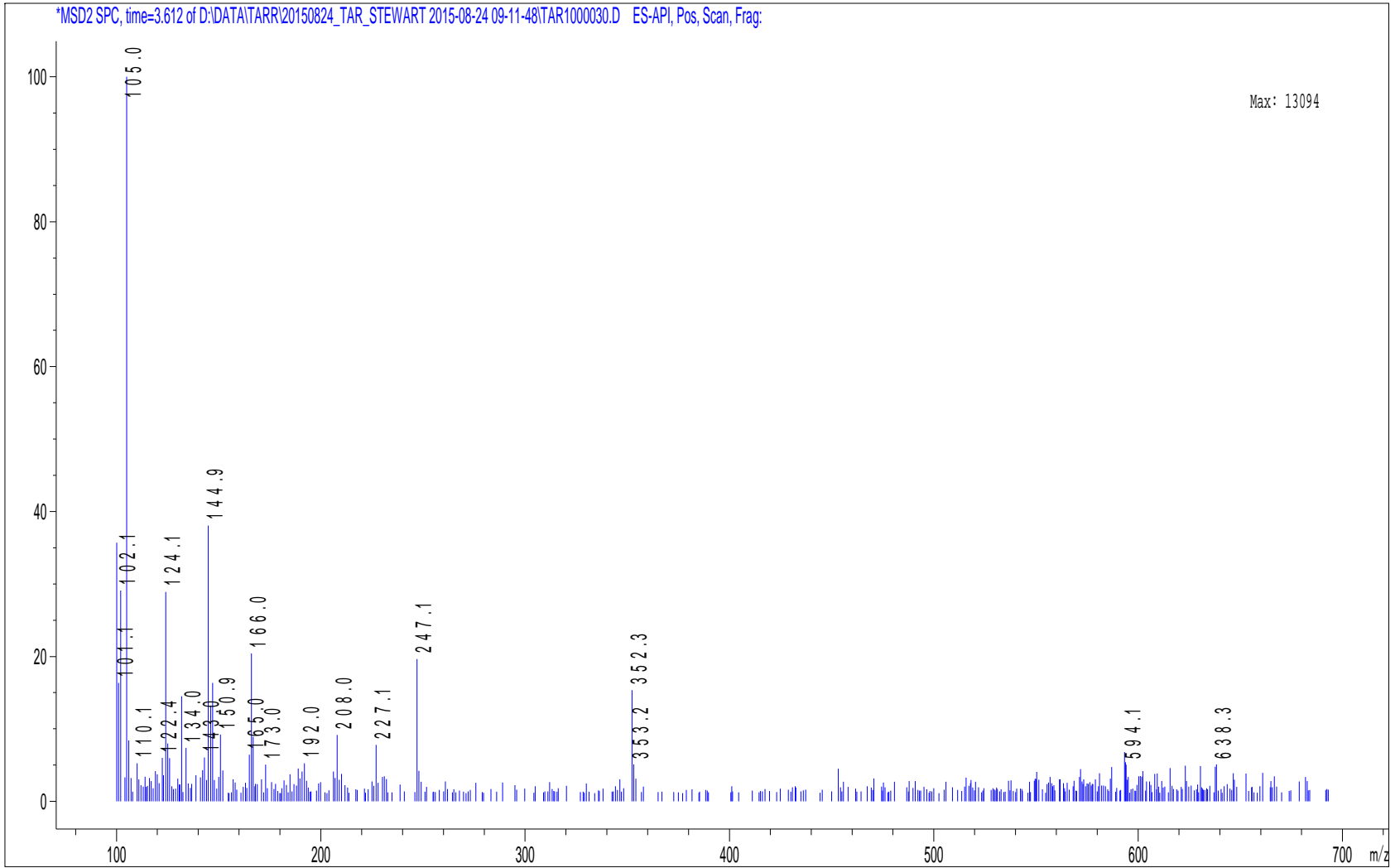
10 DC Problem (removal went up)

P2-D-07

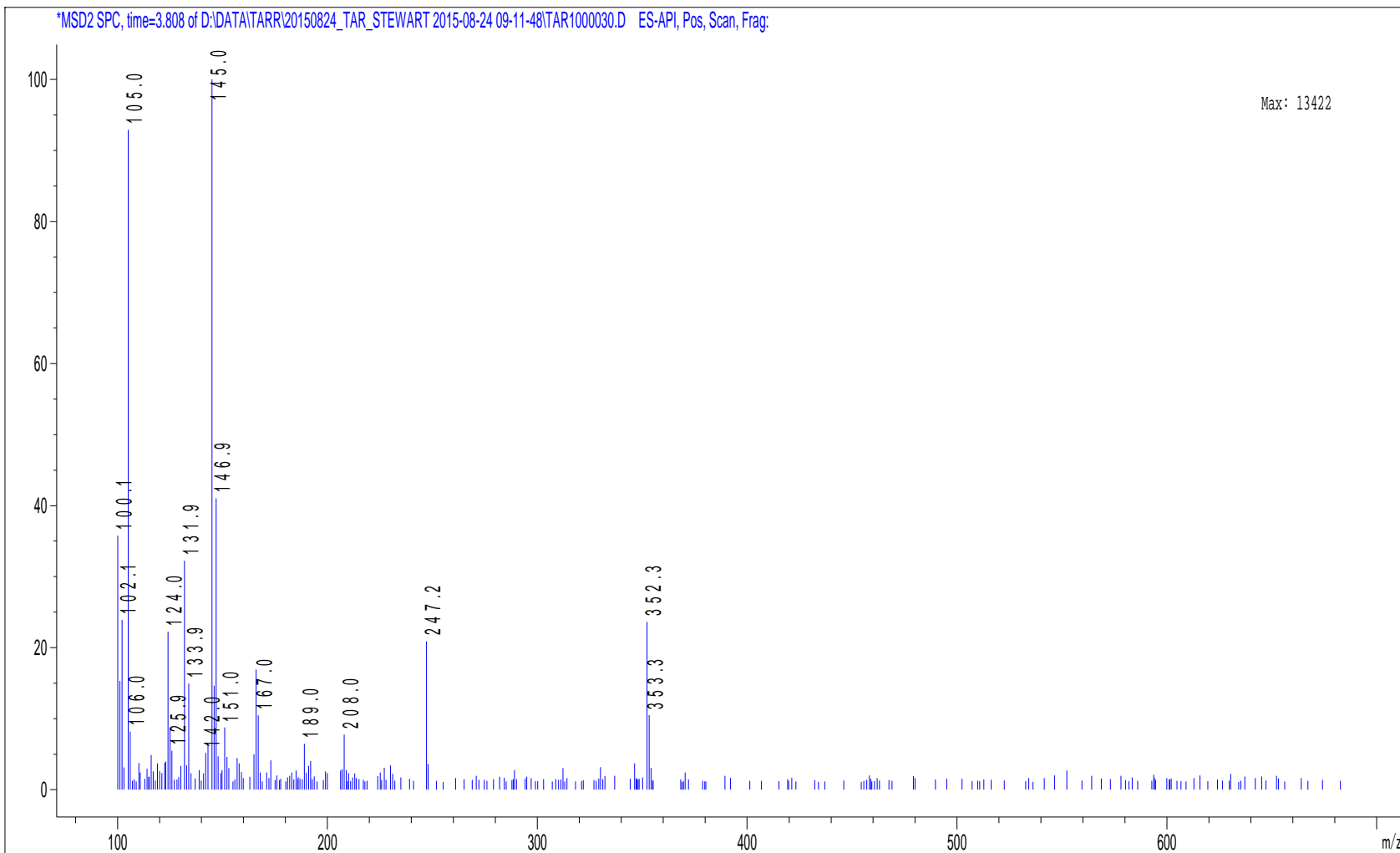




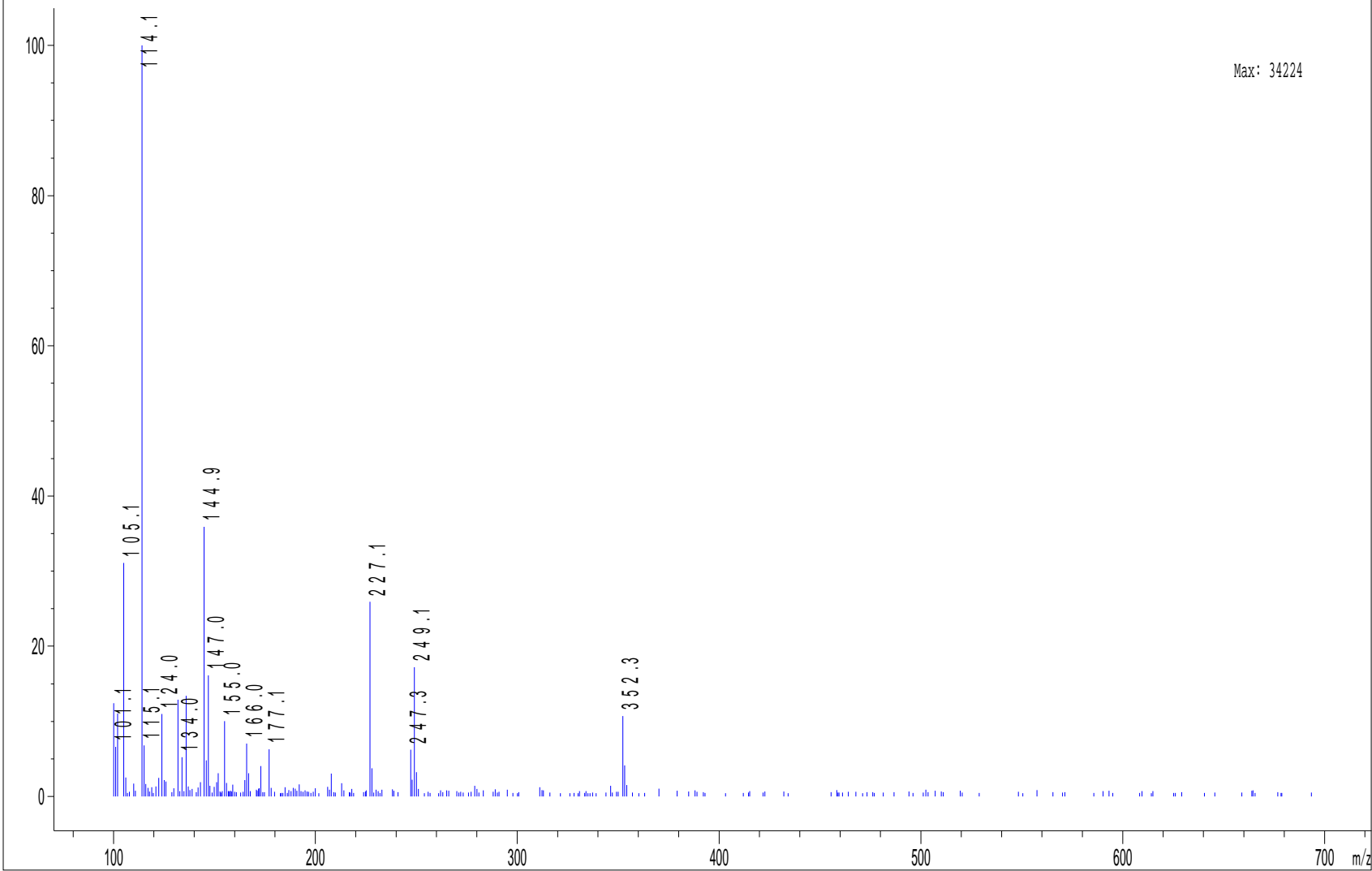








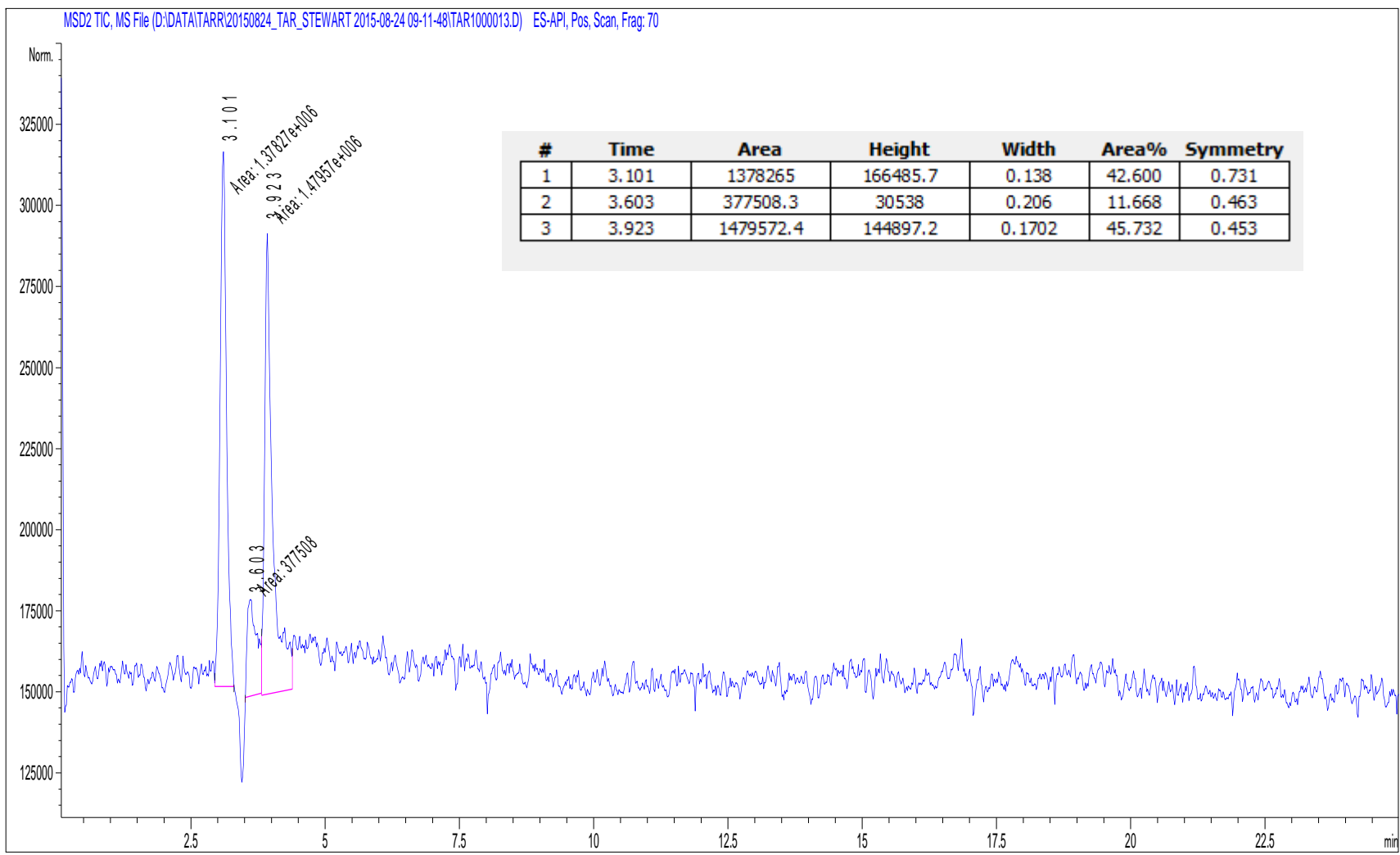
\*MSD2 SPC, time=3.938 of D:\DATA\ARR\20150824\_TAR\_STEWART 2015-08-24 09:11:48\TAR1000030.D ES-API, Pos, Scan, Frag:

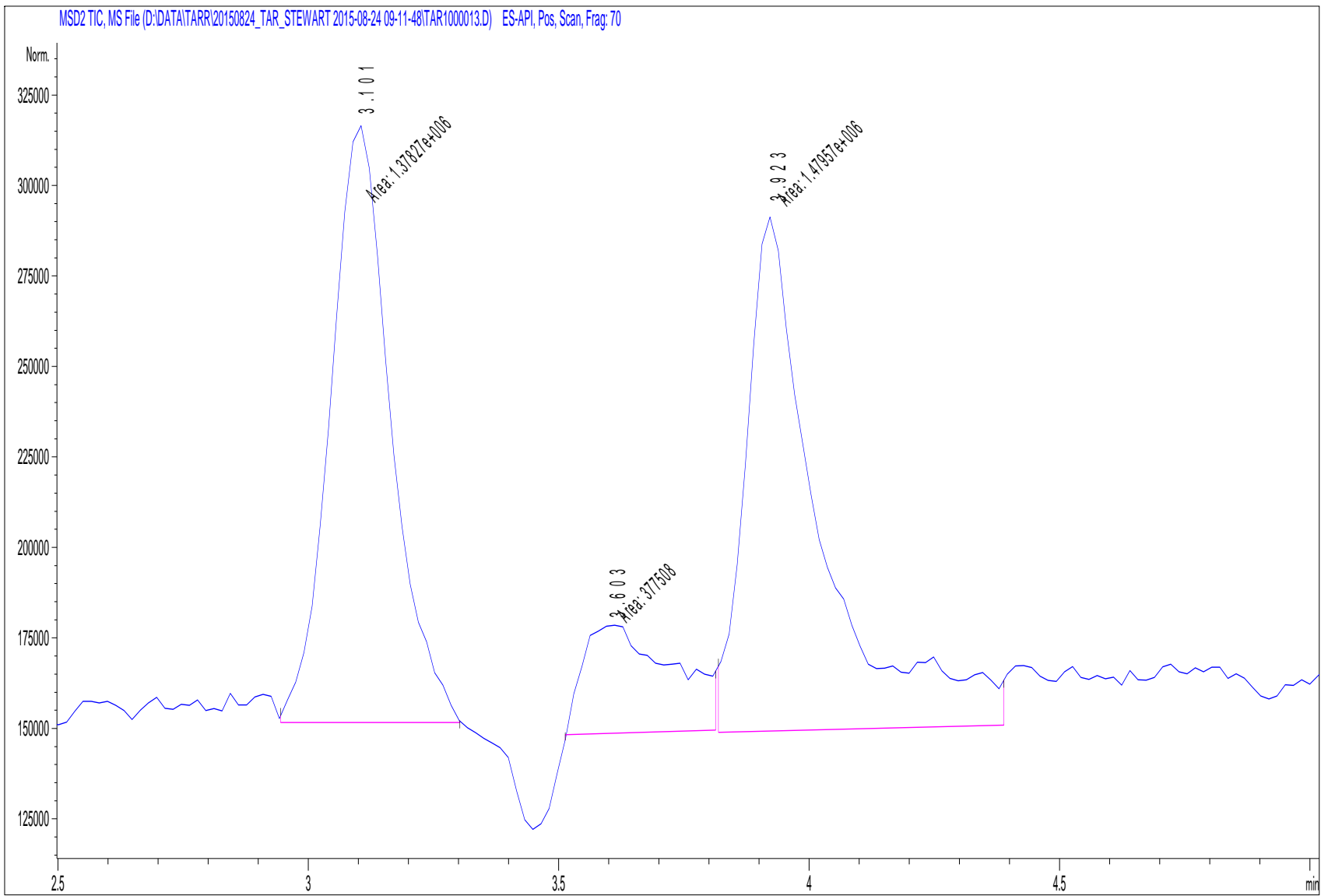


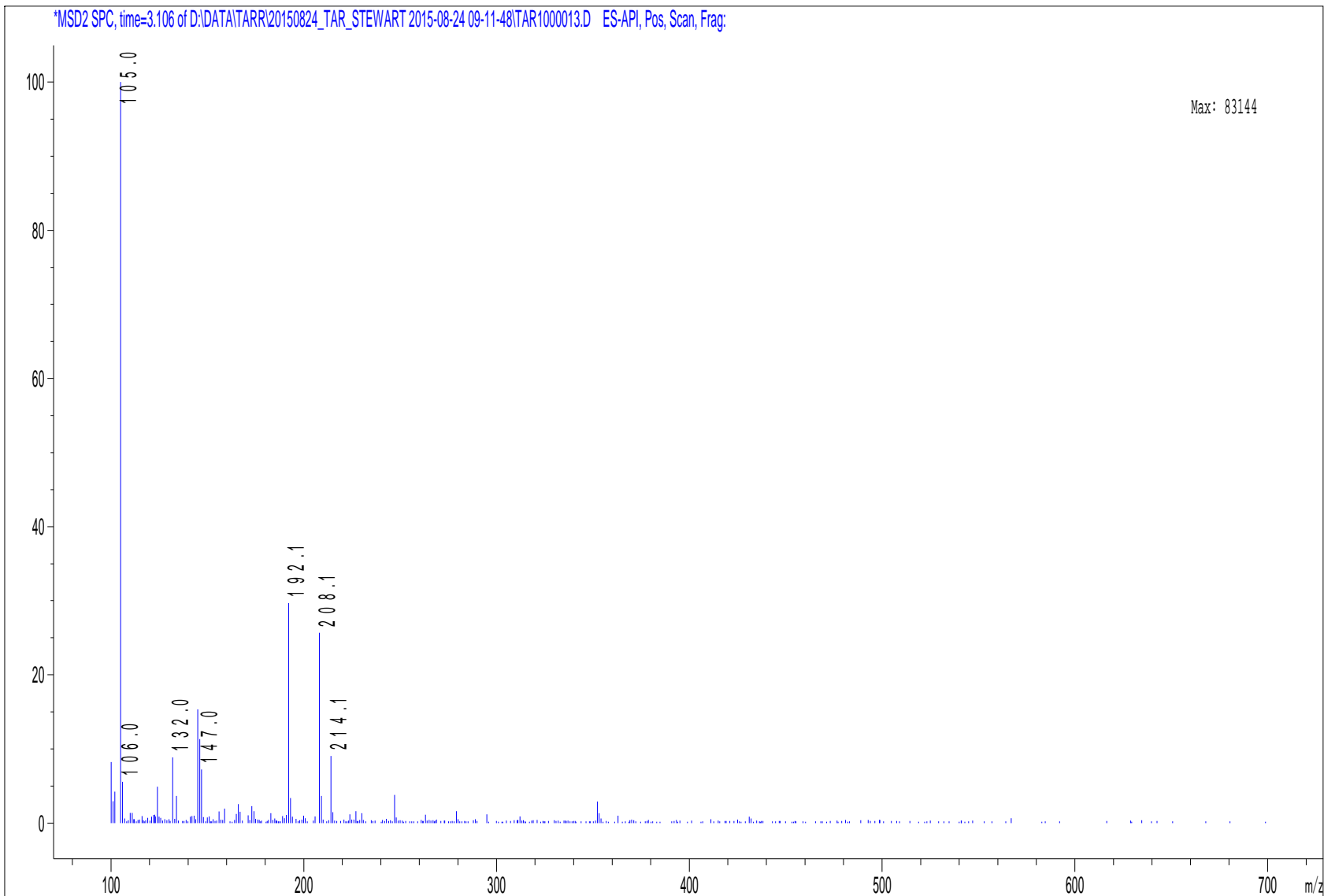
9-Jun-15

20 DC

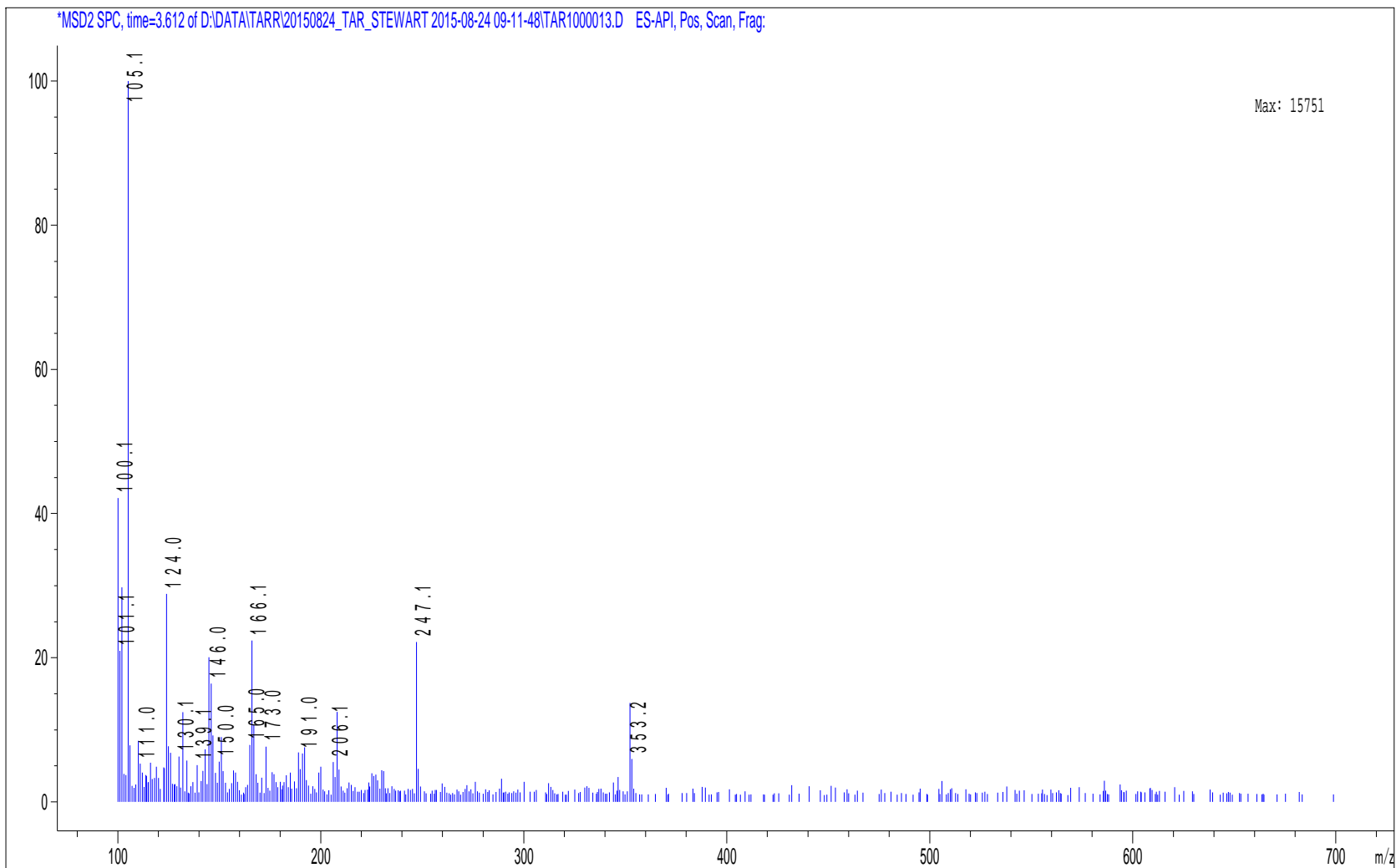
P2-B-06

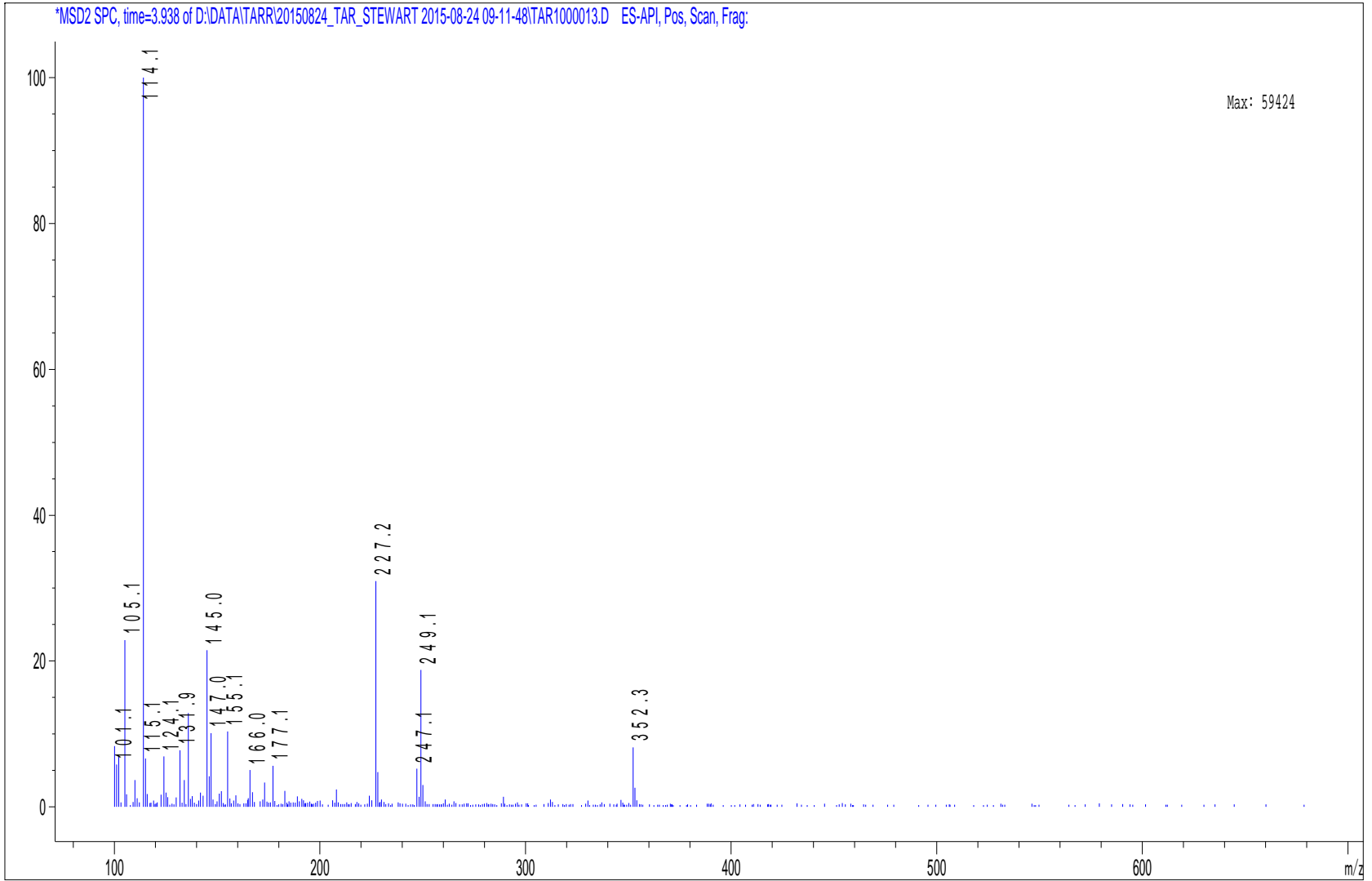






\*MSD2 SPC, time=3.612 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09:11:48\TAR1000013.D ES-API, Pos, Scan, Frag:



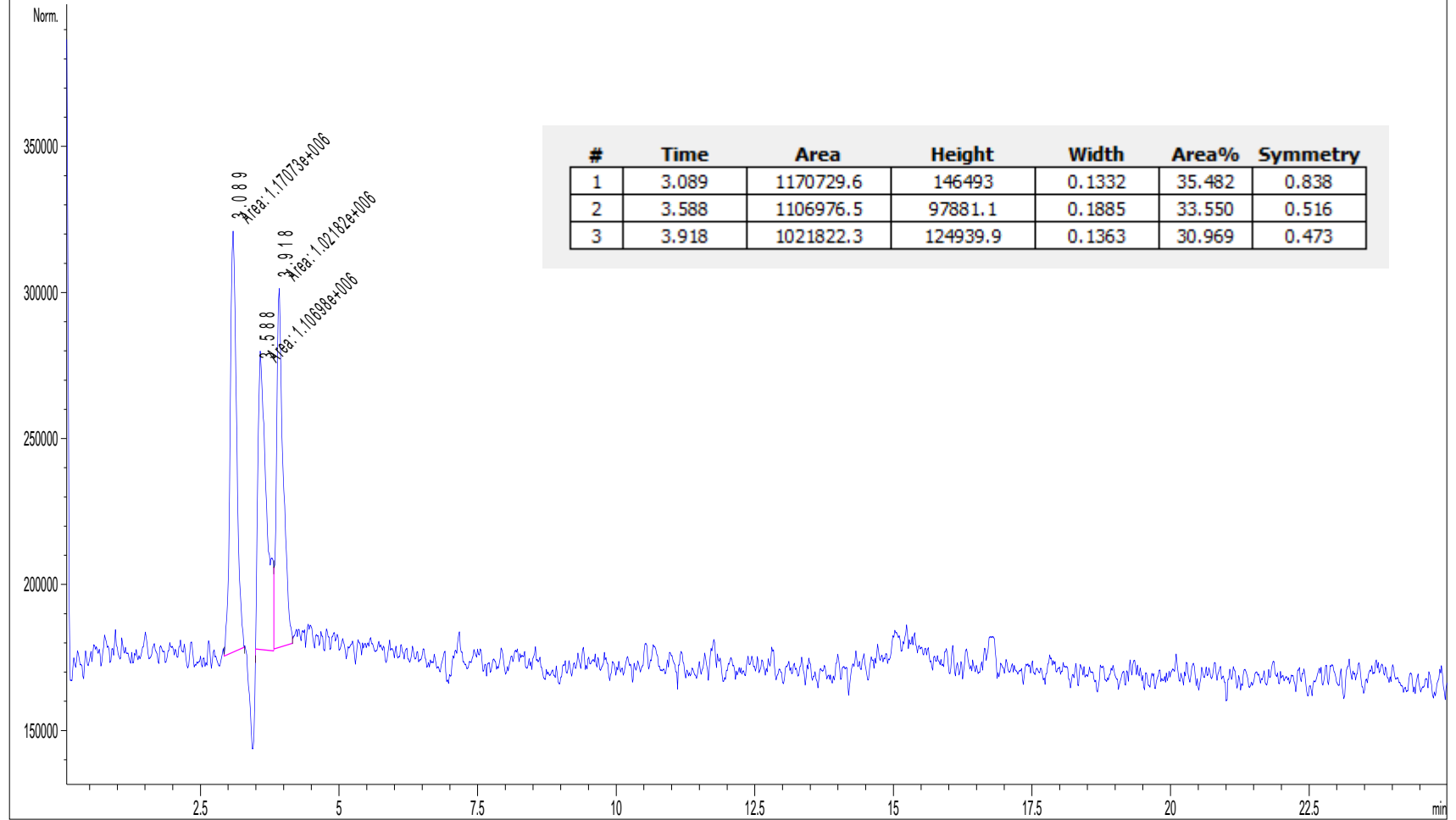


17-Jun-15

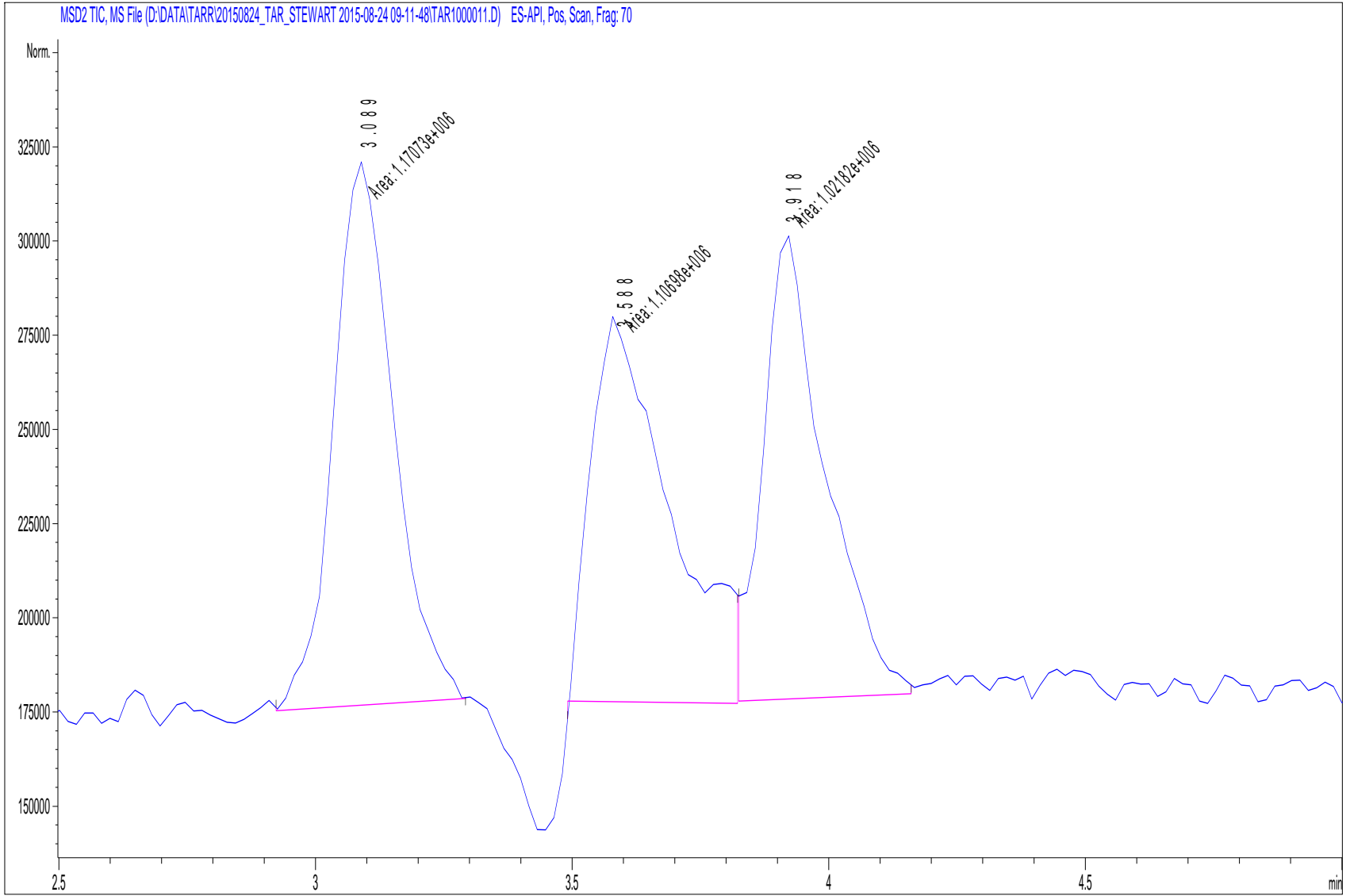
30 DC

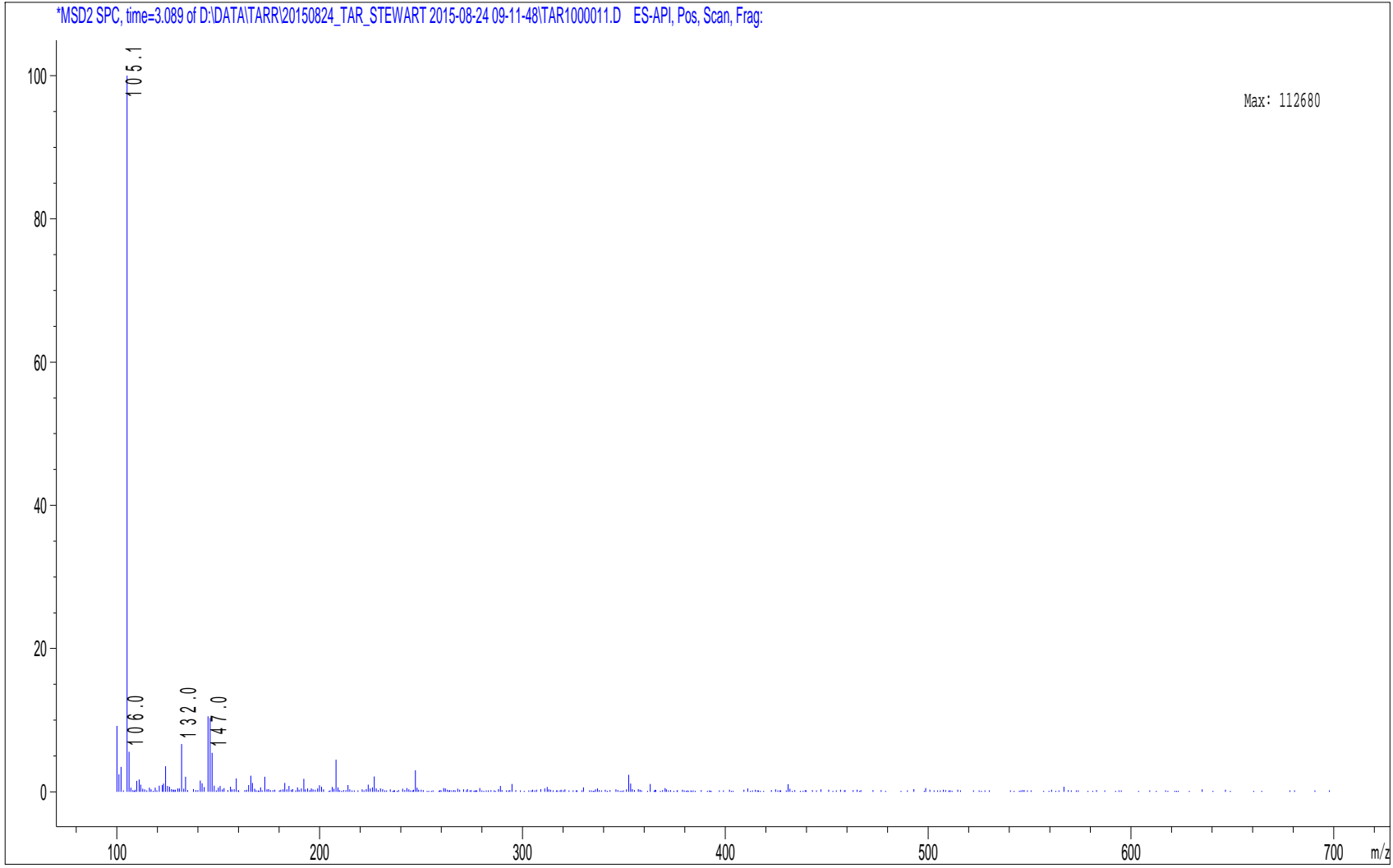
P2-B-08

MSD2 TIC, MS File (D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000011.D) ES-API, Pos, Scan, Frag: 70

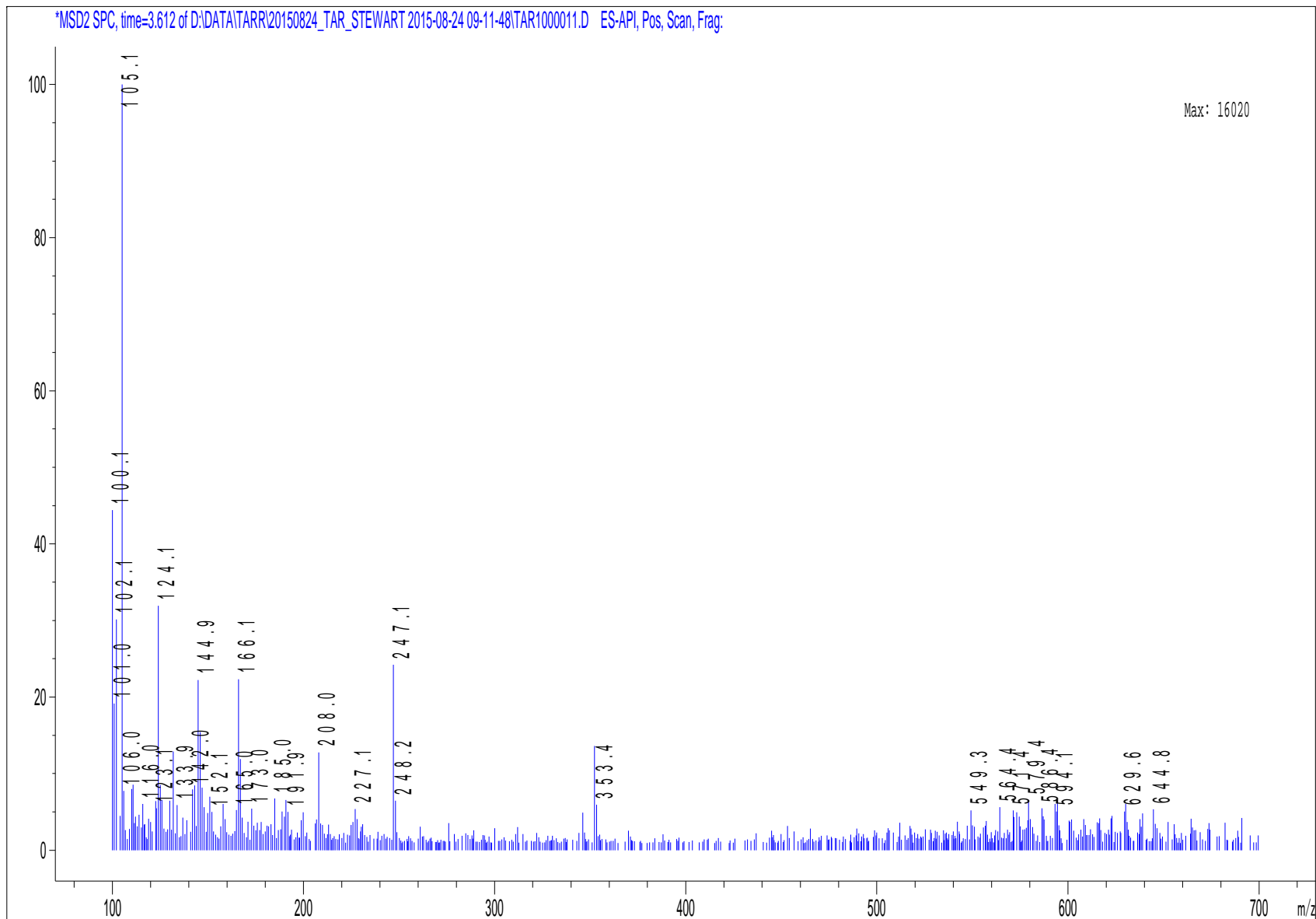


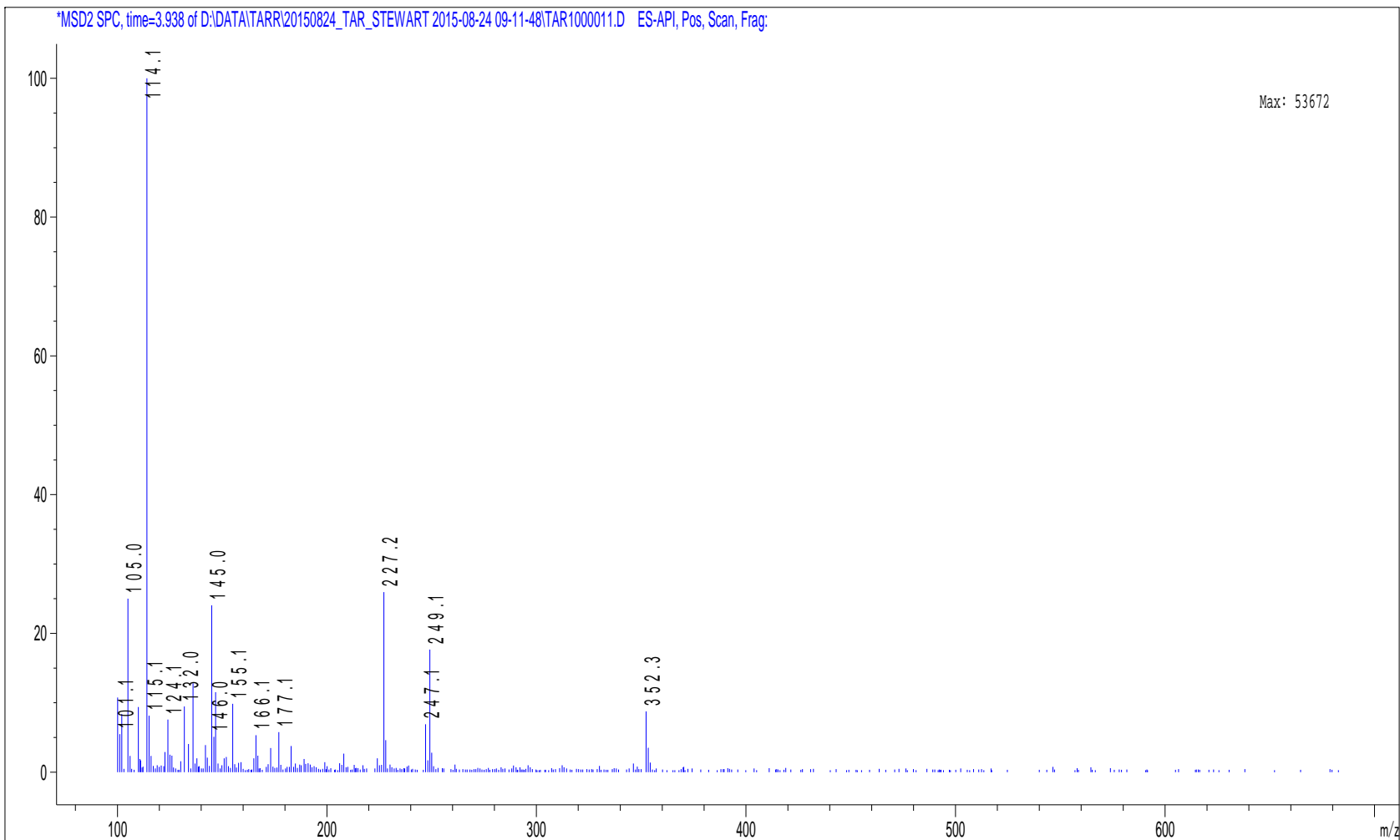






\*MSD2 SPC, time=3.612 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000011.D ES-API, Pos, Scan, Frag:

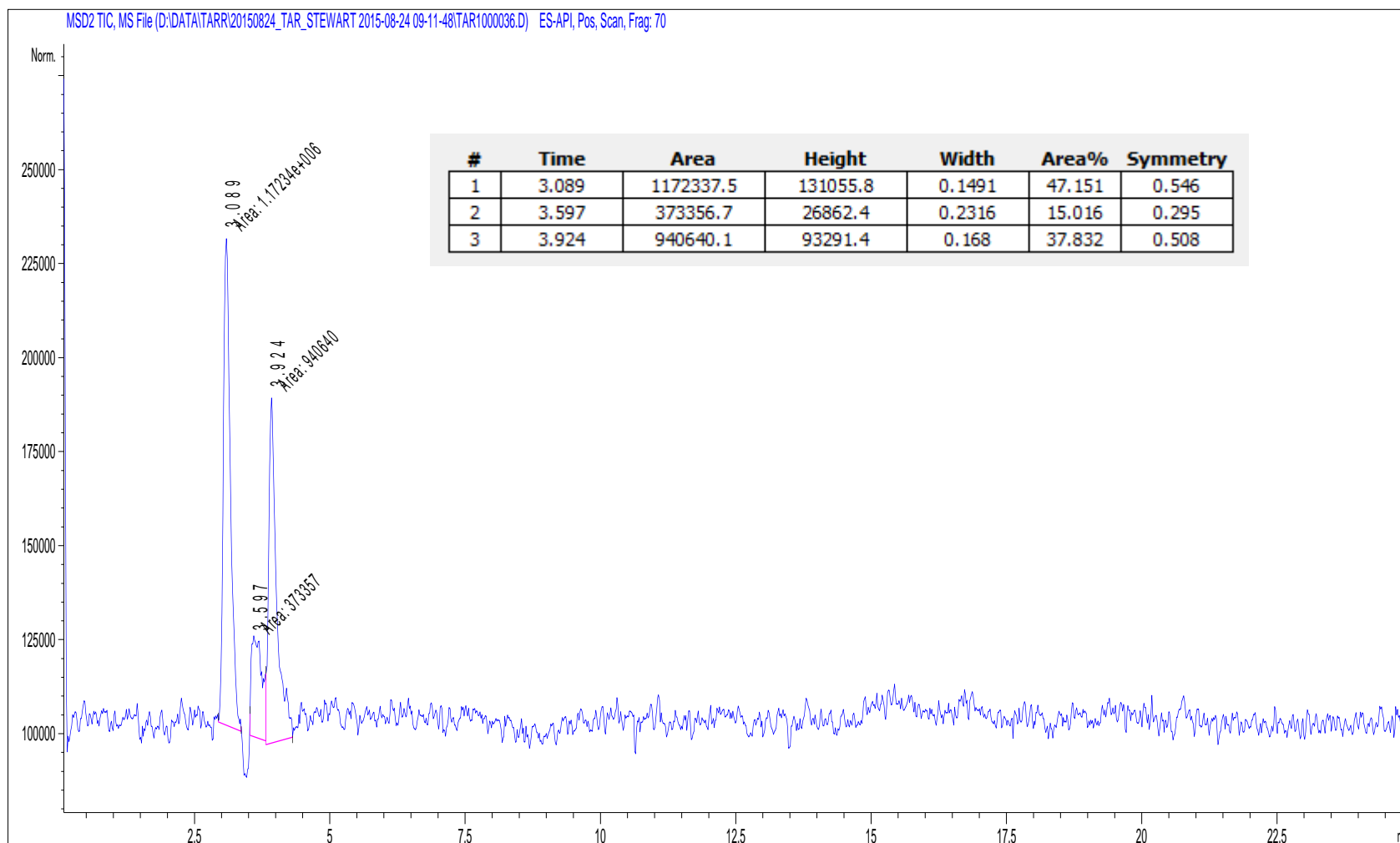


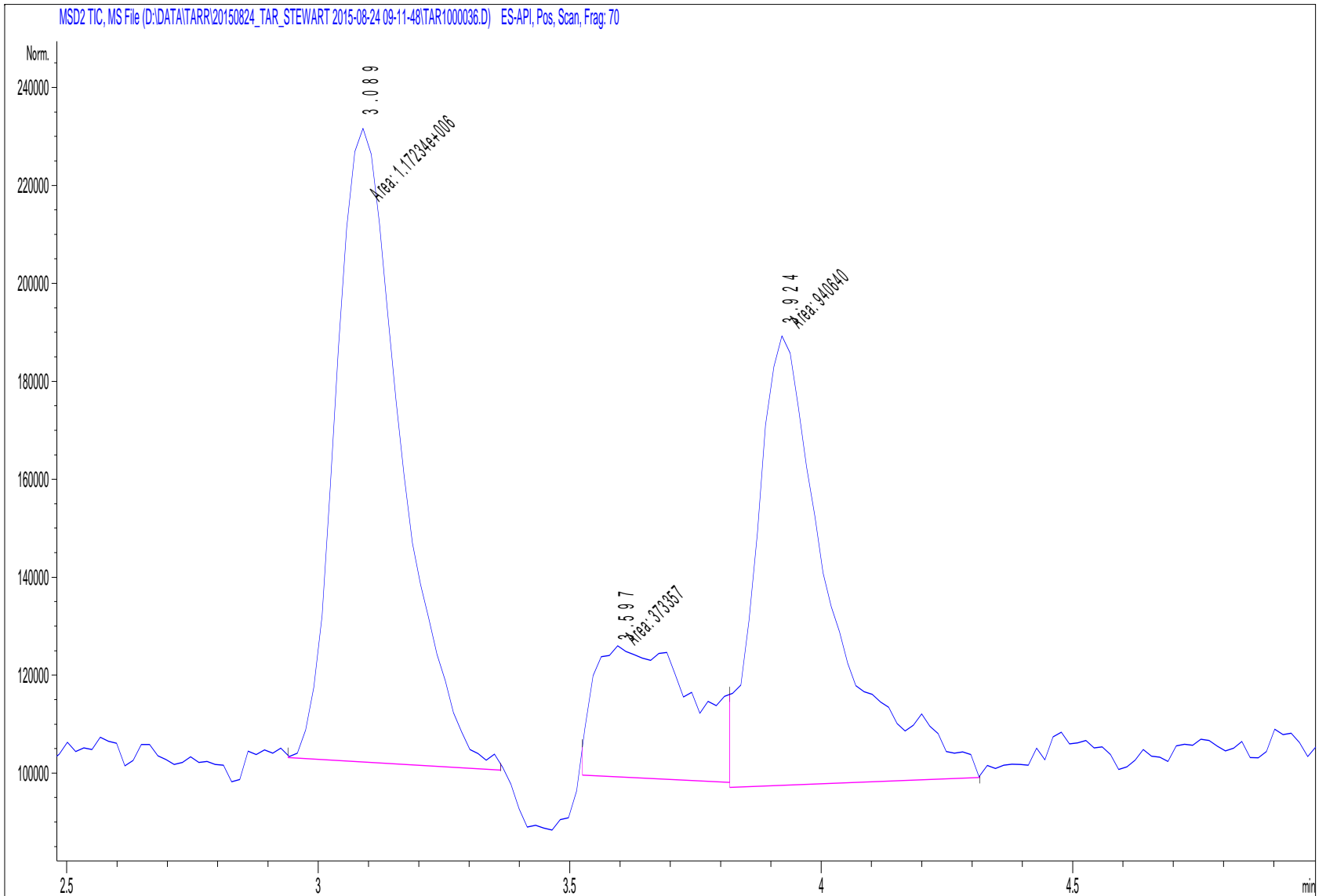


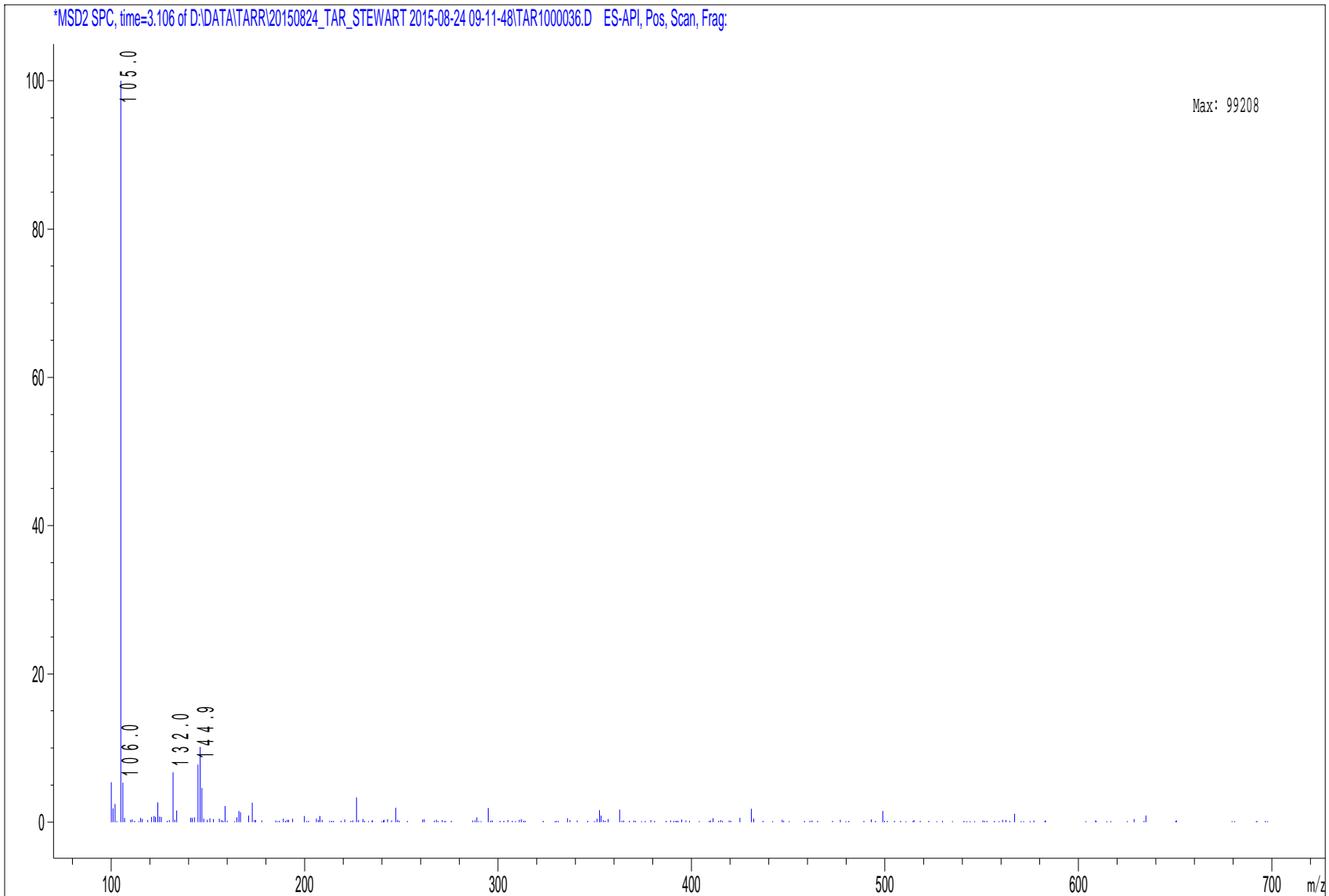
4-Aug-15

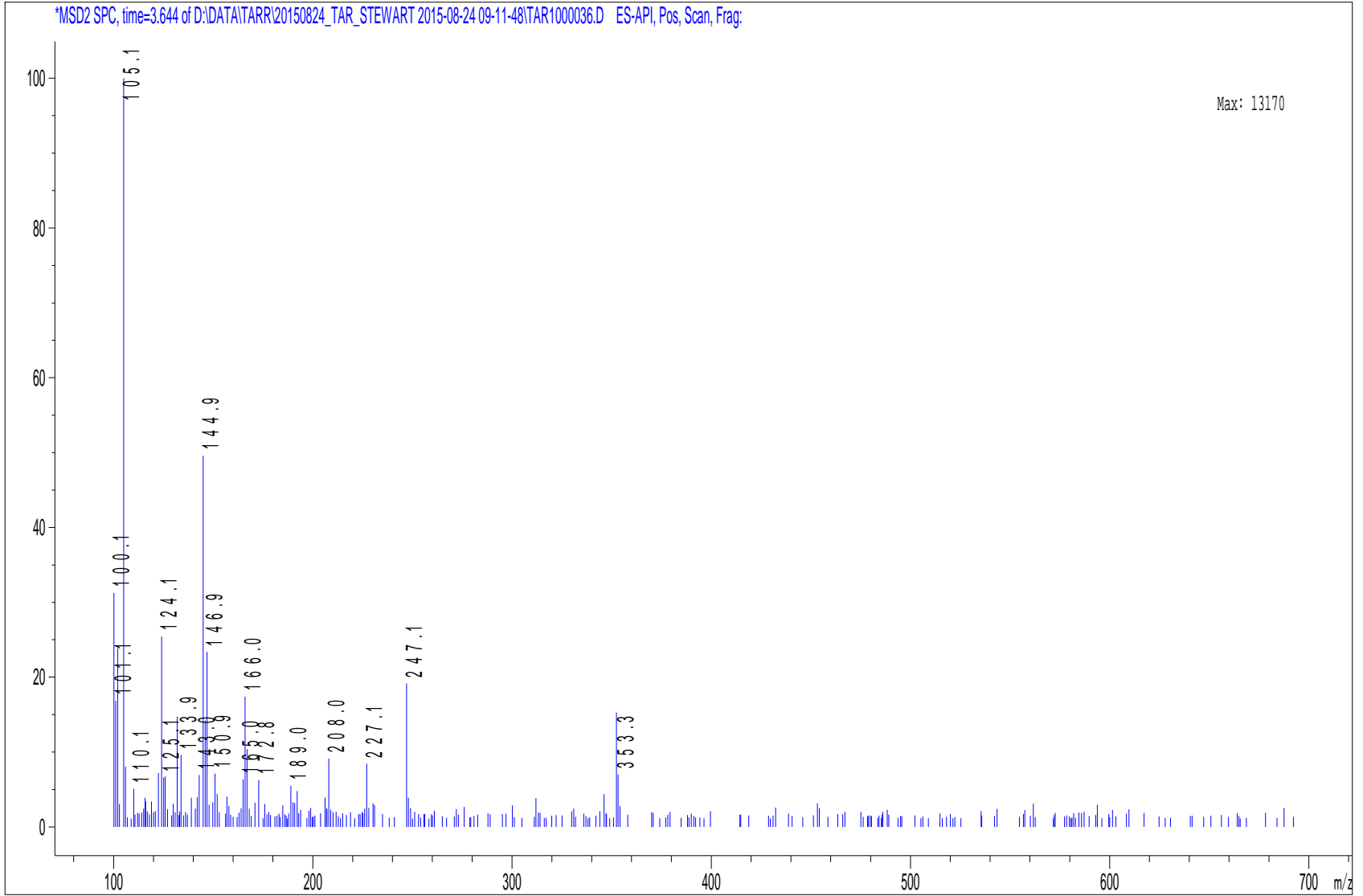
50 DC

P2-E-01

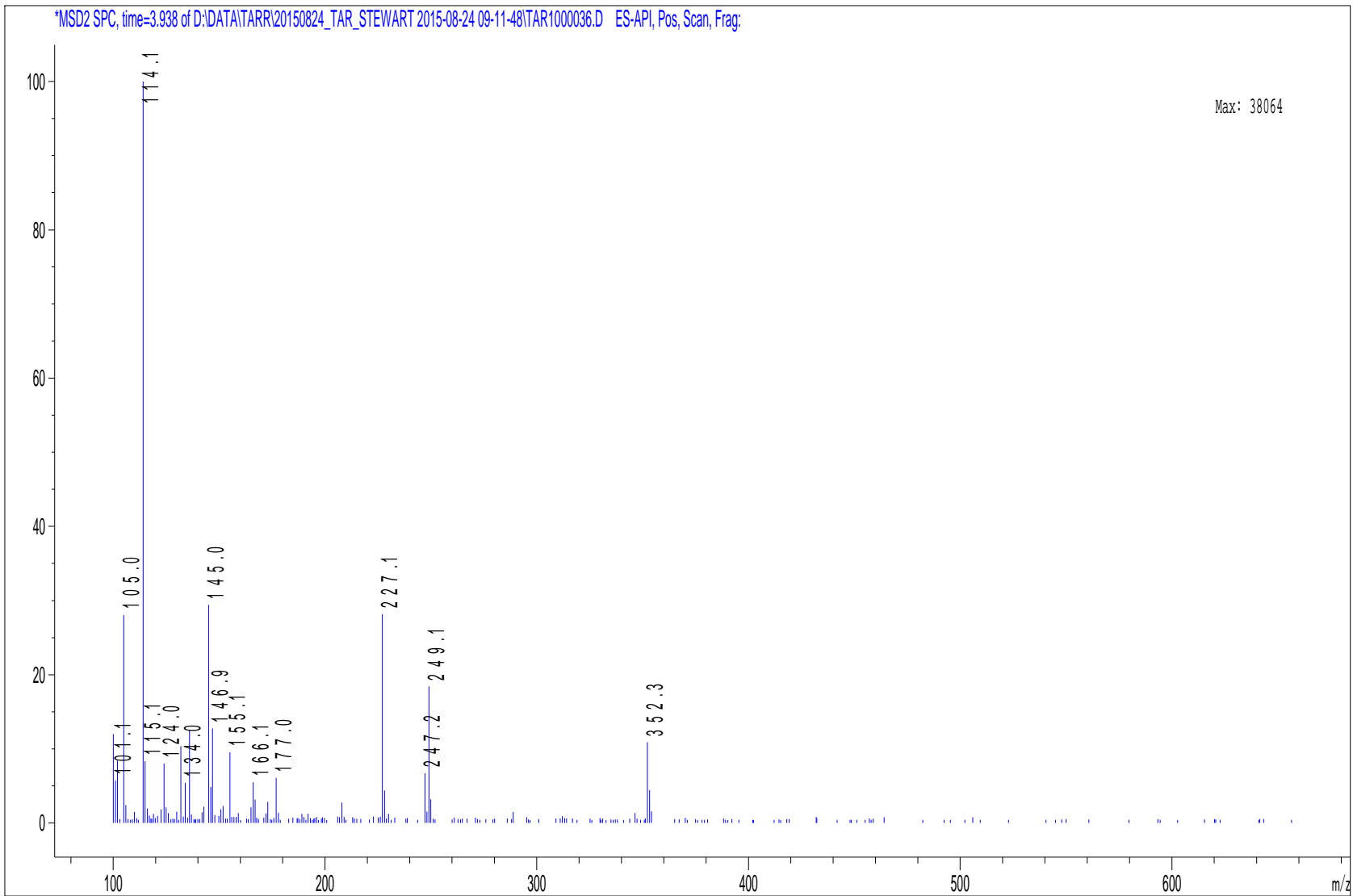










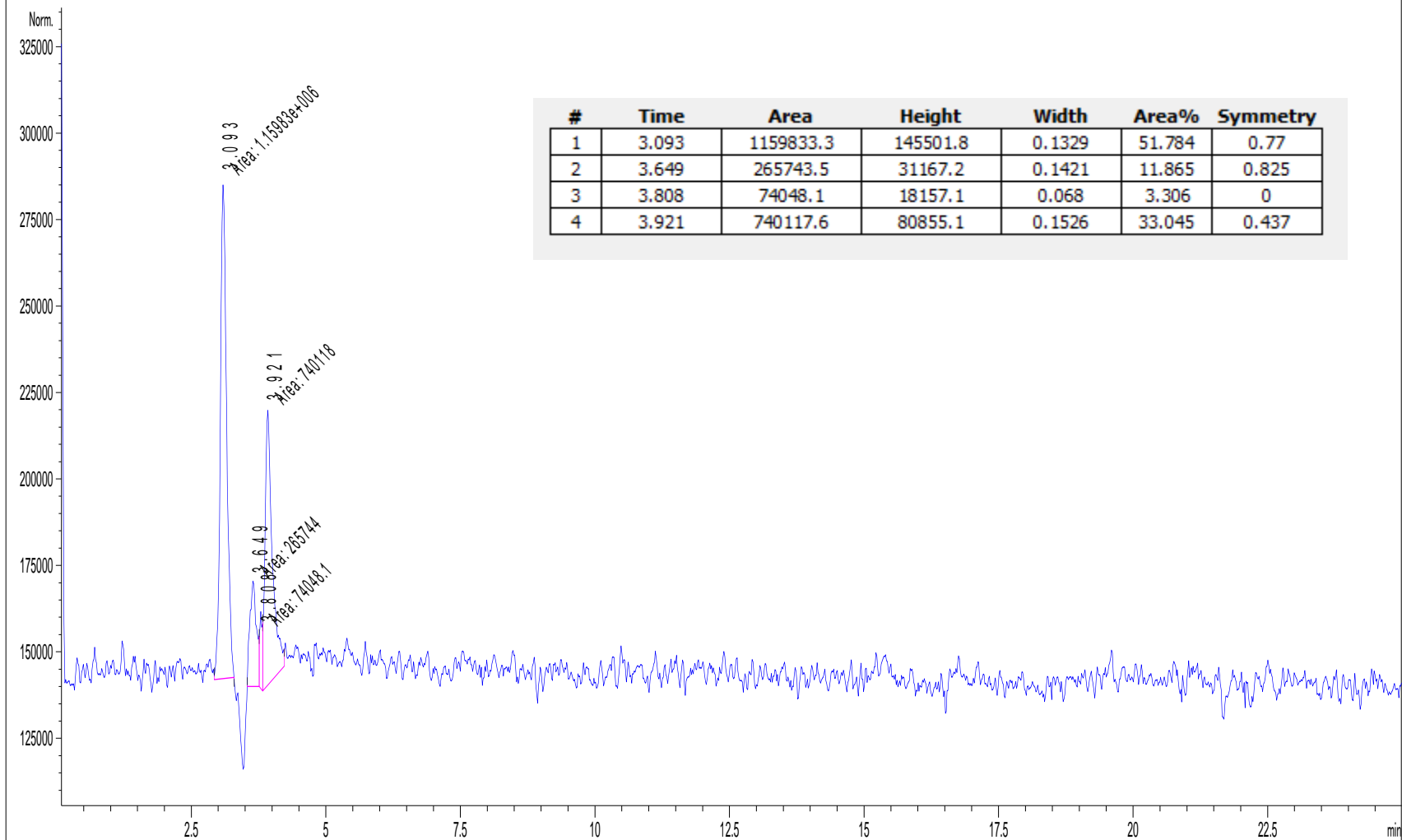


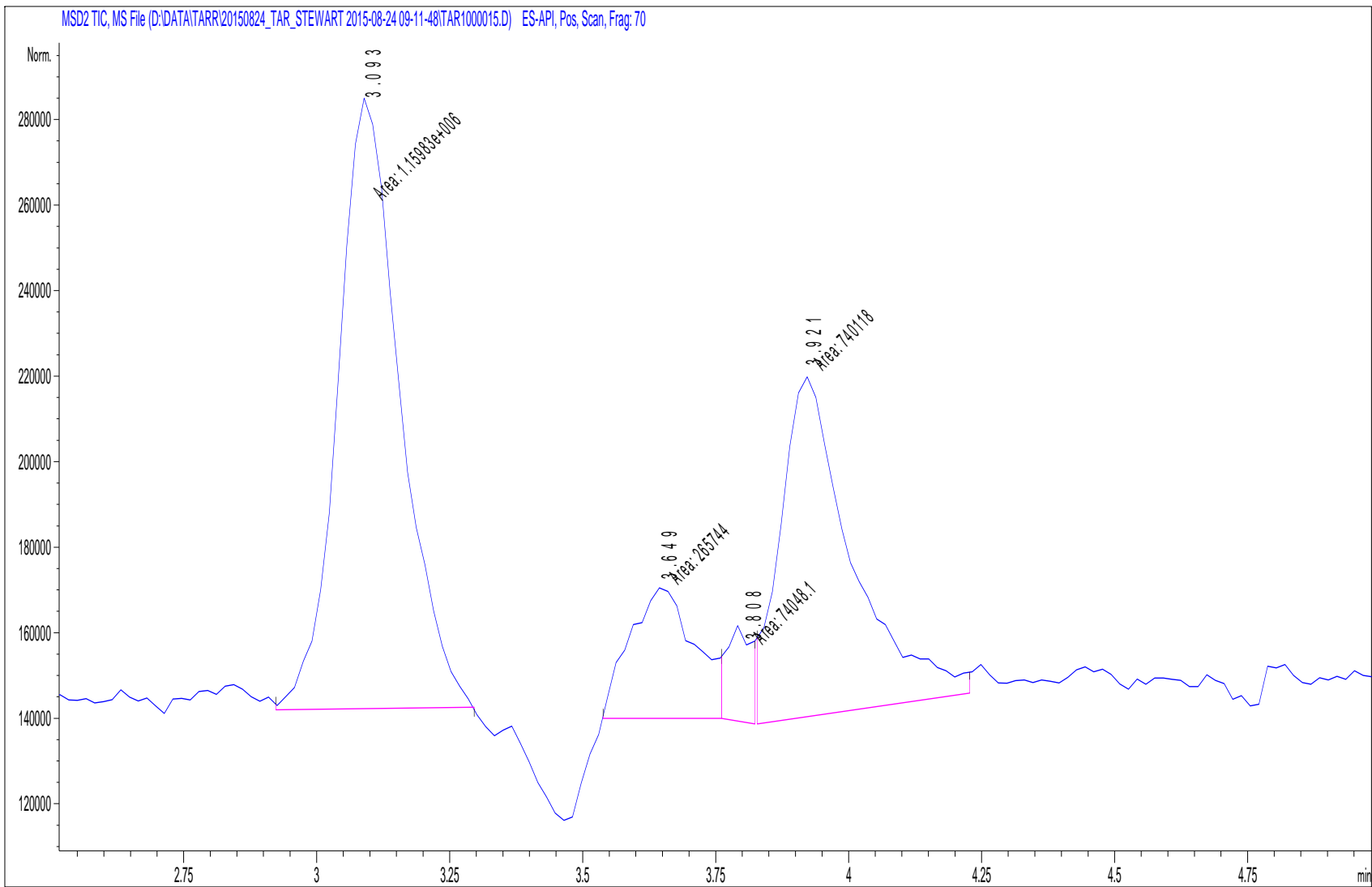
1-Jun-15

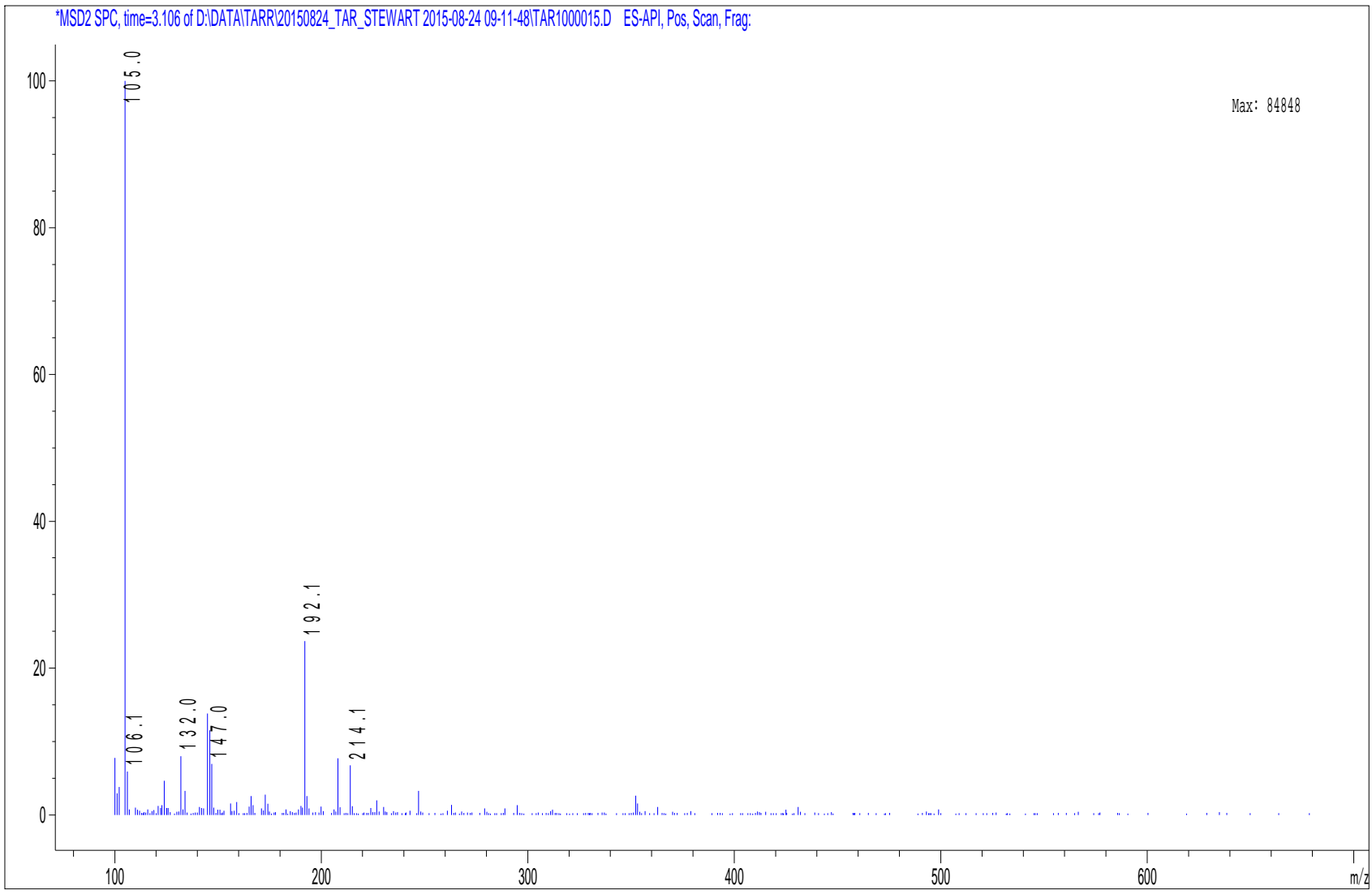
70 DC

P2-B-04

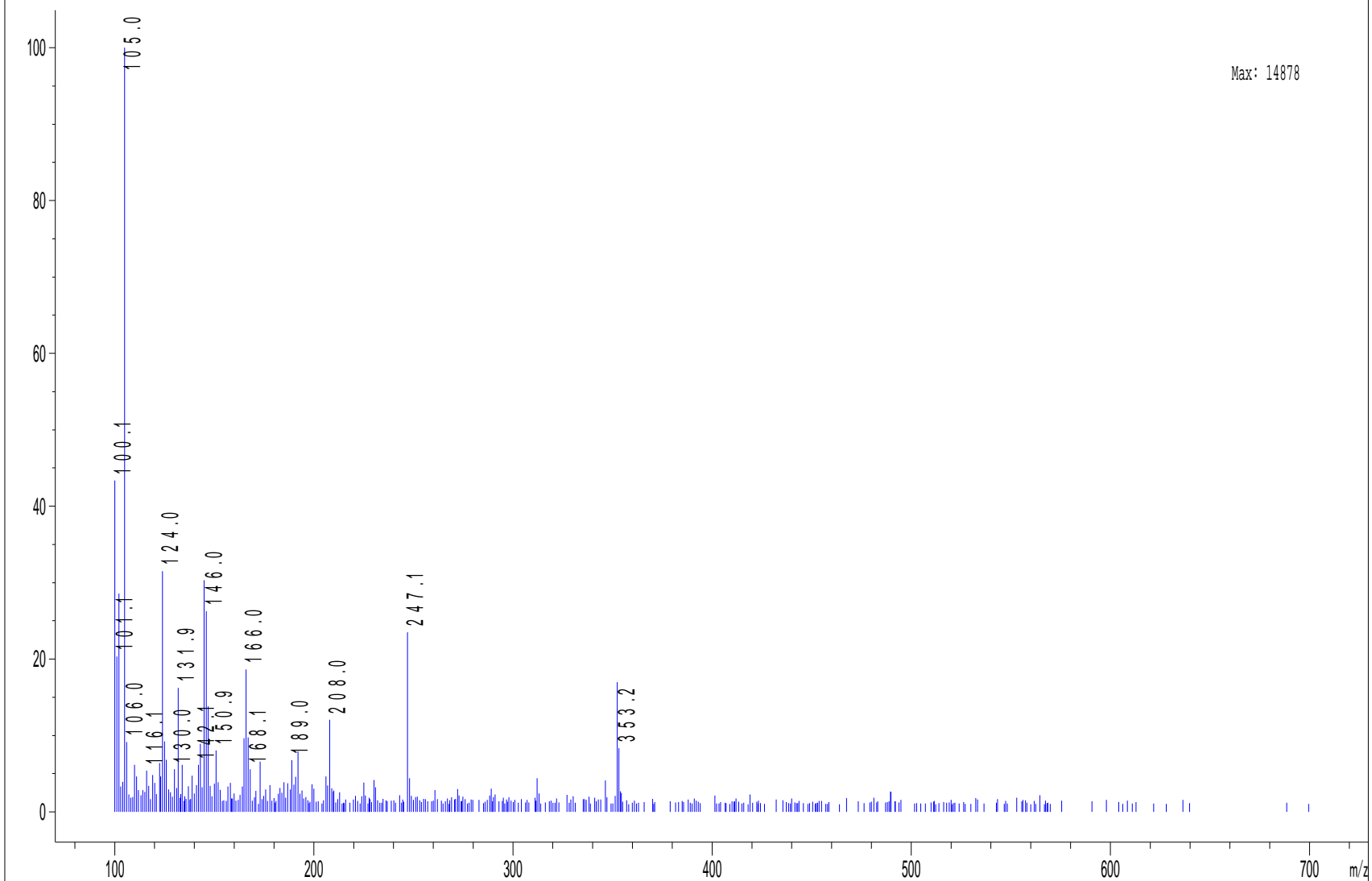
MSD2 TIC, MS File (D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000015.D) ES-API, Pos, Scan, Frag: 70



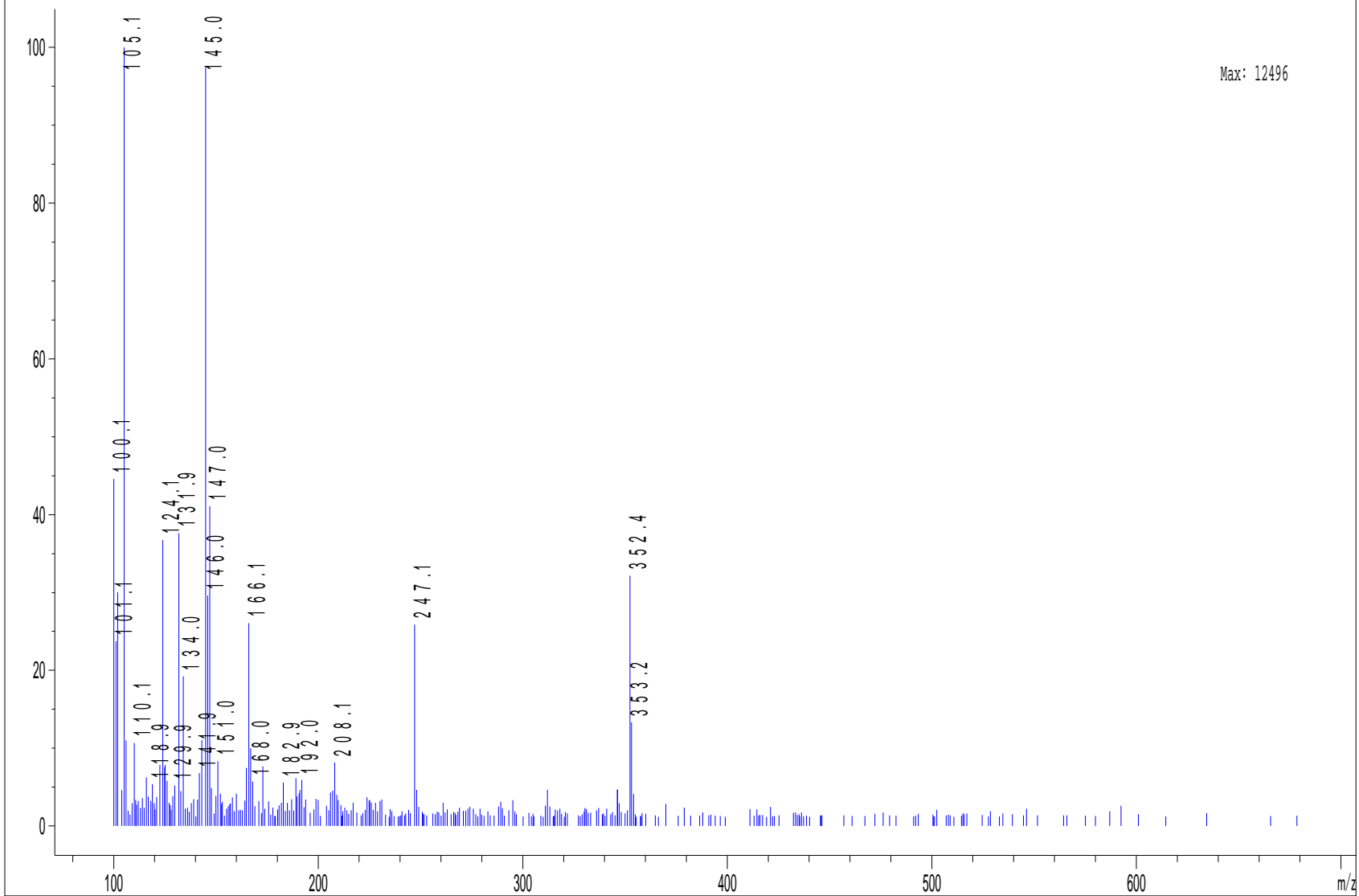


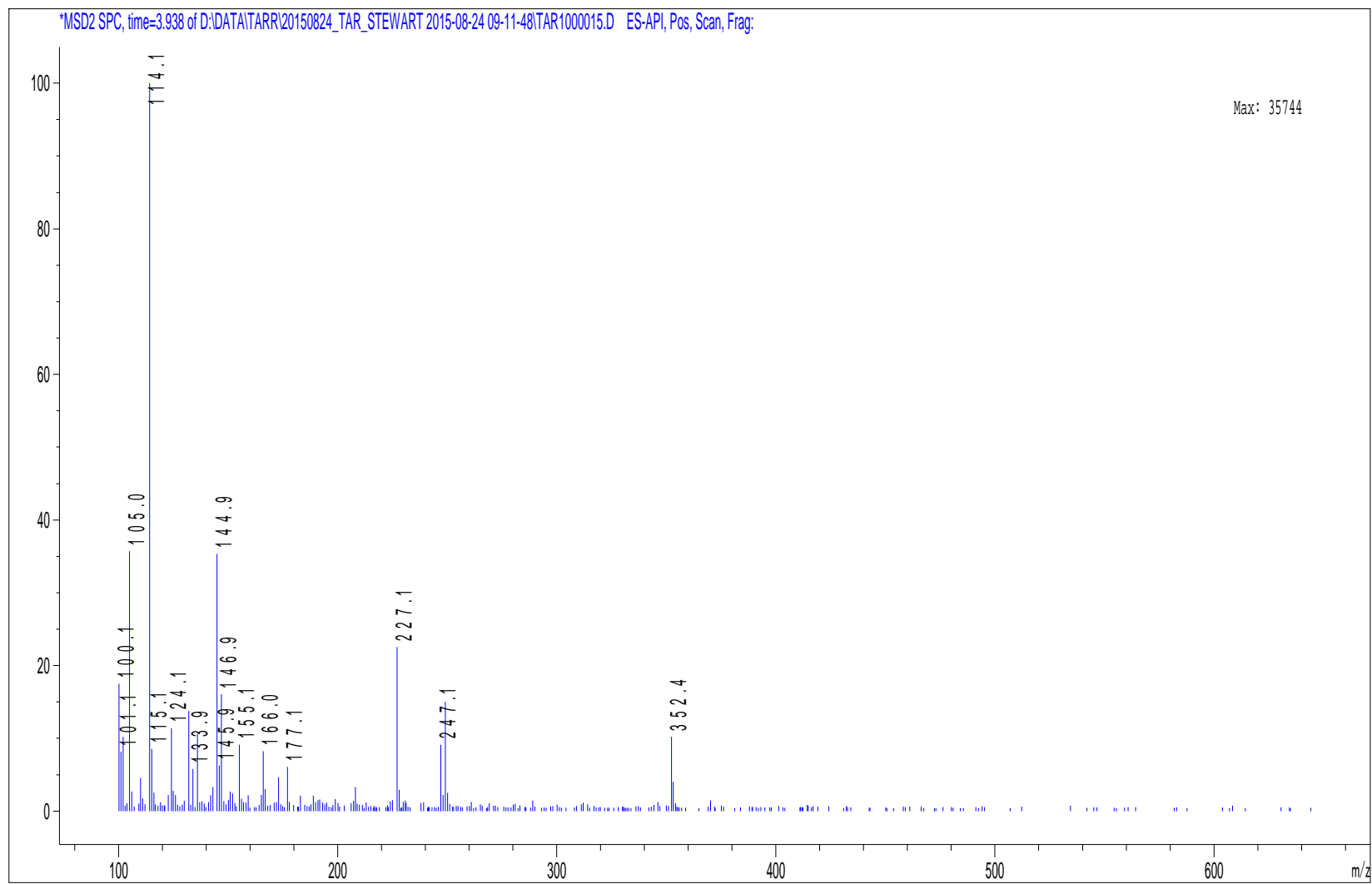


\*MSD2 SPC, time=3.661 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09:11-48\TAR1000015.D ES-API, Pos, Scan, Frag:

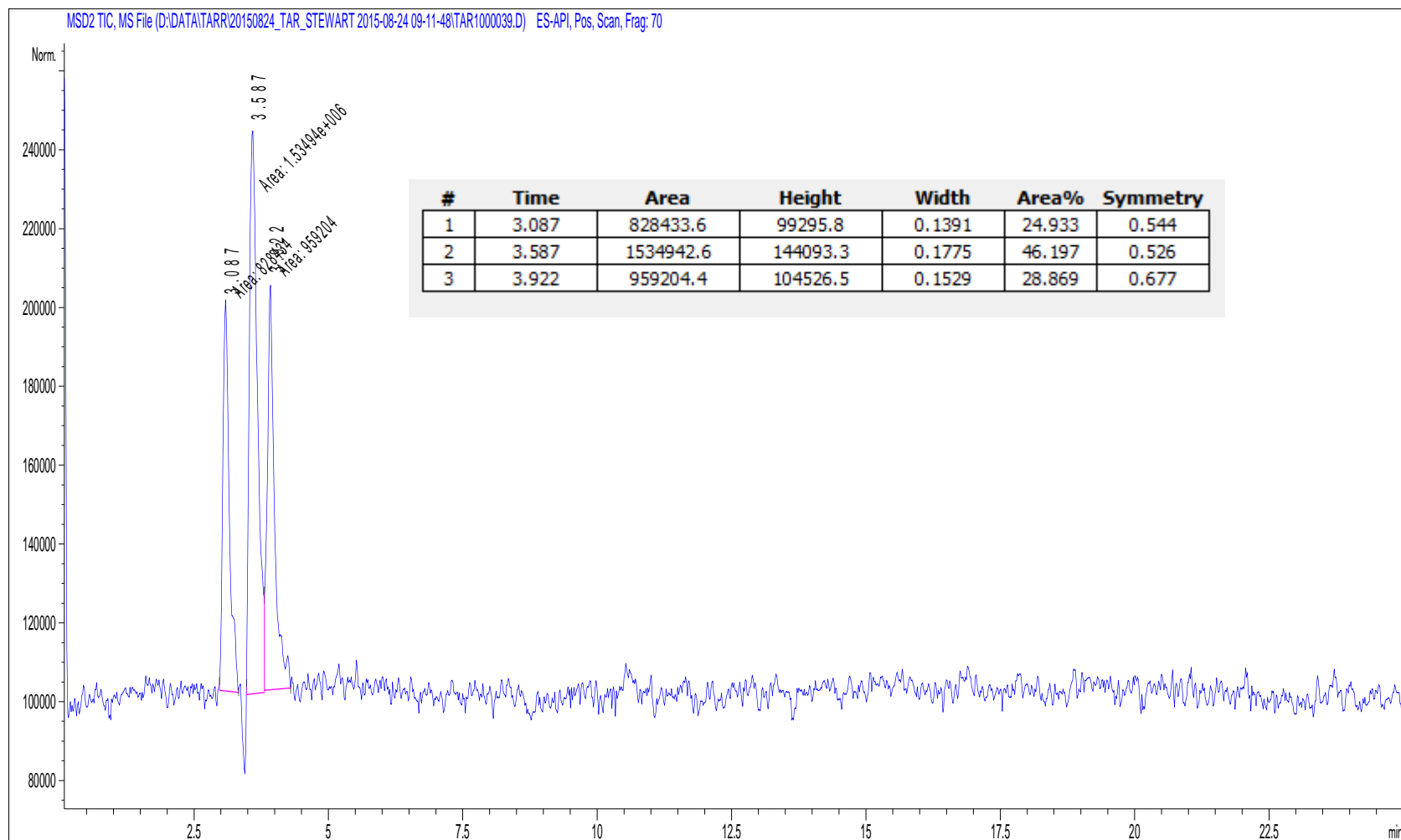


\*MSD2 SPC, time=3.791 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000015.D ES-API, Pos, Scan, Frag:

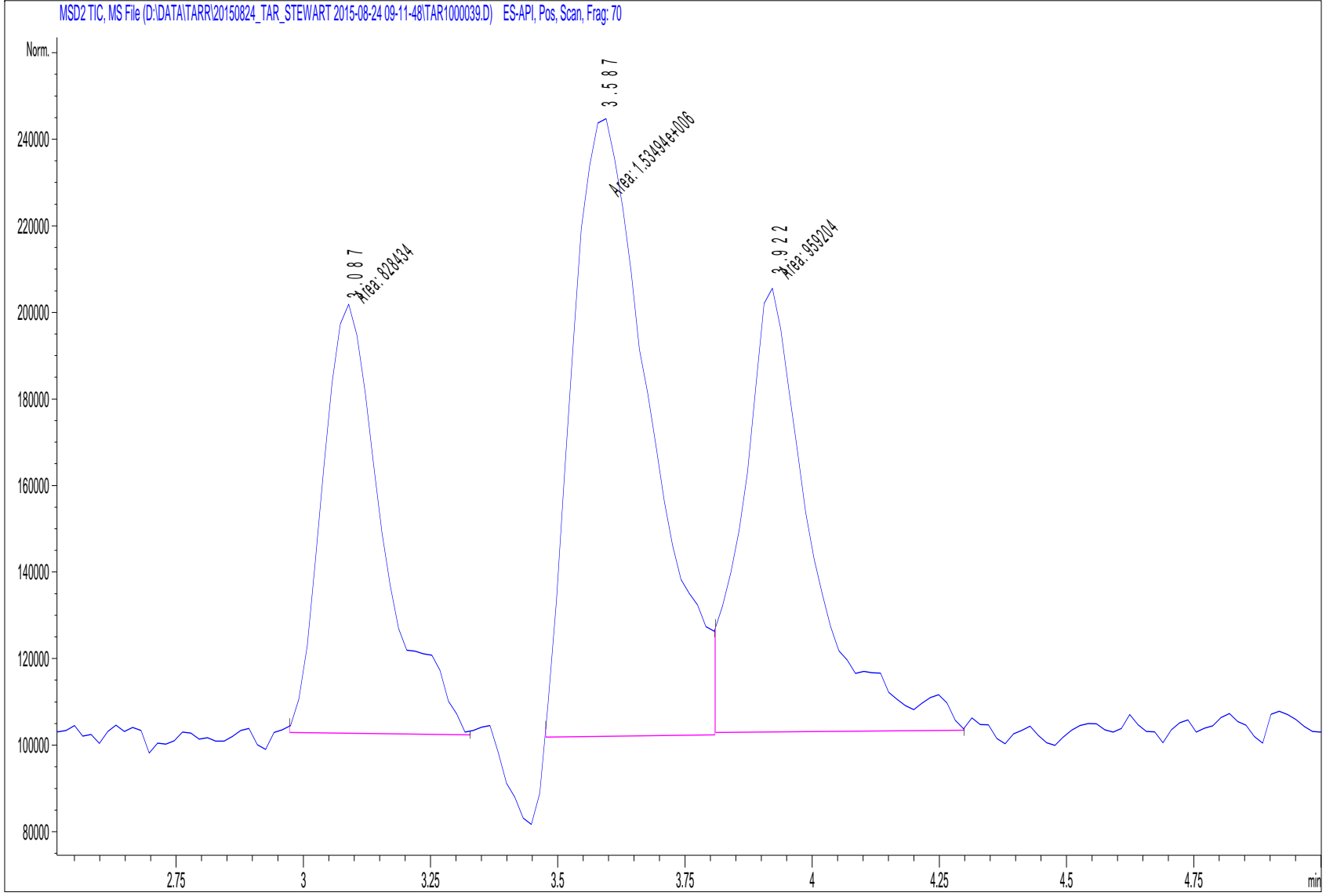


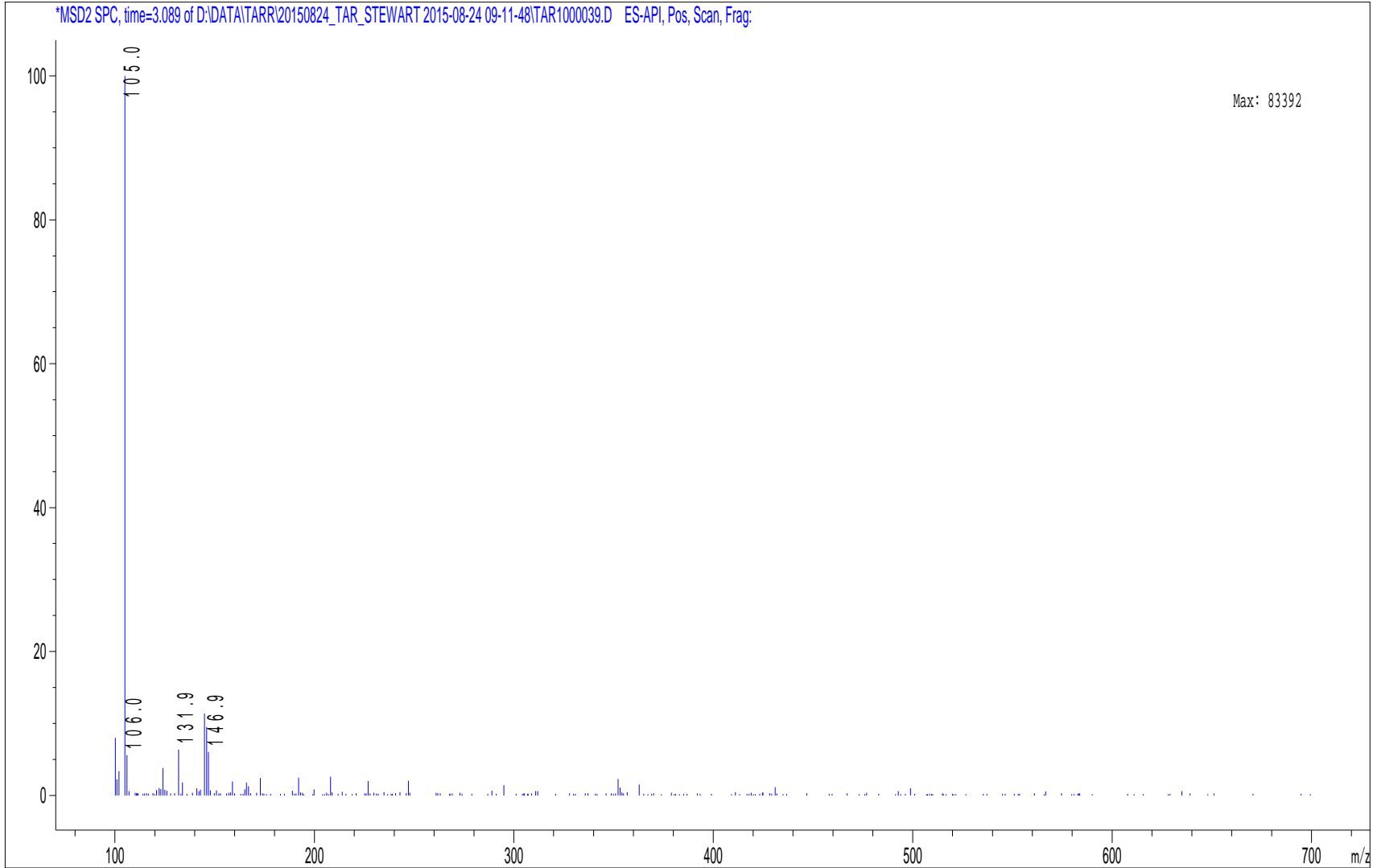


12-Aug-15  
70 DC repeat  
P2-E-03

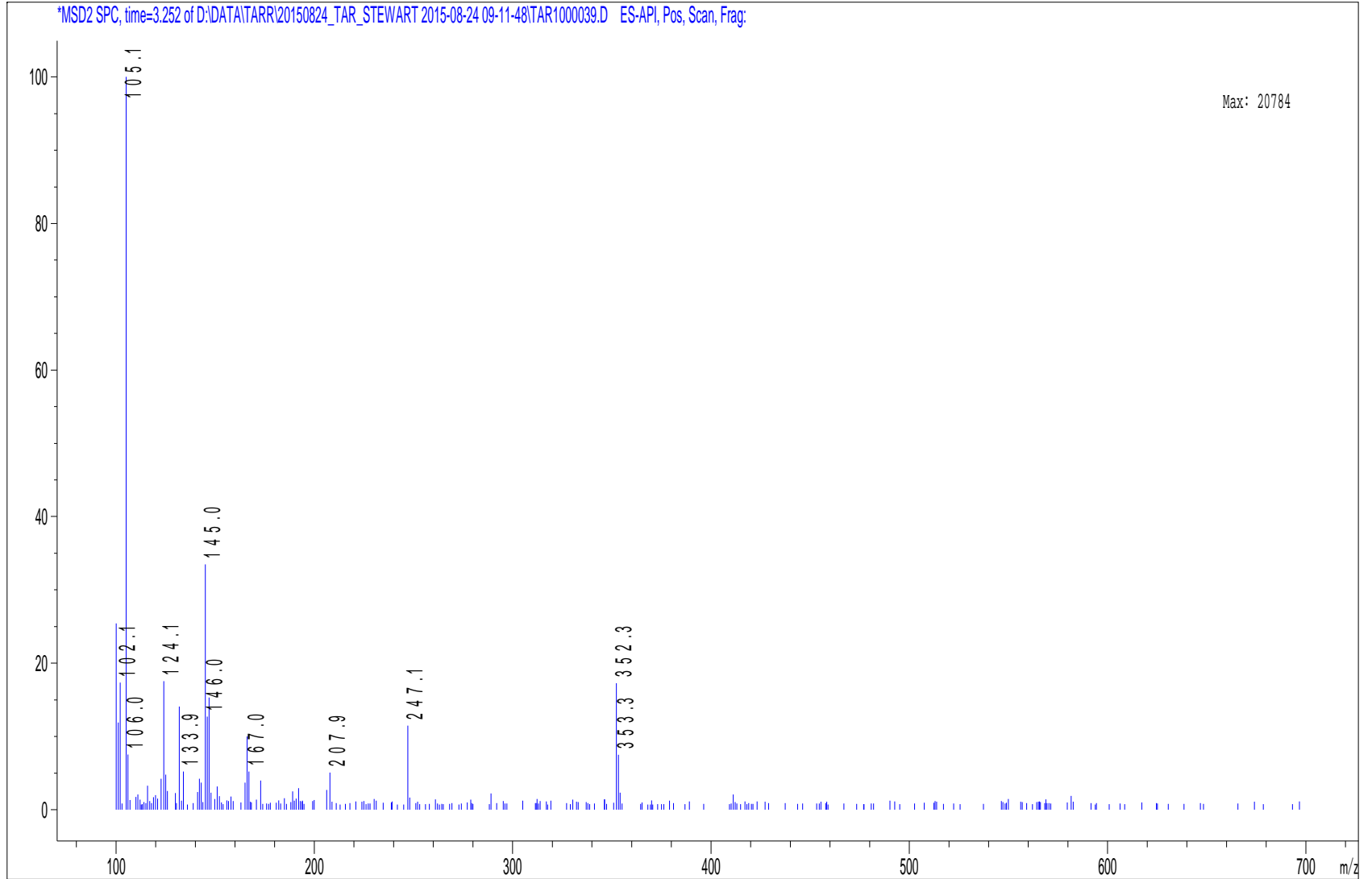


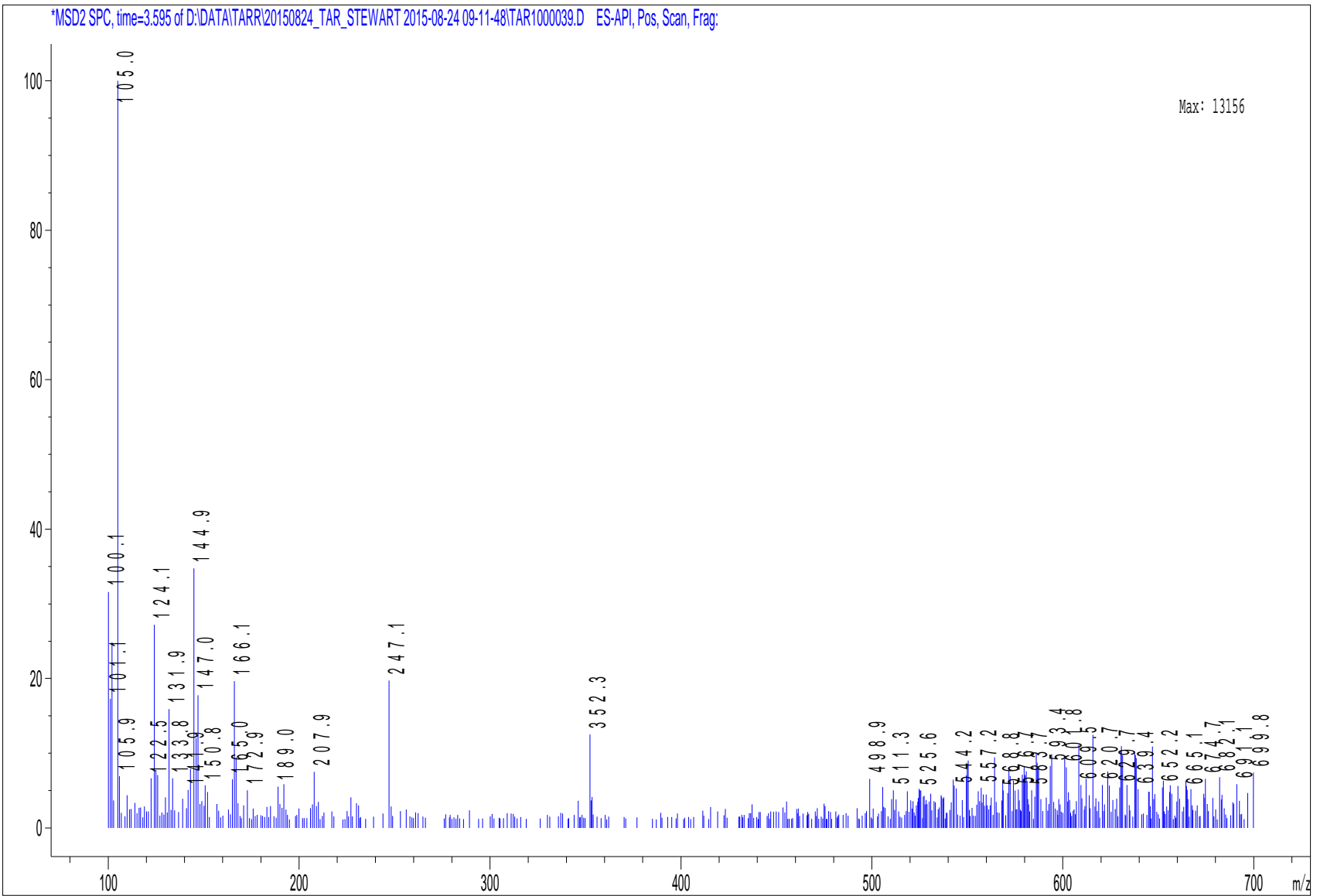




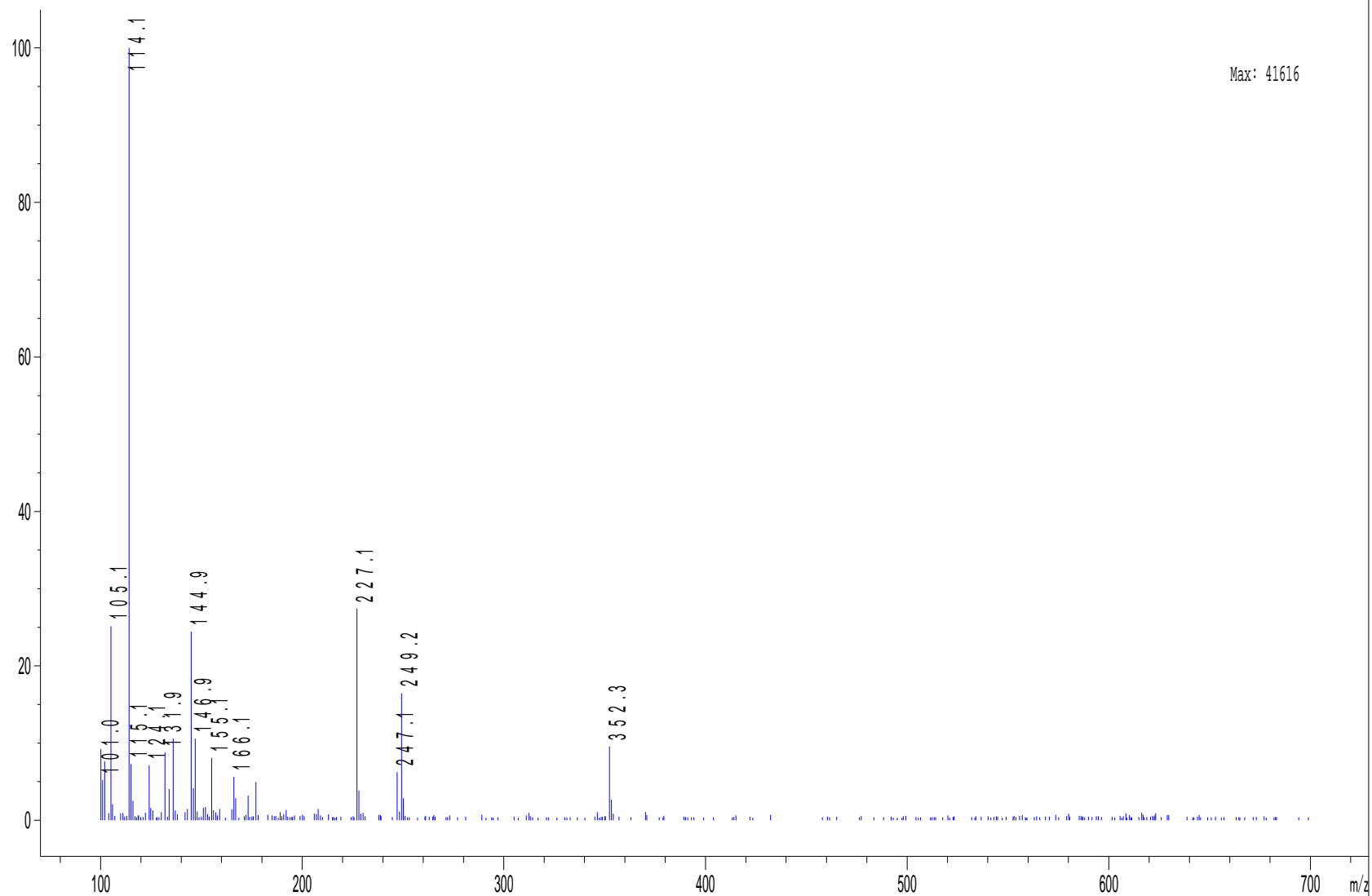


\*MSD2 SPC, time=3.252 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000039.D ES-API, Pos, Scan, Frag:





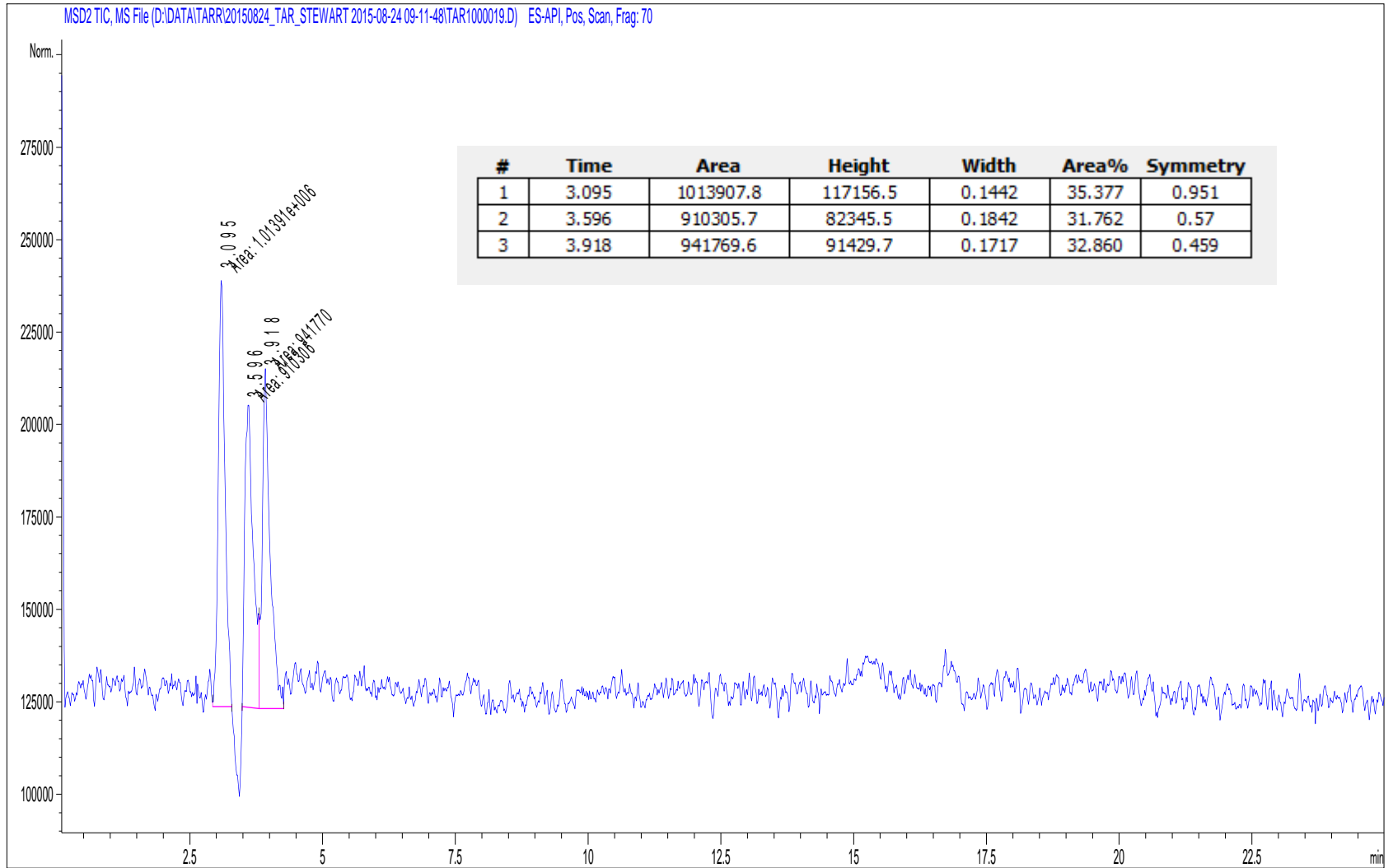
\*MSD2 SPC, time=3.938 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000039.D ES-API, Pos, Scan, Frag:



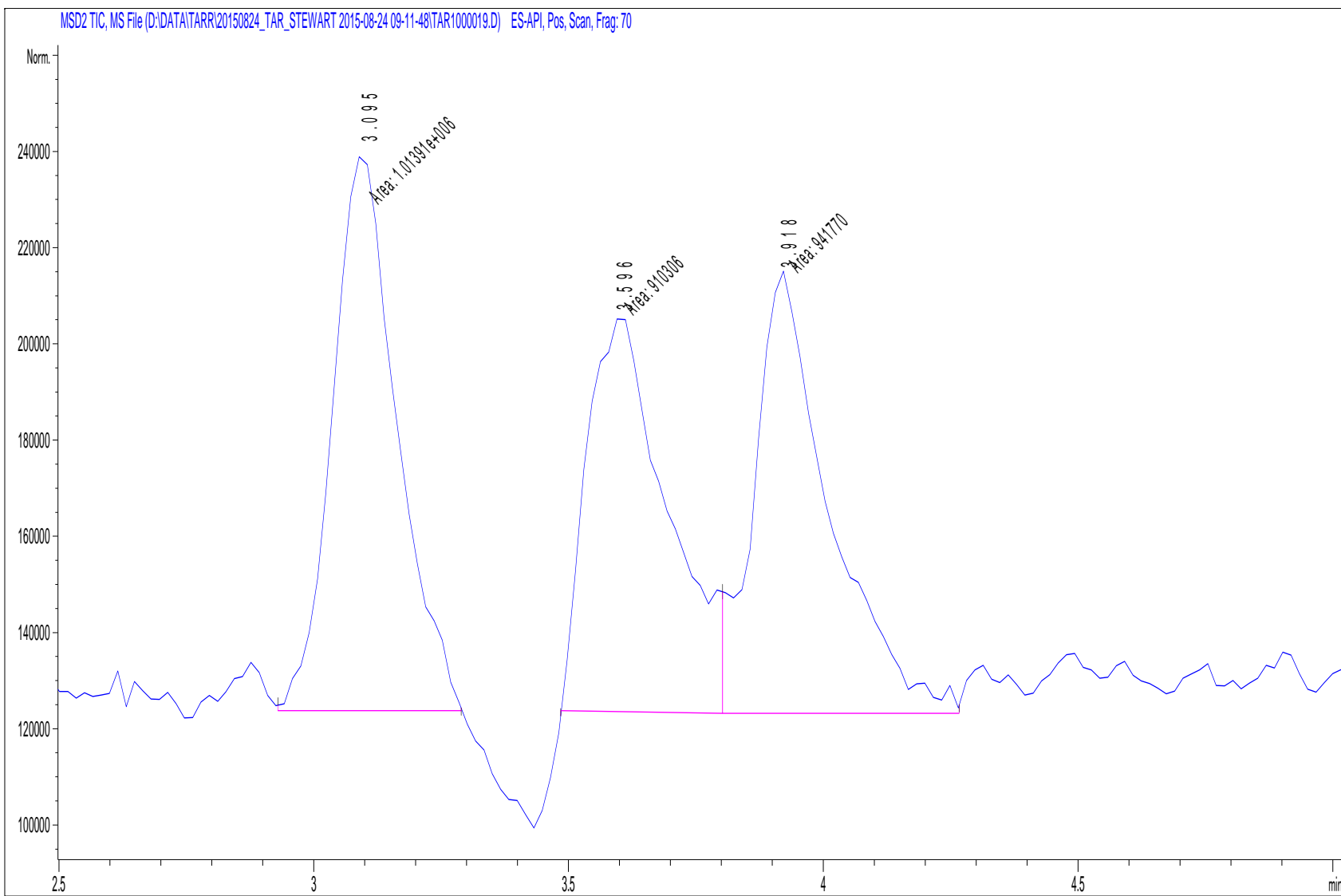
26-Jun-15

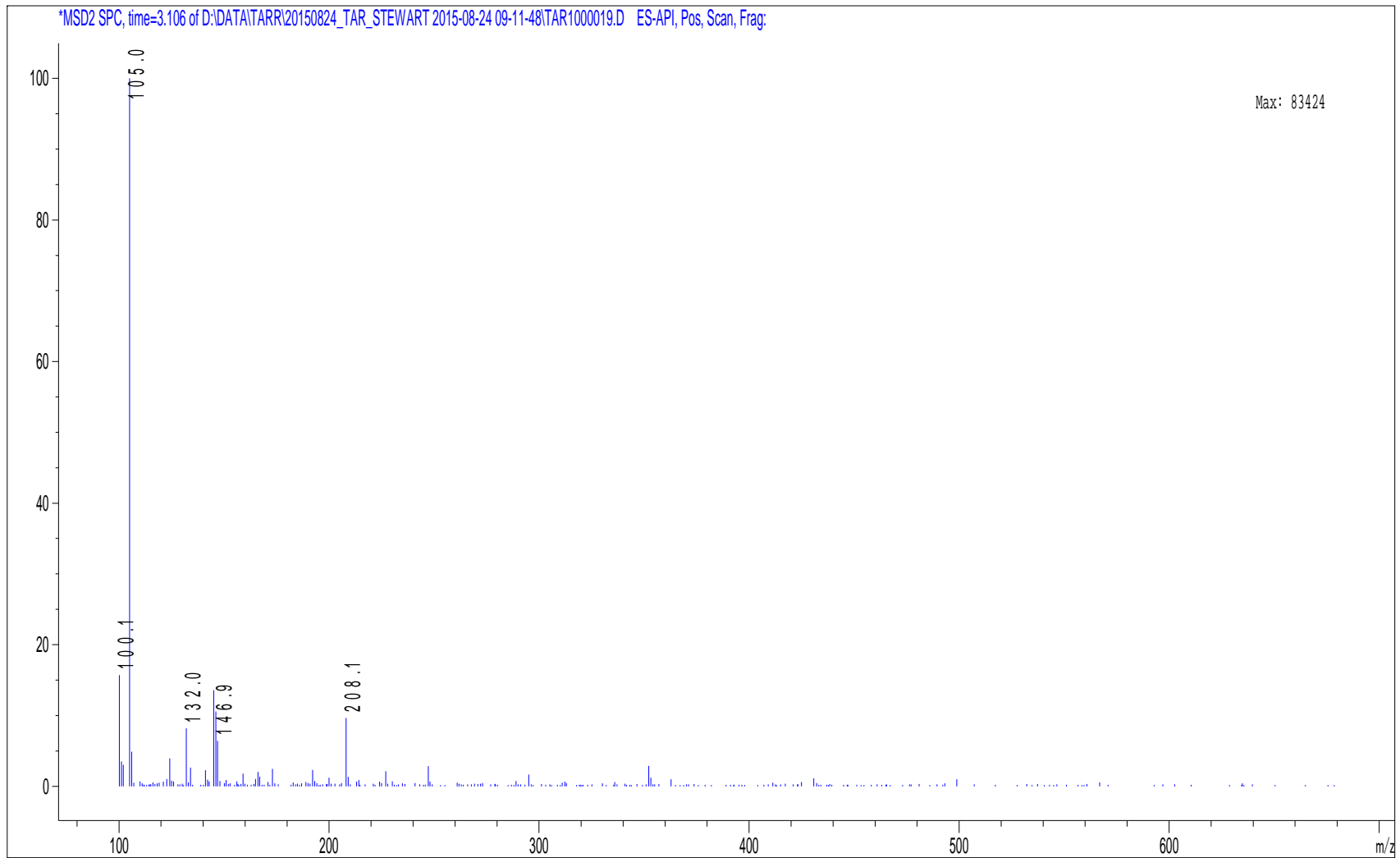
100 DC

P2-C-01



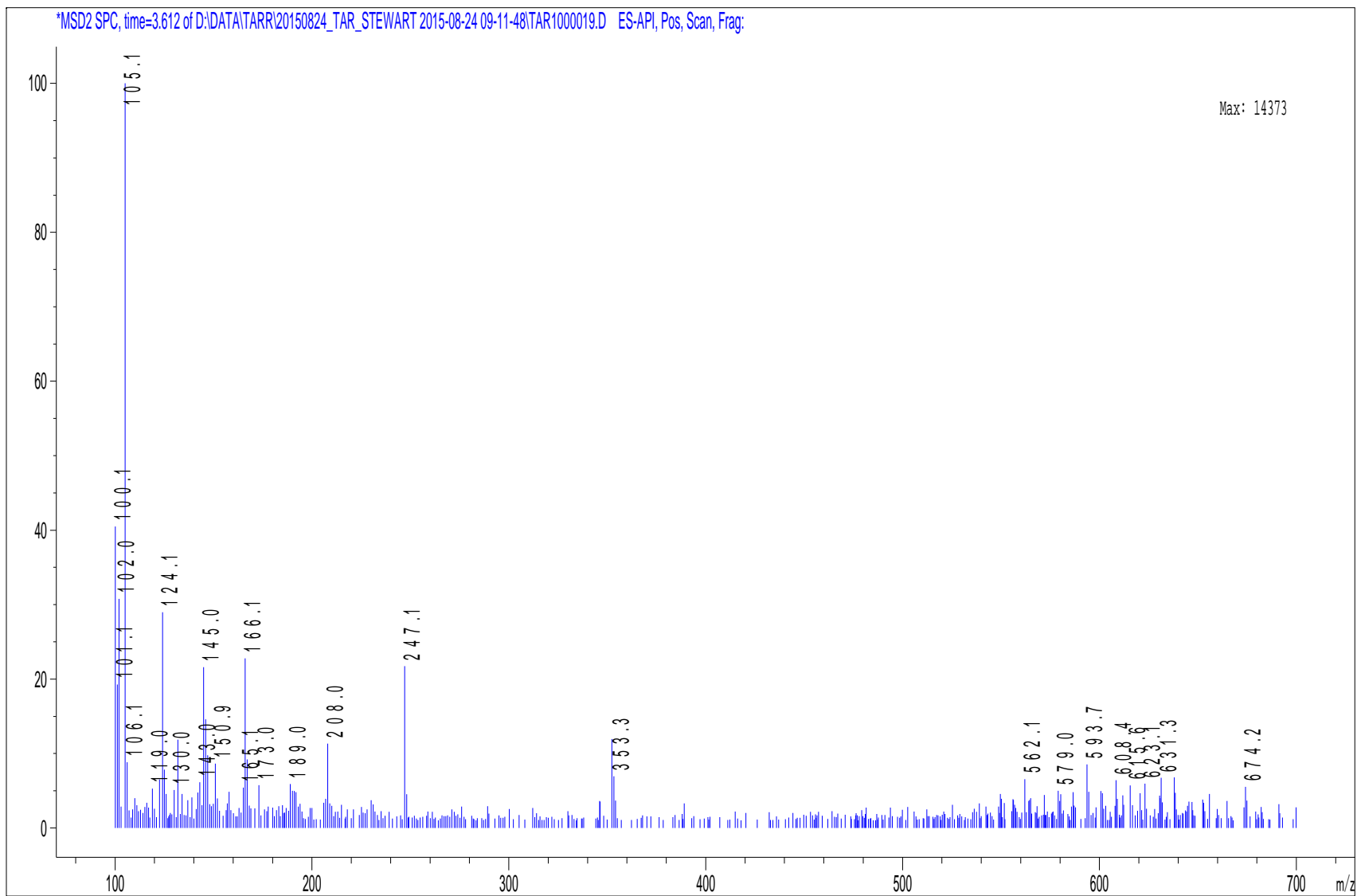
250





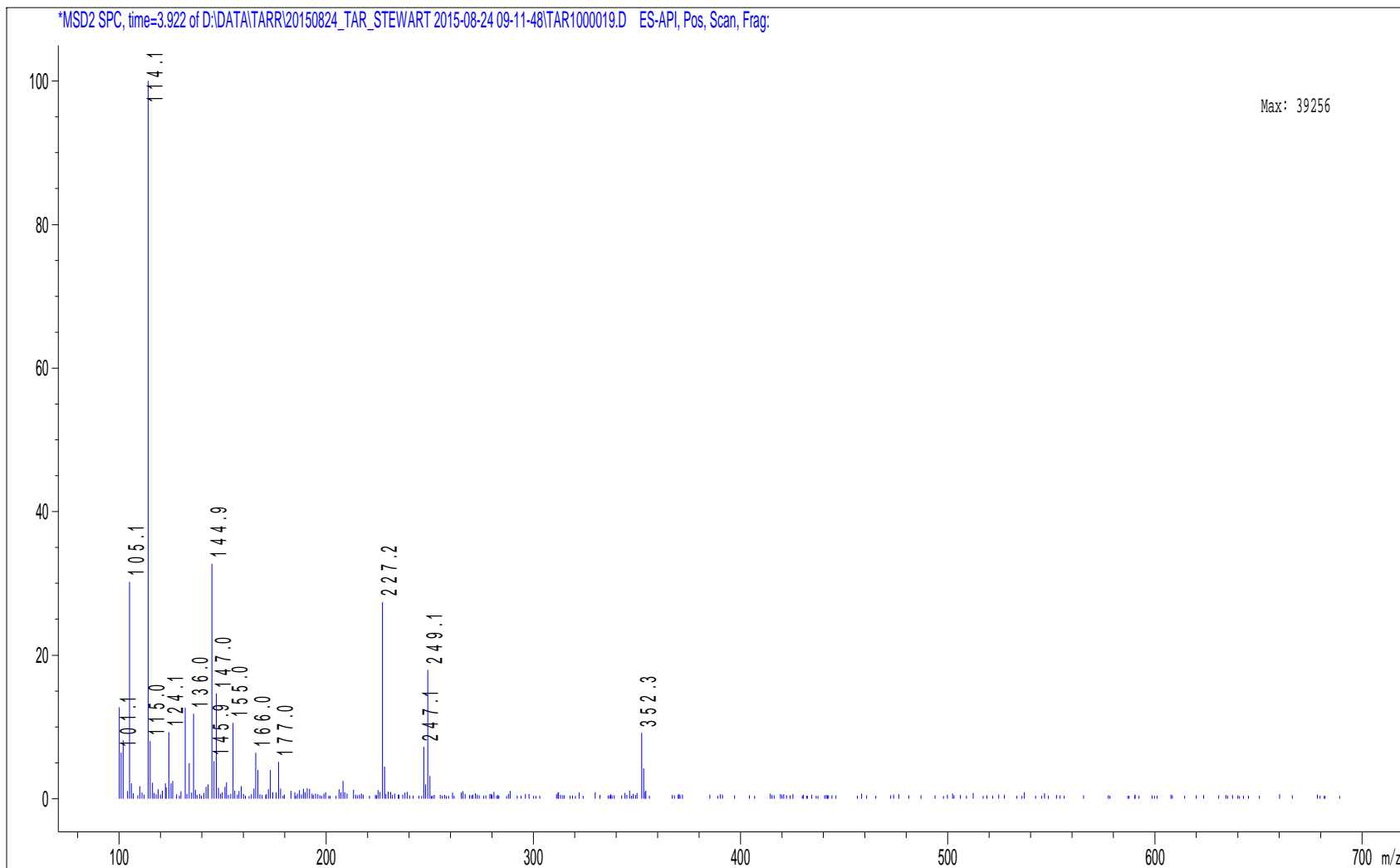


\*MSD2 SPC, time=3.612 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000019.D ES-API, Pos, Scan, Frag:



Max: 14373

\*MSD2 SPC, time=3.922 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000019.D ES-API, Pos, Scan, Frag:

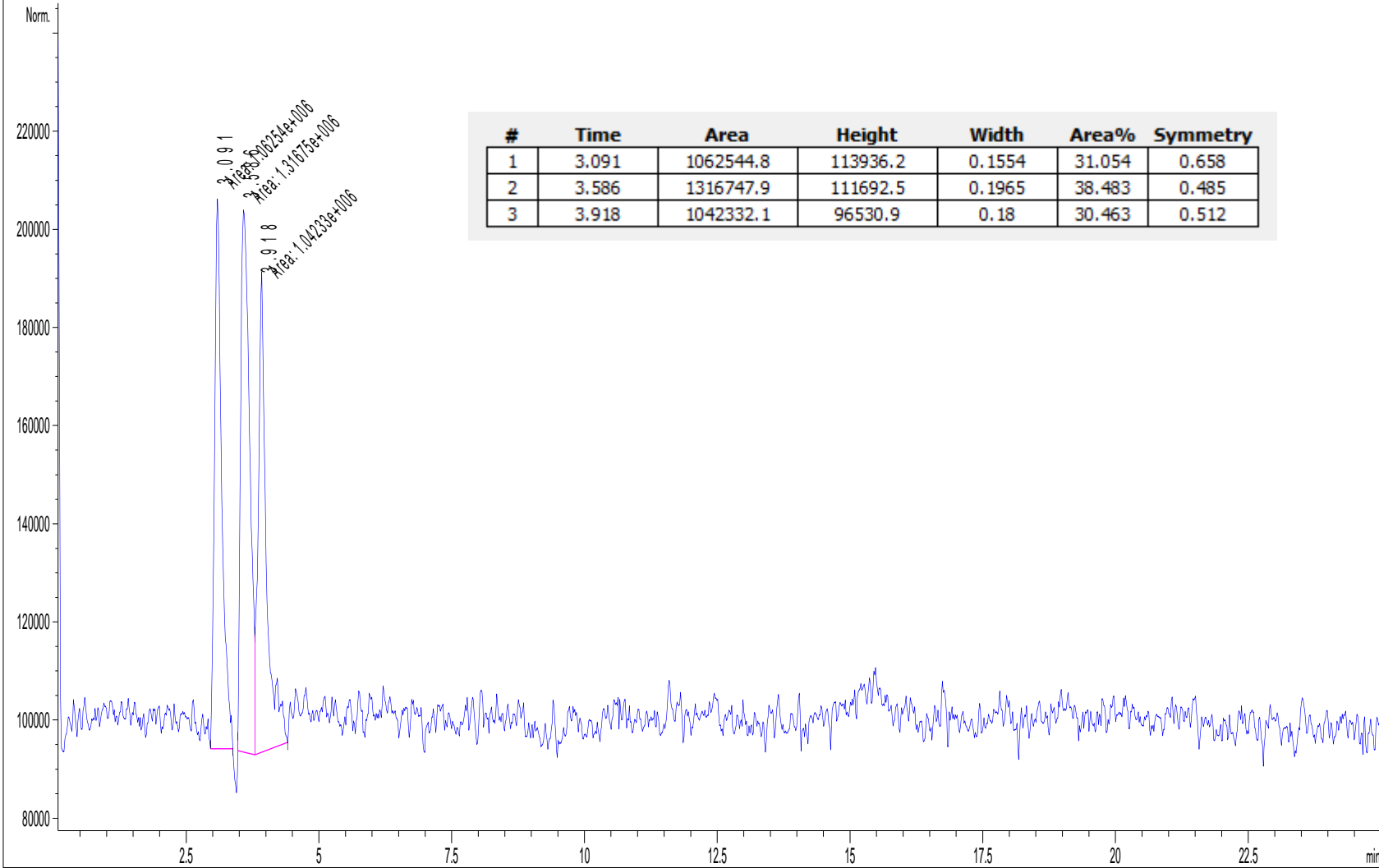


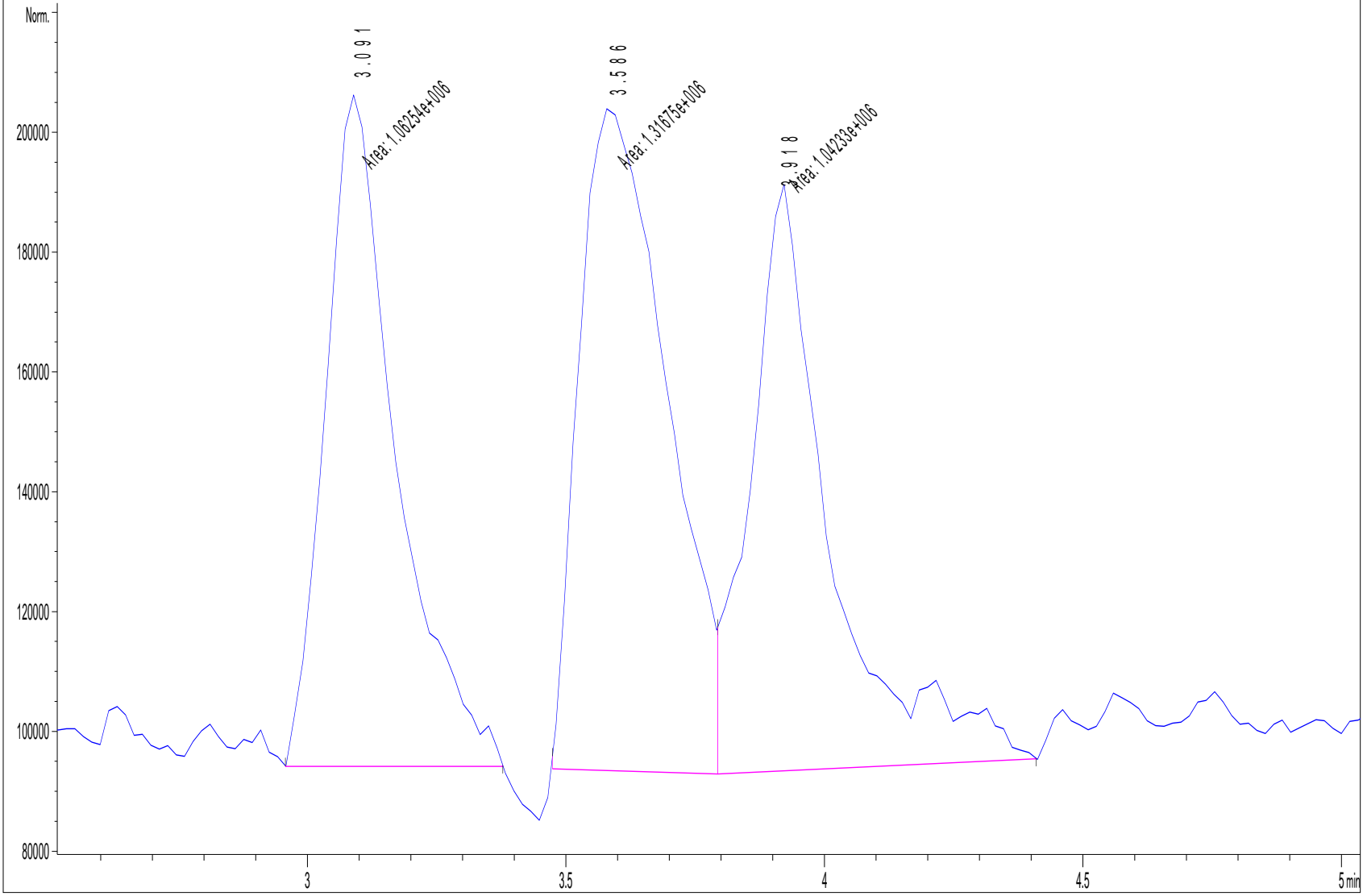
24-Jun-15

100 DC problem (no removal)

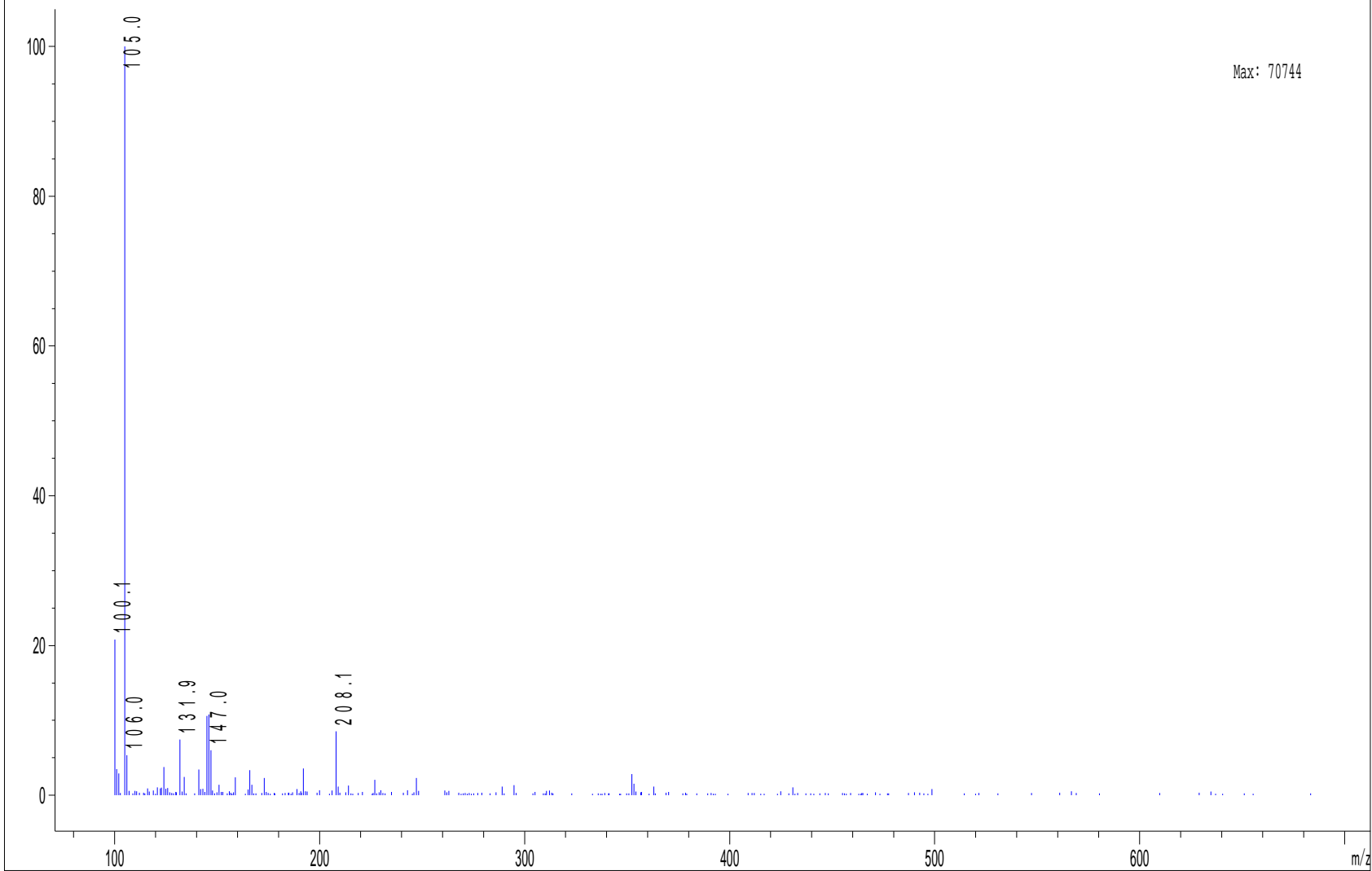
P2-E-07

MSD2 TIC, MS File (D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000043.D) ES-API, Pos, Scan, Frag: 70

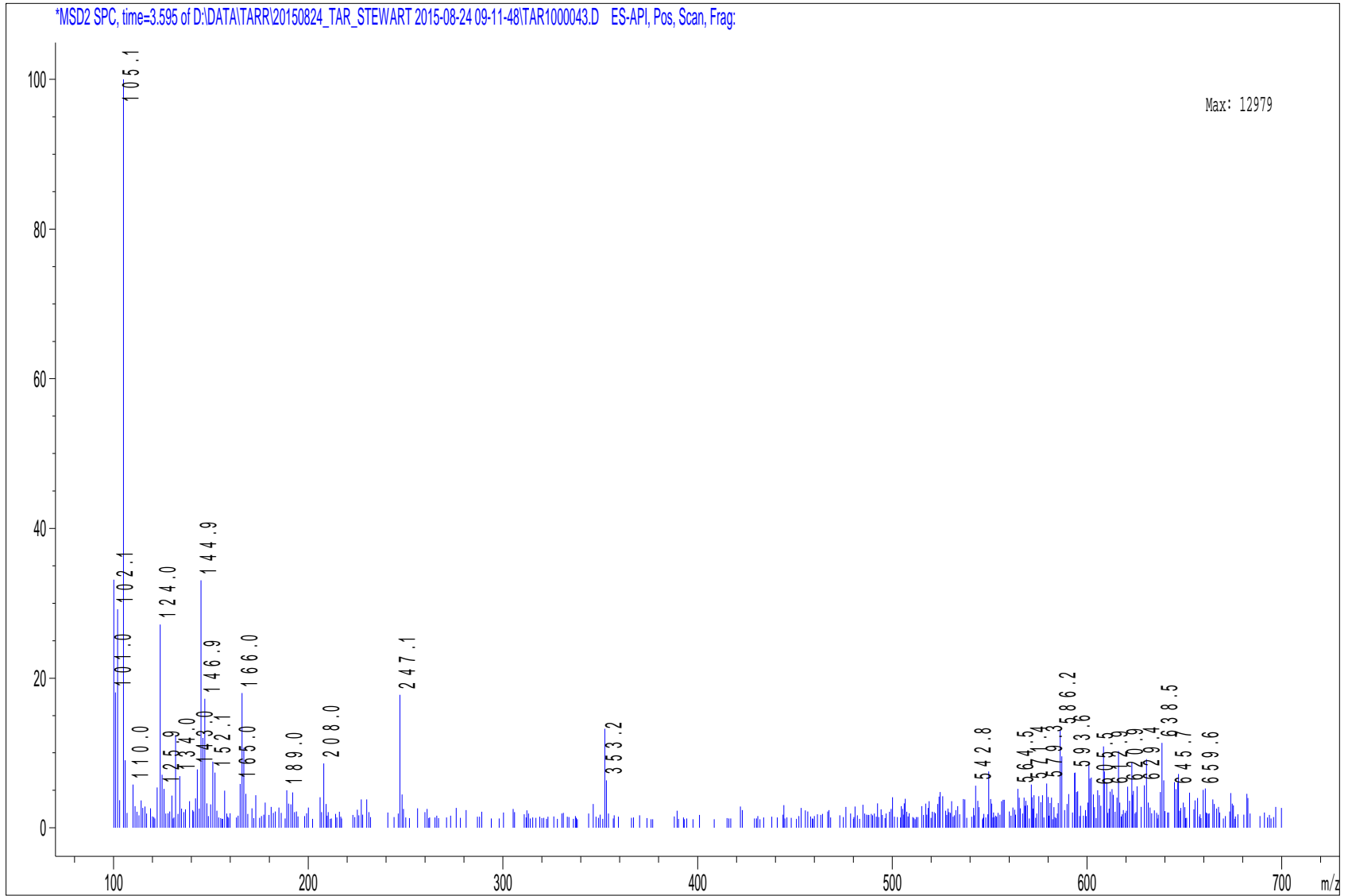


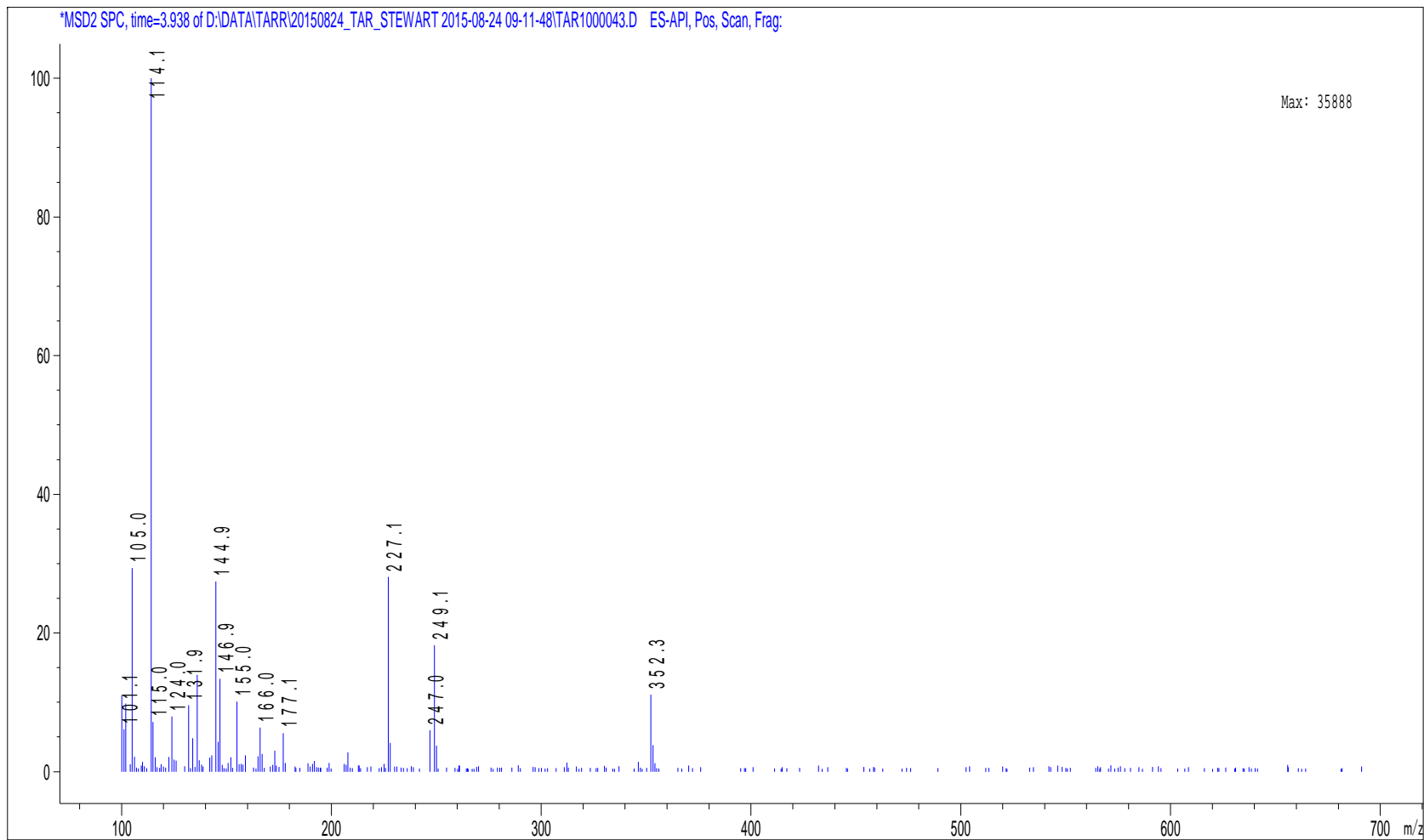


\*MSD2 SPC, time=3.106 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000043.D ES-API, Pos, Scan, Frag:



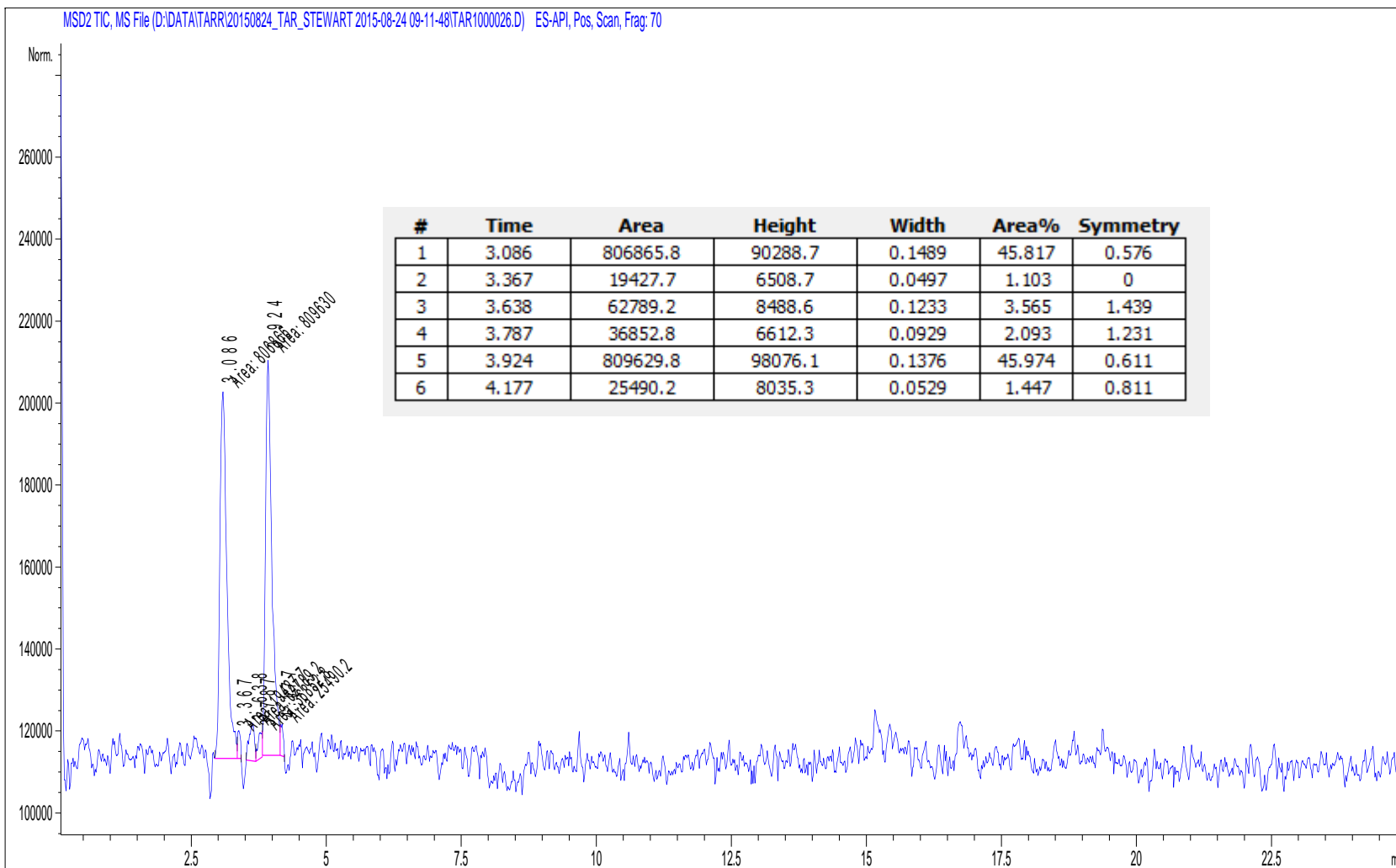
\*MSD2 SPC, time=3.595 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000043.D ES-API, Pos, Scan, Frag:



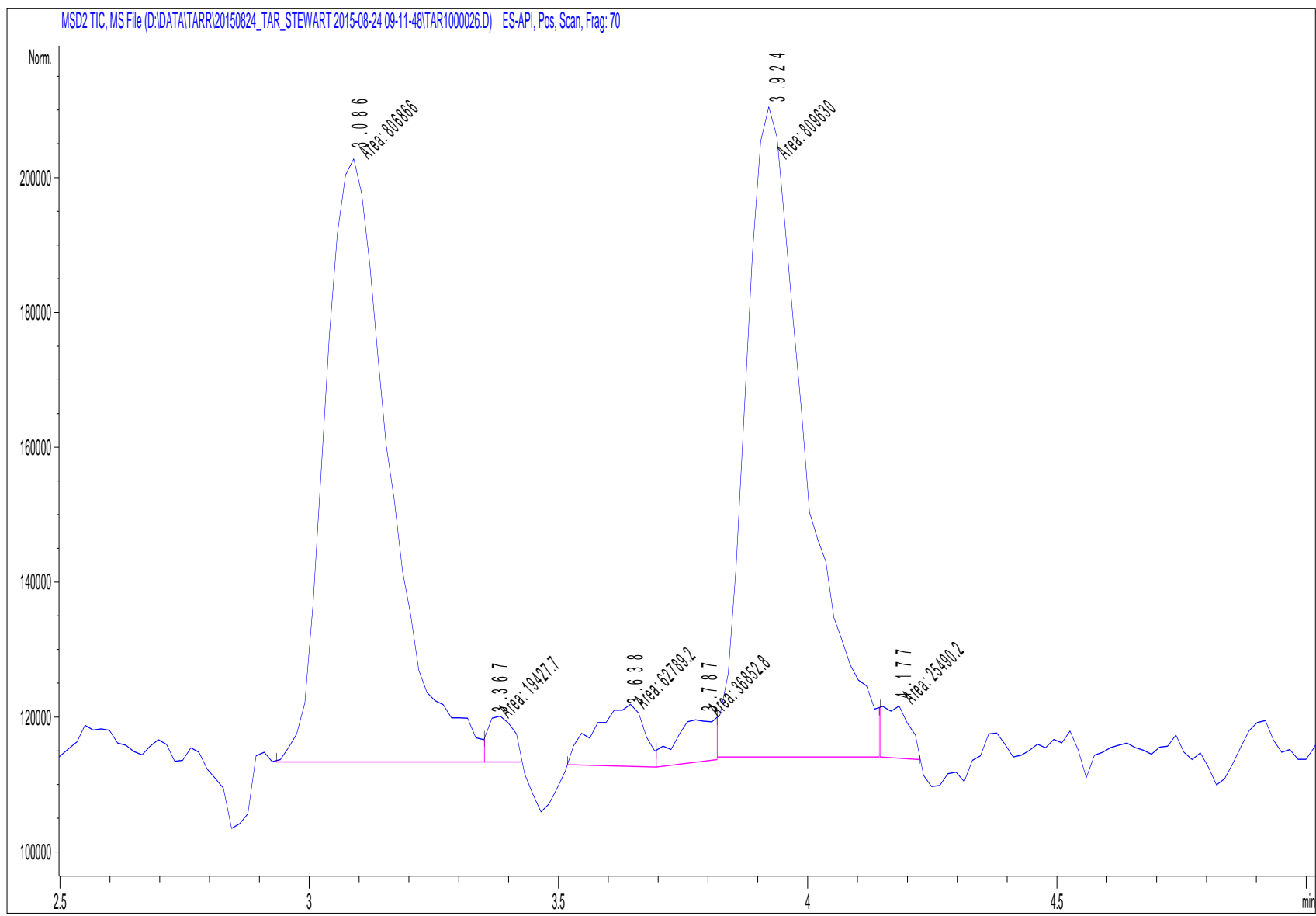


pH 7

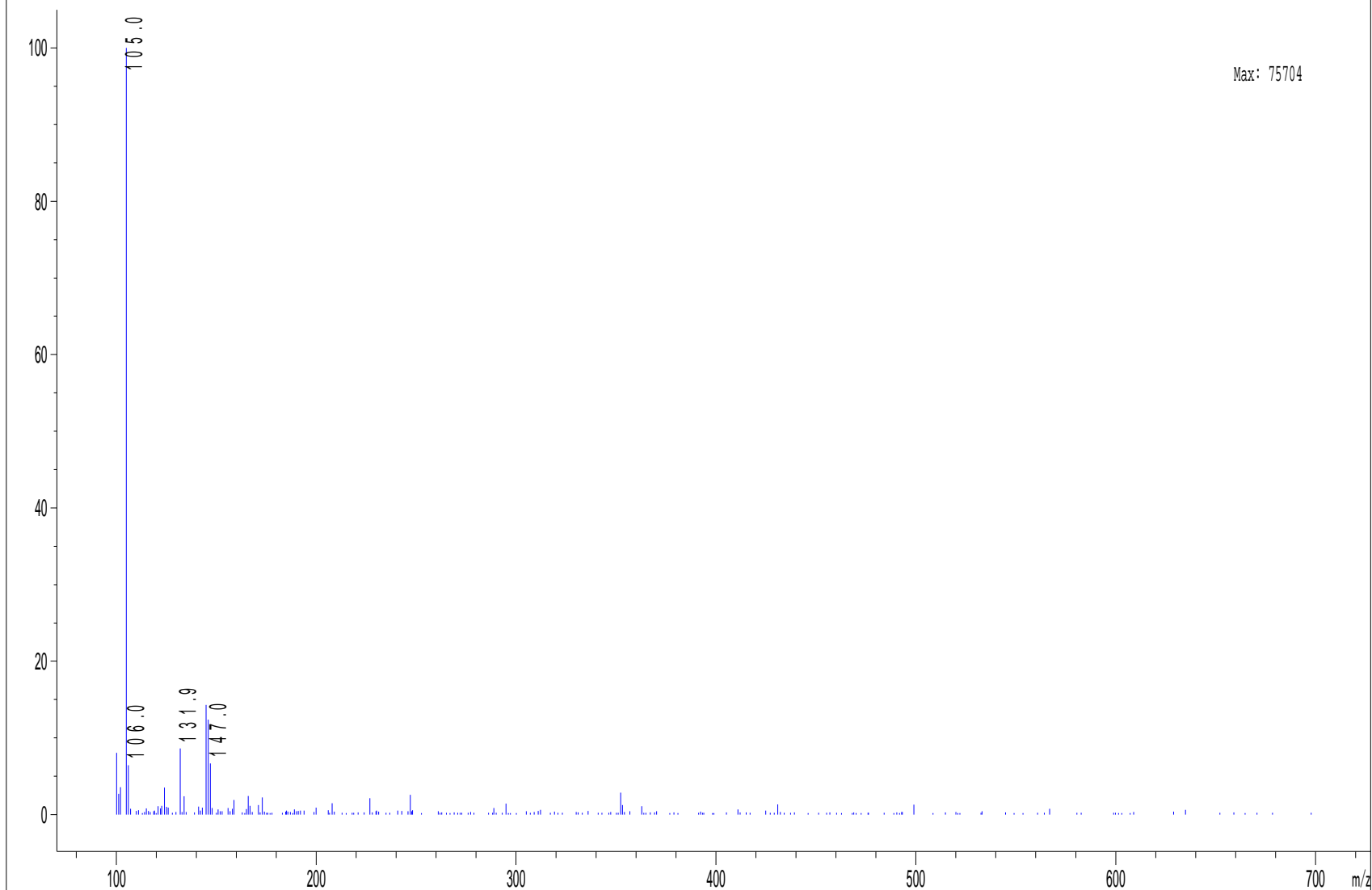
14-Jul-15  
H2O2 Ctrl  
P2-C-08



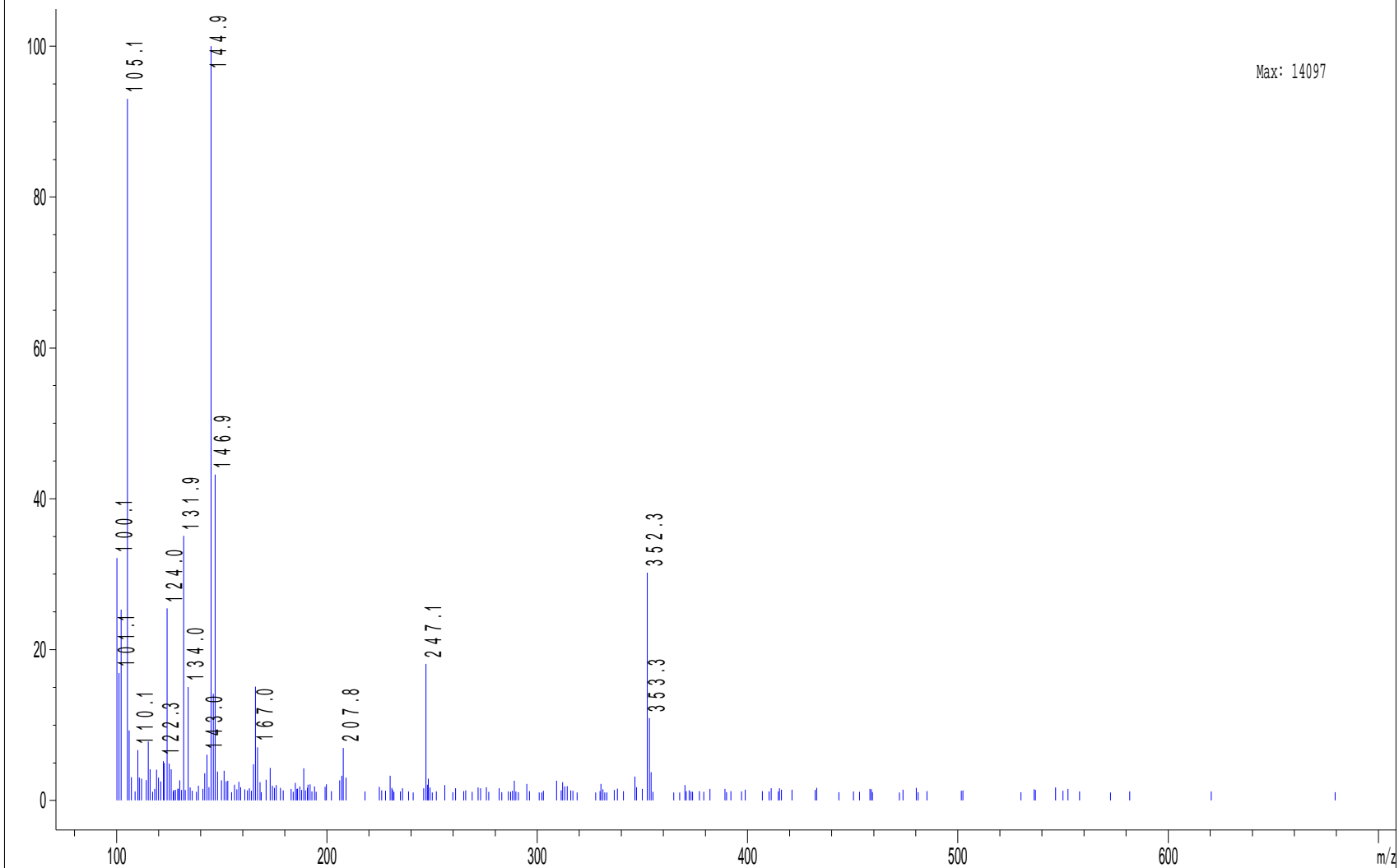




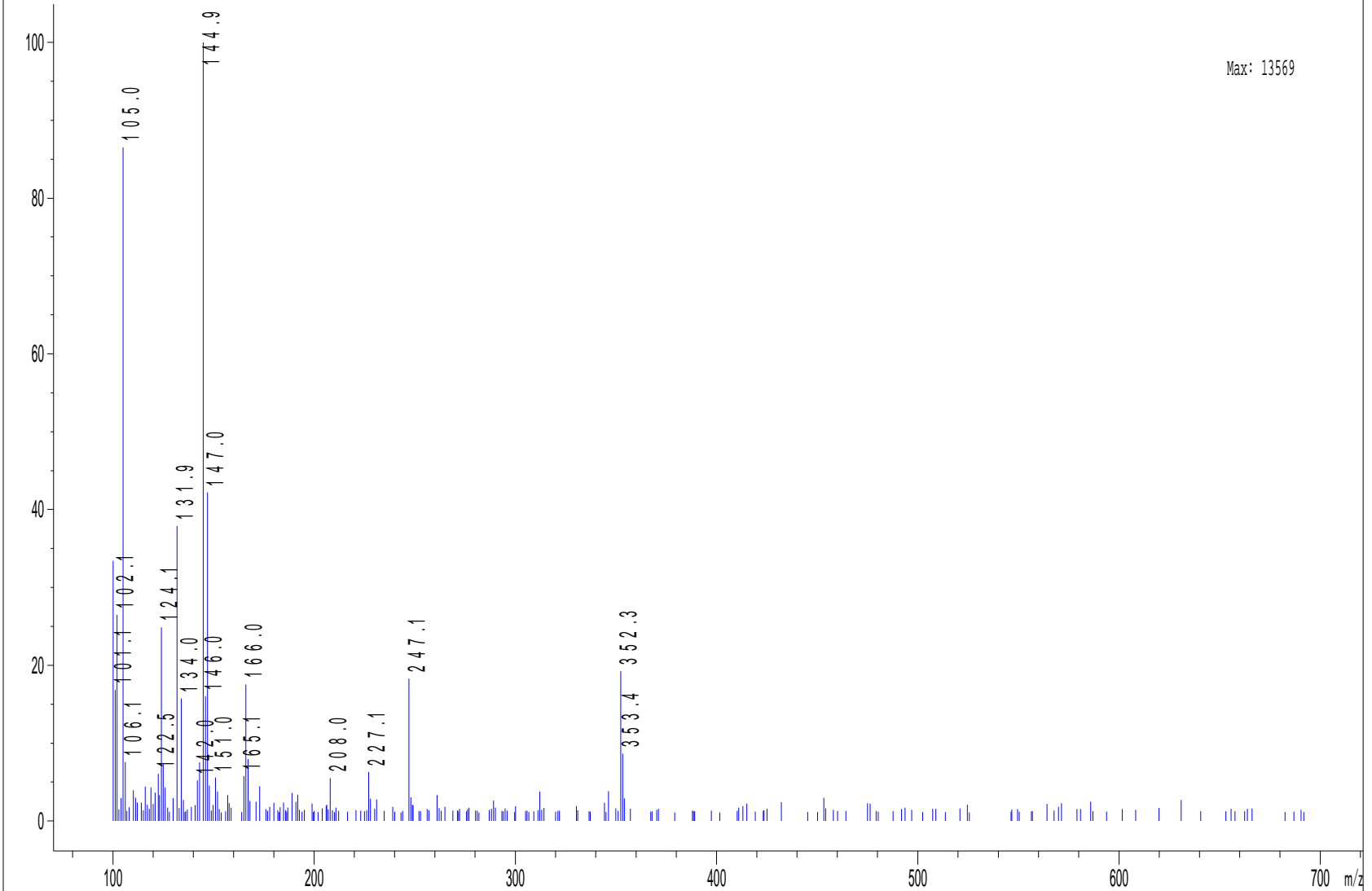
\*MSD2 SPC, time=3.106 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000026.D ES-API, Pos, Scan, Frag:



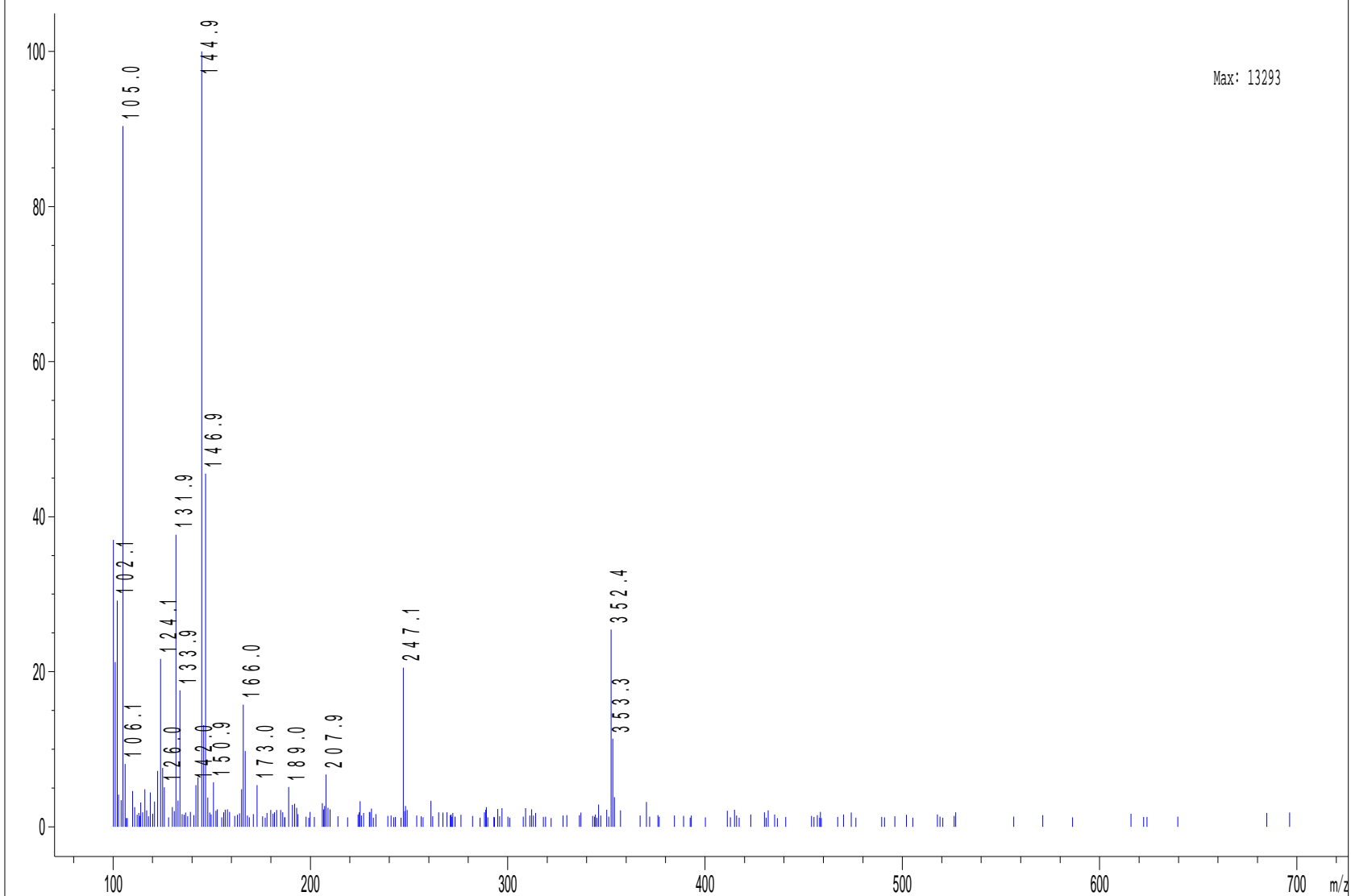
\*MSD2 SPC, time=3.383 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000026.D ES-API, Pos, Scan, Frag:

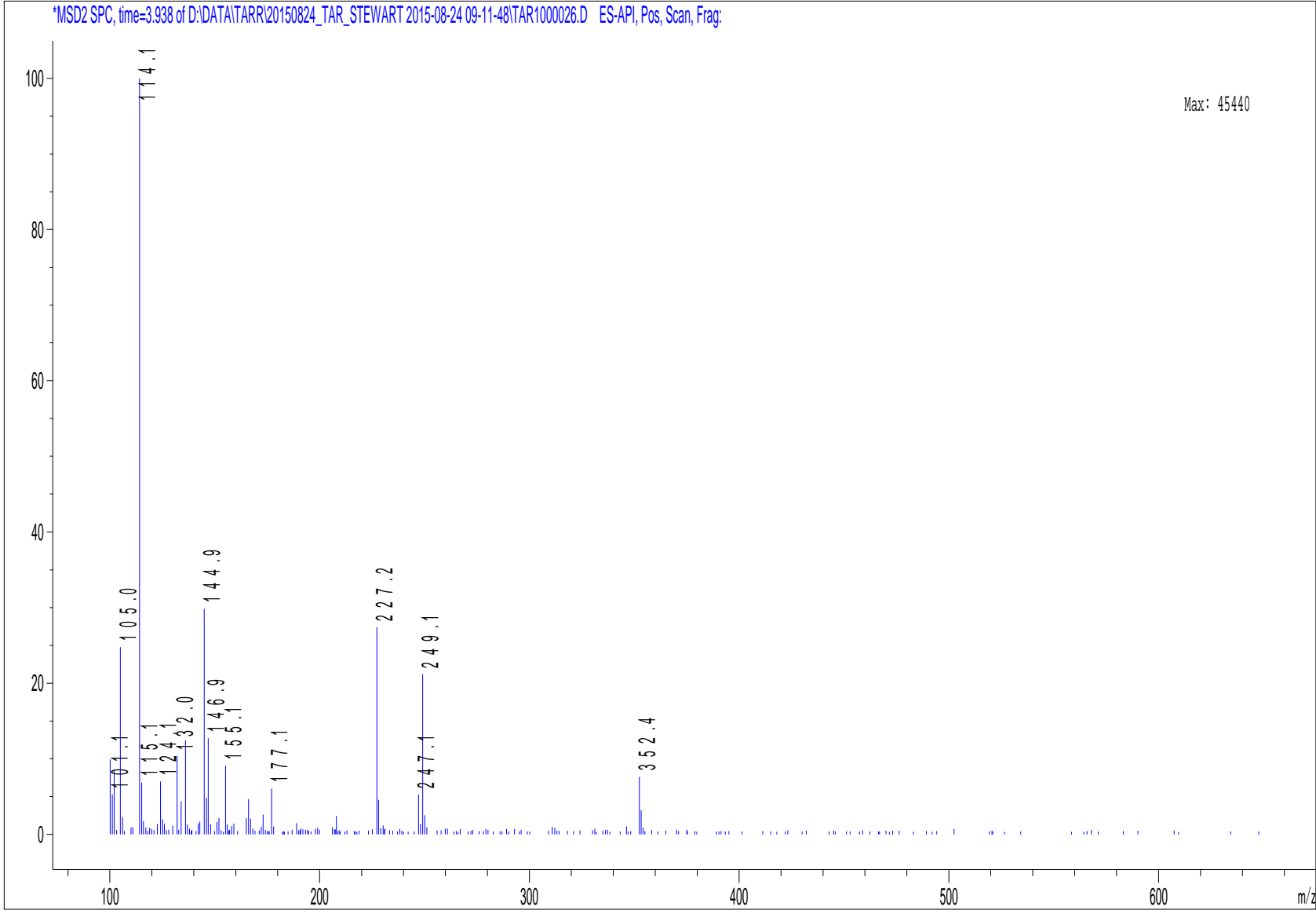


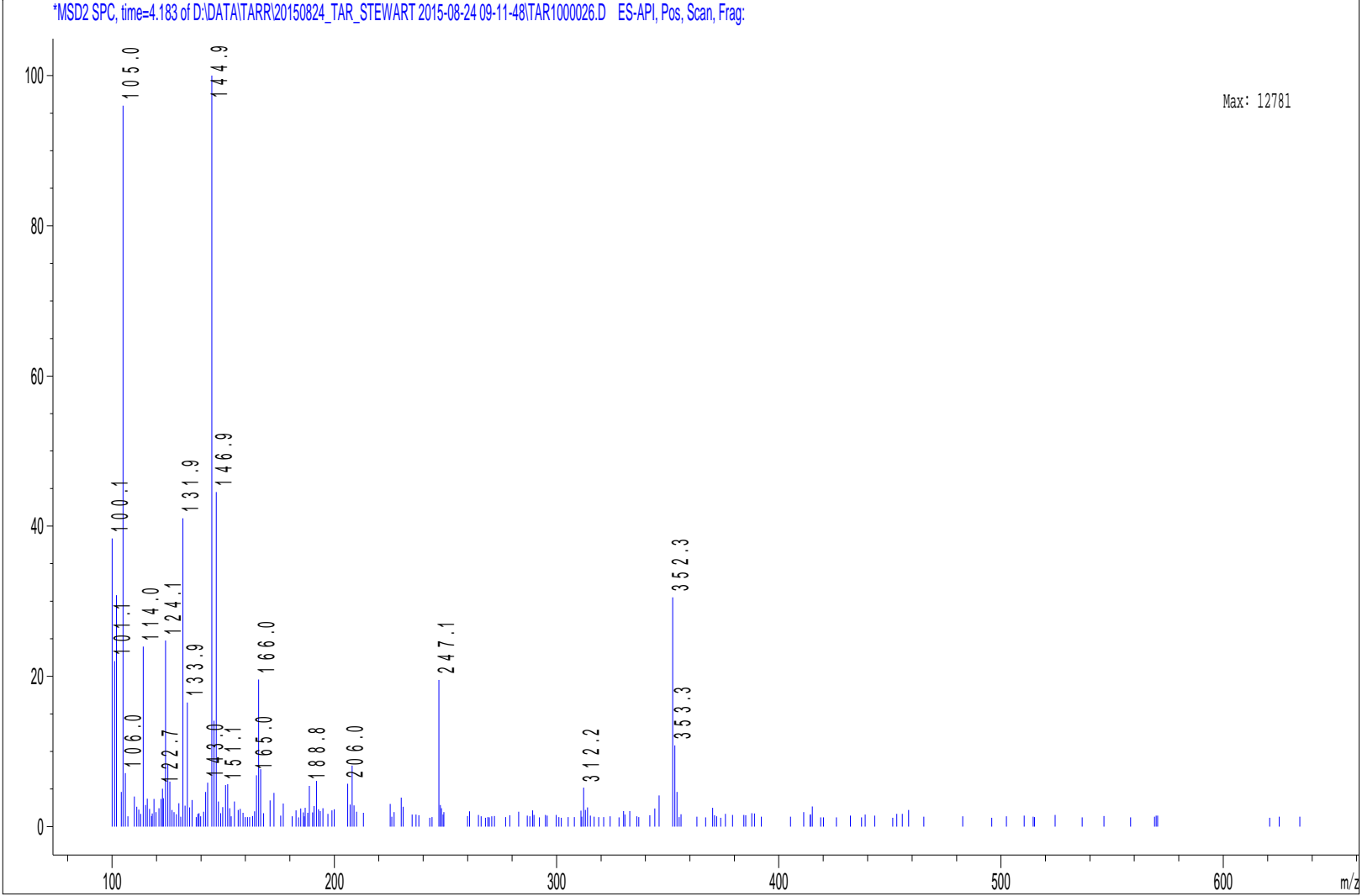
\*MSD2 SPC, time=3.628 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000026.D ES-API, Pos, Scan, Frag:



\*MSD2 SPC, time=3.775 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000026.D ES-API, Pos, Scan, Frag:



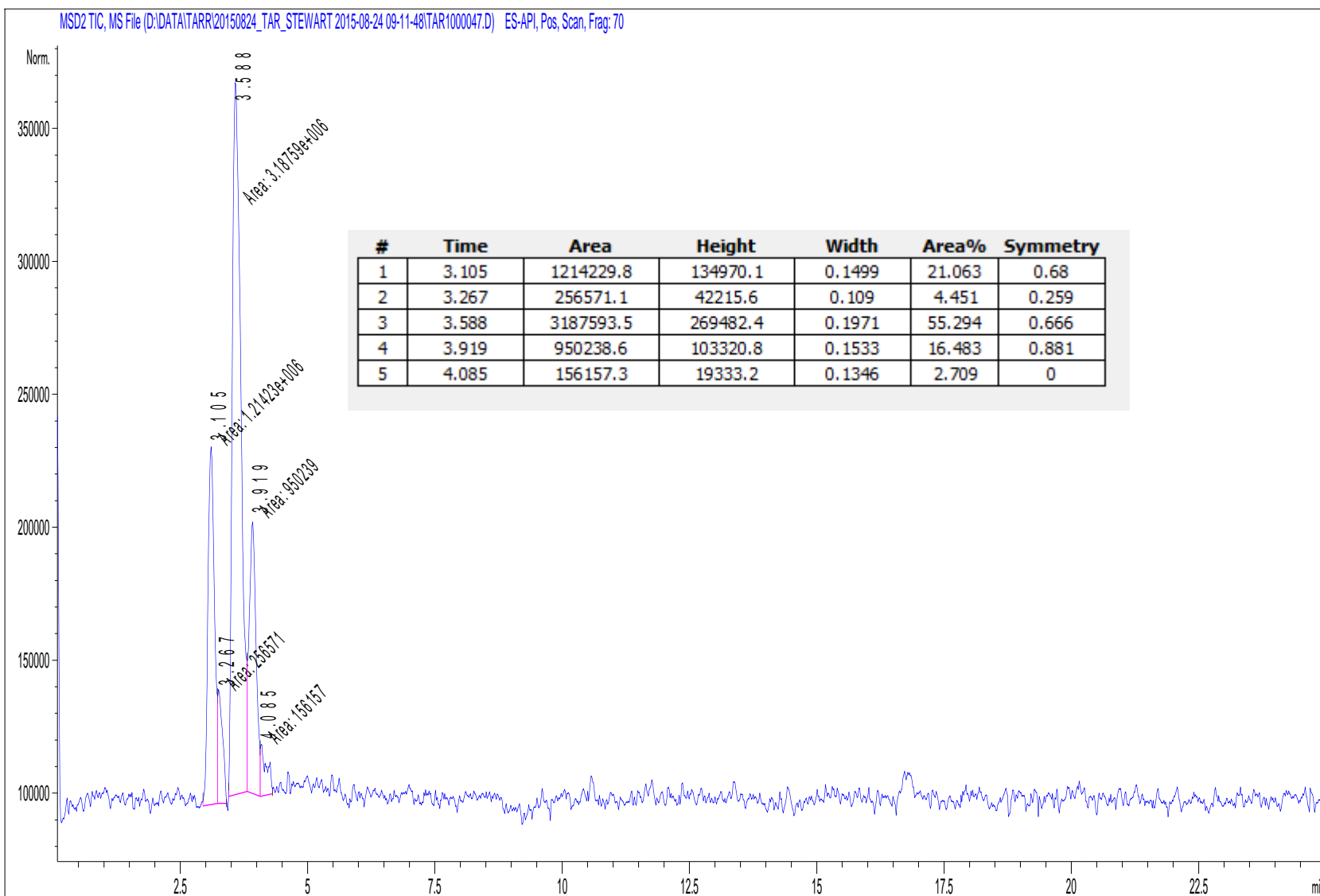




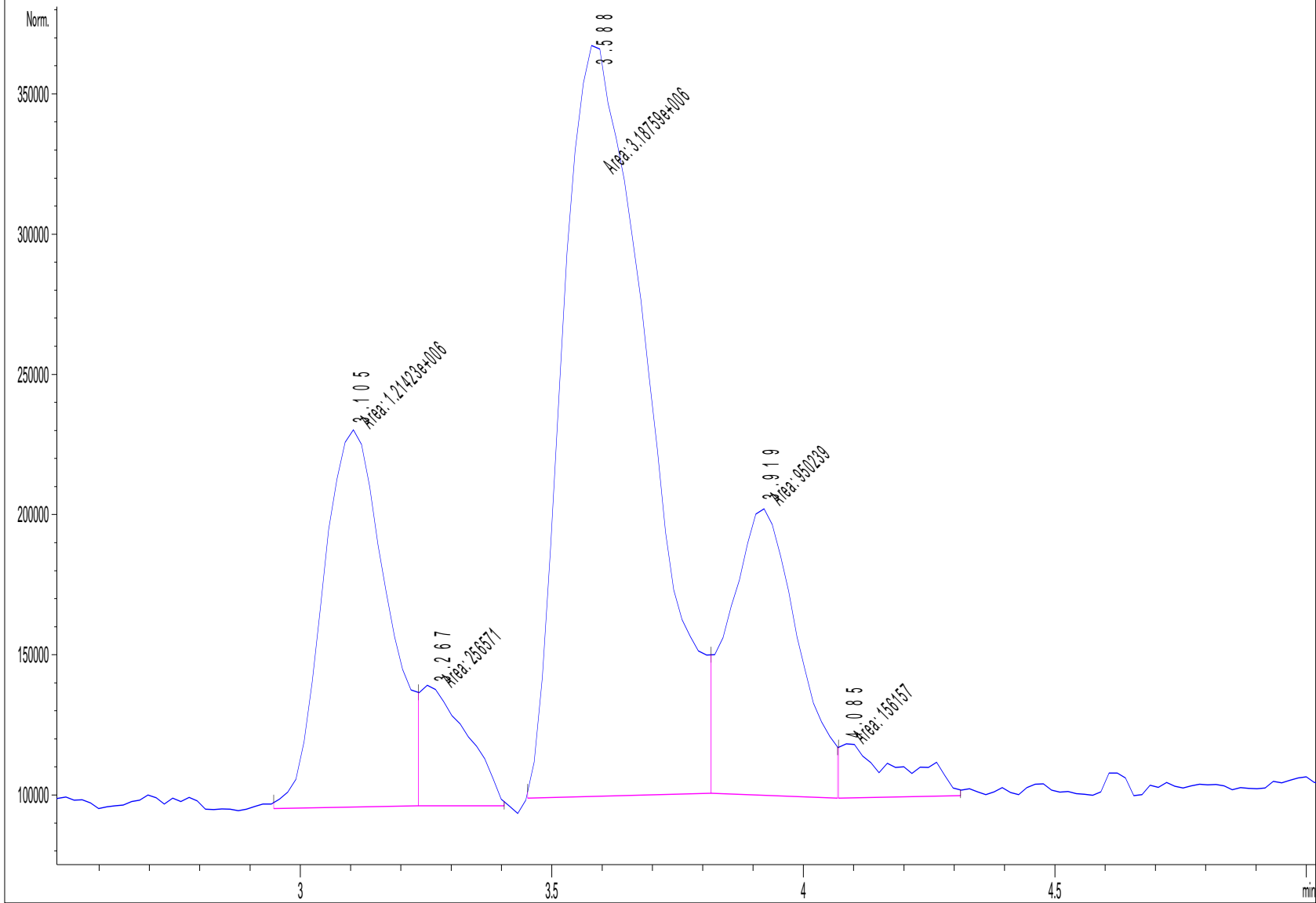
7-Mar-15

0 DC

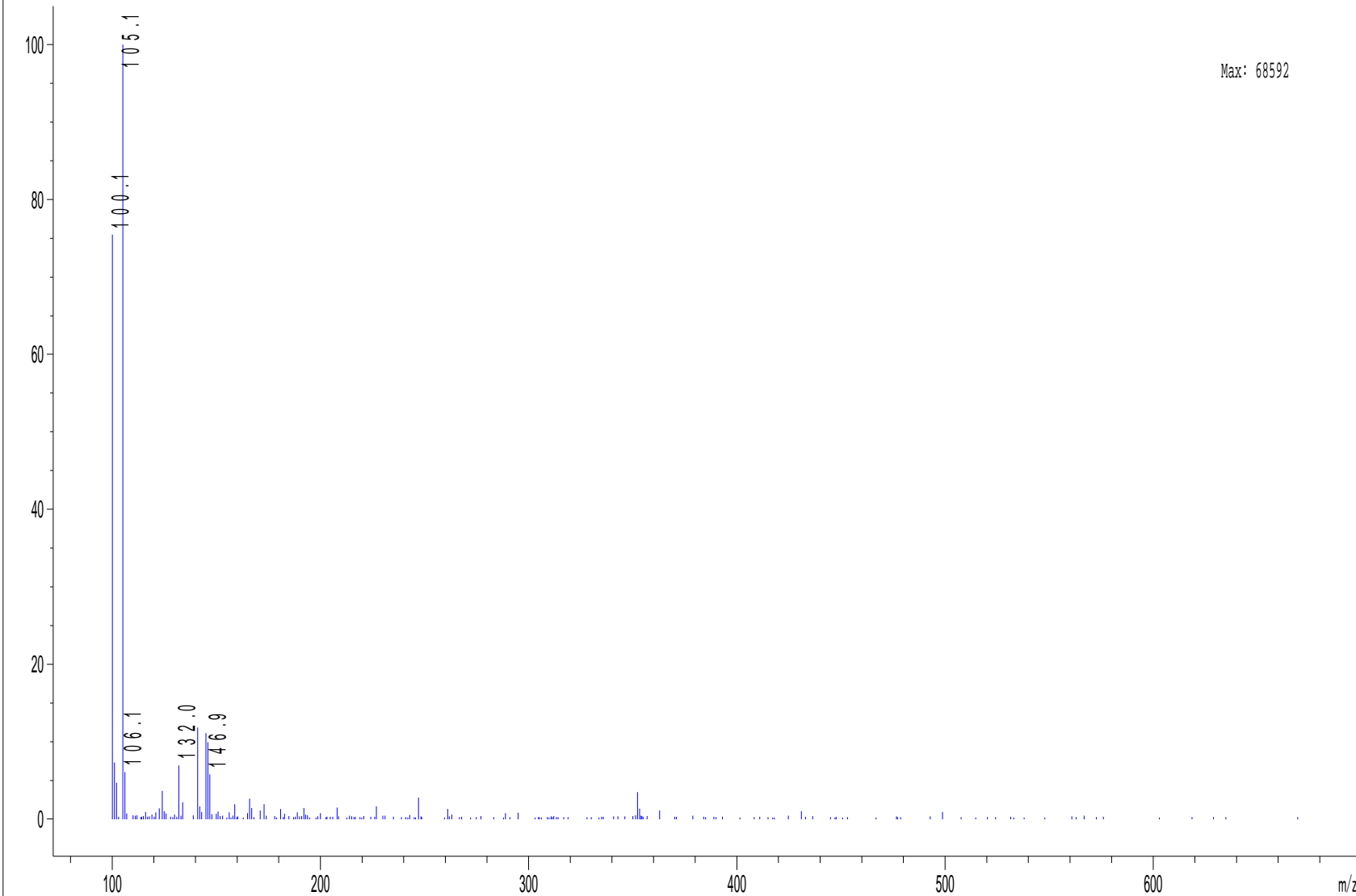
P2-A-02



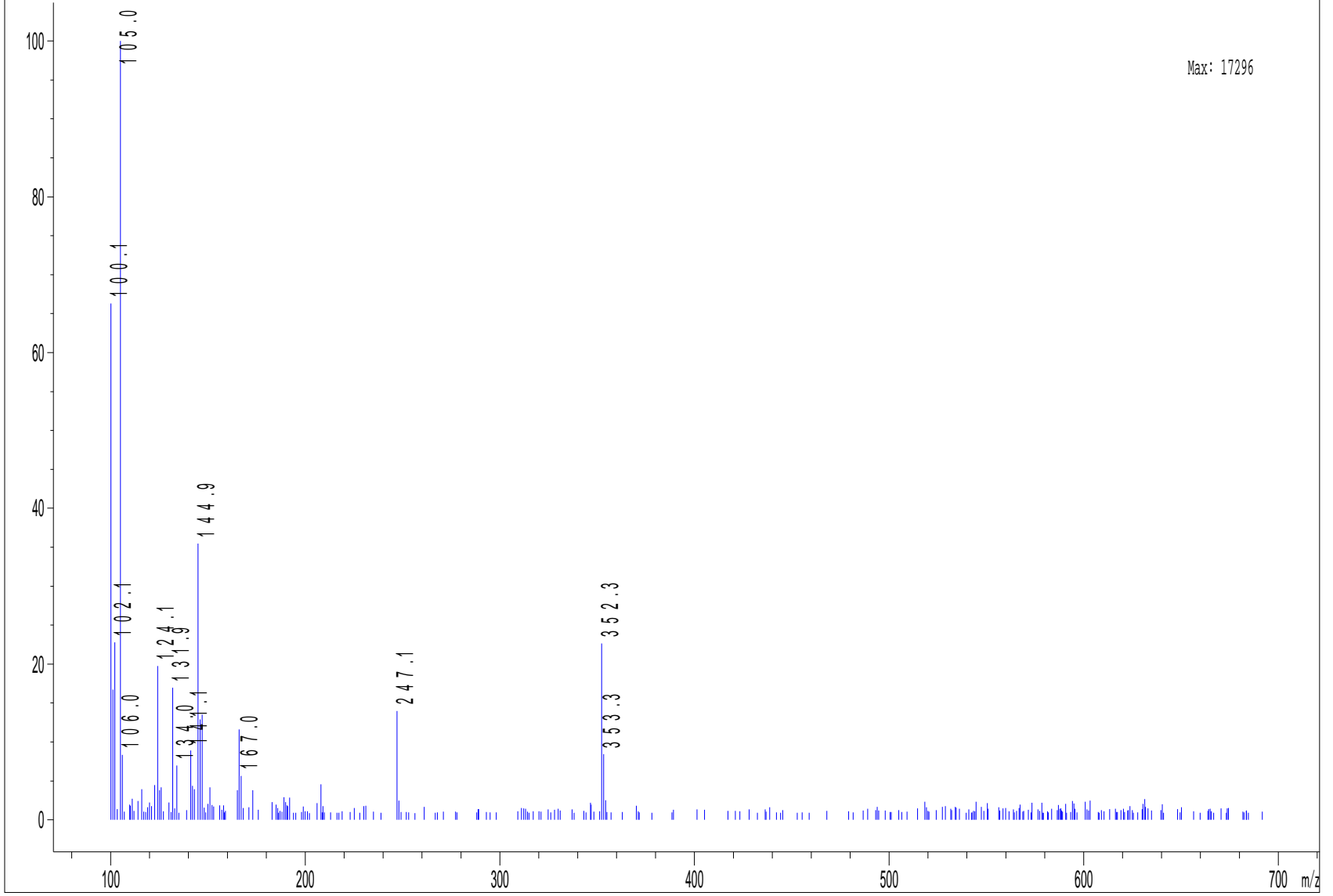




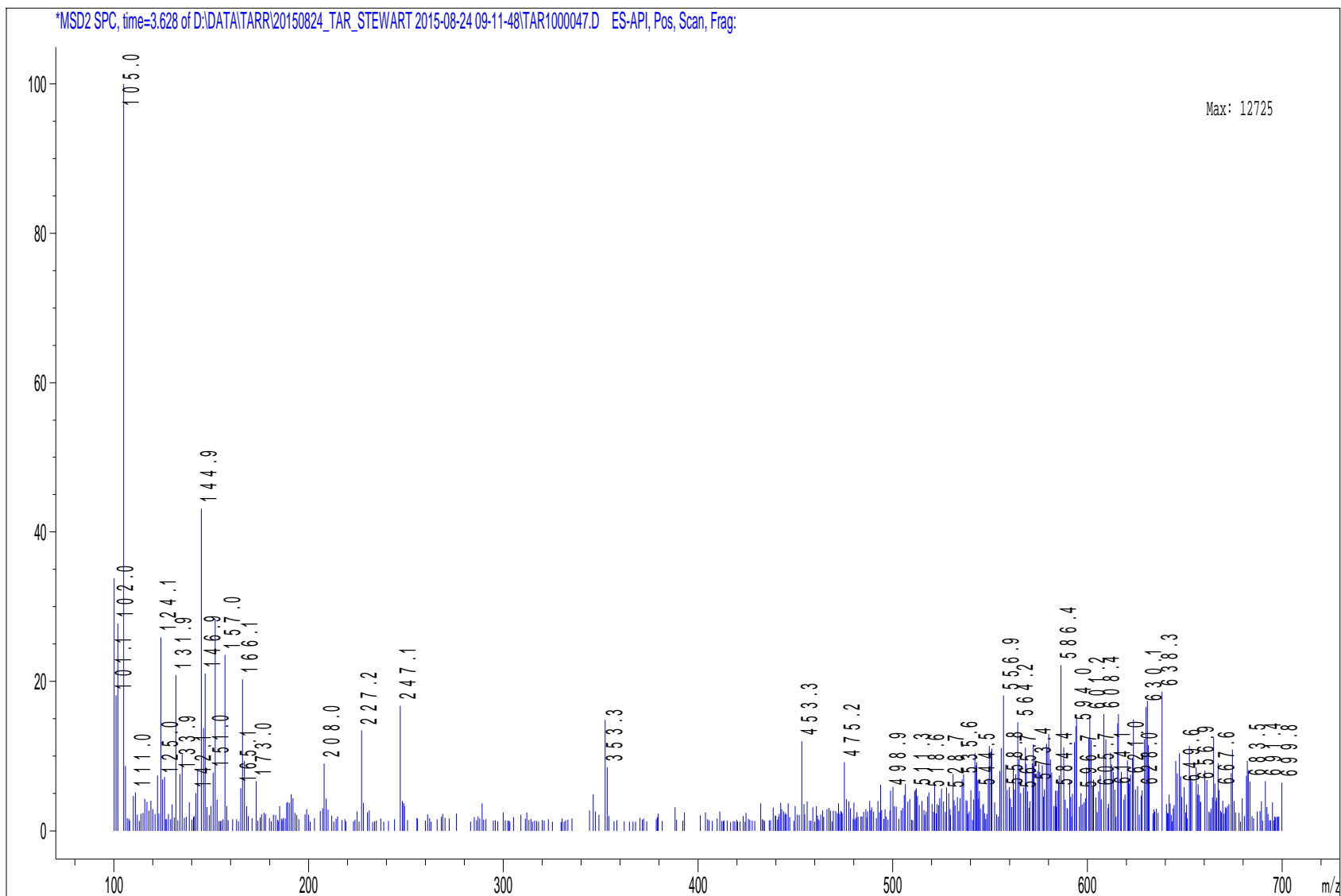
\*MSD2 SPC, time=3.106 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09:11:48\TAR1000047.D ES-API, Pos, Scan, Frag:



\*MSD2 SPC, time=3.285 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000047.D ES-API, Pos, Scan, Frag:

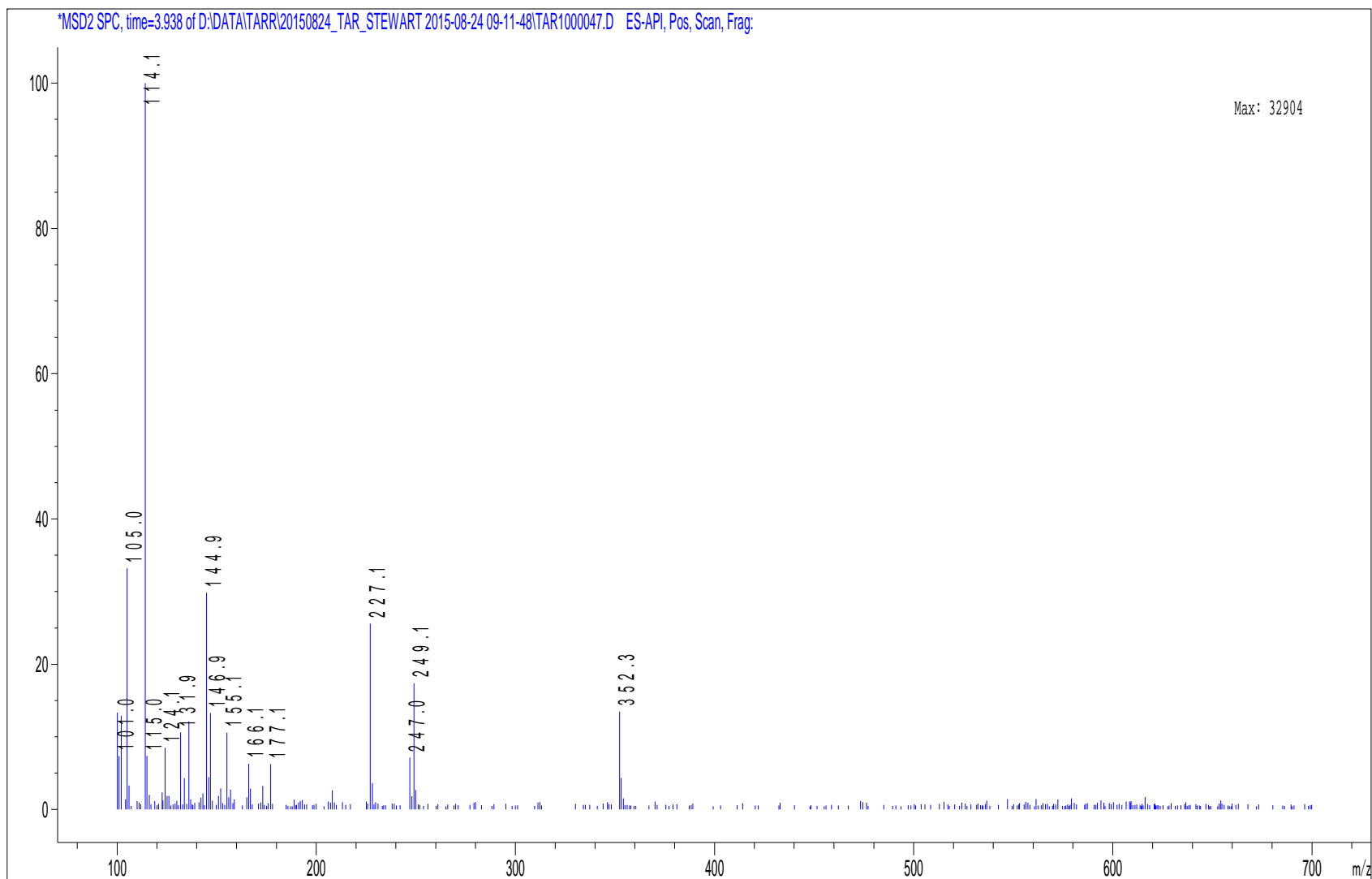


\*MSD2 SPC, time=3.628 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000047.D ES-API, Pos, Scan, Frag:

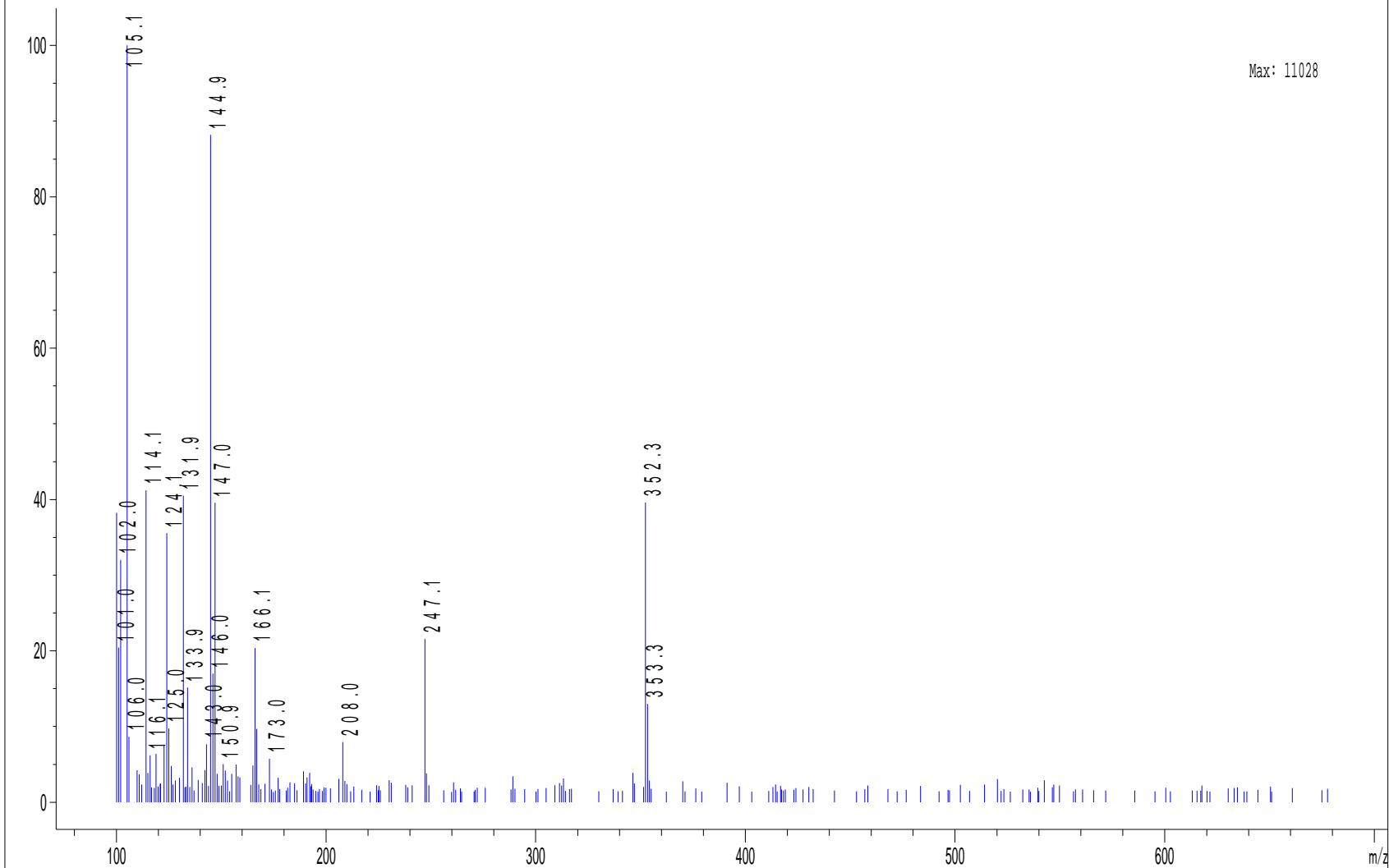


Max: 12725

\*MSD2 SPC, time=3.938 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09:11:48\TAR1000047.D ES-API, Pos, Scan, Frag:



\*MSD2 SPC, time=4.118 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09:11:48\TAR1000047.D ES-API, Pos, Scan, Frag:

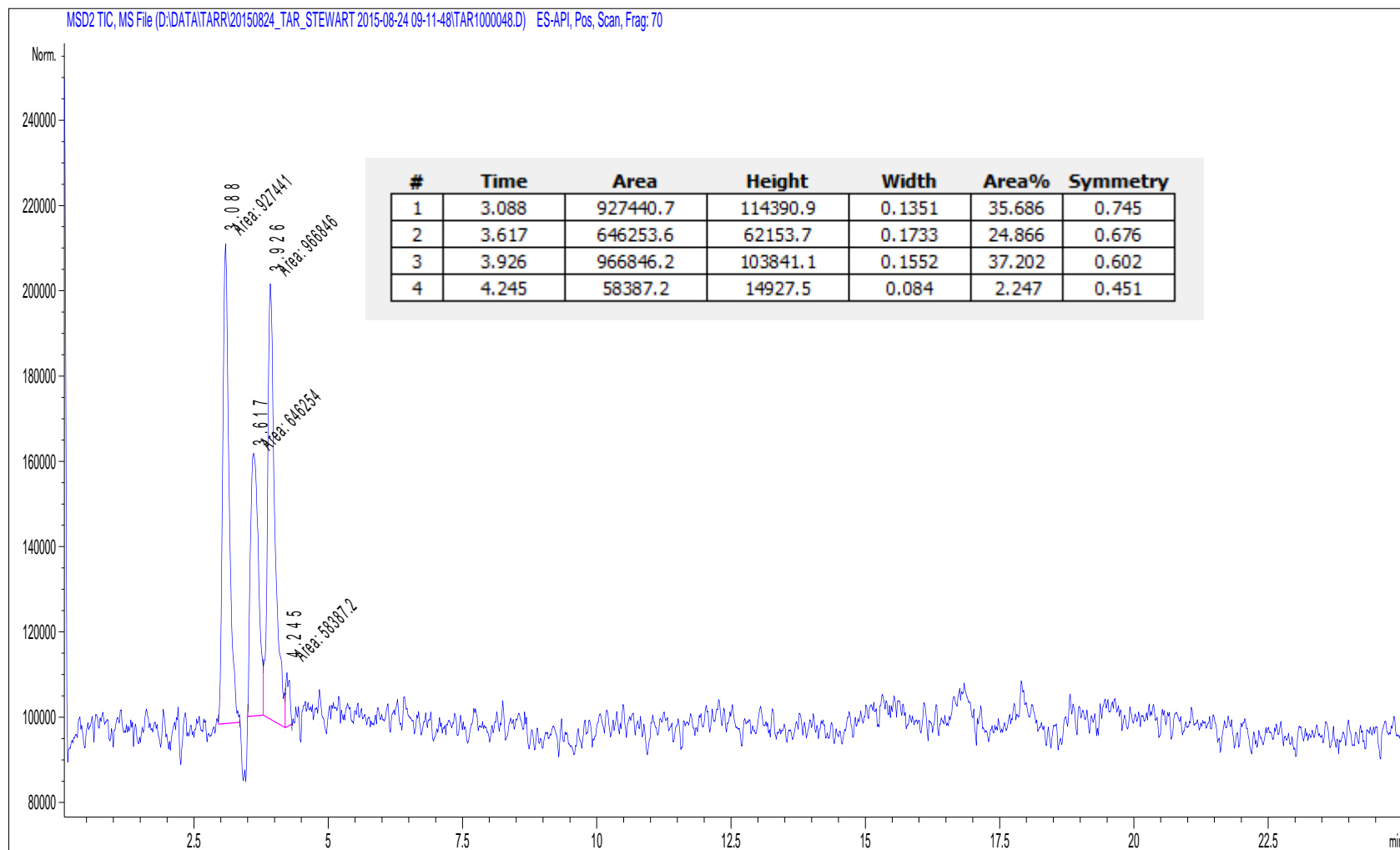


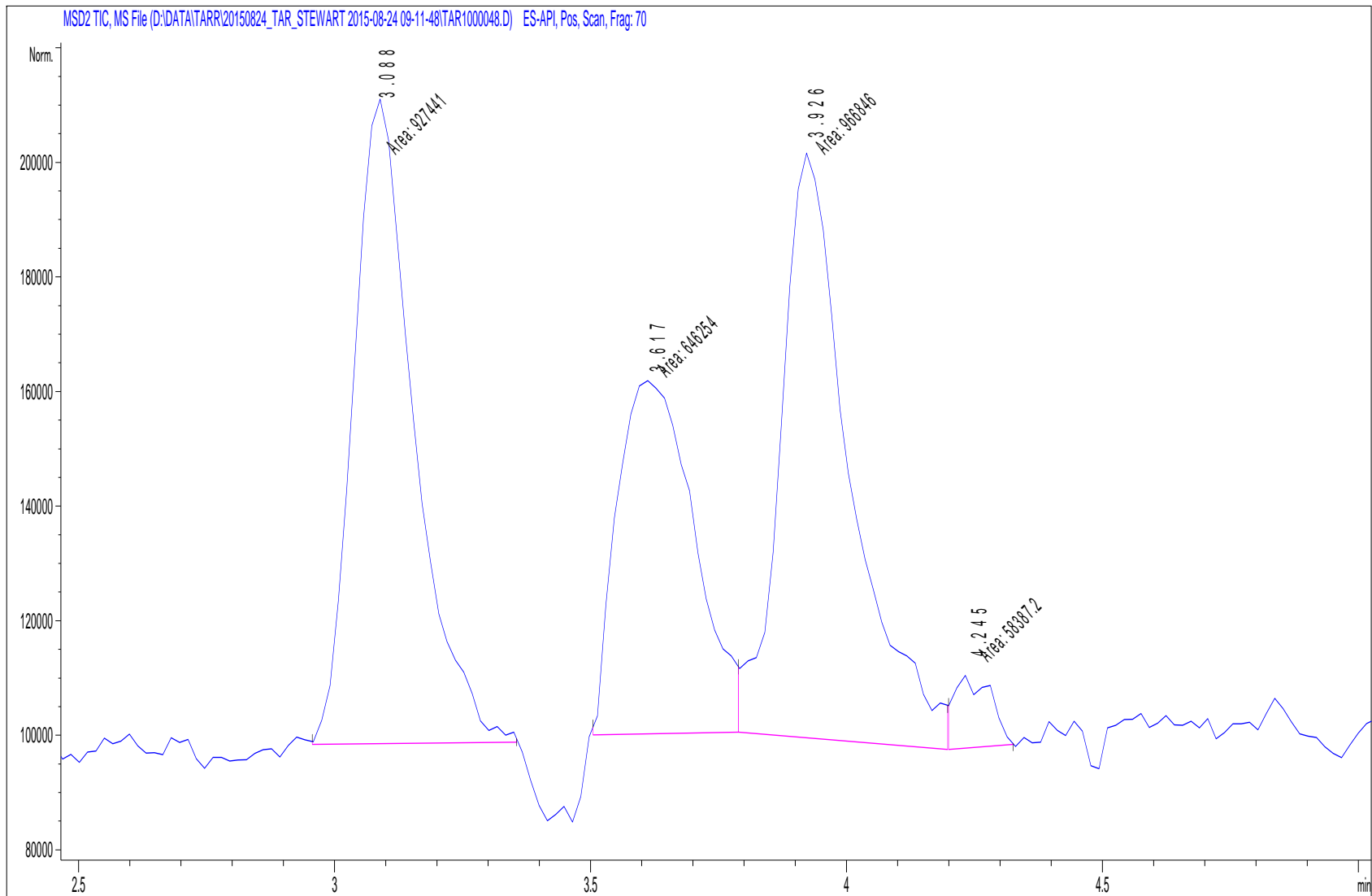
Max: 11028

13-Mar-15

5 DC

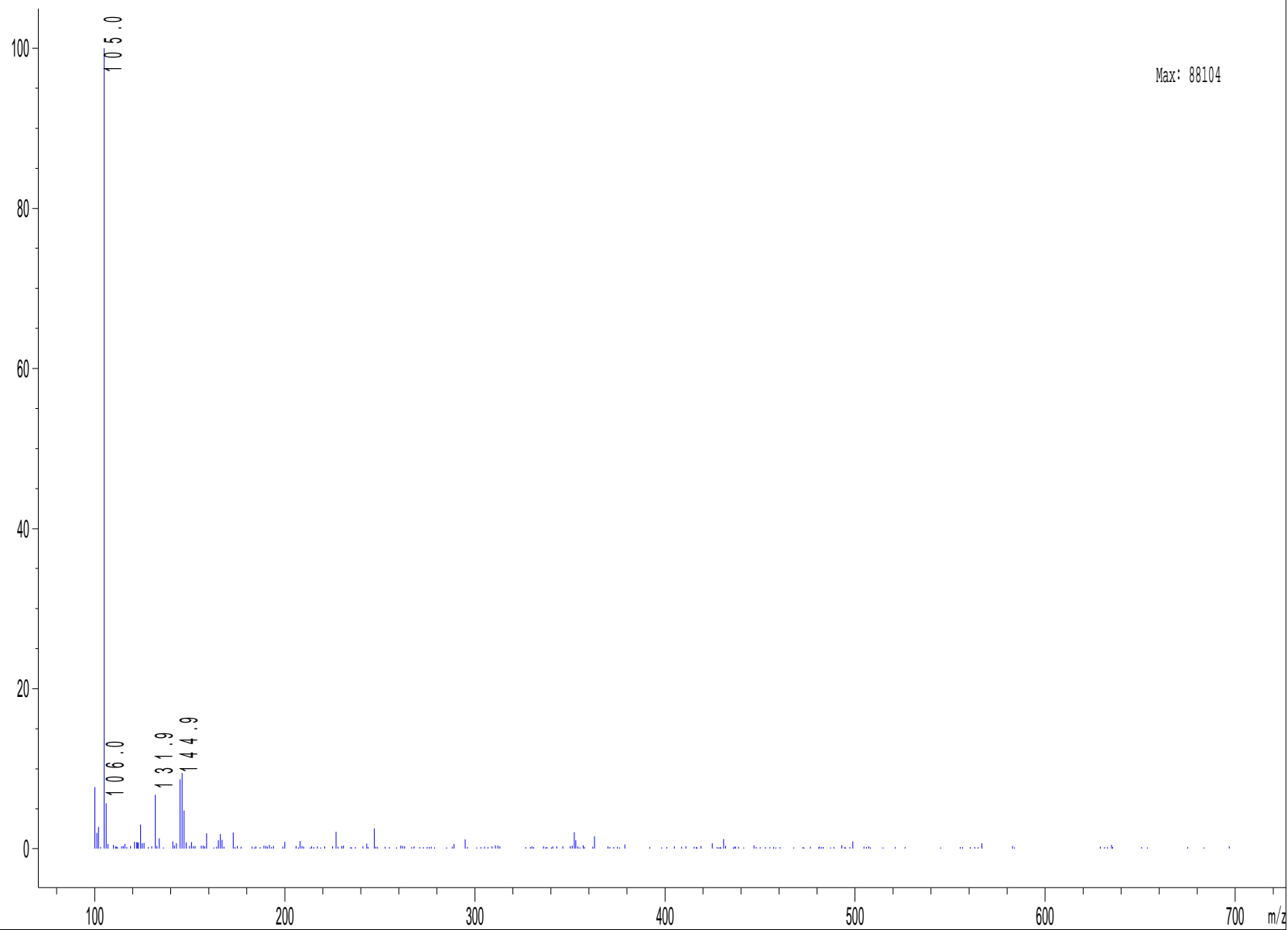
P2-A-03



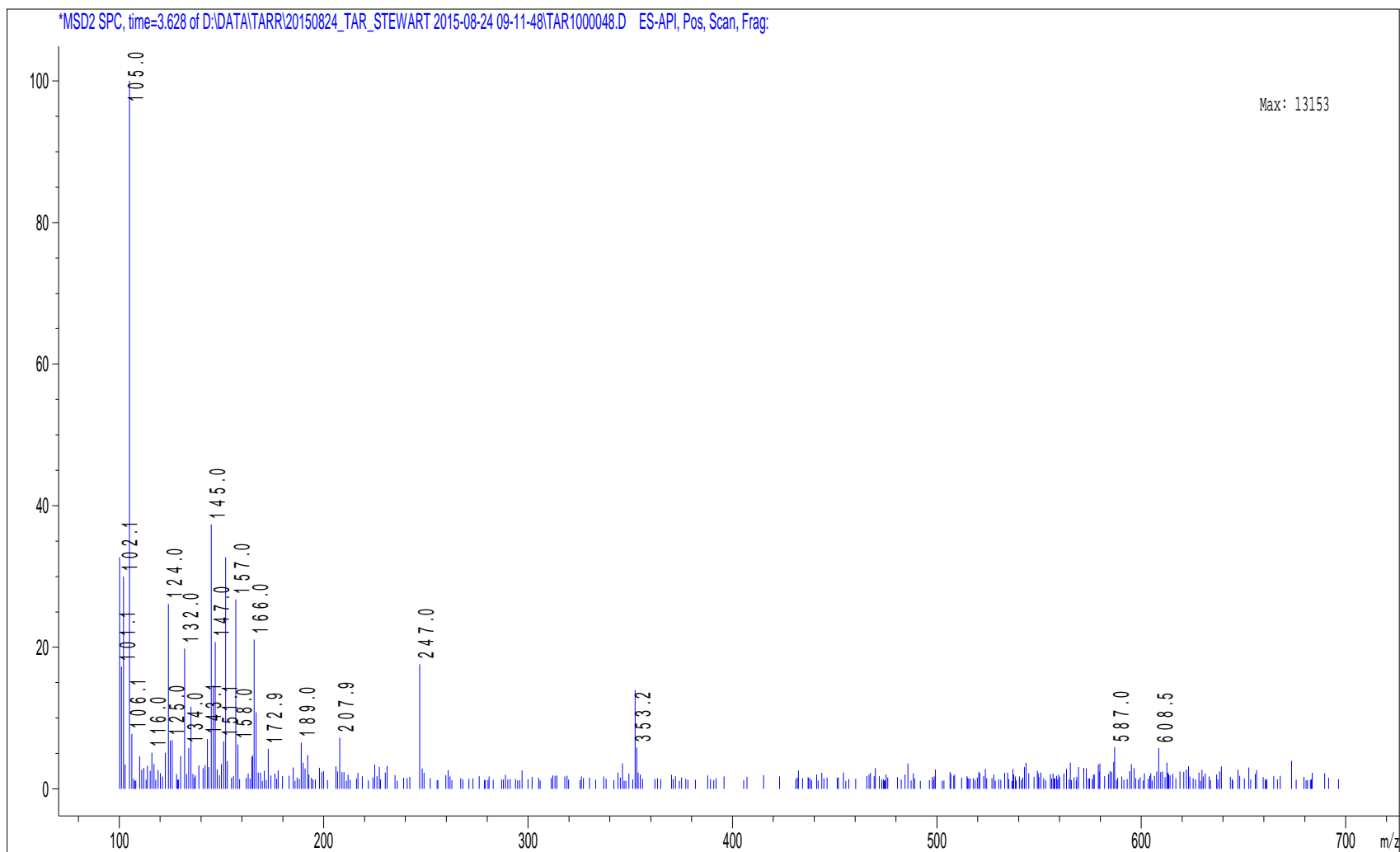


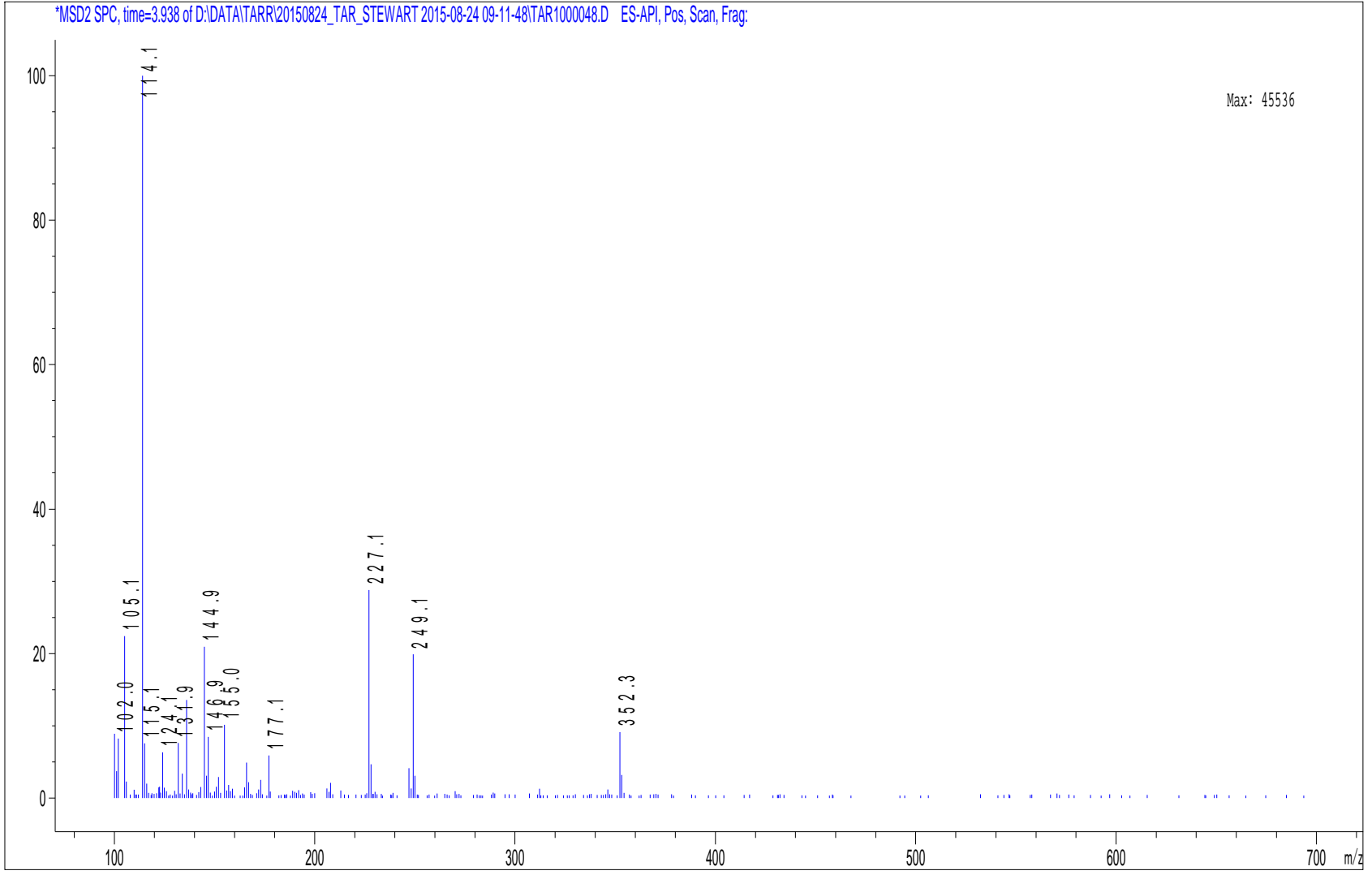


\*MSD2 SPC, time=3.106 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09:11:48\TAR1000048.D ES-API, Pos, Scan, Frag:

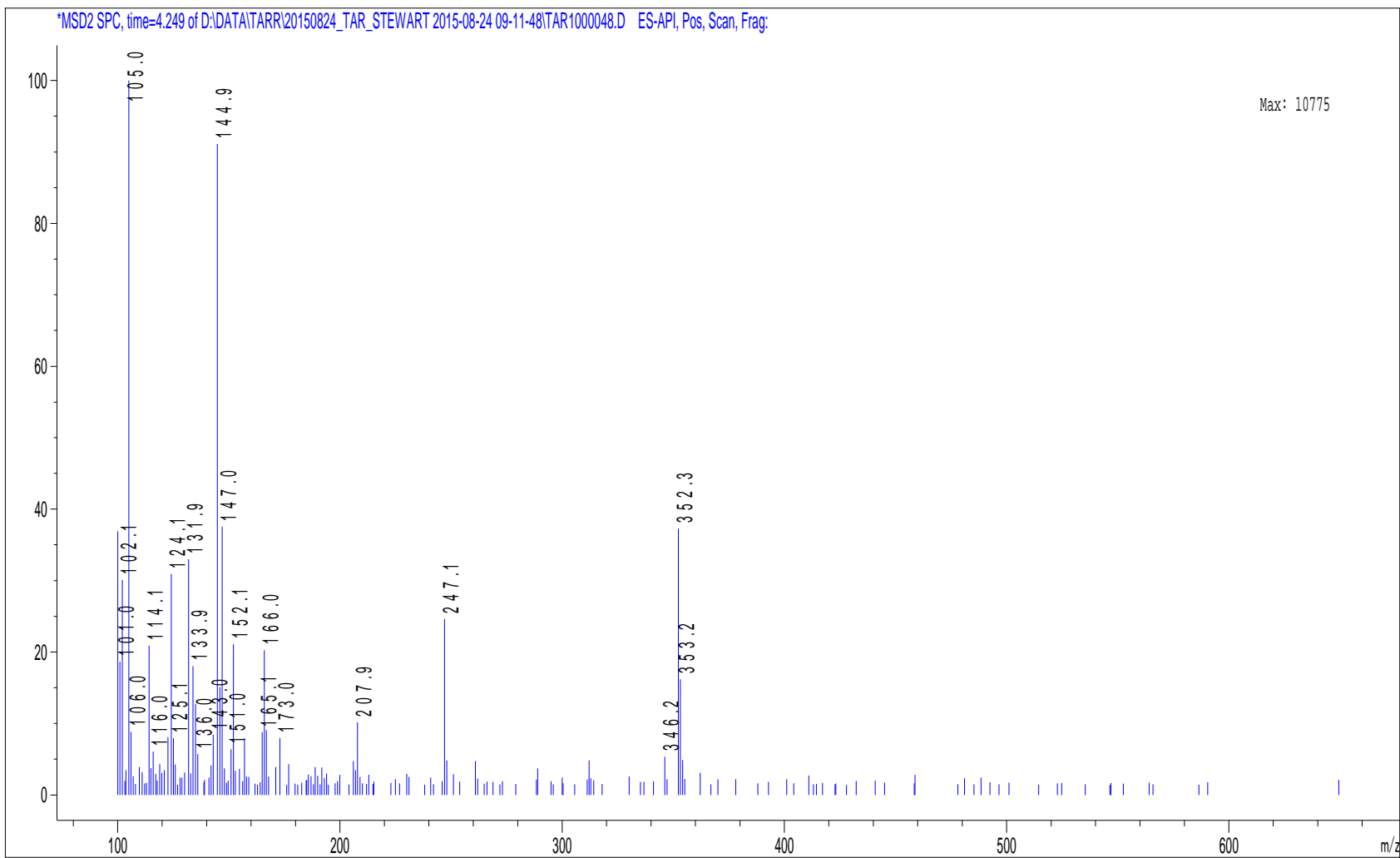


\*MSD2 SPC, time=3.628 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000048.D ES-API, Pos, Scan, Frag:





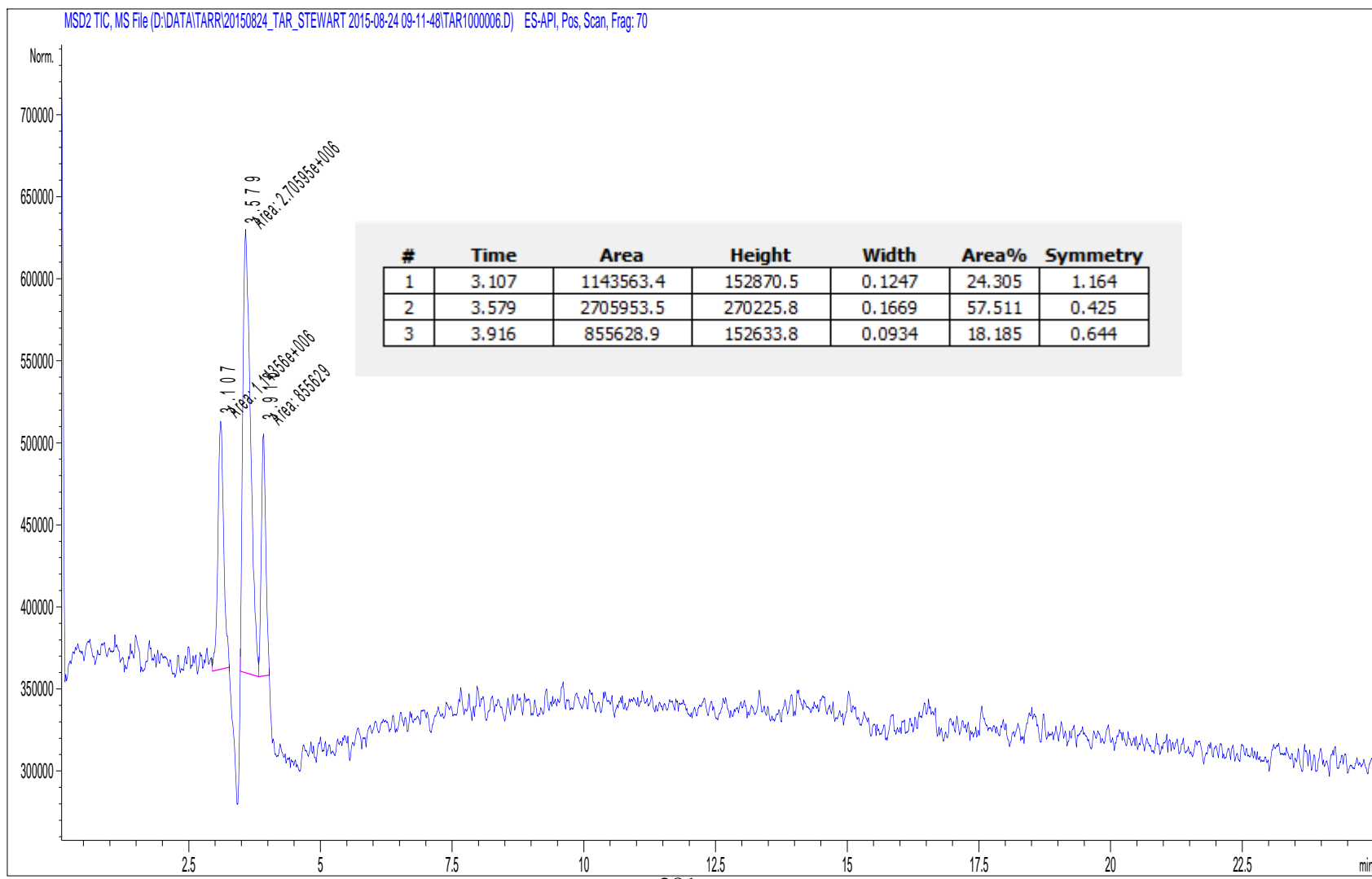
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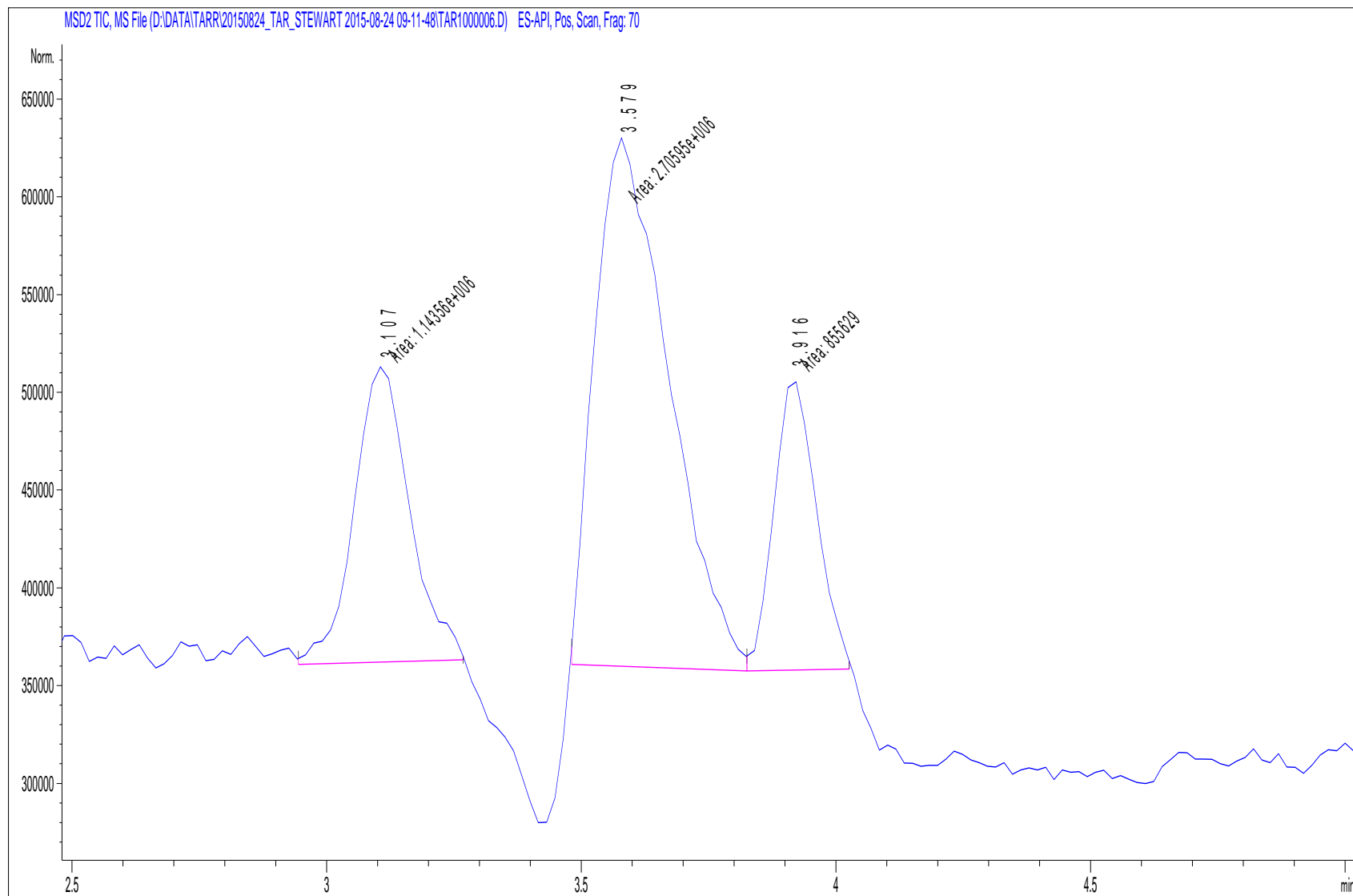


9-Apr-15

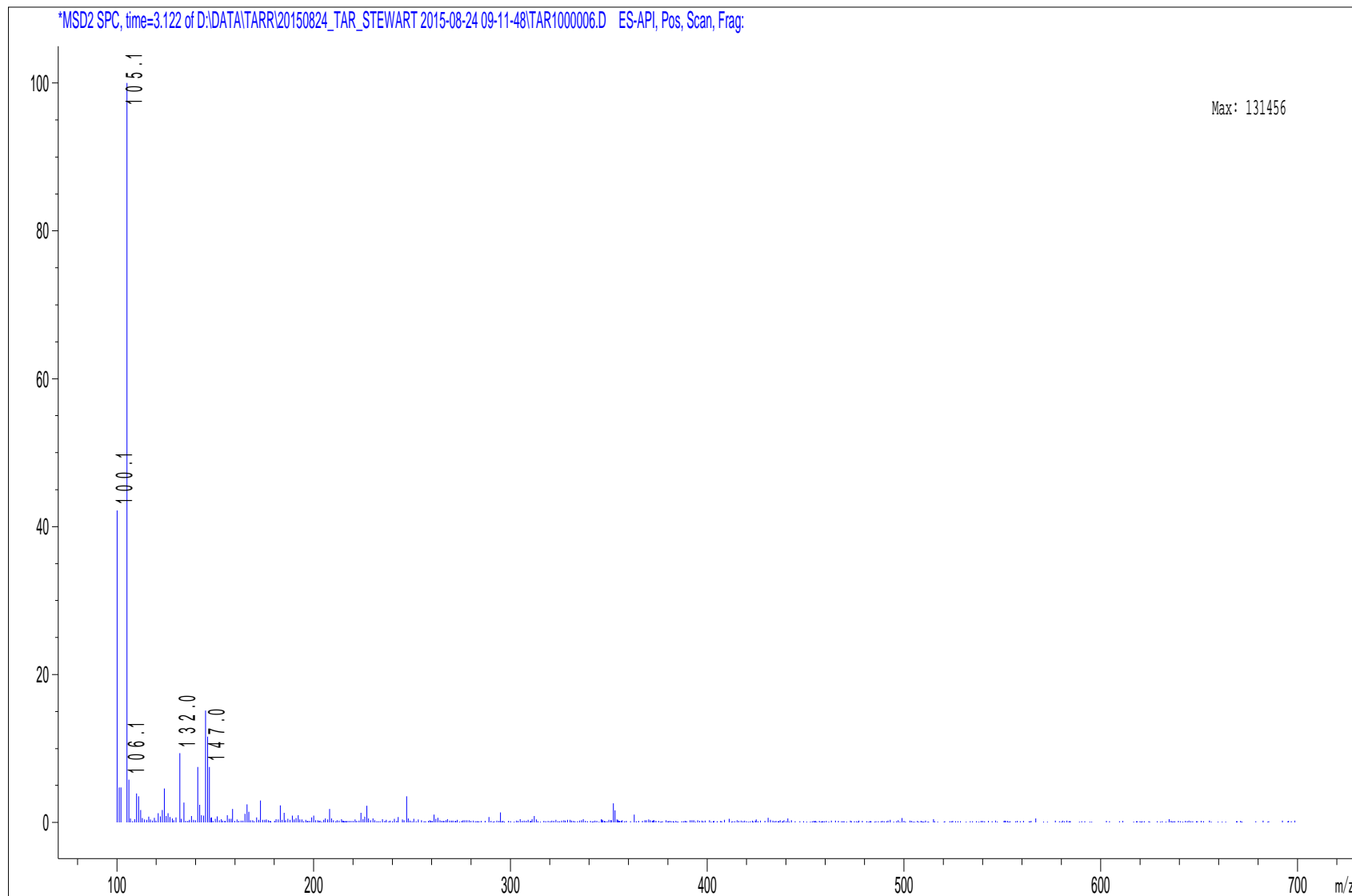
10 DC

P2-A-06

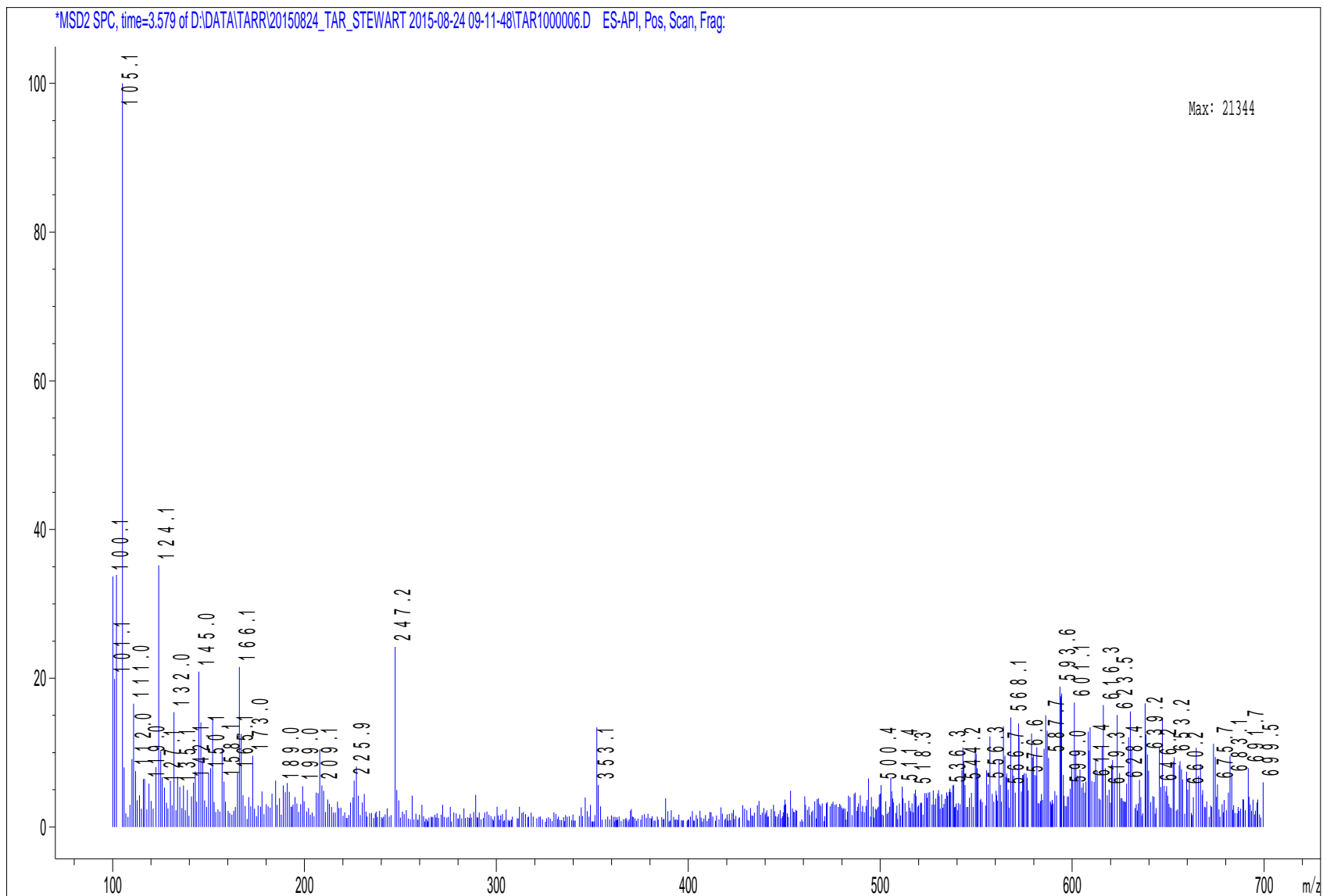




\*MSD2 SPC, time=3.122 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09:11-48\TAR1000006.D ES-API, Pos, Scan, Frag:

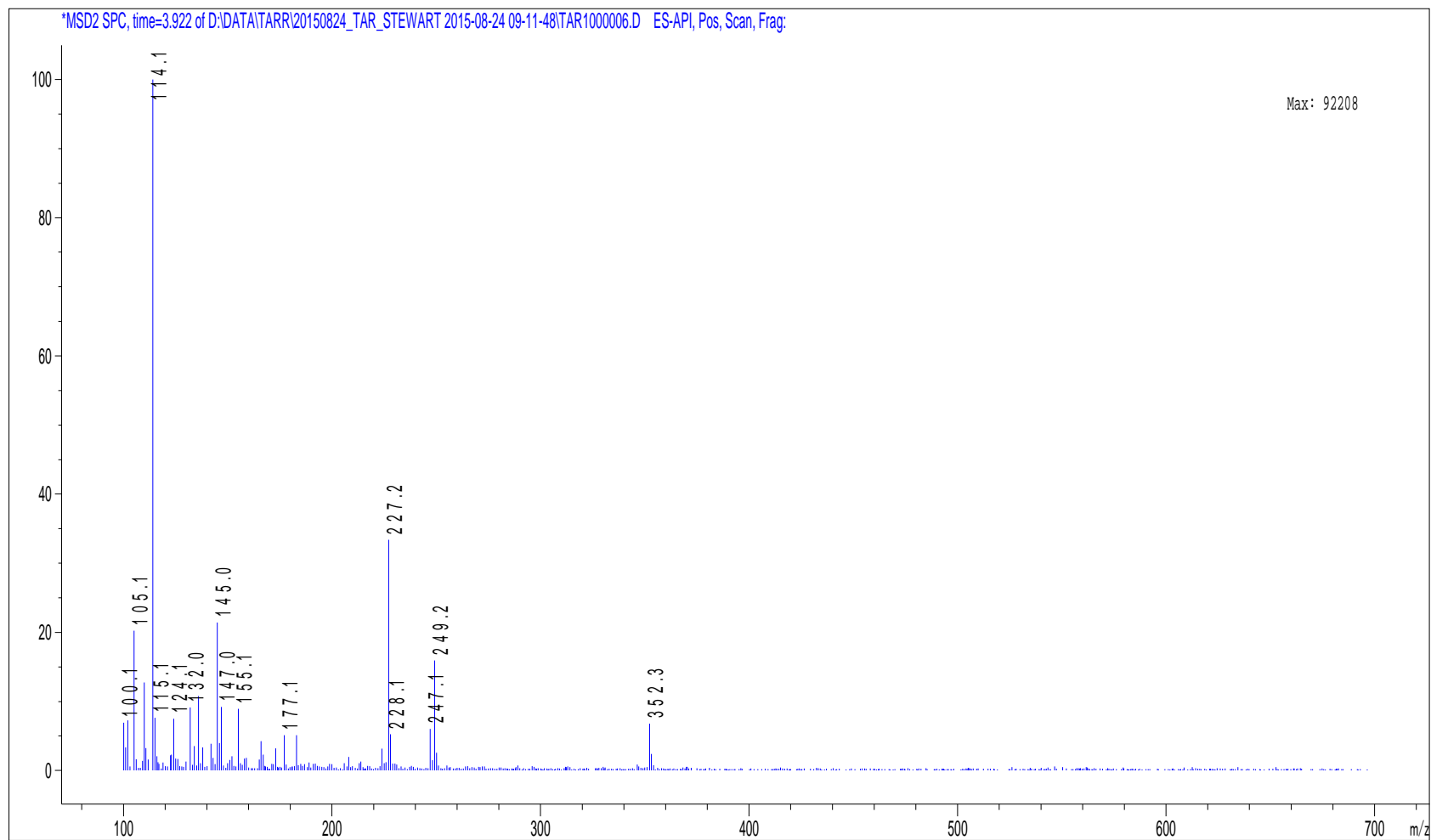


\*MSD2 SPC, time=3.579 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09:11-48\TAR1000006.D ES-API, Pos, Scan, Frag:



Max: 21344

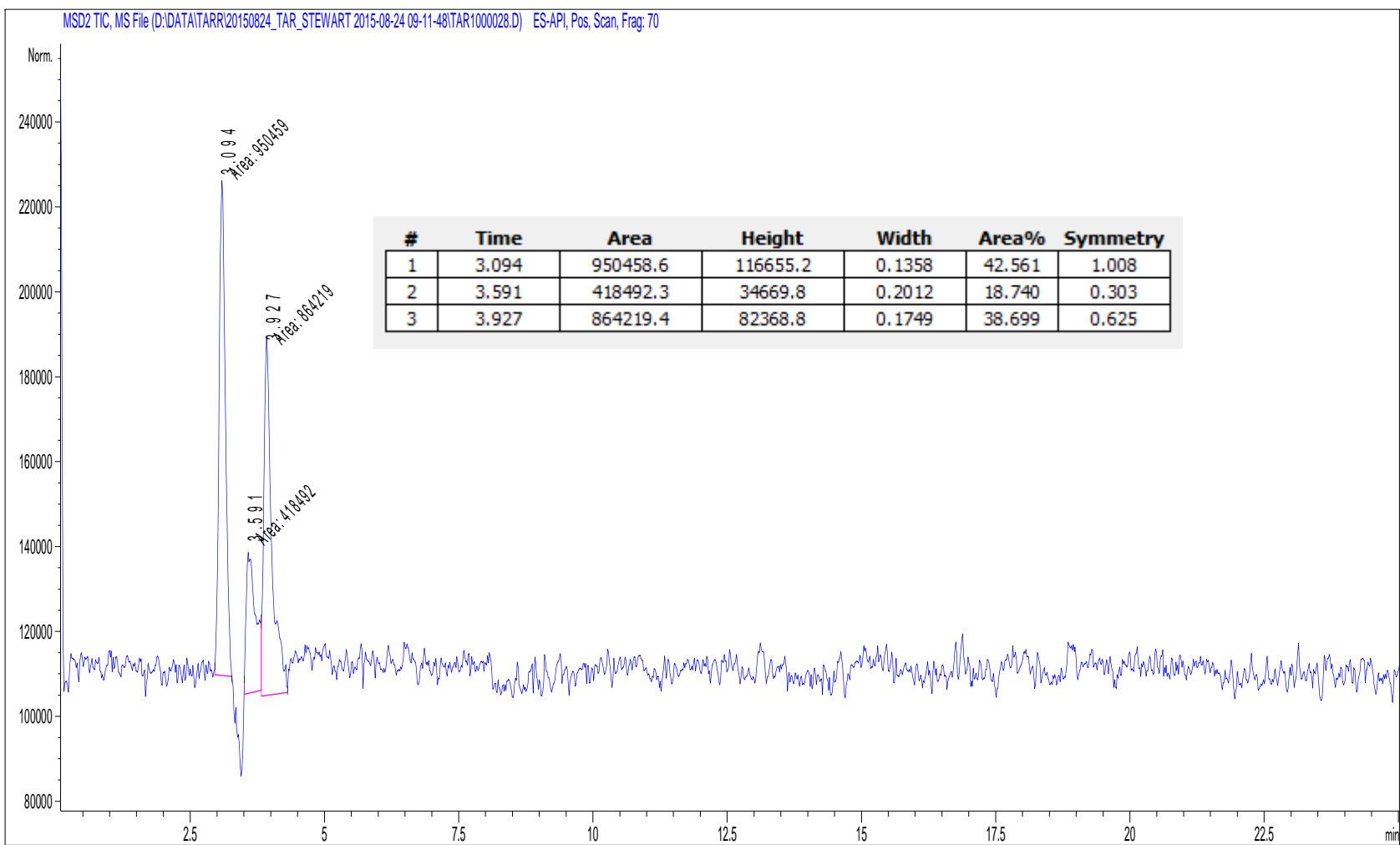


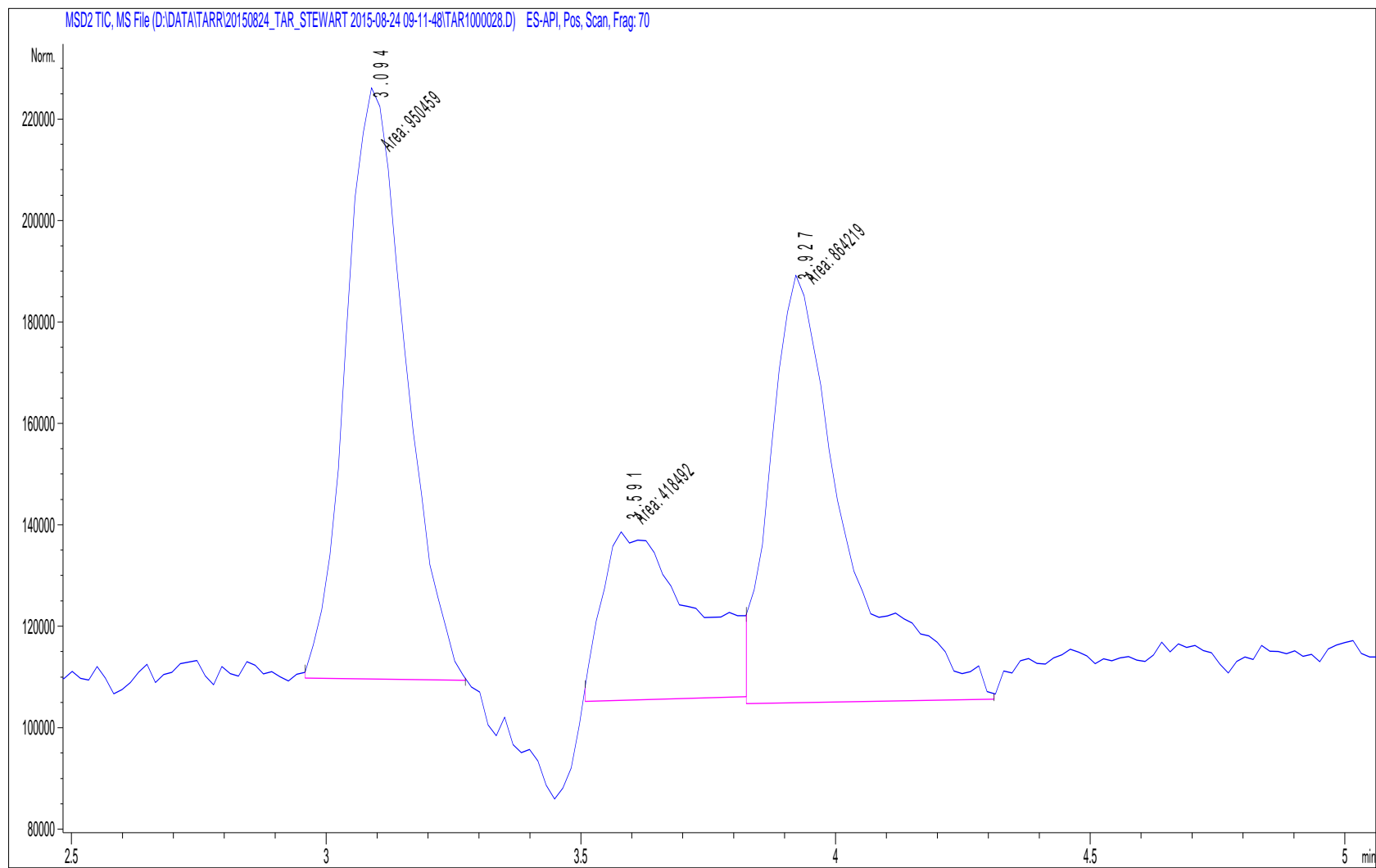


6-Aug-15

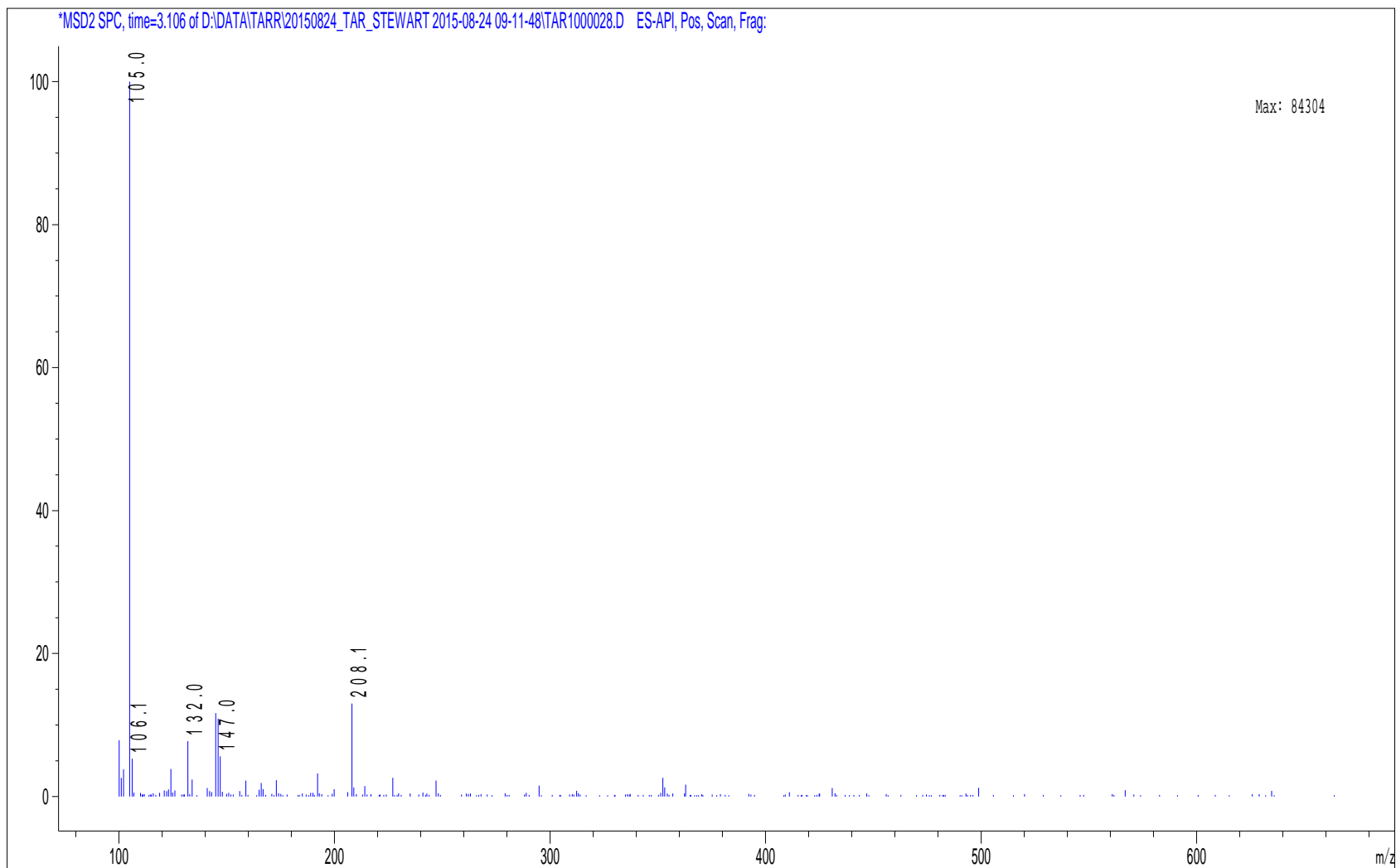
20 DC

P2-D-09

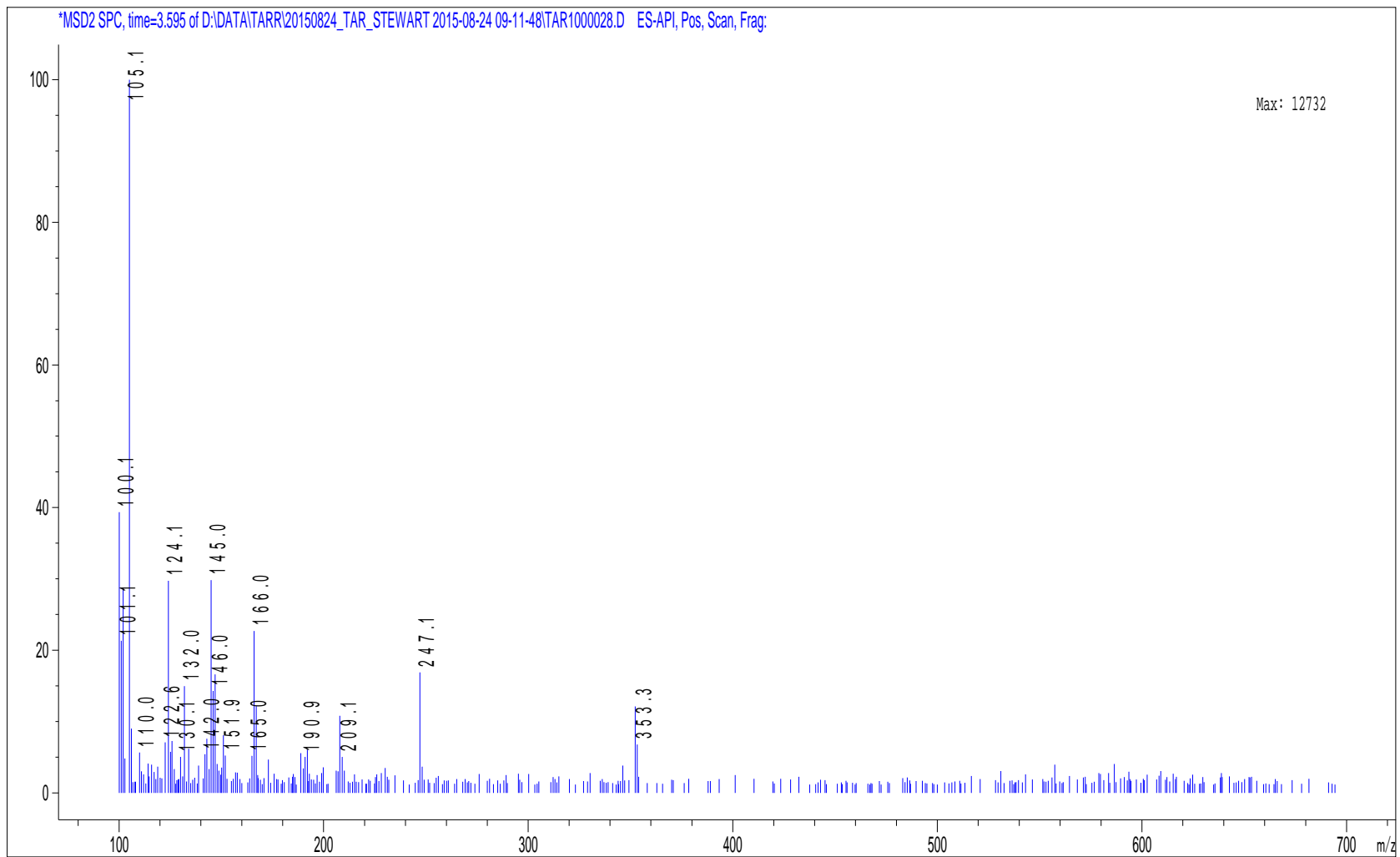




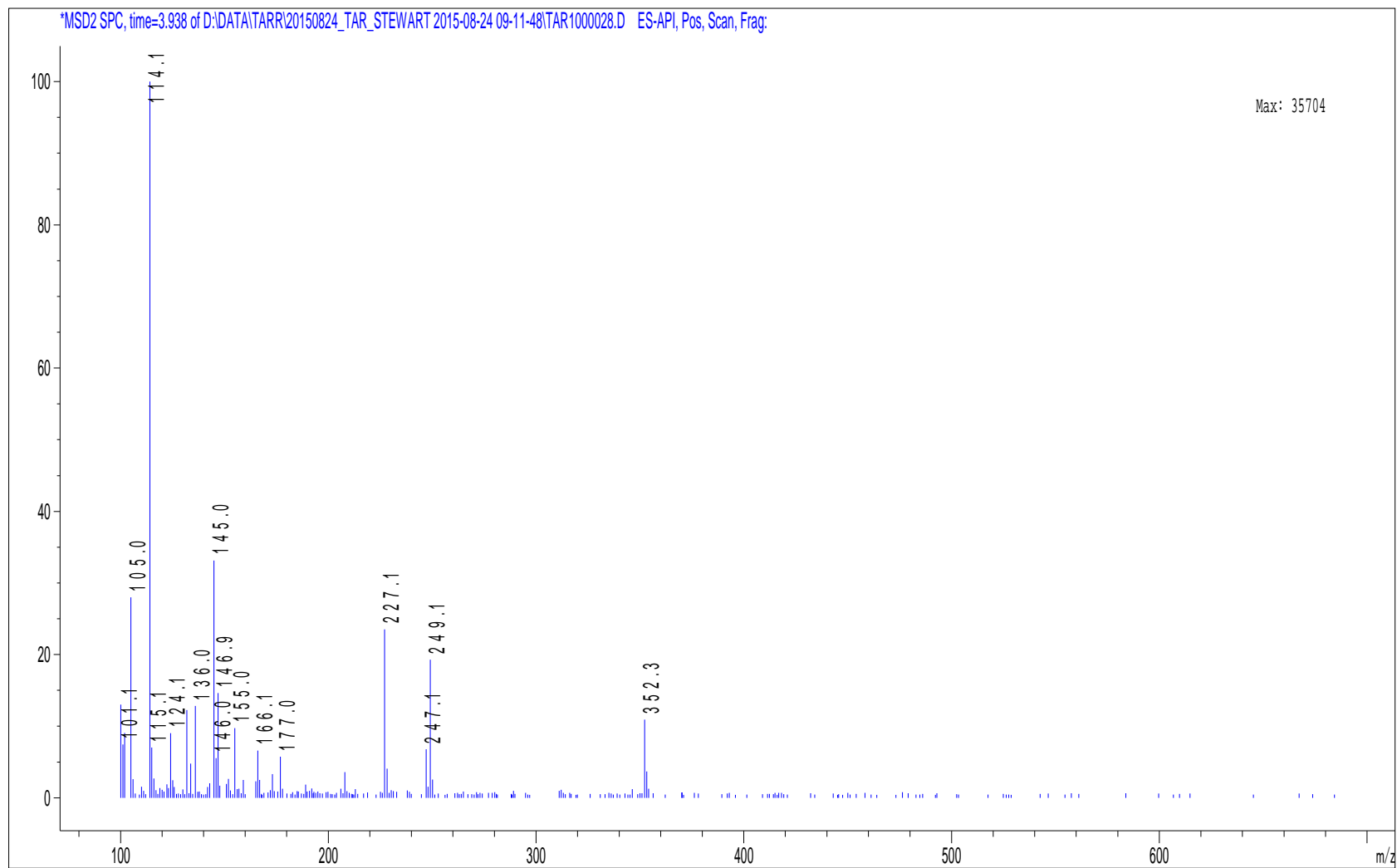
\*MSD2 SPC, time=3.106 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000028.D ES-API, Pos, Scan, Frag:



\*MSD2 SPC, time=3.595 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000028.D ES-API, Pos, Scan, Frag:



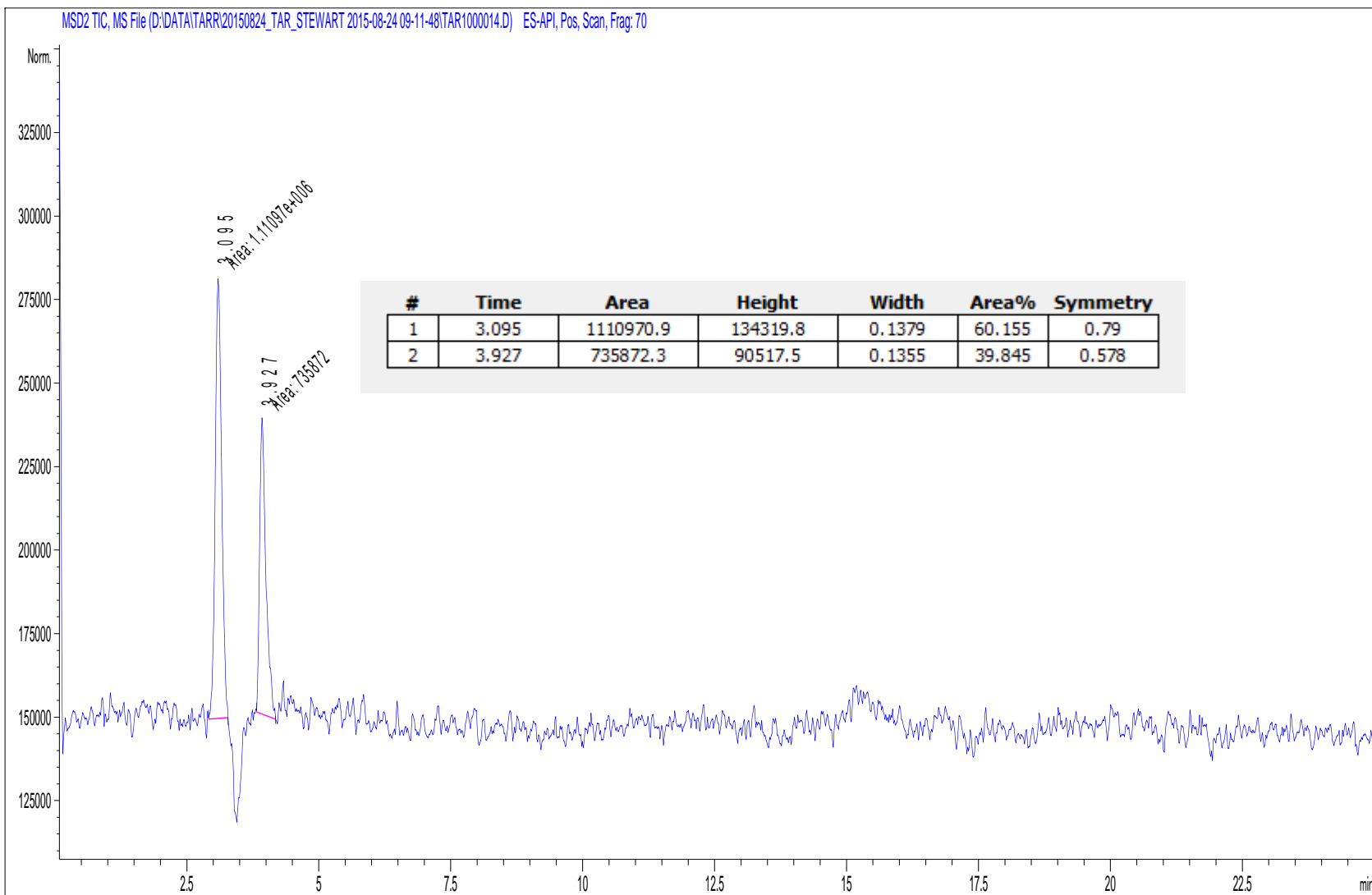
\*MSD2 SPC, time=3.938 of D:\DATA\ARRI\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000028.D ES-API, Pos, Scan, Frag:

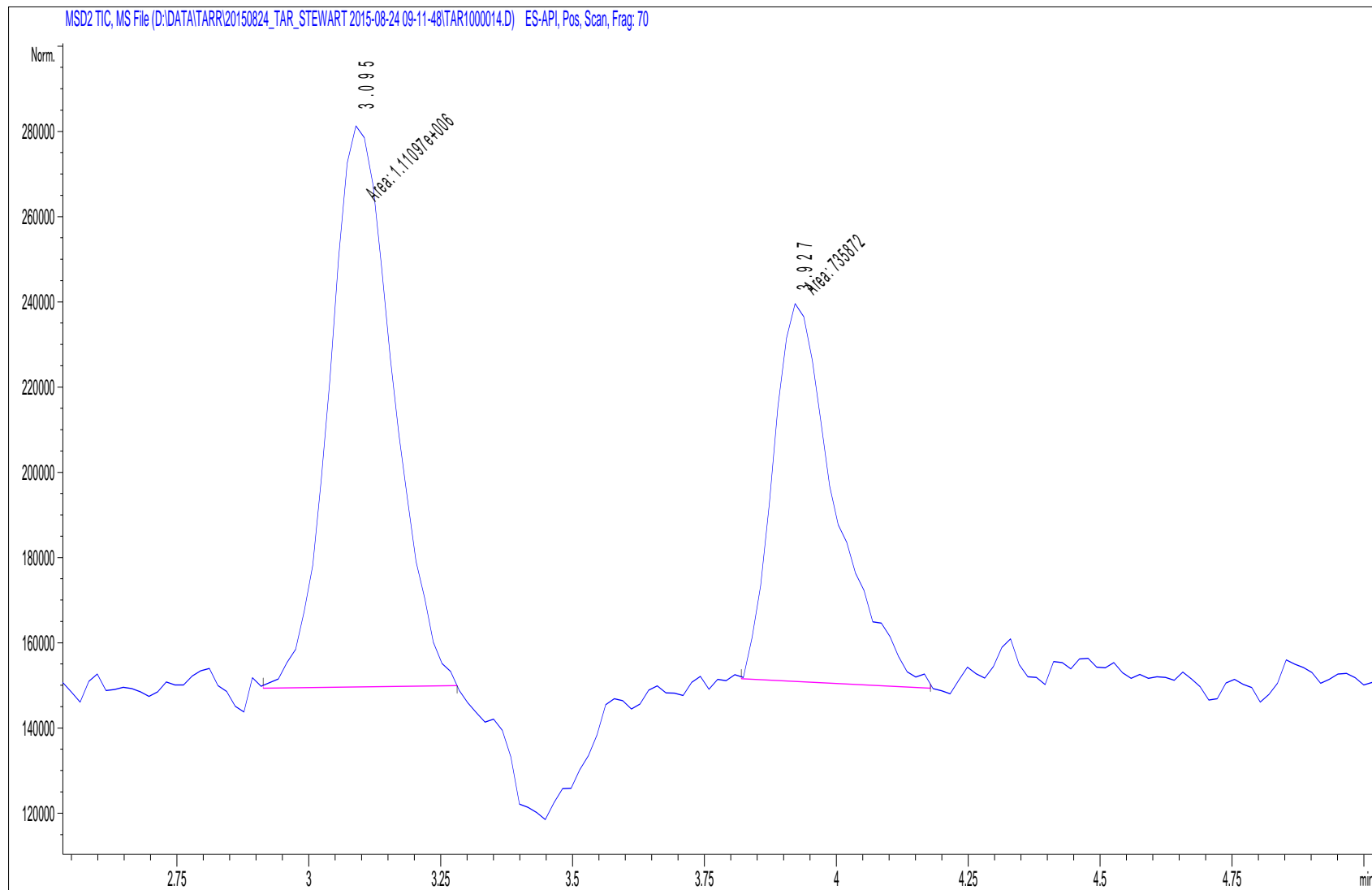


3-Jun-15

30 DC

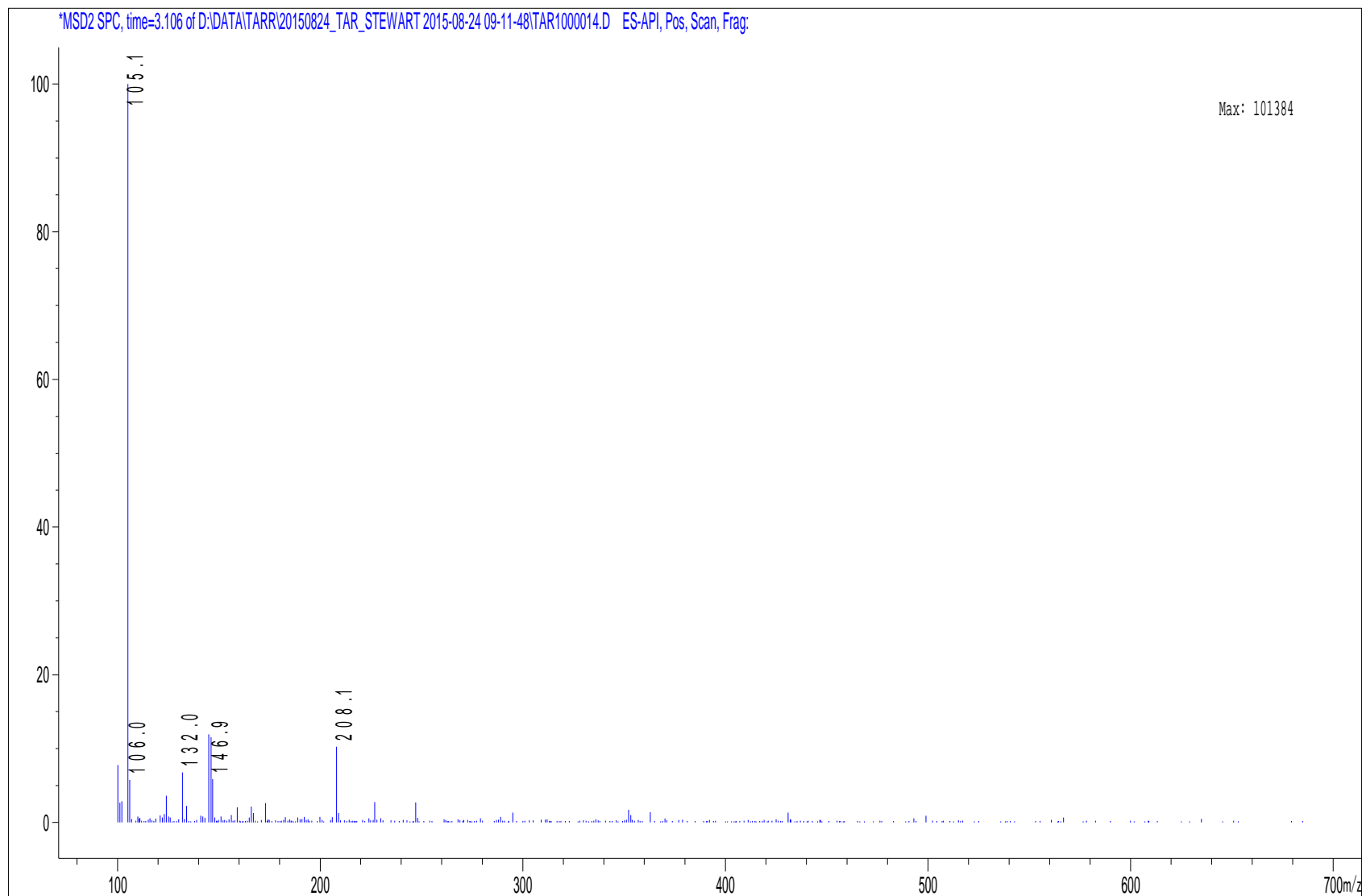
P2-B-05



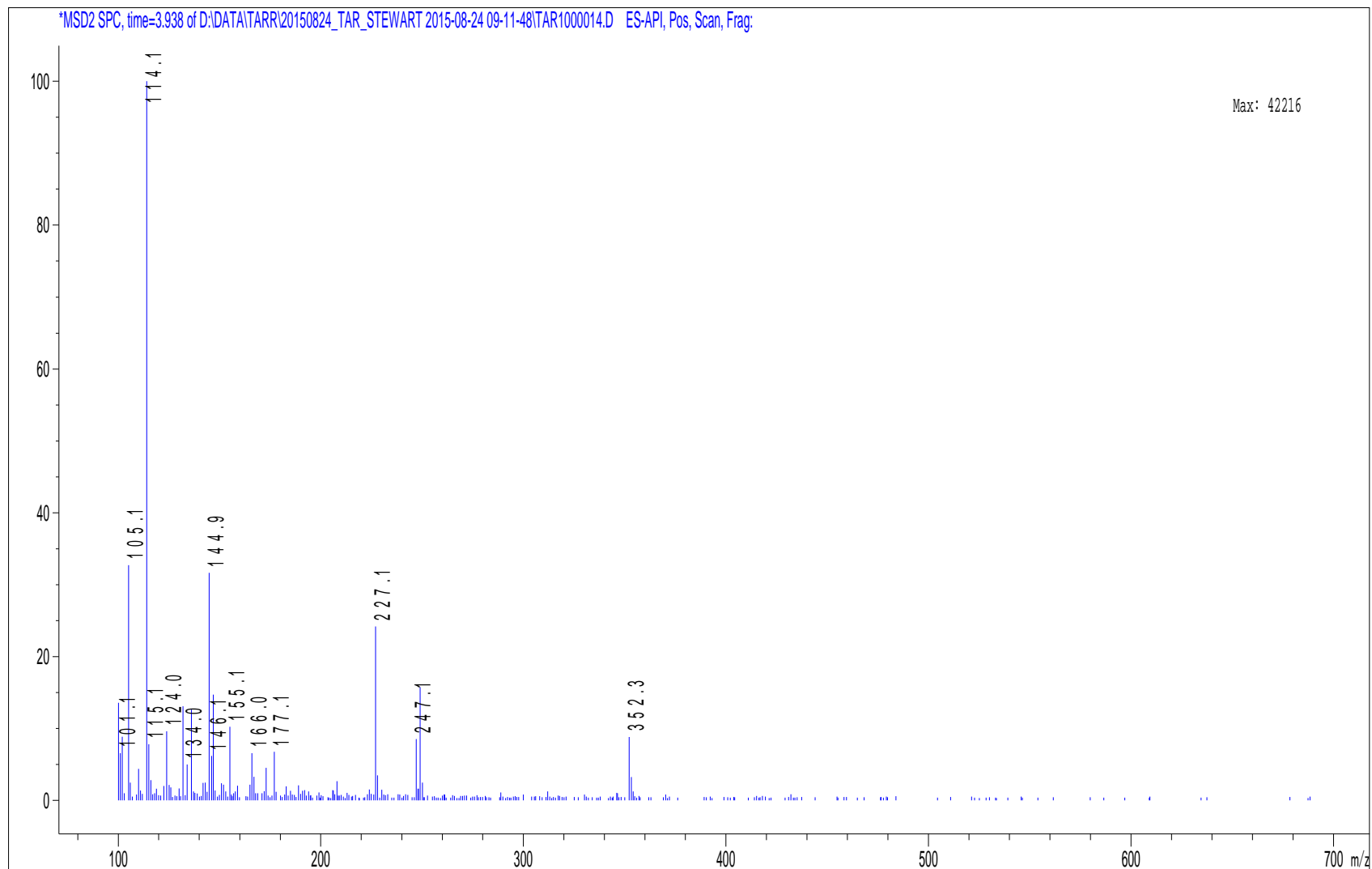




\*MSD2 SPC, time=3.106 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09:11:48\TAR1000014.D ES-API, Pos, Scan, Frag:



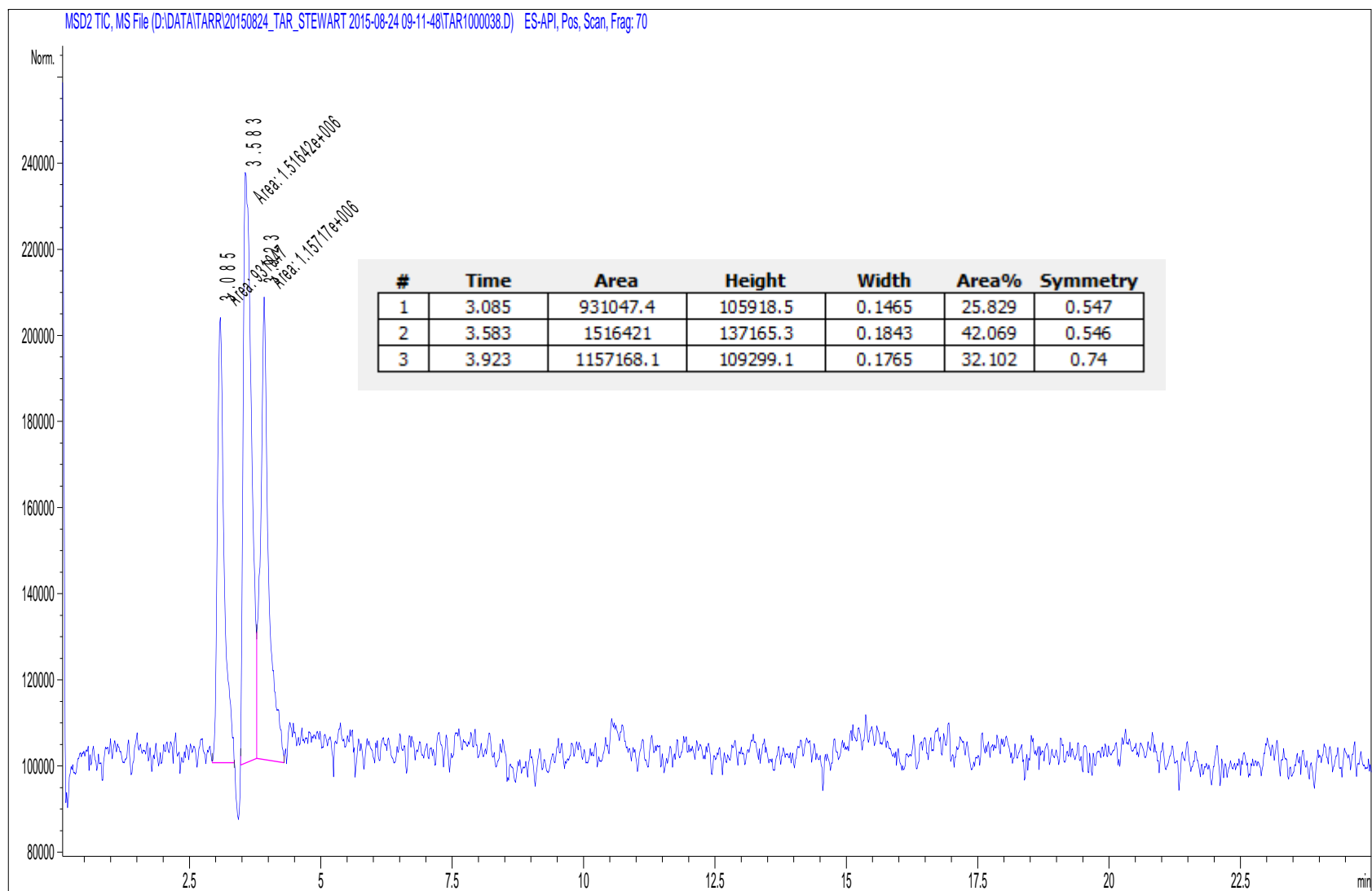
\*MSD2 SPC, time=3.938 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000014.D ES-API, Pos, Scan, Frag:

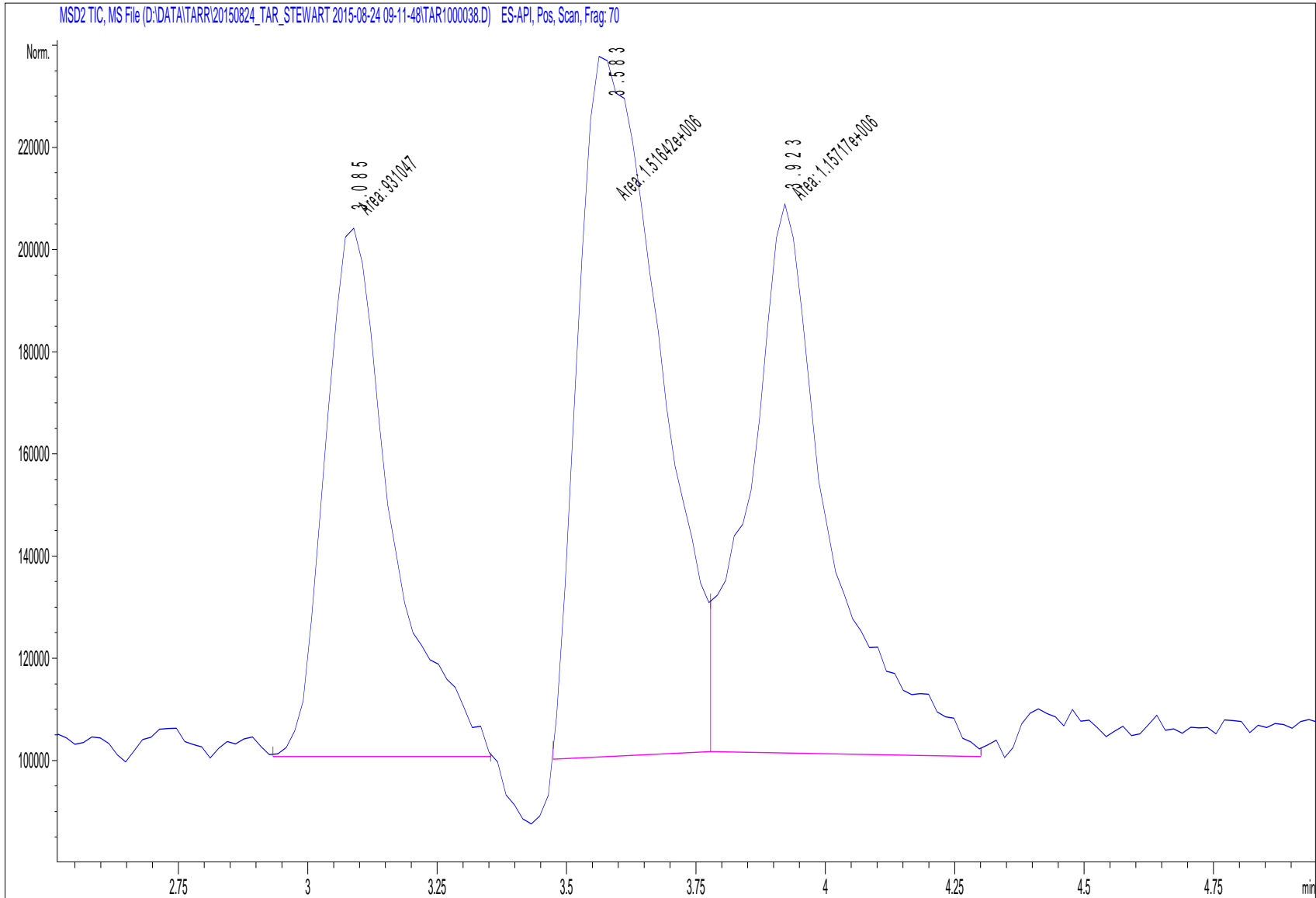


11-Aug-15

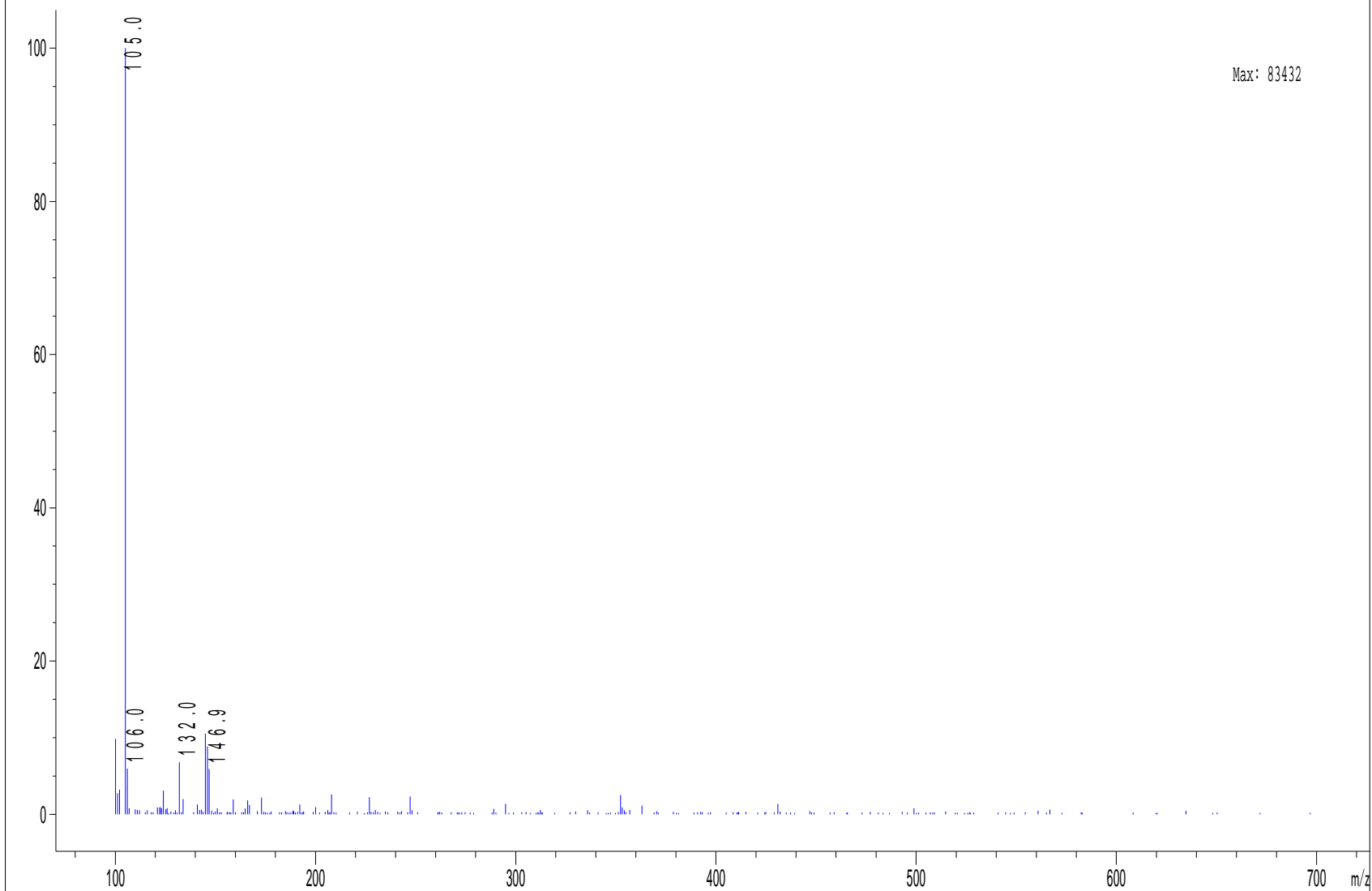
50 DC

P2-E-02

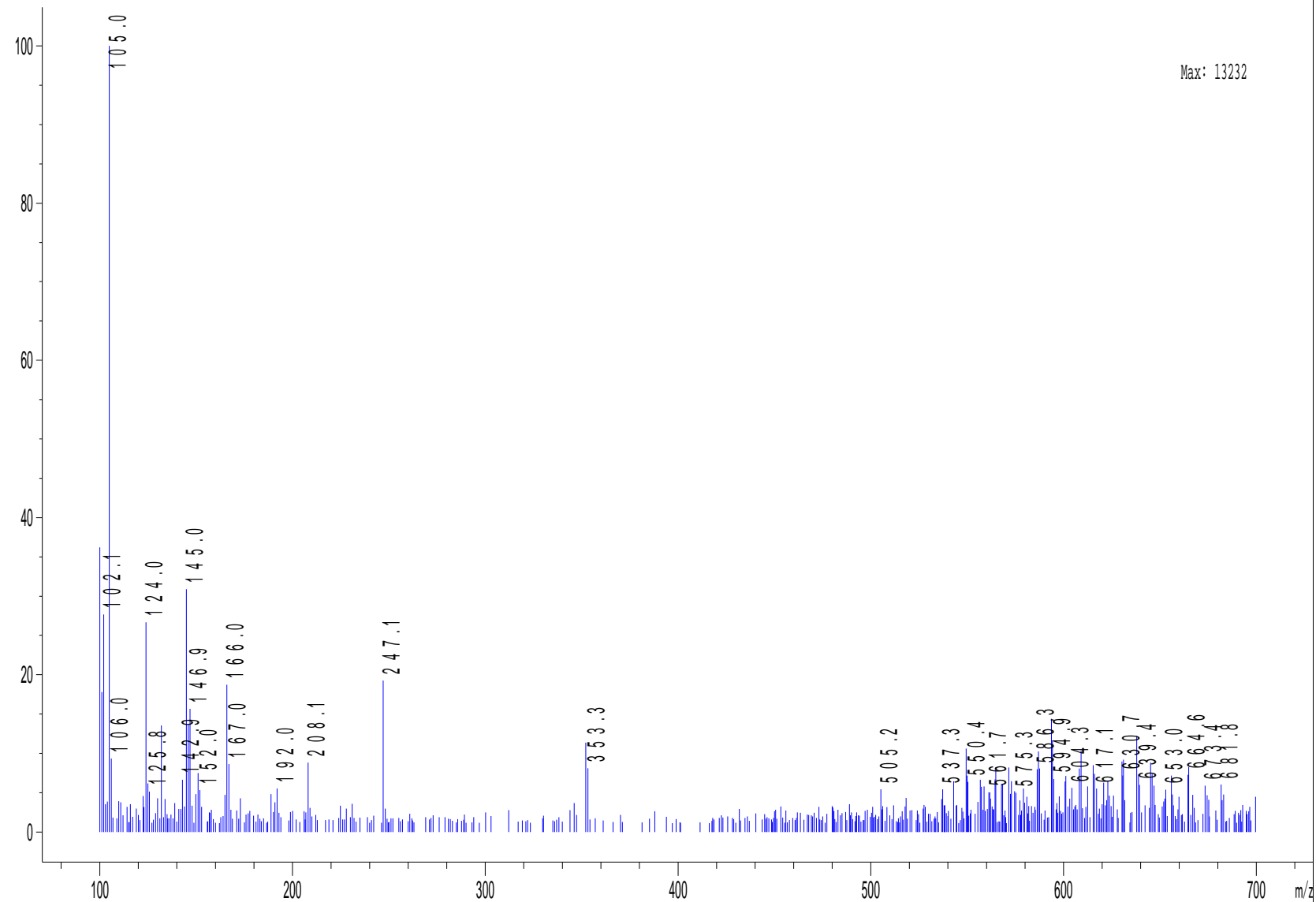




\*MSD2 SPC, time=3.089 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09:11:48\TAR1000038.D ES-API, Pos, Scan, Frag:

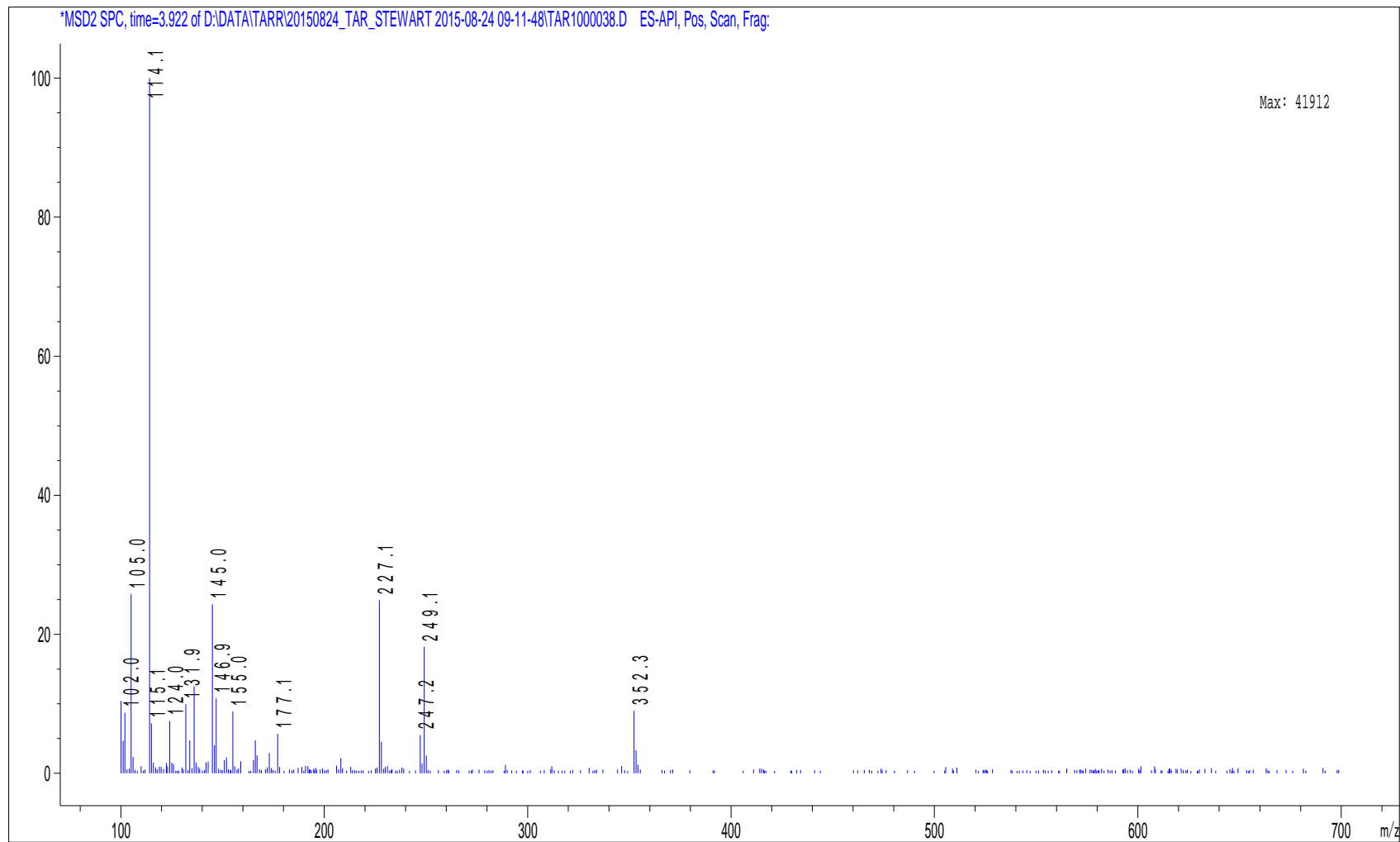


\*MSD2 SPC, time=3.595 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000038.D ES-API, Pos, Scan, Frag:



Max: 13232

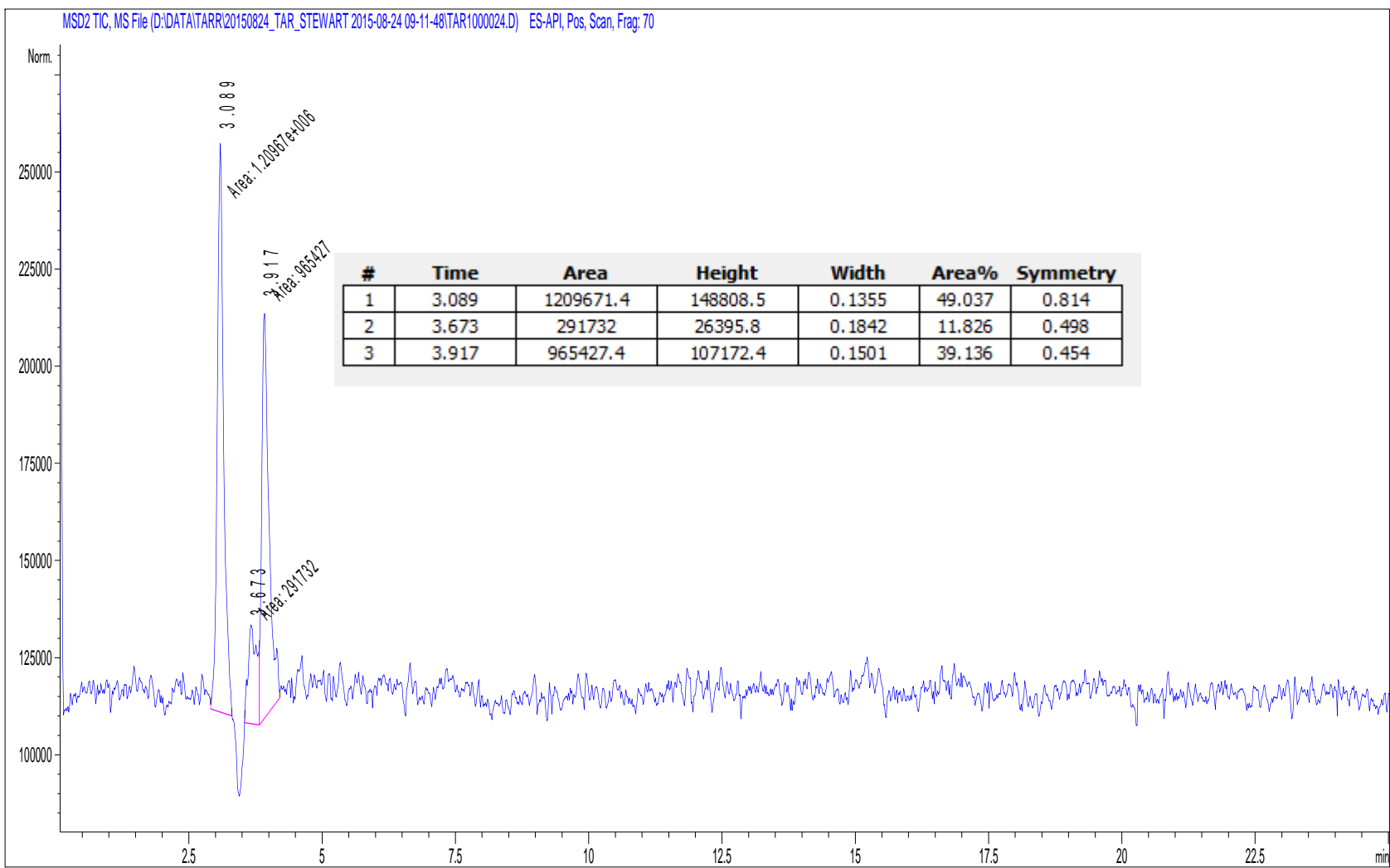
\*MSD2 SPC, time=3.922 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000038.D ES-API, Pos, Scan, Frag:



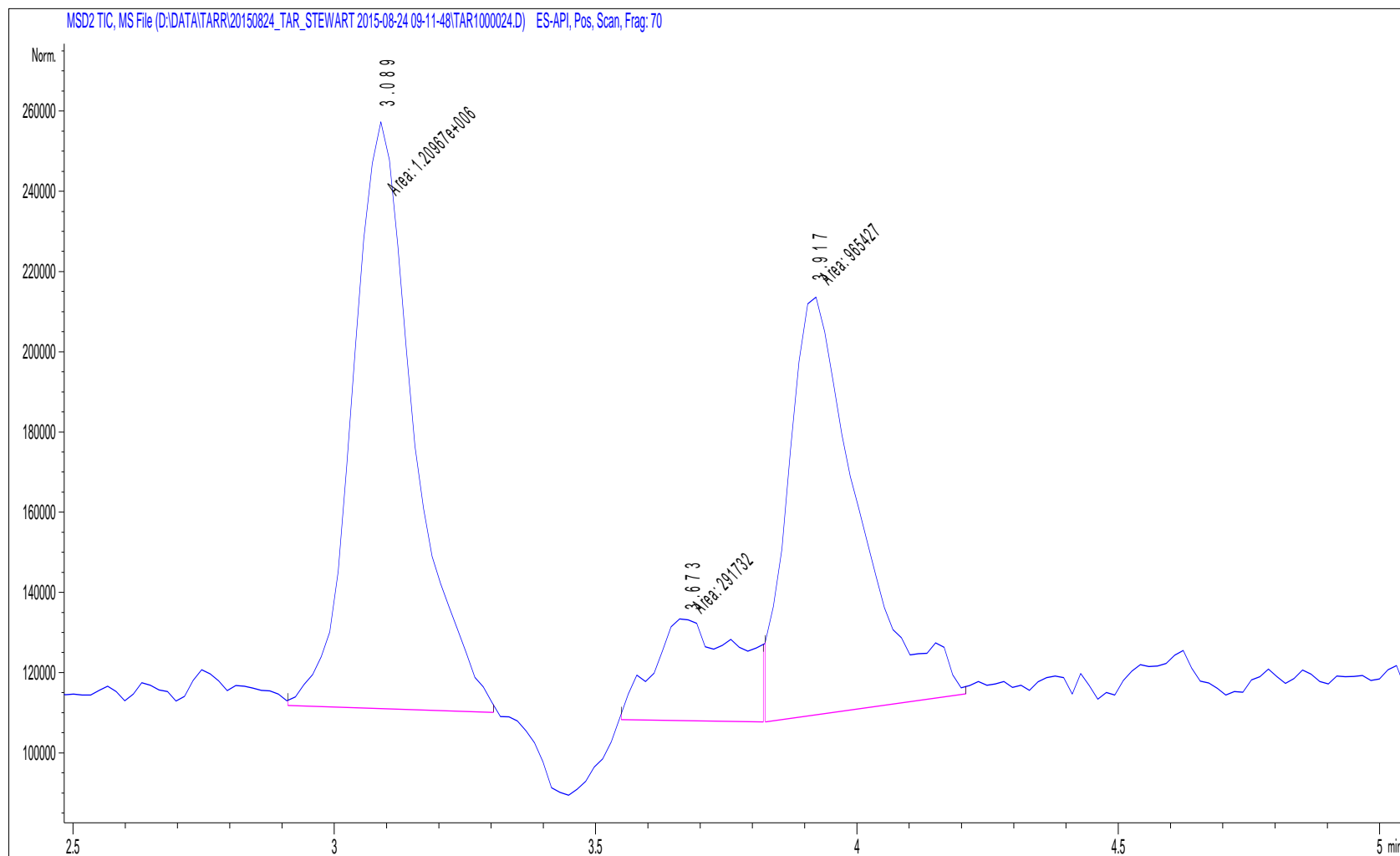
13-Jul-15

70 DC

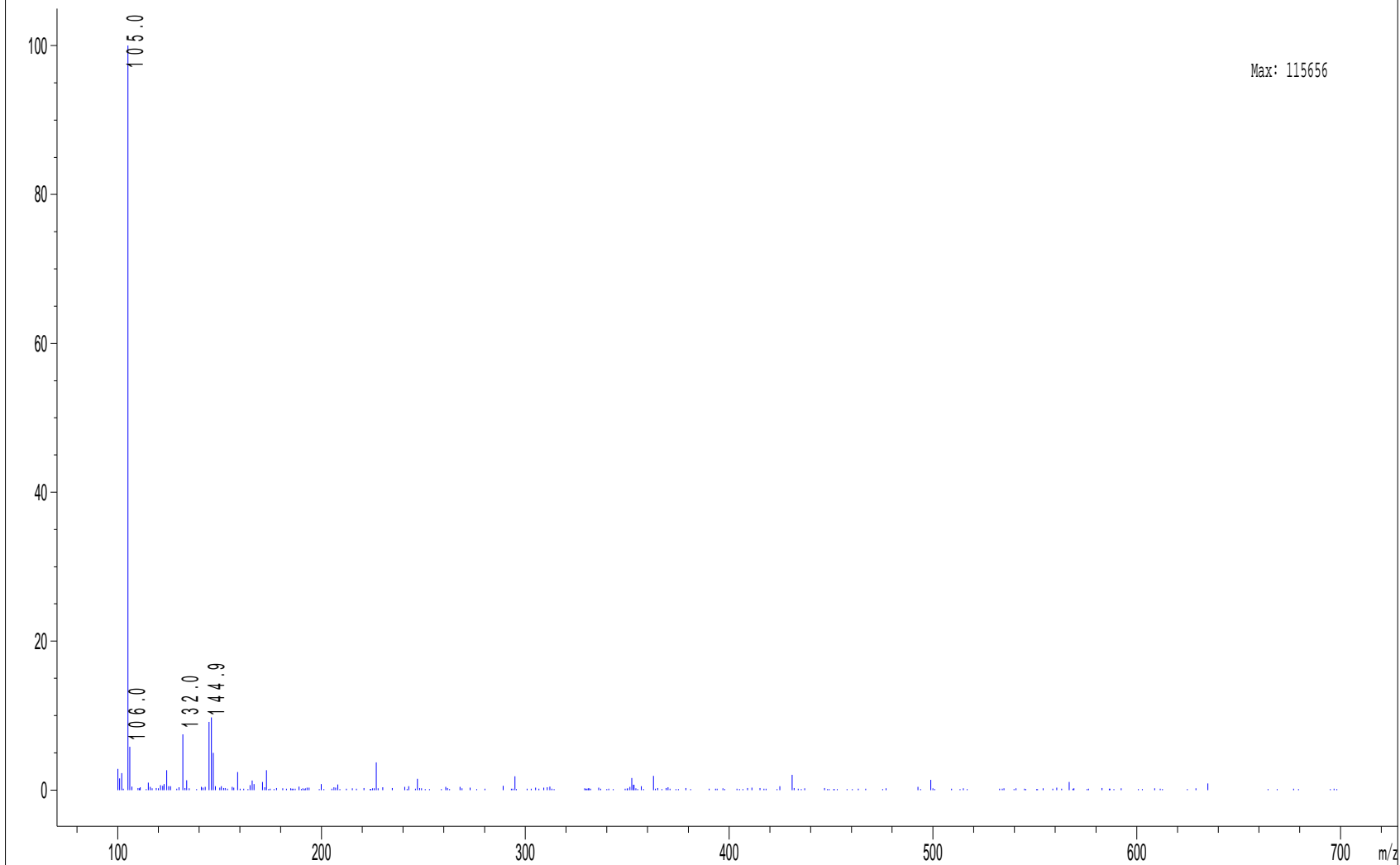
P2-C-06



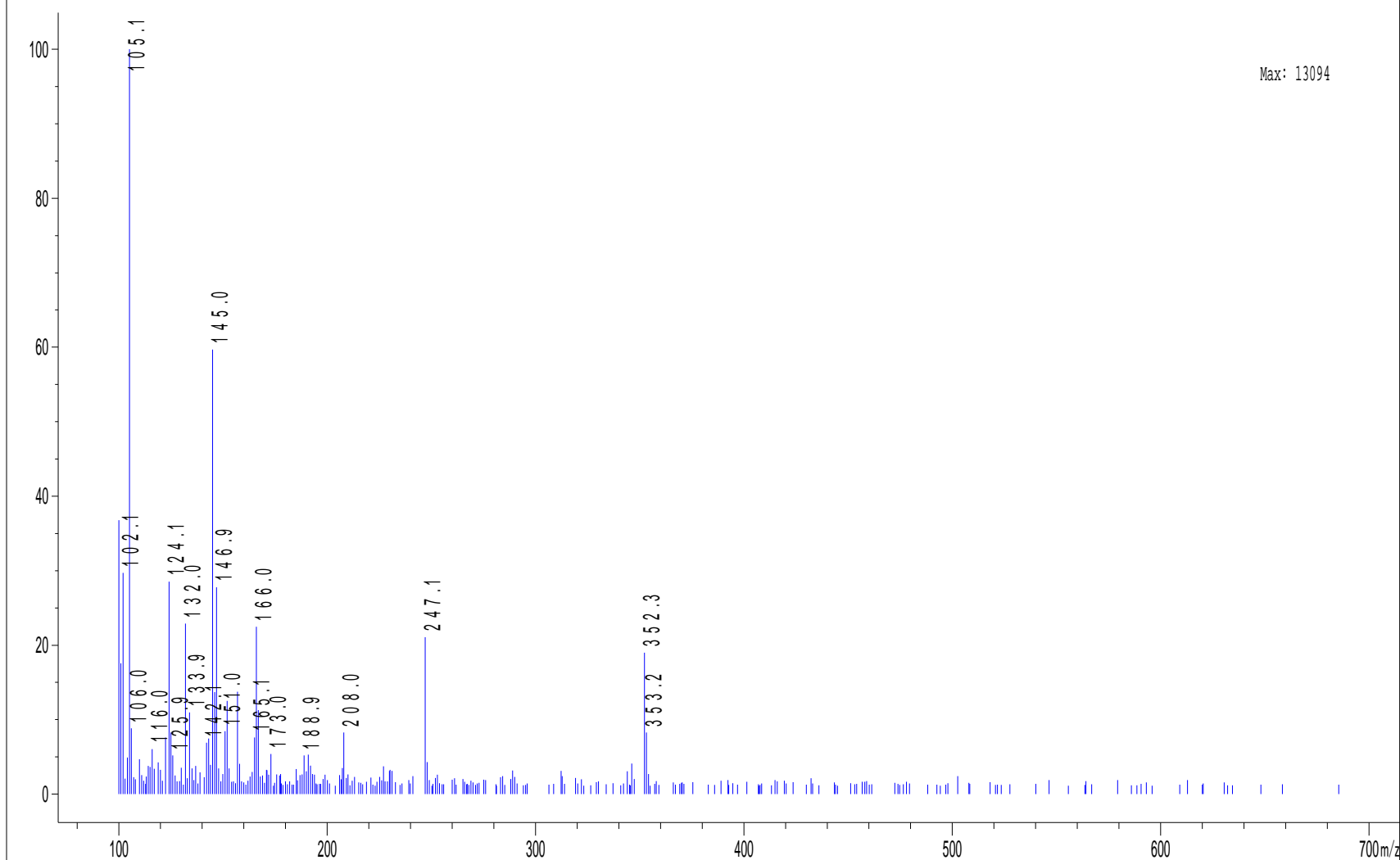




\*MSD2 SPC, time=3.089 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09:11:48\TAR1000024.D ES-API, Pos, Scan, Frag:

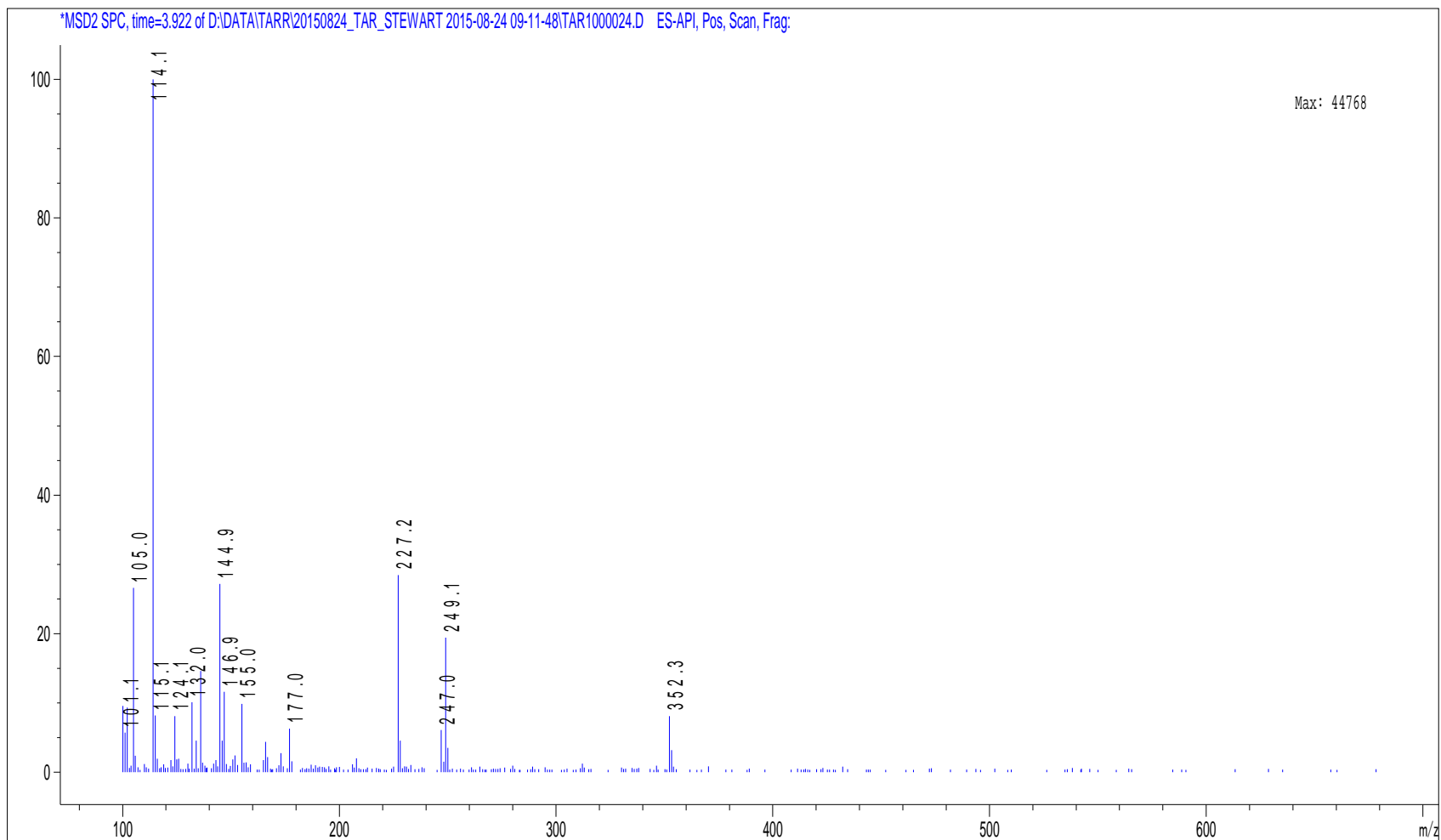


\*MSD2 SPC, time=3.677 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000024.D ES-API, Pos, Scan, Frag:



Max: 13094

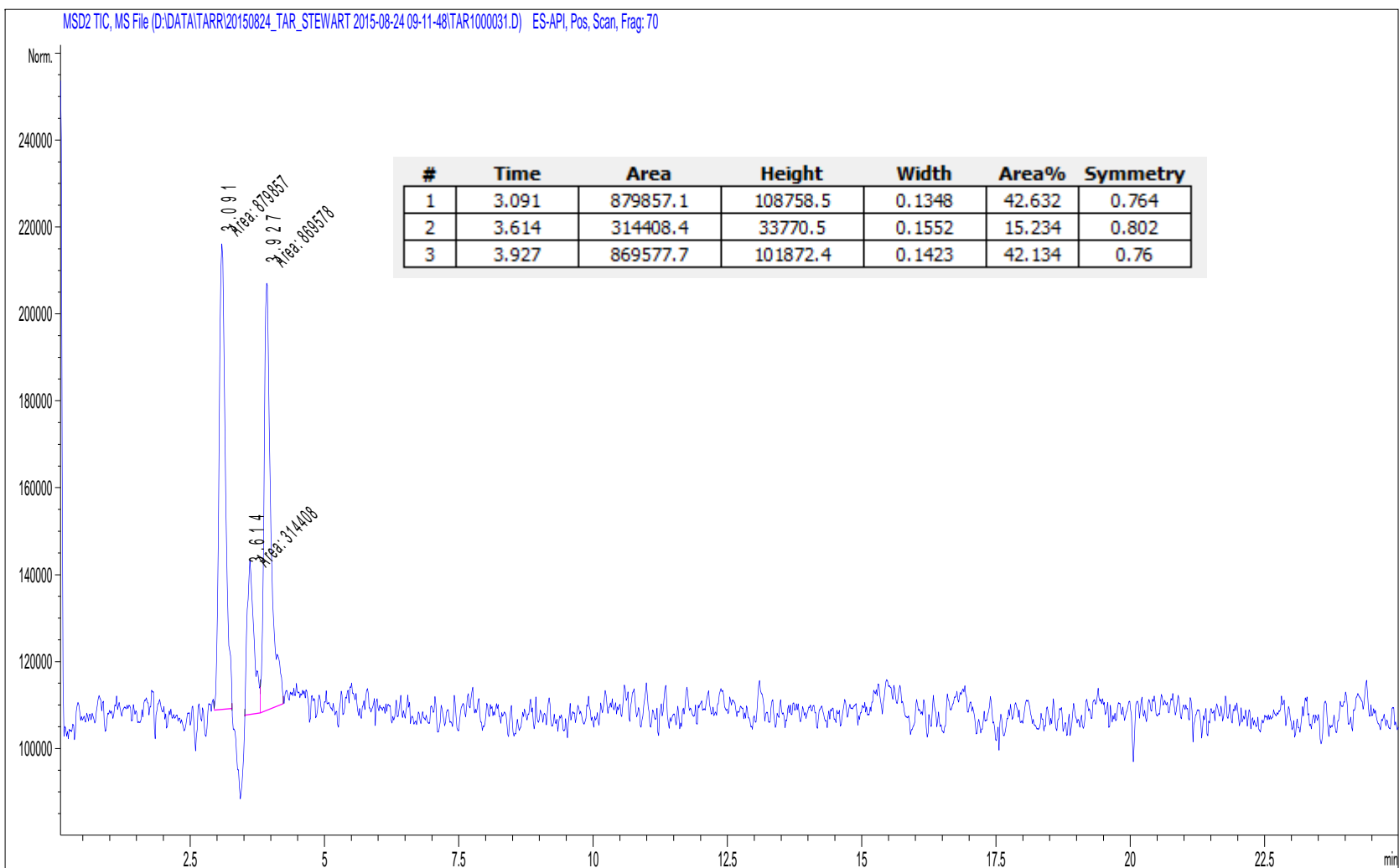
\*MSD2 SPC, time=3.922 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09:11:48\TAR1000024.D ES-API, Pos, Scan, Frag:

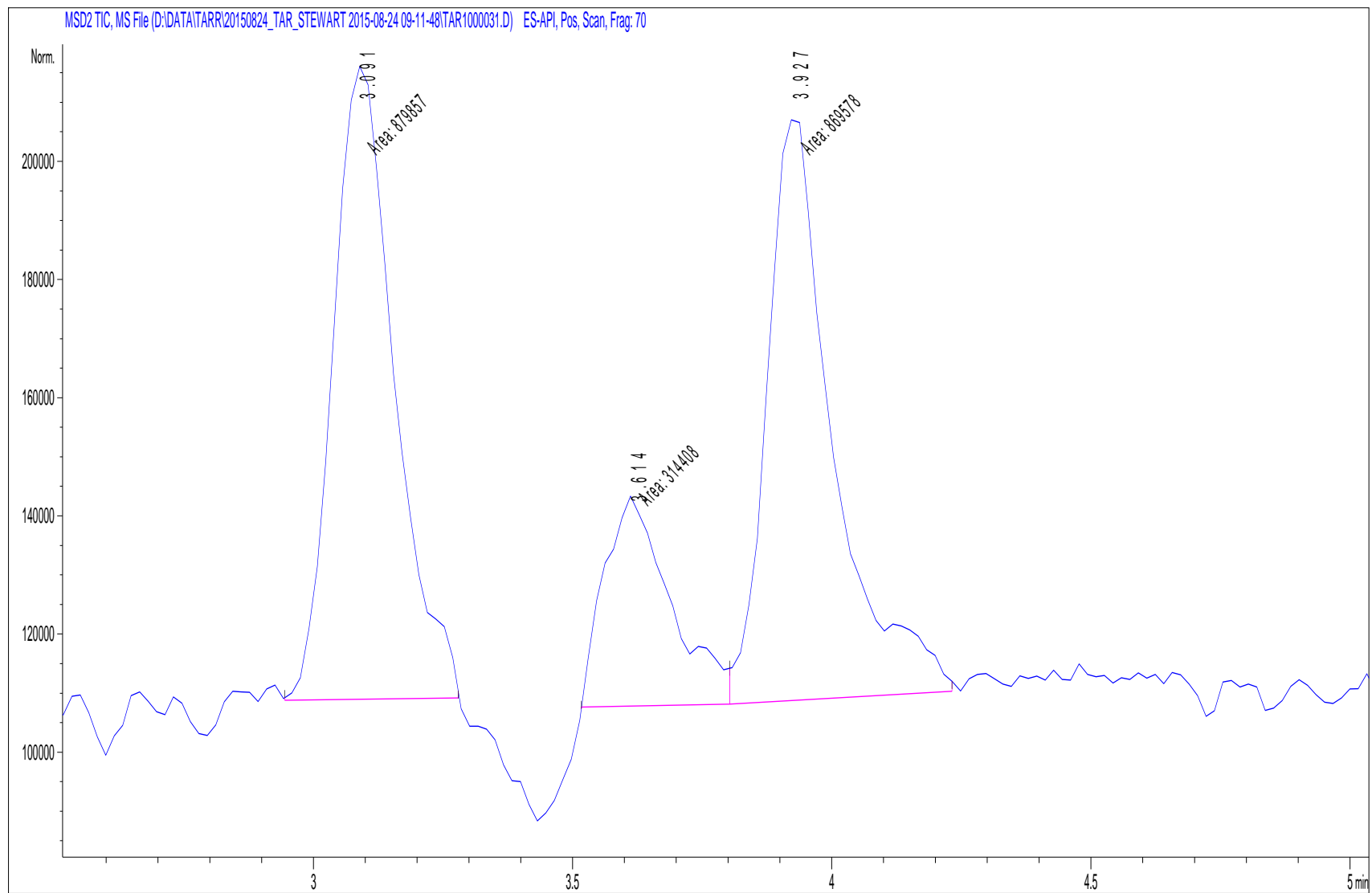


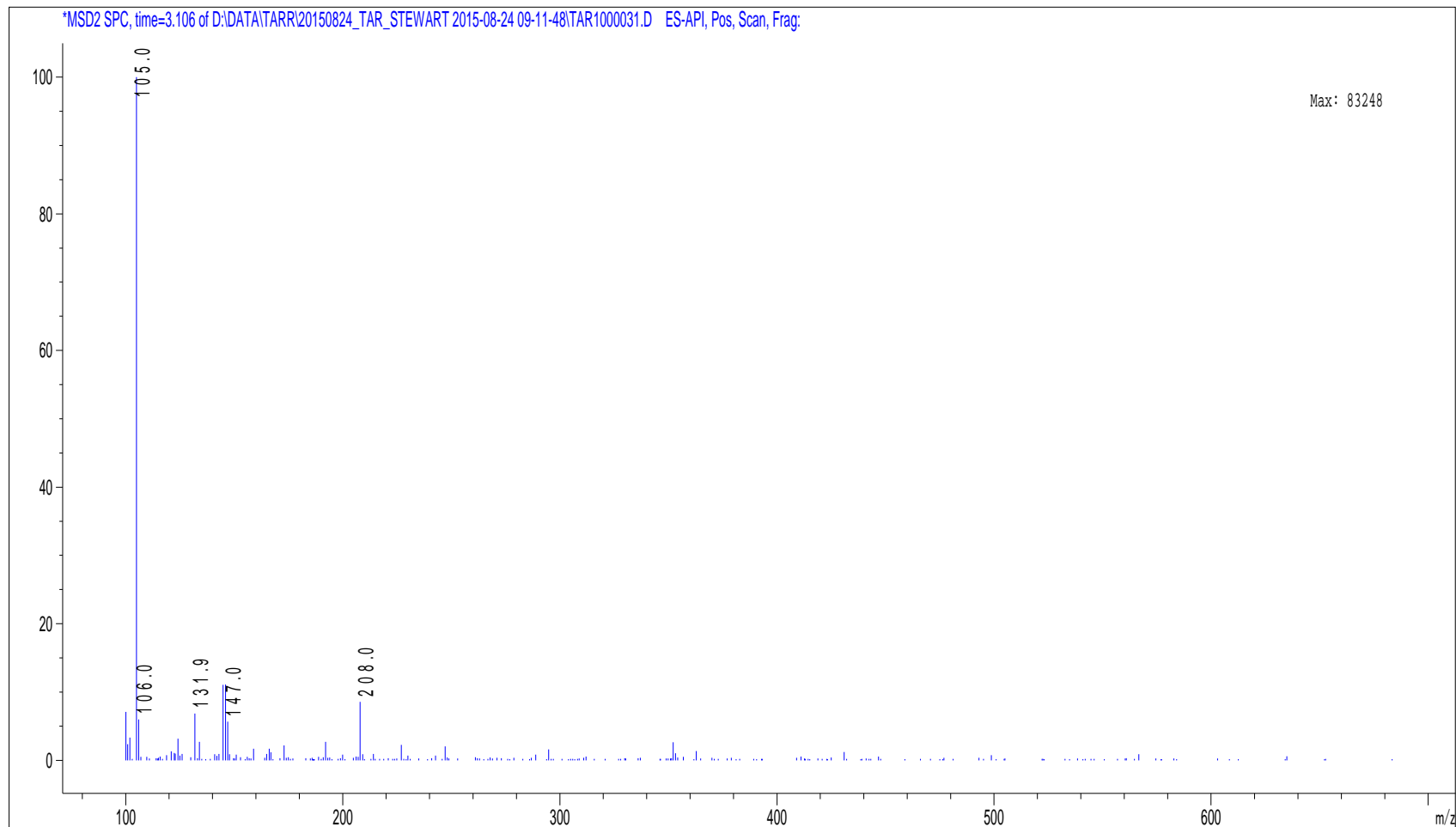
30-Jul-15

100 DC

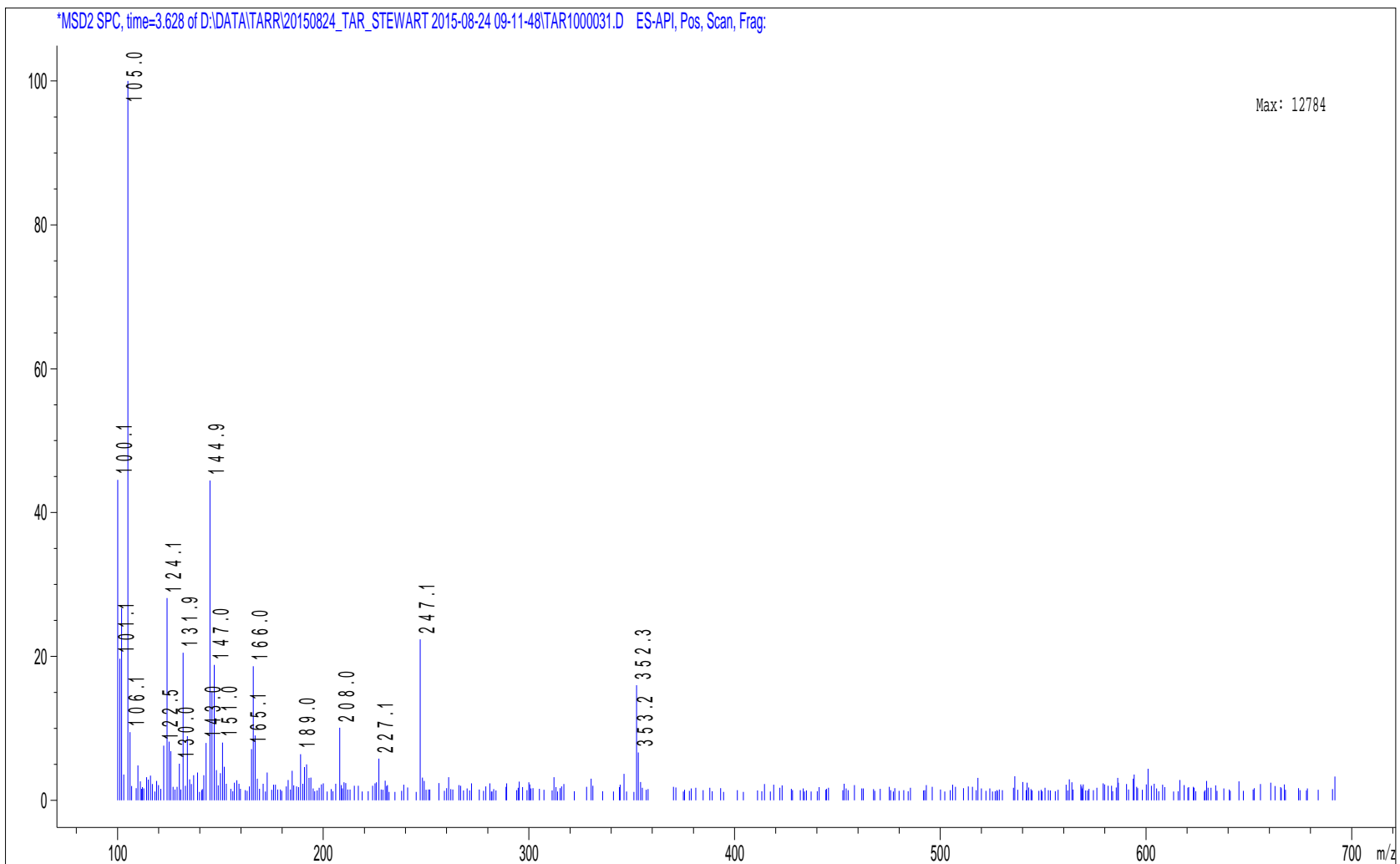
P2-D-06





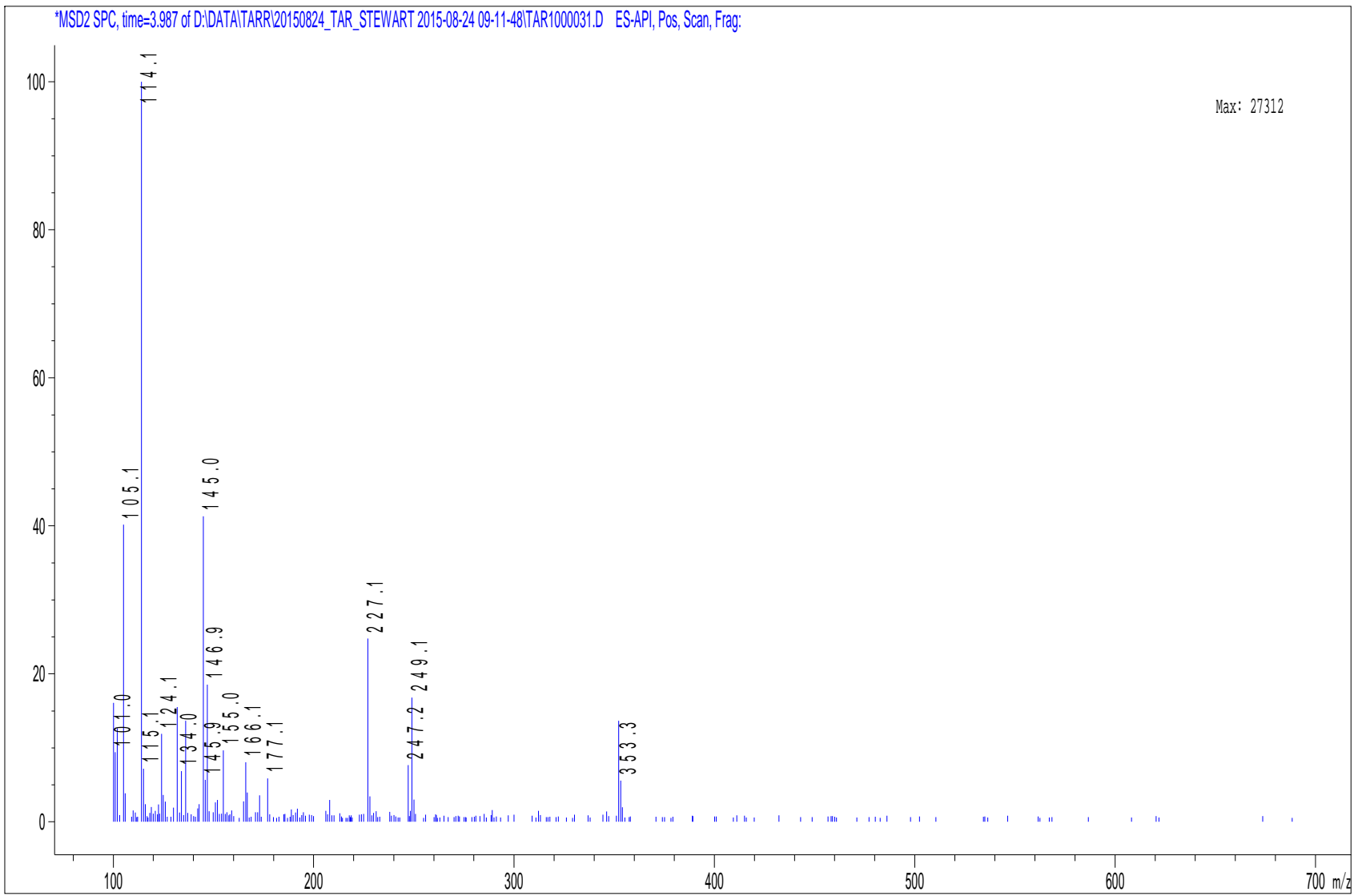


\*MSD2 SPC, time=3.628 of D:\DATA\ARRI\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000031.D ES-API, Pos, Scan, Frag:



Max: 12784

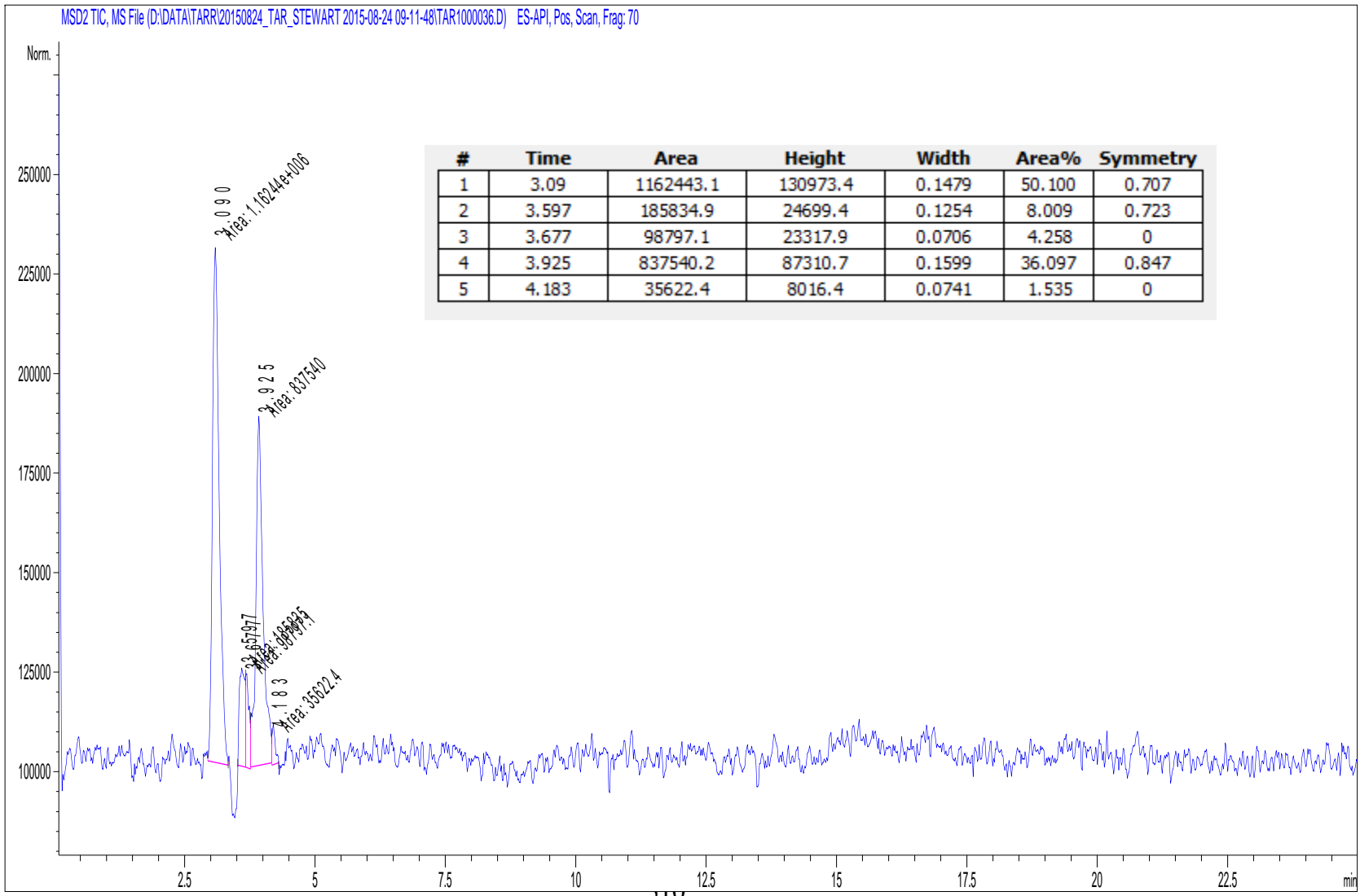


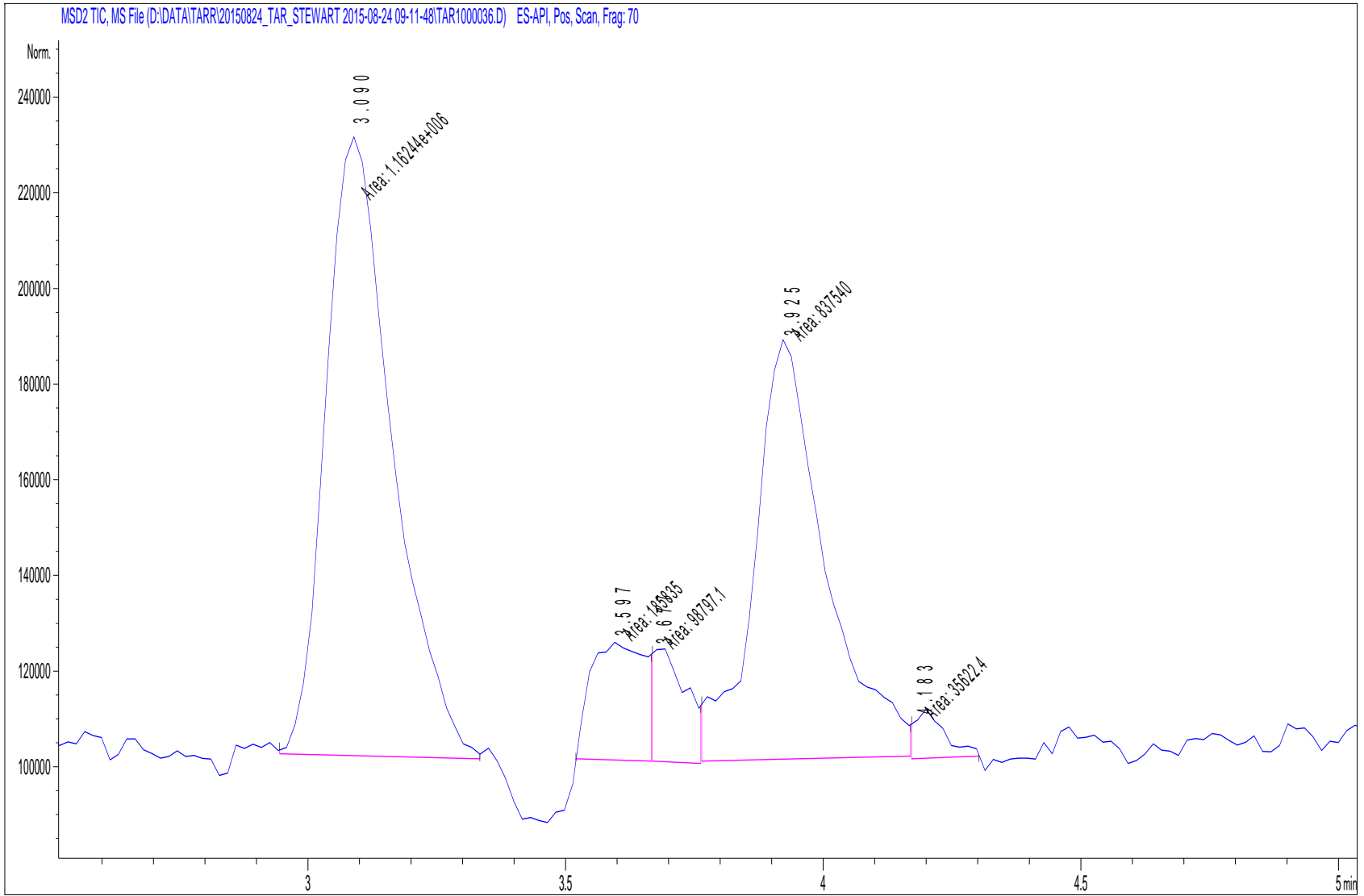


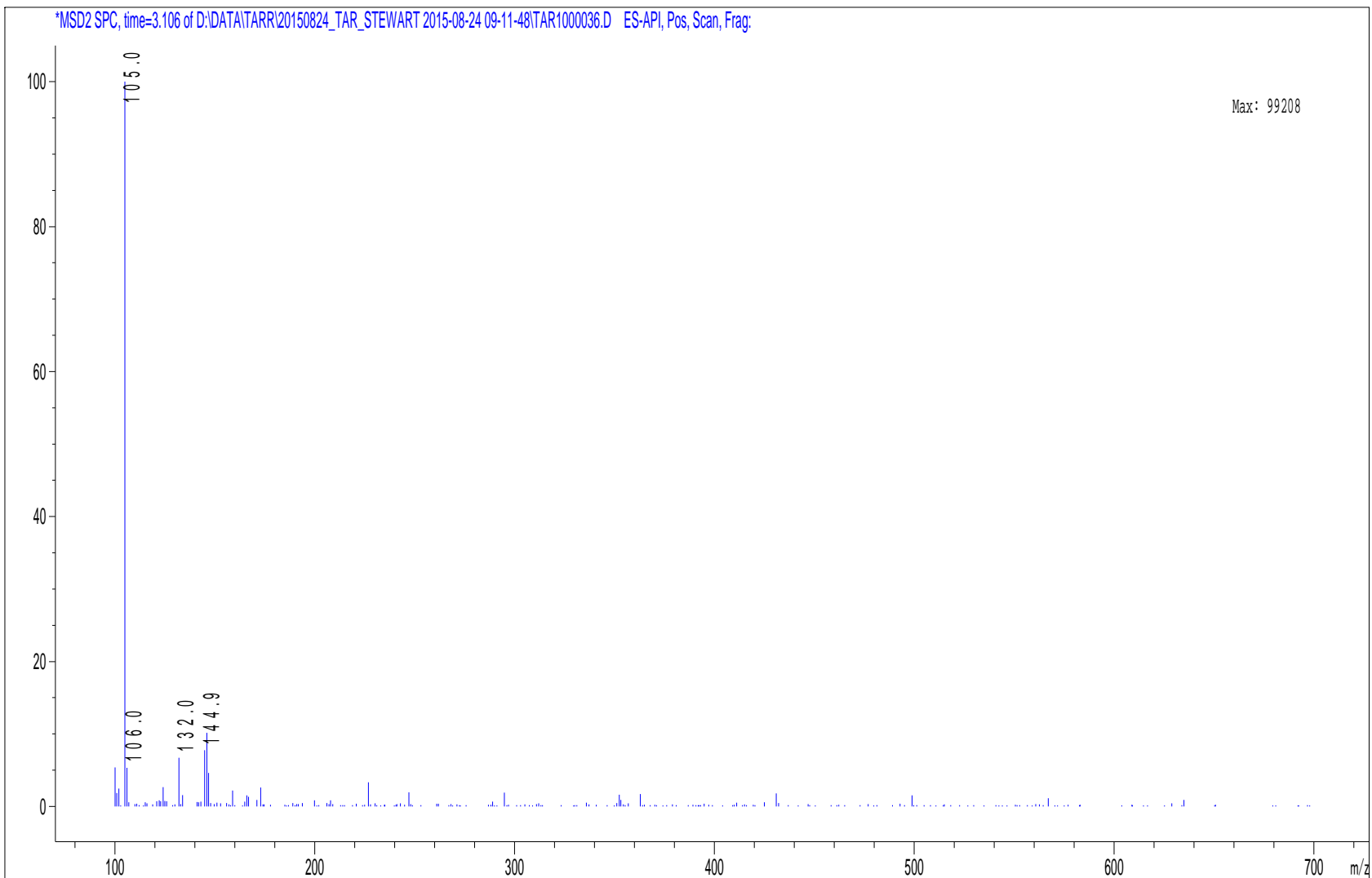
16-Jul-15

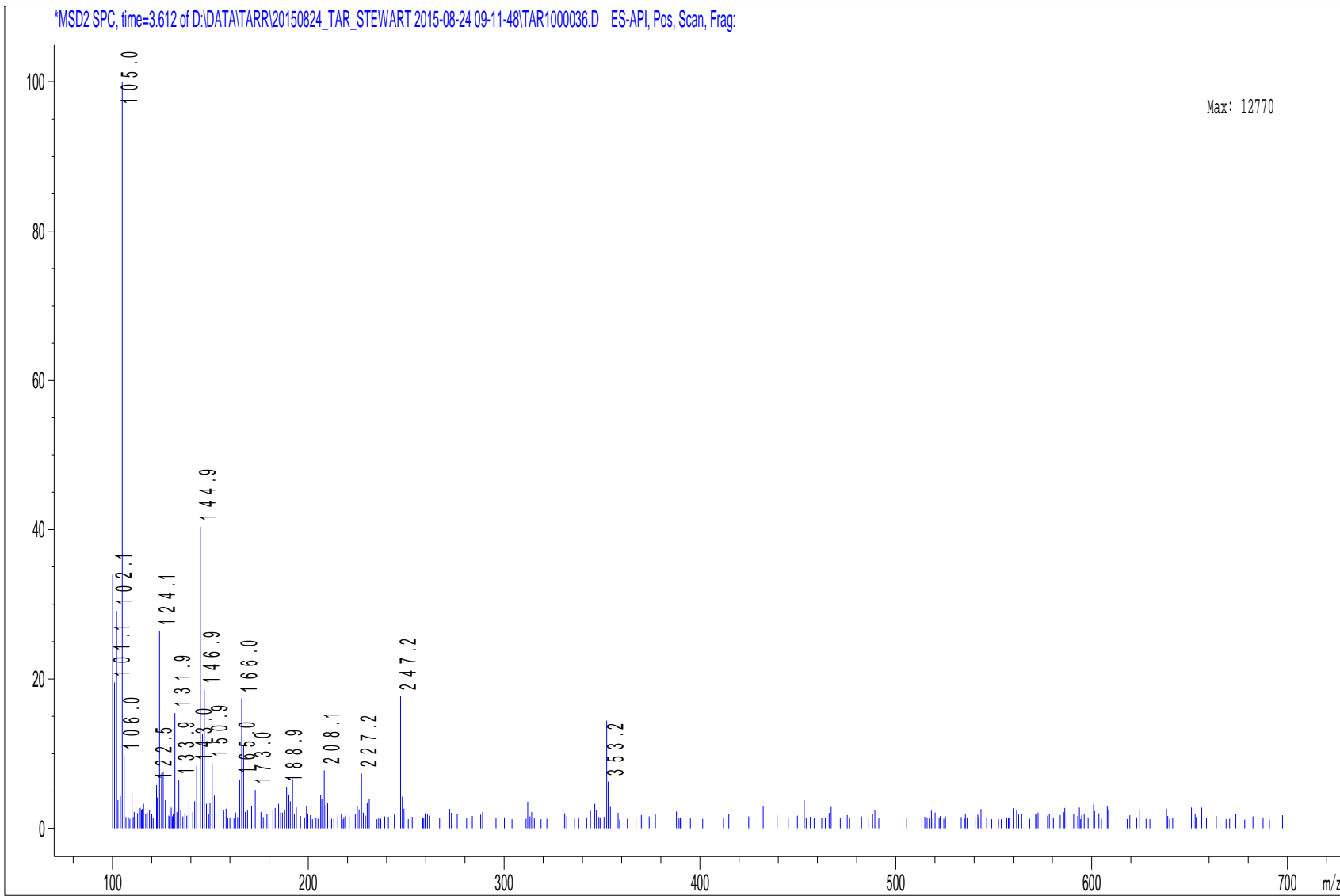
100 DC Problem no removal

P2-D-01

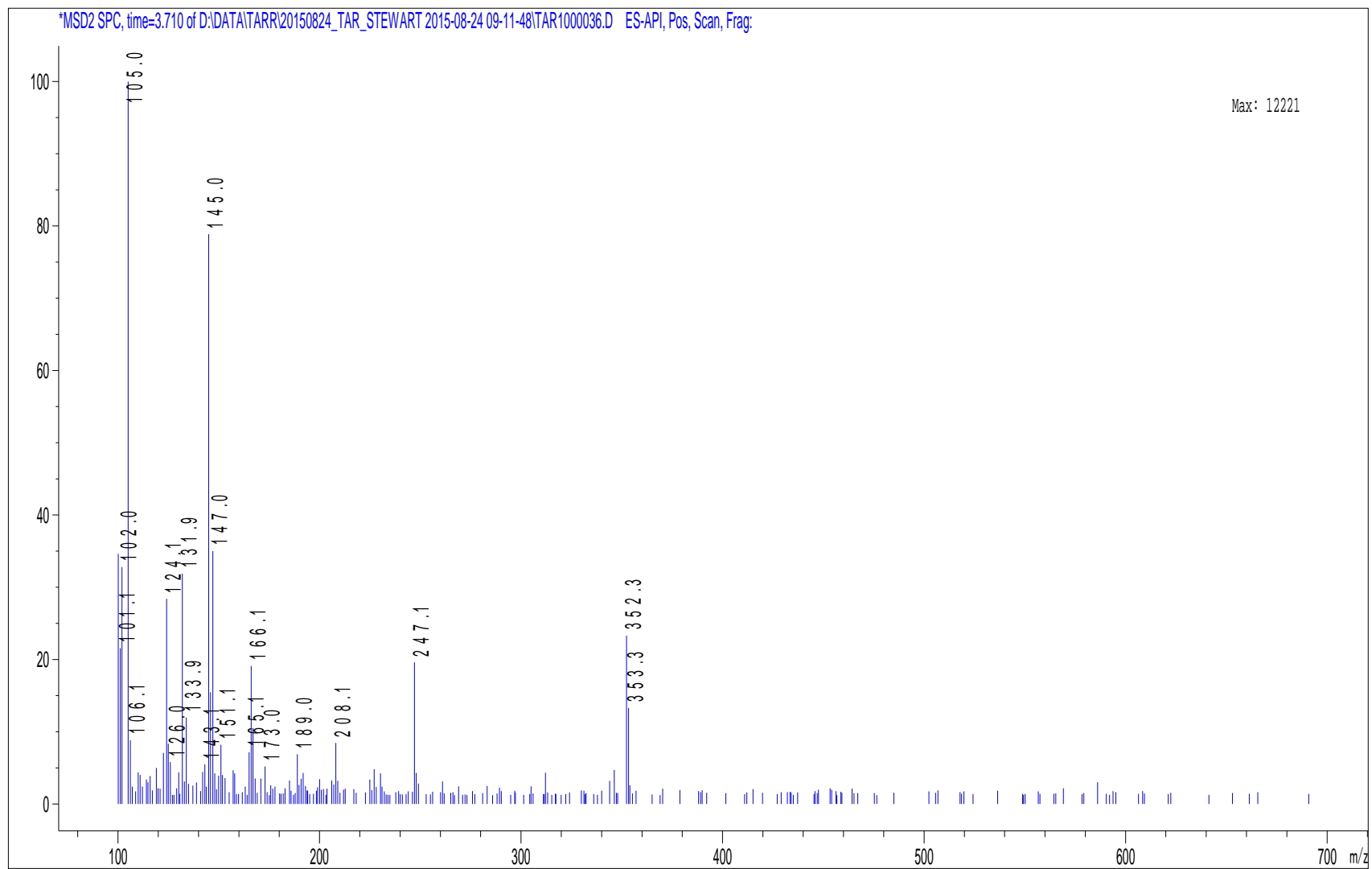




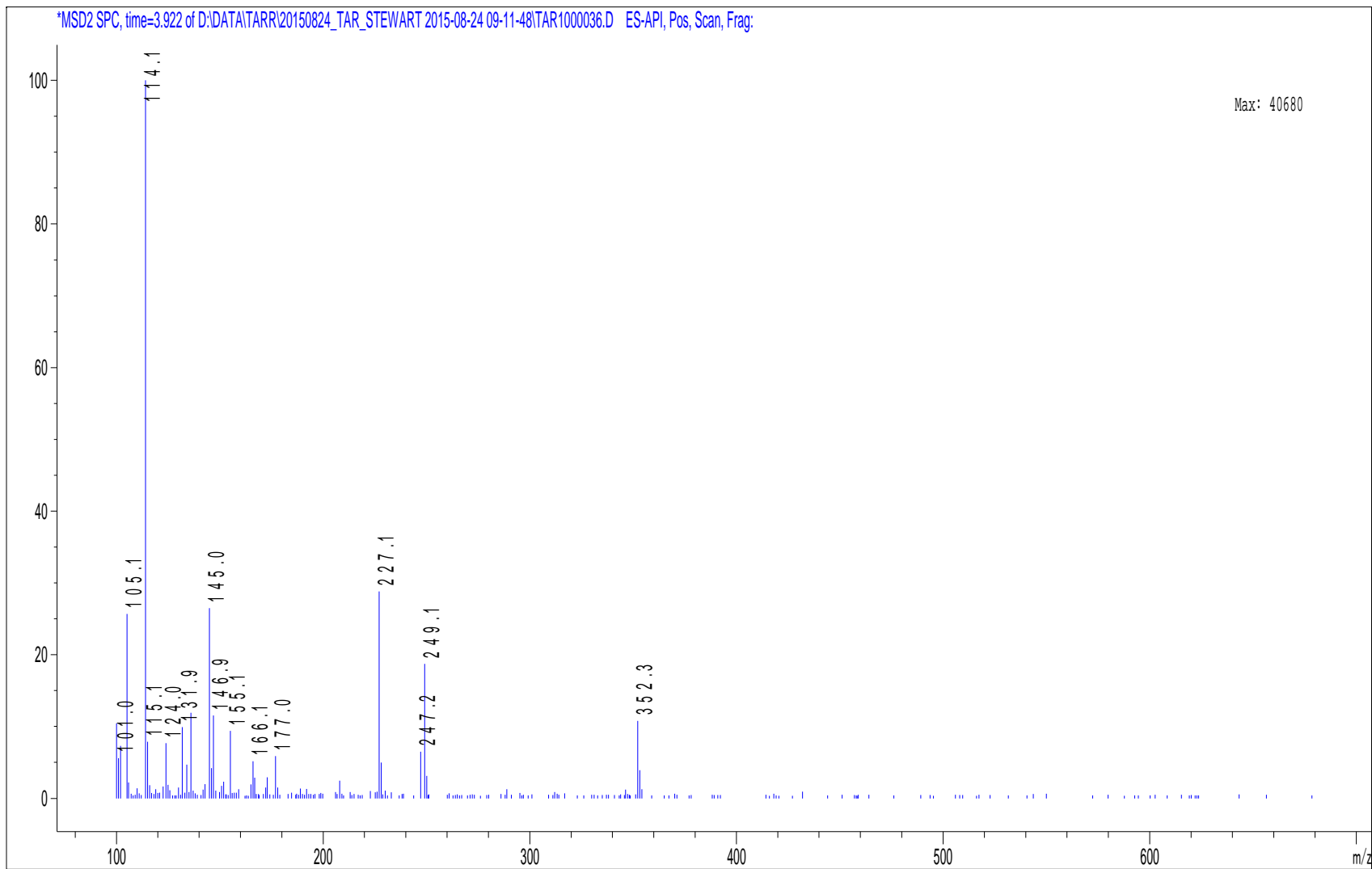




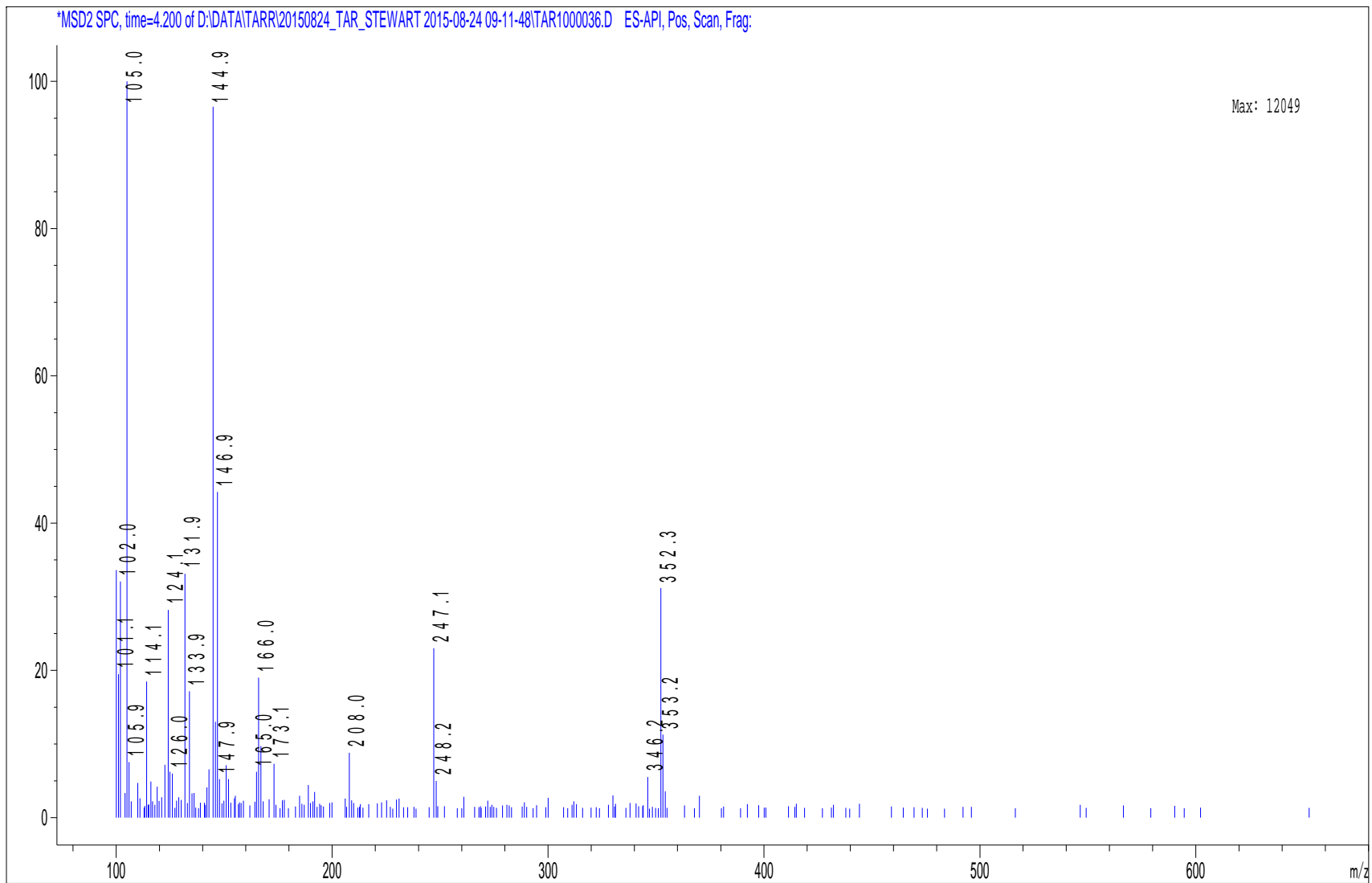
\*MSD2 SPC, time=3.710 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000036.D ES-API, Pos, Scan, Frag:



\*MSD2 SPC, time=3.922 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000036.D ES-API, Pos, Scan, Frag:



\*MSD2 SPC, time=4.200 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000036.D ES-API, Pos, Scan, Frag:



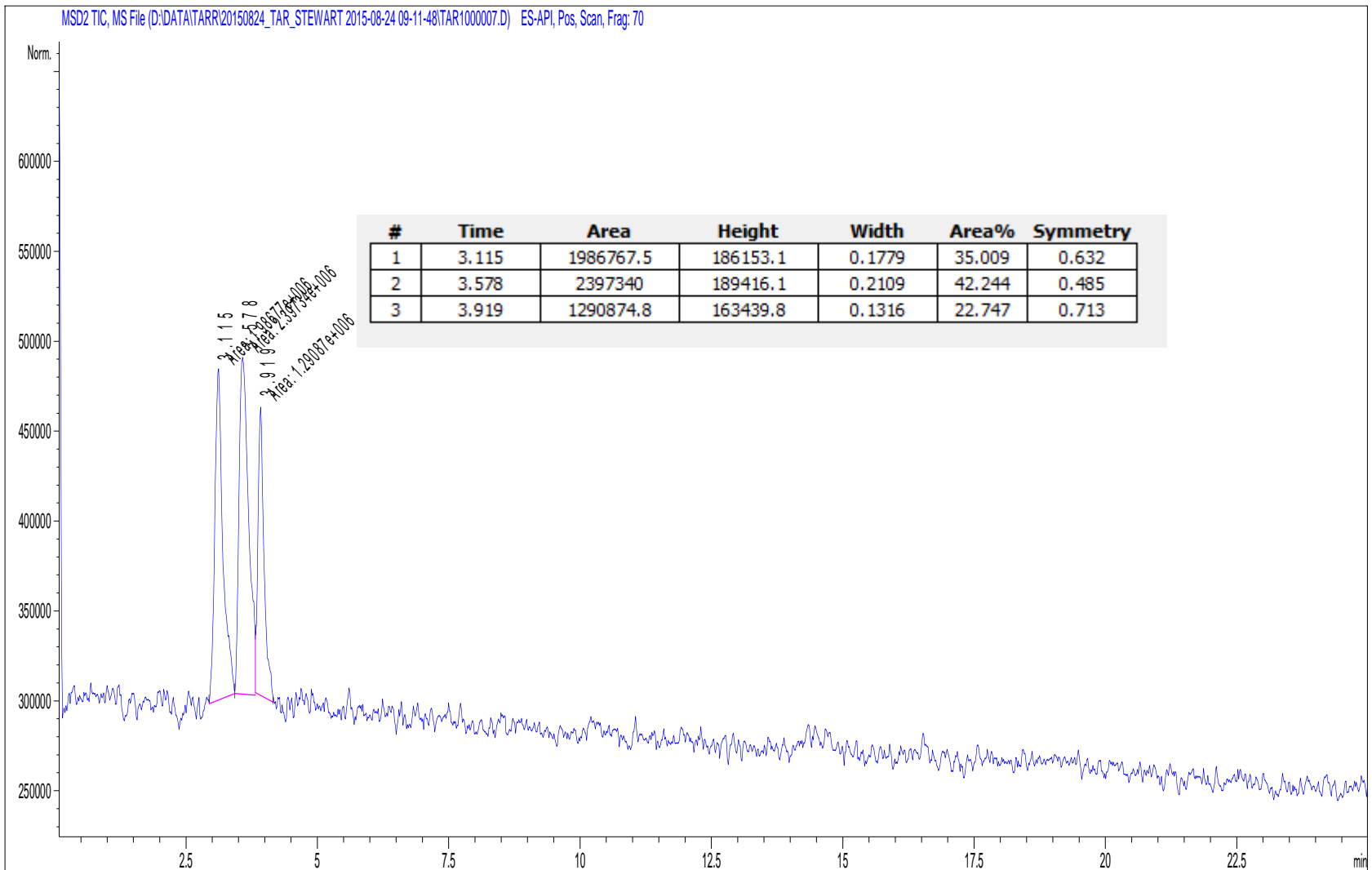


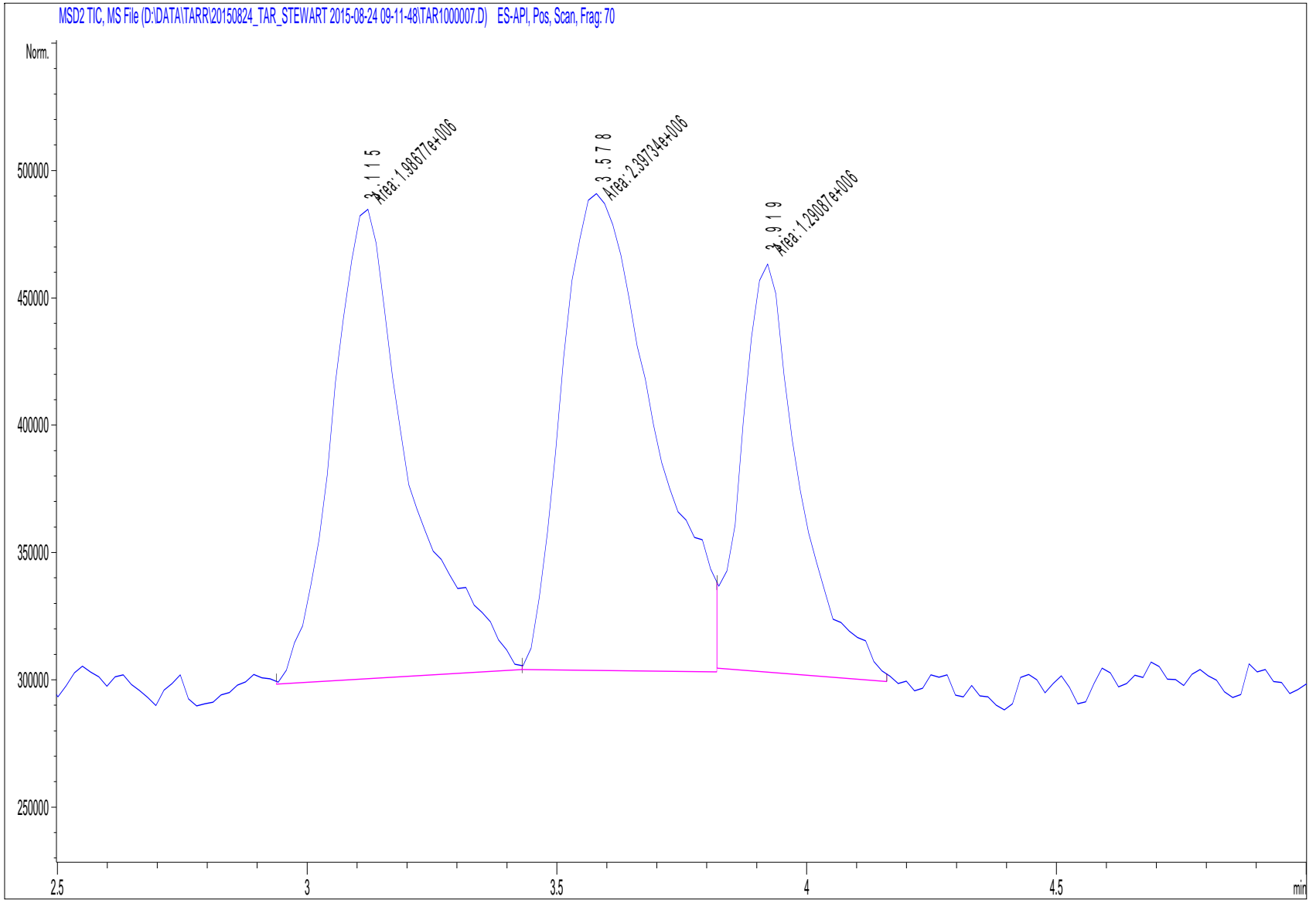
# pH 8

16-Apr-15

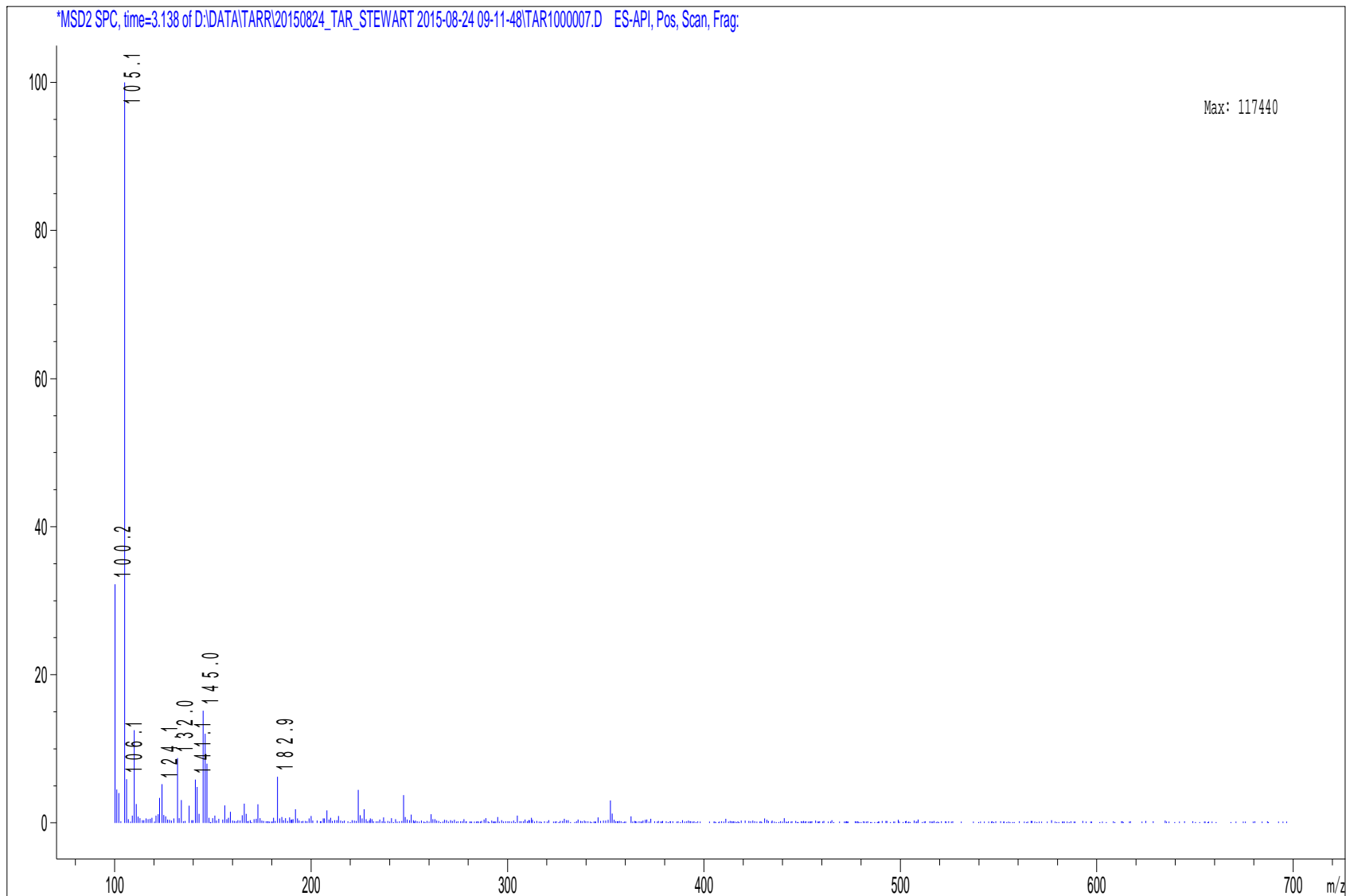
H2O2 Ctrl

P2-A-07

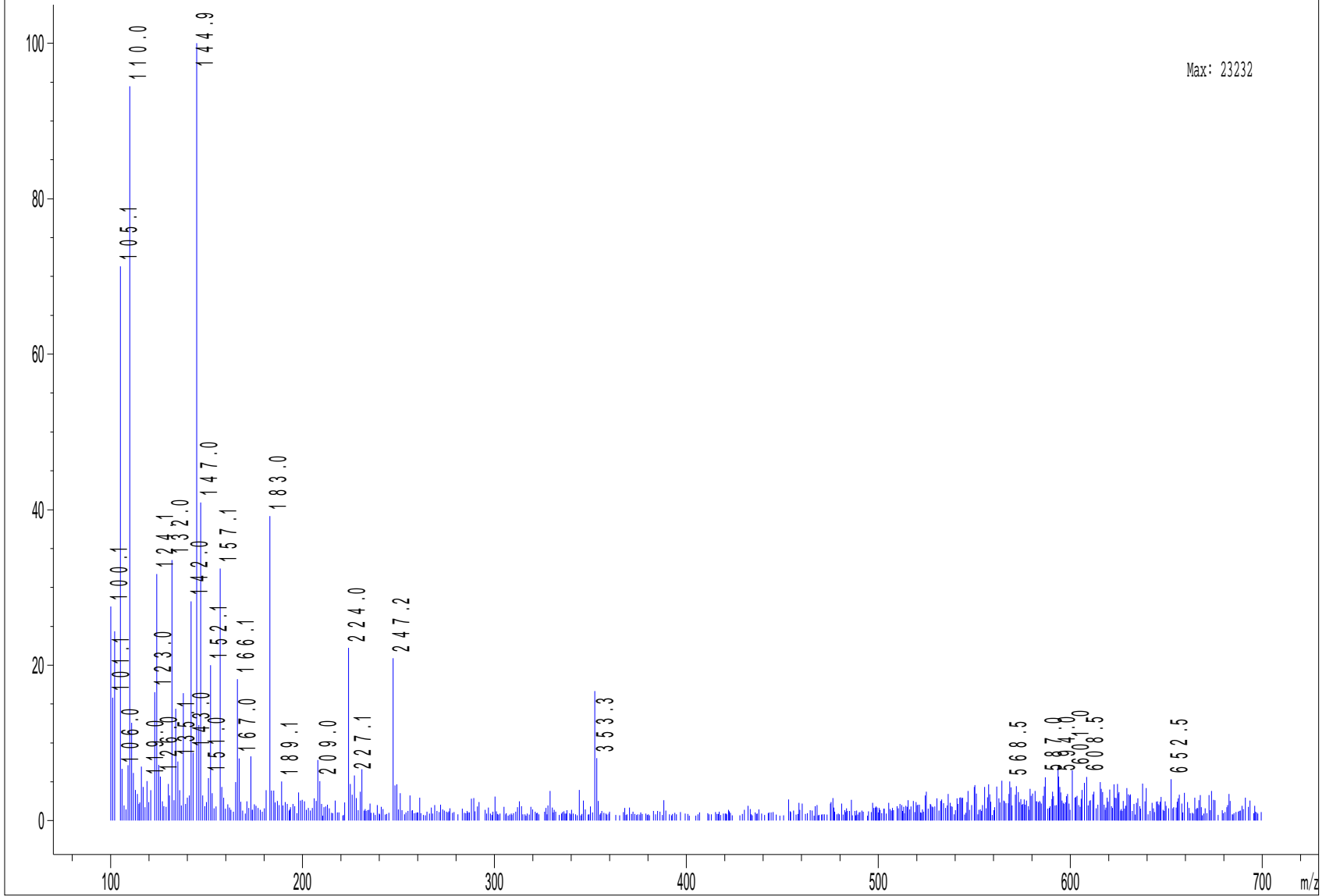


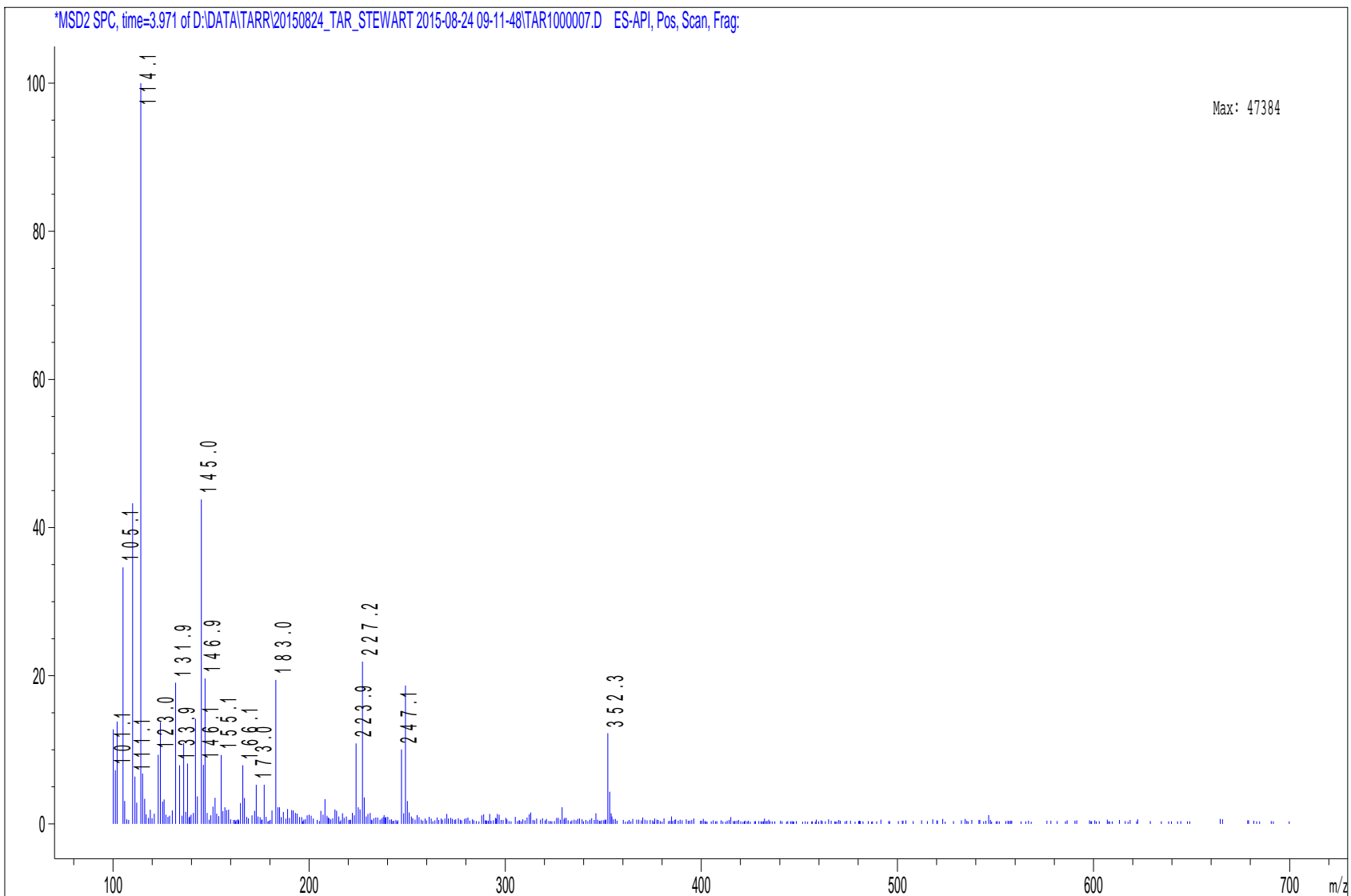


\*MSD2 SPC, time=3.138 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09:11:48\TAR1000007.D ES-API, Pos, Scan, Frag:



\*MSD2 SPC, time=3.628 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09:11:48\TAR1000007.D ES-API, Pos, Scan, Frag:

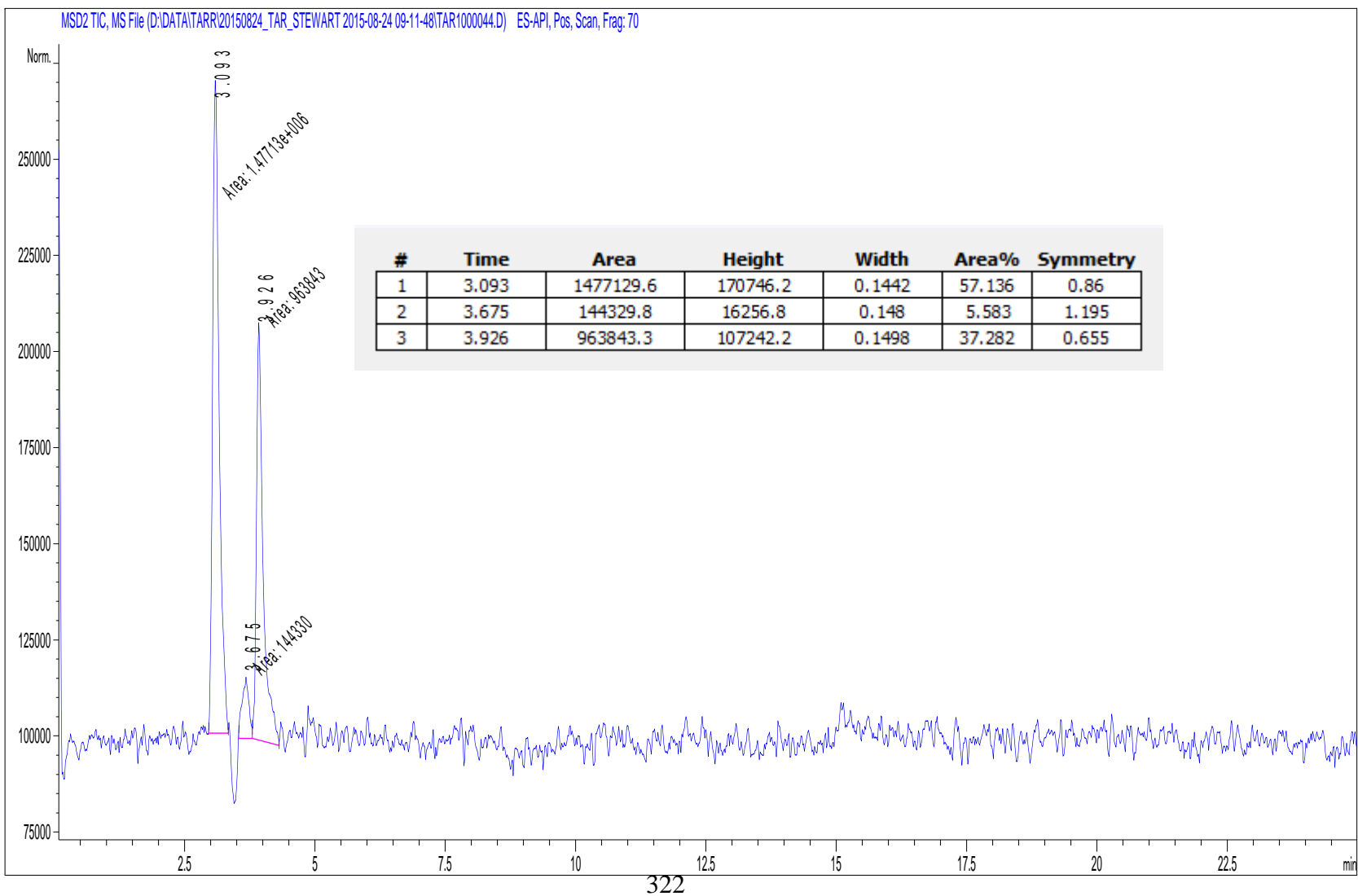


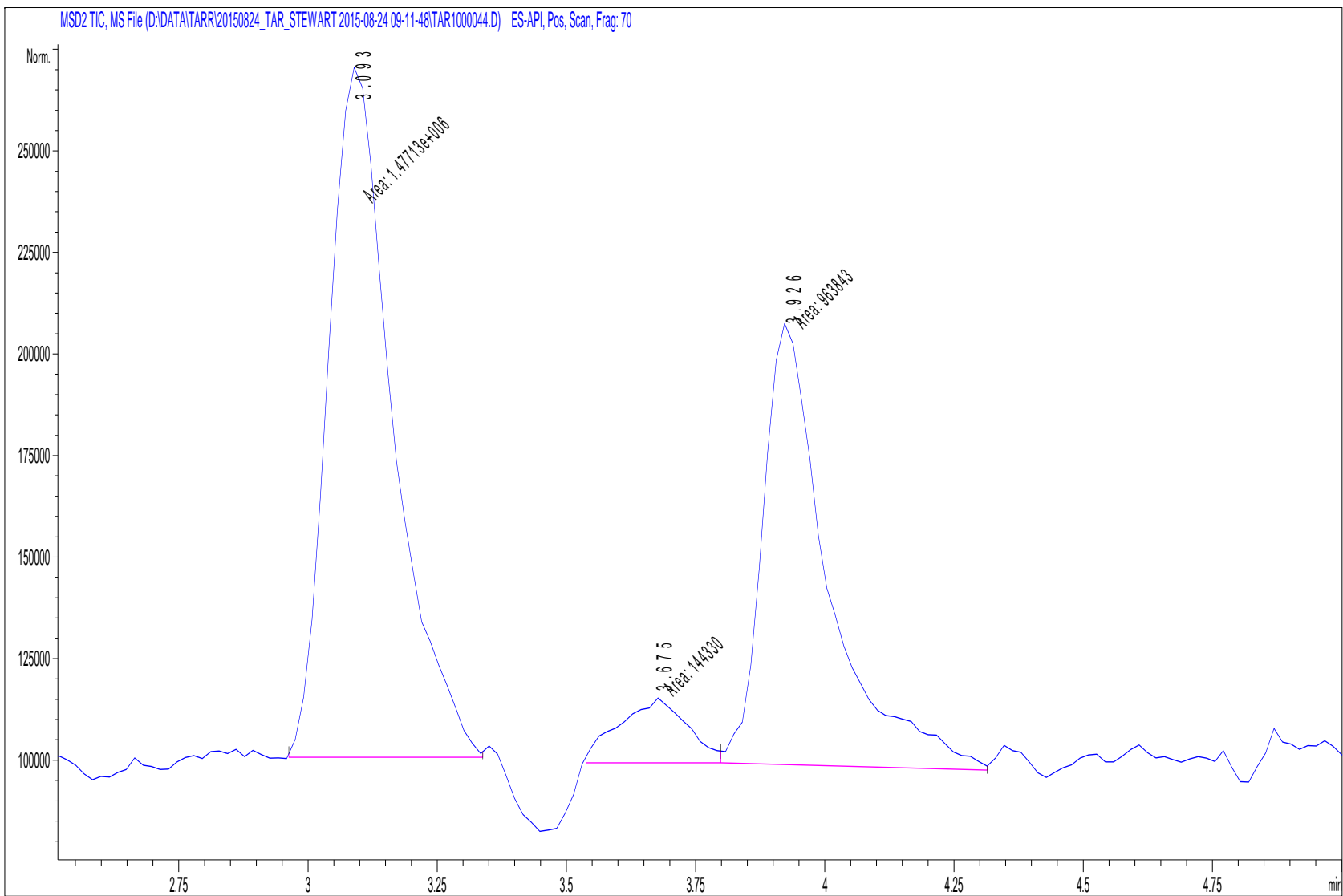


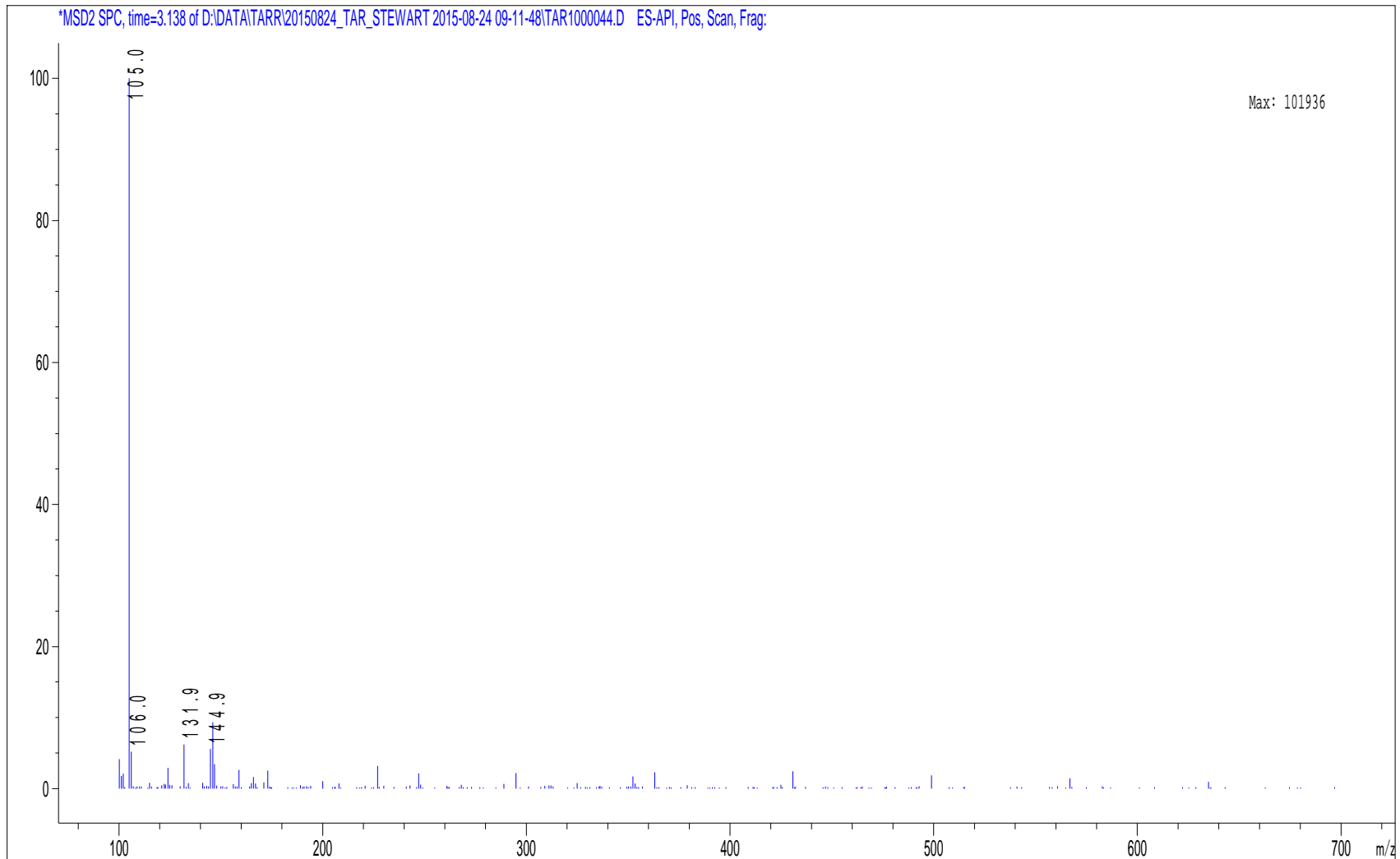
15-Jul-15

0 DC

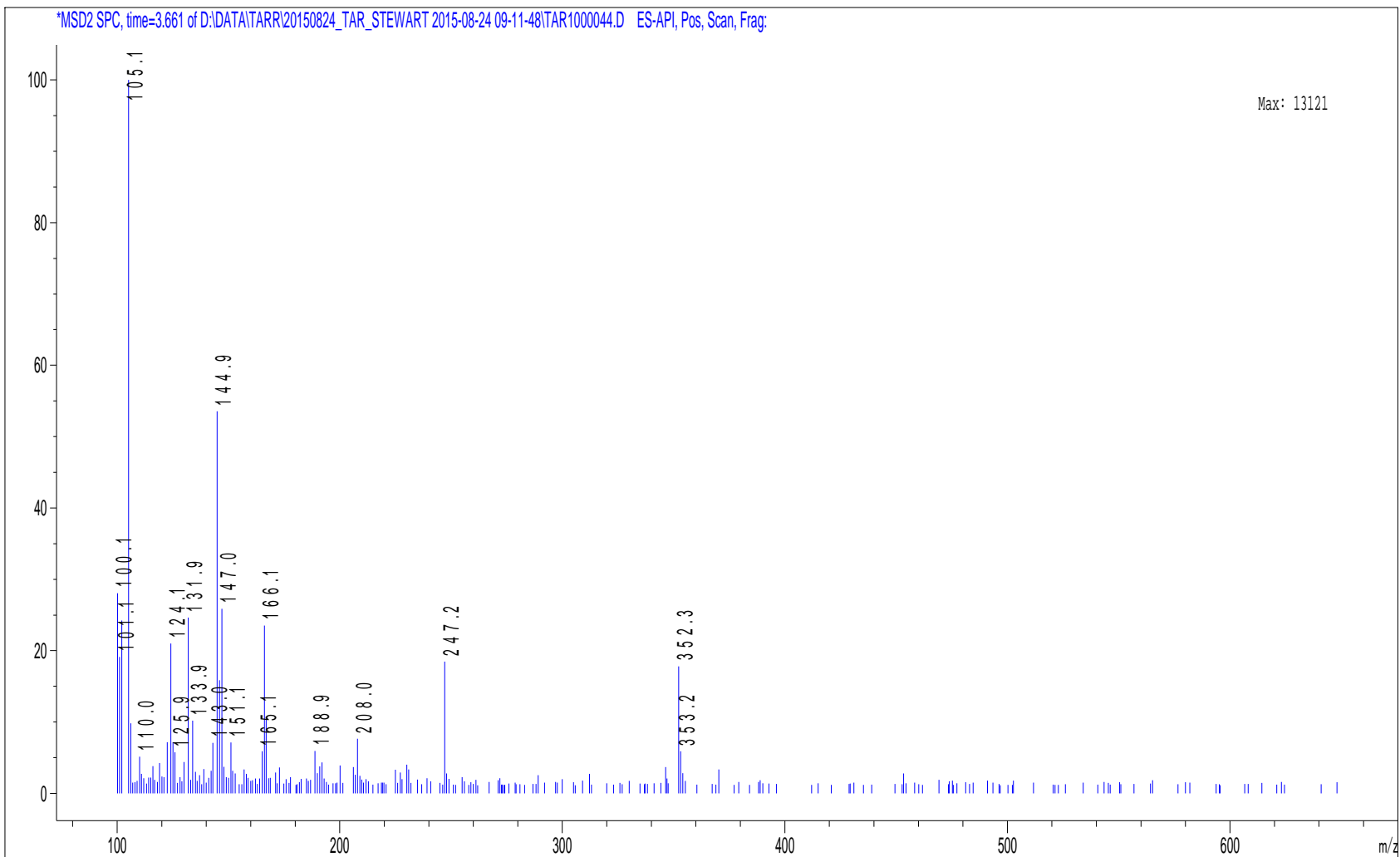
P2-E-08



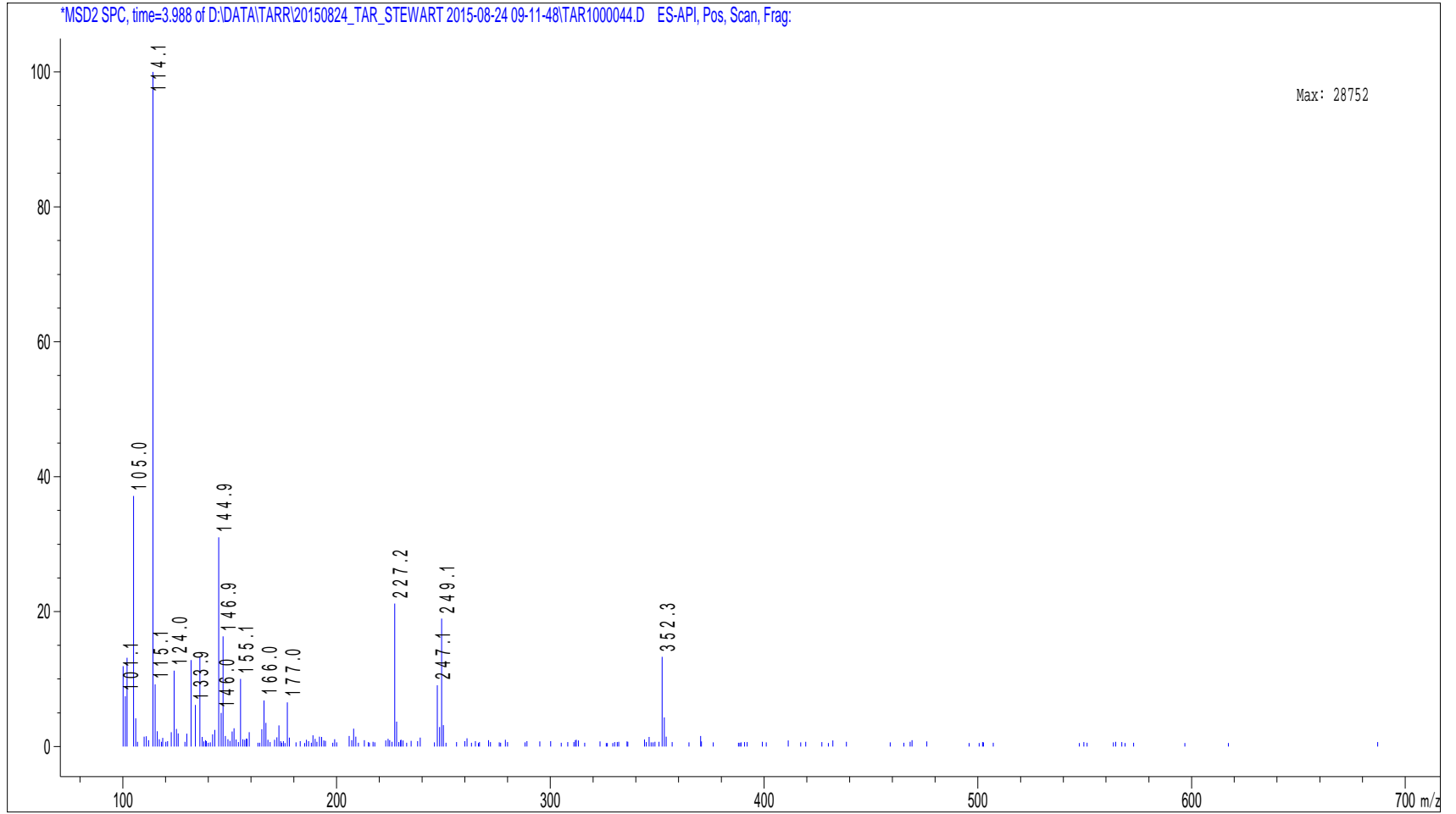








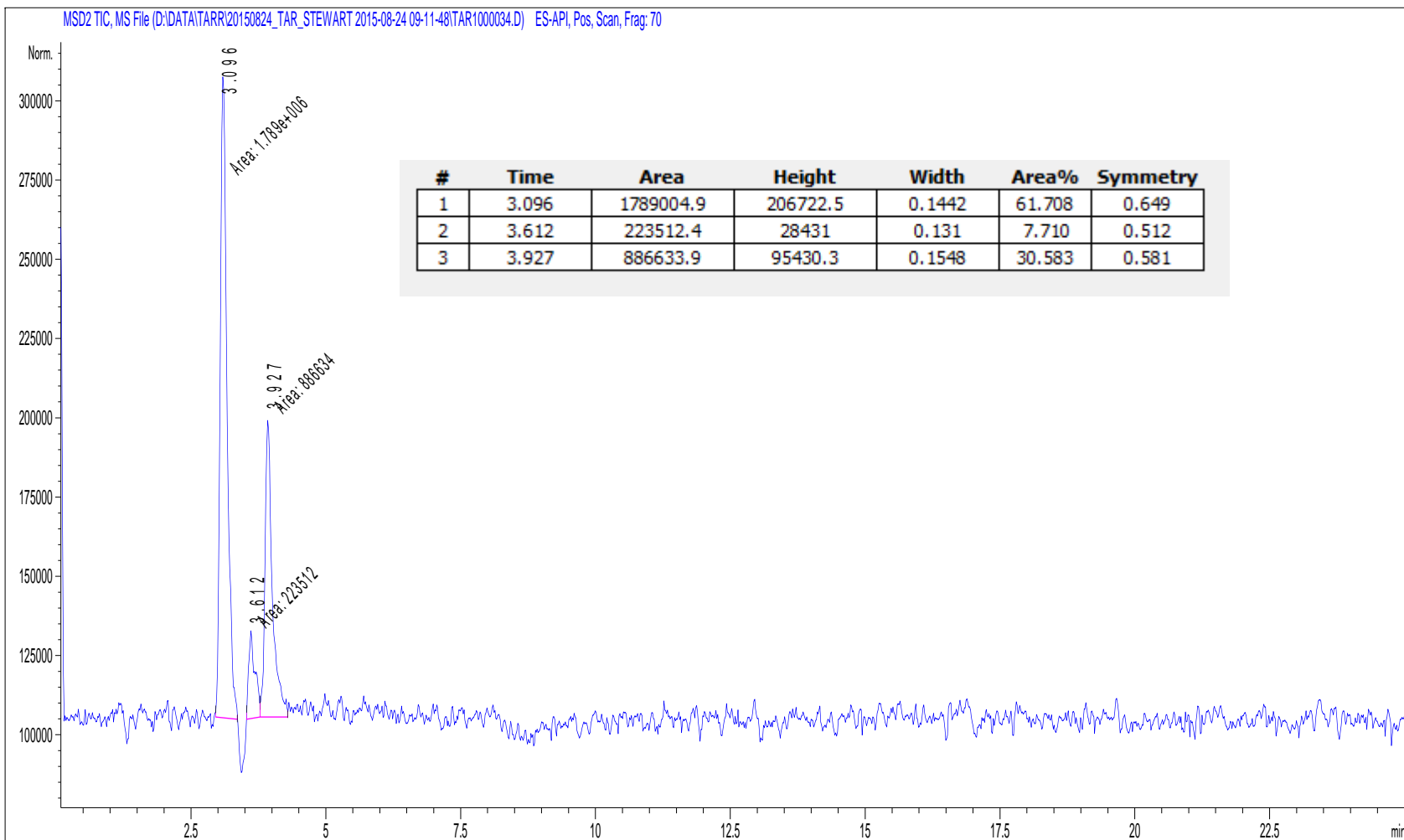
\*MSD2 SPC, time=3.988 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000044.D ES-API, Pos, Scan, Frag:

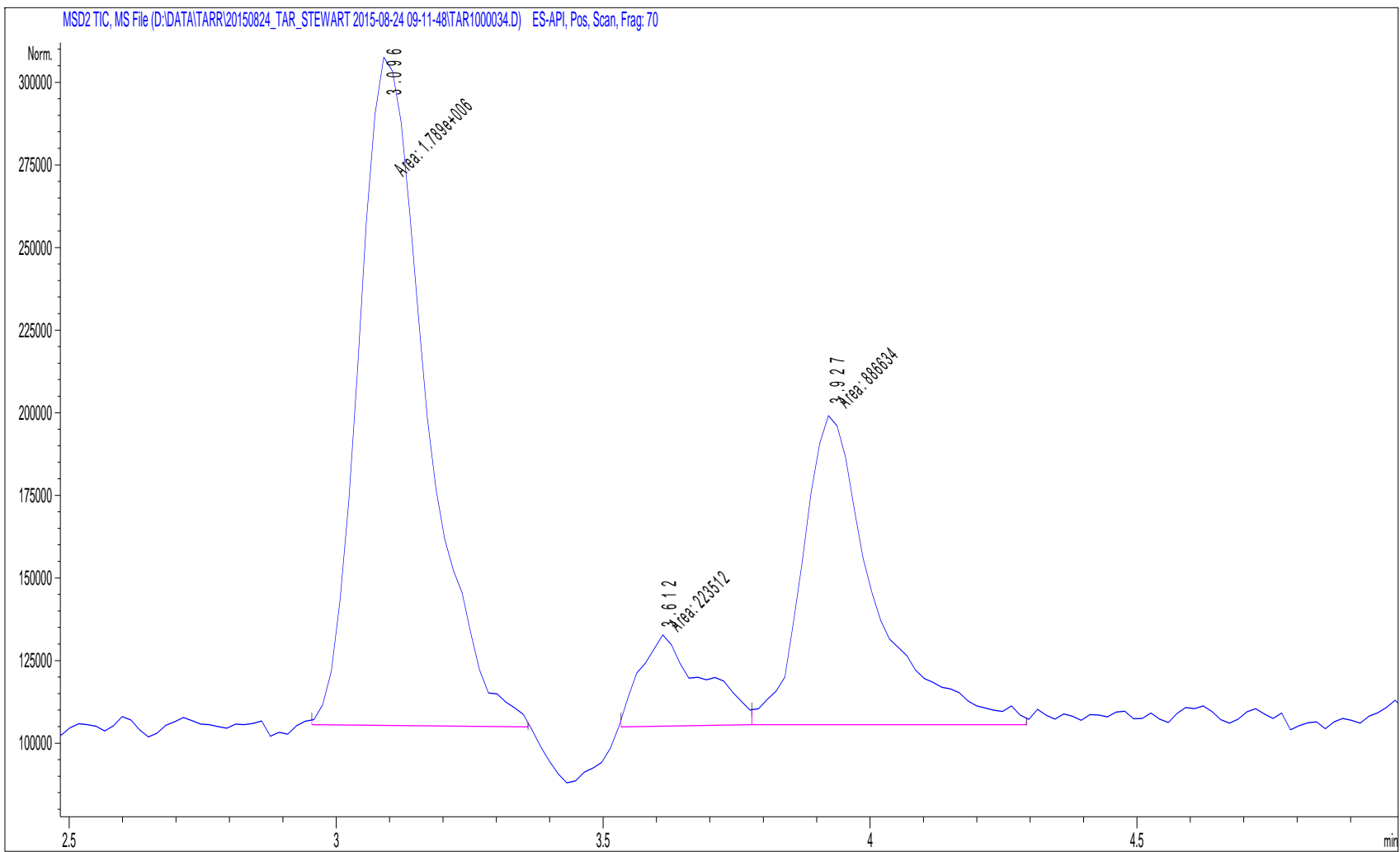


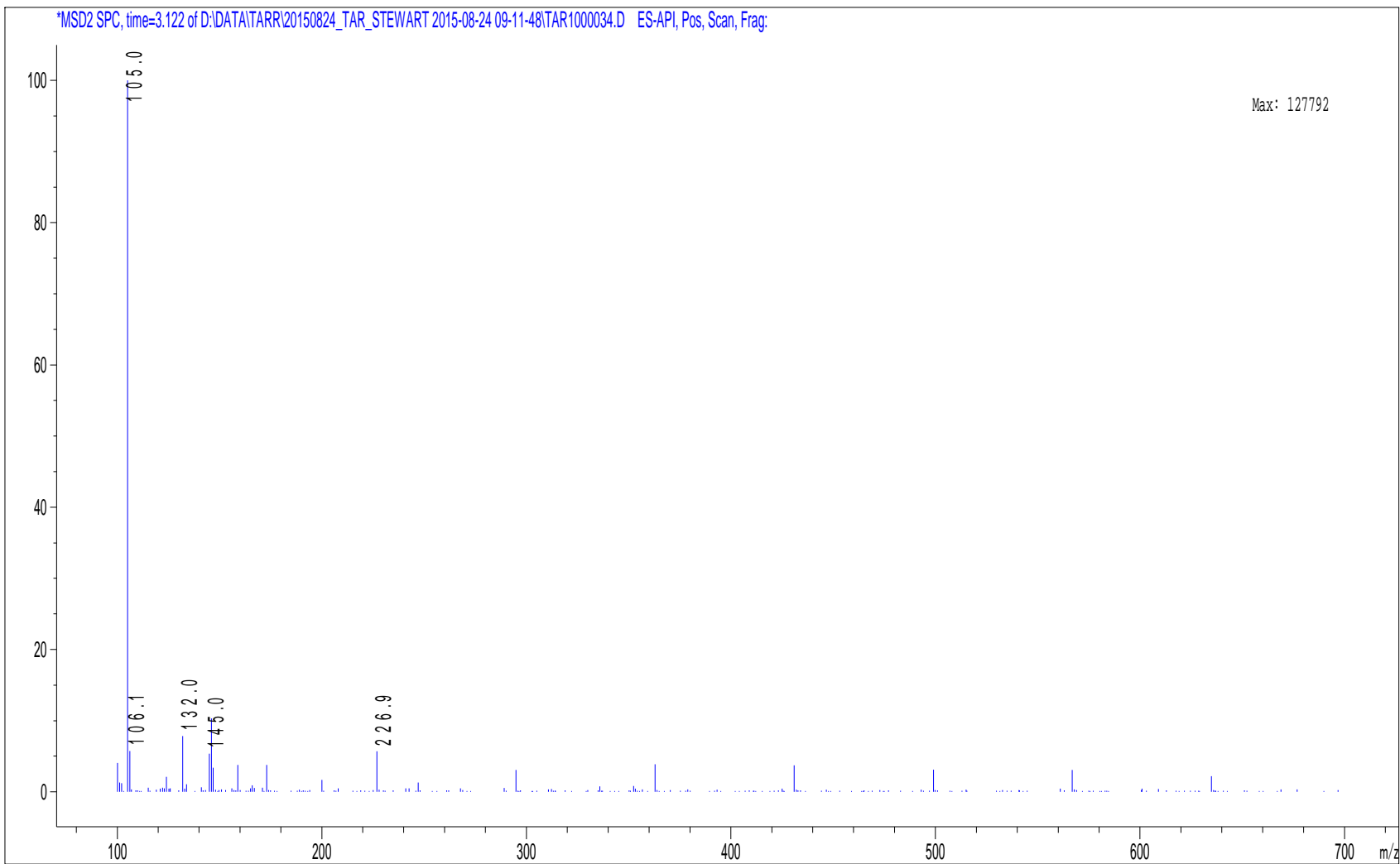
21-Jul-15

5 DC

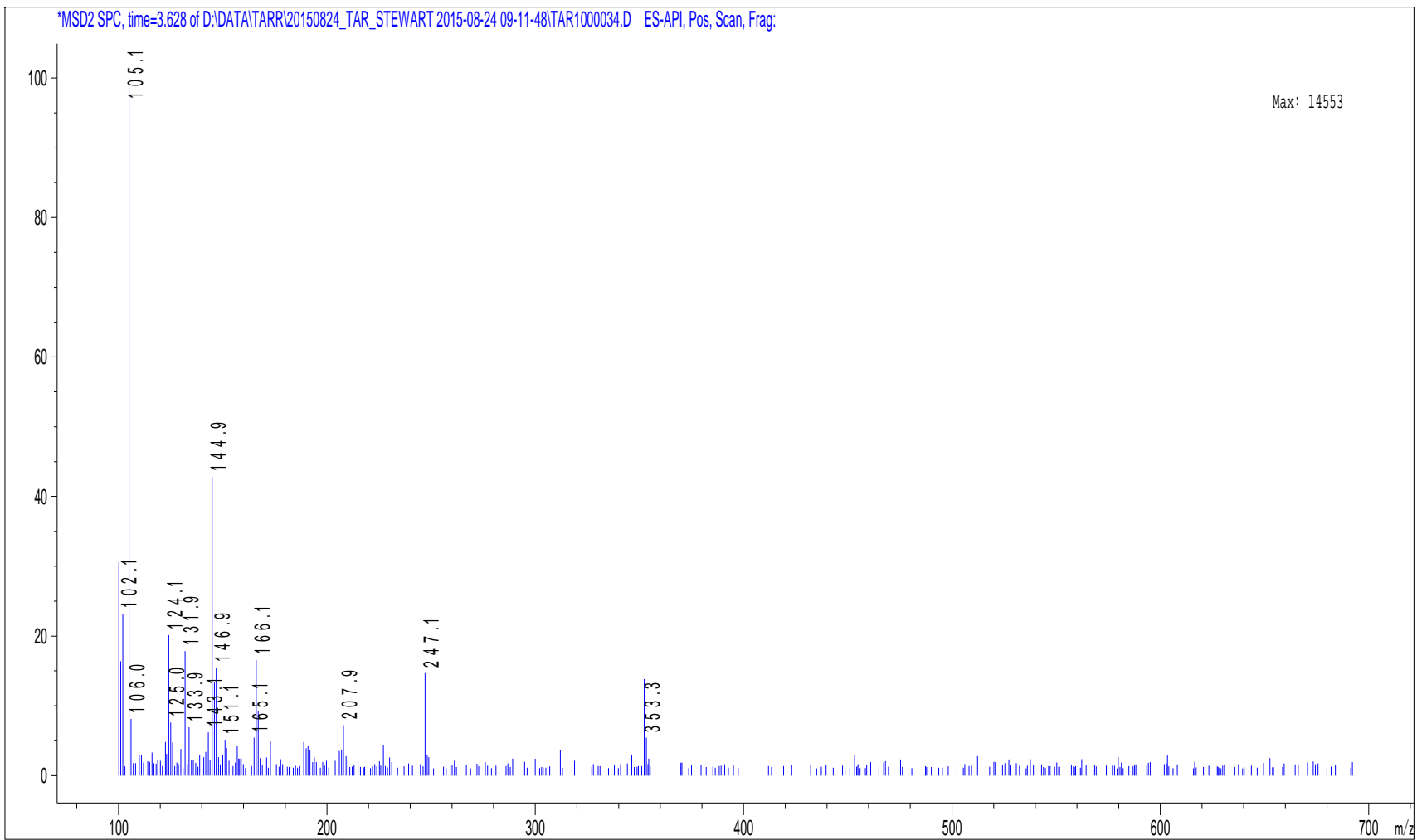
P2-D-03



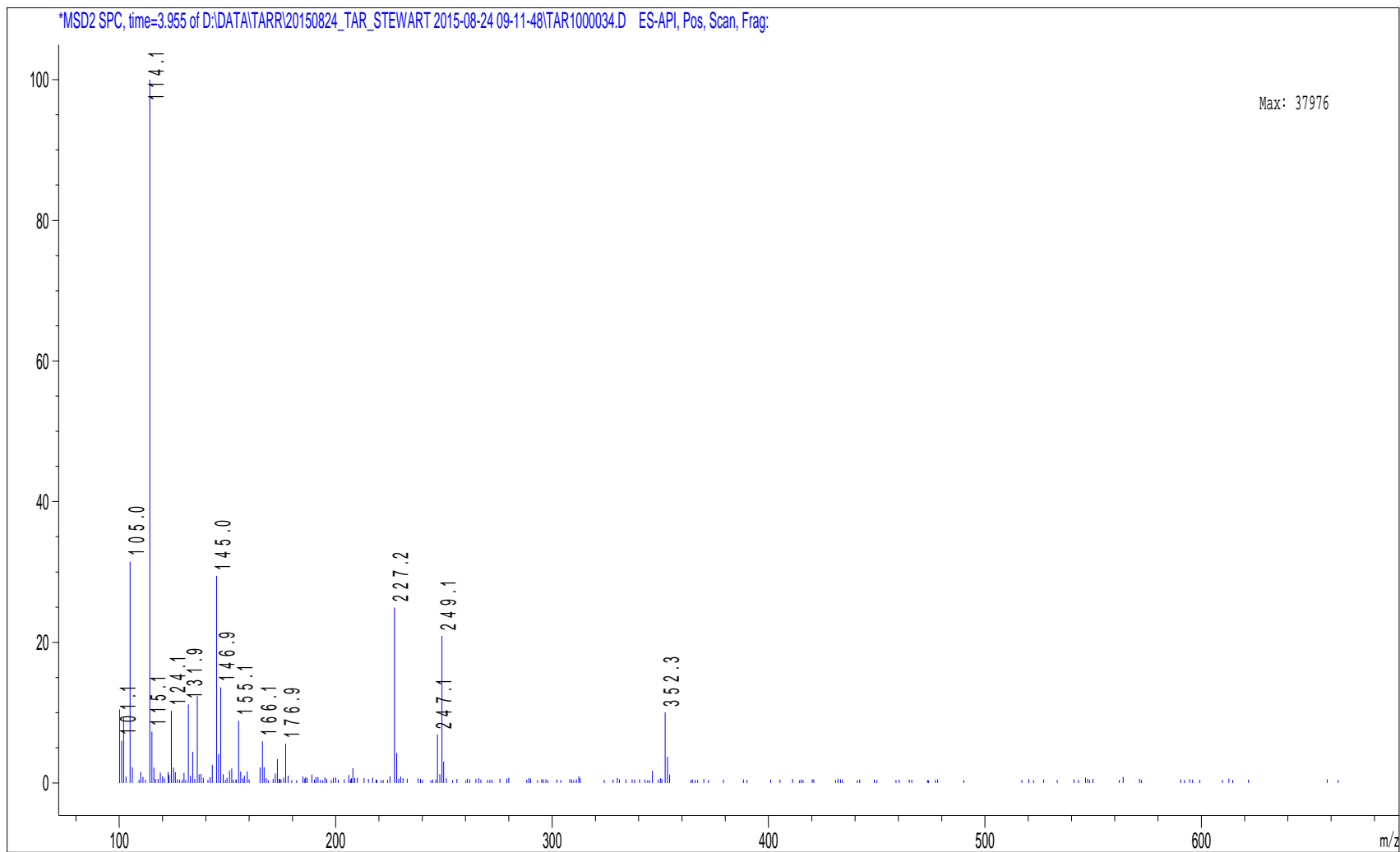




\*MSD2 SPC, time=3.628 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000034.D ES-API, Pos, Scan, Frag:



\*MSD2 SPC, time=3.955 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000034.D ES-API, Pos, Scan, Frag:

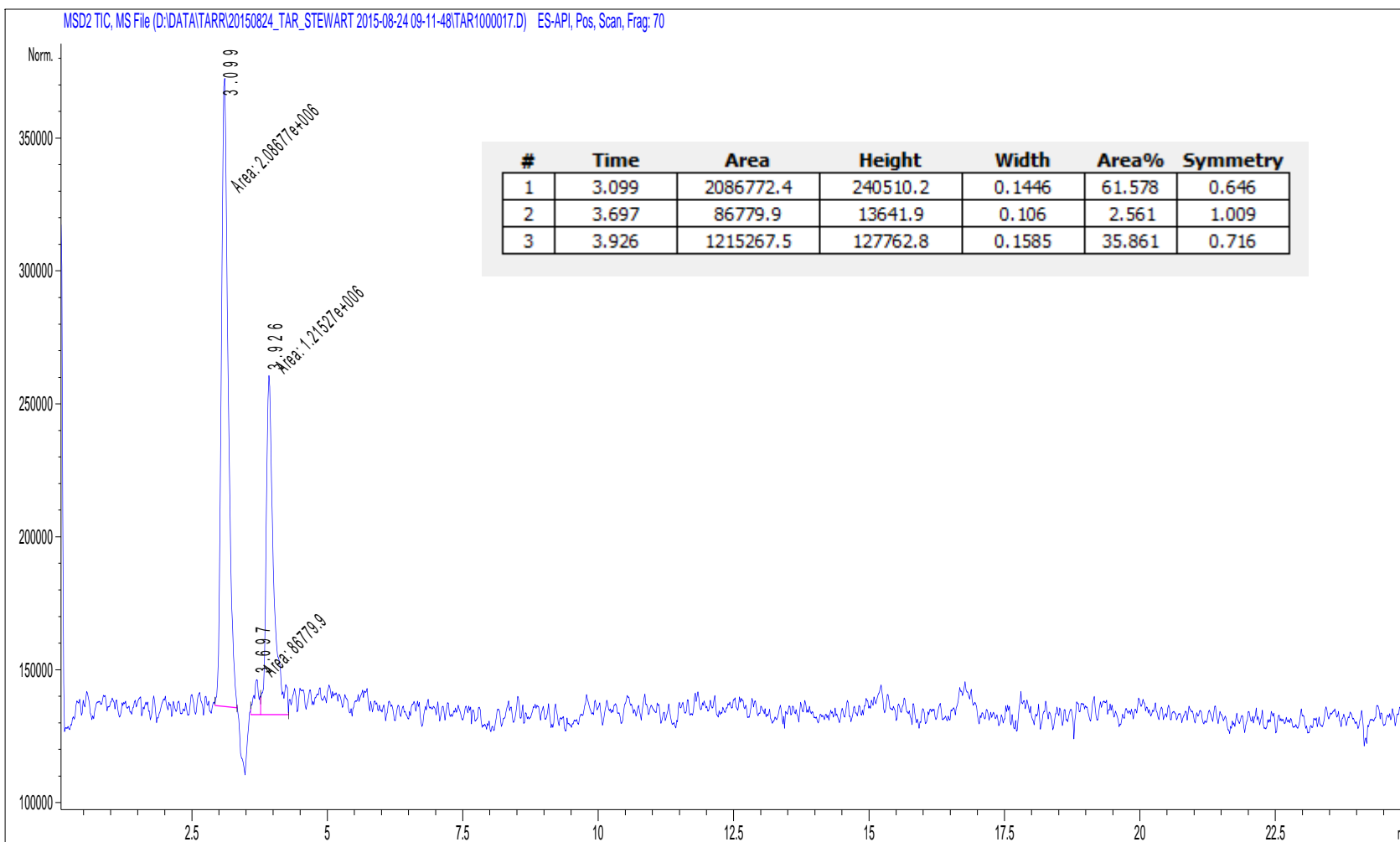


Max: 37976

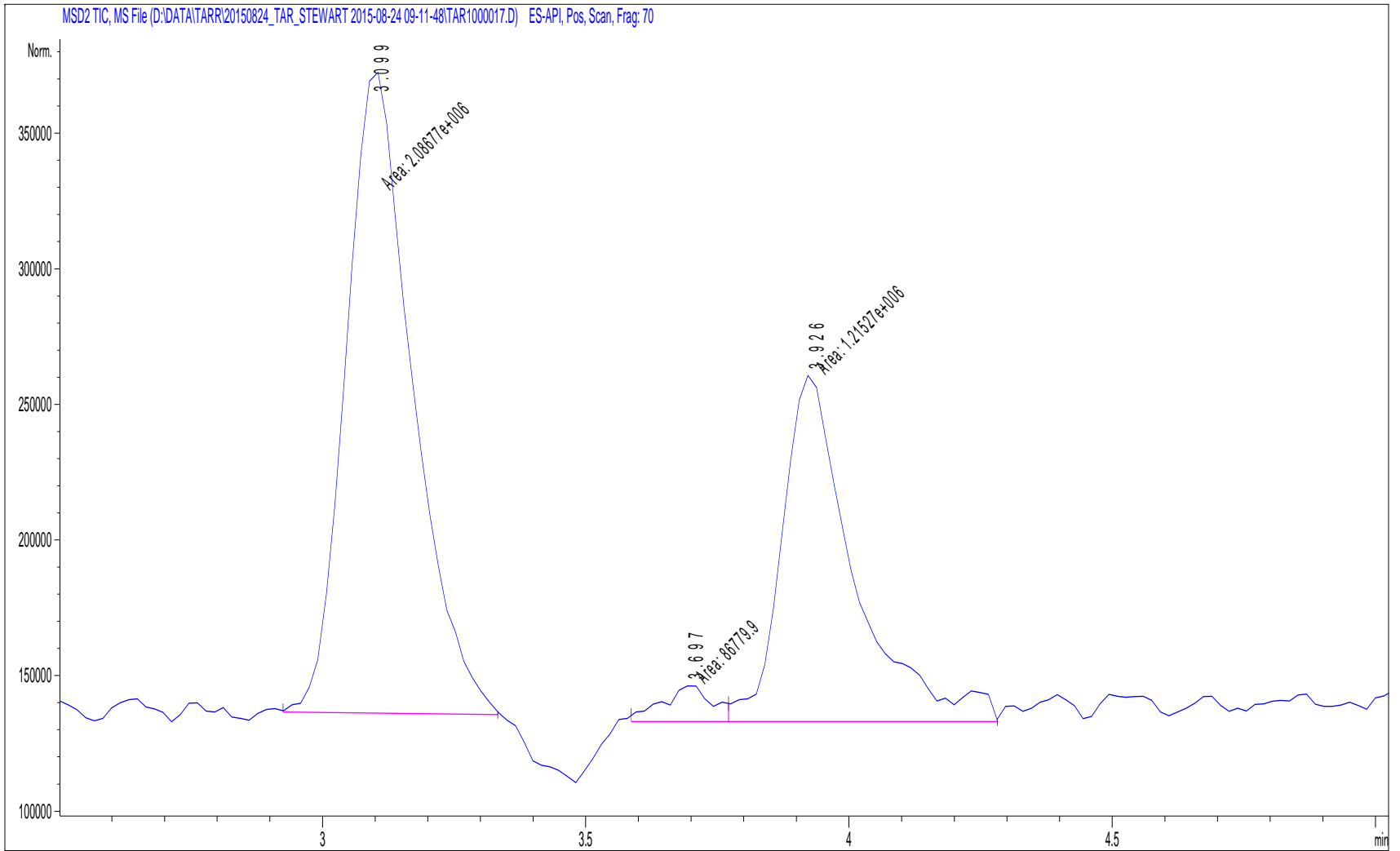
27-May-15

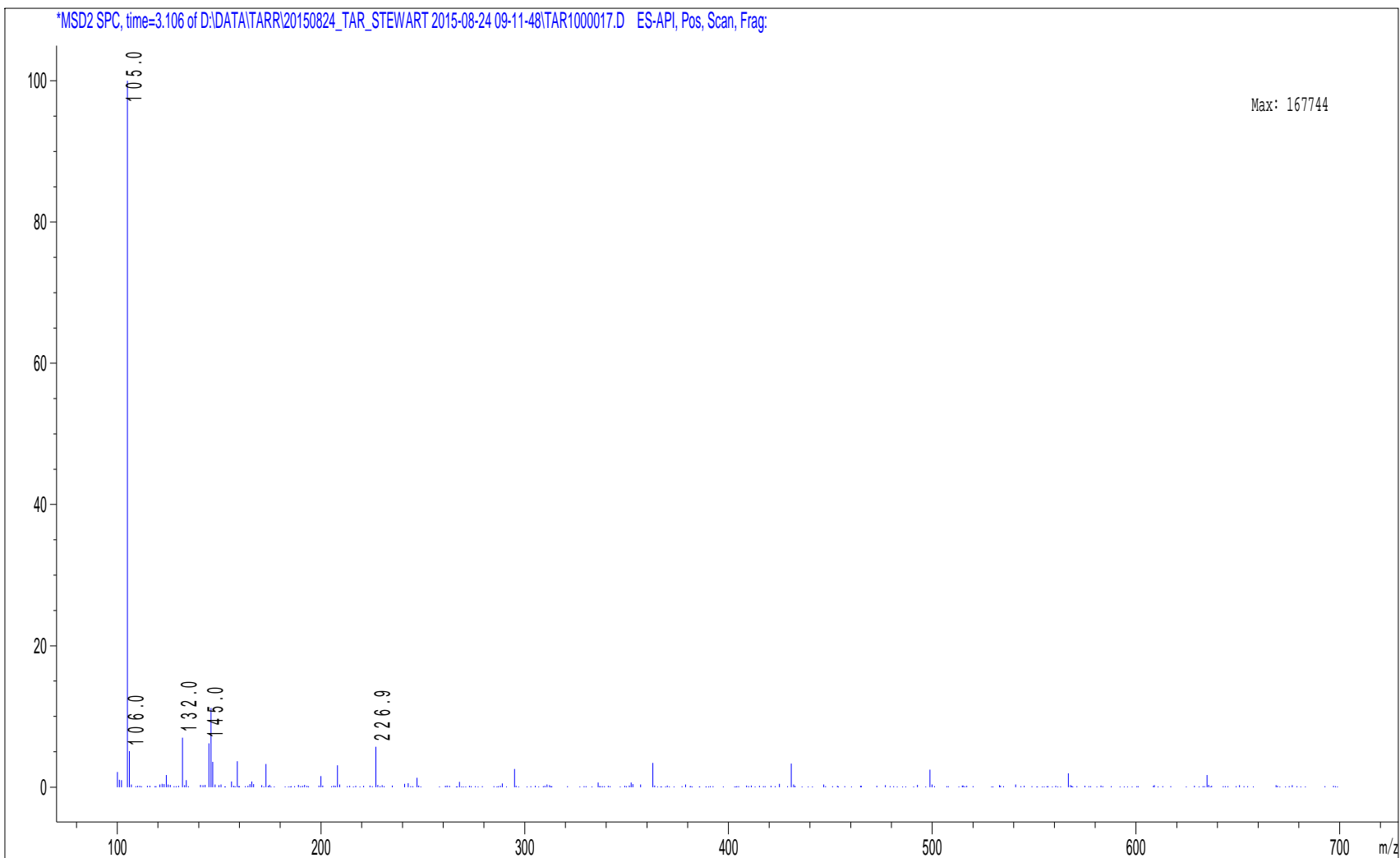
10 DC

P2-B-02

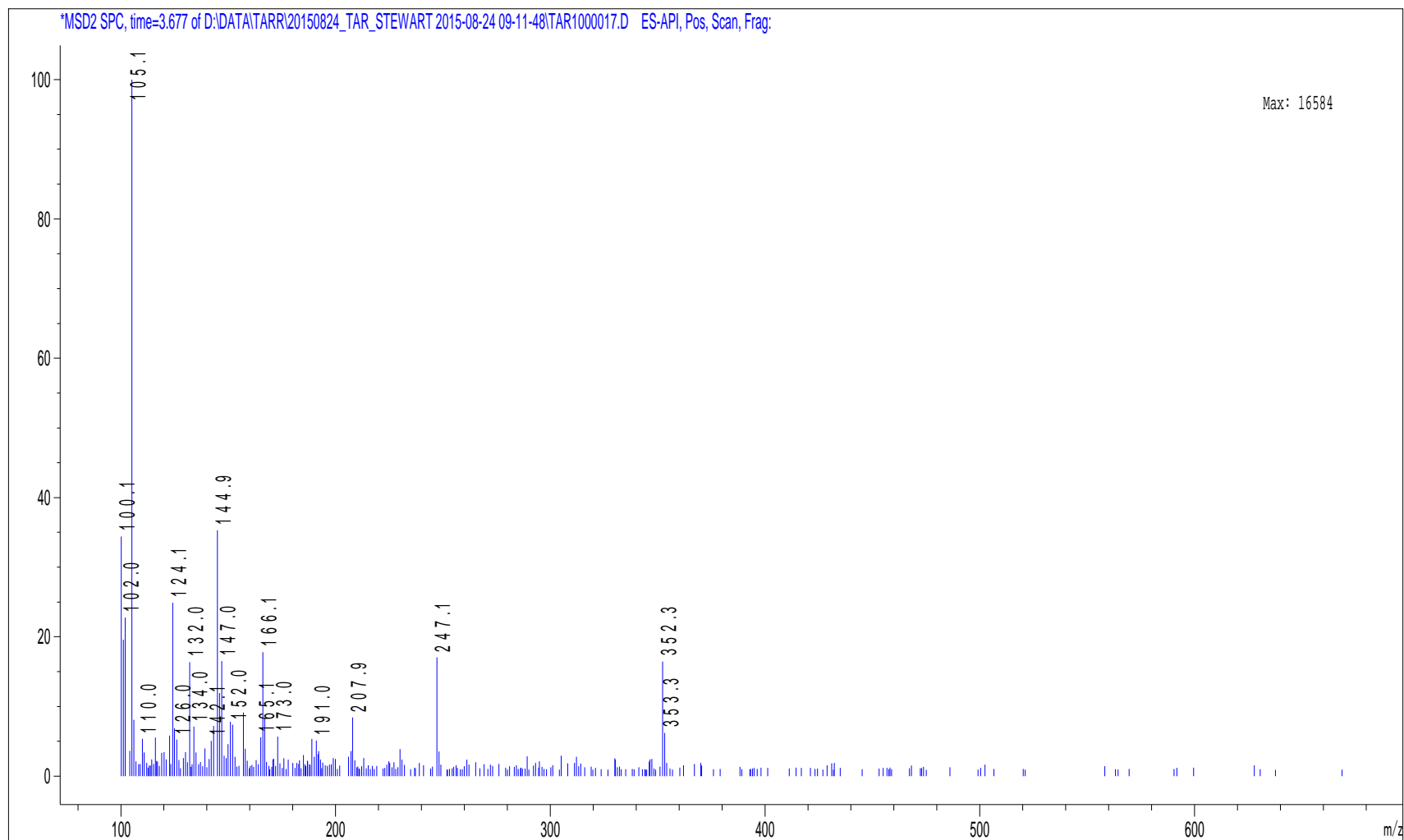




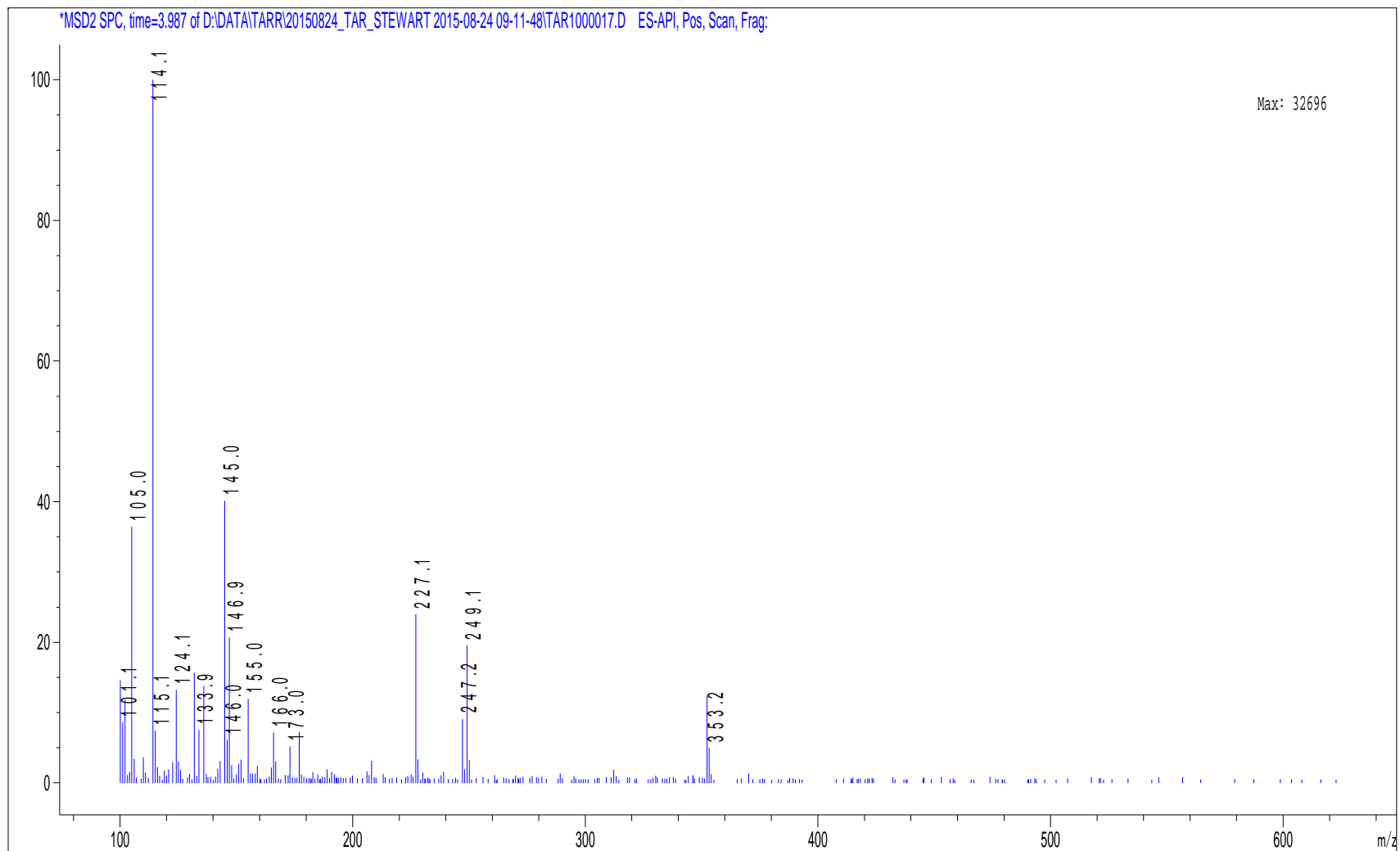




\*MSD2 SPC, time=3.677 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000017.D ES-API, Pos, Scan, Frag:



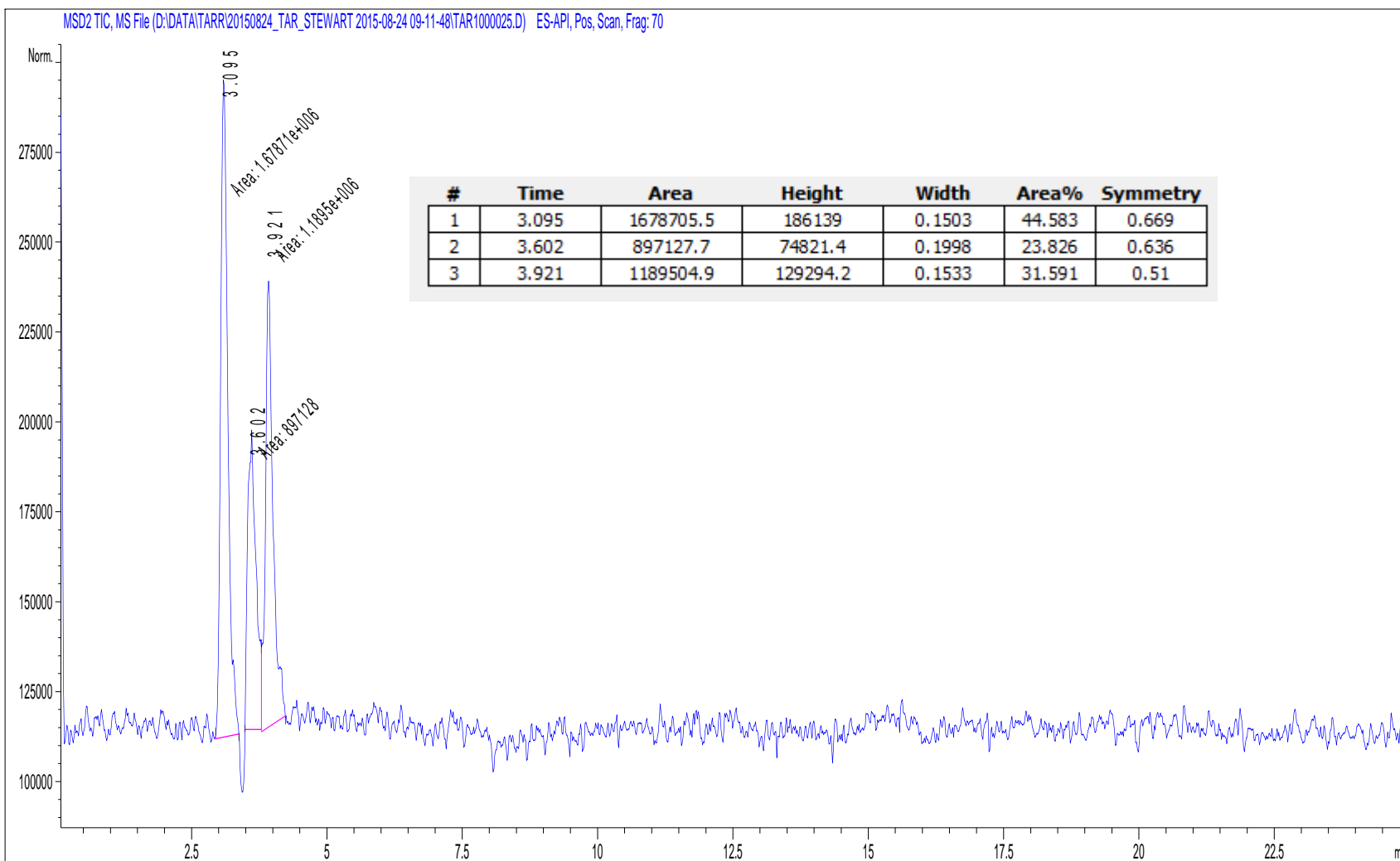
Max: 16584

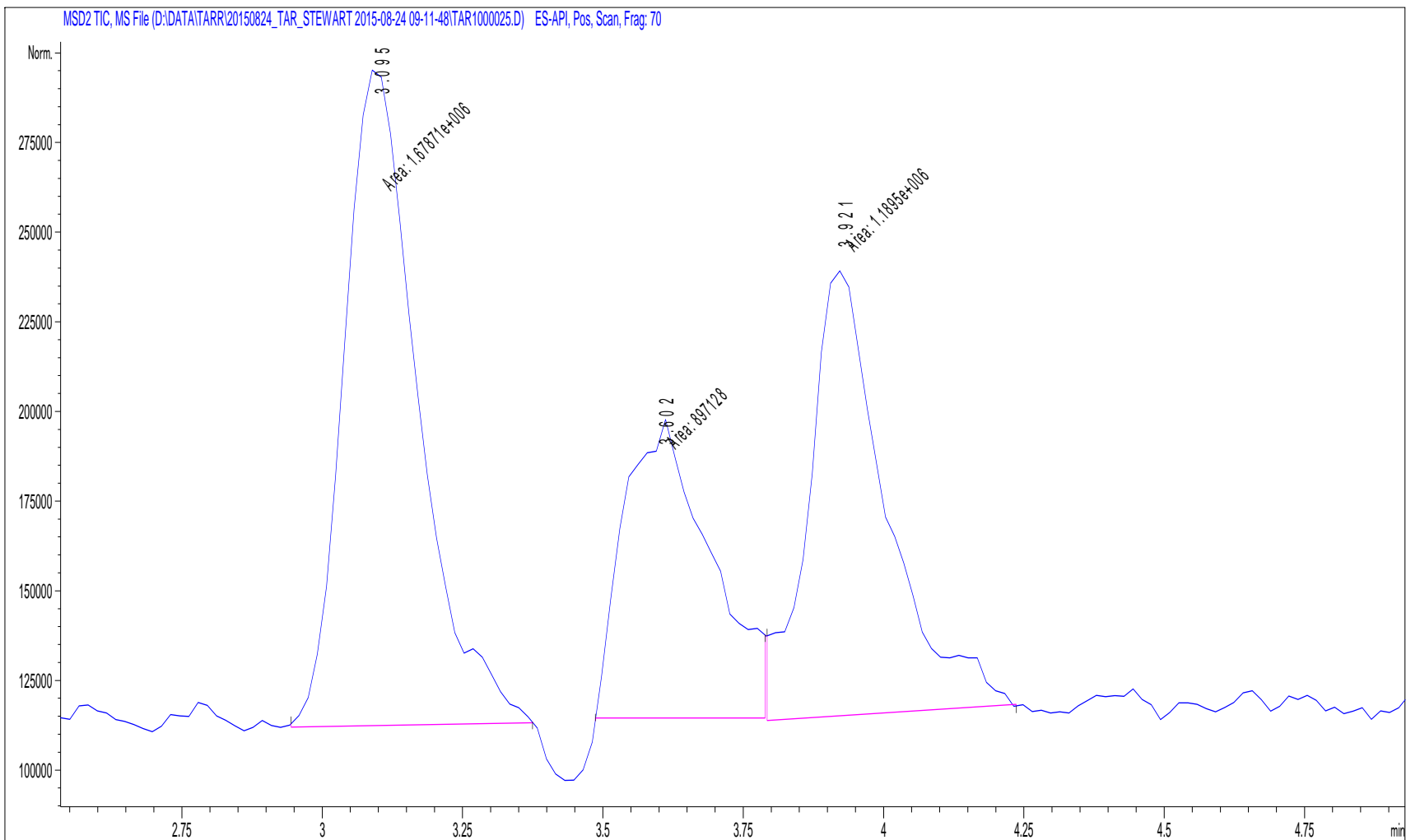


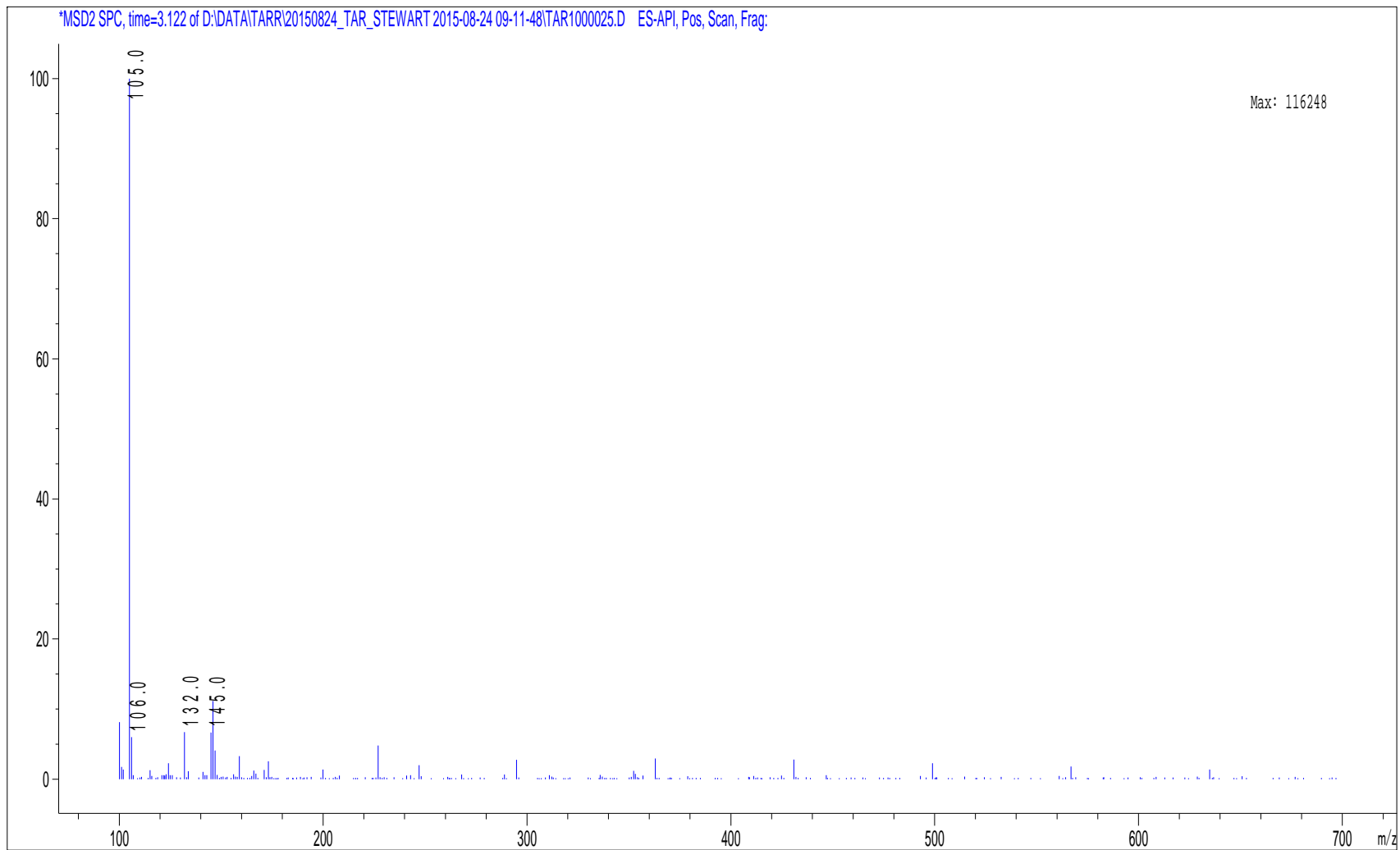
10-Jul-15

20 DC

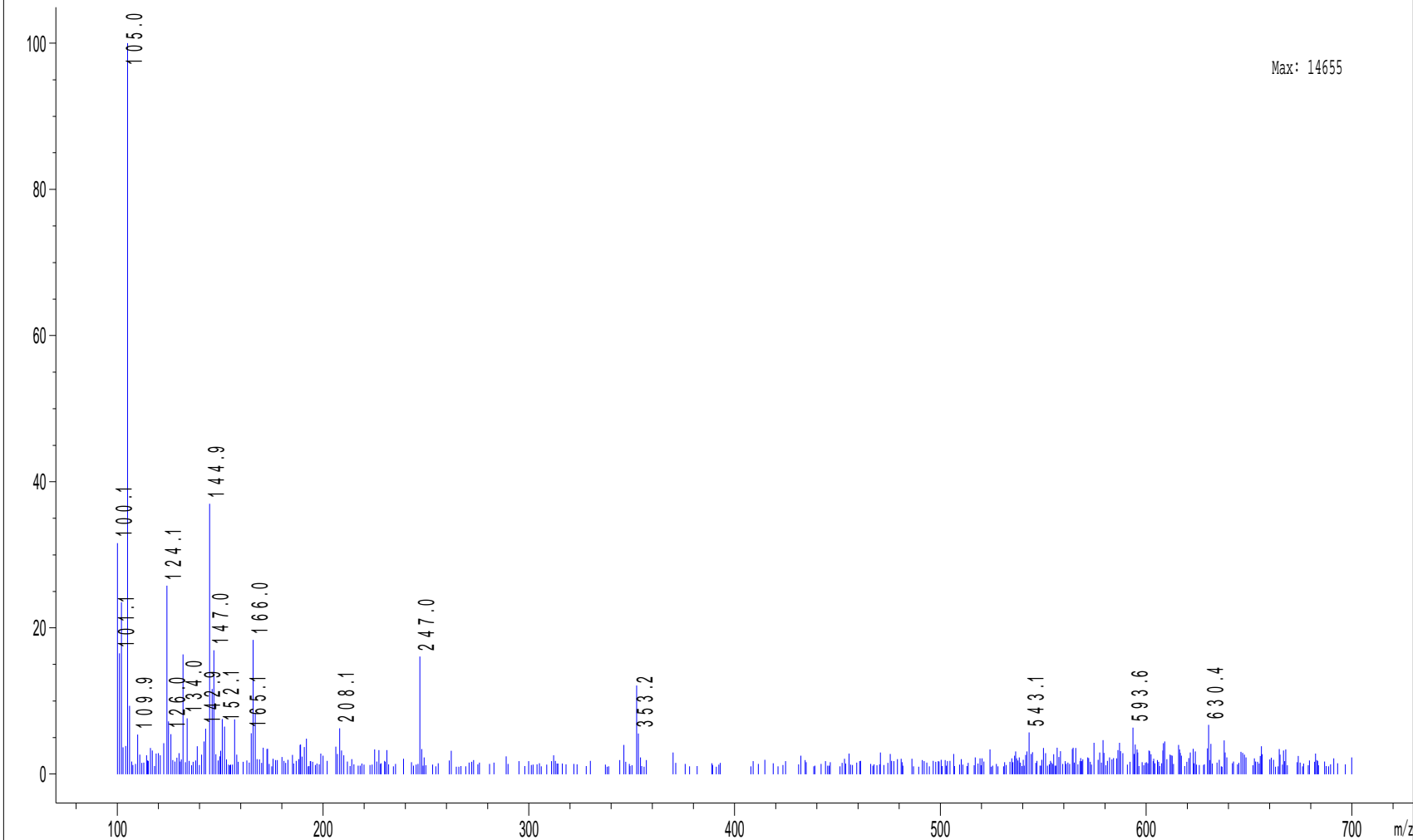
P2-C-07



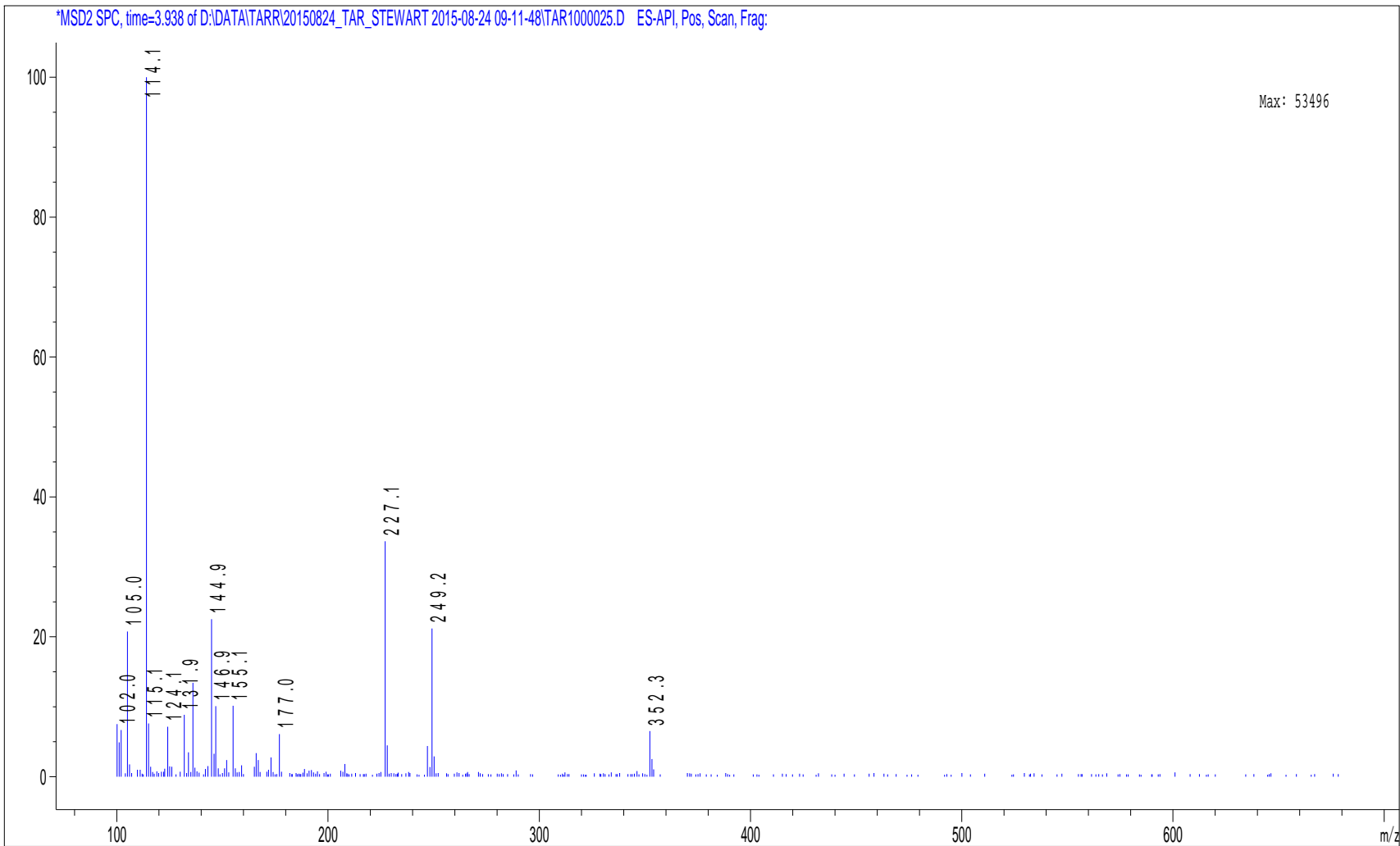




\*MSD2 SPC, time=3.628 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000025.D ES-API, Pos, Scan, Frag:



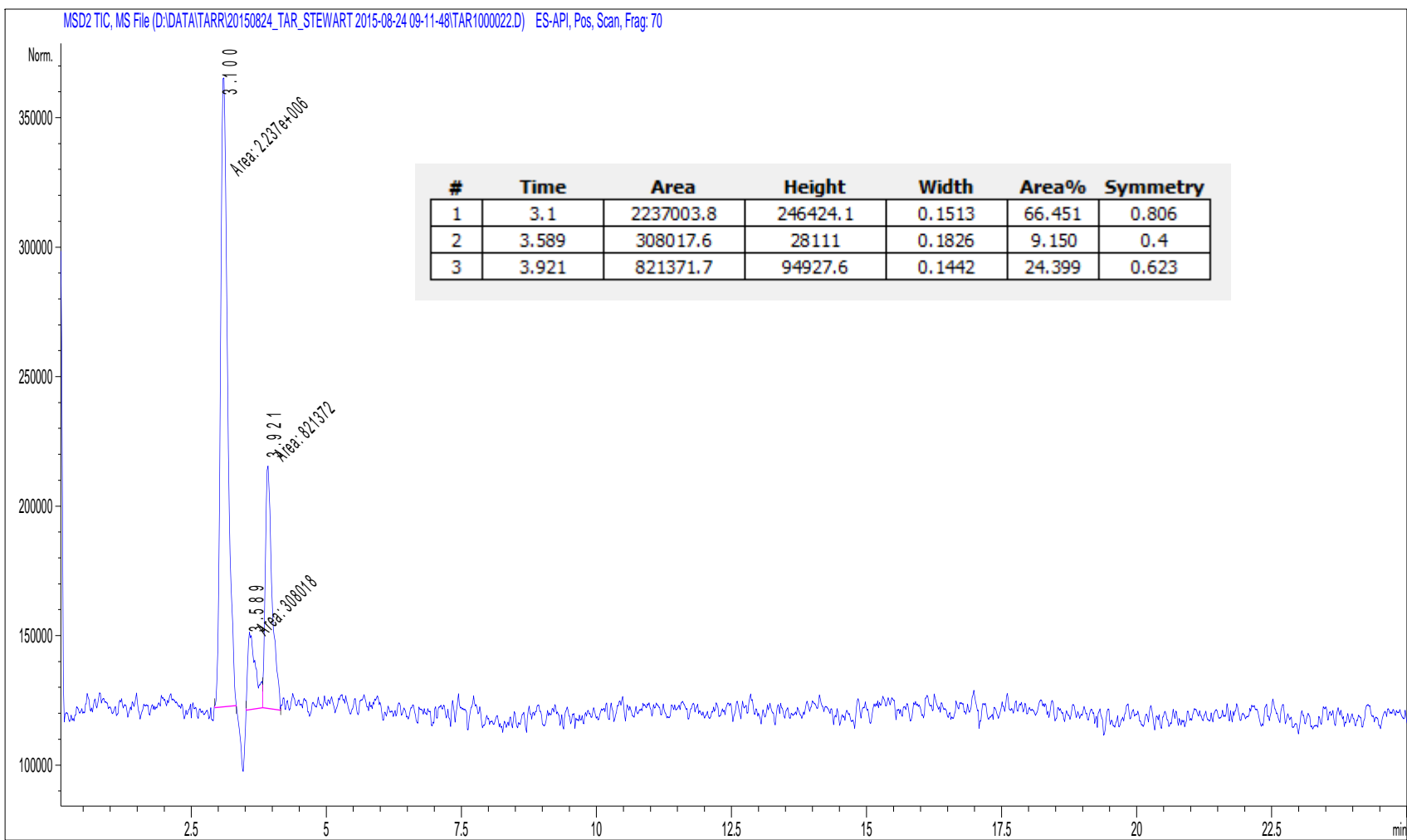


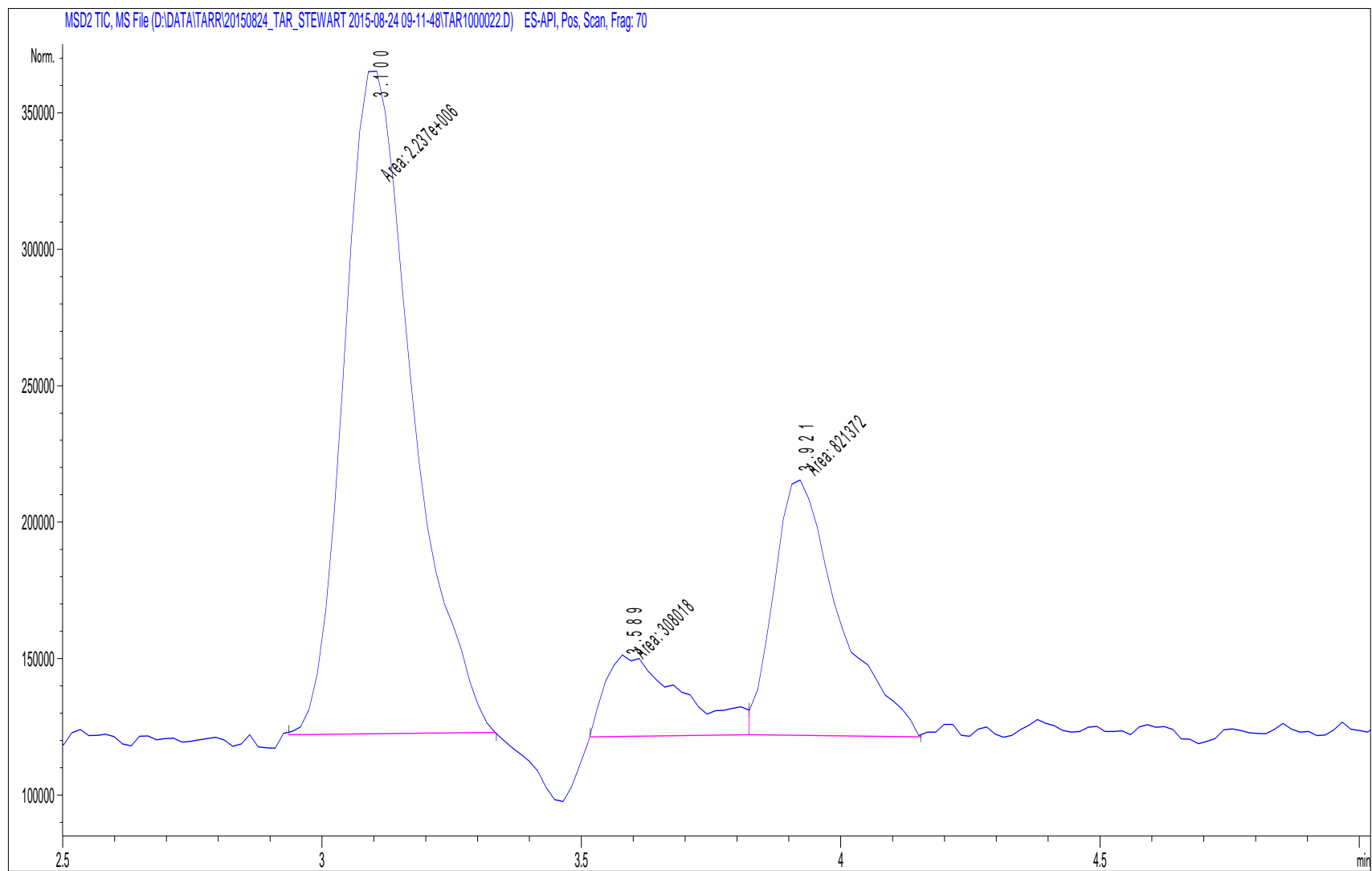


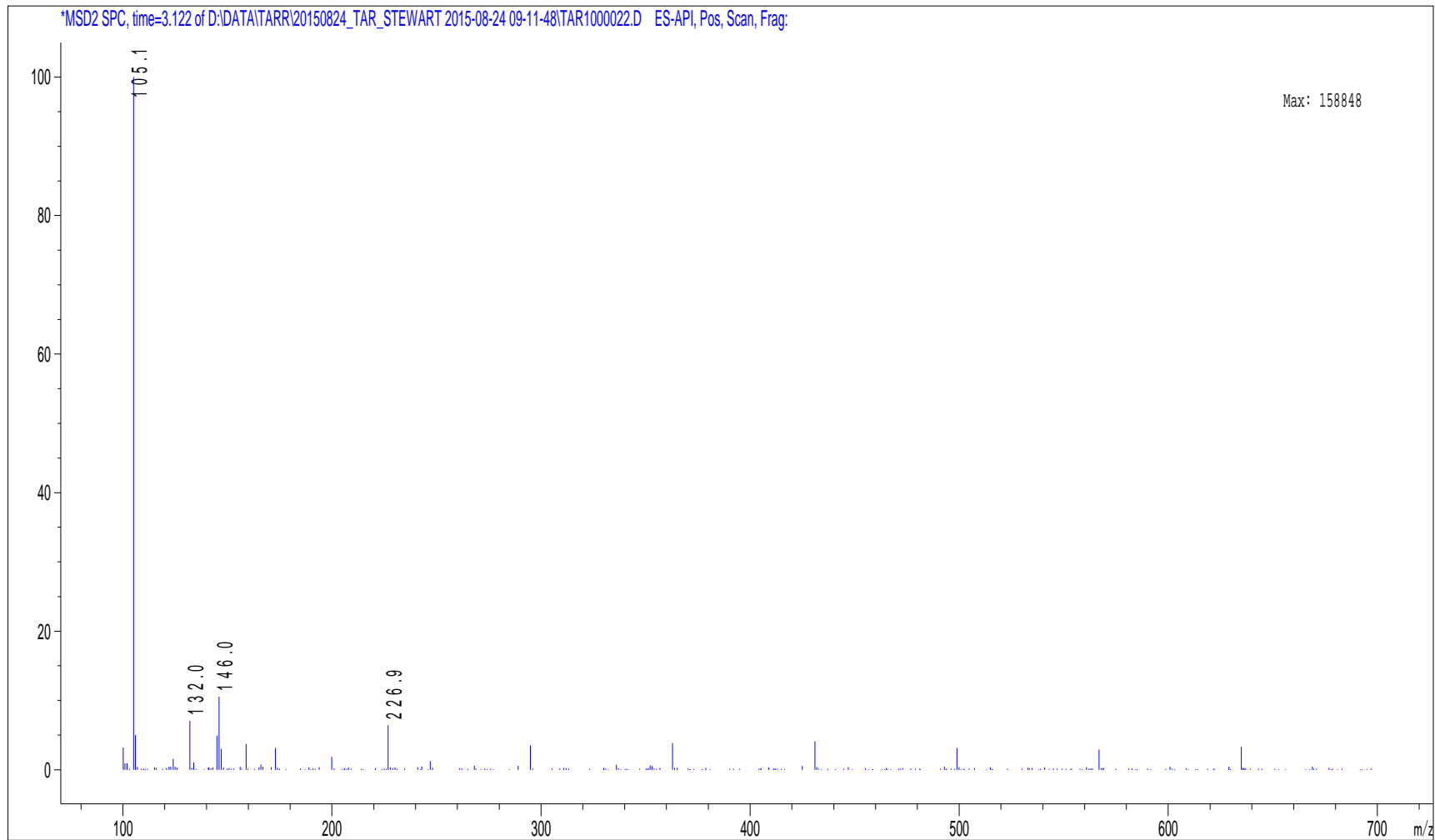
2-Jul-15

30 DC

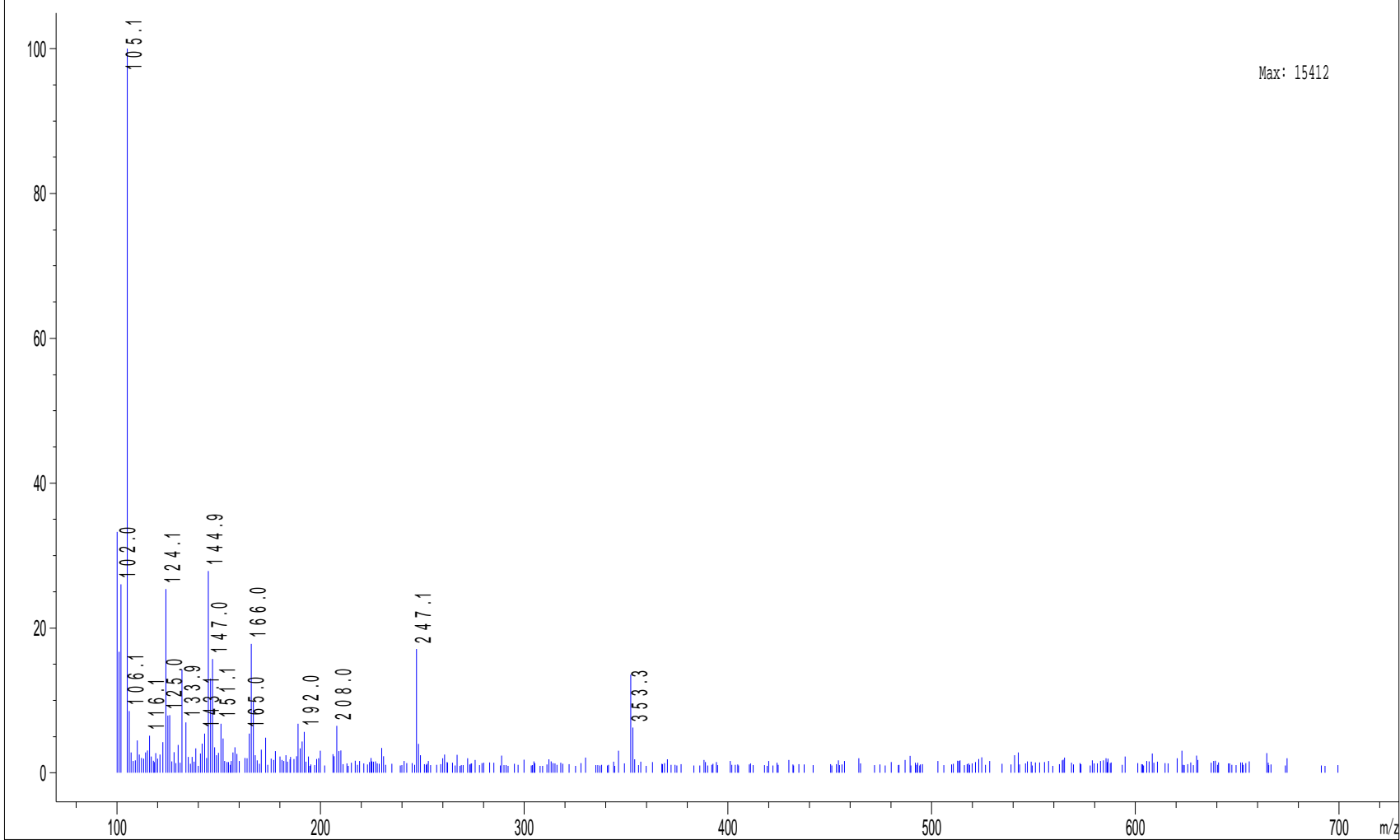
P2-C-04



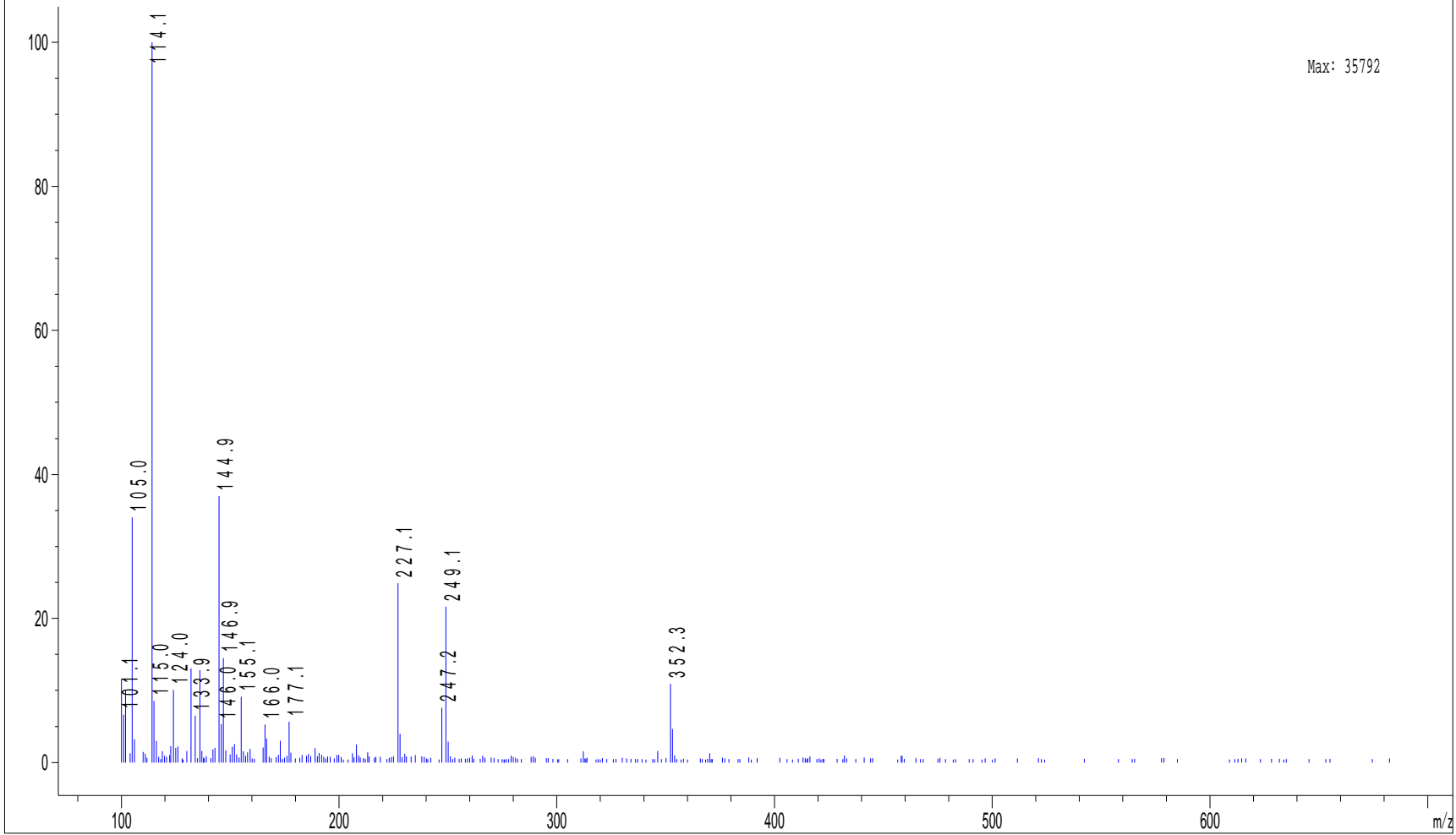




\*MSD2 SPC, time=3.628 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000022.D ES-API, Pos, Scan, Frag:



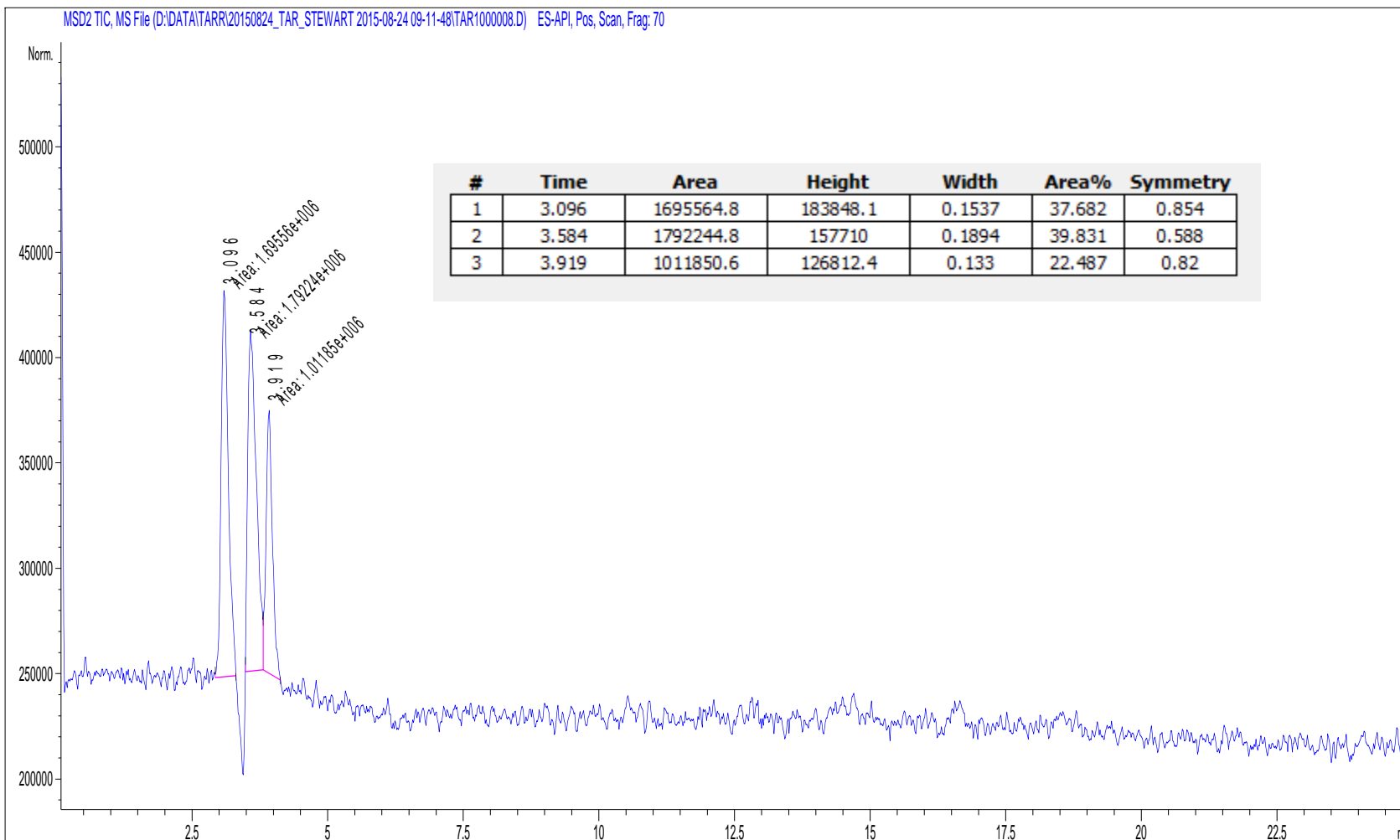
\*MSD2 SPC, time=3.955 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000022.D ES-API, Pos, Scan, Frag:

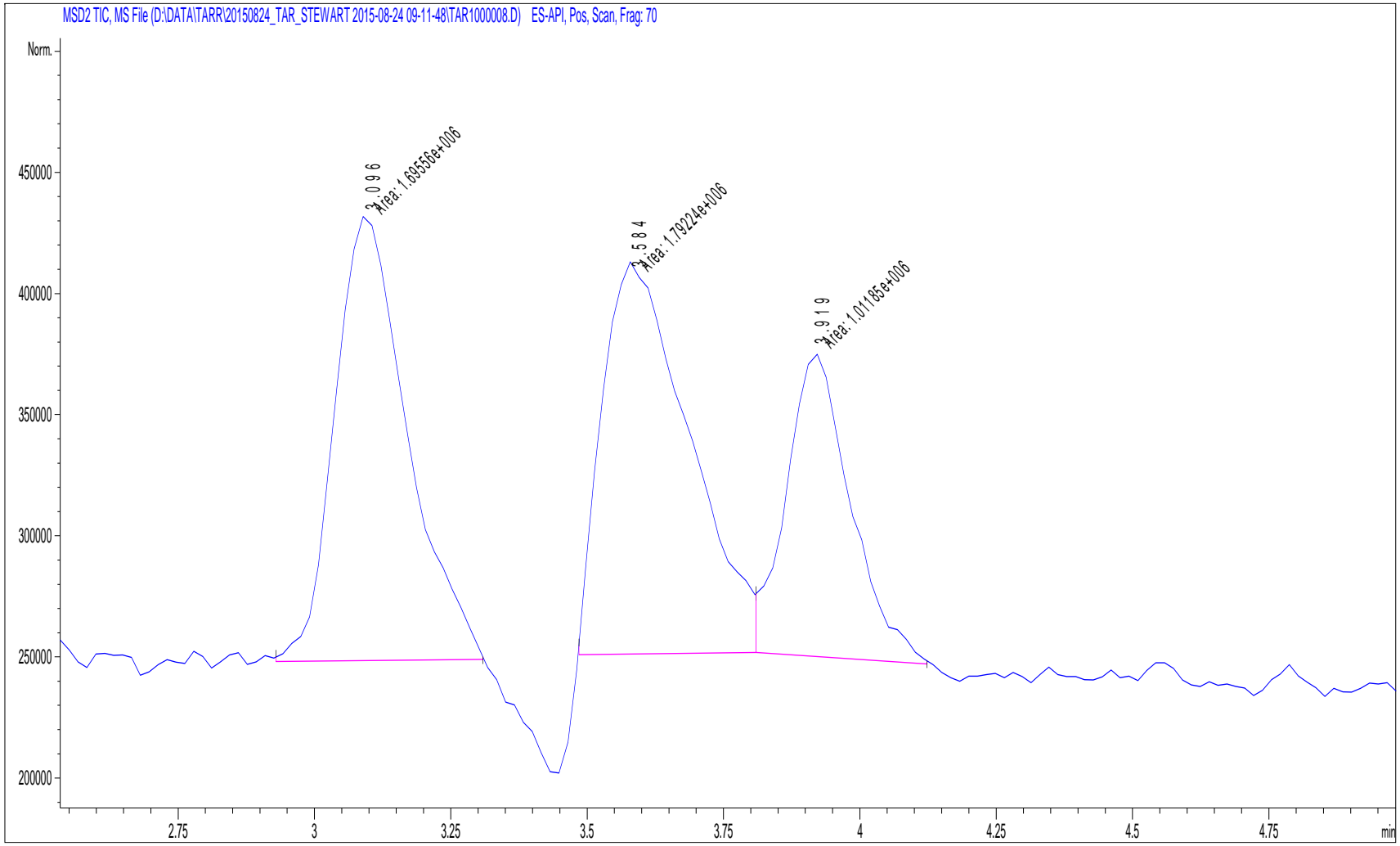


23-Apr-15

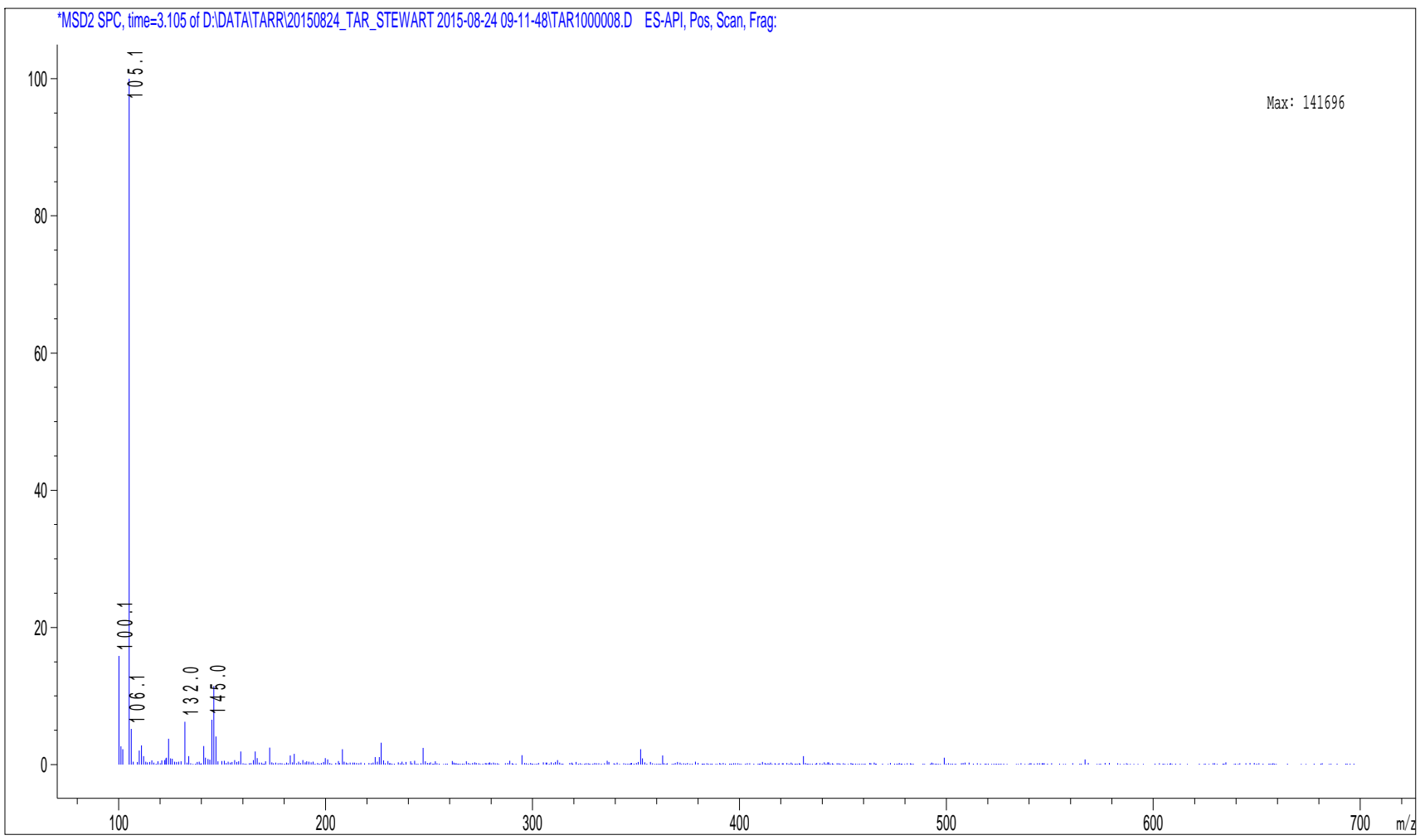
50 DC

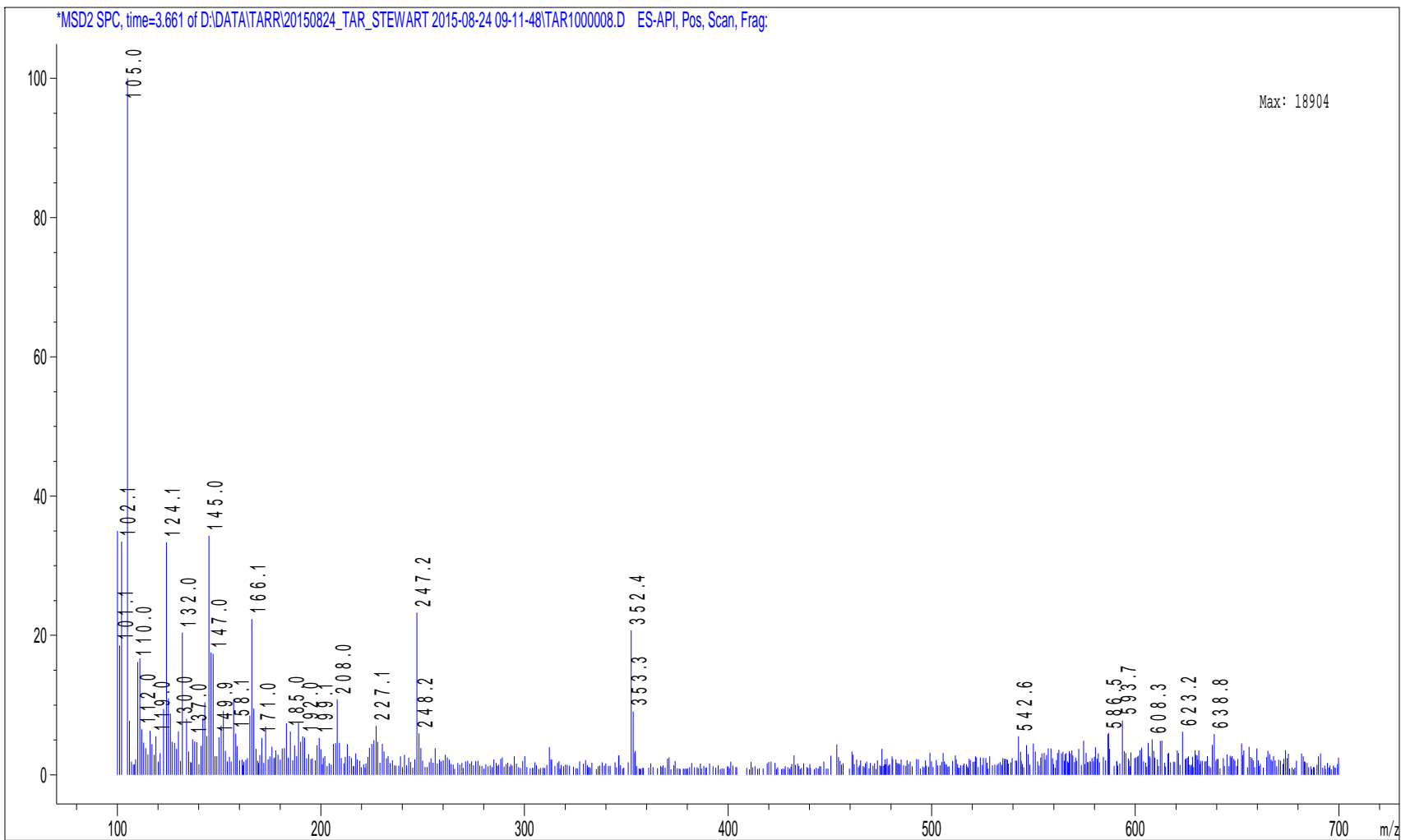
P2-A-08

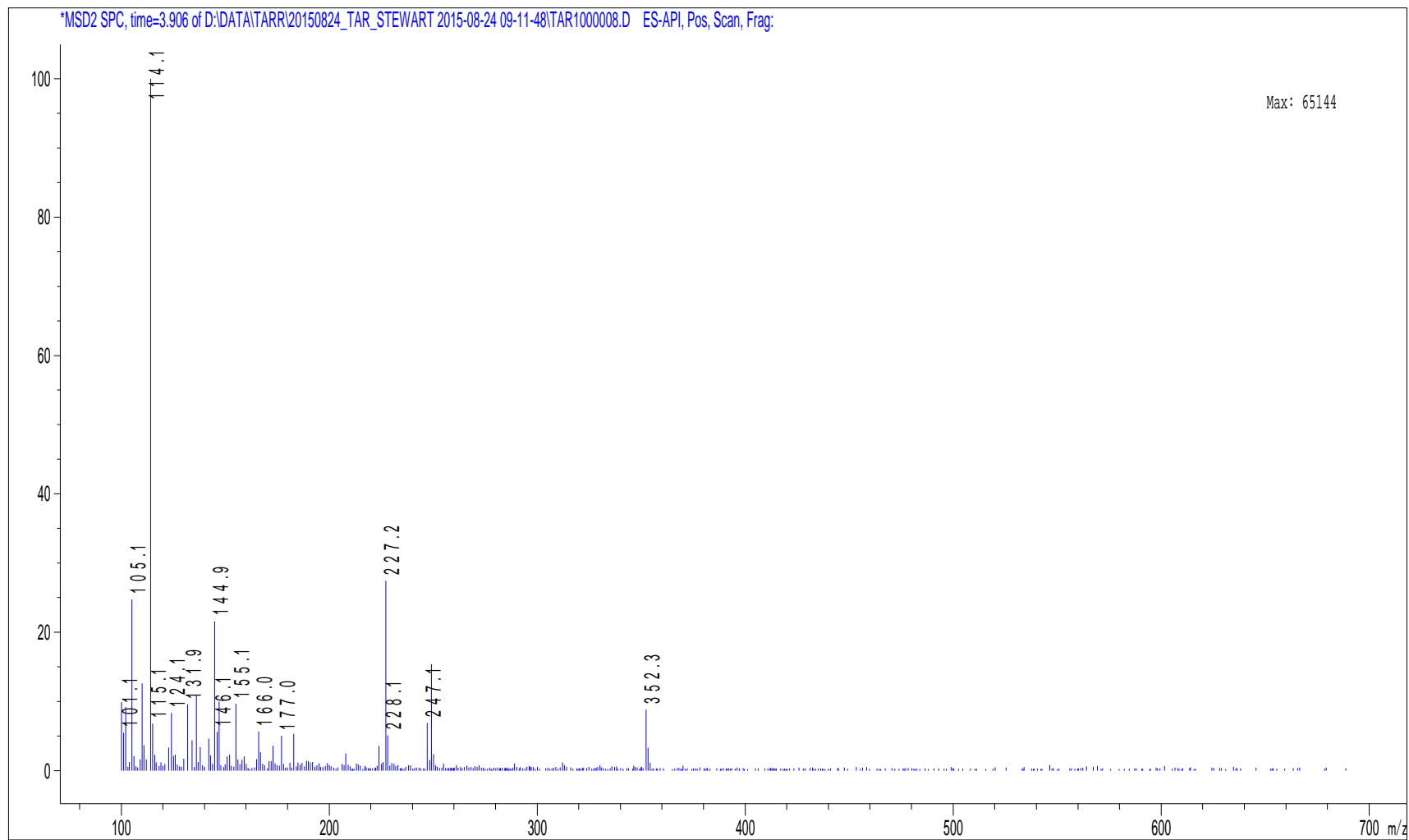








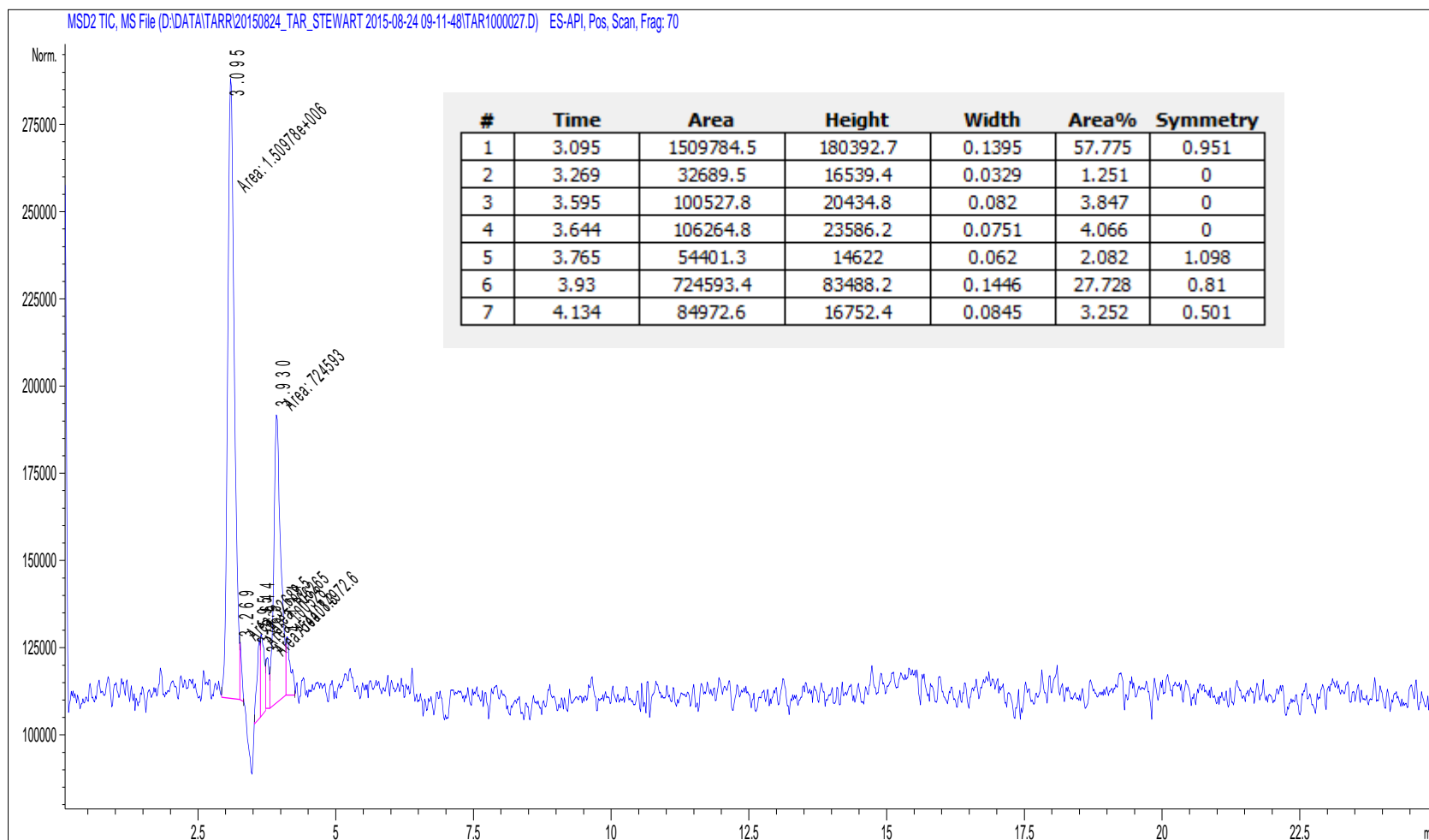


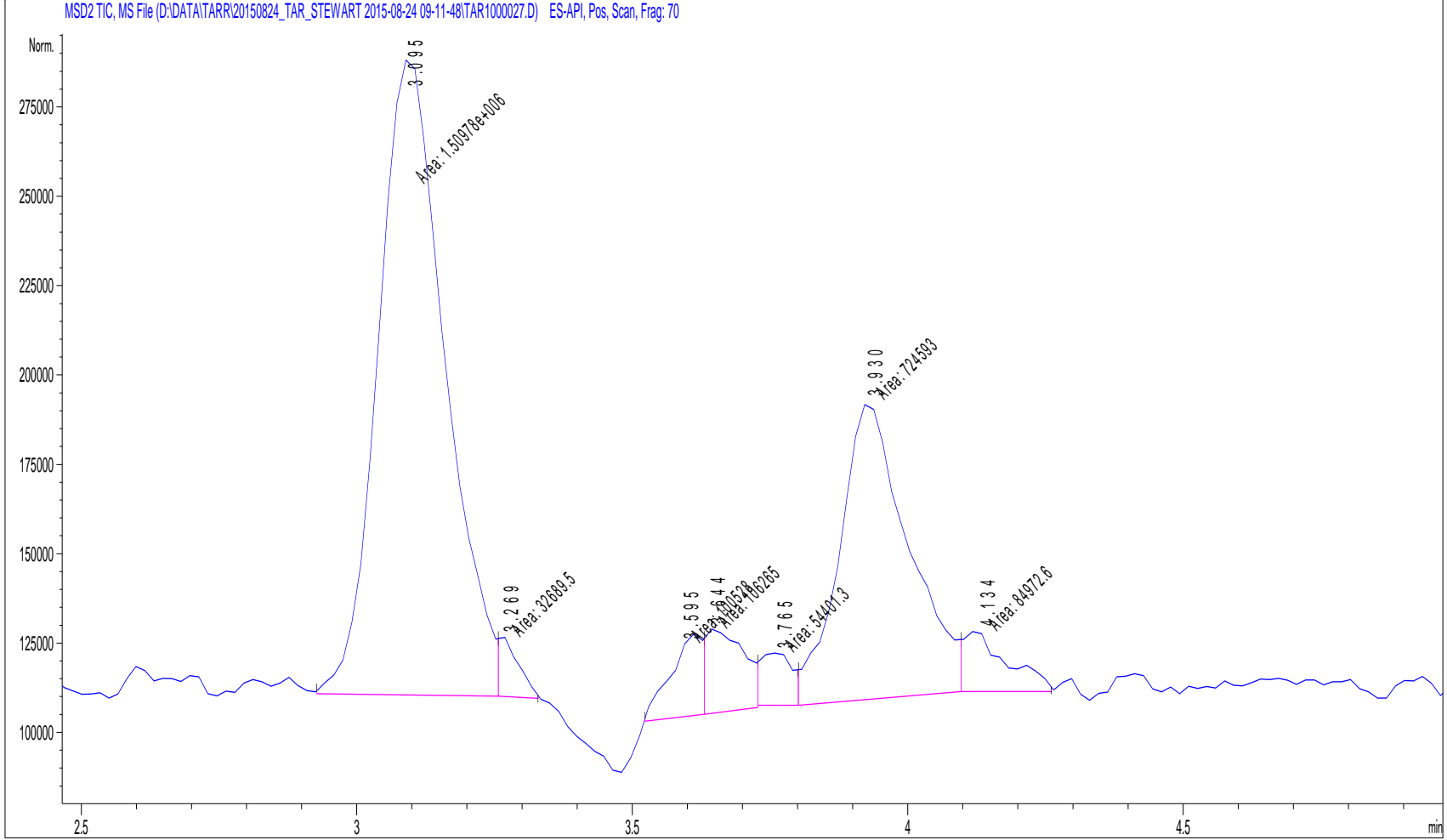


9-Jul-15

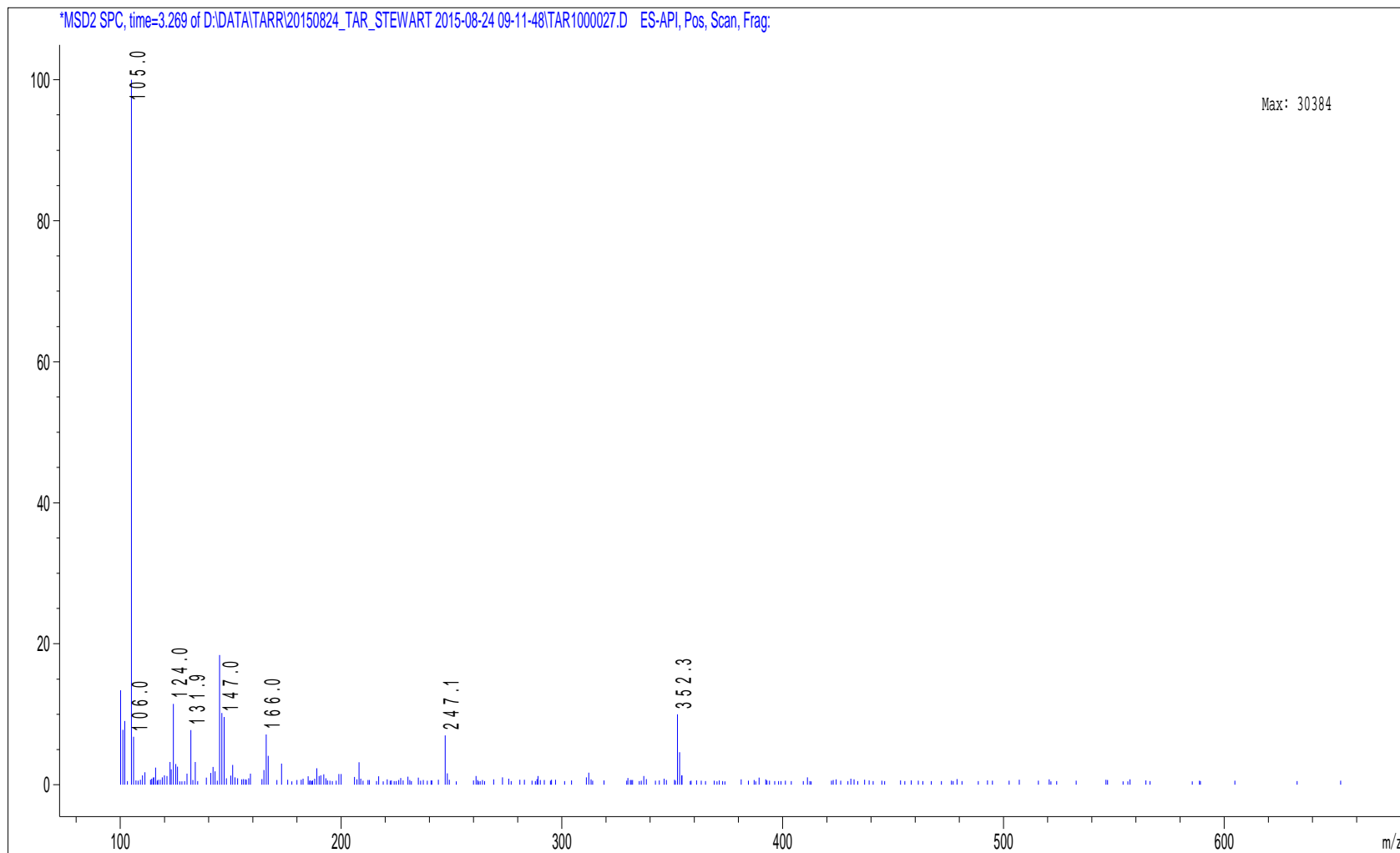
70 DC

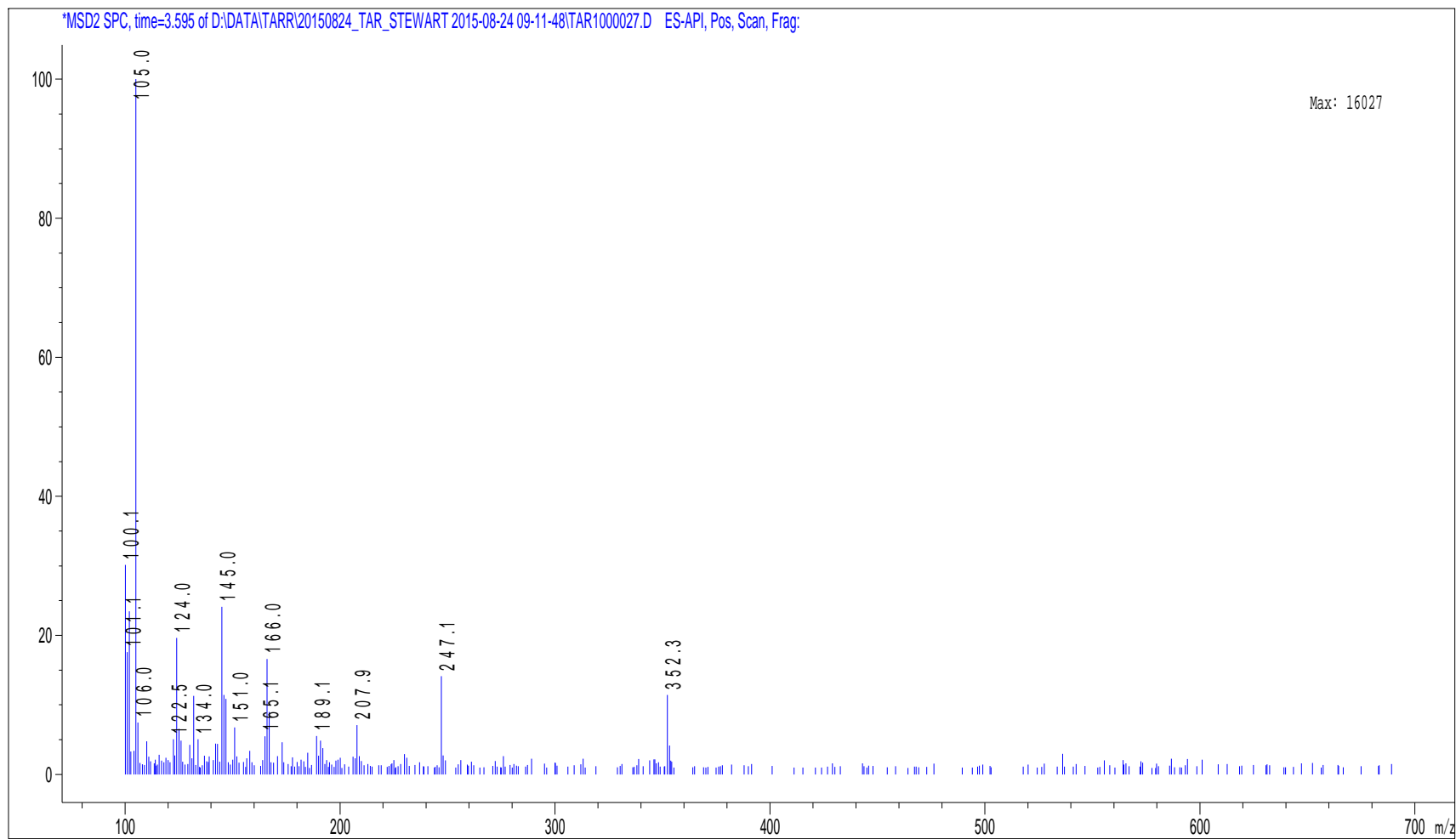
P2-C-09



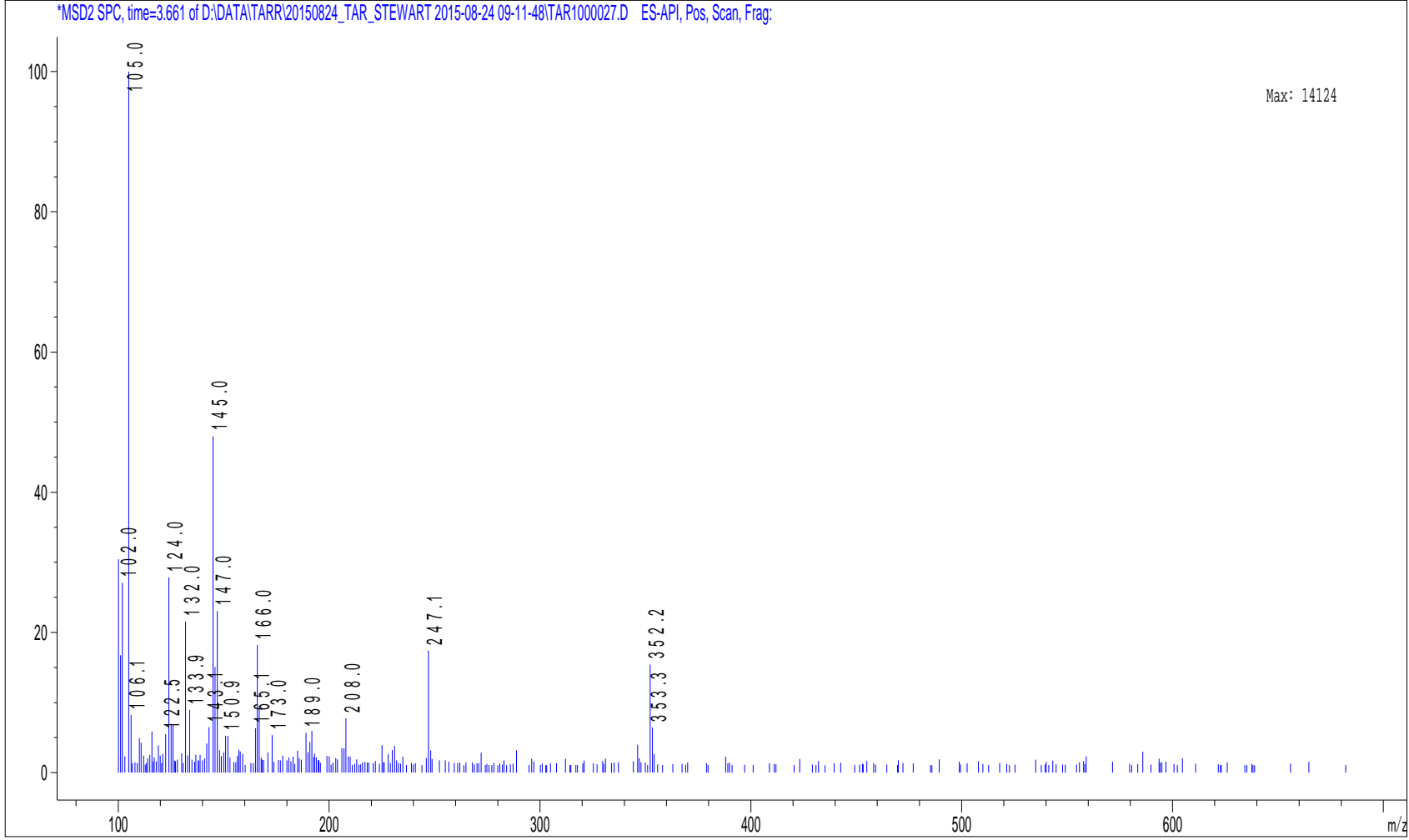




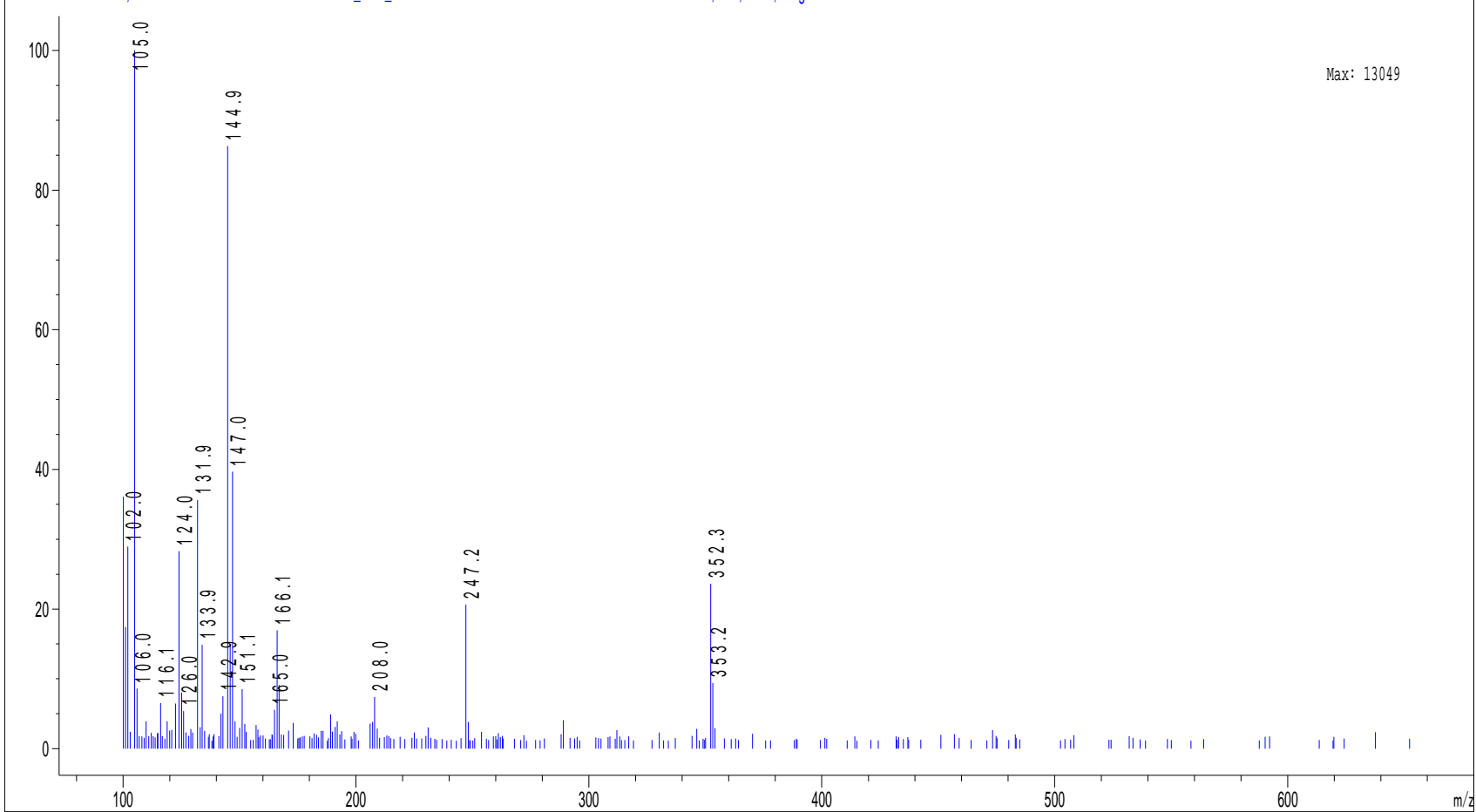




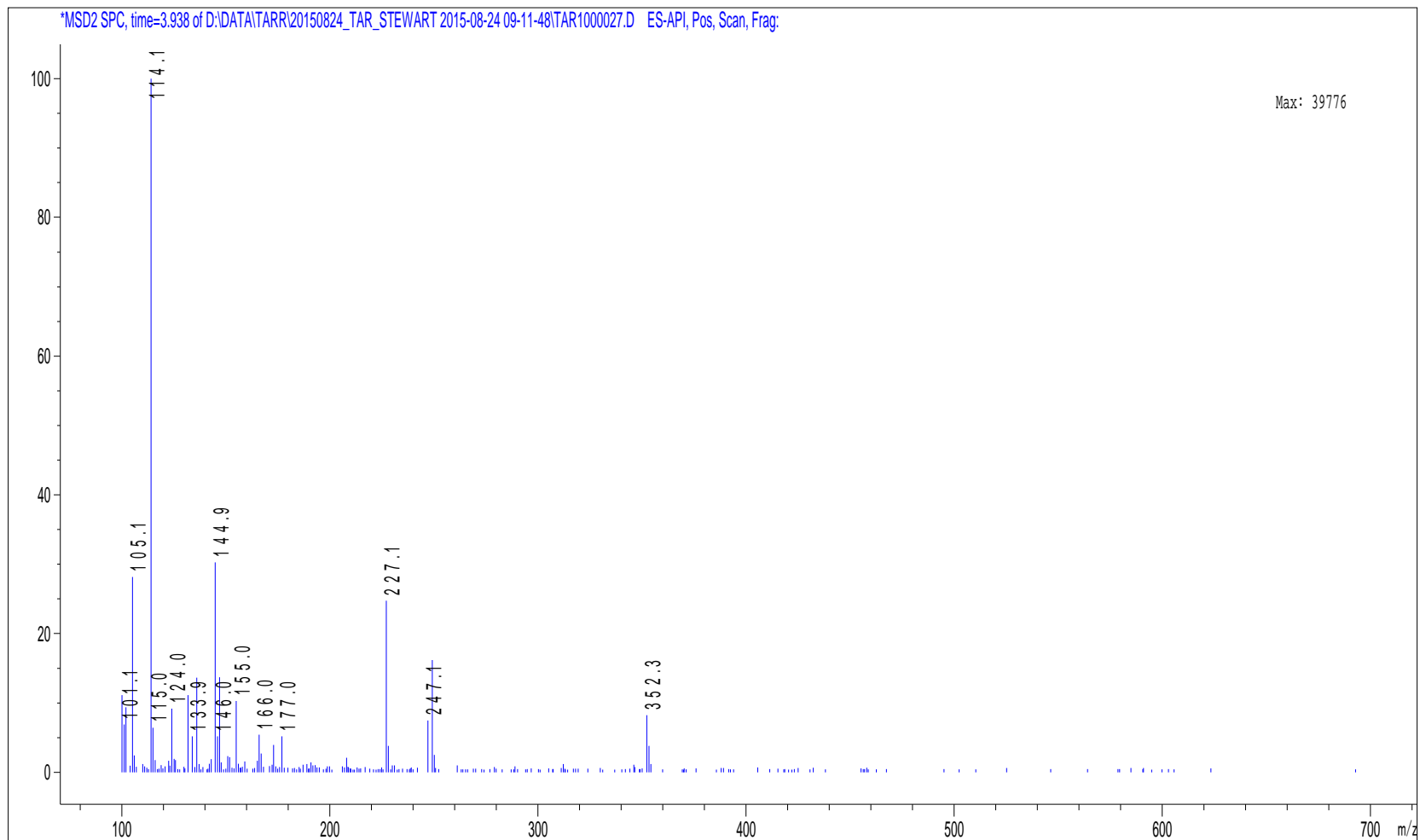




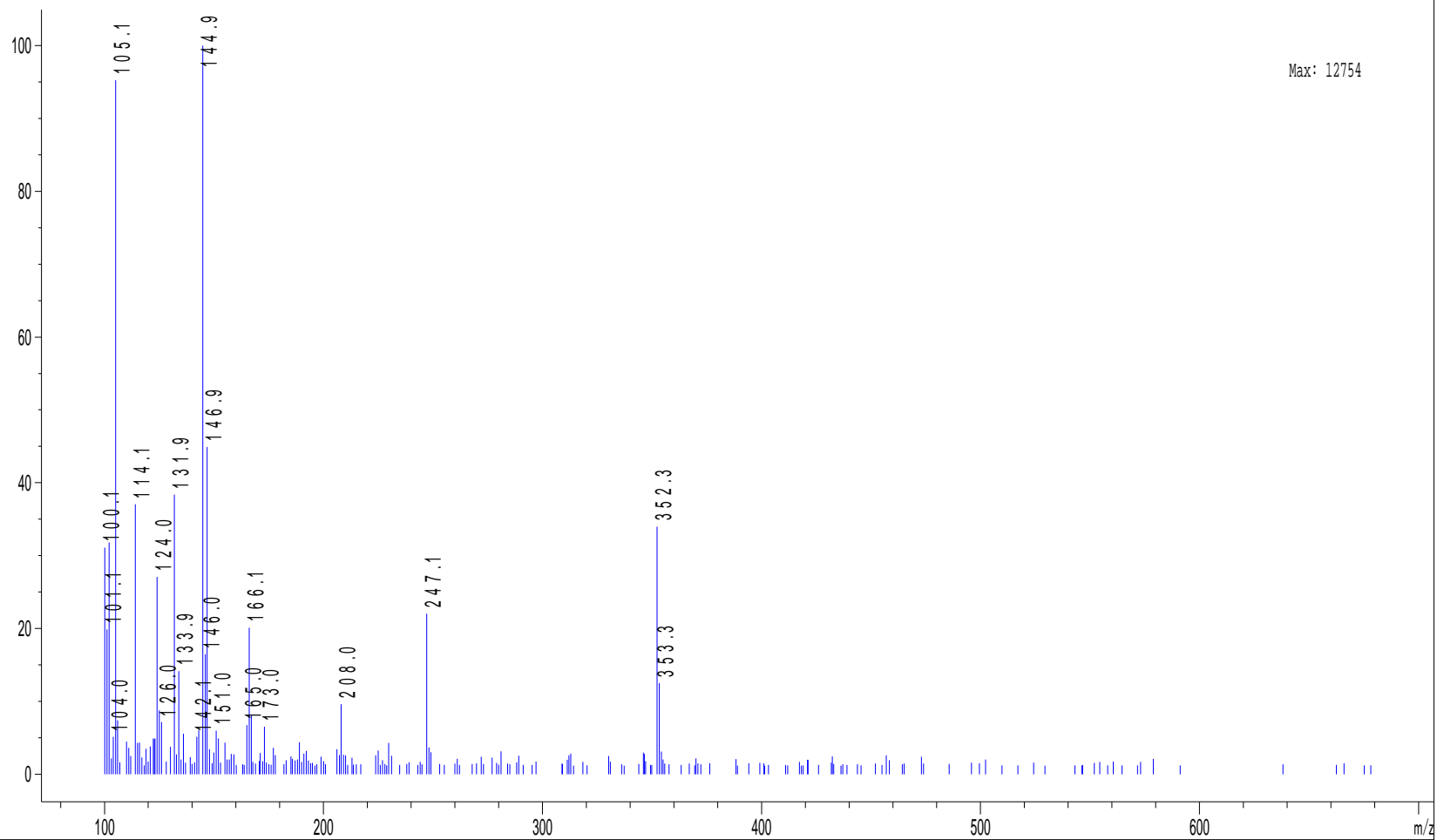
\*MSD2 SPC, time=3.759 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000027.D ES-API, Pos, Scan, Frag:



Max: 13049



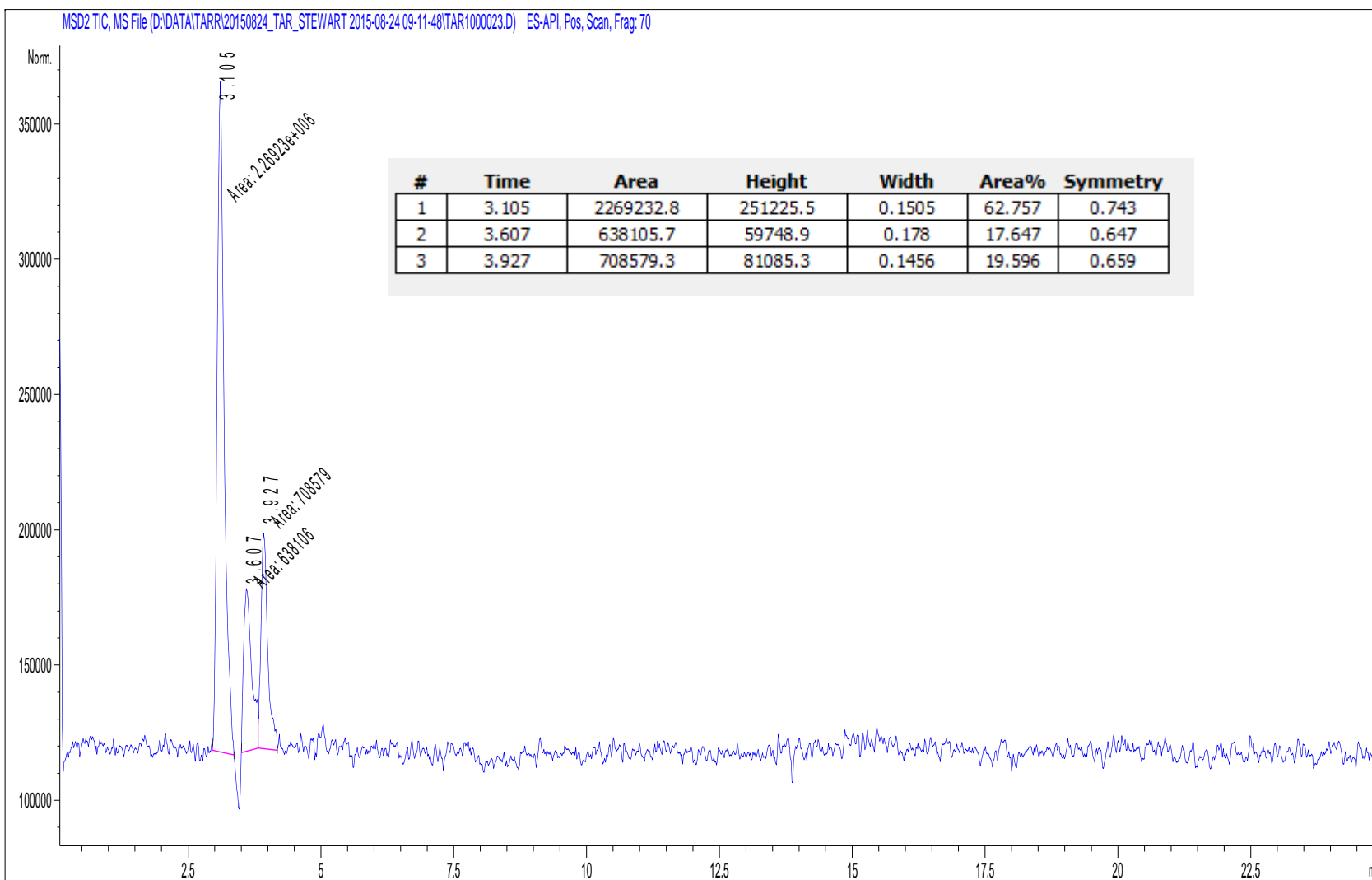
\*MSD2 SPC, time=4.118 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000027.D ES-API, Pos, Scan, Frag:

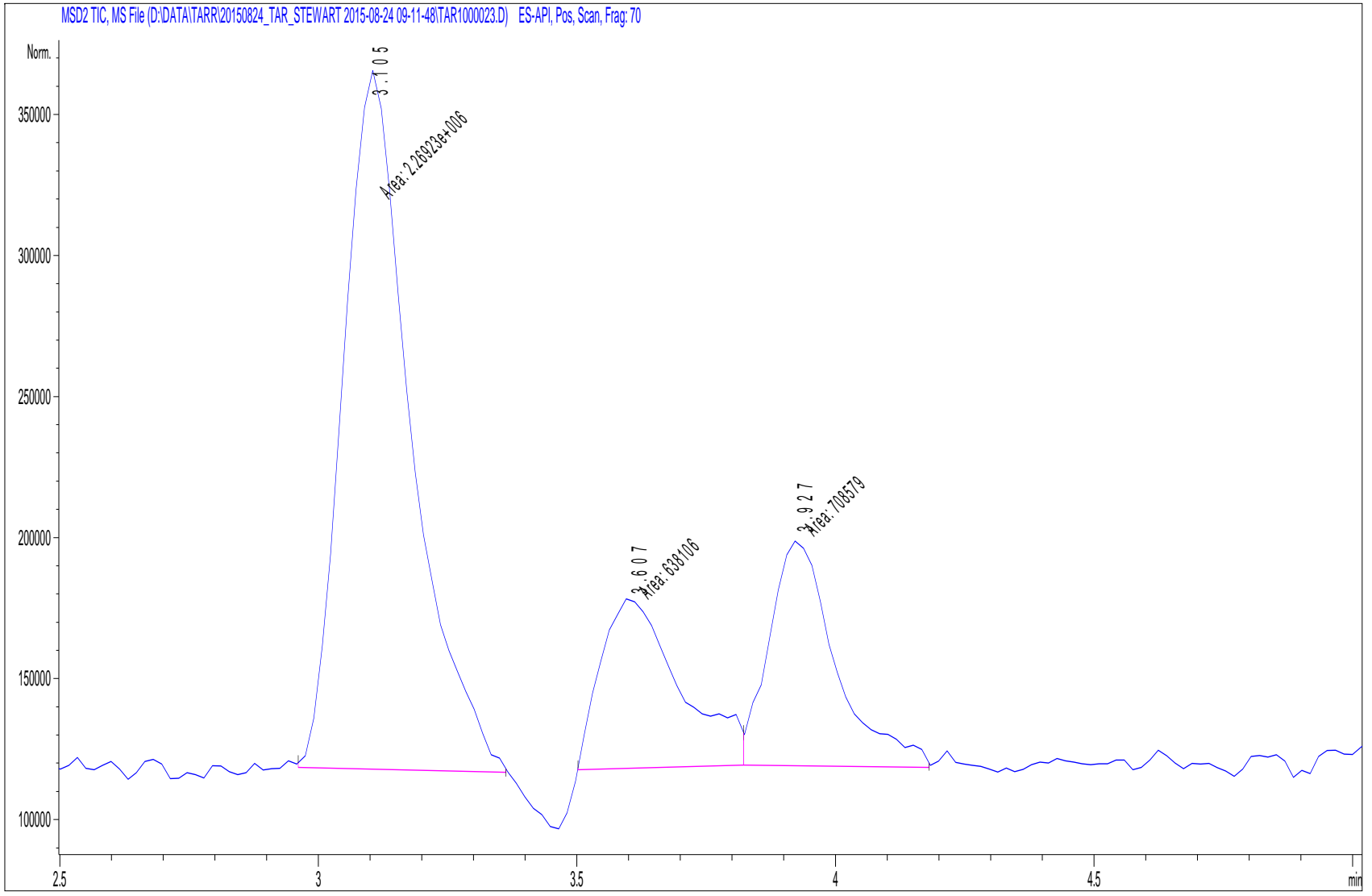


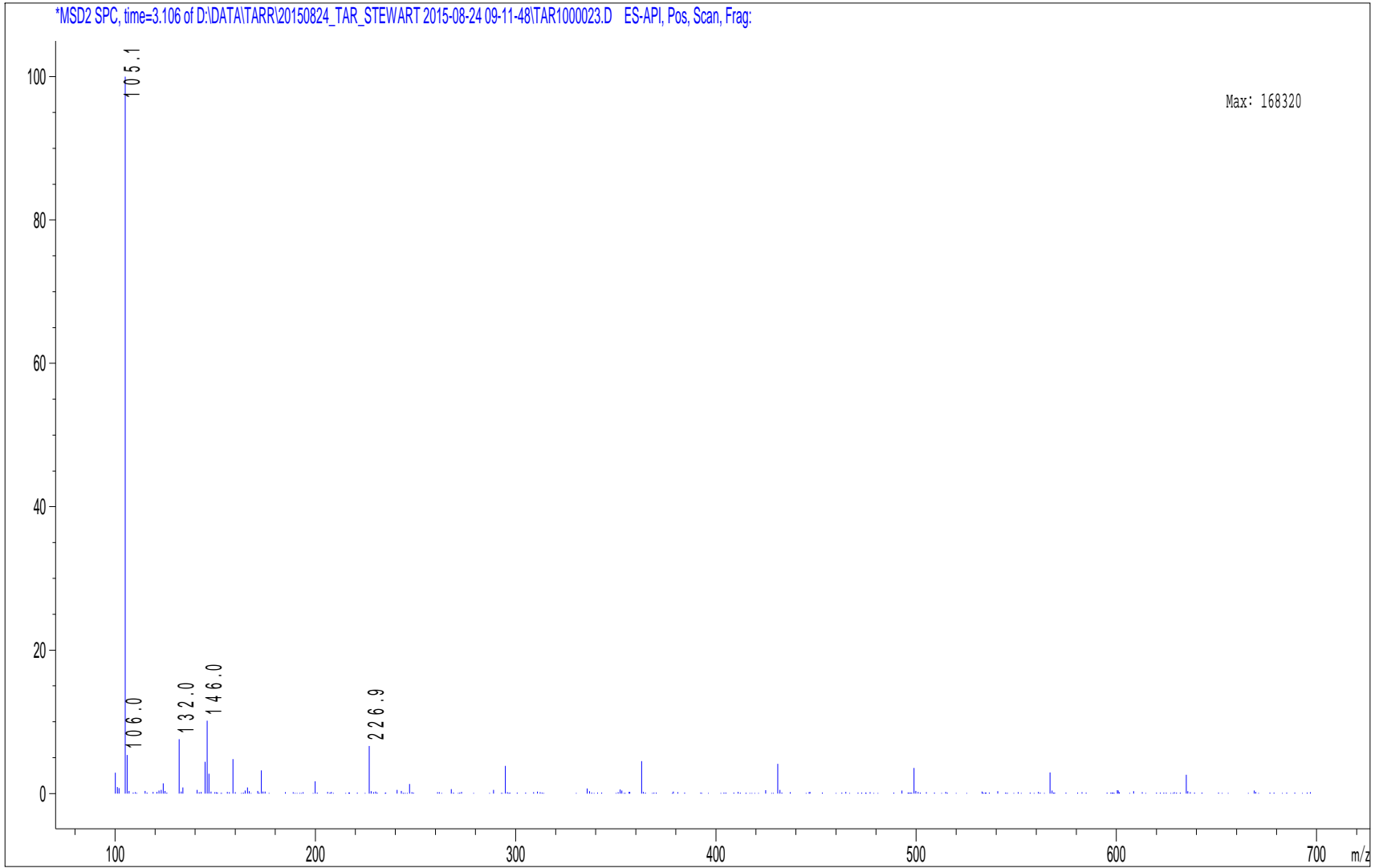
6-Jul-15

100 DC

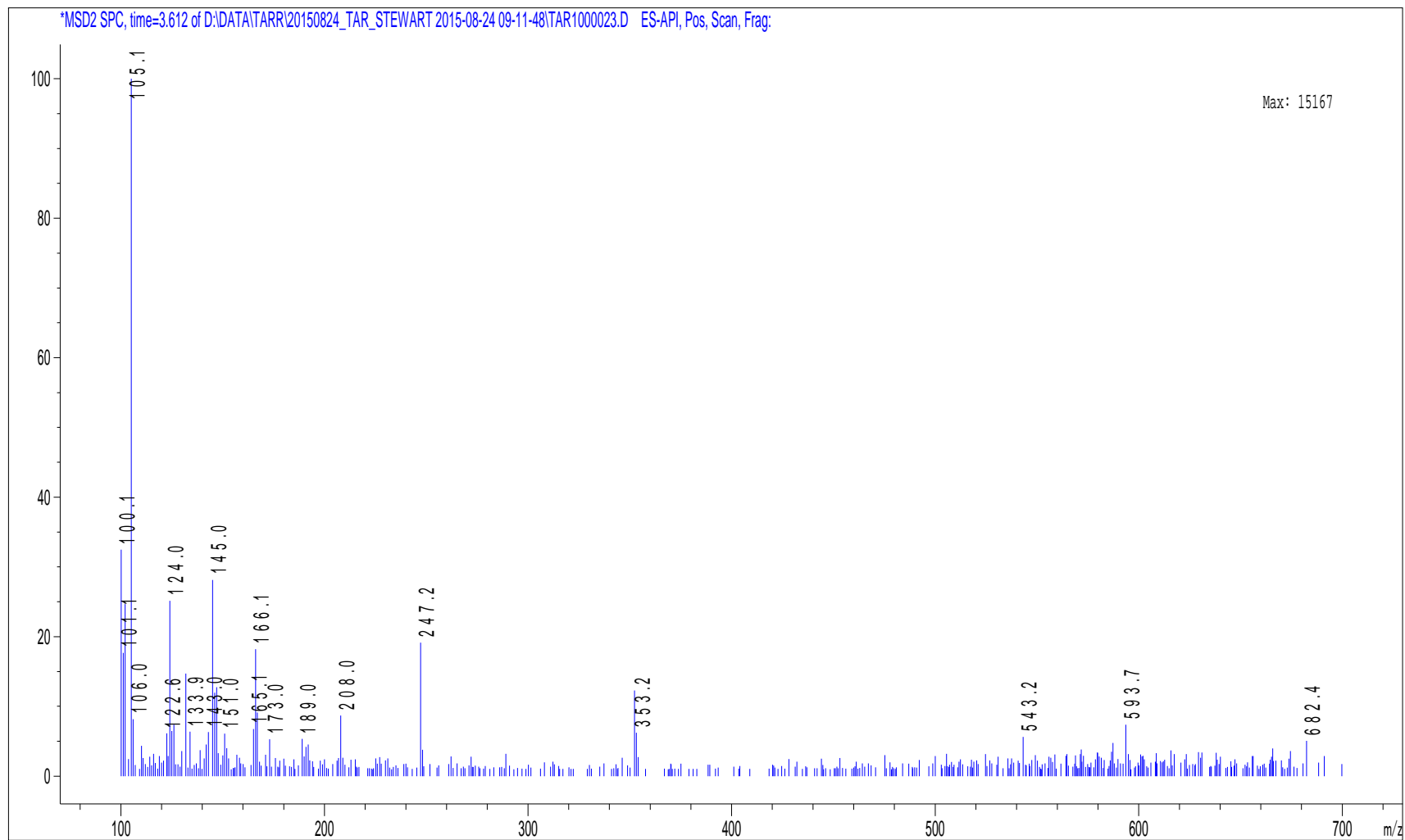
P2-C-05





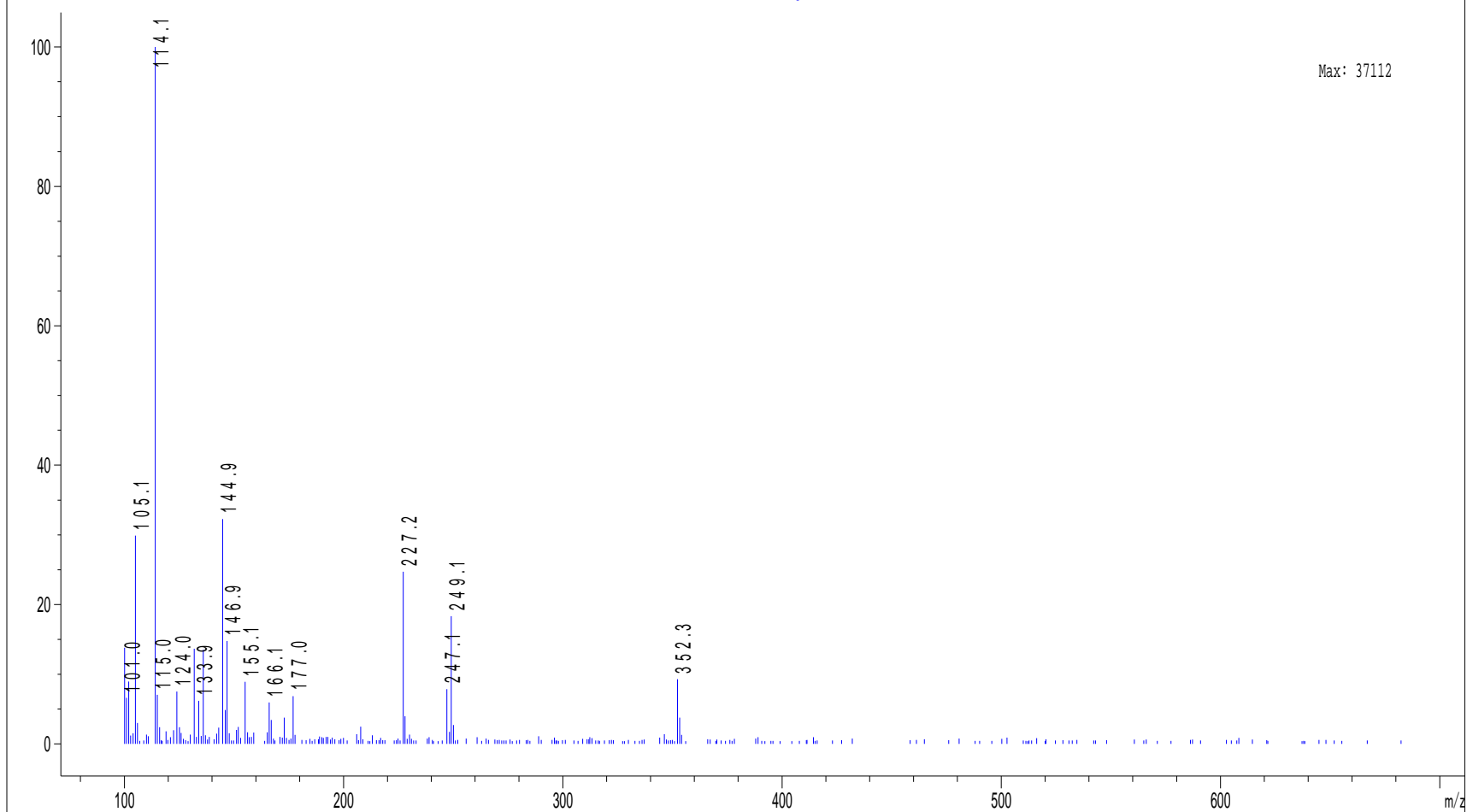


\*MSD2 SPC, time=3.612 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000023.D ES-API, Pos, Scan, Frag:





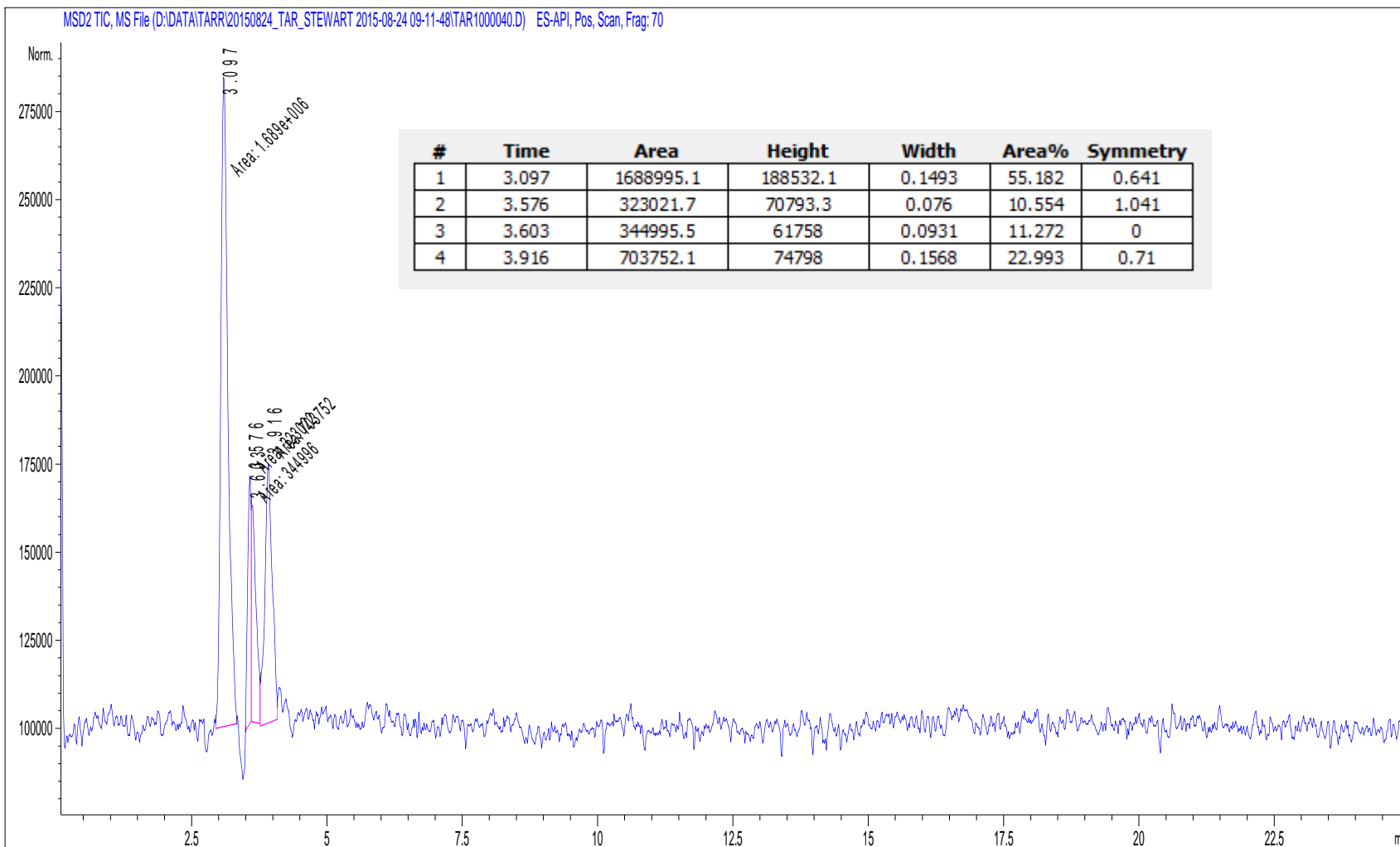
\*MSD2 SPC, time=3.938 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000023.D ES-API, Pos, Scan, Frag:

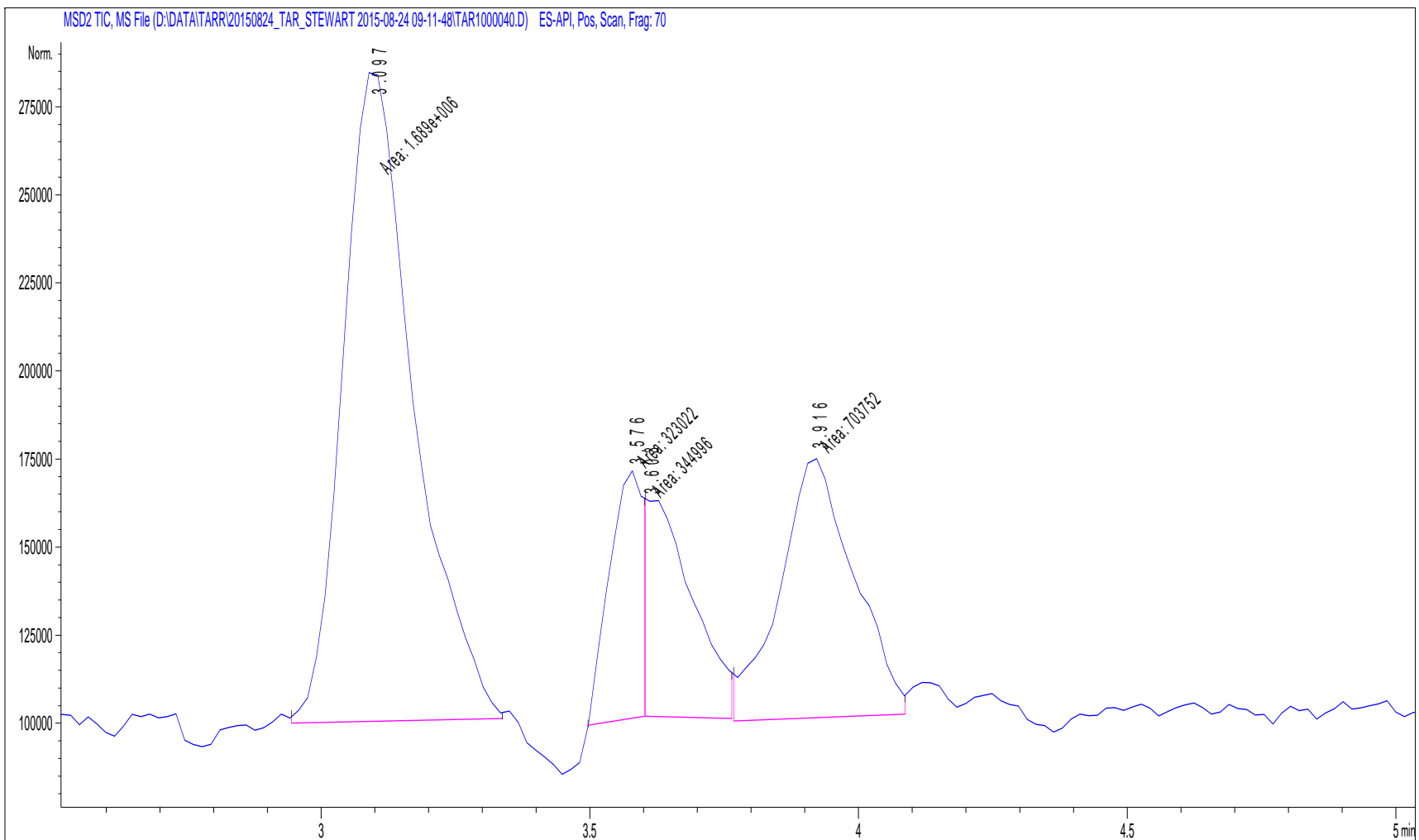


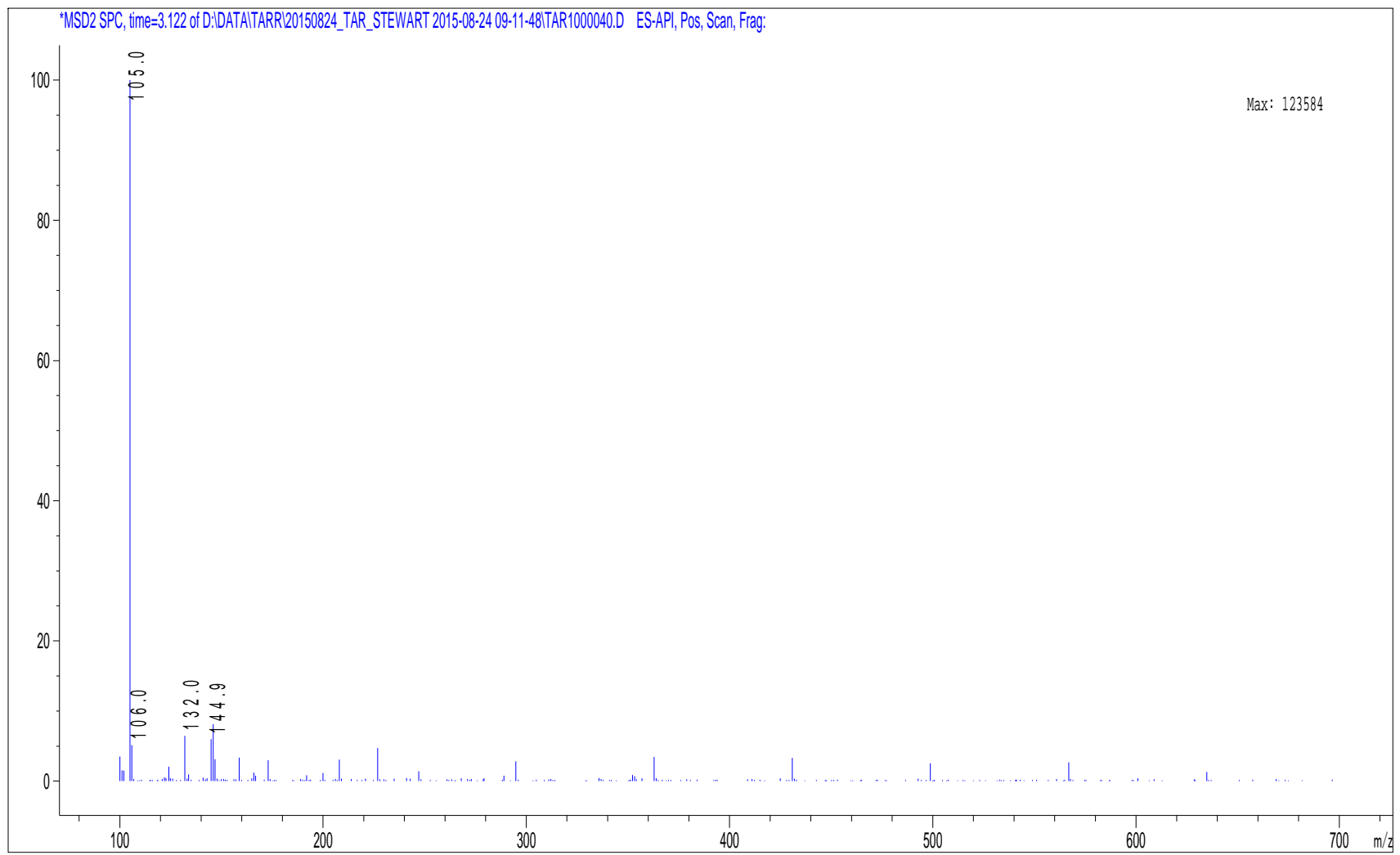
13-Aug-15

100 DC Repeat

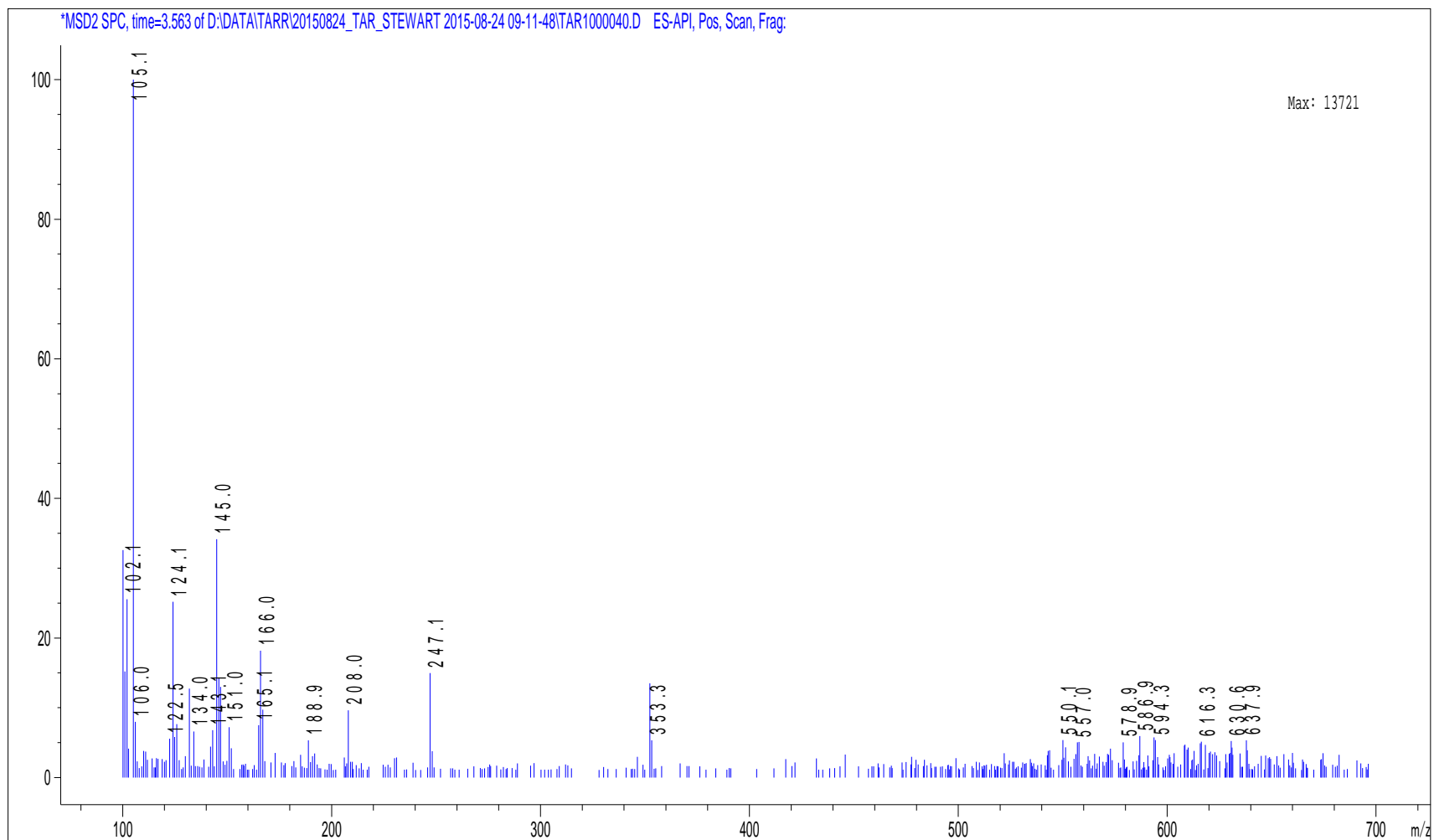
P2-E-04

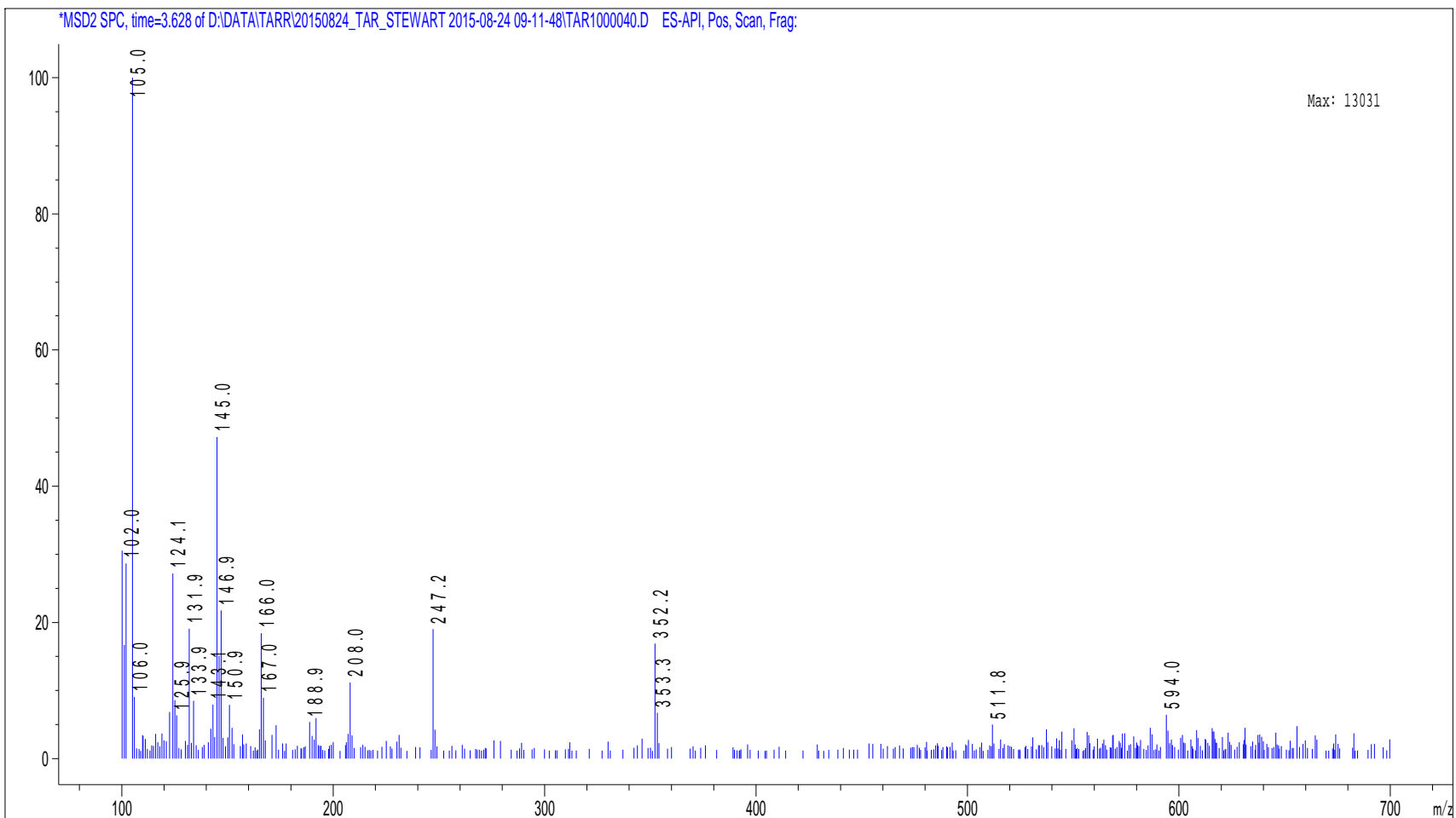


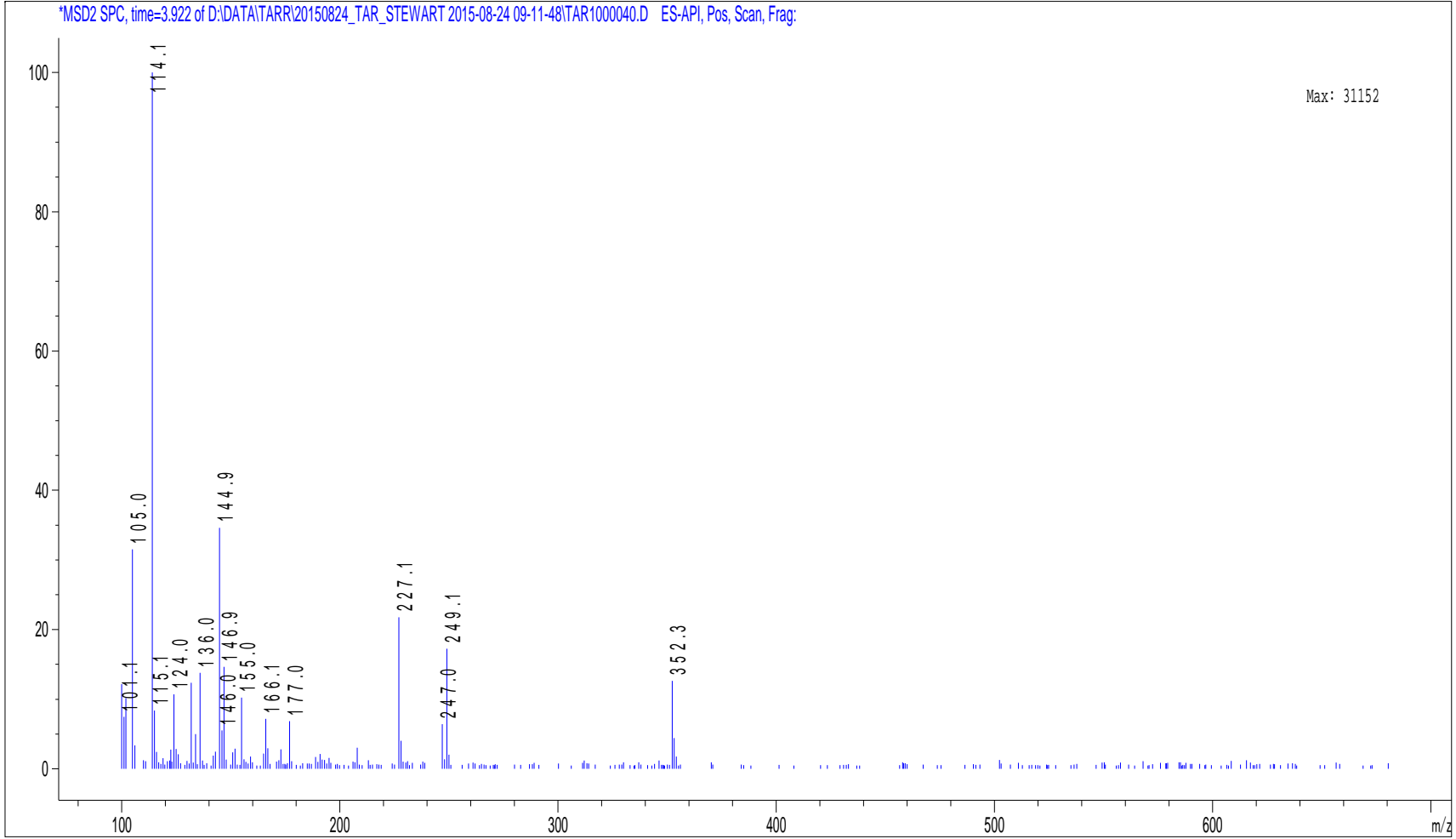




\*MSD2 SPC, time=3.563 of D:\DATA\ARR\20150824\_TAR\_STEWART 2015-08-24 09:11:48\TAR1000040.D ES-API, Pos, Scan, Frag:

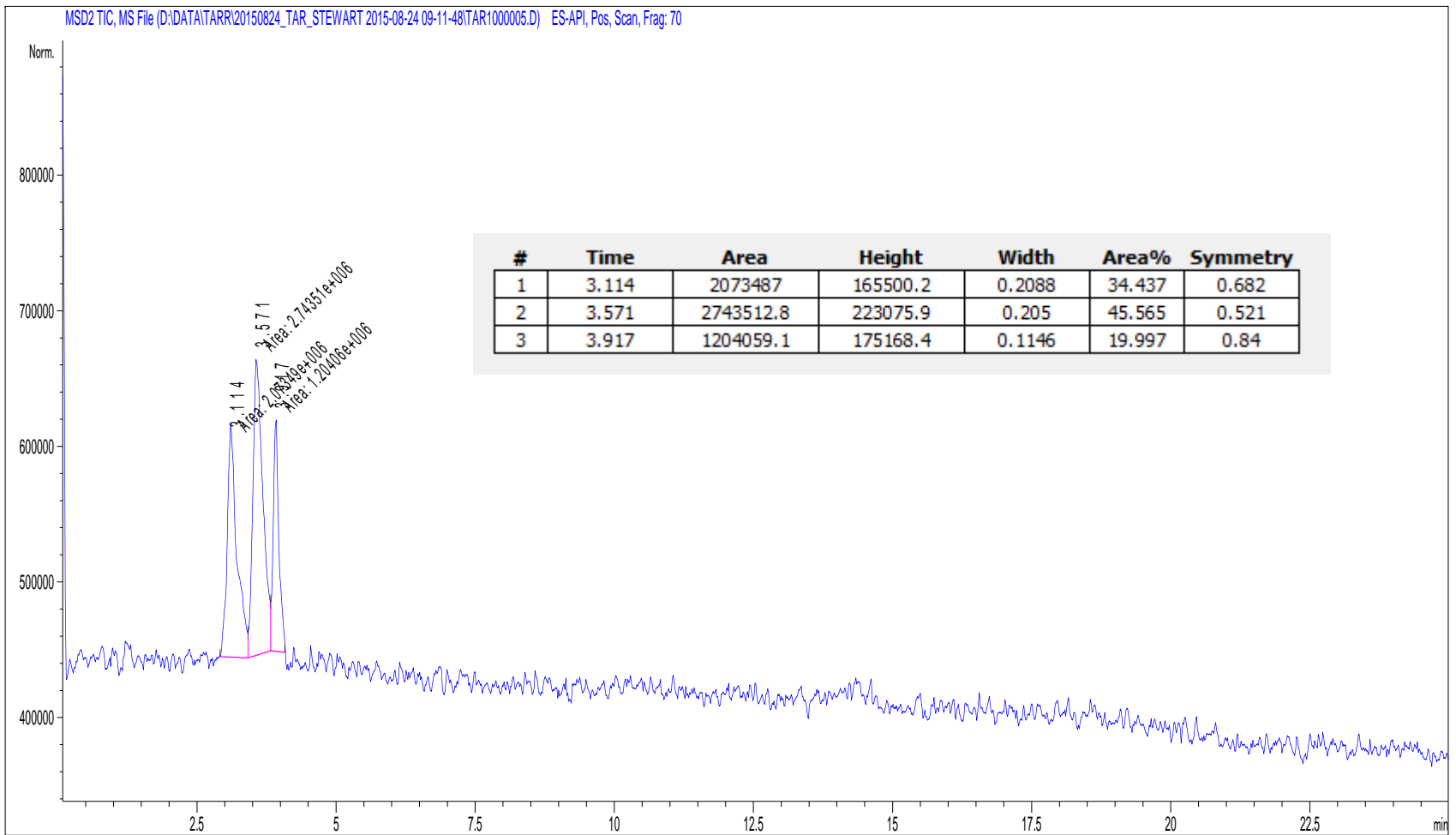




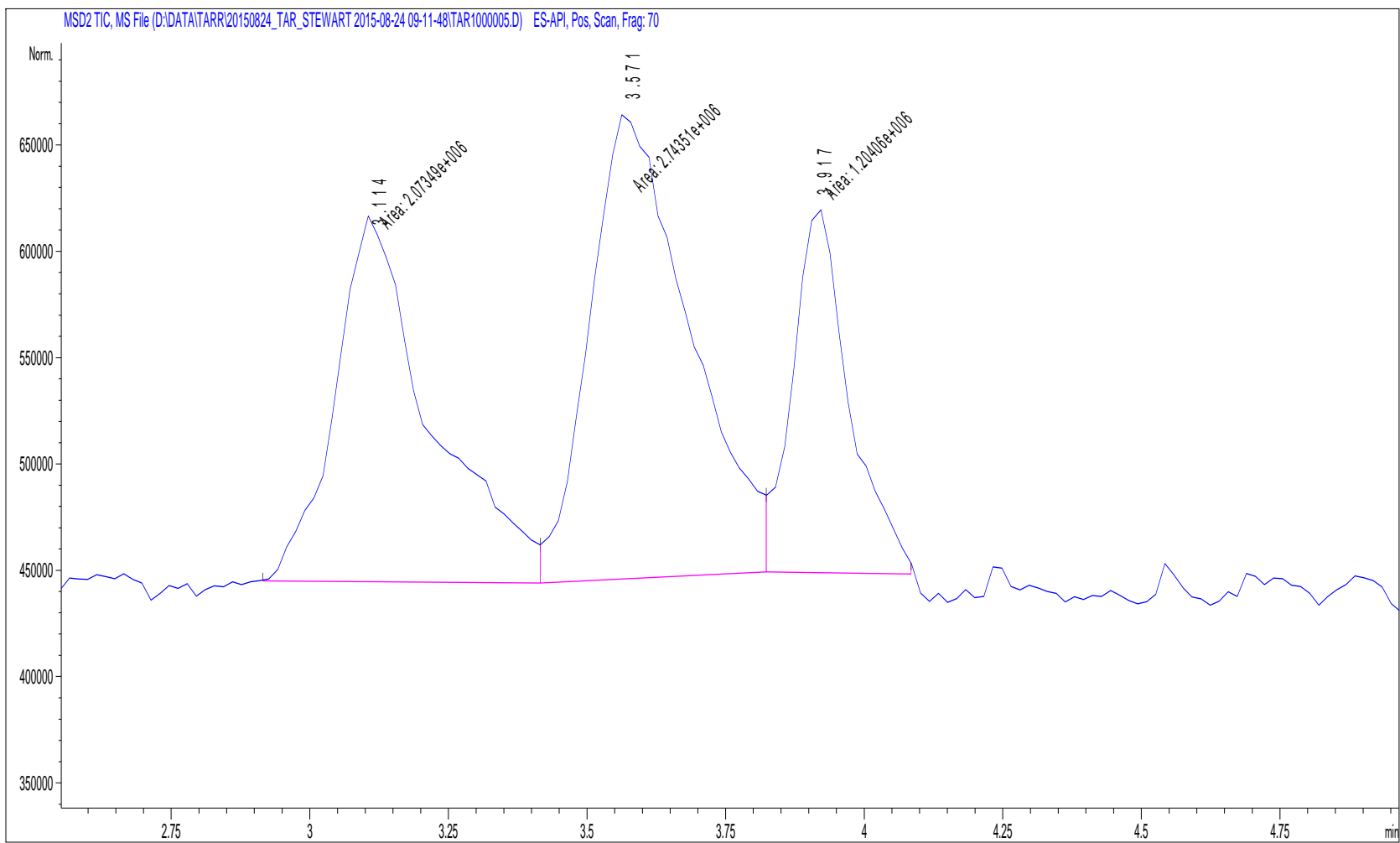


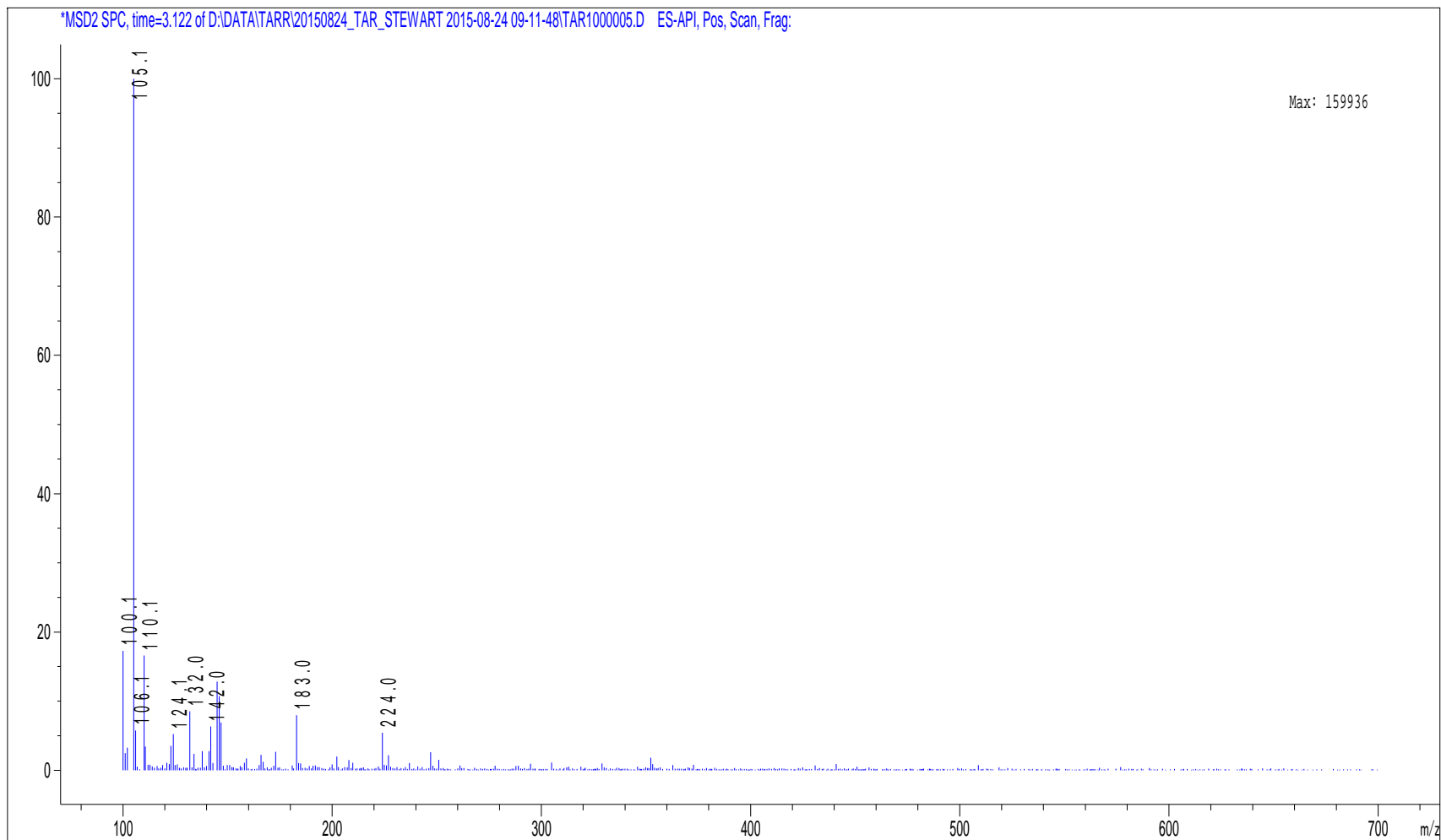
# pH 9

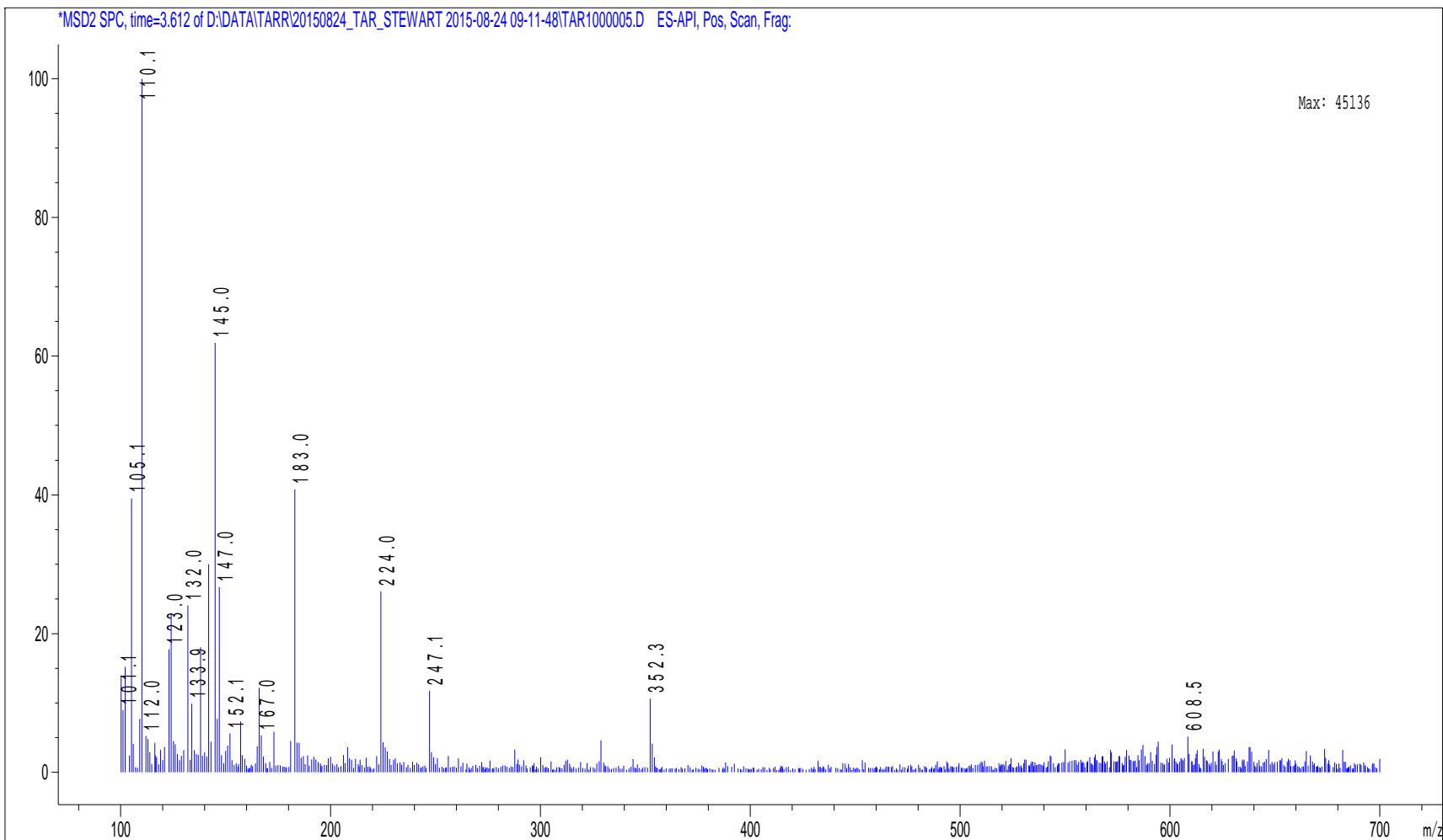
8-Apr-15  
H2O2 Ctrl  
P2-A-05



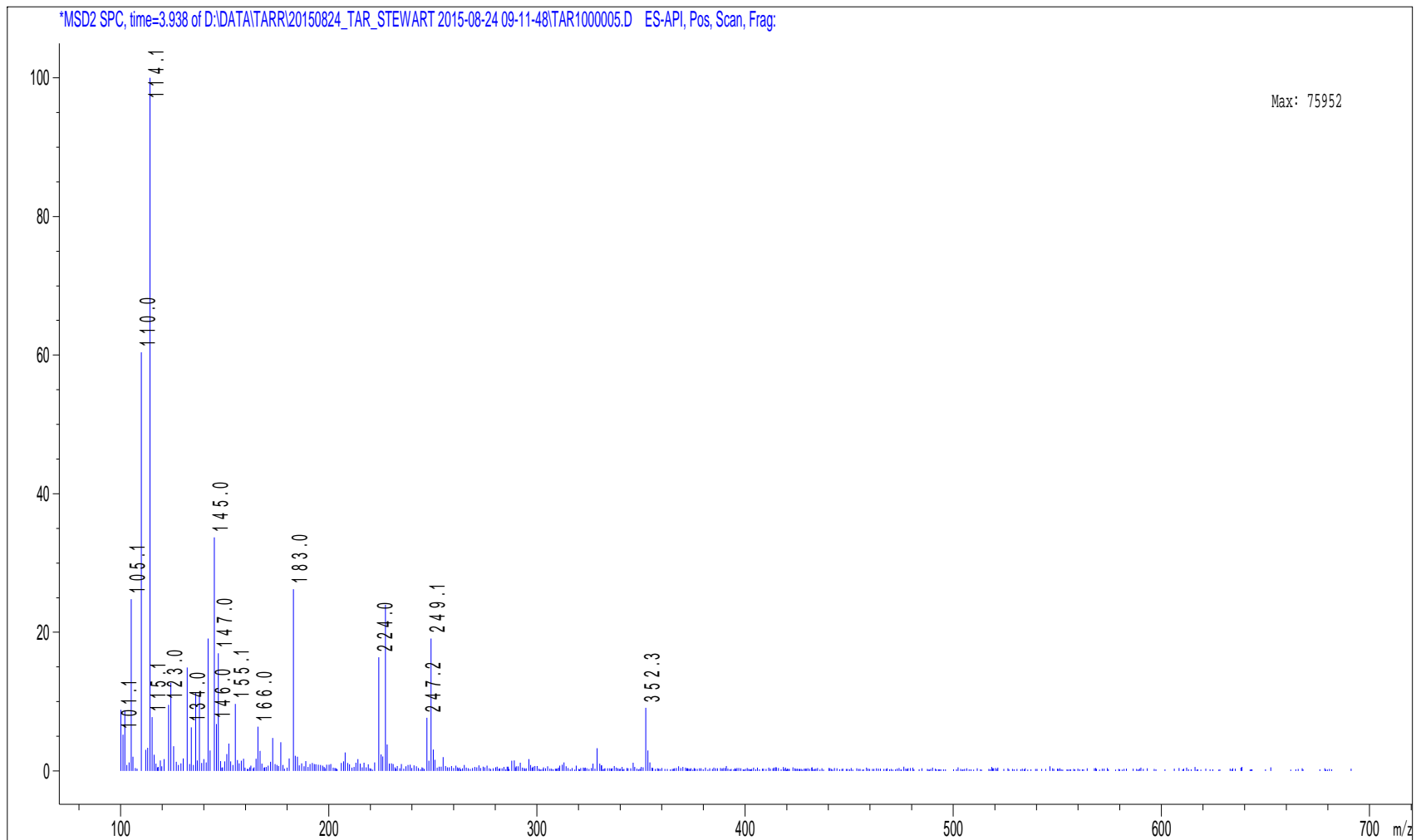








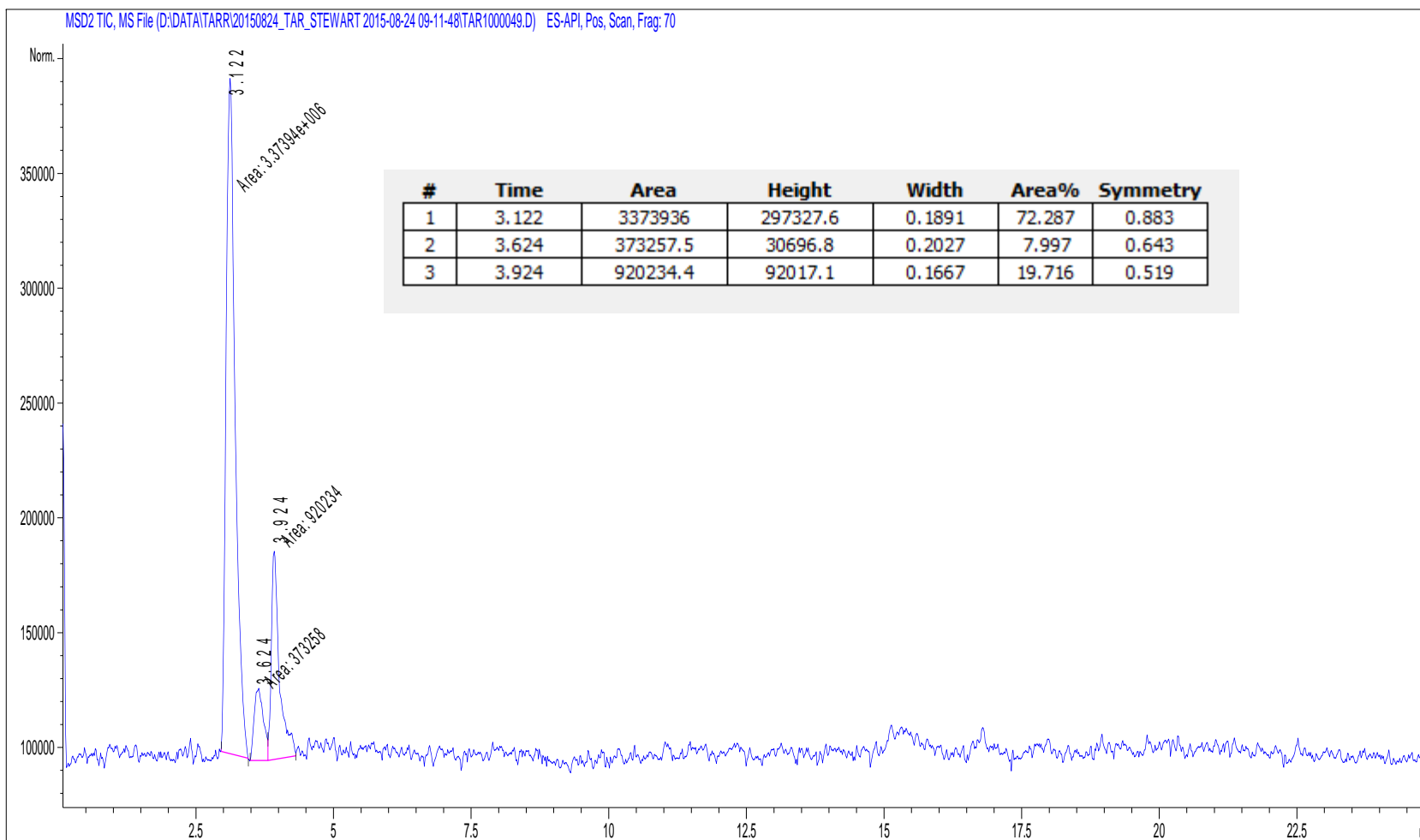
\*MSD2 SPC, time=3.938 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000005.D ES-API, Pos, Scan, Frag:

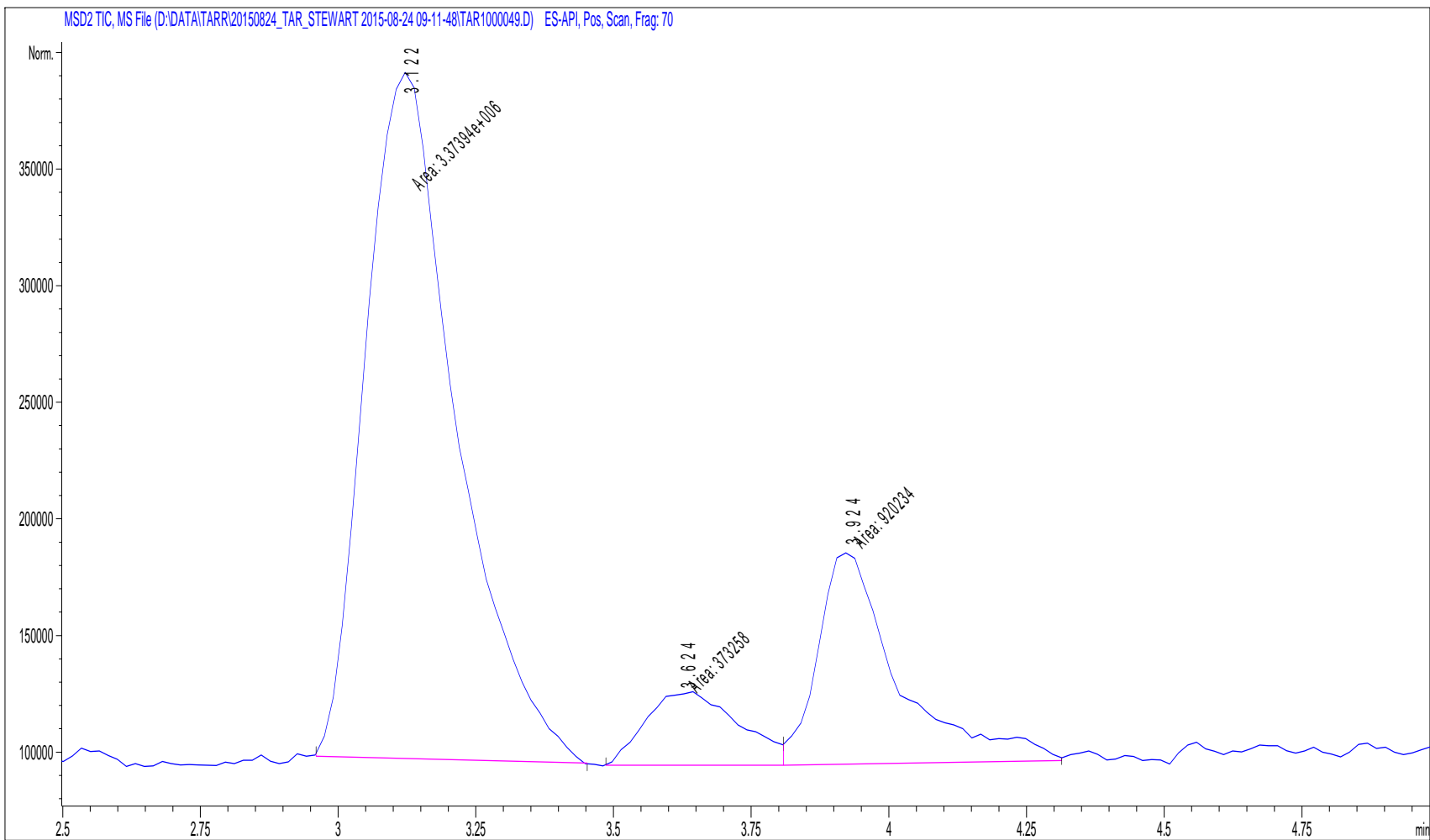


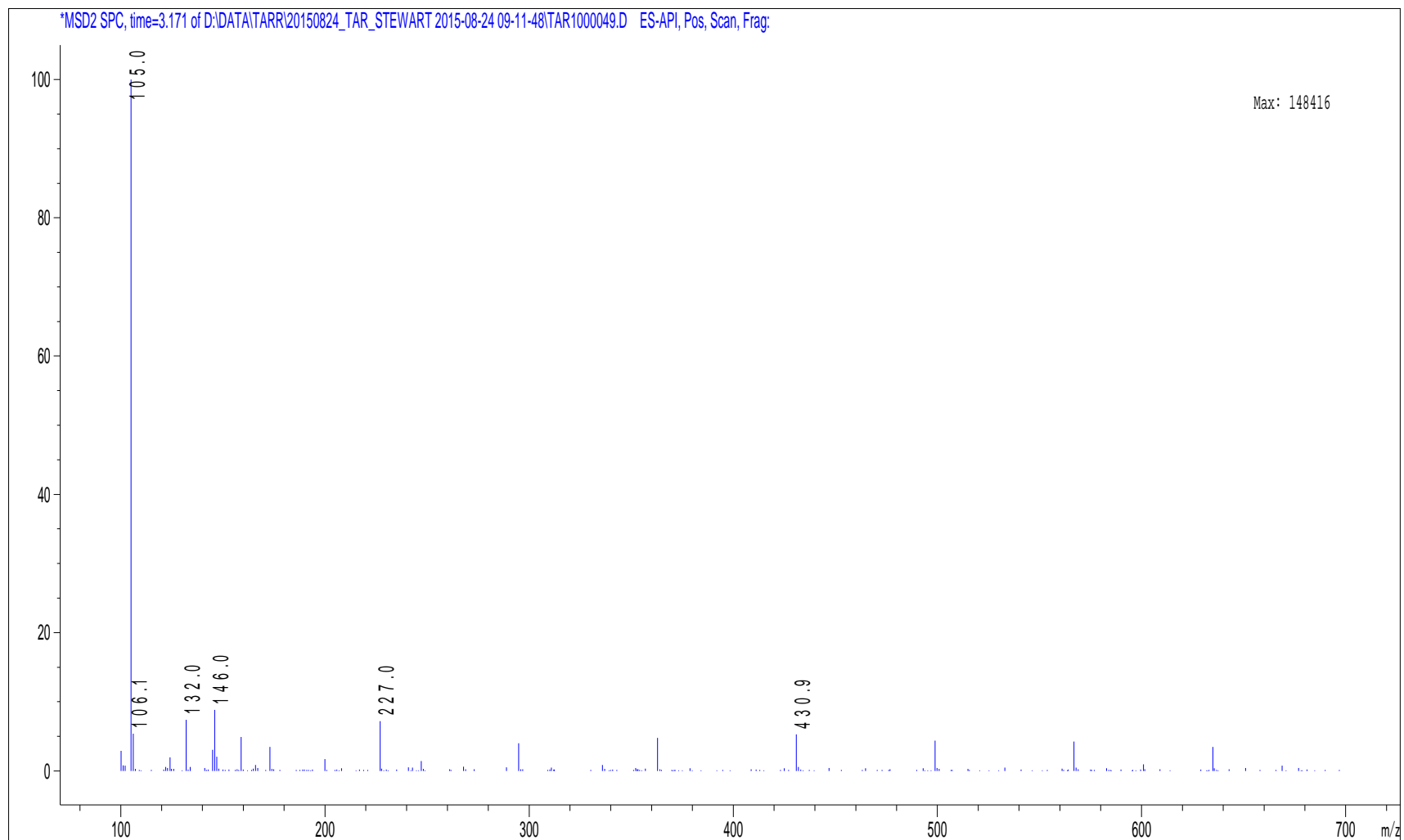
16-Mar-15

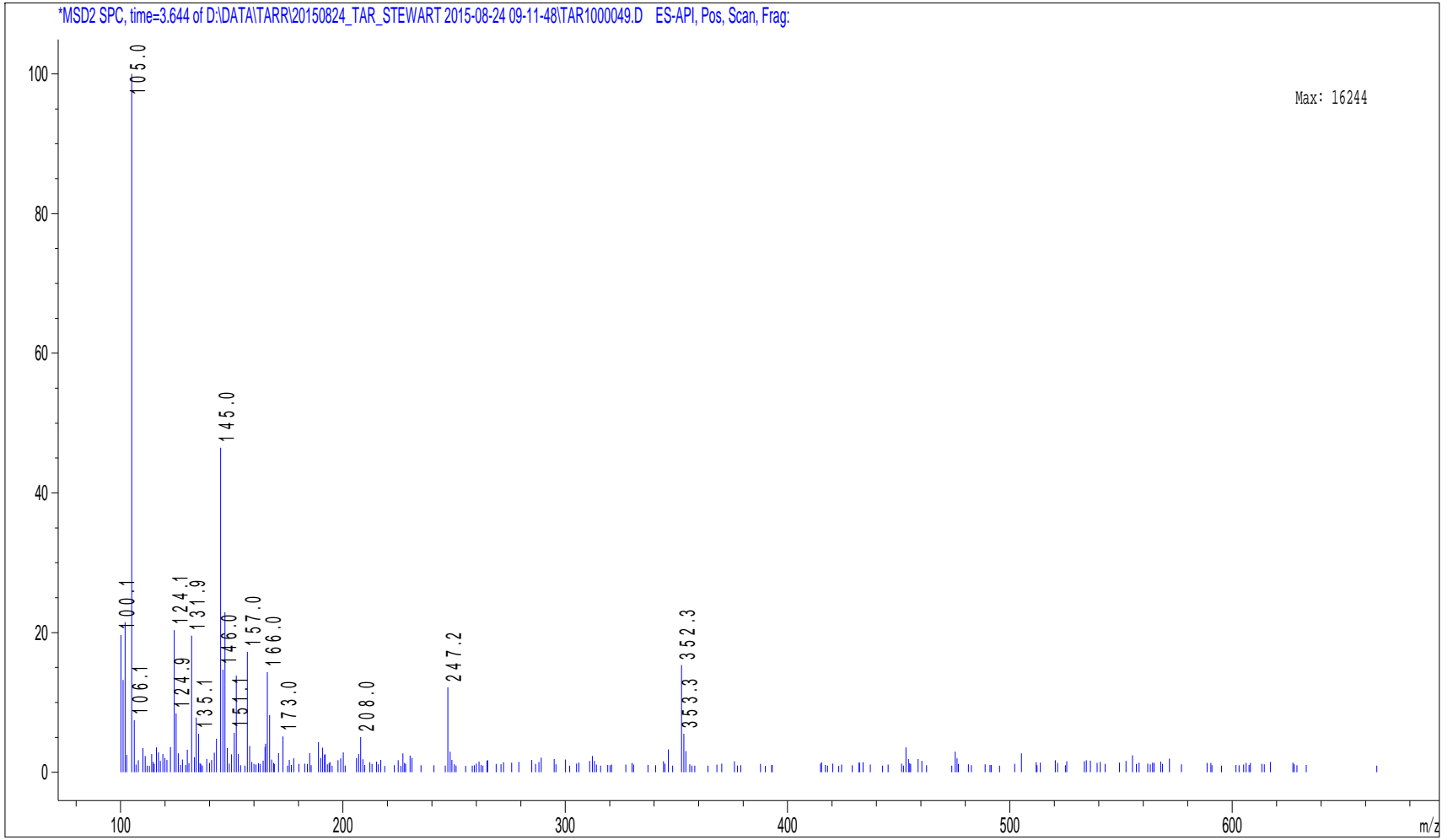
0 DC

P2-A-04



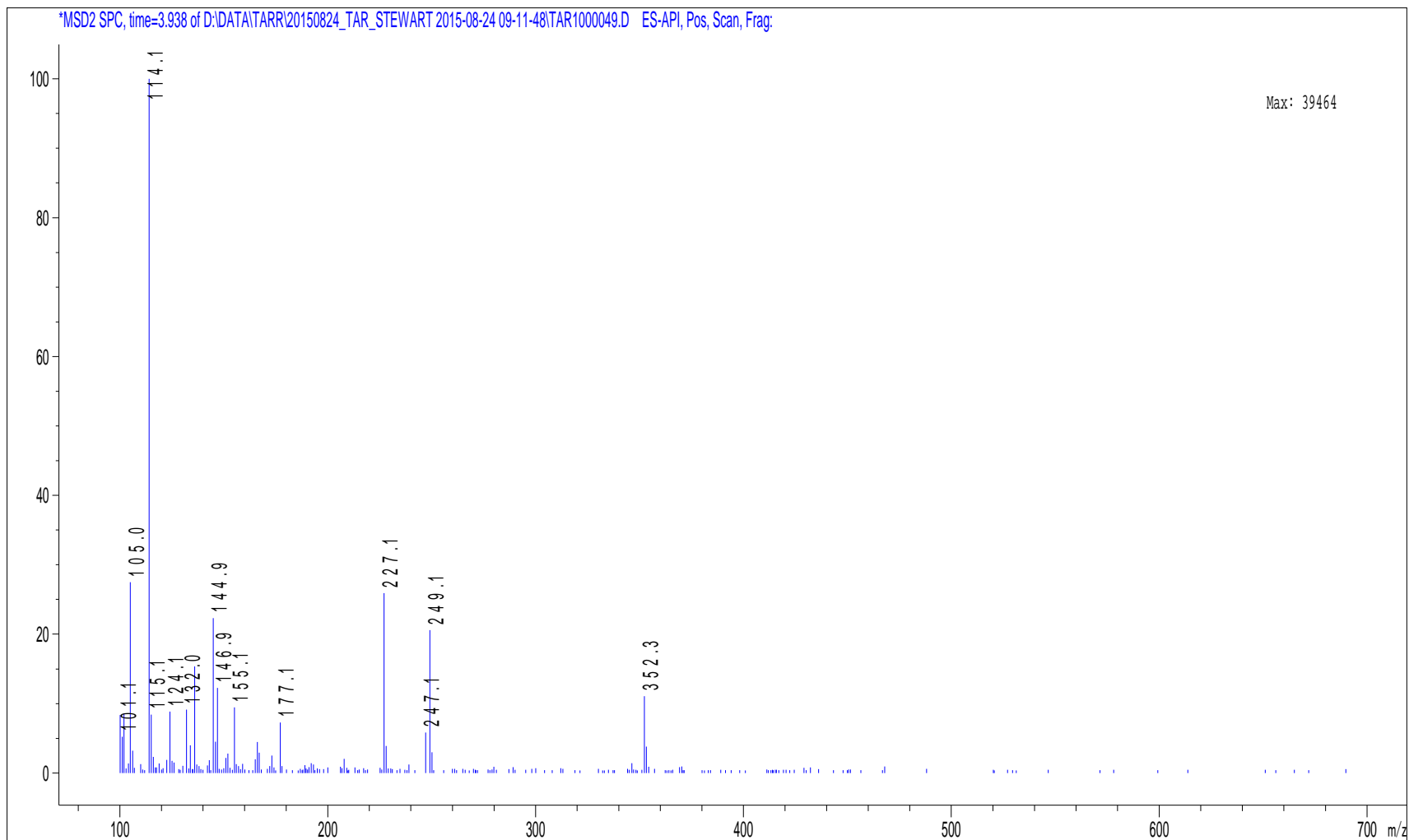








\*MSD2 SPC, time=3.938 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000049.D ES-API, Pos, Scan, Frag:

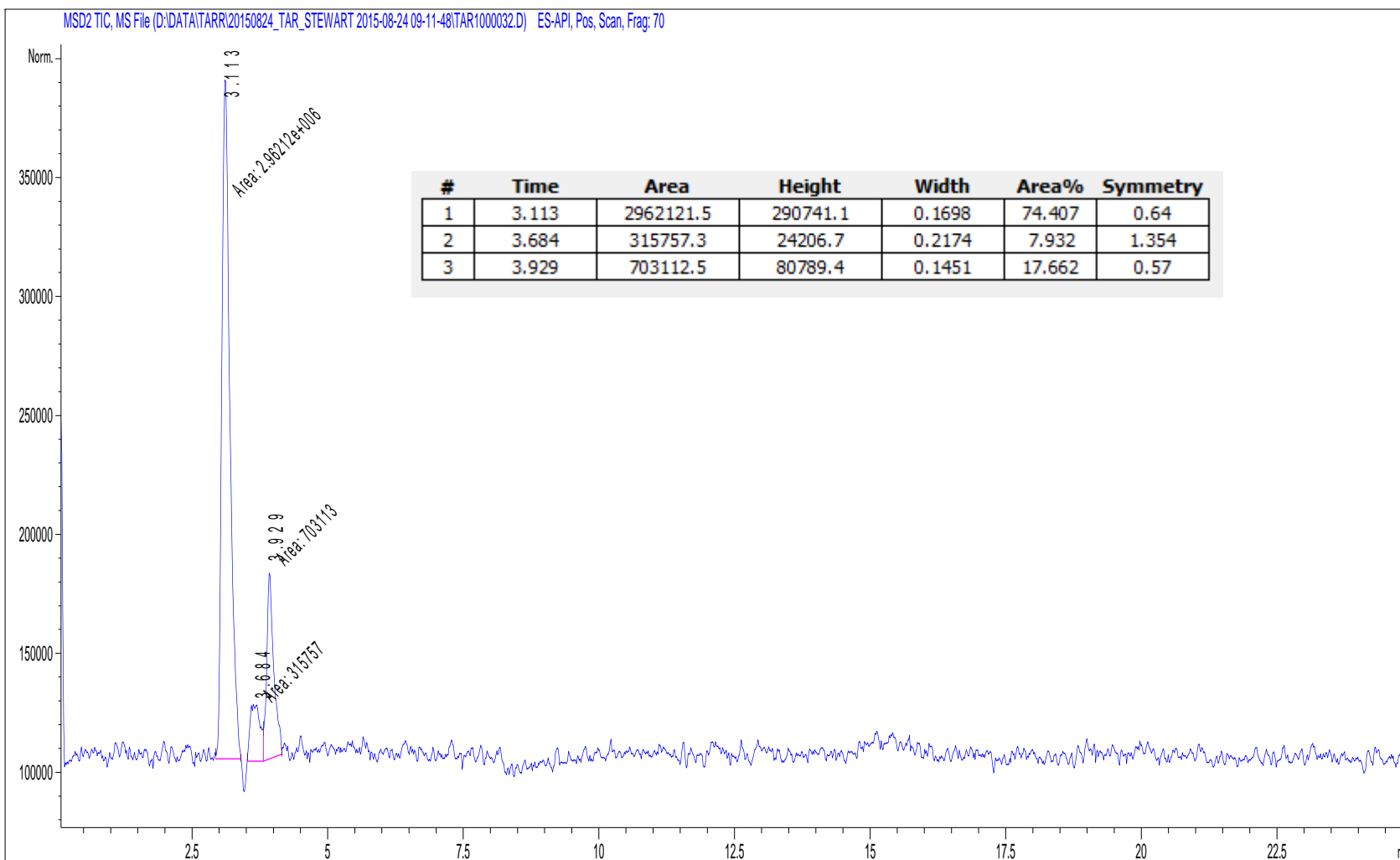


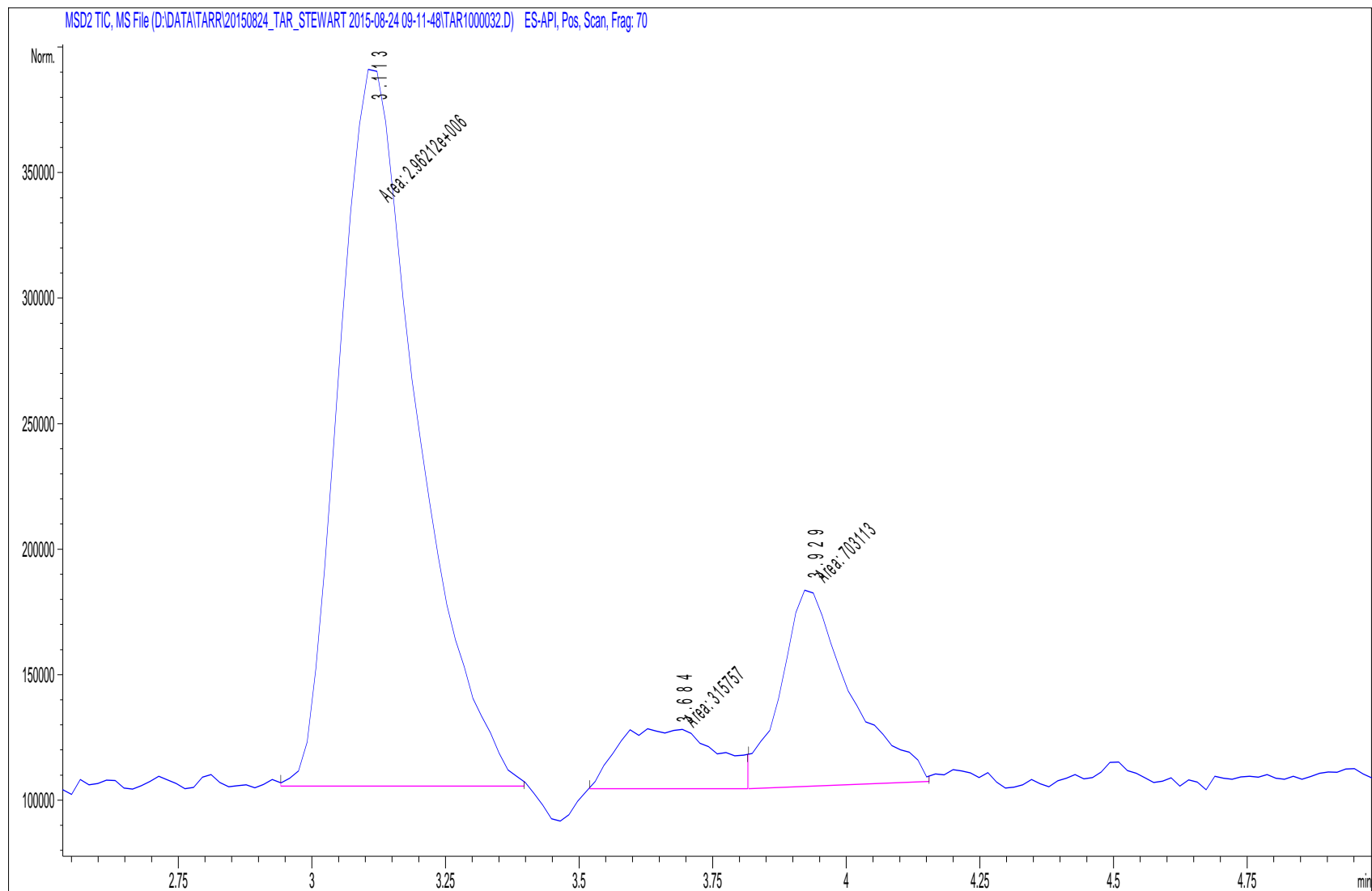
Max: 39464

28-Jul-15

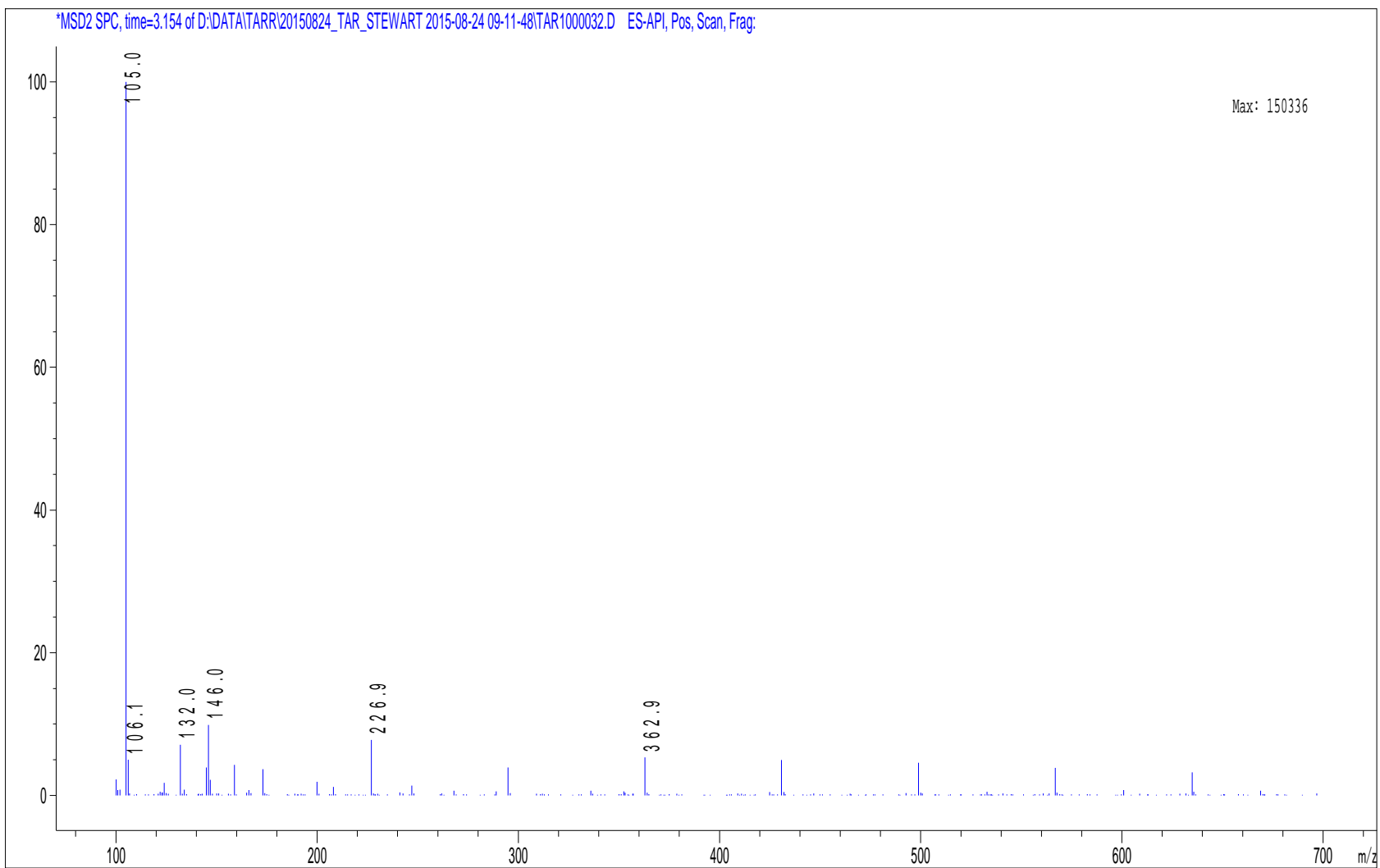
5 DC

P2-D-05

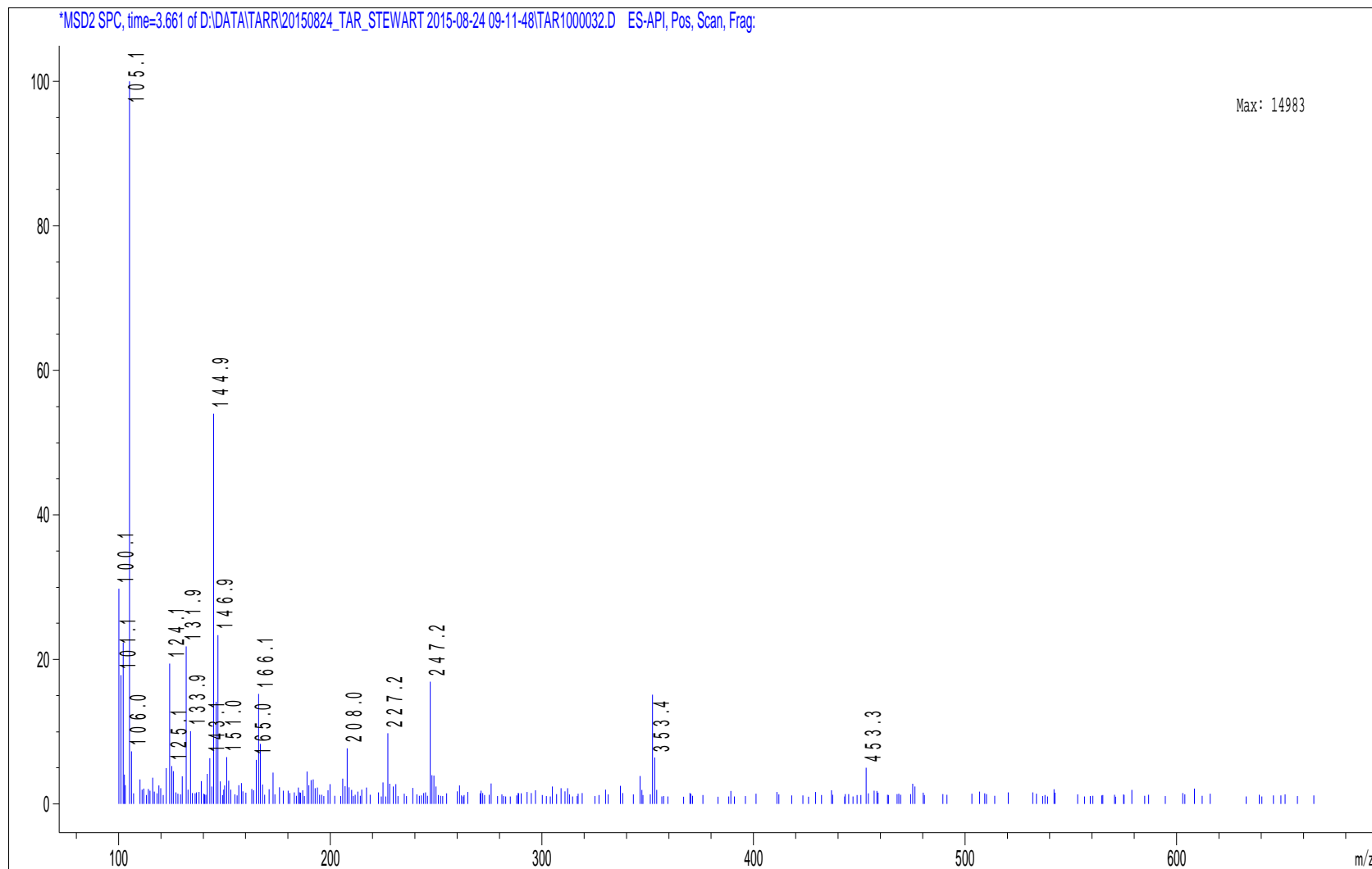




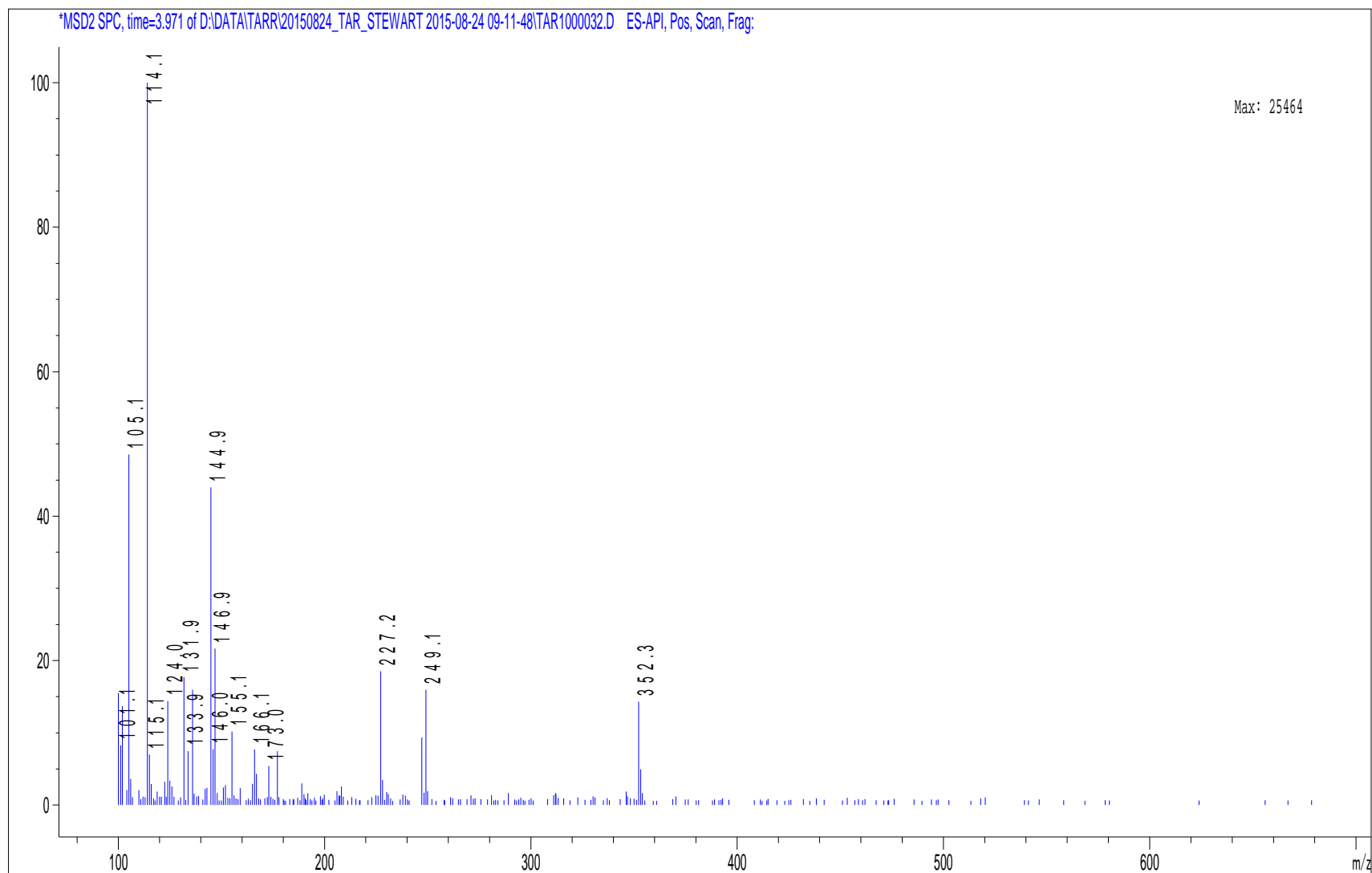
\*MSD2 SPC, time=3.154 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000032.D ES-API, Pos, Scan, Frag:



\*MSD2 SPC, time=3.661 of D:\DATA\ARRI\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000032.D ES-API, Pos, Scan, Frag:



\*MSD2 SPC, time=3.971 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000032.D ES-API, Pos, Scan, Frag:

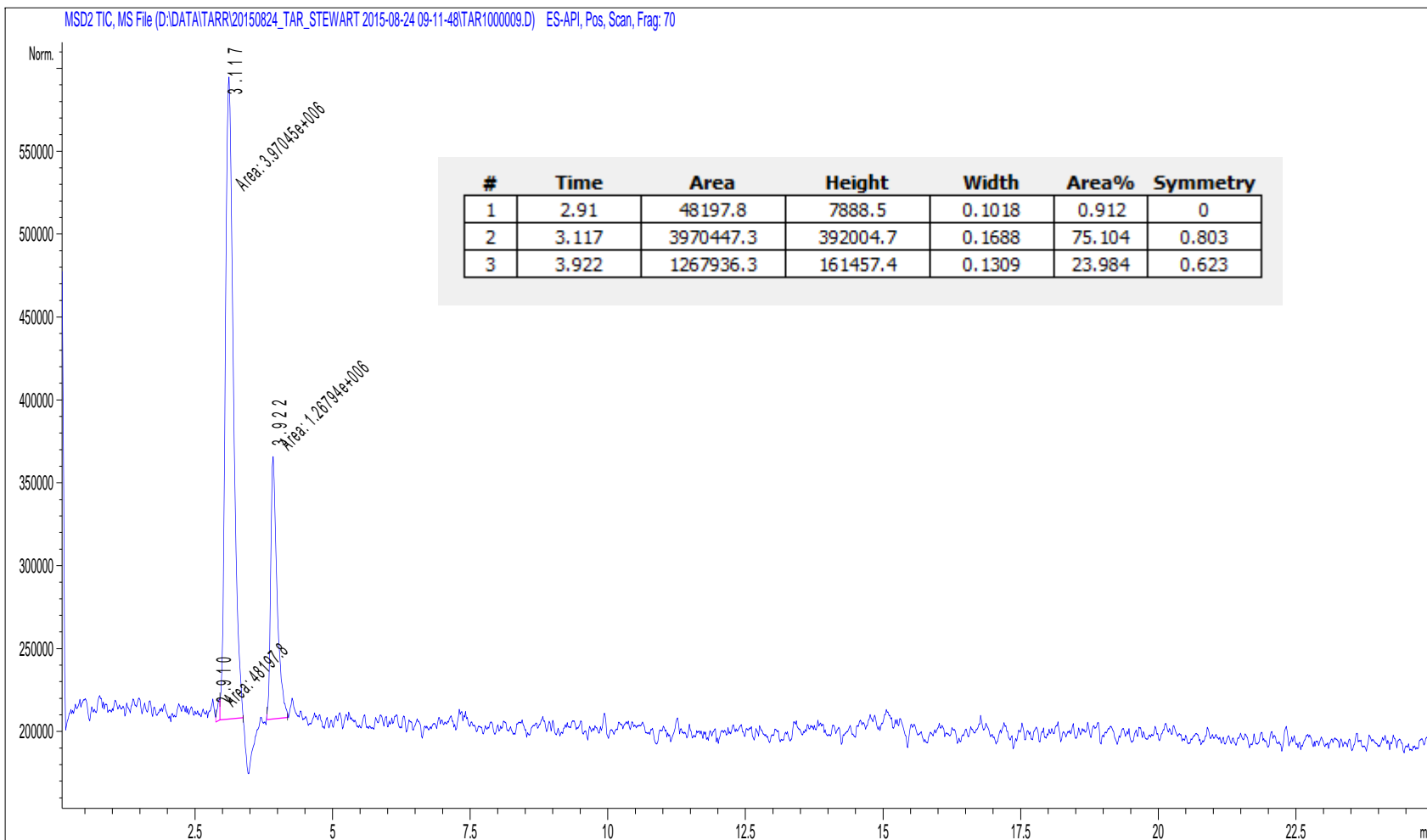


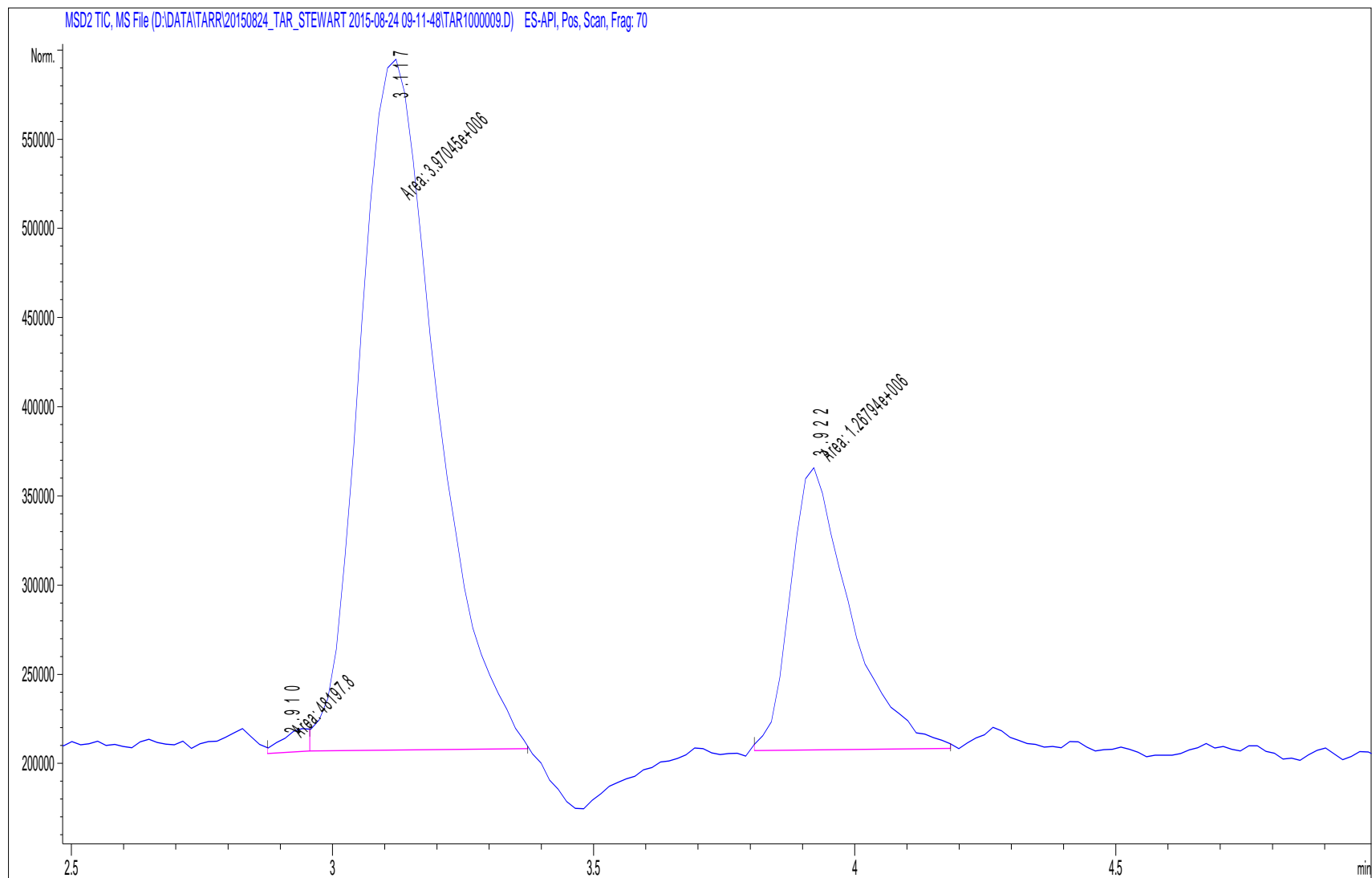
Max: 25464

30-Apr-15

10 DC

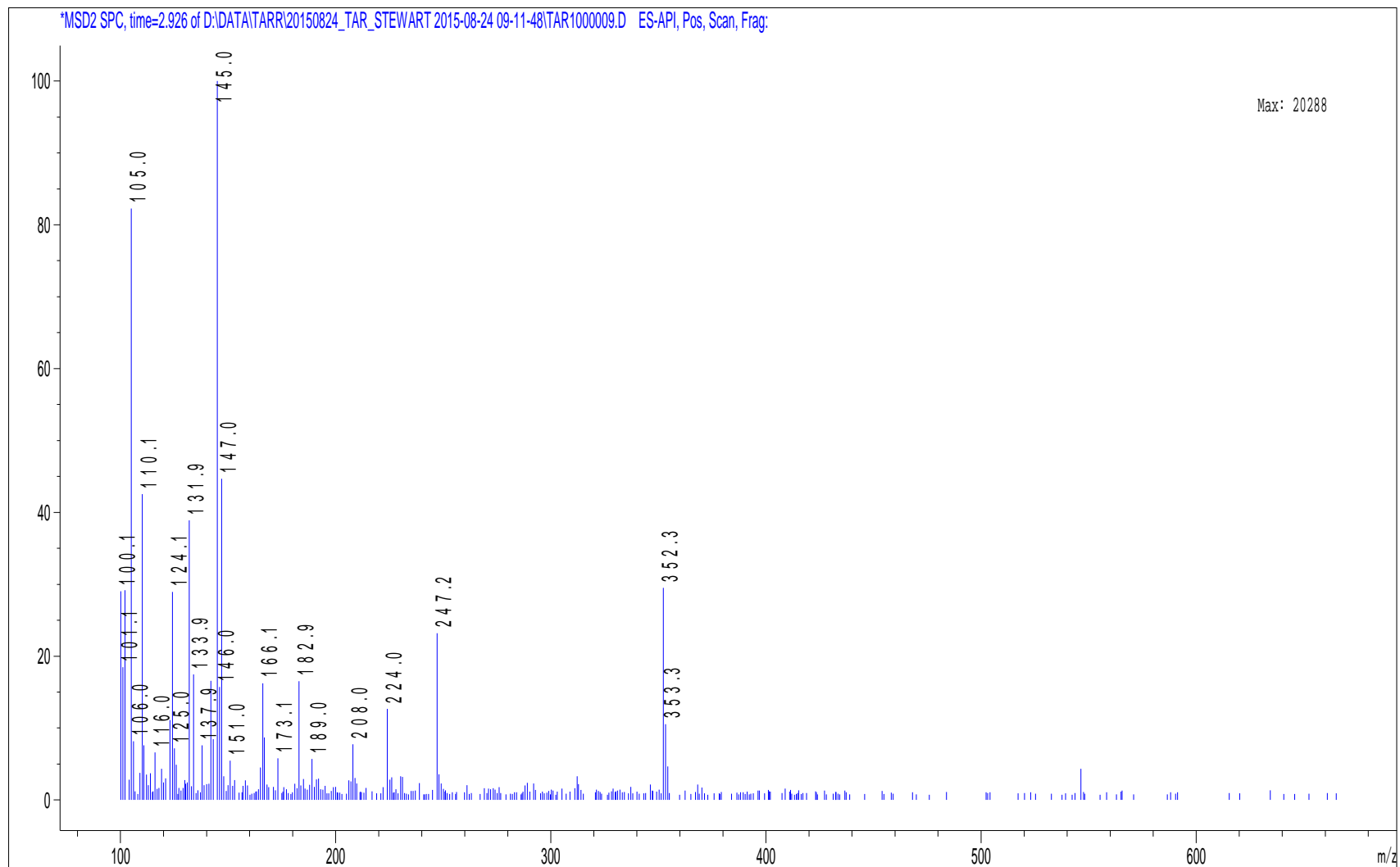
P2-A-09



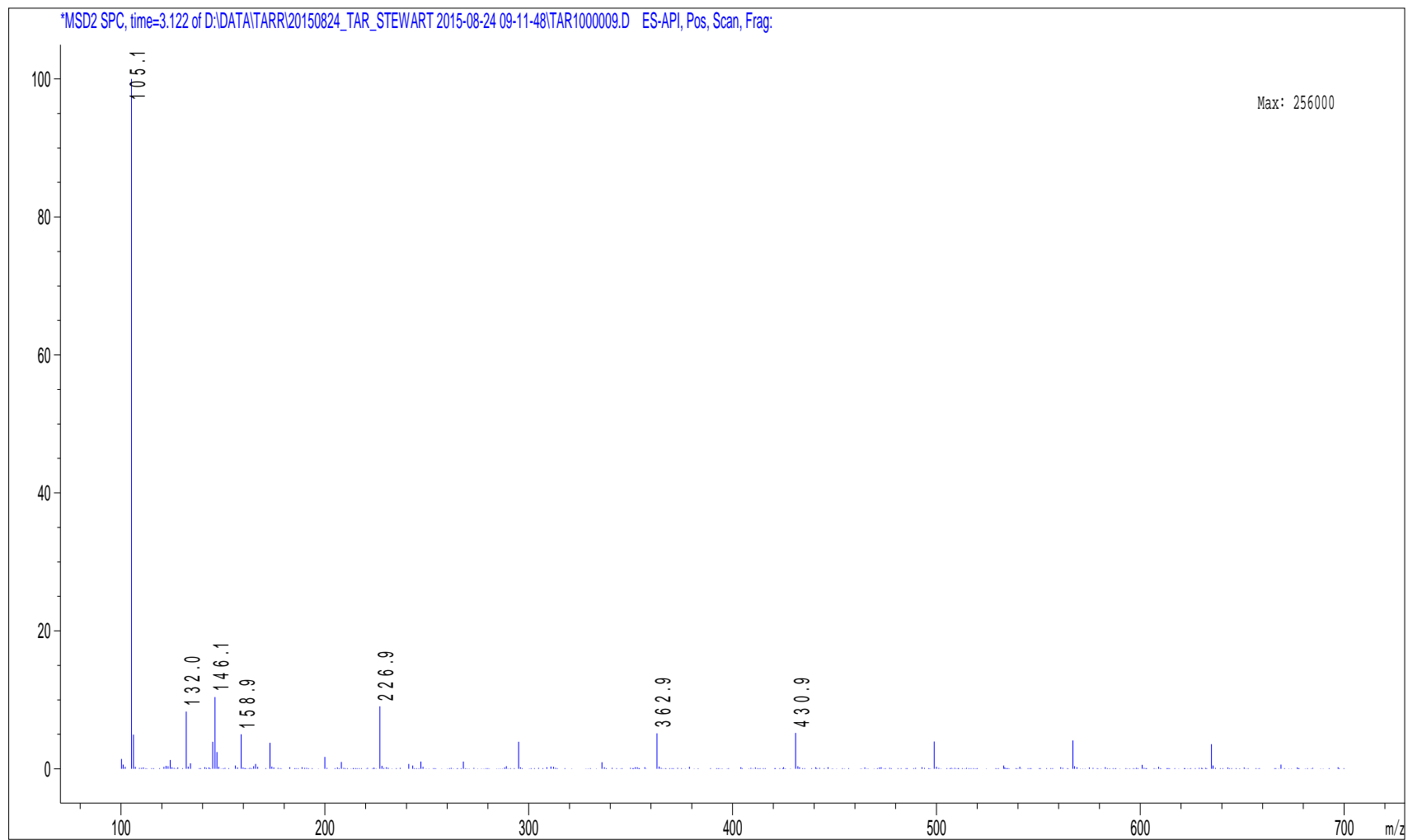




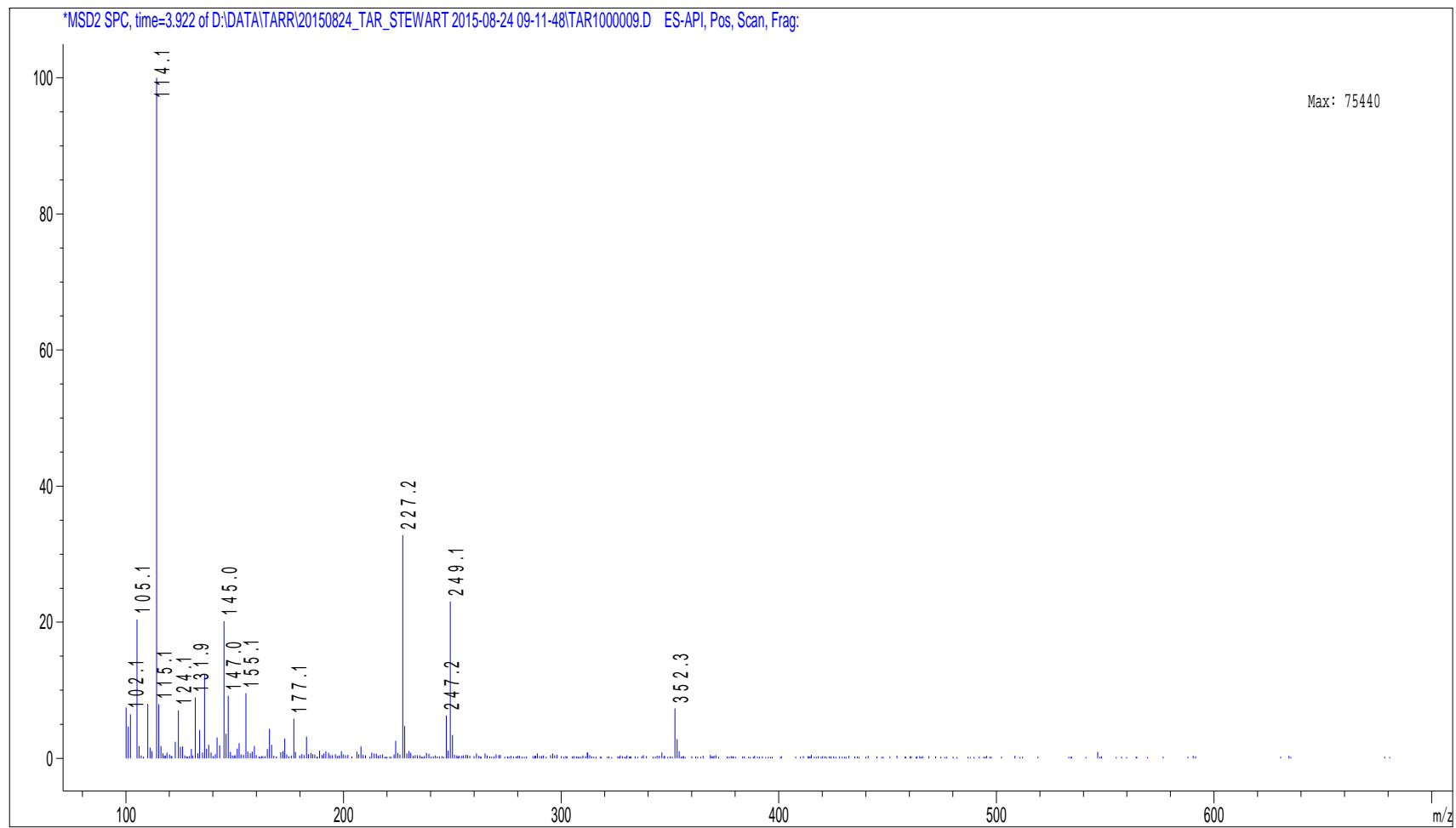
\*MSD2 SPC, time=2.926 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000009.D ES-API, Pos, Scan, Frag:



Max: 20288



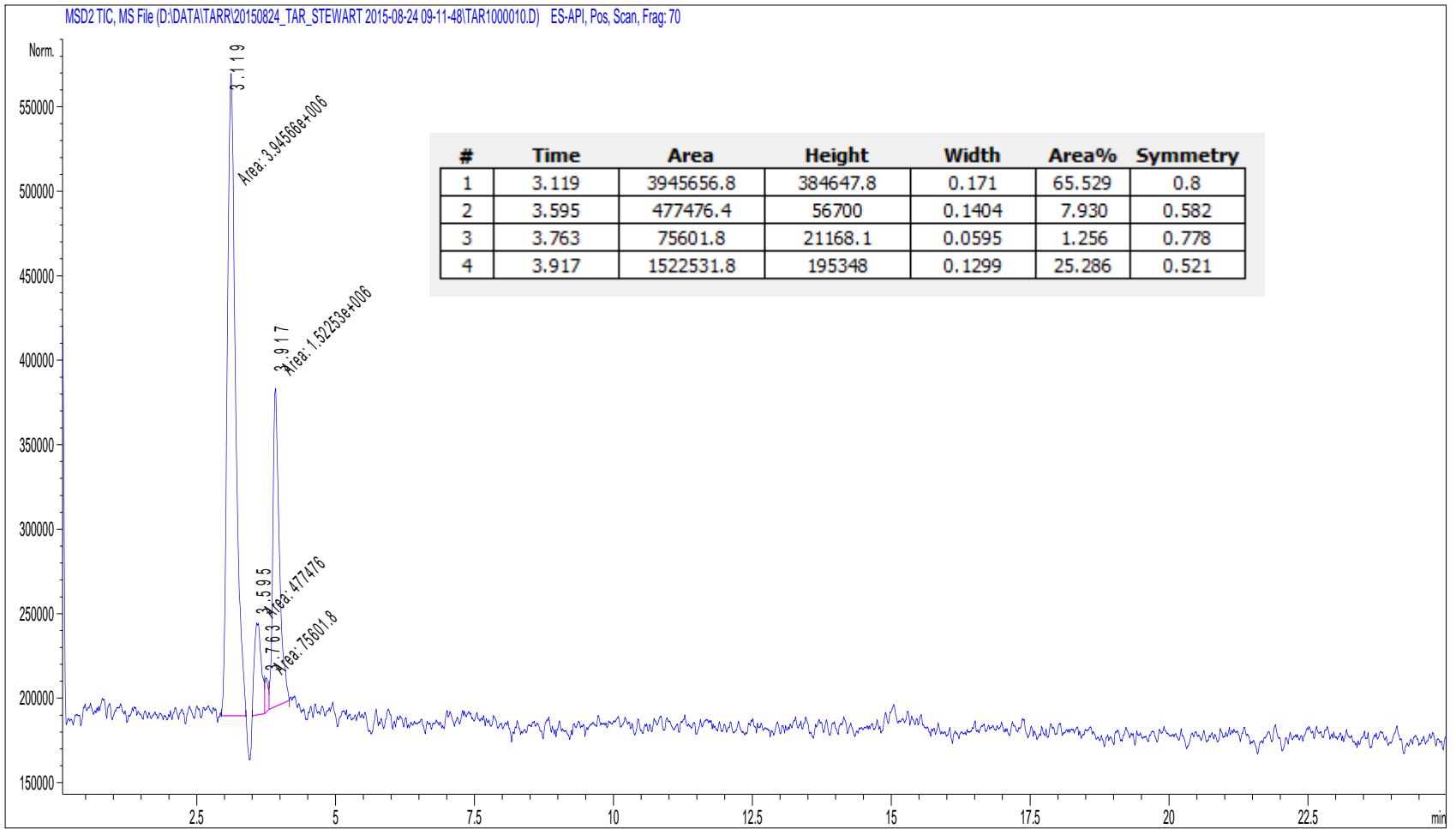
\*MSD2 SPC, time=3.922 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000009.D ES-API, Pos, Scan, Frag:

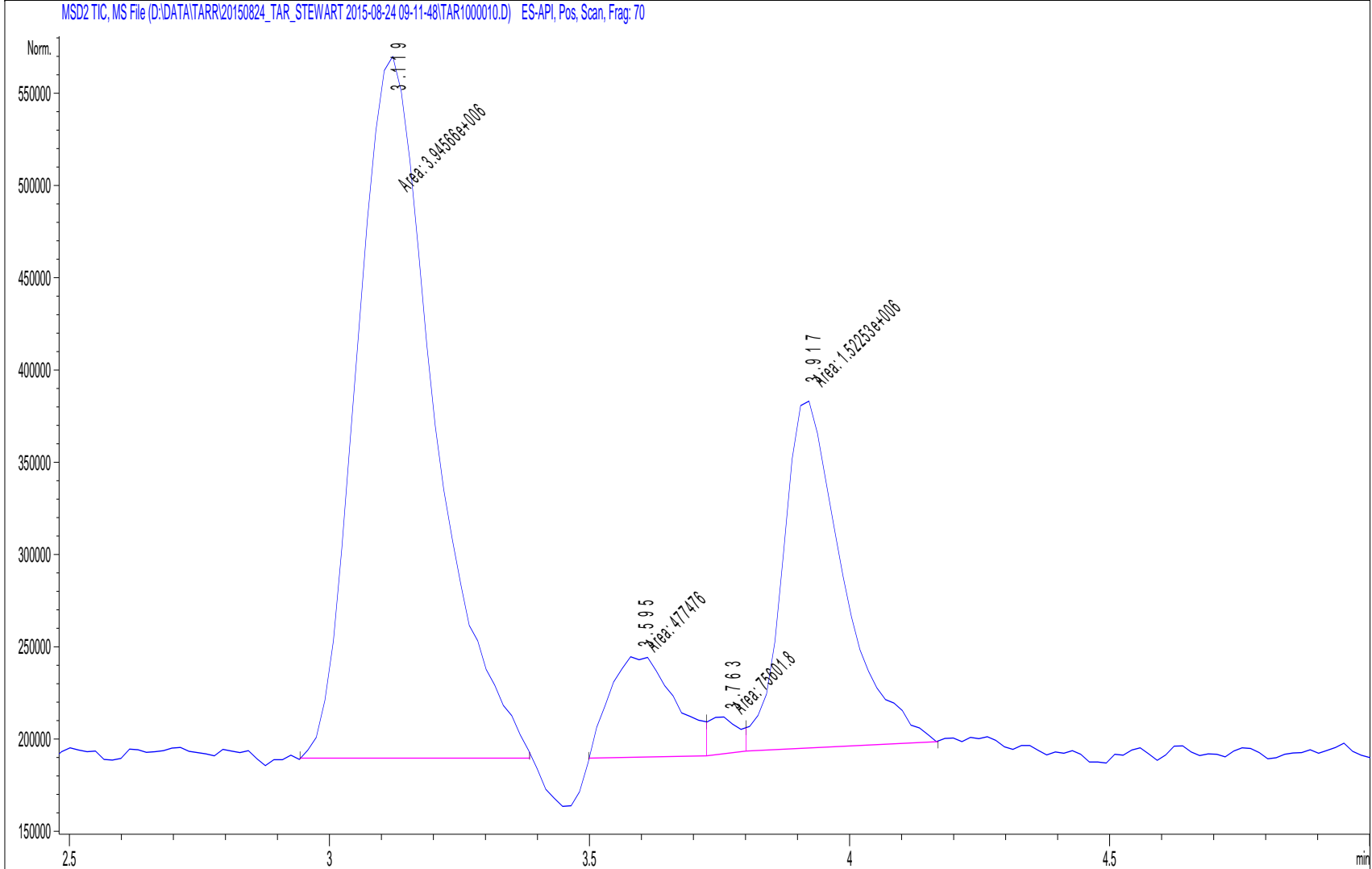


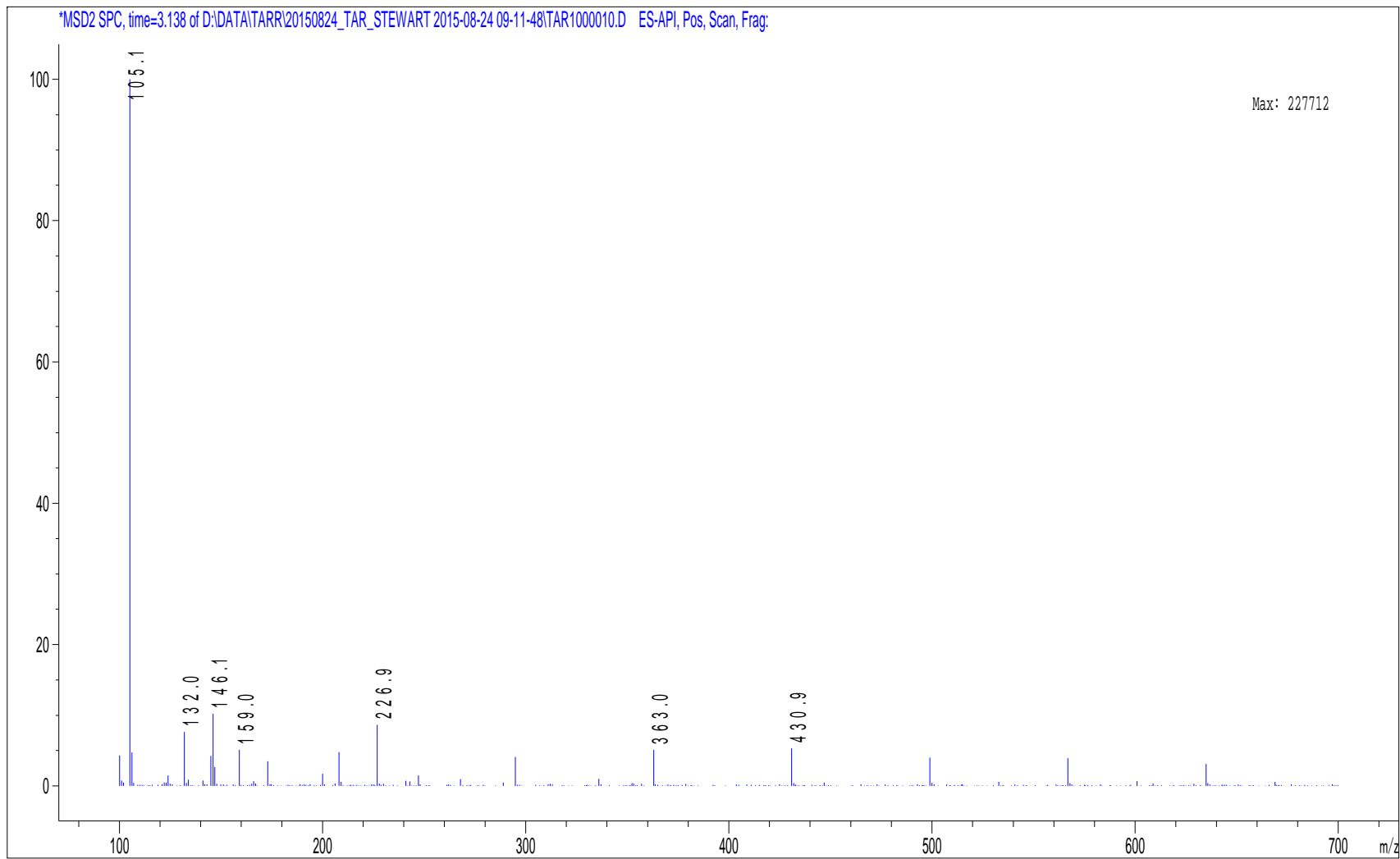
22-Jun-15

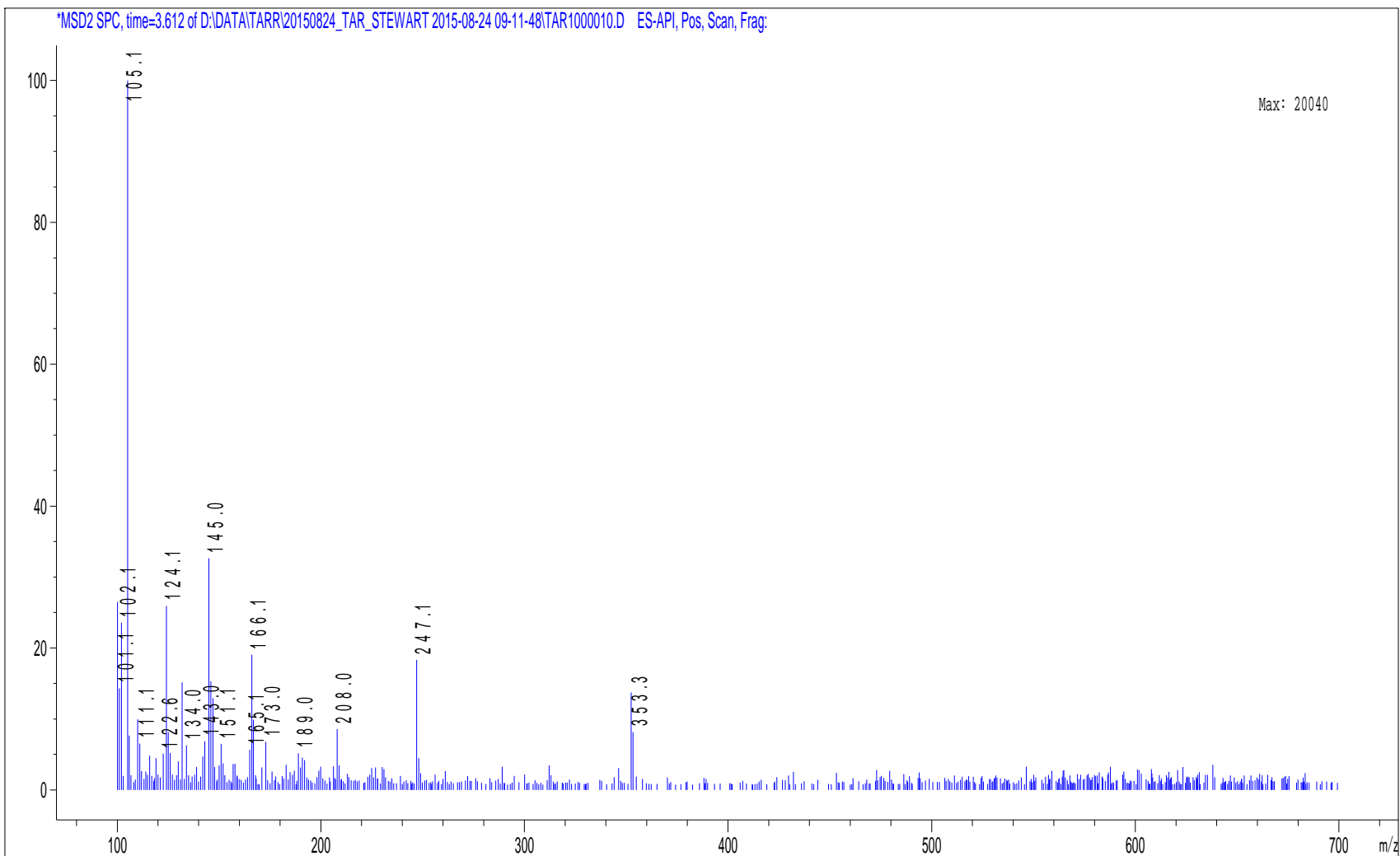
20 DC

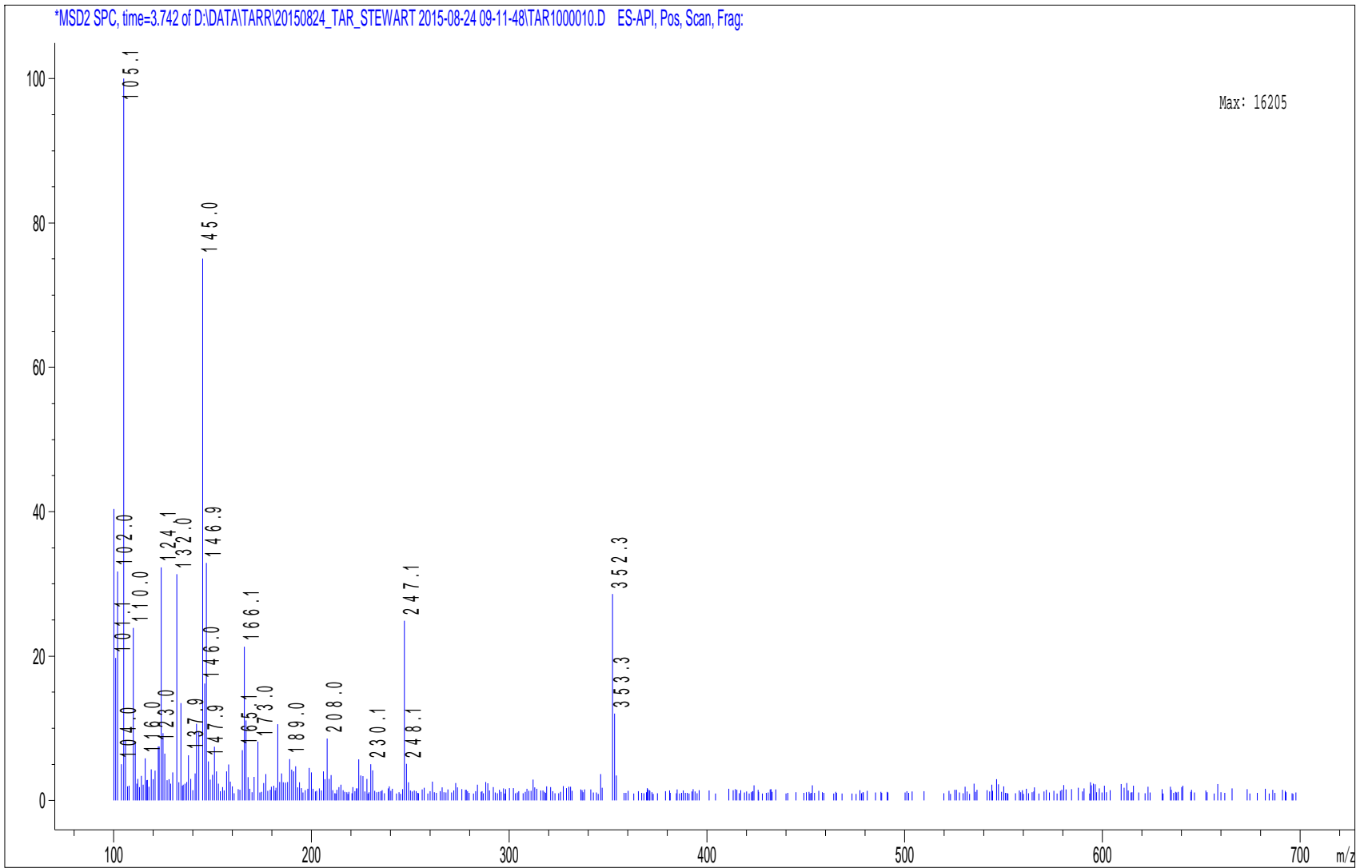
P2-B-09



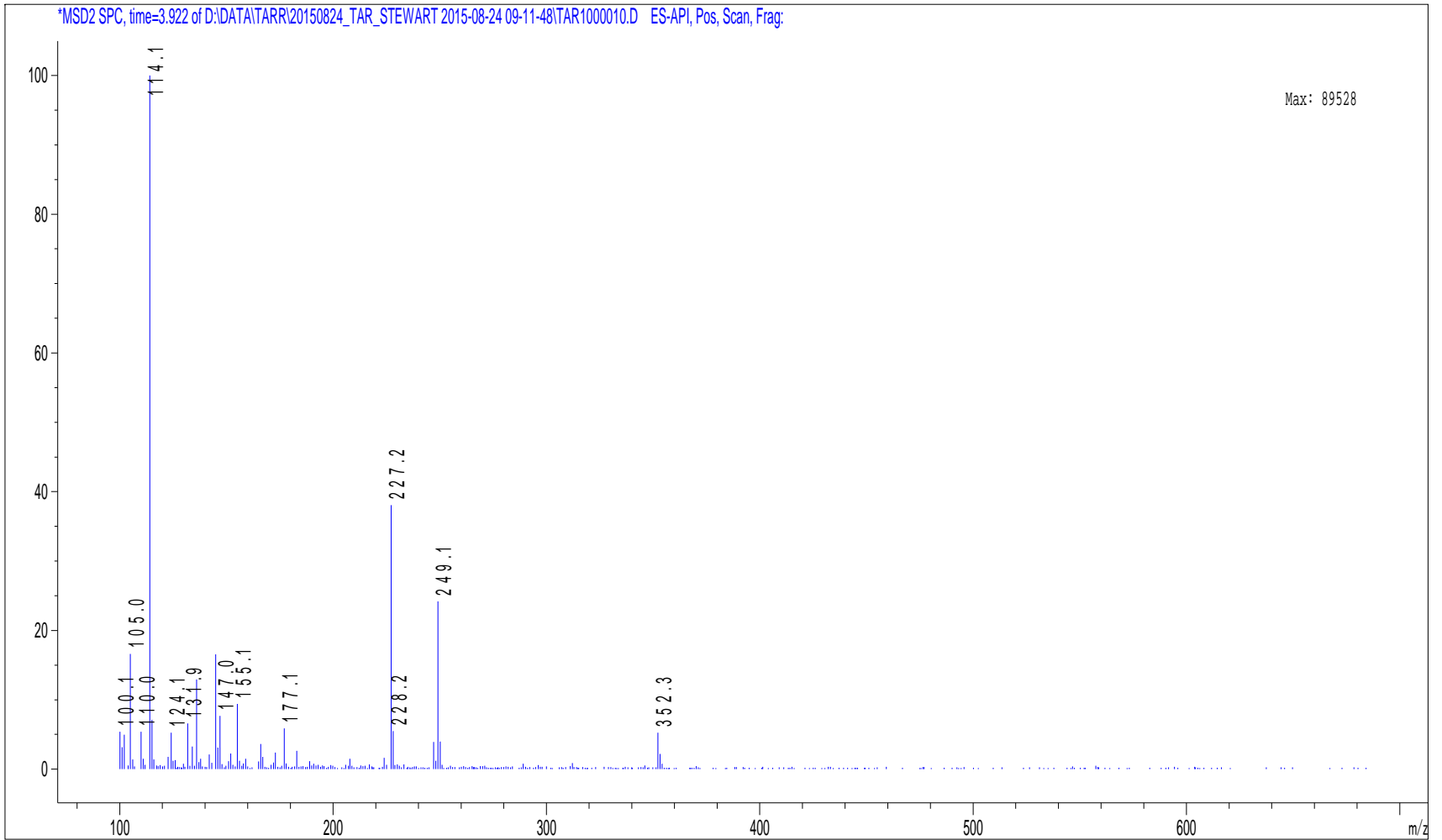








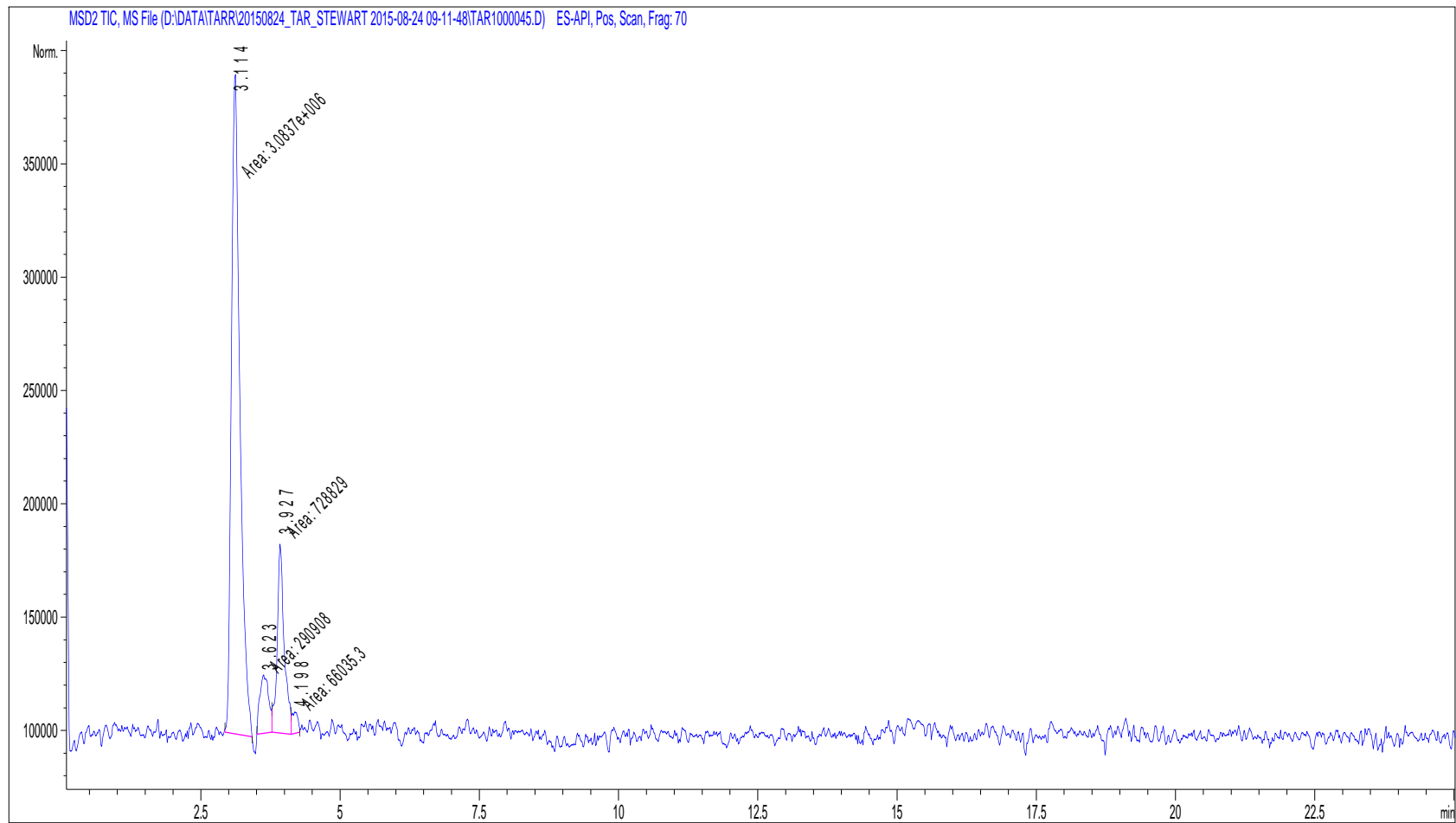


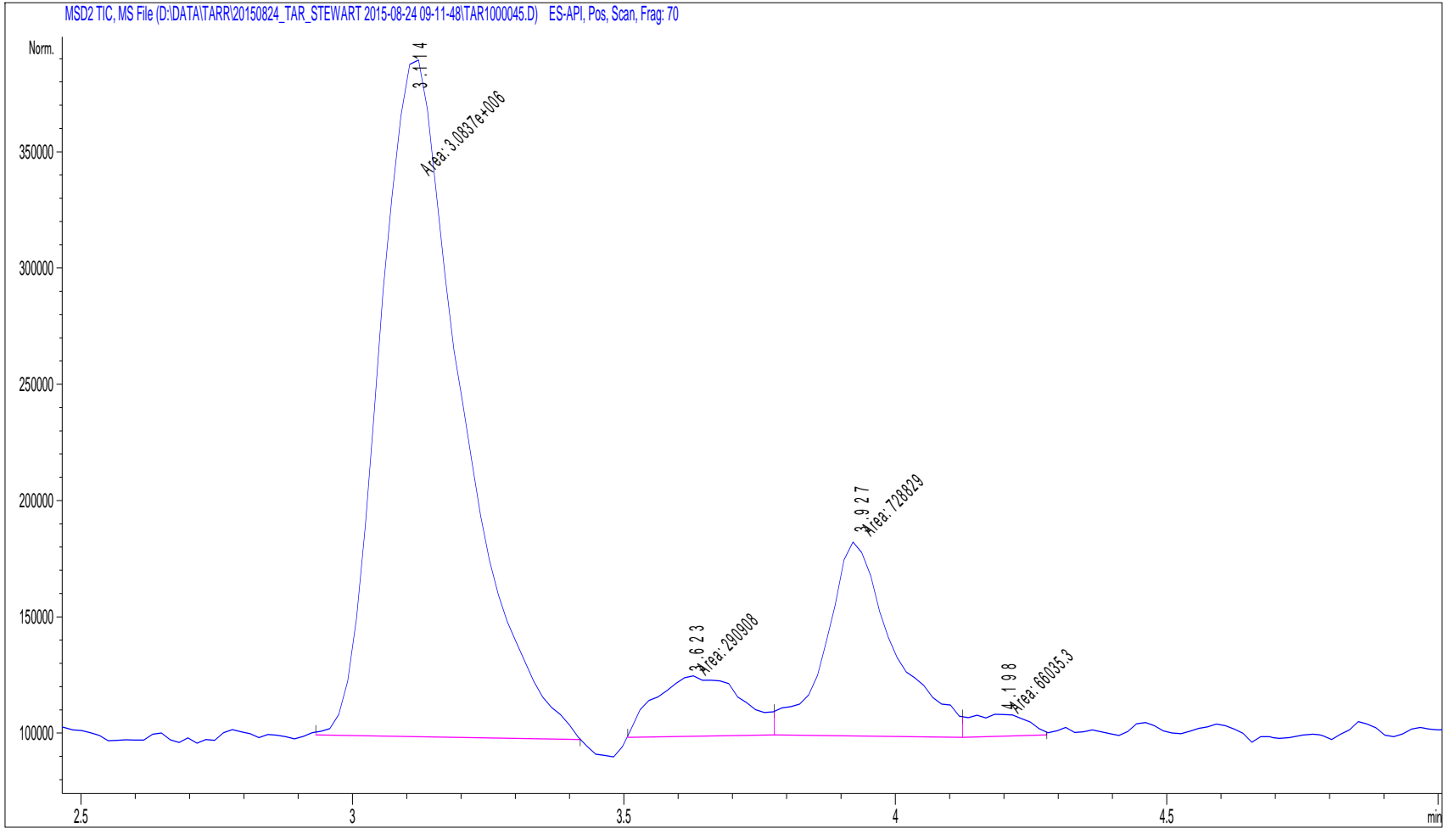


5-Aug-15

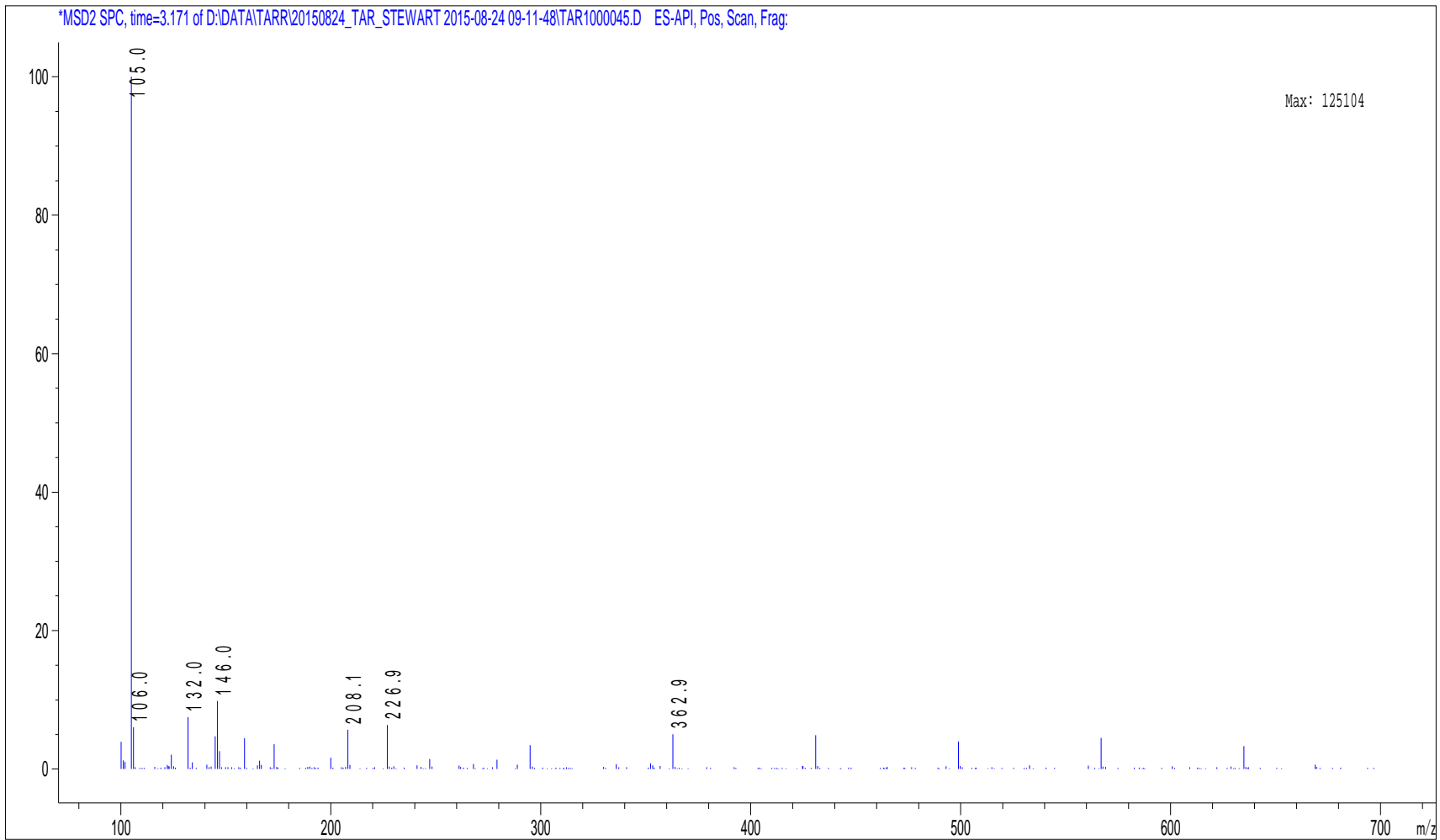
30 DC

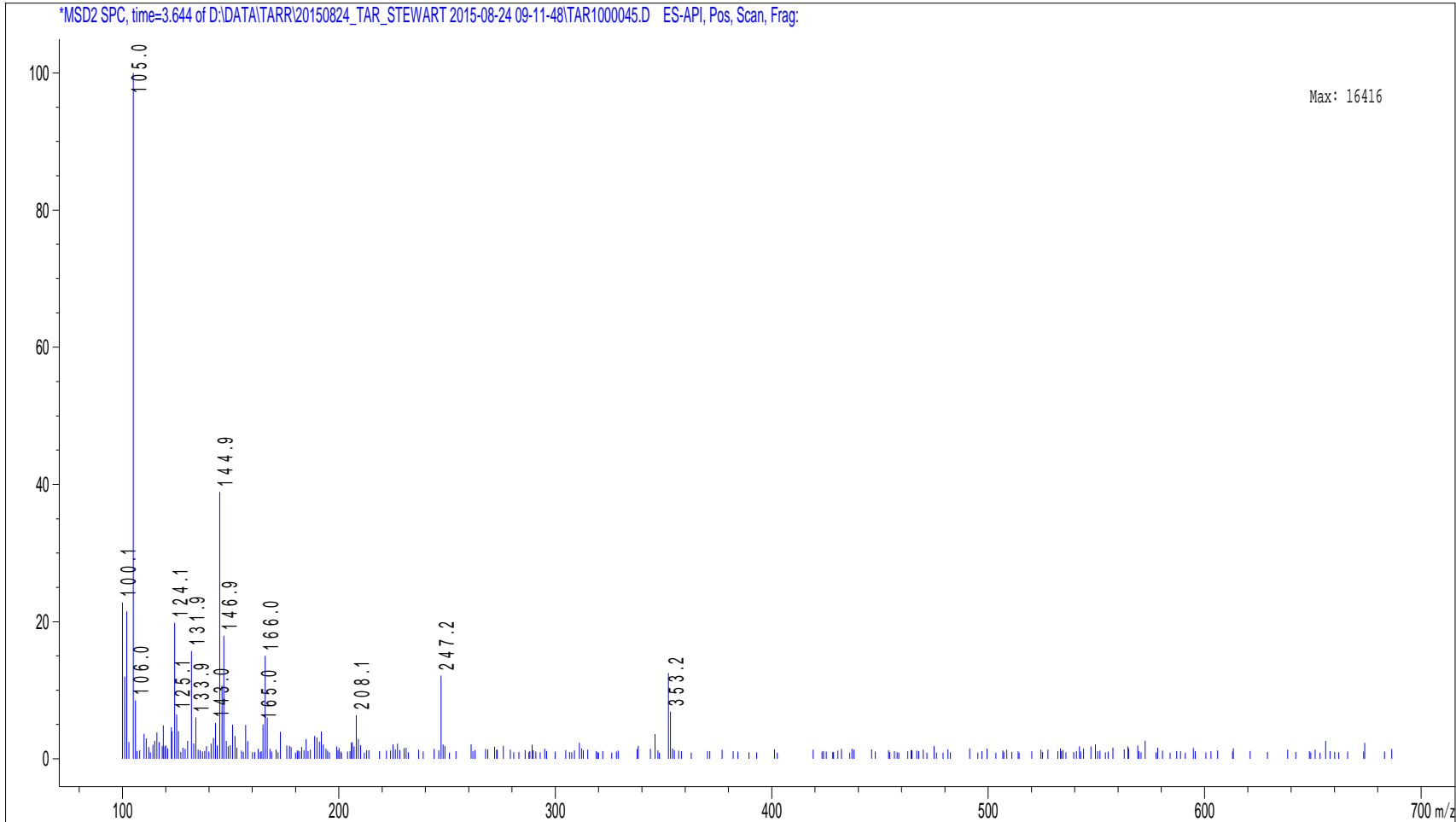
P2-E-09



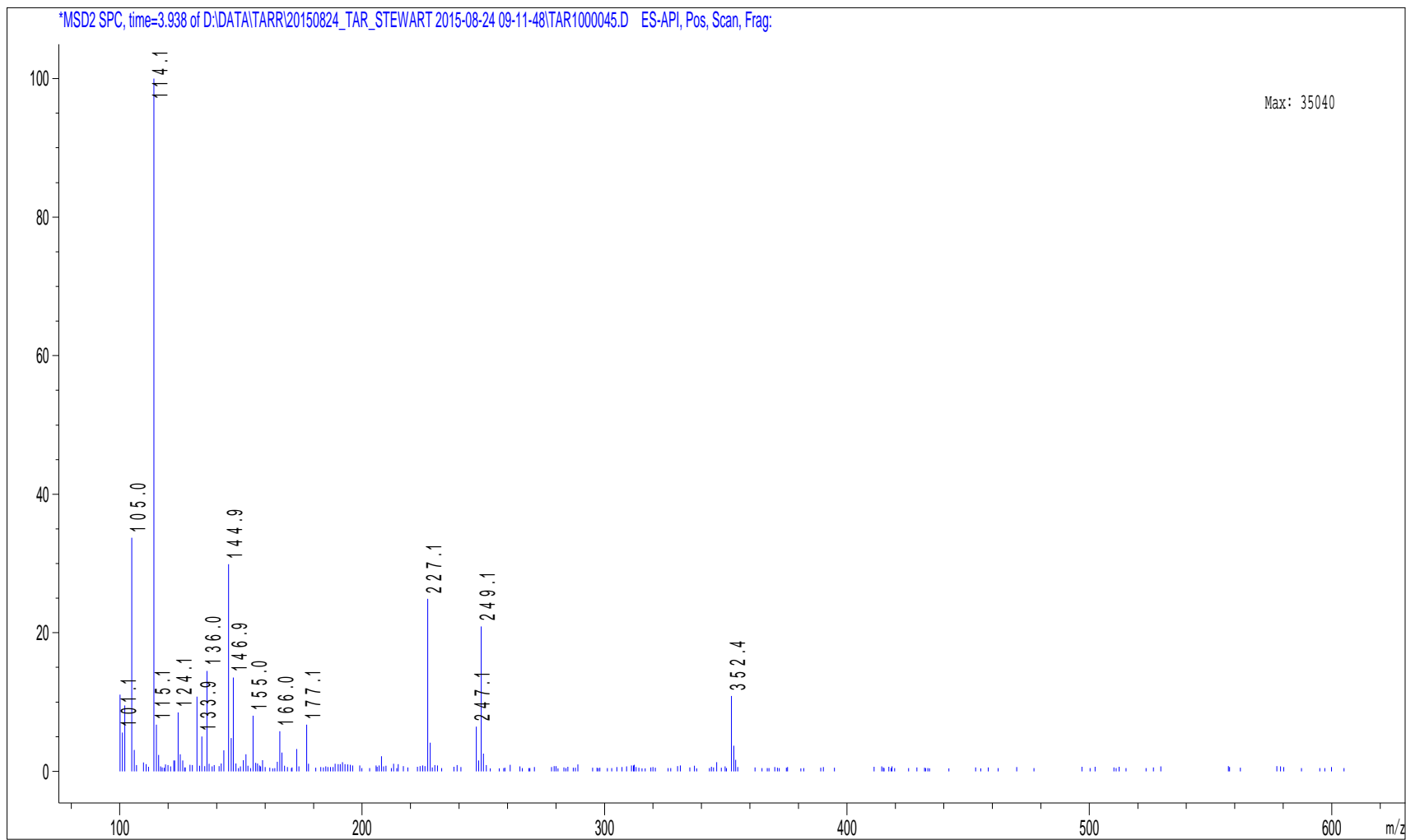


\*MSD2 SPC, time=3.171 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000045.D ES-API, Pos, Scan, Frag;

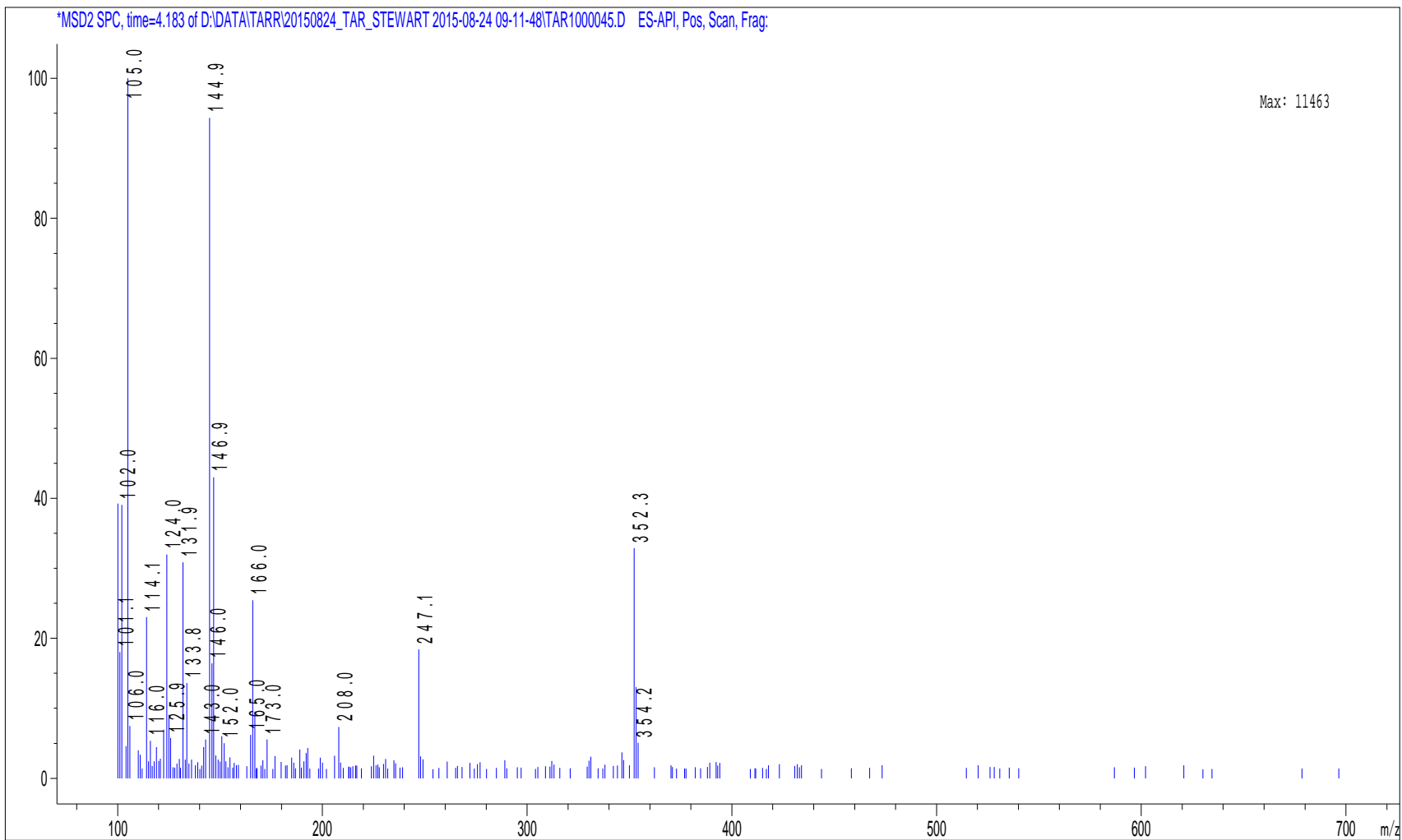




\*MSD2 SPC, time=3.938 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000045.D ES-API, Pos, Scan, Frag:



\*MSD2 SPC, time=4.183 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000045.D ES-API, Pos, Scan, Frag:

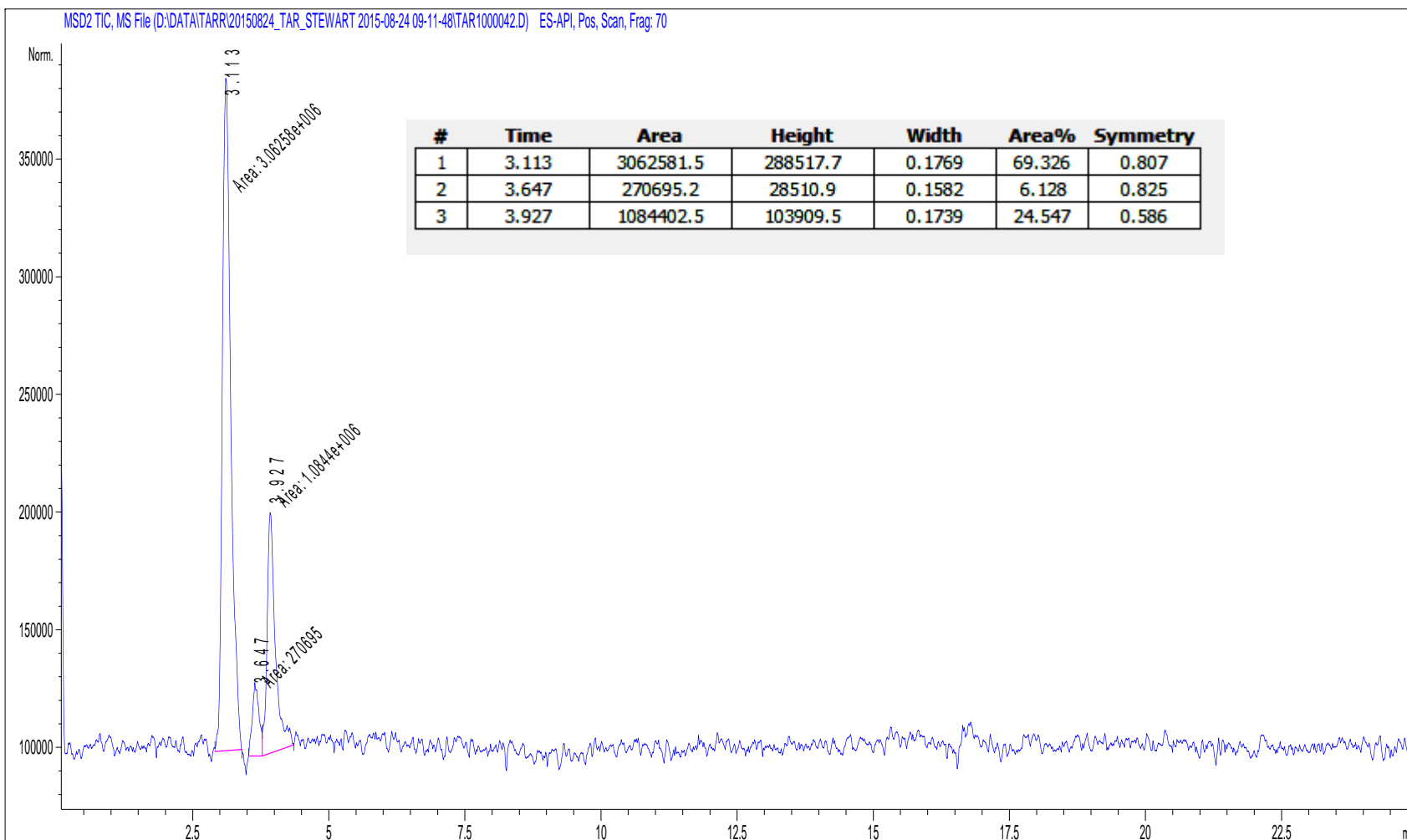


Max: 11463

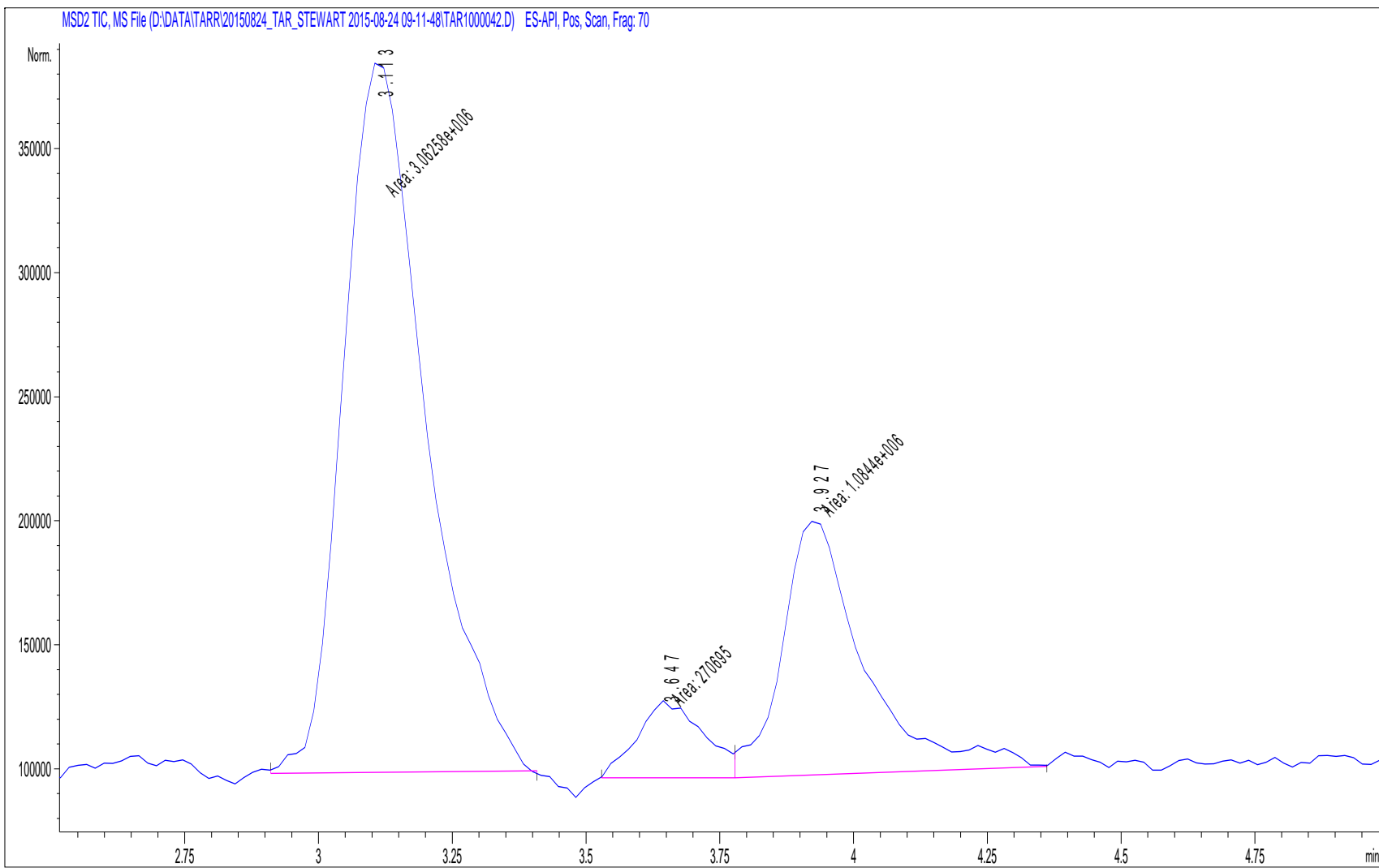
7-May-15

50 DC

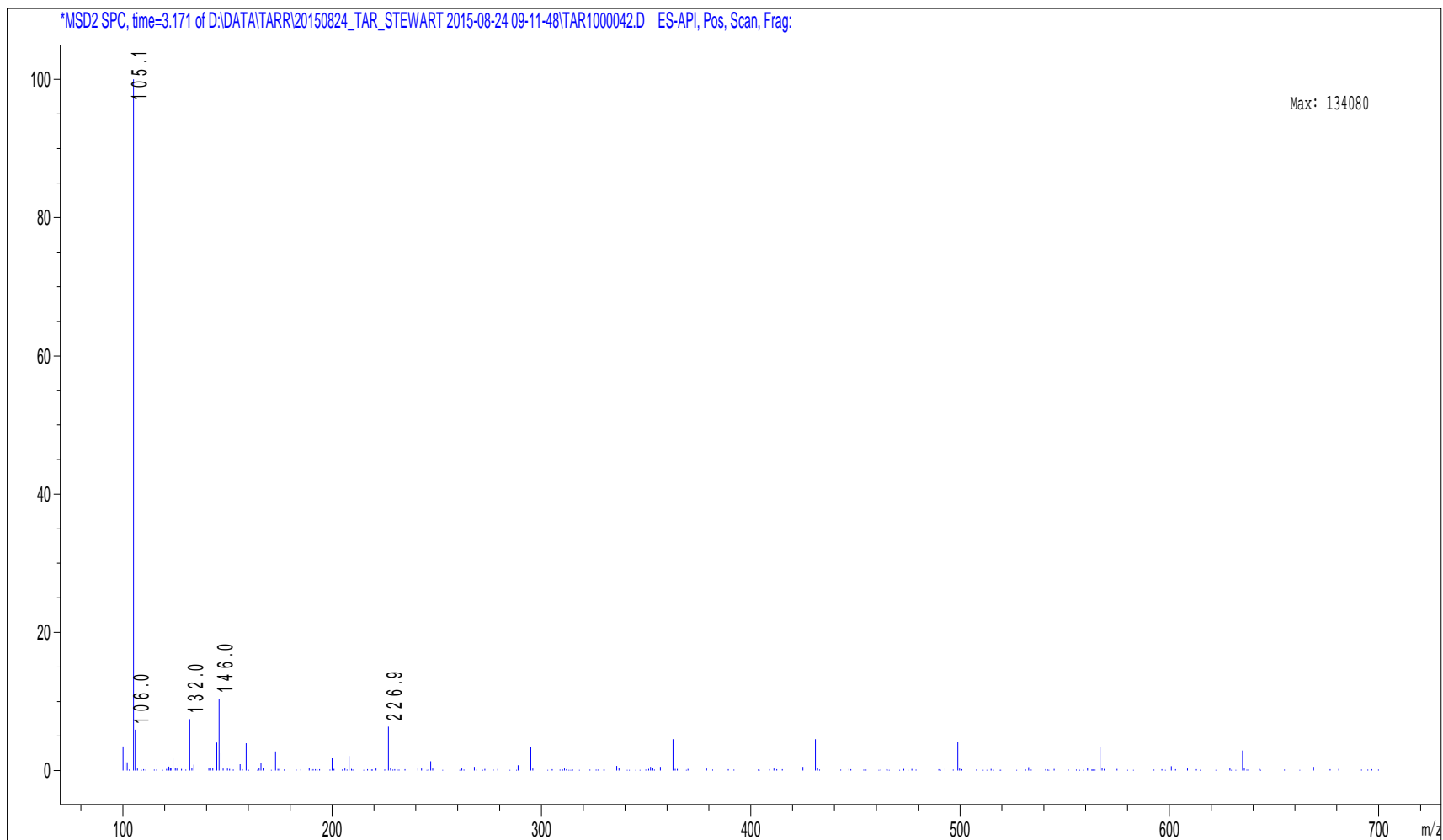
P2-E-06



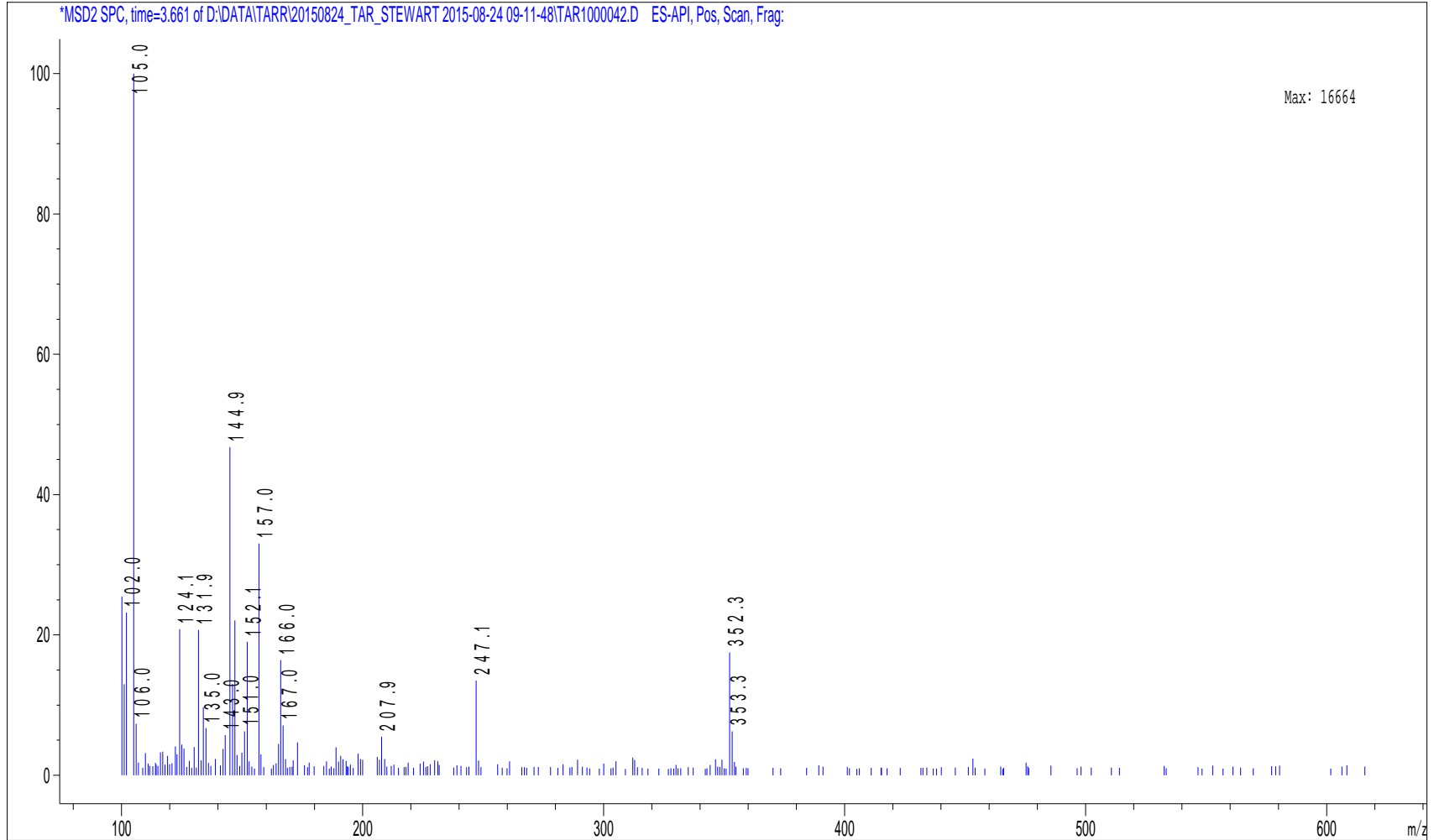




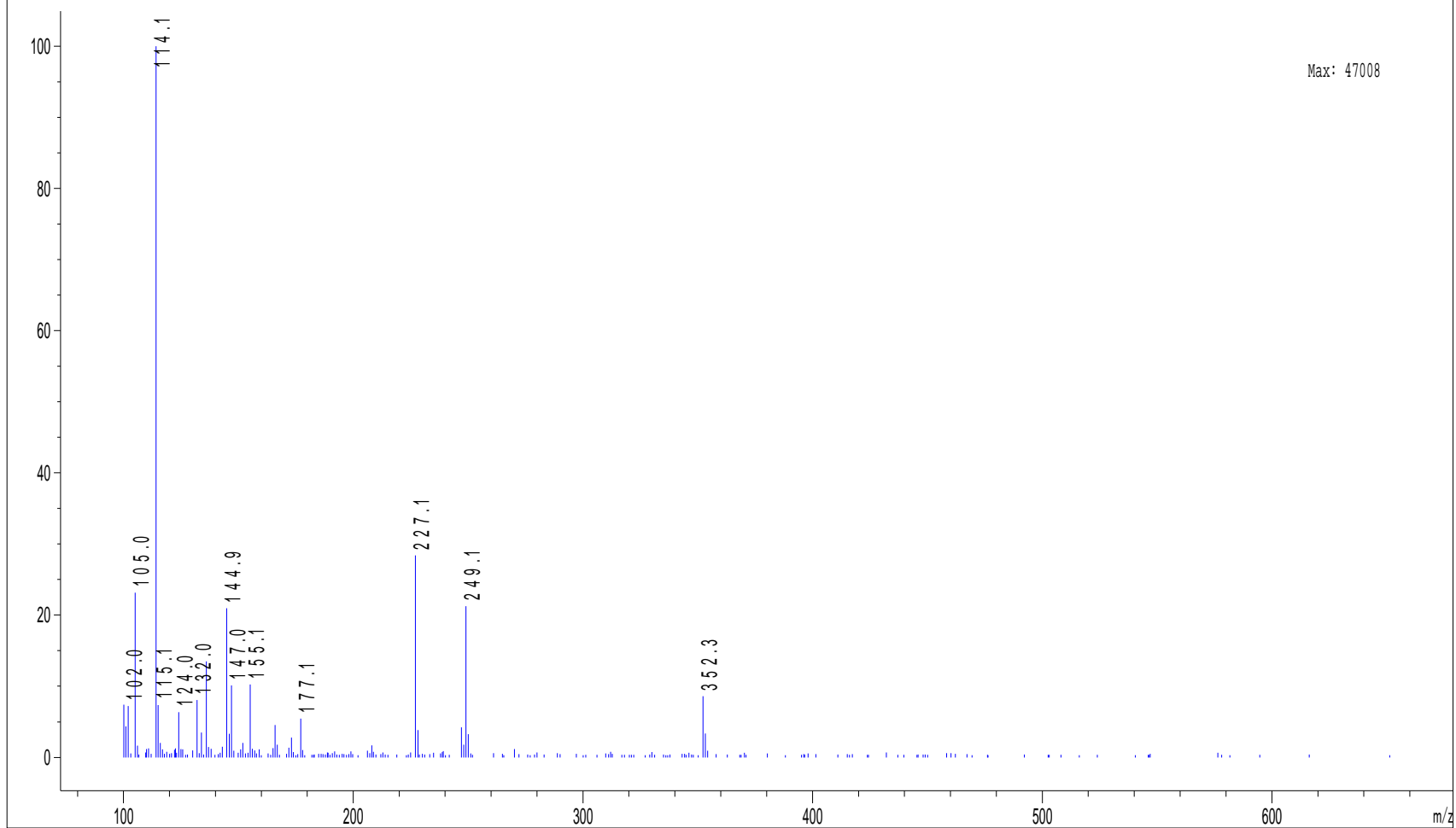
\*MSD2 SPC, time=3.171 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000042.D ES-API, Pos, Scan, Frag:



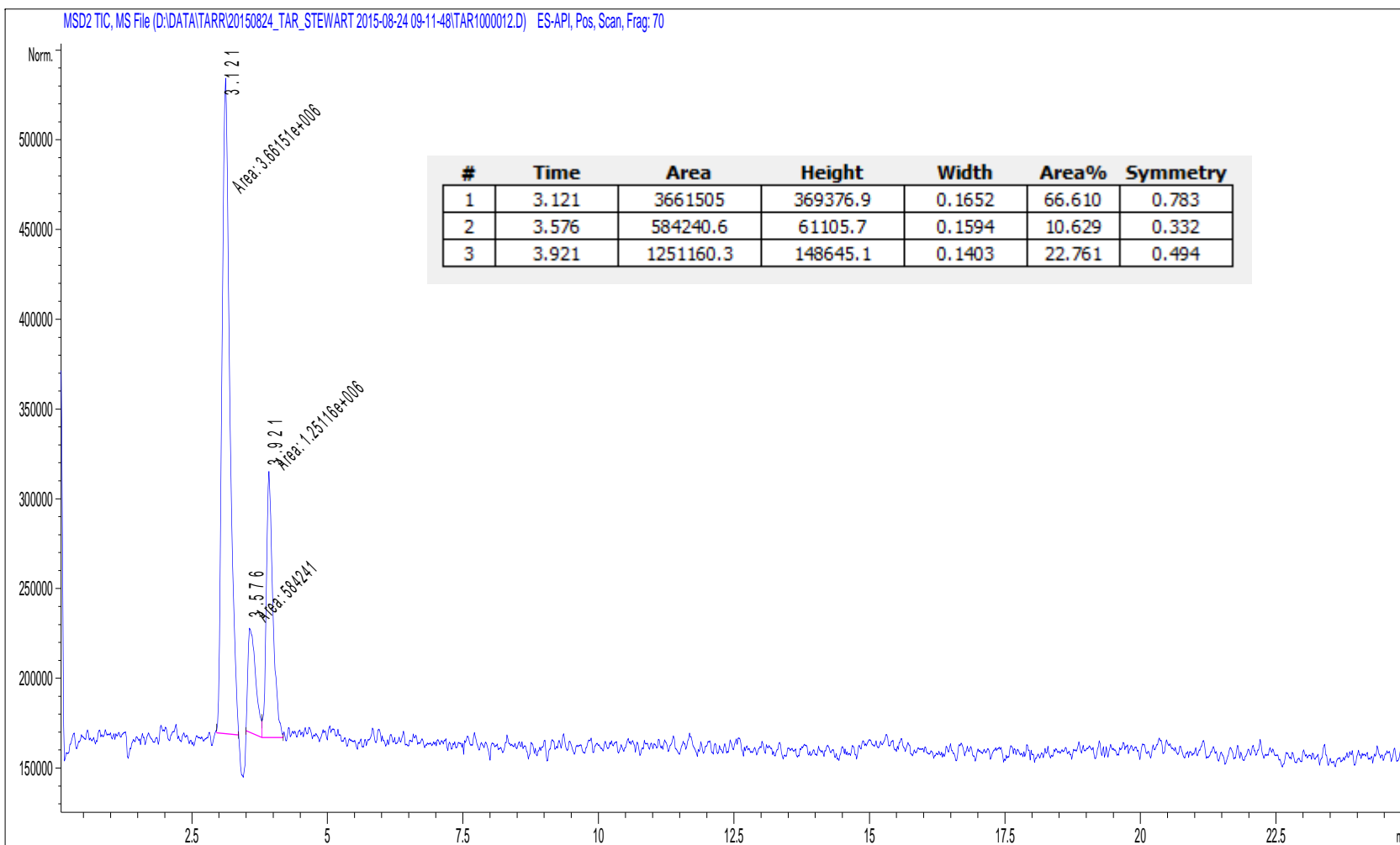
\*MSD2 SPC, time=3.661 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000042.D ES-API, Pos, Scan, Frag:

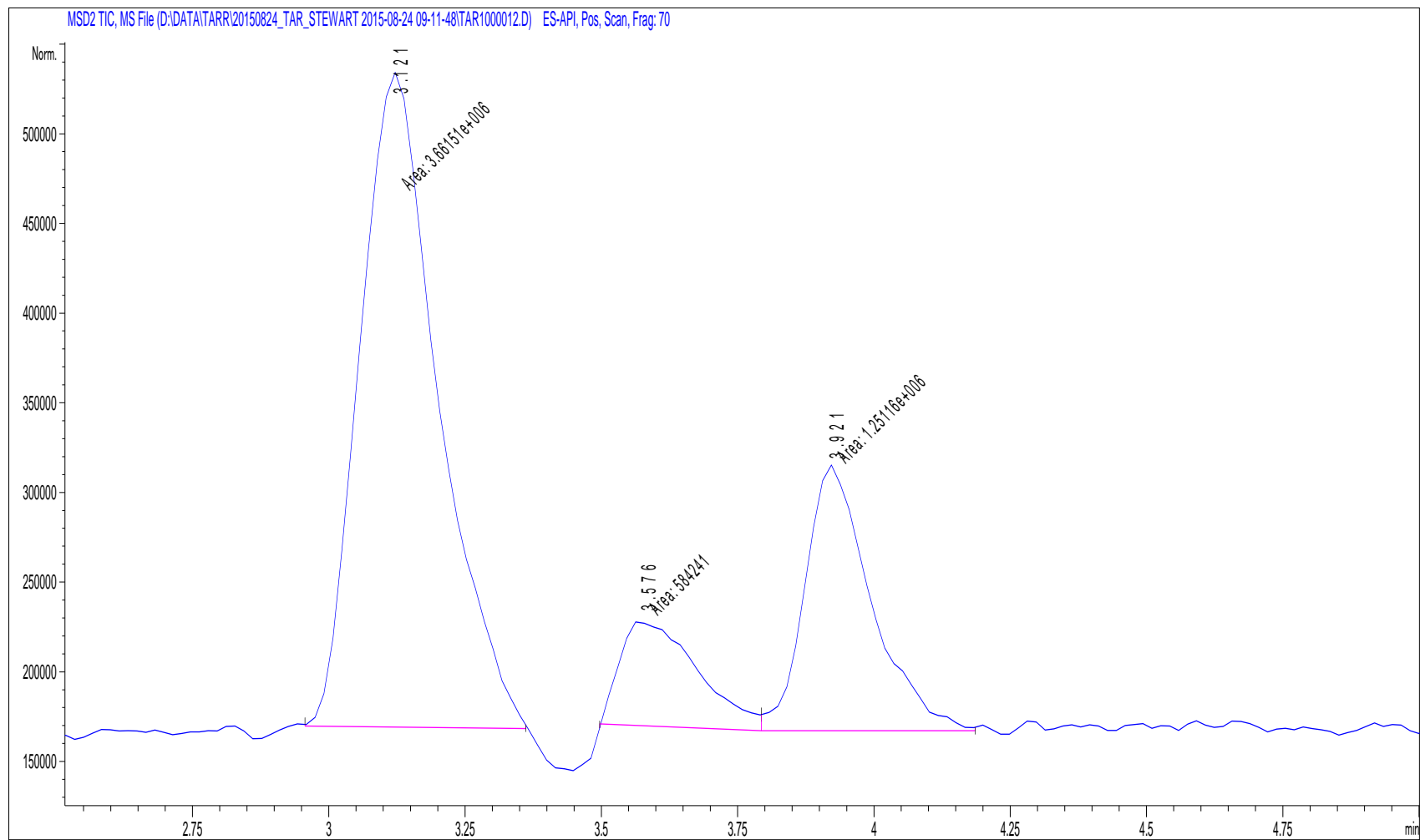


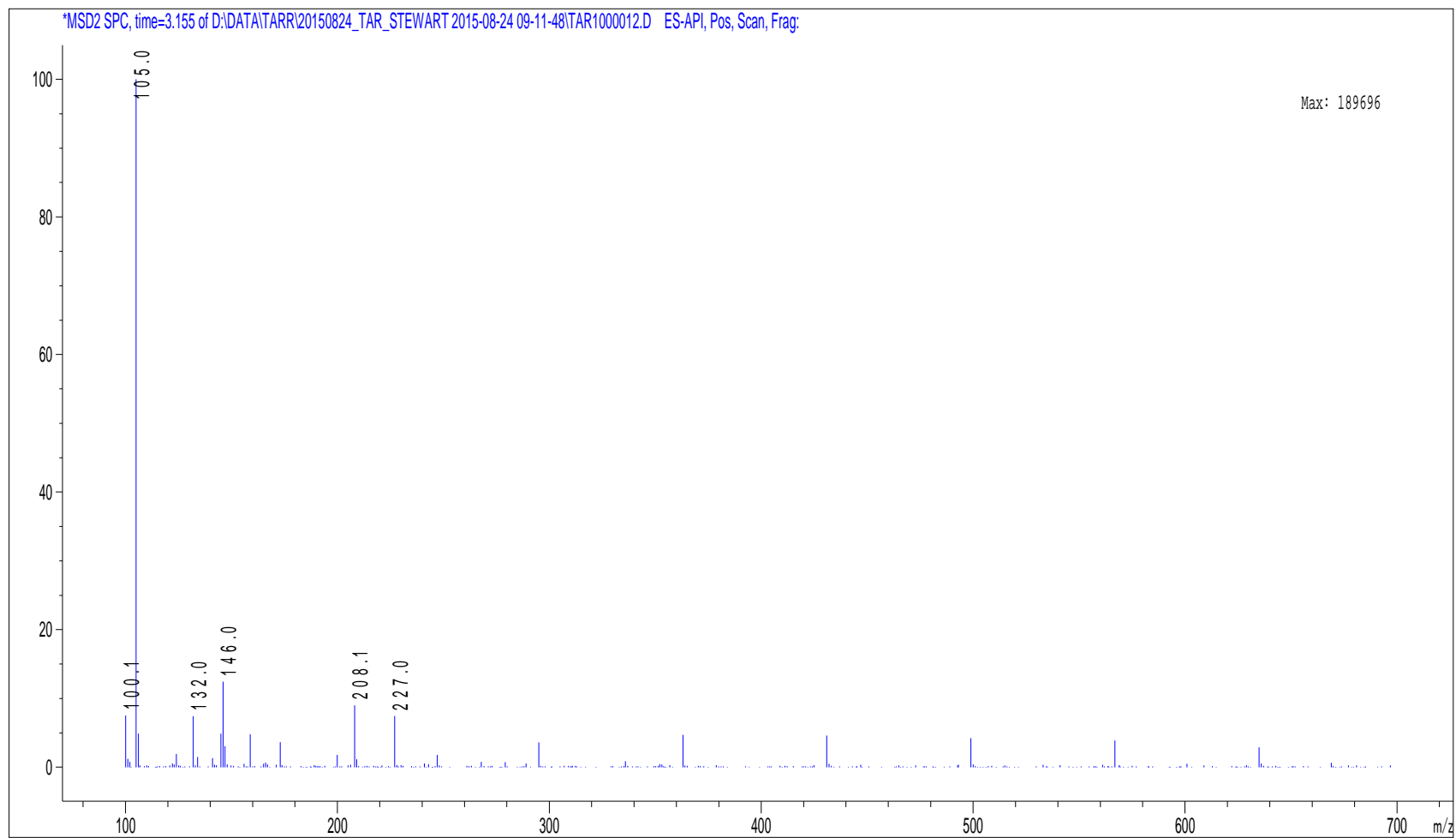
\*MSD2 SPC, time=3.938 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000042.D ES-API, Pos, Scan, Frag:

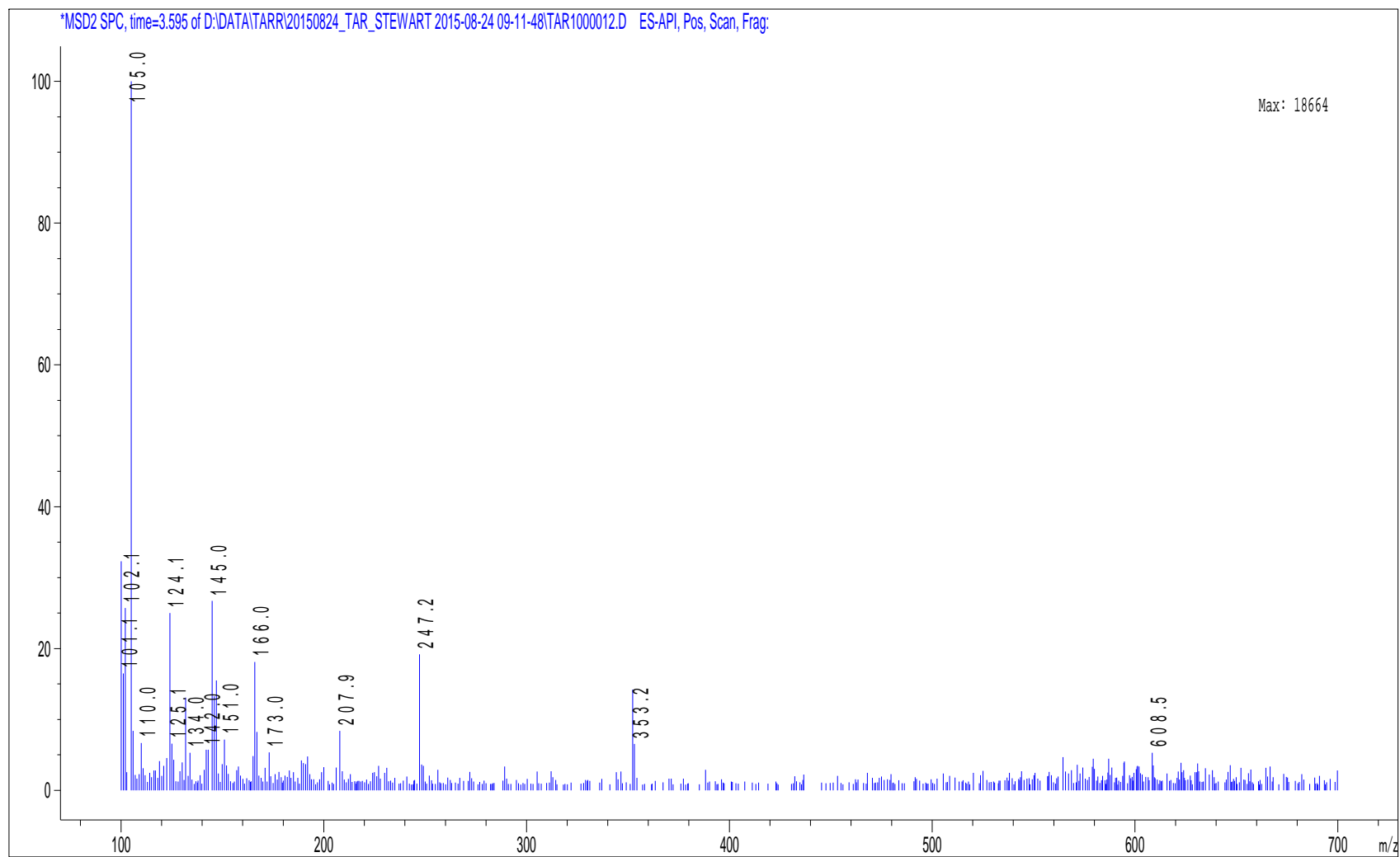


15-Jun-15  
50 DC Repeat  
P2-B-07

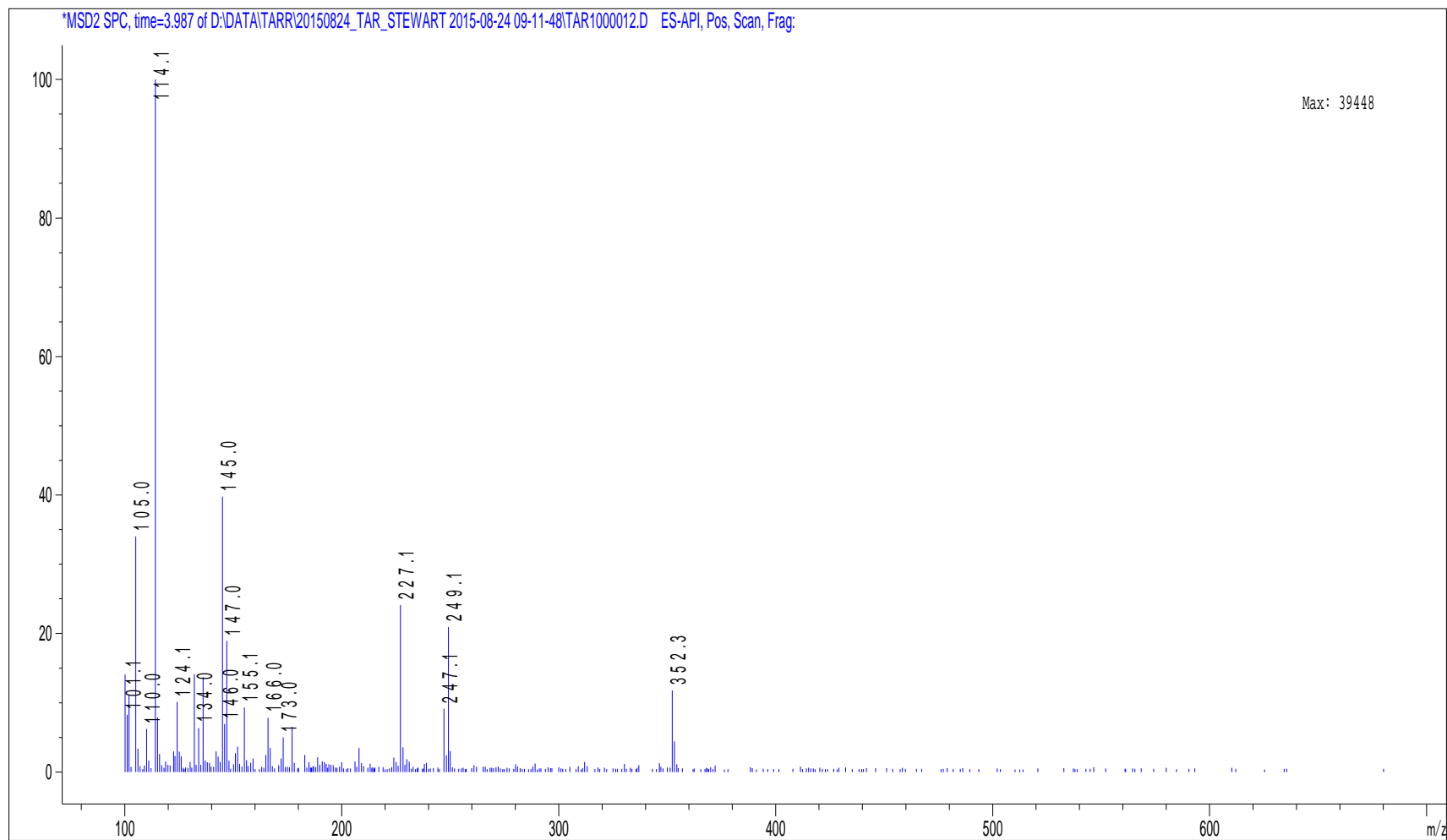








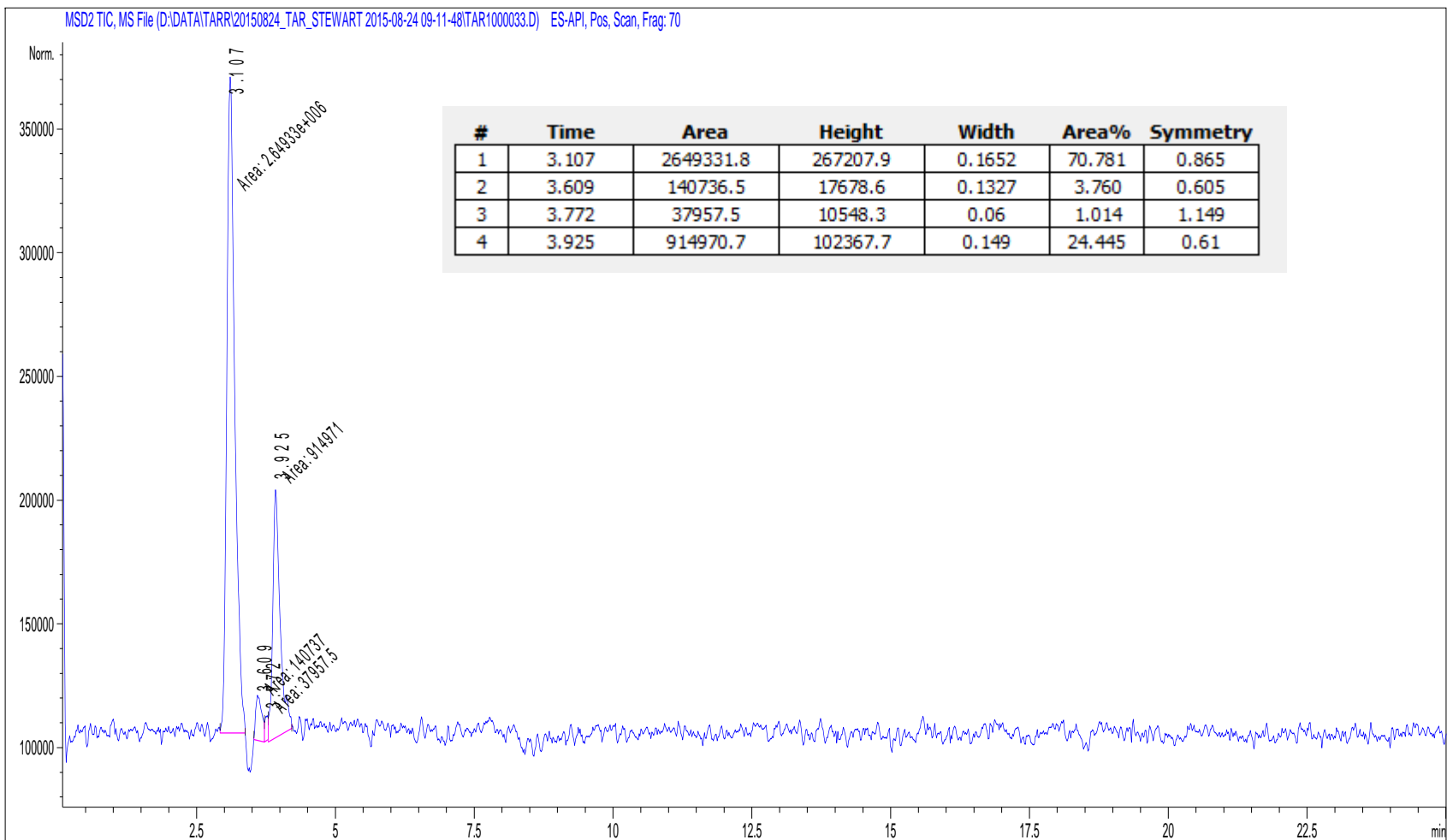


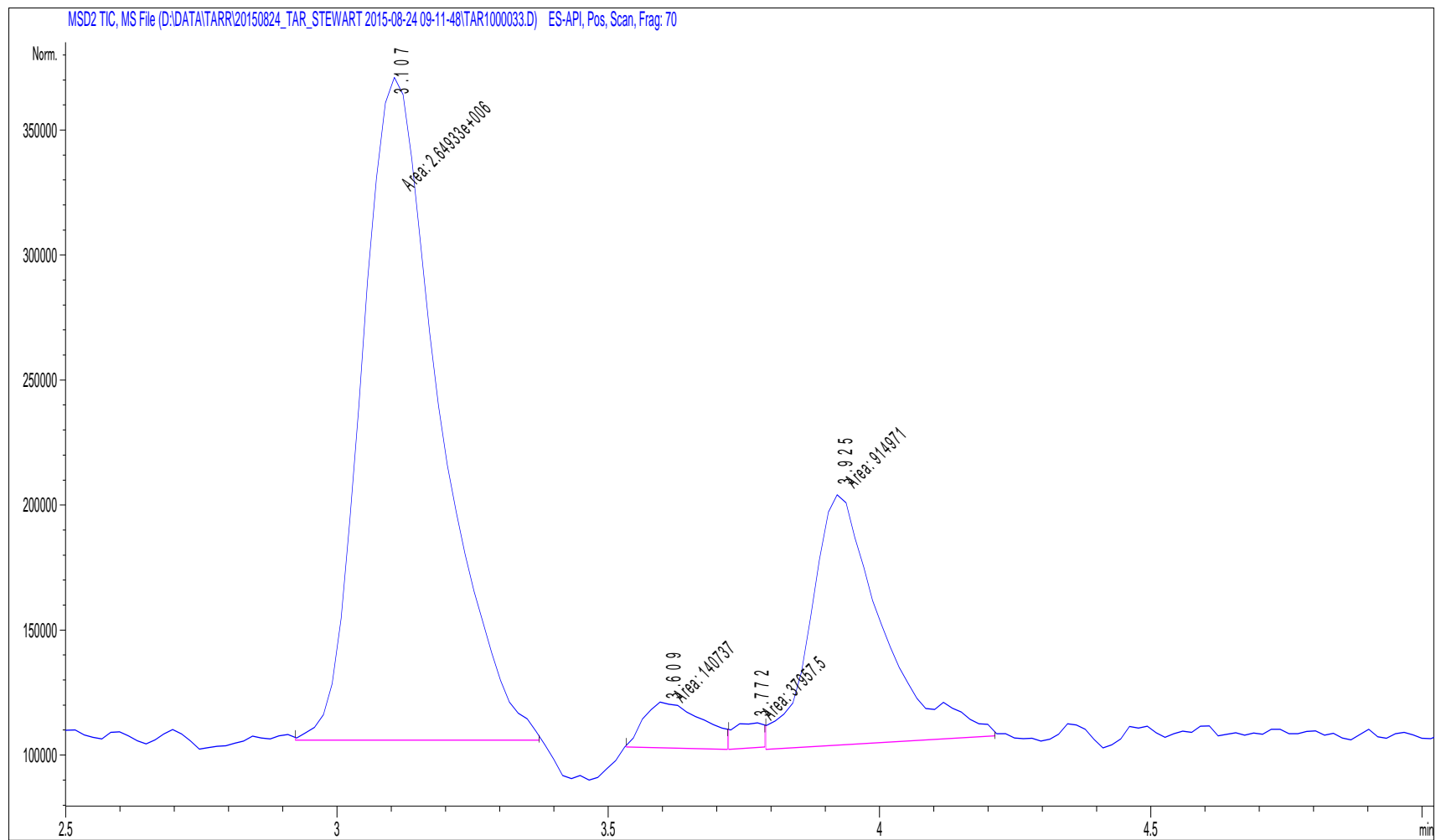


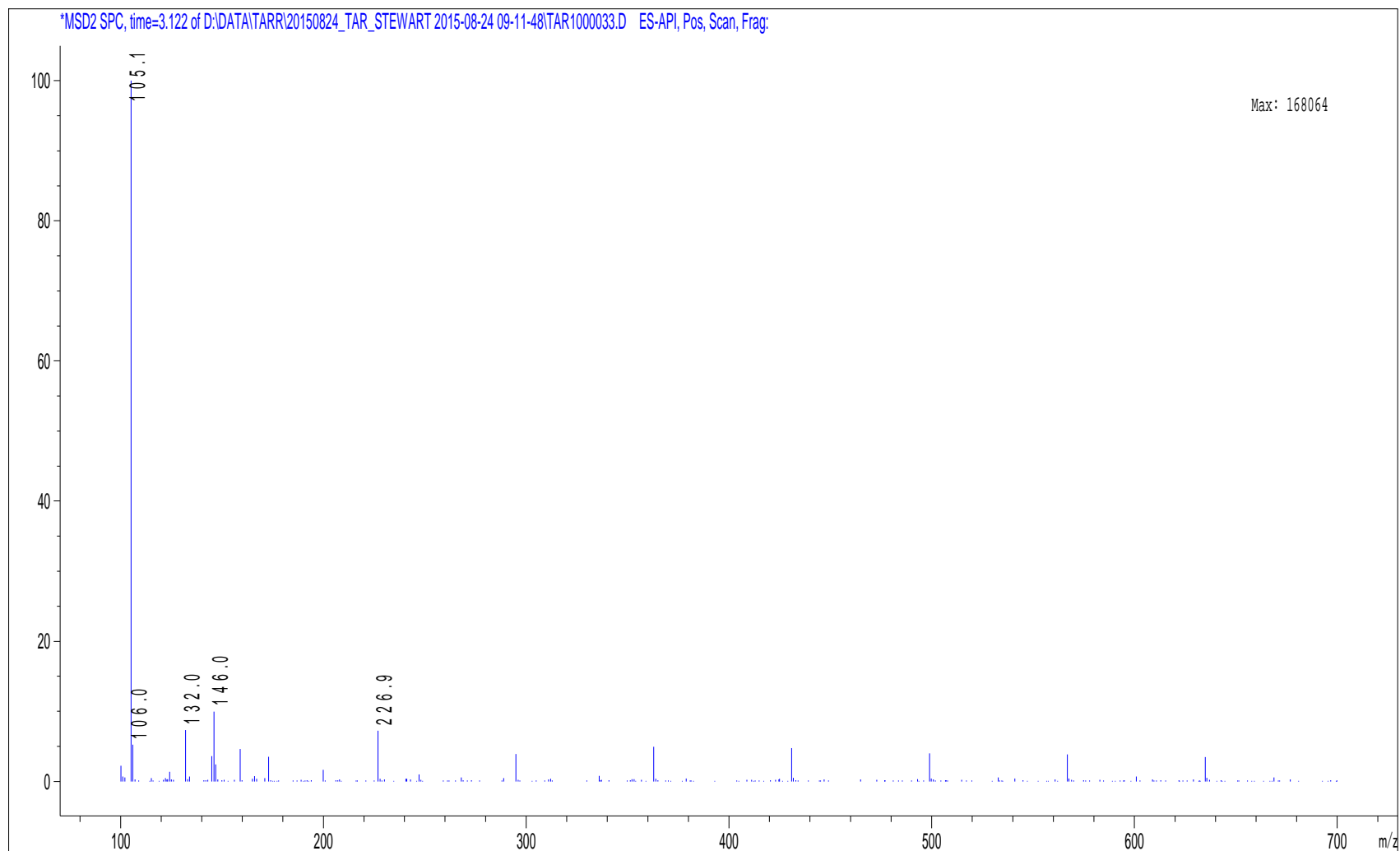
23-Jul-15

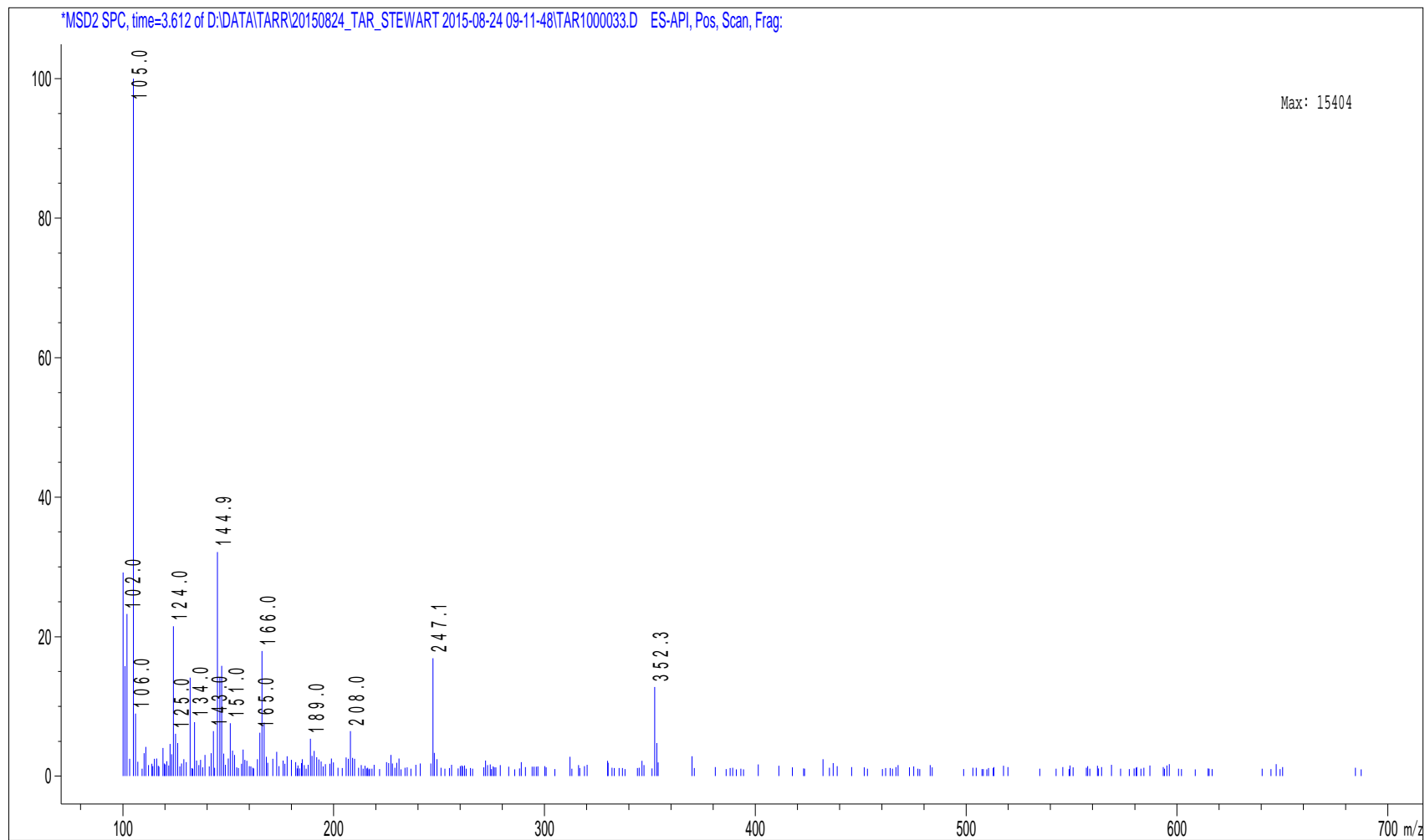
70 DC

P2-D-04

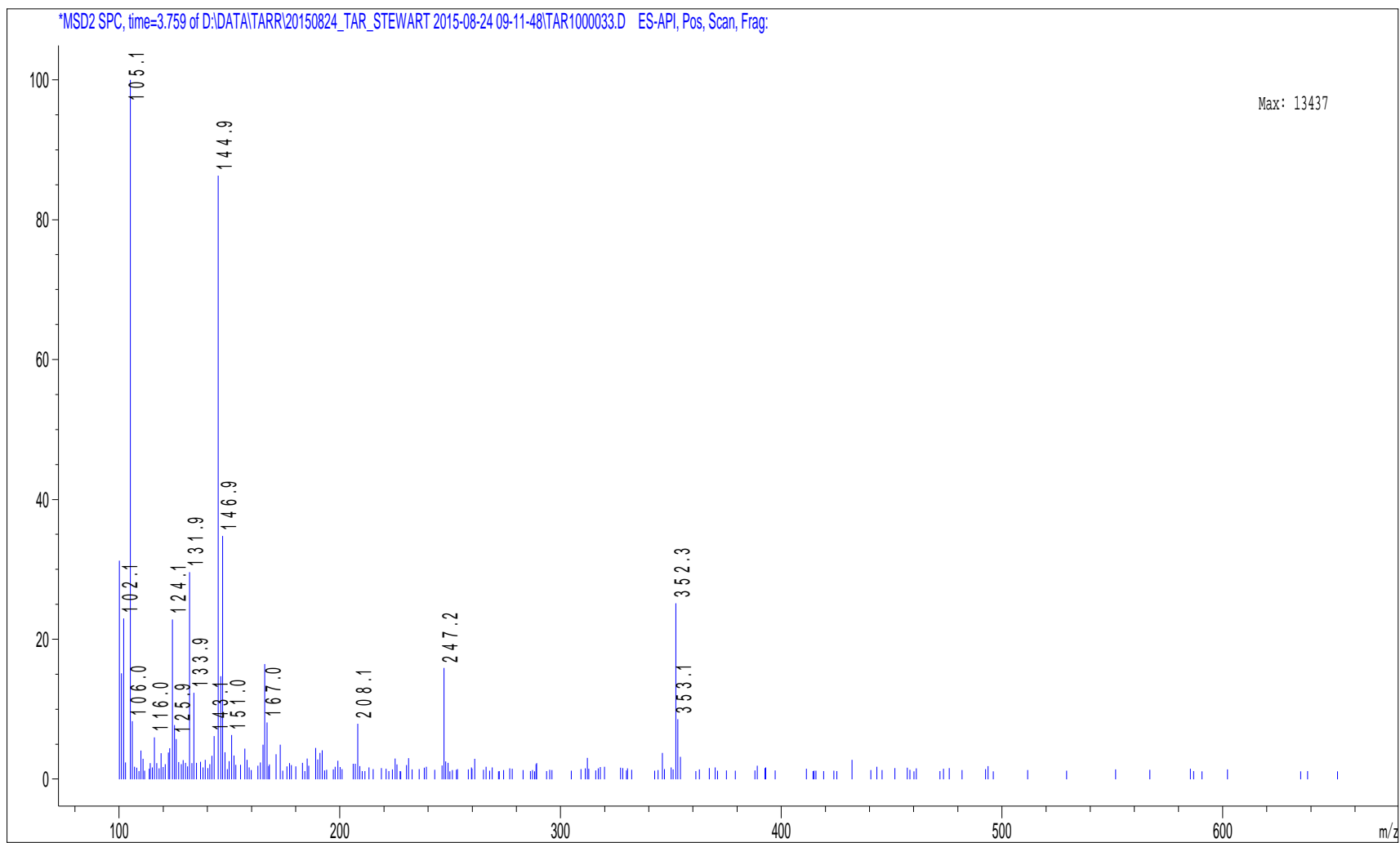






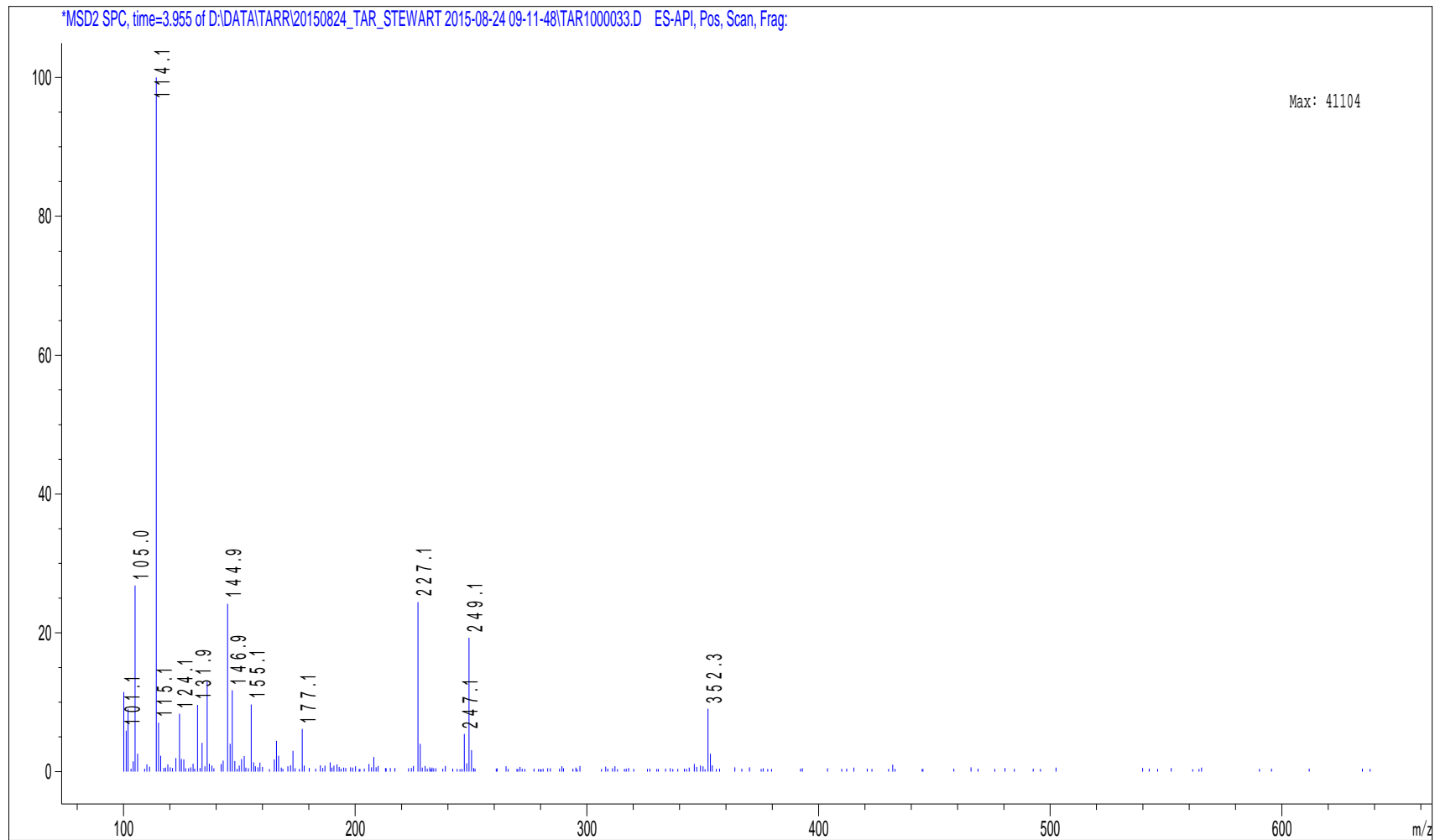


\*MSD2 SPC, time=3.759 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000033.D ES-API, Pos, Scan, Frag:

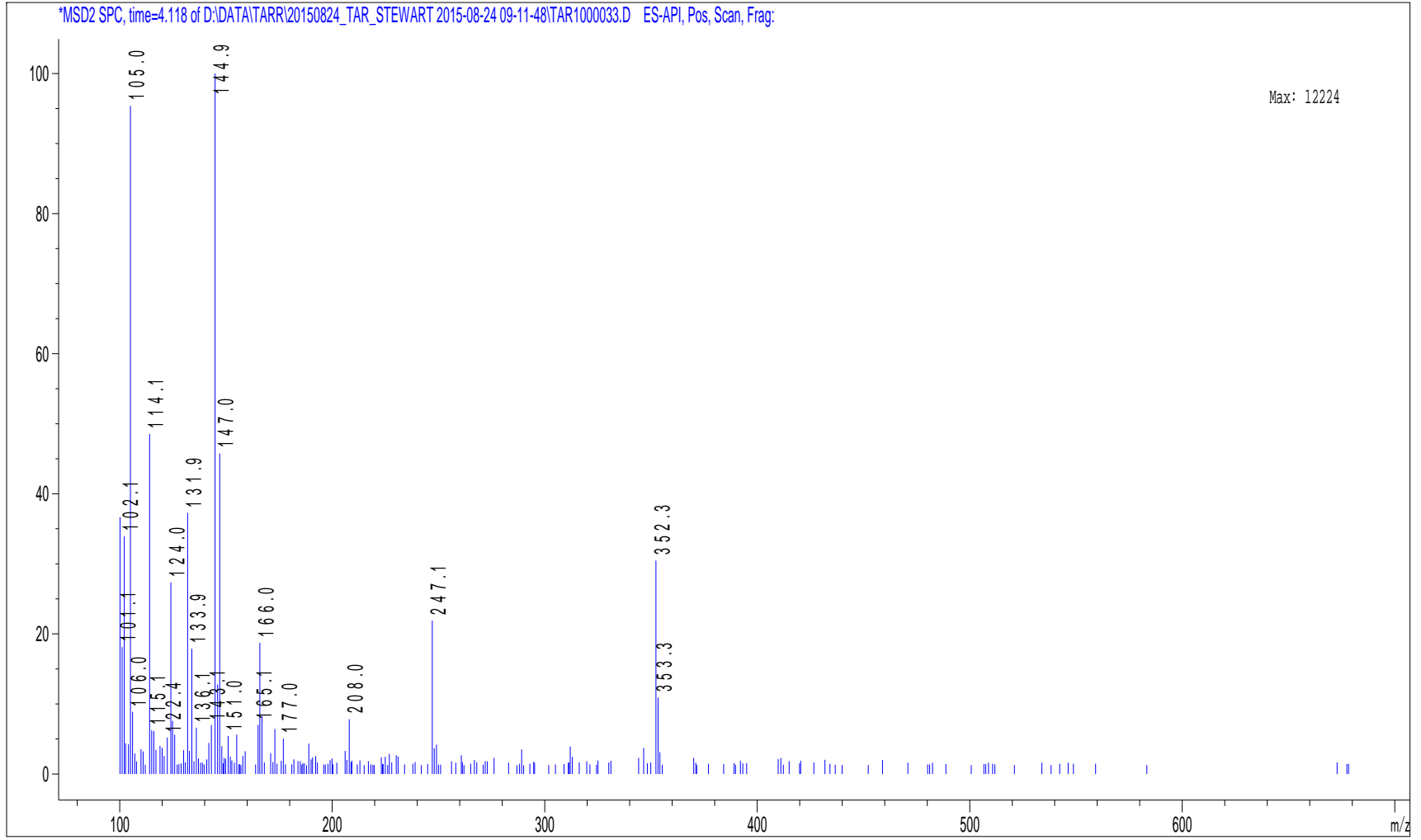


Max: 13437

\*MSD2 SPC, time=3.955 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000033.D ES-API, Pos, Scan, Frag:



\*MSD2 SPC, time=4.118 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000033.D ES-API, Pos, Scan, Frag:

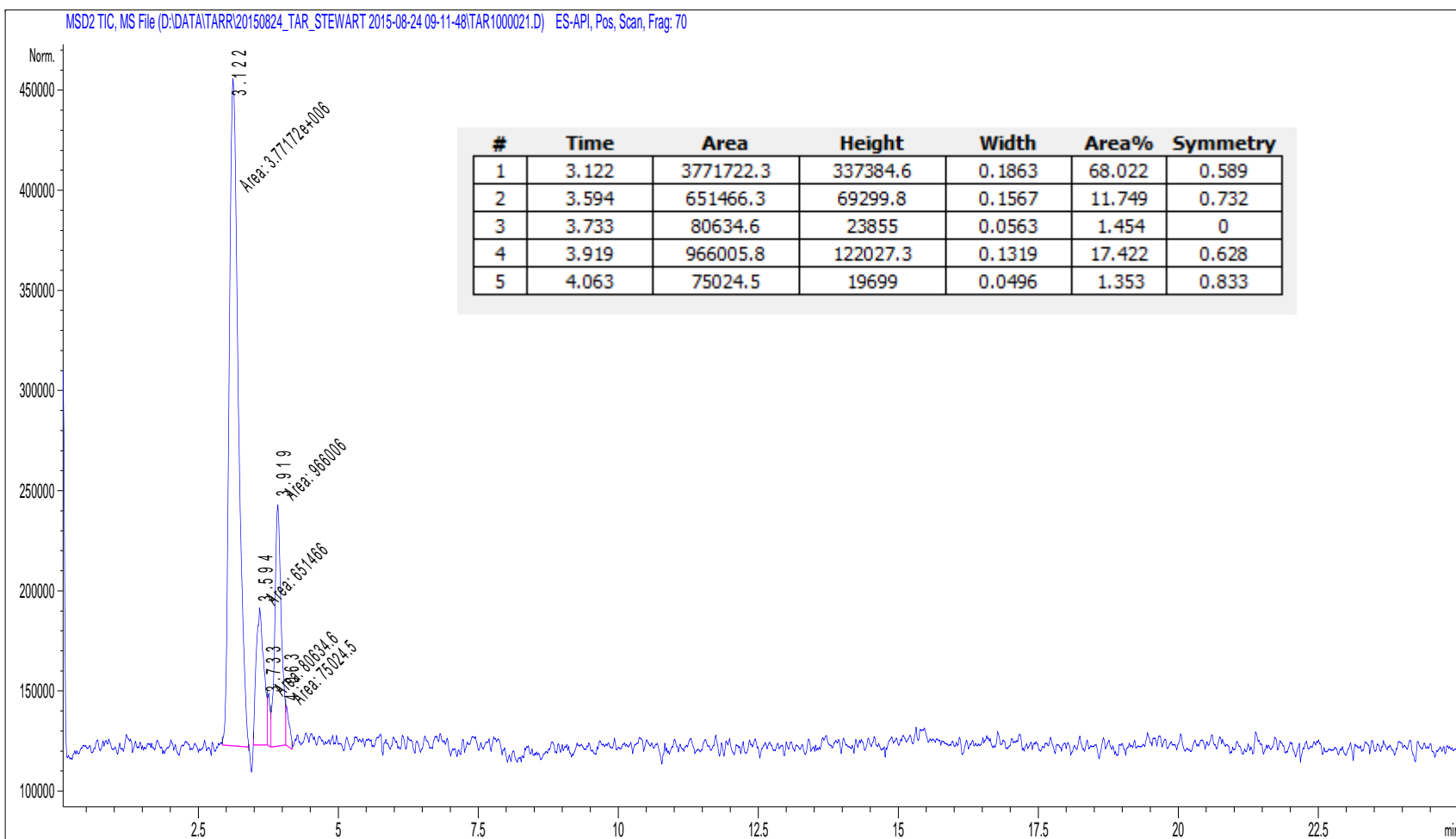


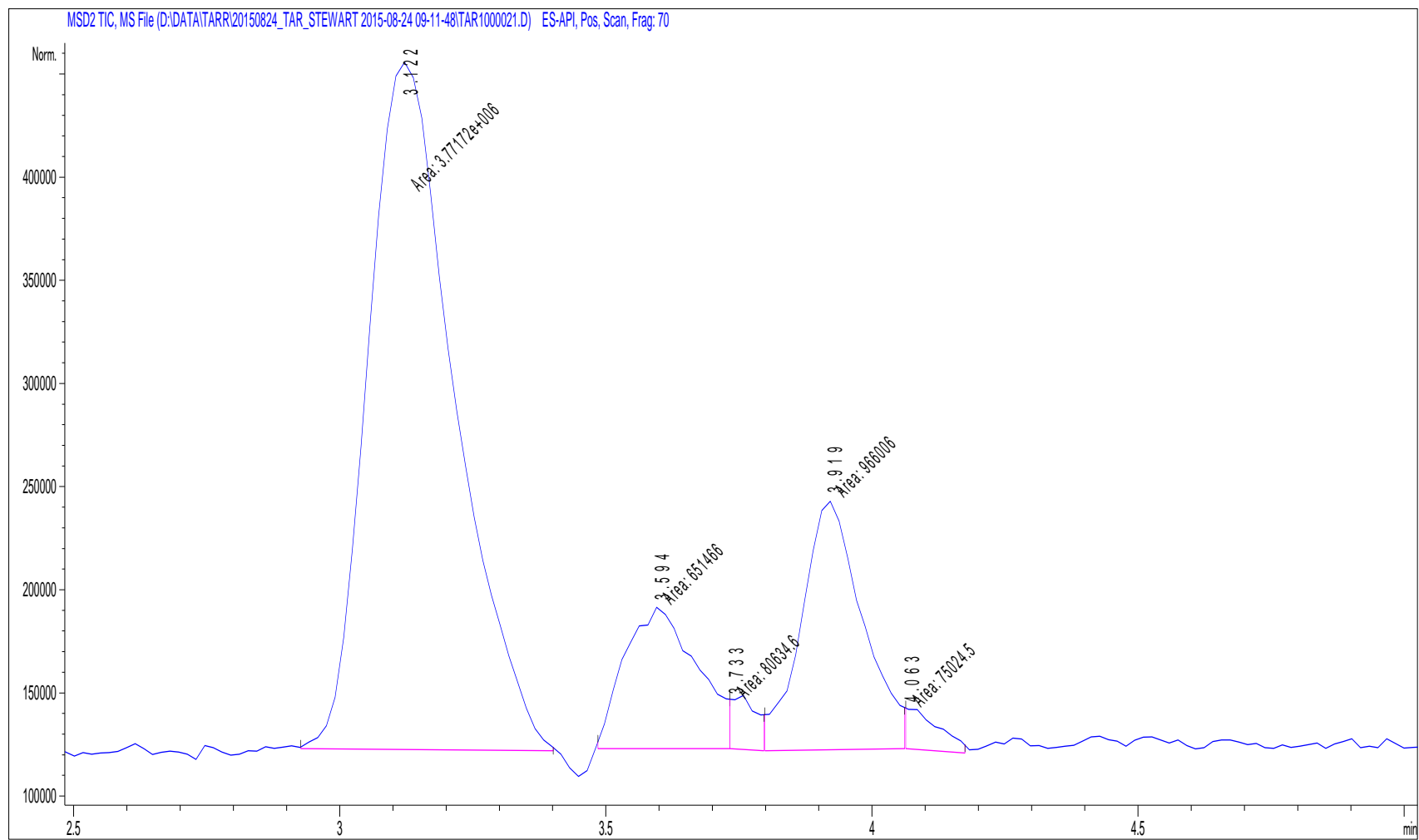


1-Jul-15

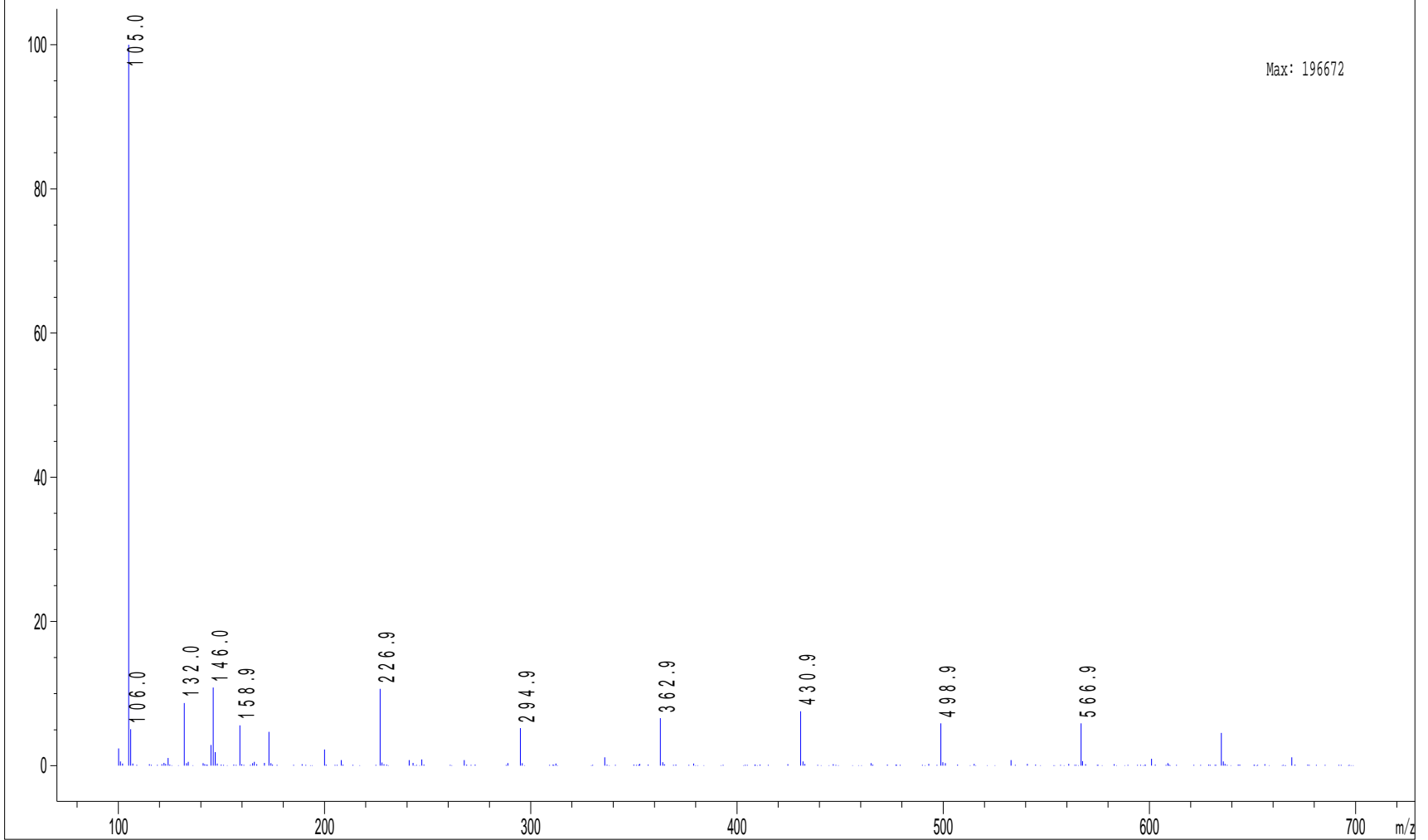
100 DC

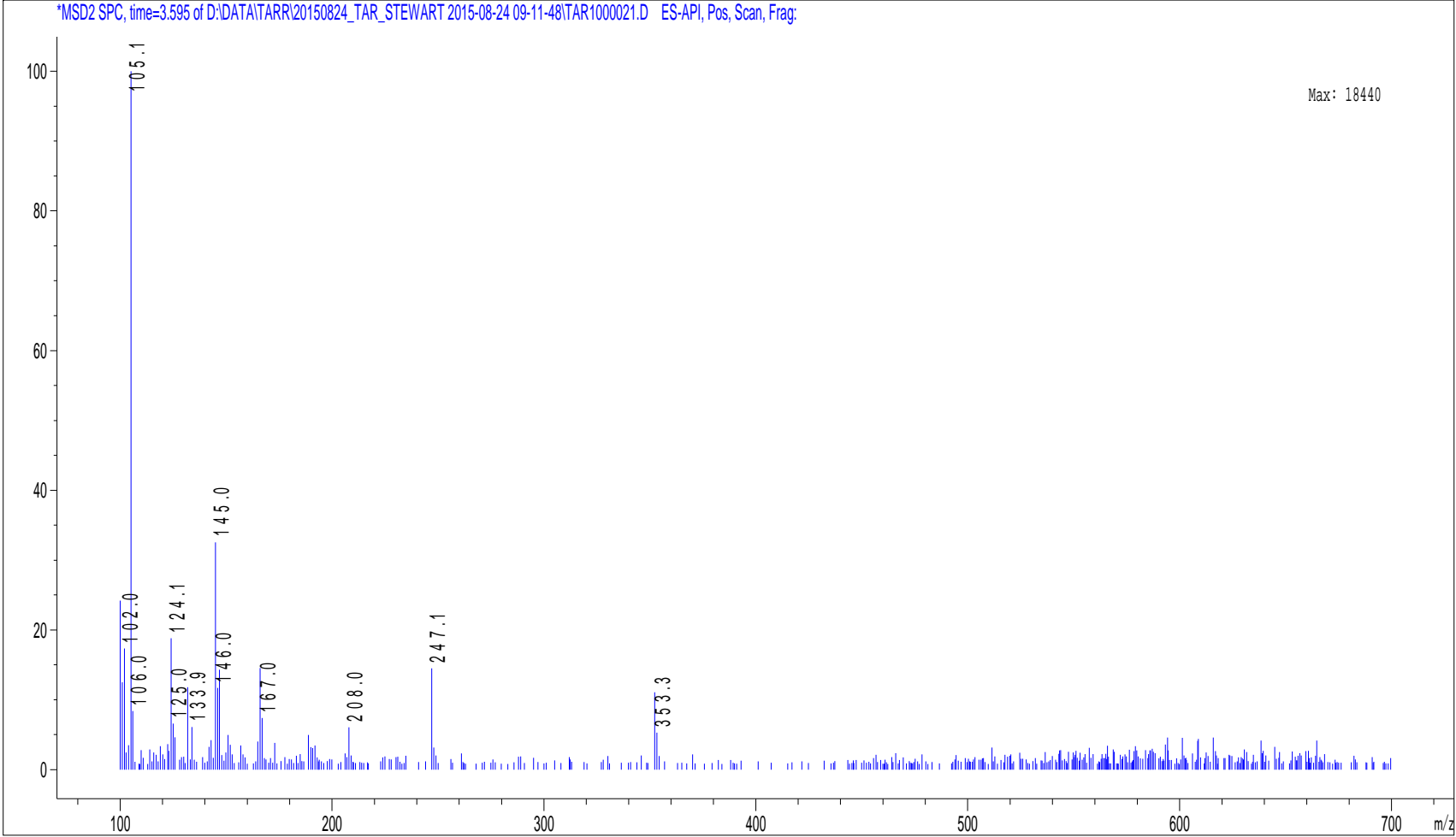
P2-C-03



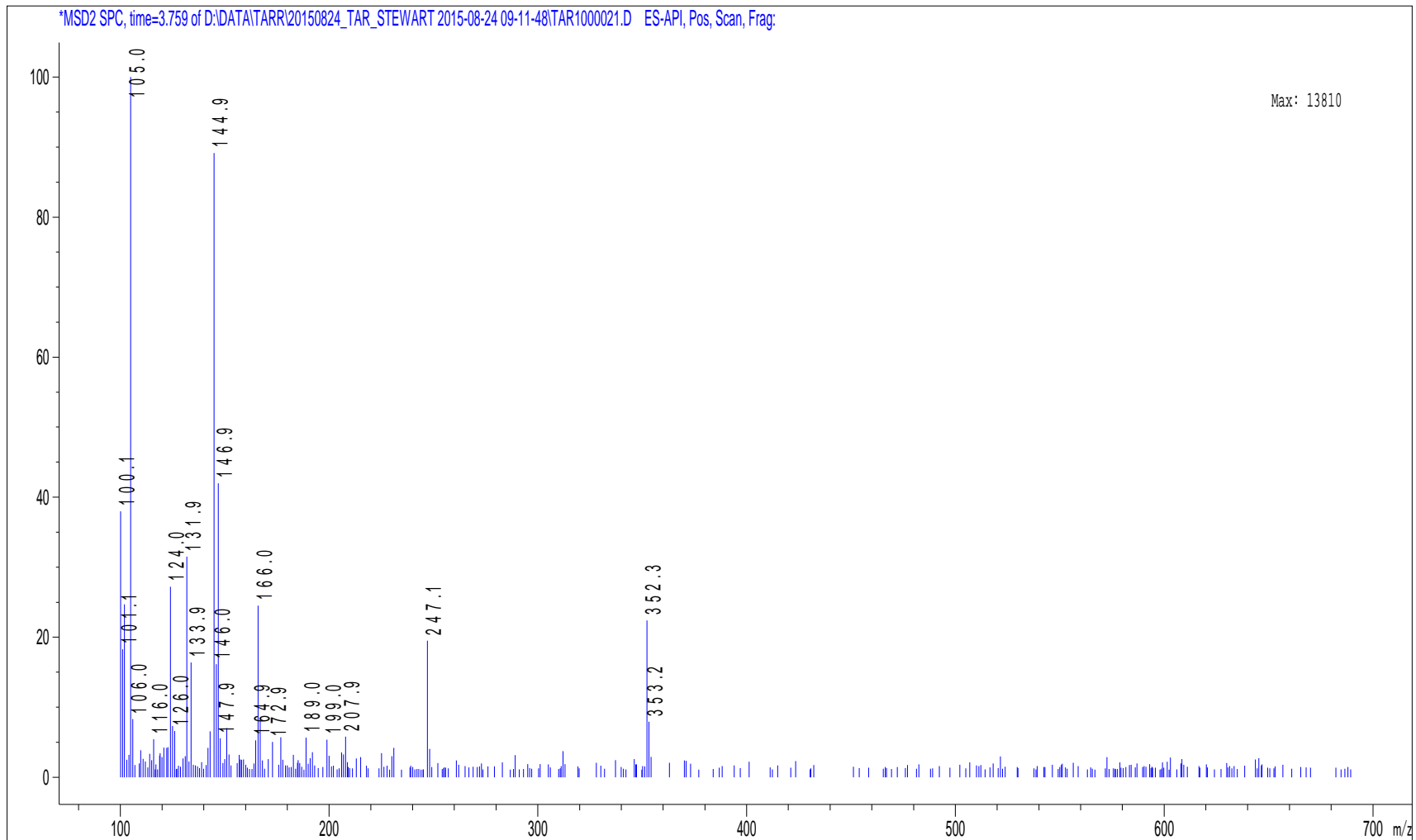


\*MSD2 SPC, time=3.122 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000021.D ES-API, Pos, Scan, Frag:

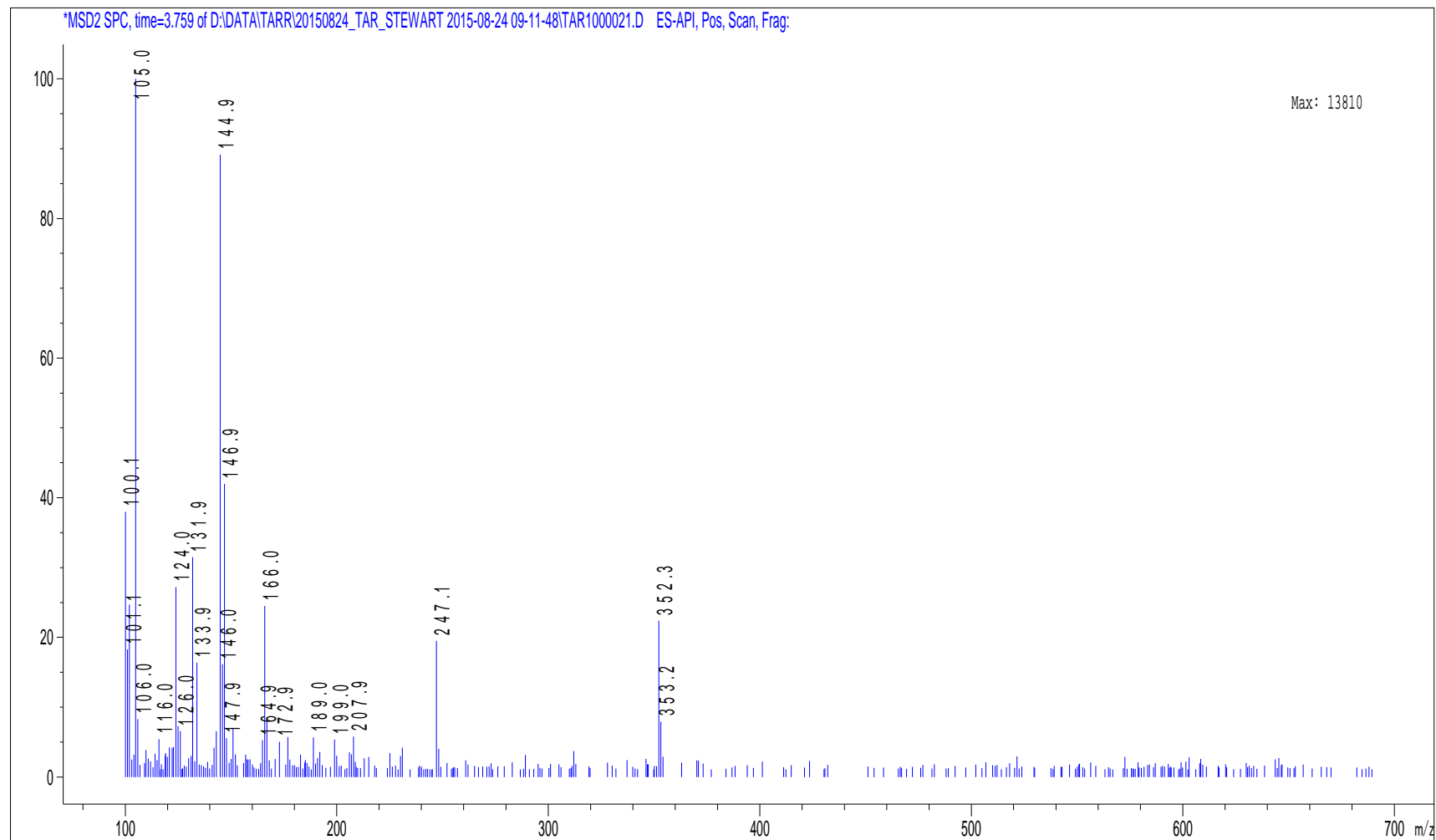




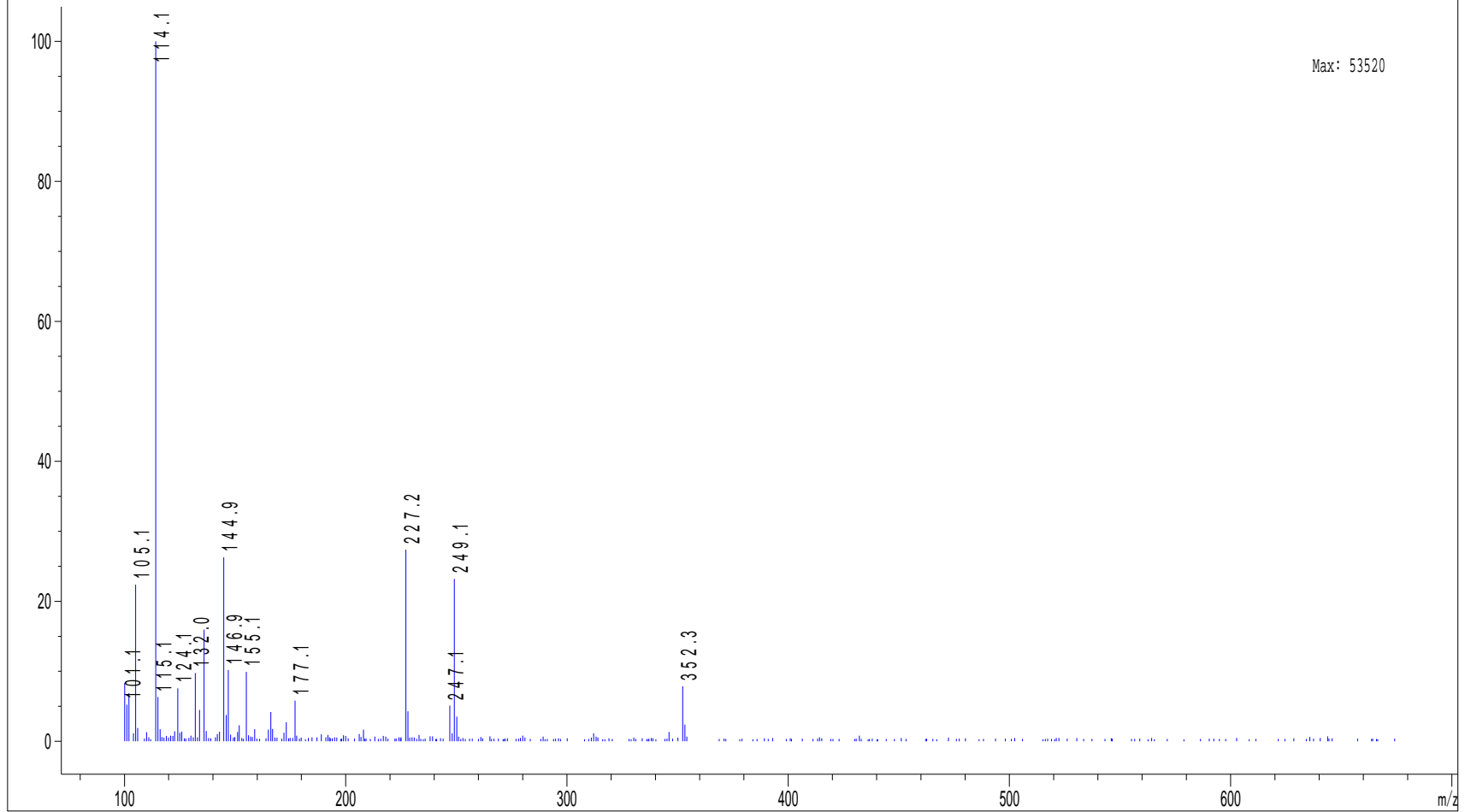
\*MSD2 SPC, time=3.759 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000021.D ES-API, Pos, Scan, Frag:



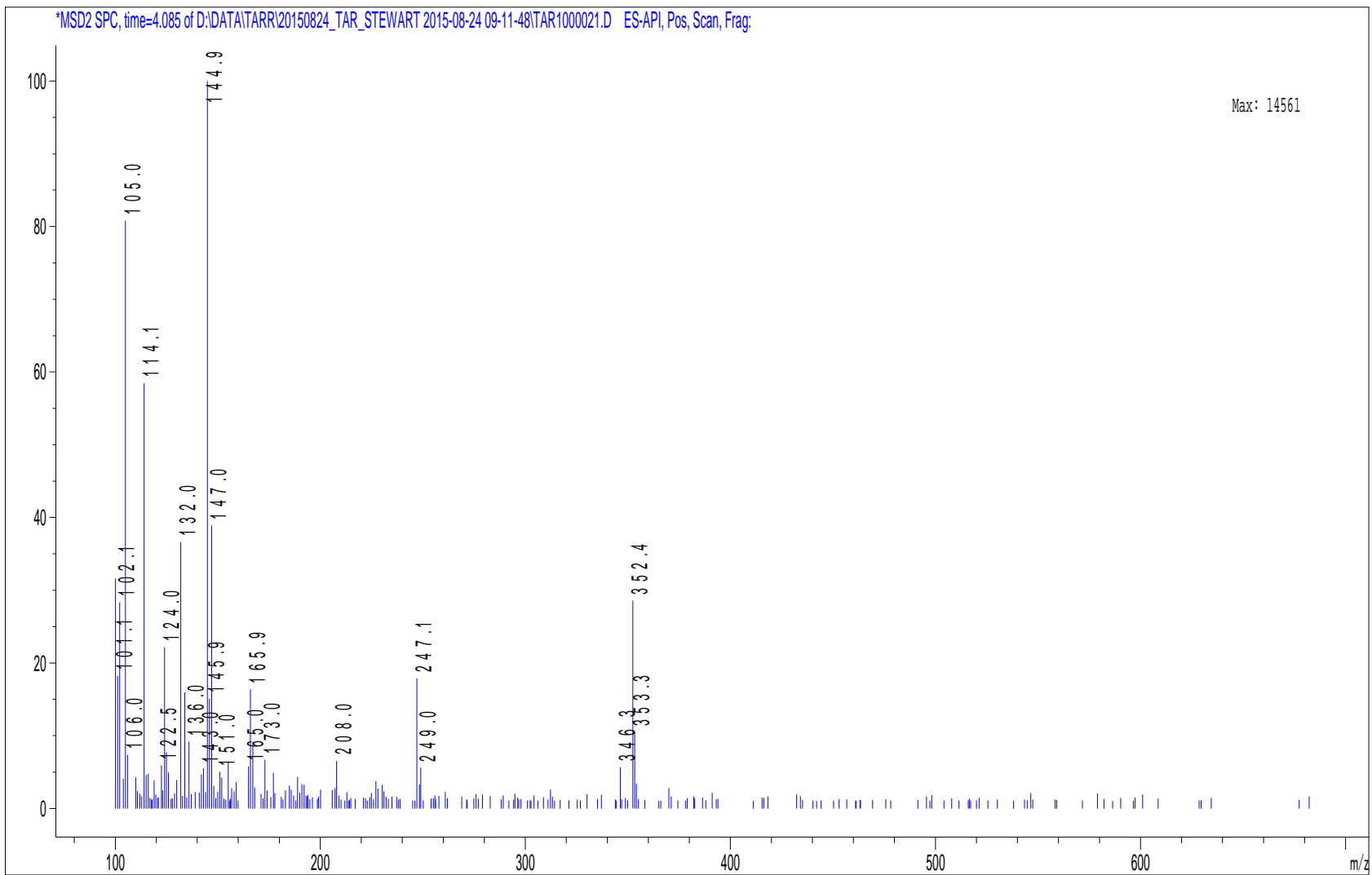
\*MSD2 SPC, time=3.759 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000021.D ES-API, Pos, Scan, Frag:



\*MSD2 SPC, time=3.922 of D:\DATA\TARR\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000021.D ES-API, Pos, Scan, Frag:



\*MSD2 SPC, time=4.085 of D:\DATA\ARRI\20150824\_TAR\_STEWART 2015-08-24 09-11-48\TAR1000021.D ES-API, Pos, Scan, Frag:

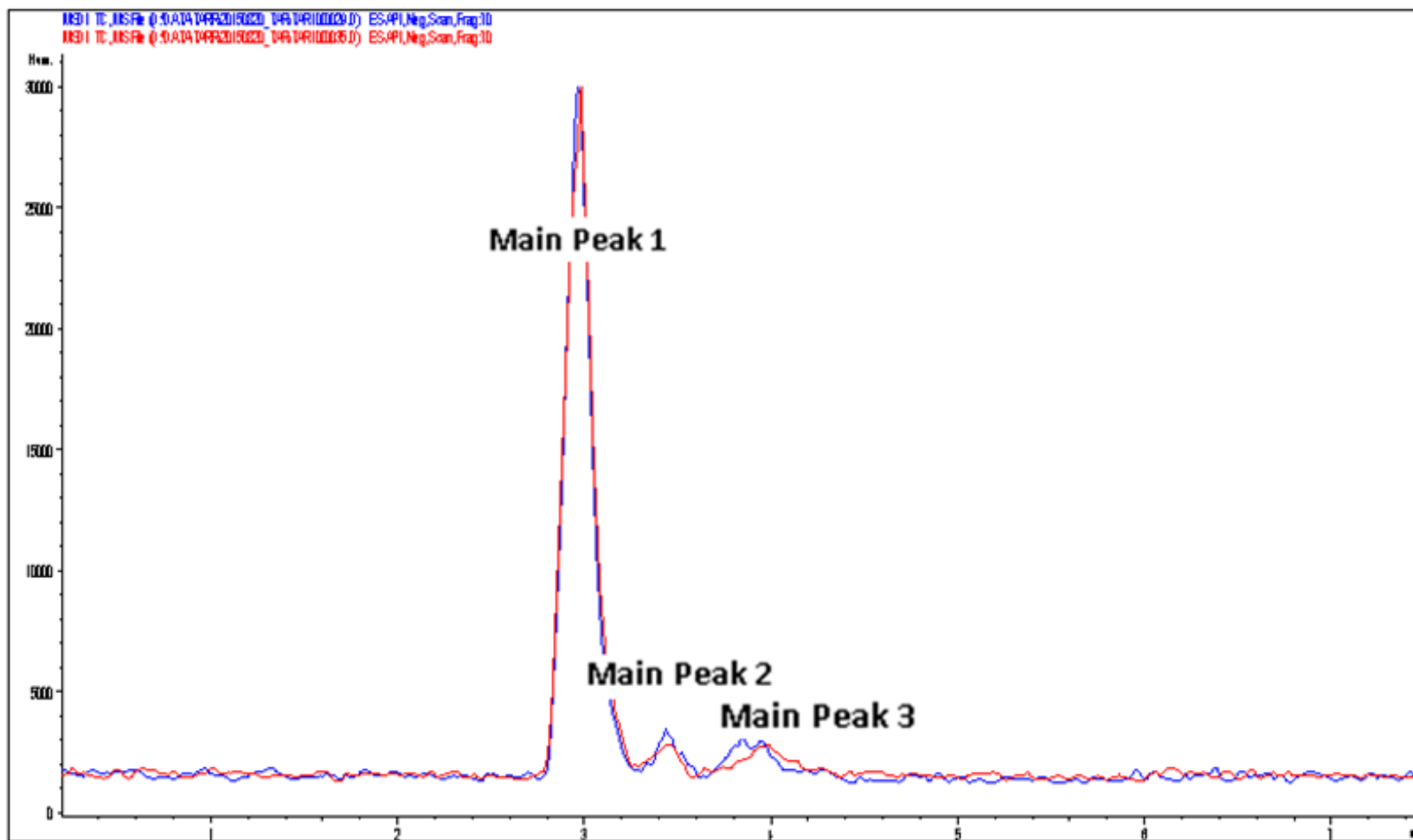


Max: 14561



## Appendix K: Negative Ionization HPLC Chromatograms and Mass Spectroscopy

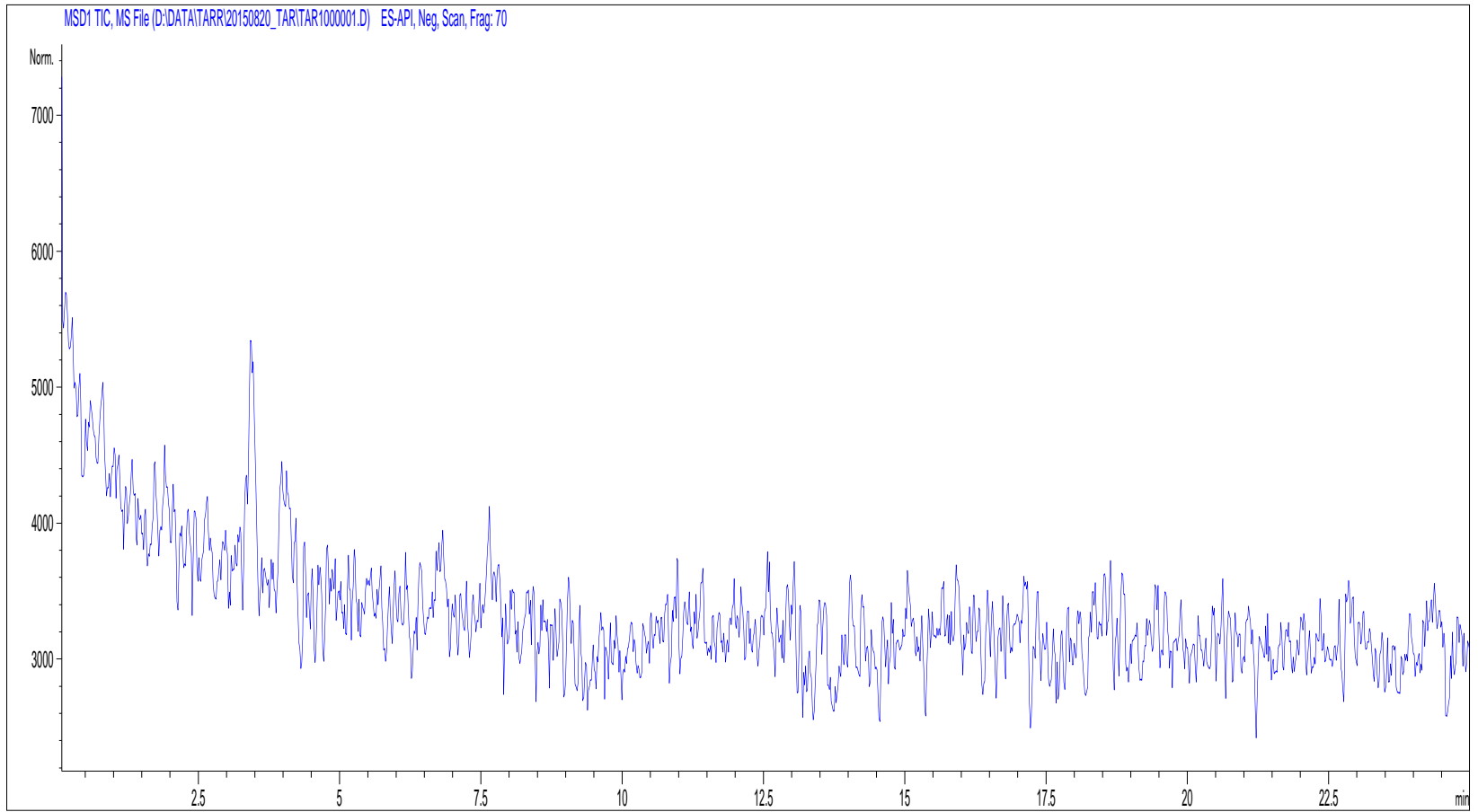
### Example Negative Chromatogram



# Baselines, Standards, Misc.

20-Aug-15  
Baseline - DI Water

P2-A-01

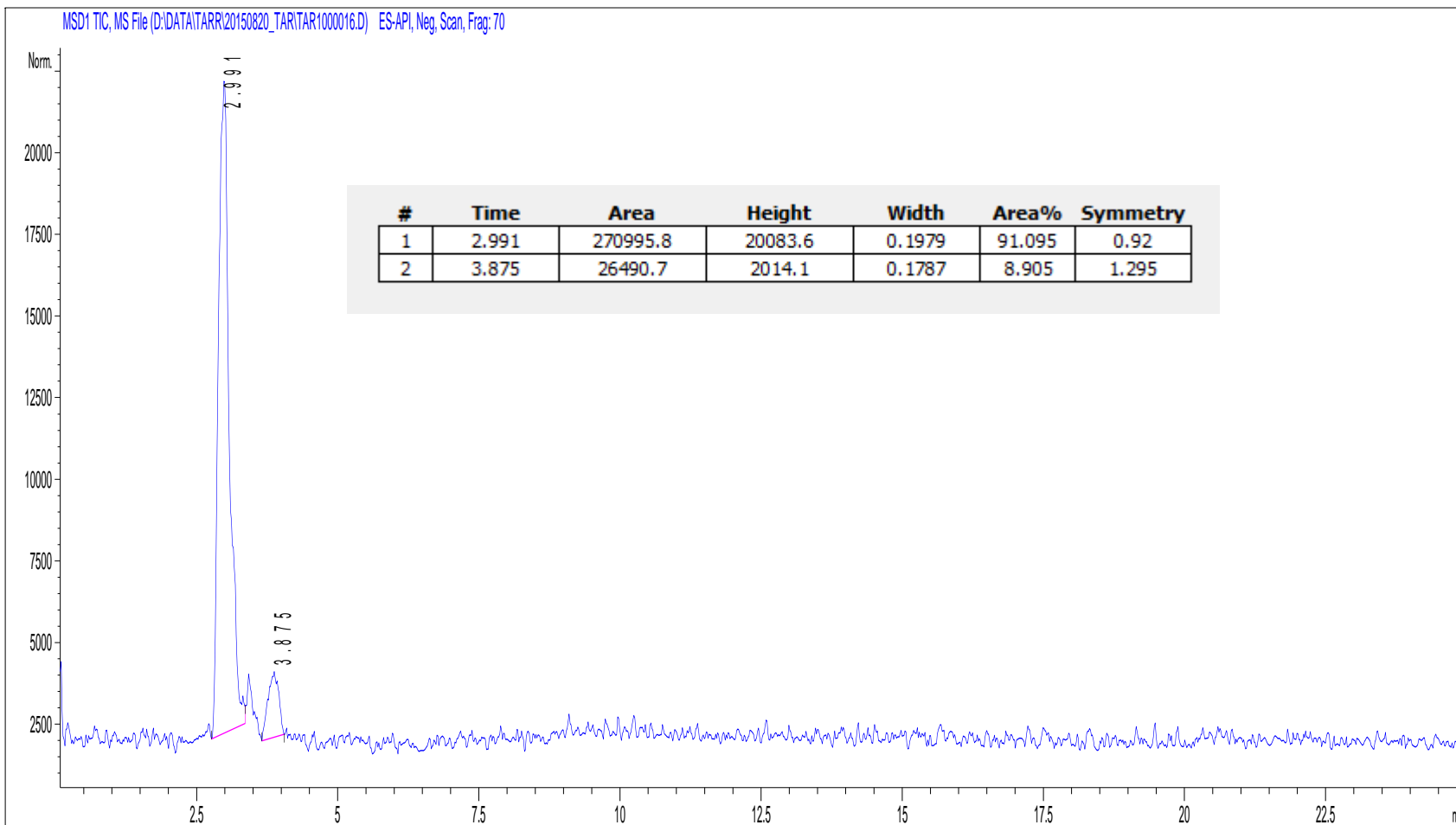


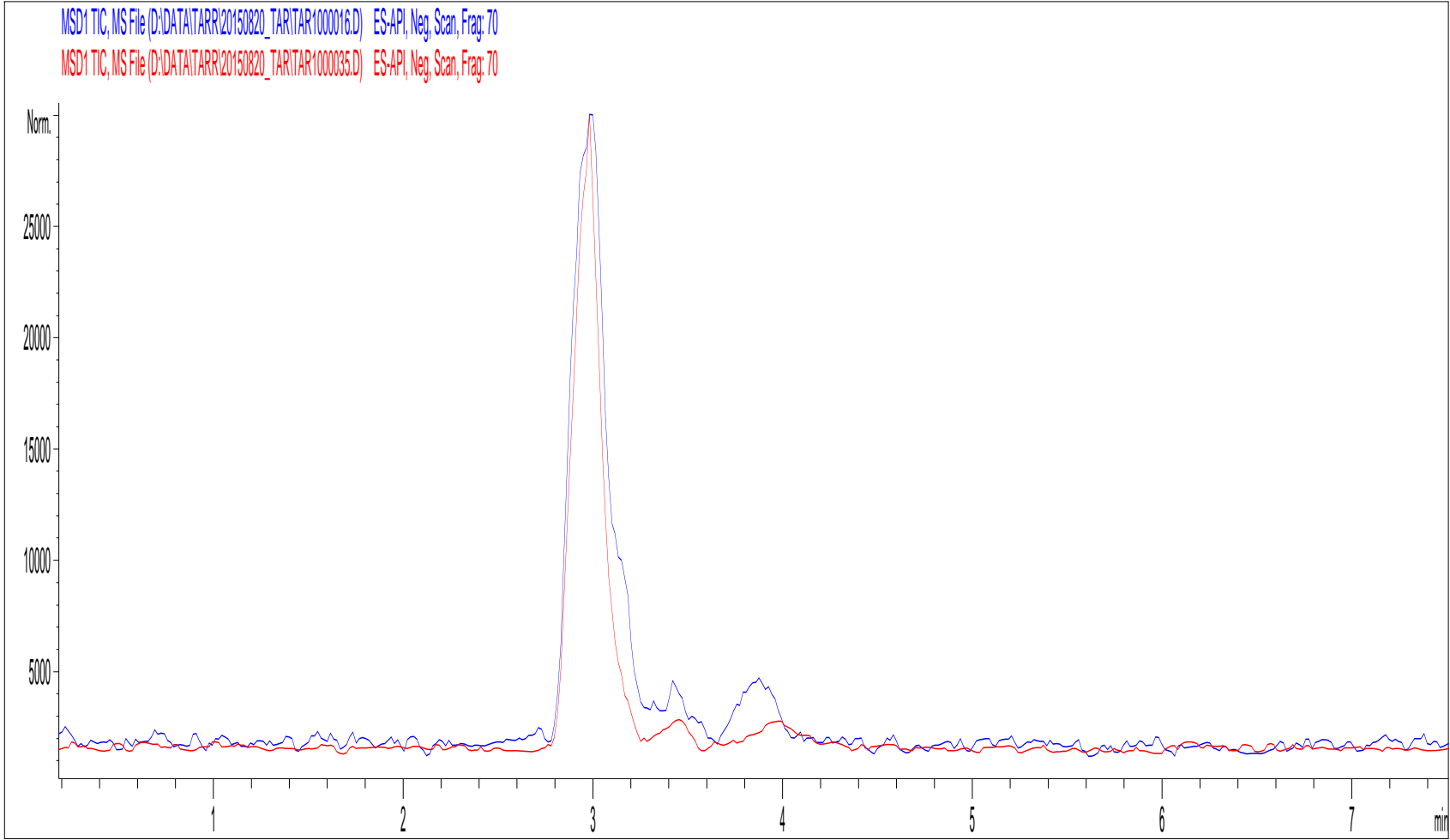
29-May-15

70

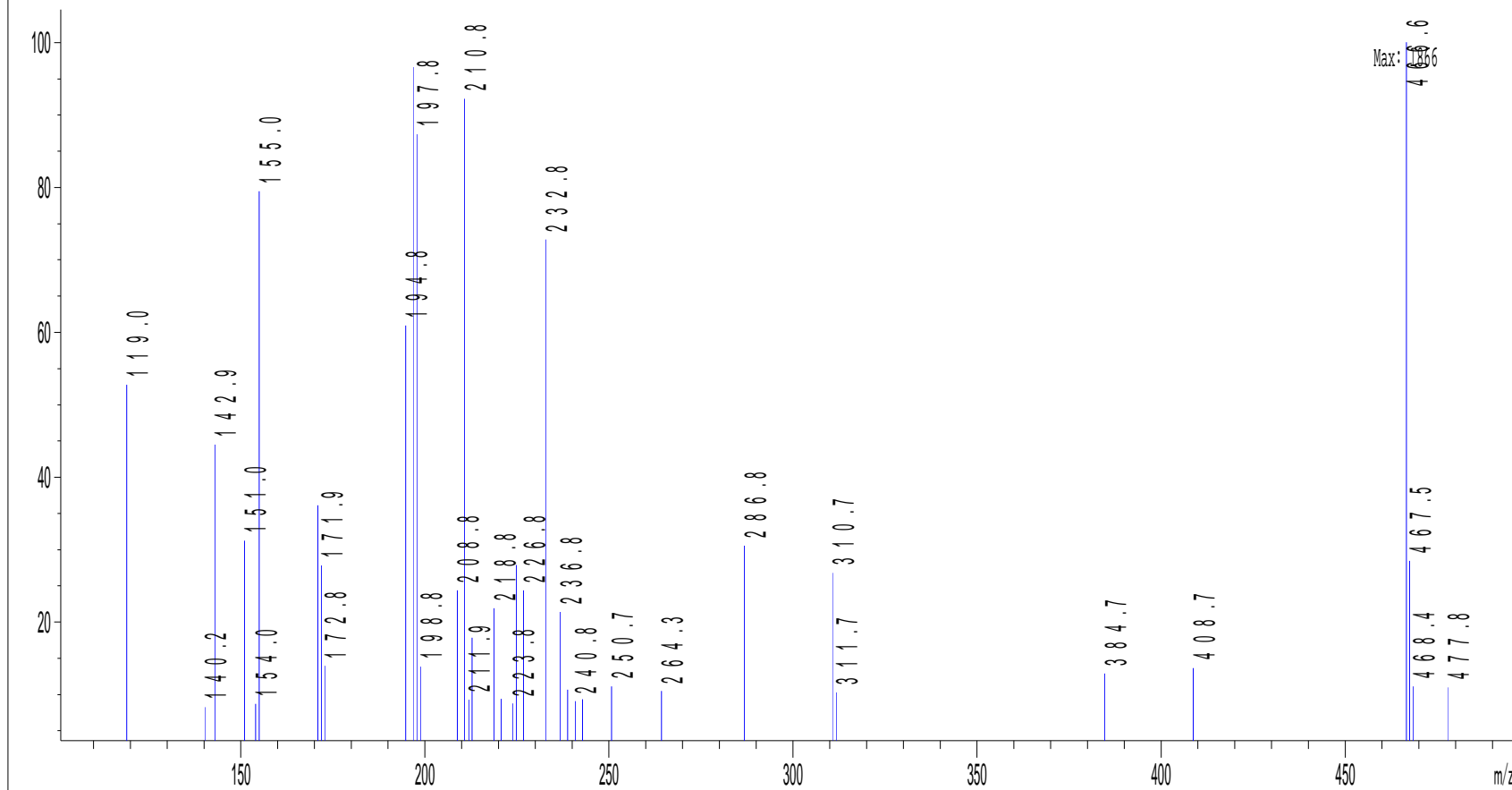
5

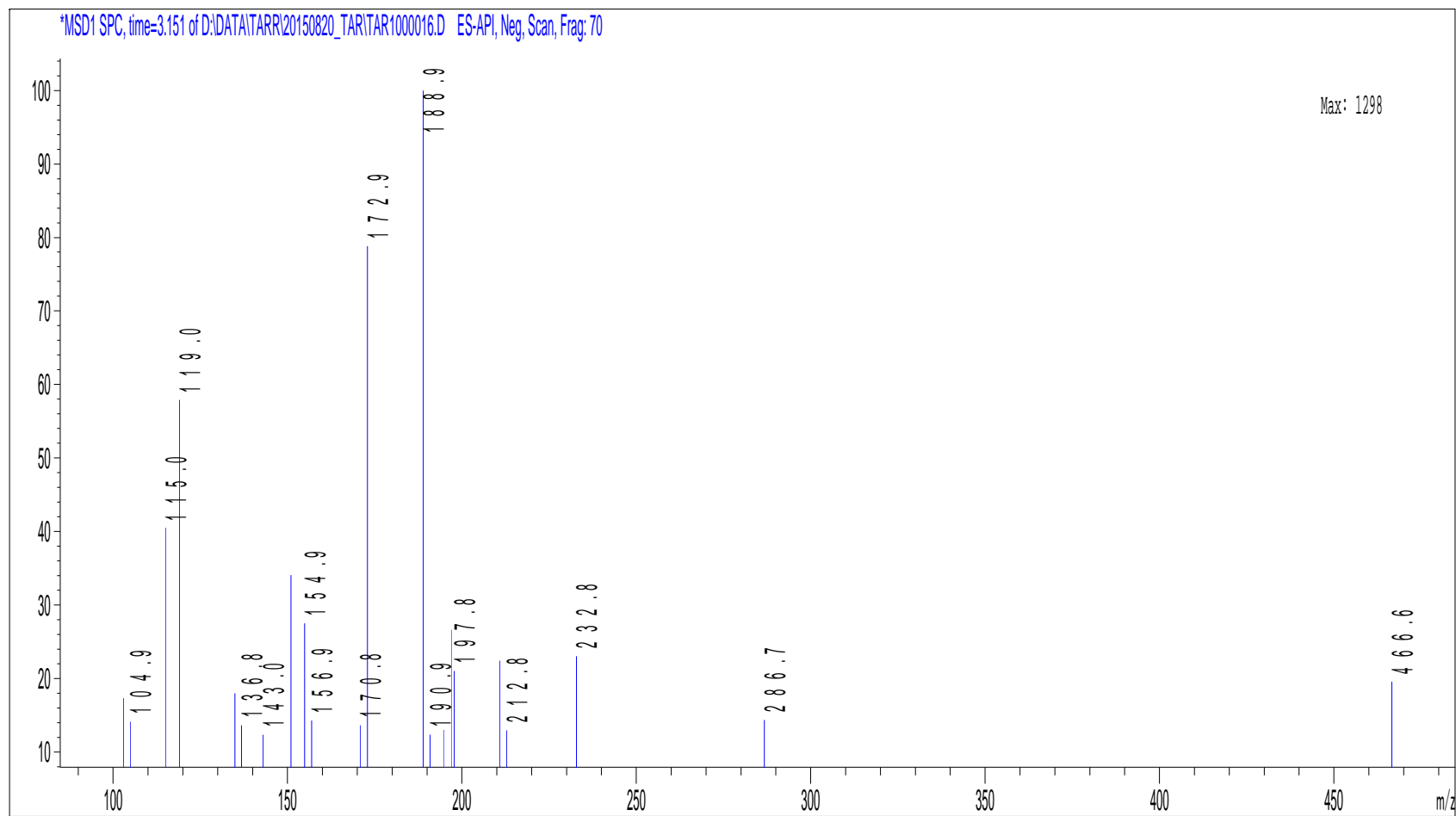
P2-B-03

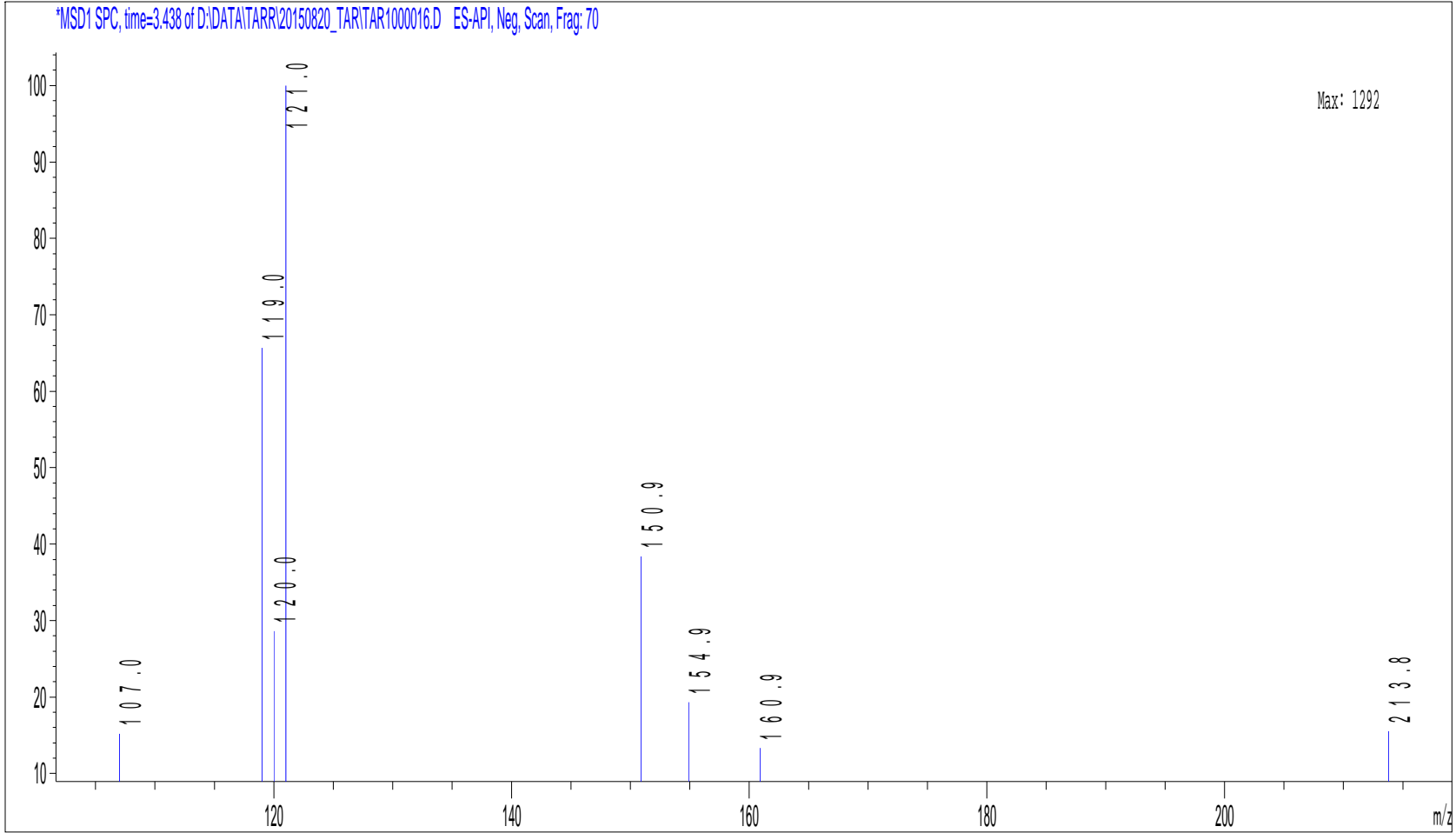




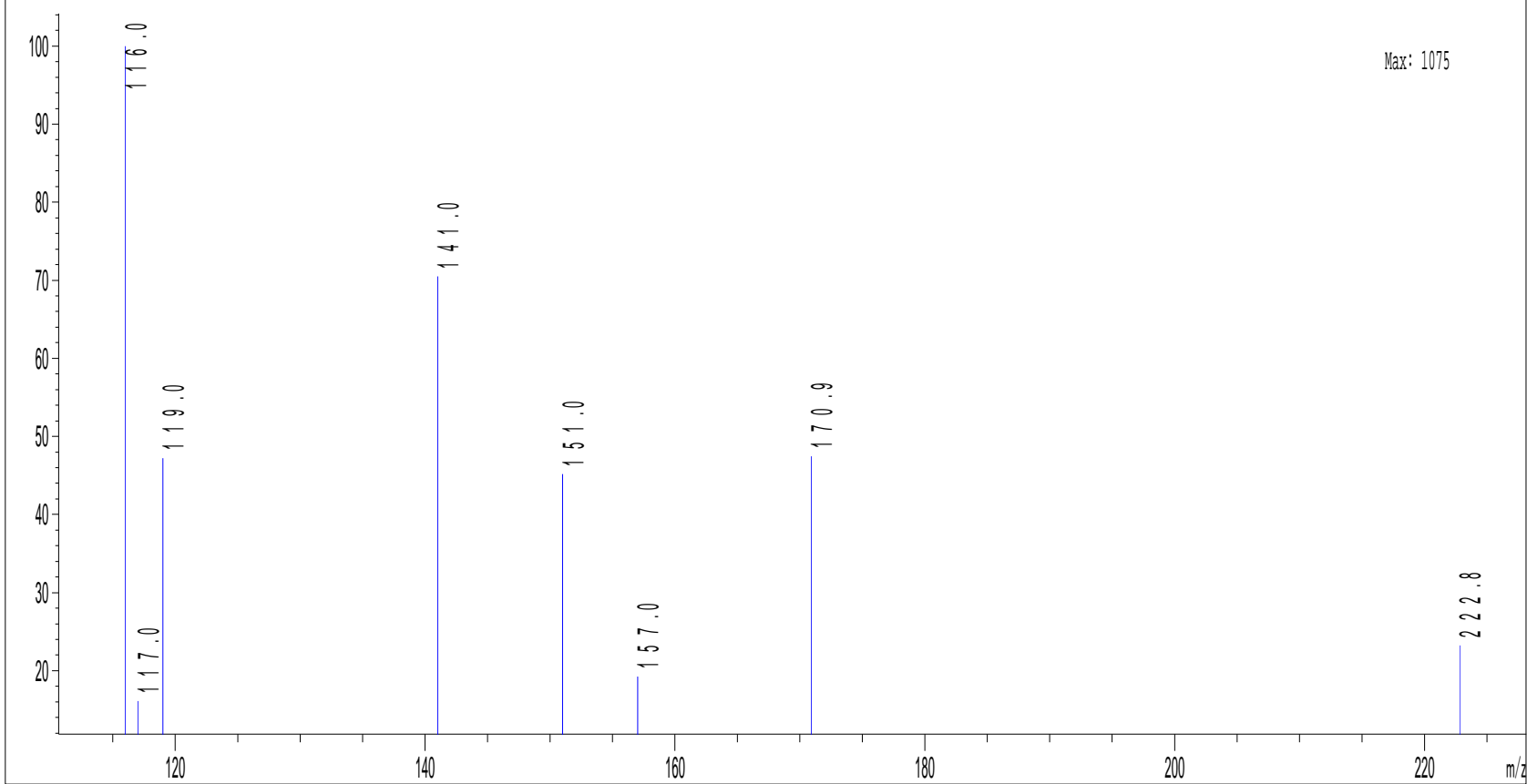
\*MSD1 SPC, time=2.999 of D:\DATA\TARR\20150820\_TARITAR1000016.D ES-API, Neg, Scan, Frag: 70





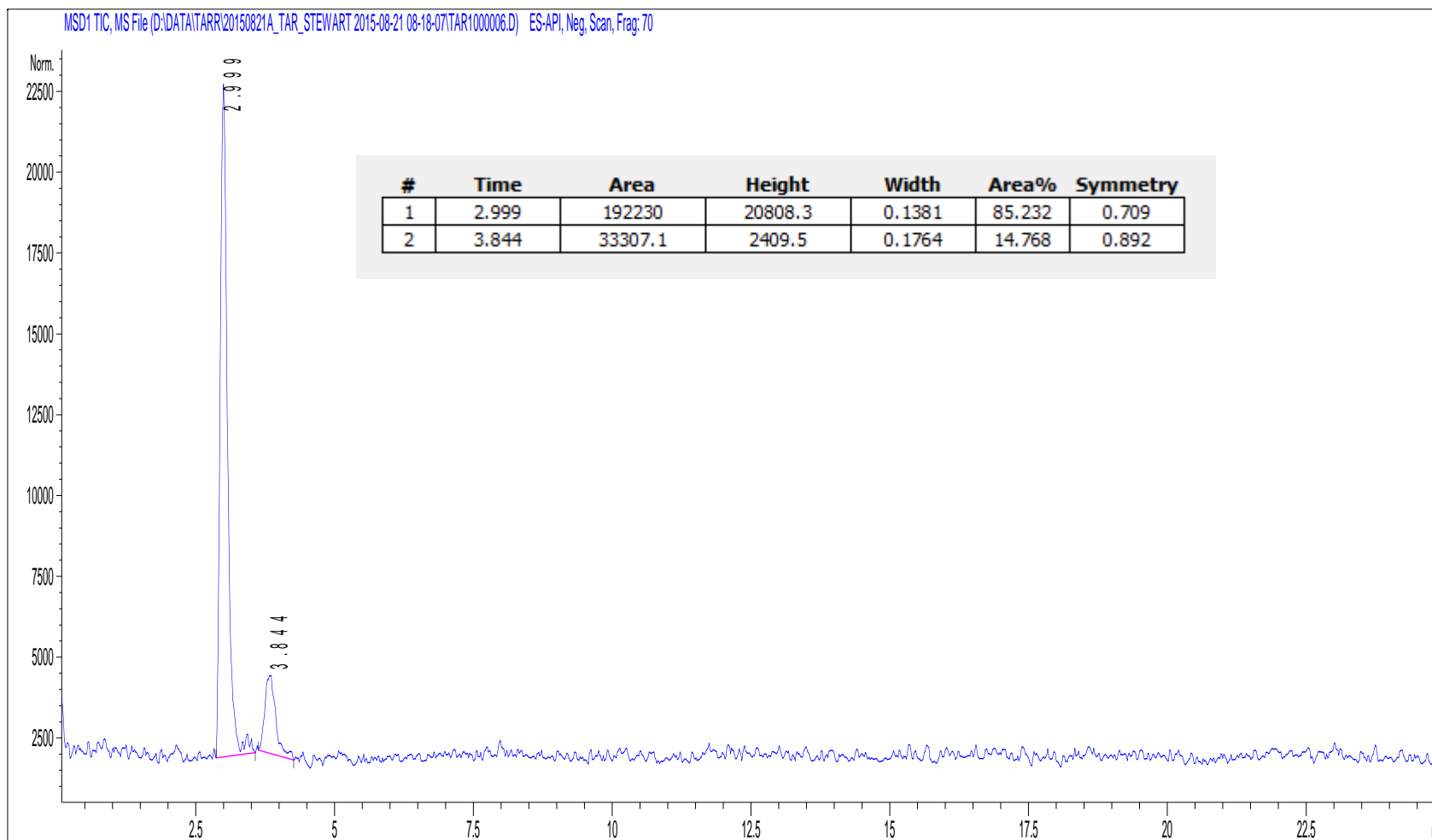


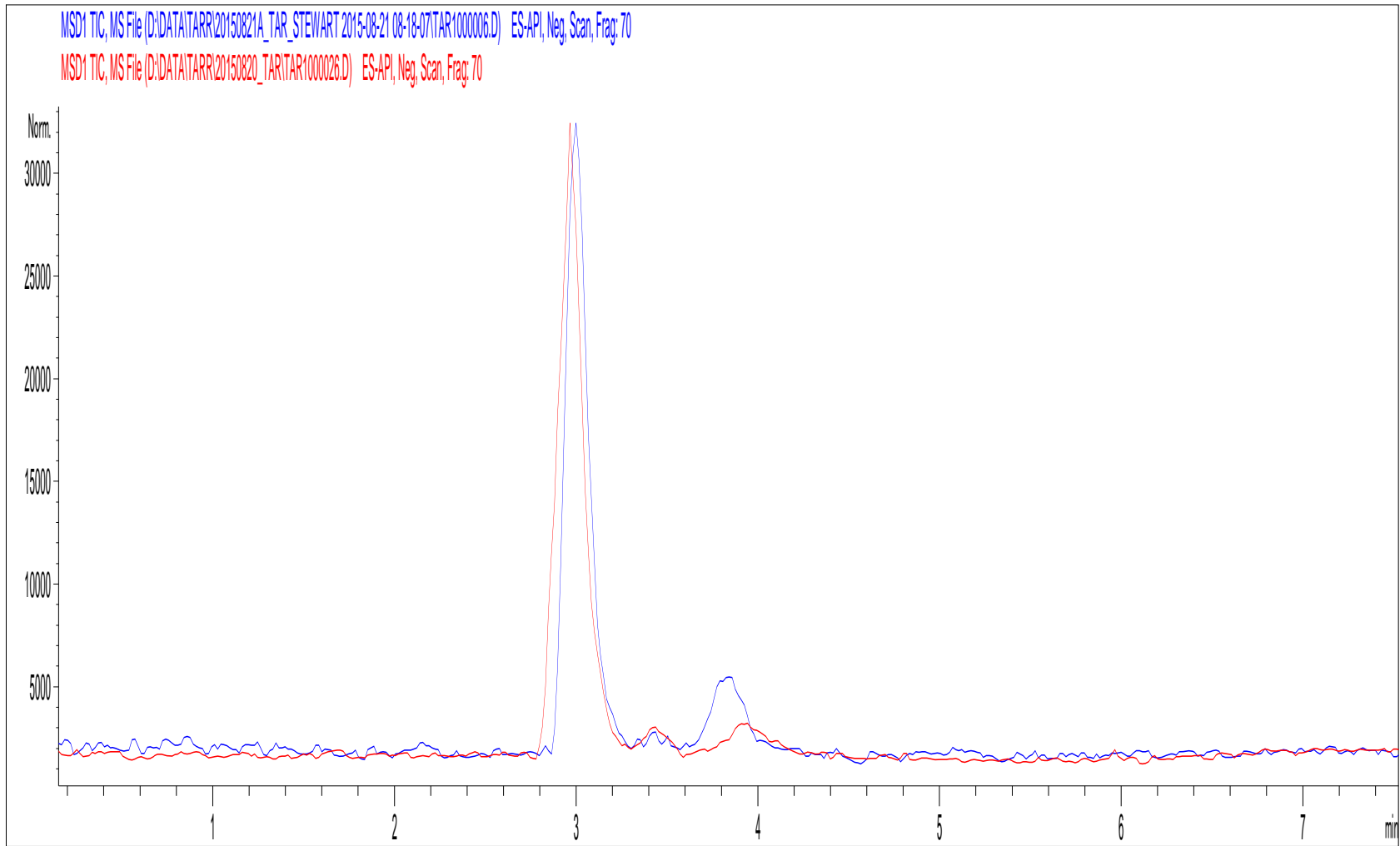
\*MSD1 SPC, time=3.859 of D:\DATA\TARR\20150820\_TAR\TAR1000016.D ES-API, Neg, Scan, Frag: 70

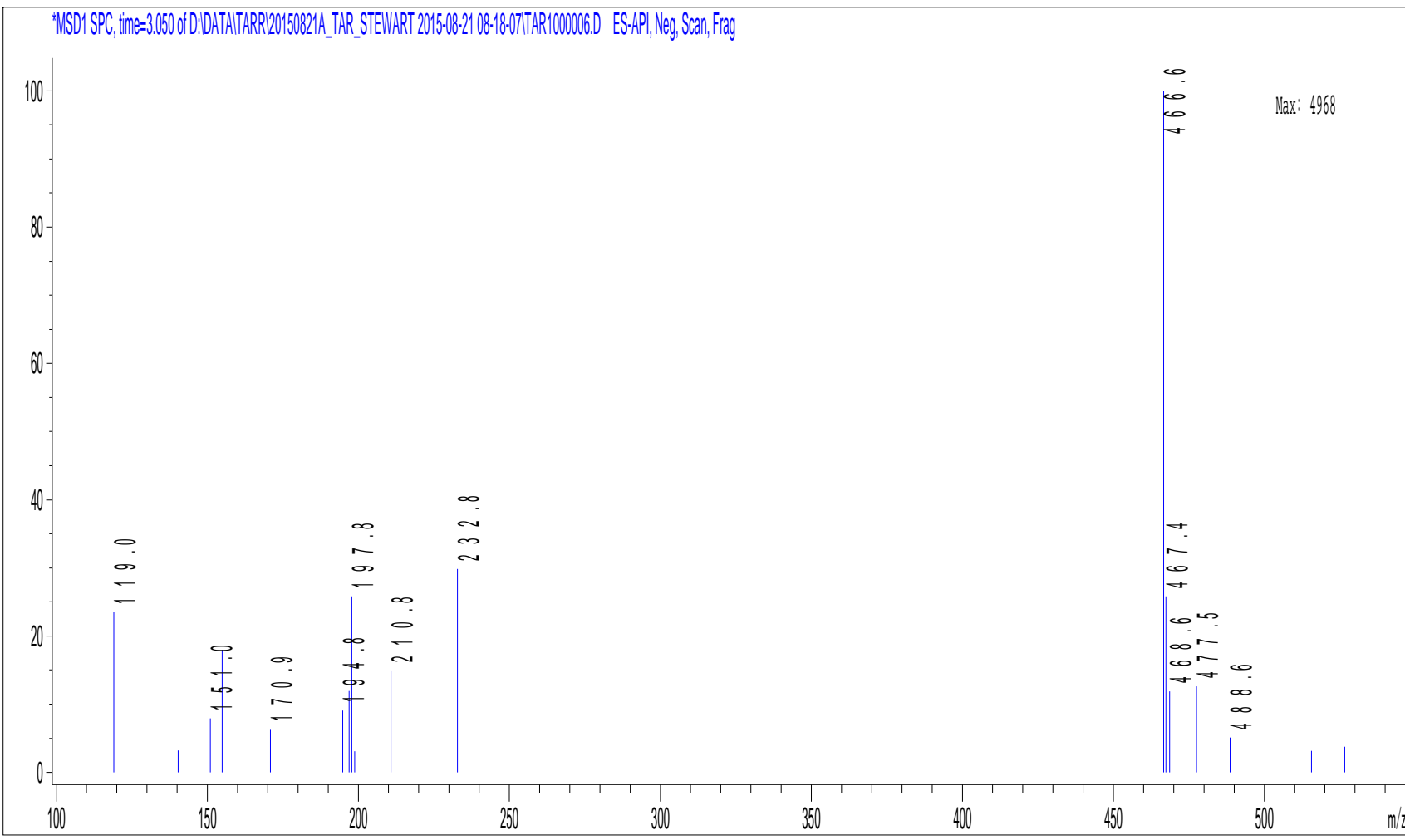


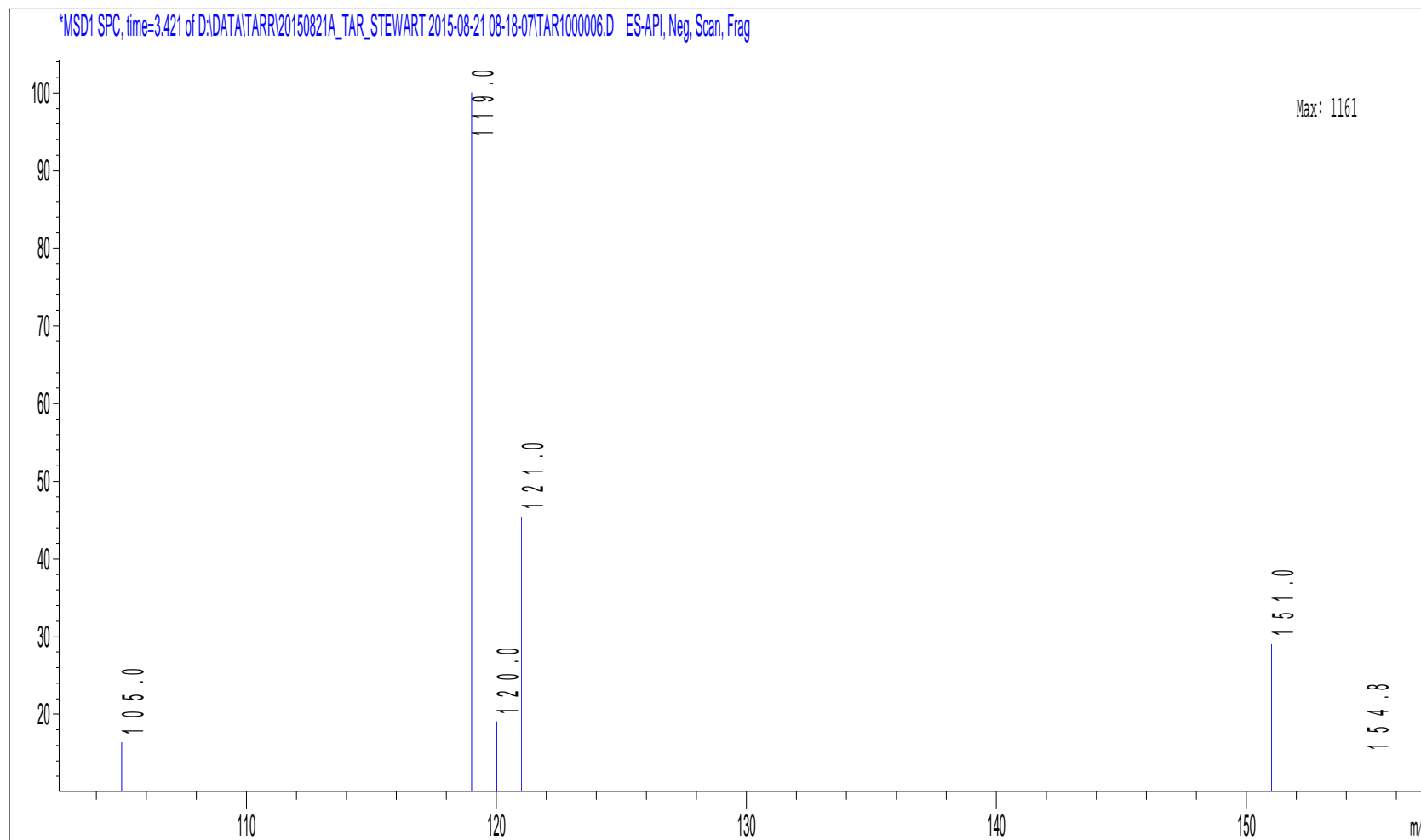


11-Aug-15  
UNTREATED SOLUTION  
7  
P2-E-05

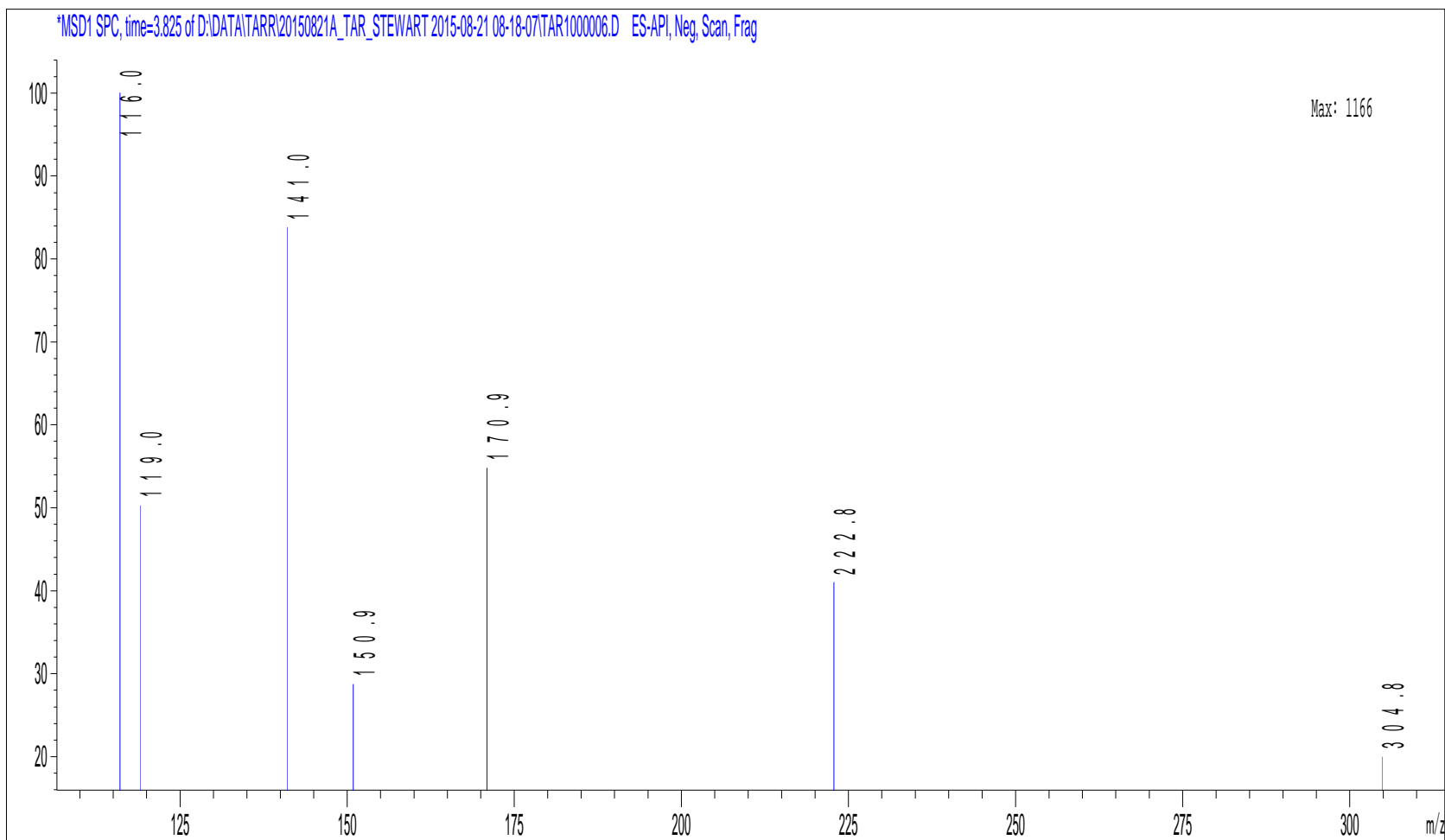








\*MSD1 SPC, time=3.825 of D:\DATA\TARR\20150821A\_TAR\_STEWART 2015-08-21 08-18-07\TAR1000006.D ES-API, Neg, Scan, Frag



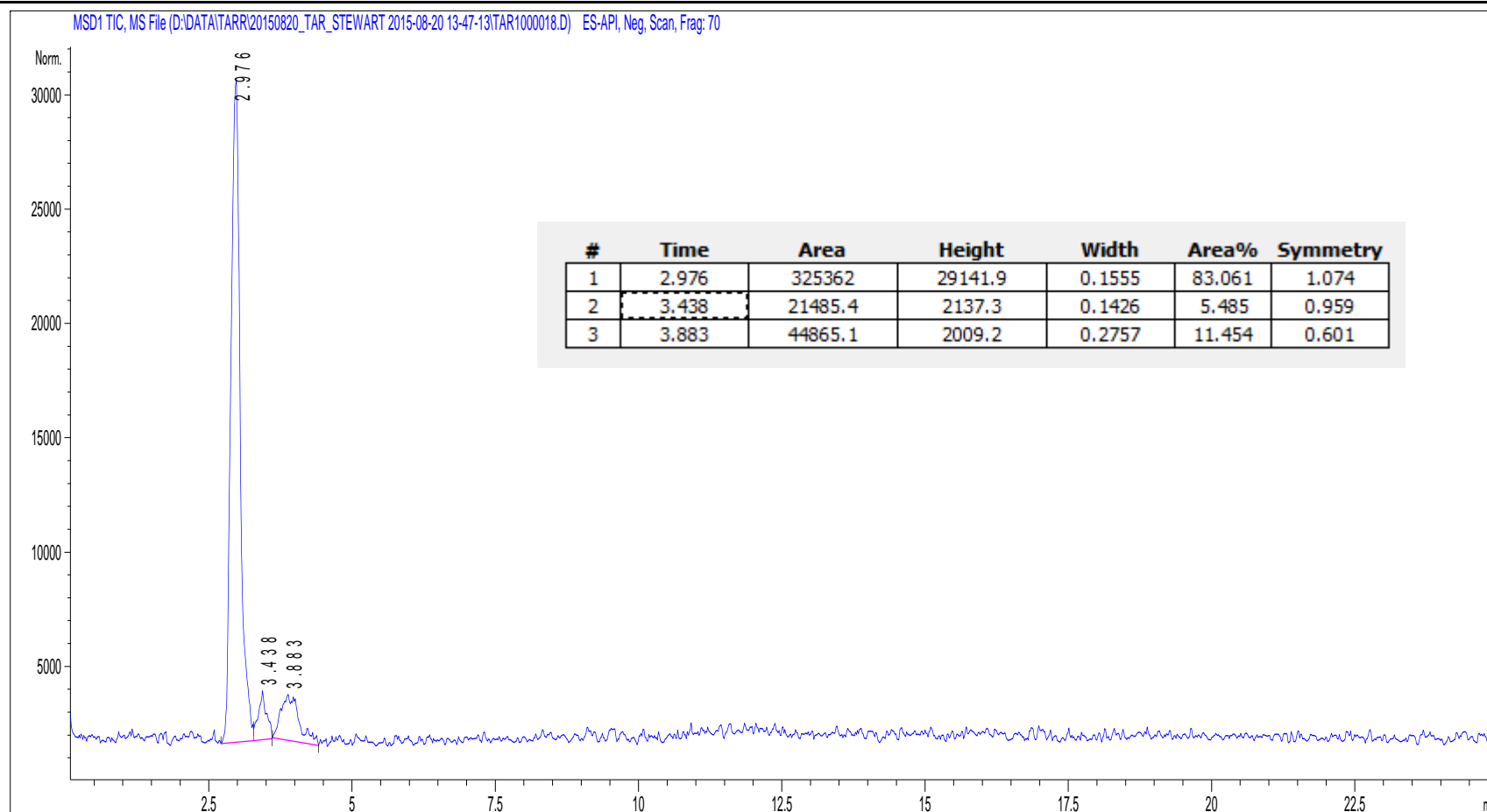
pH 6

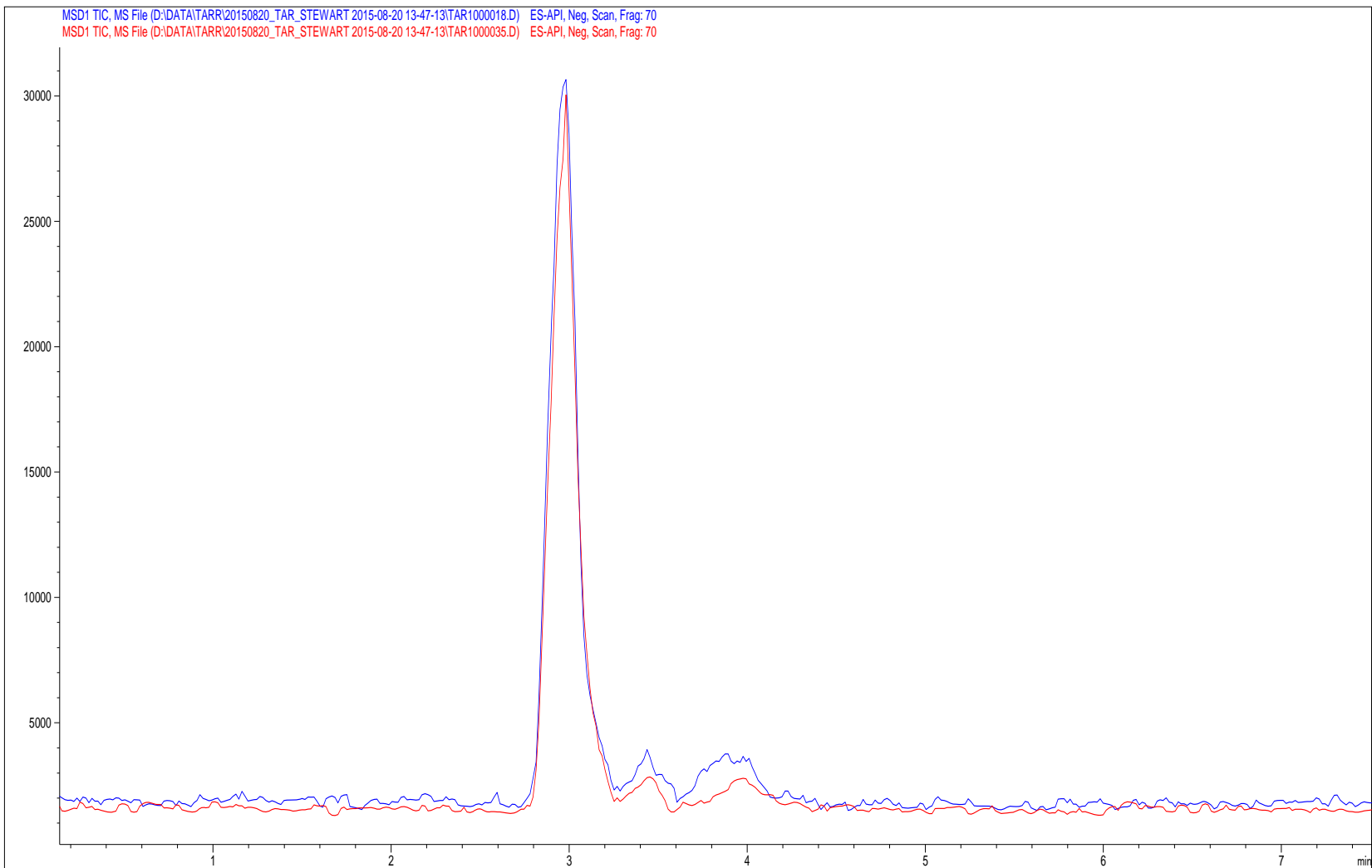
14-May-15

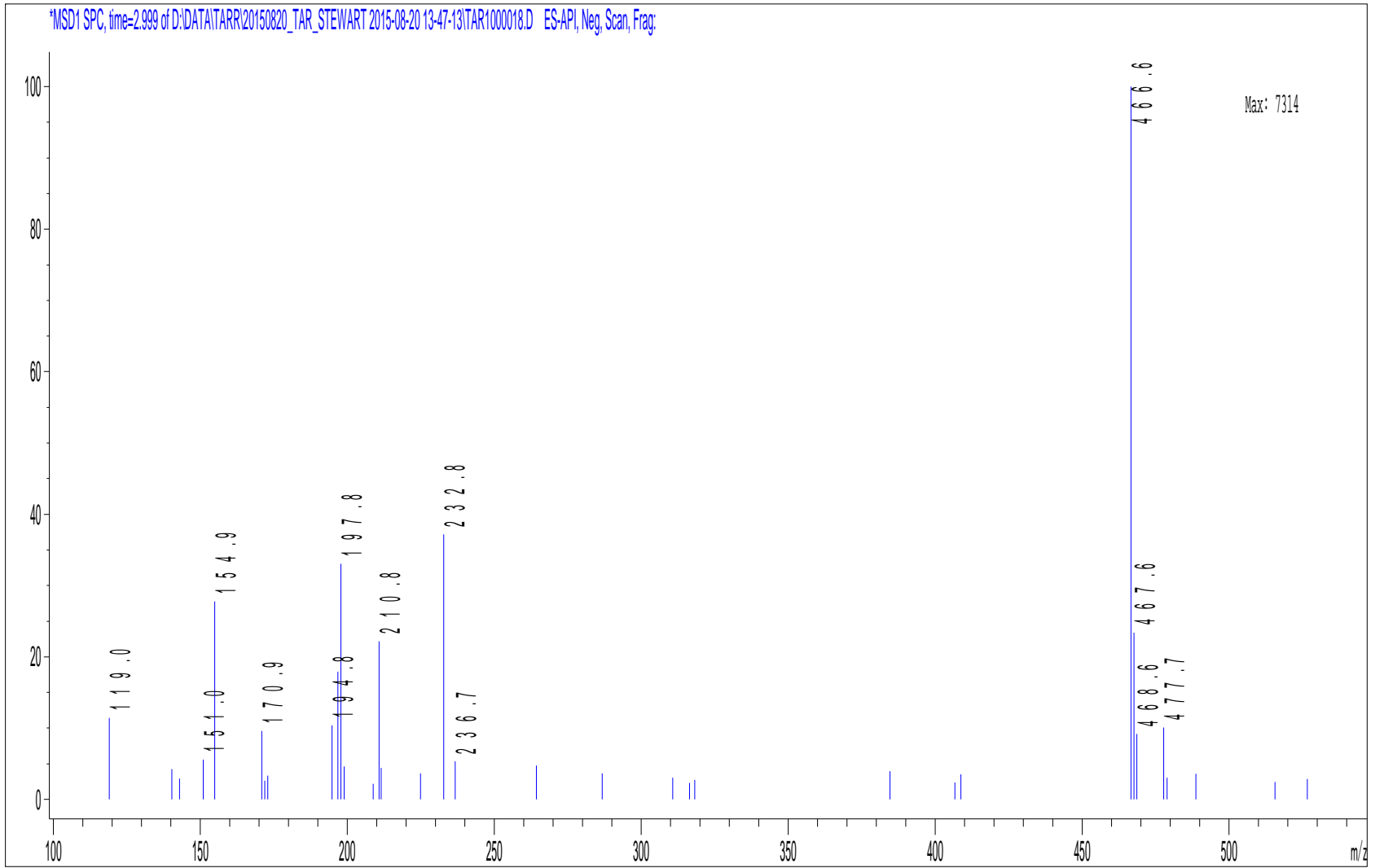
0 DC

6

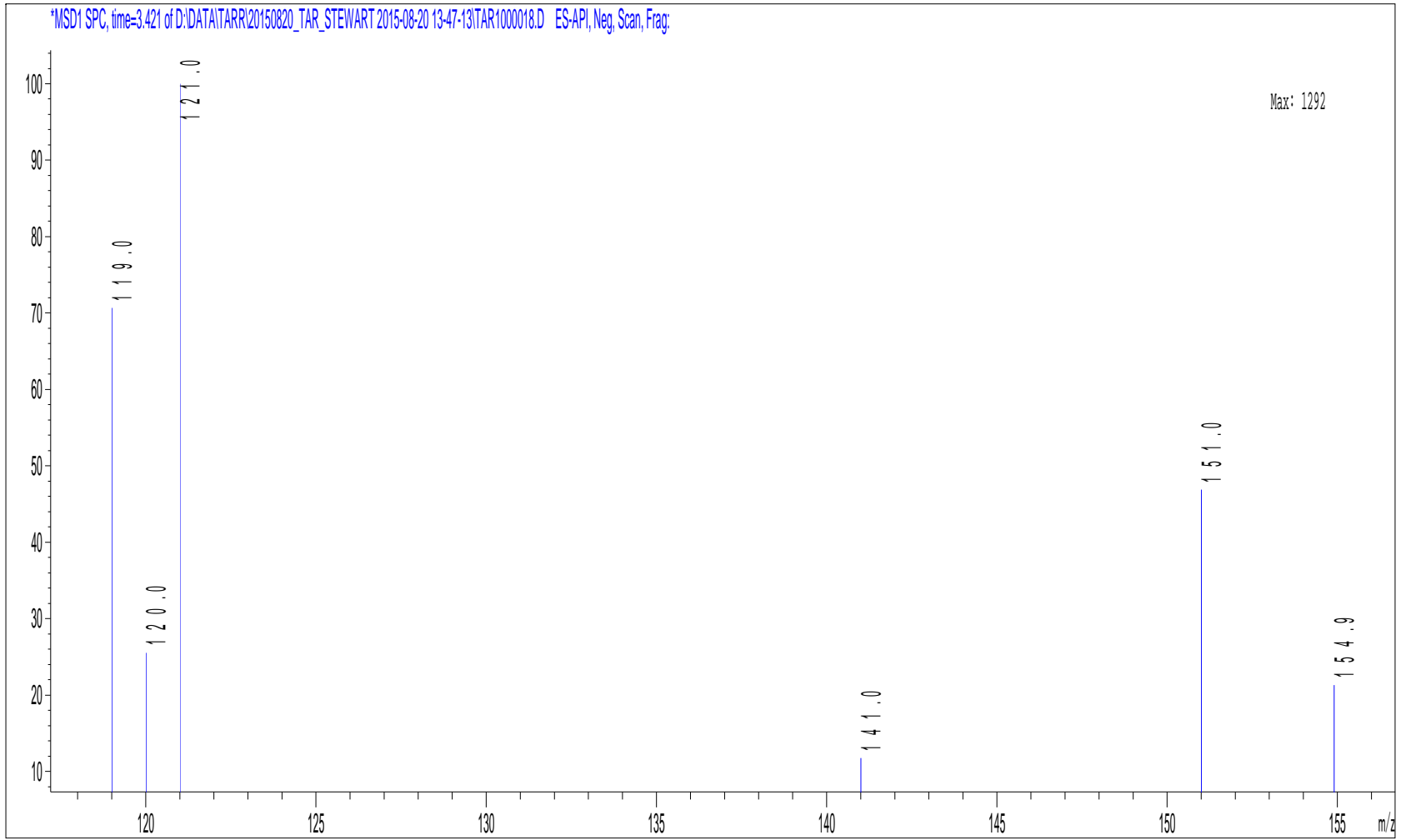
P2-B-01

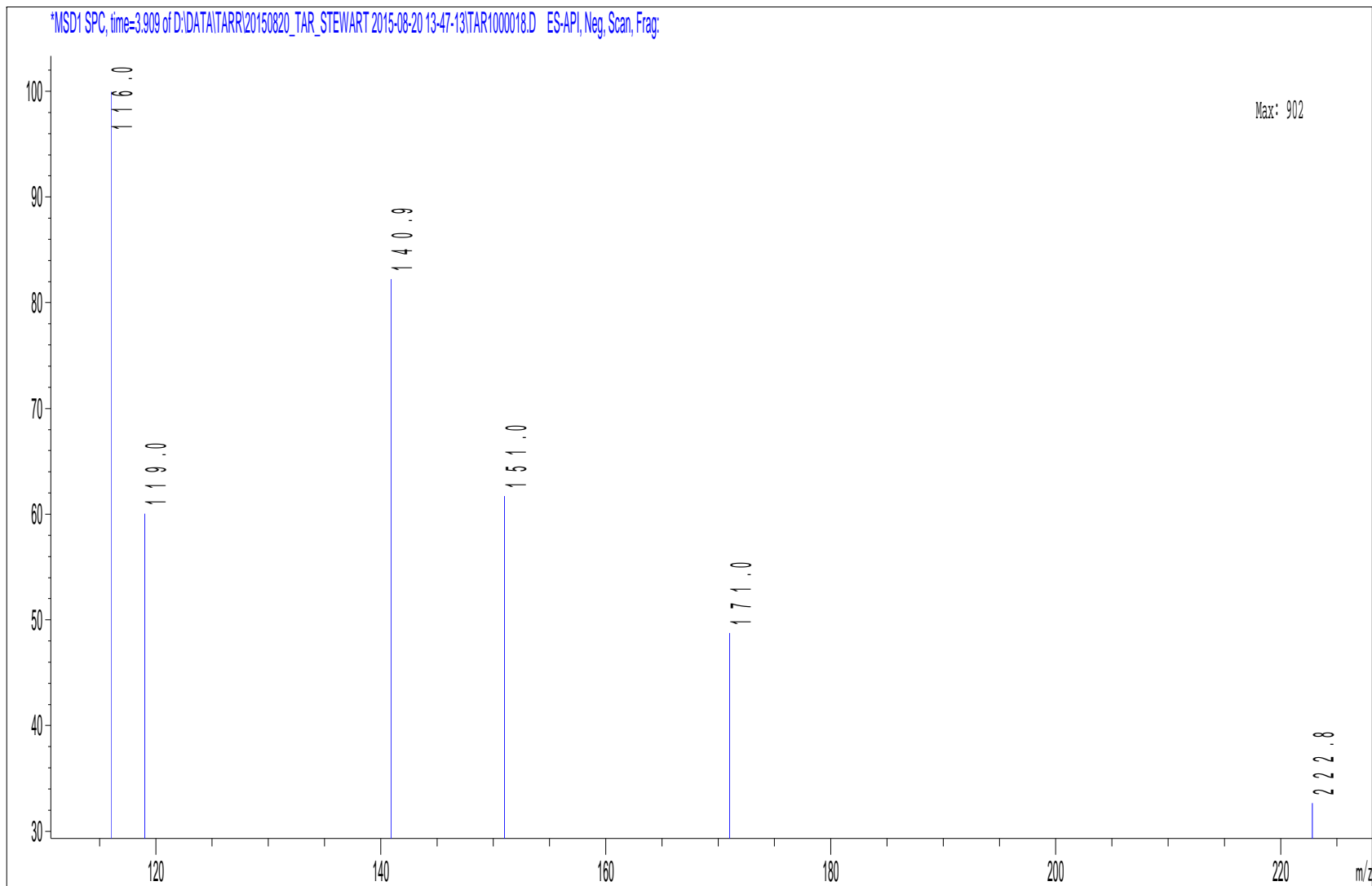










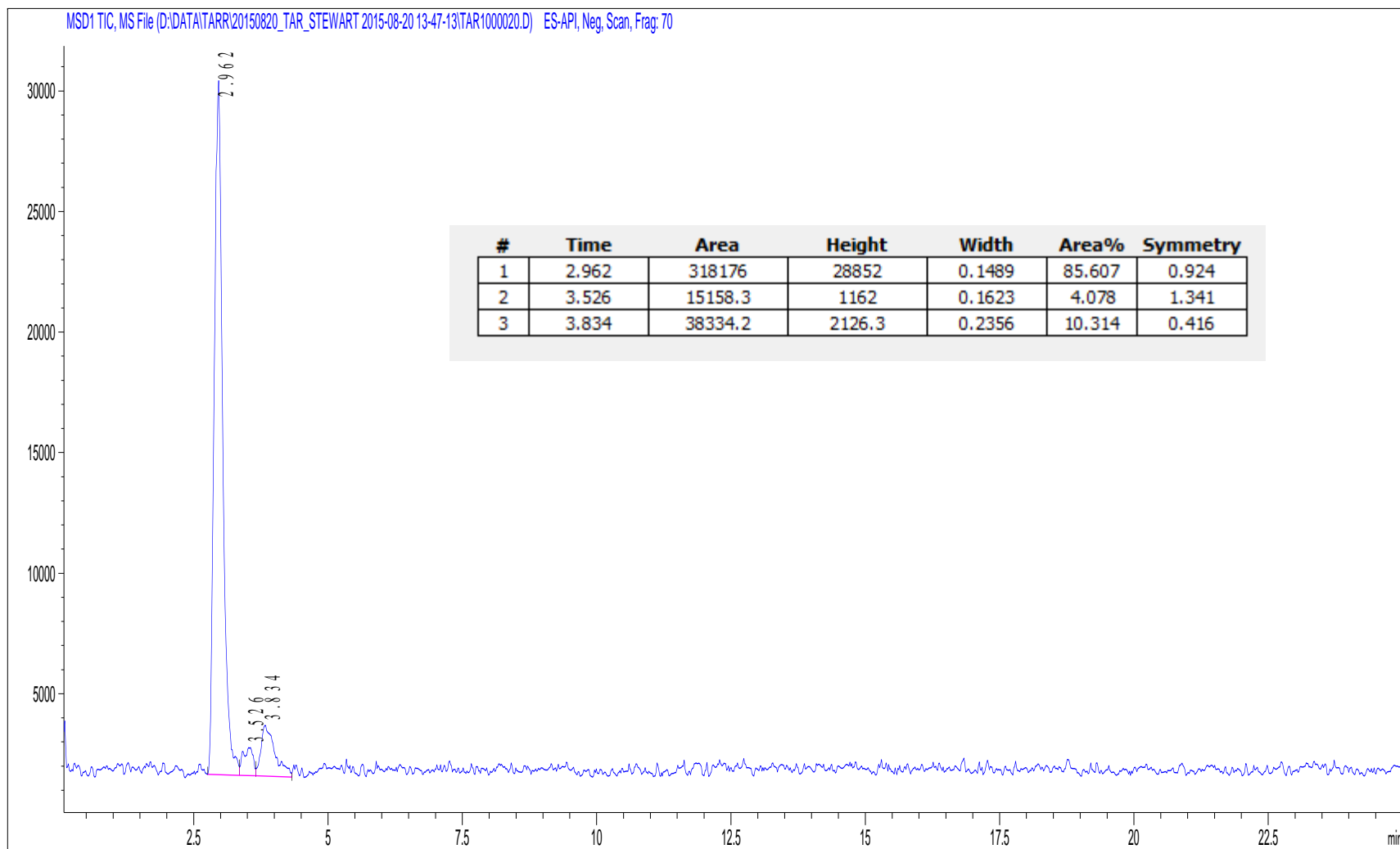


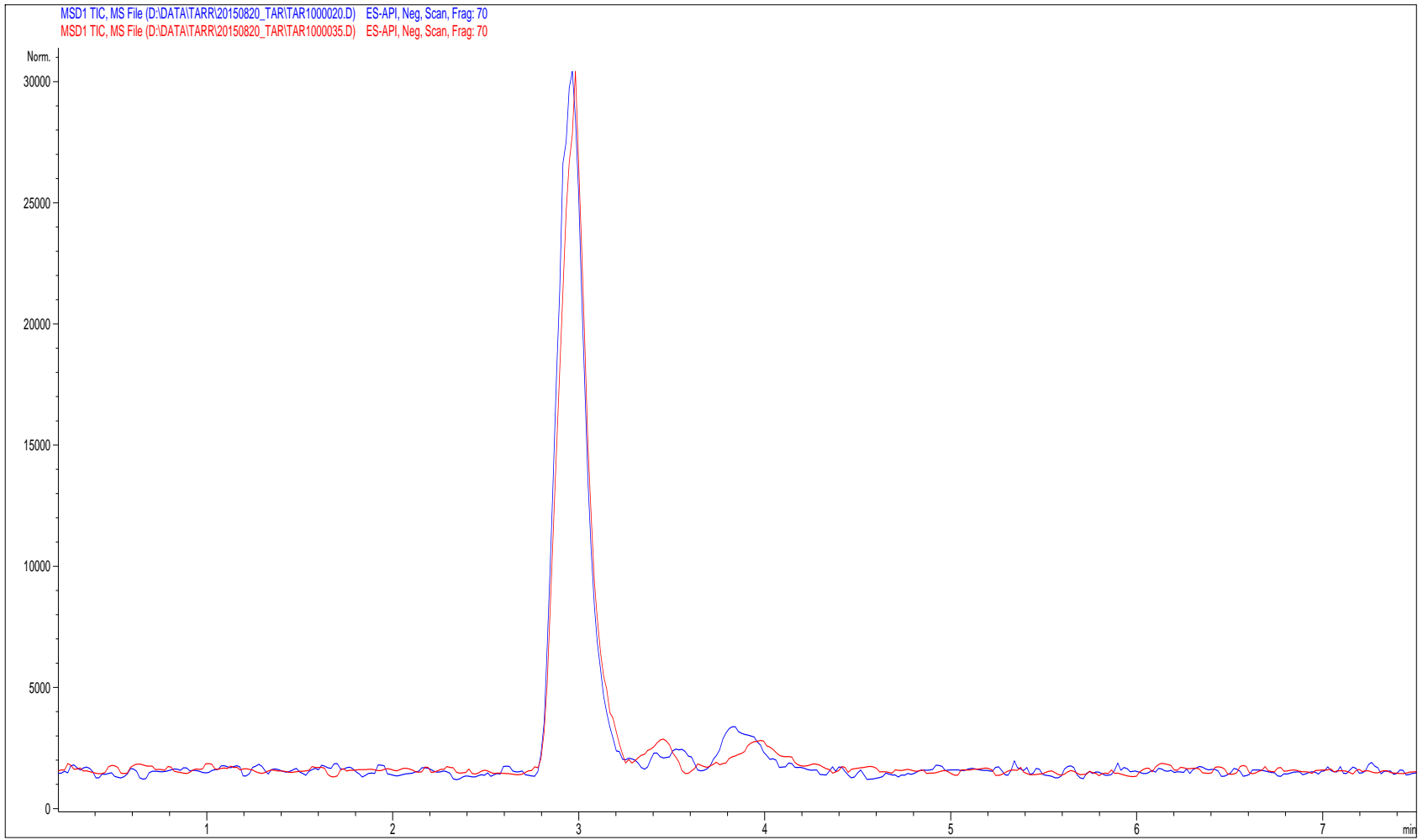
29-Jun-15

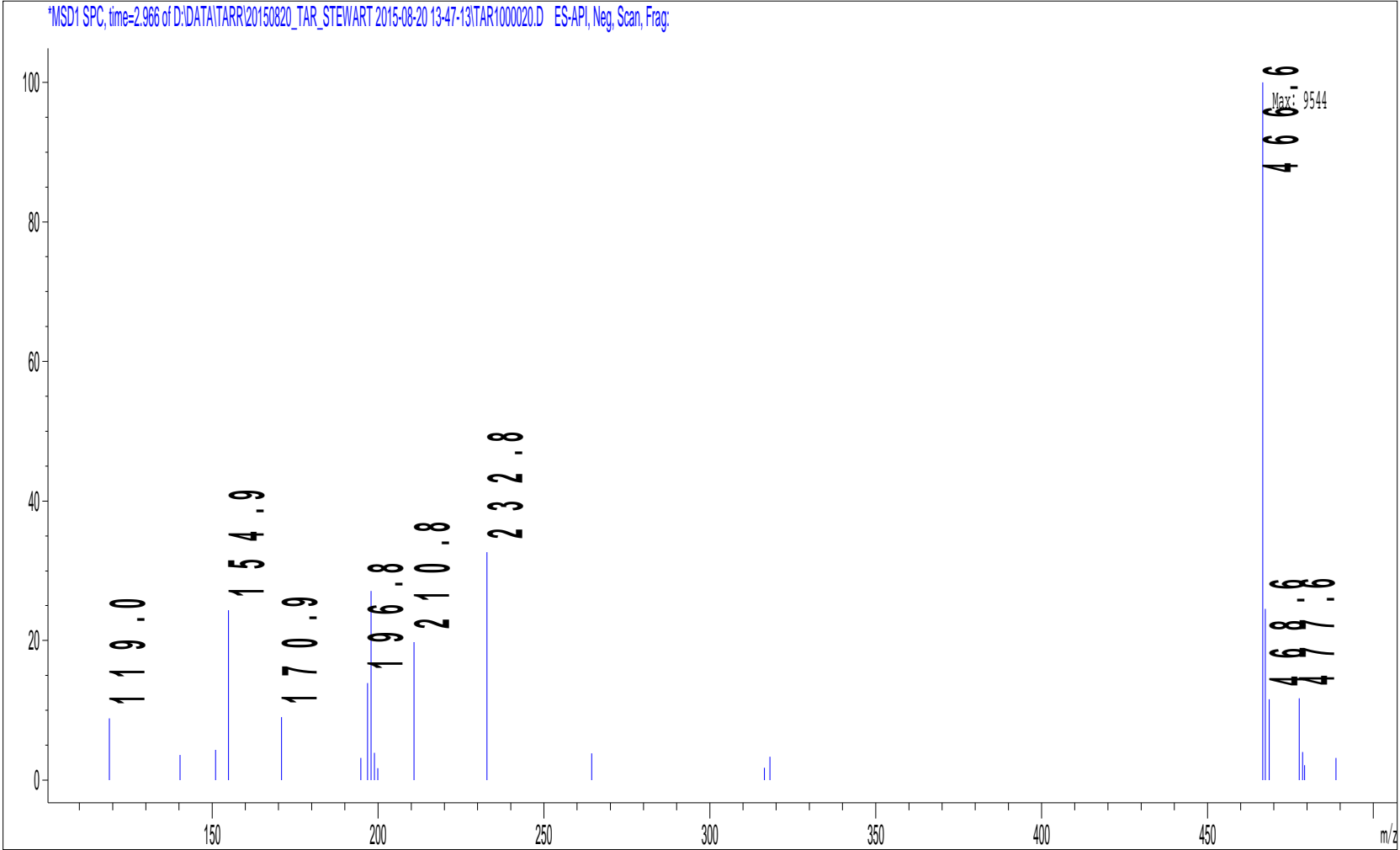
5 DC

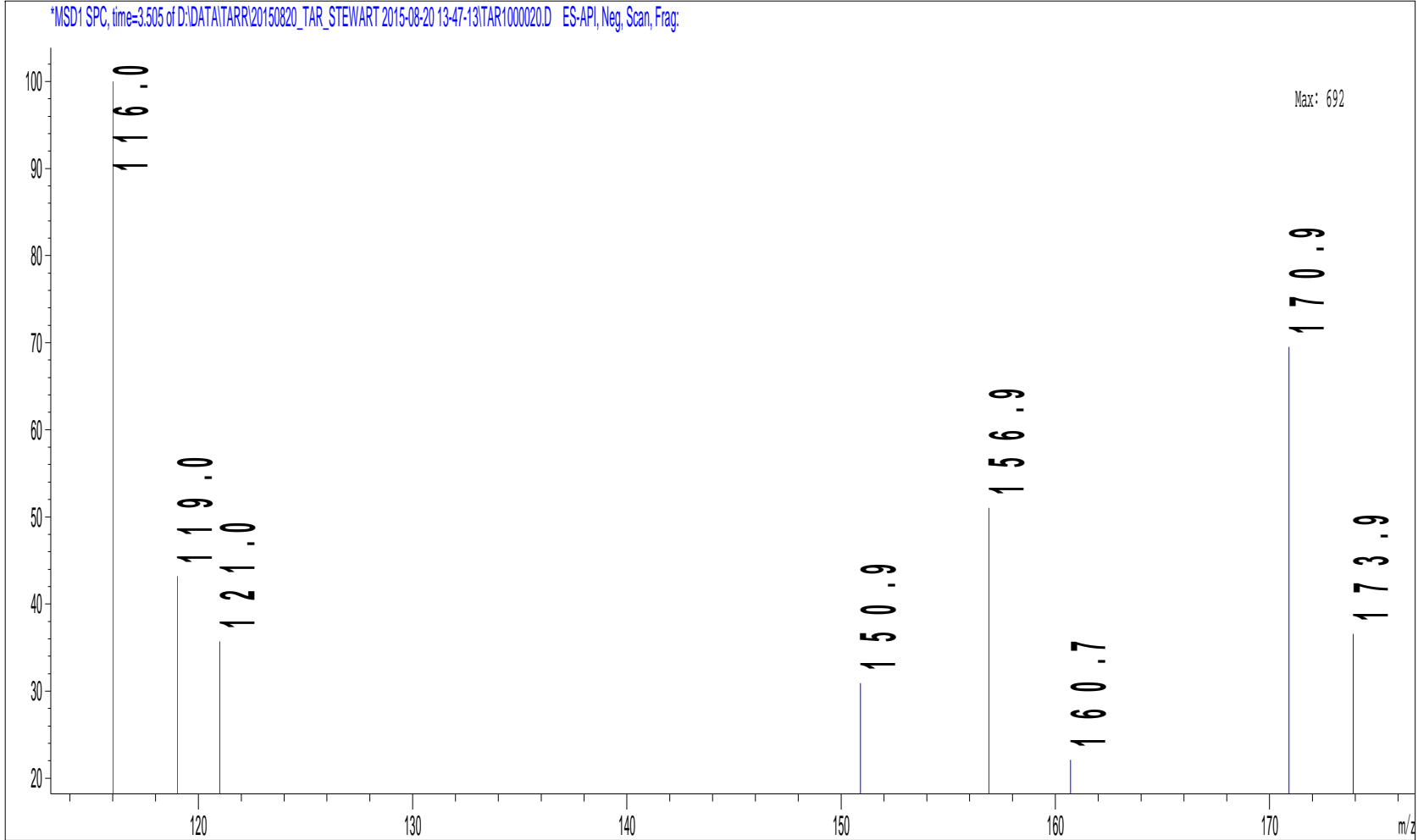
6

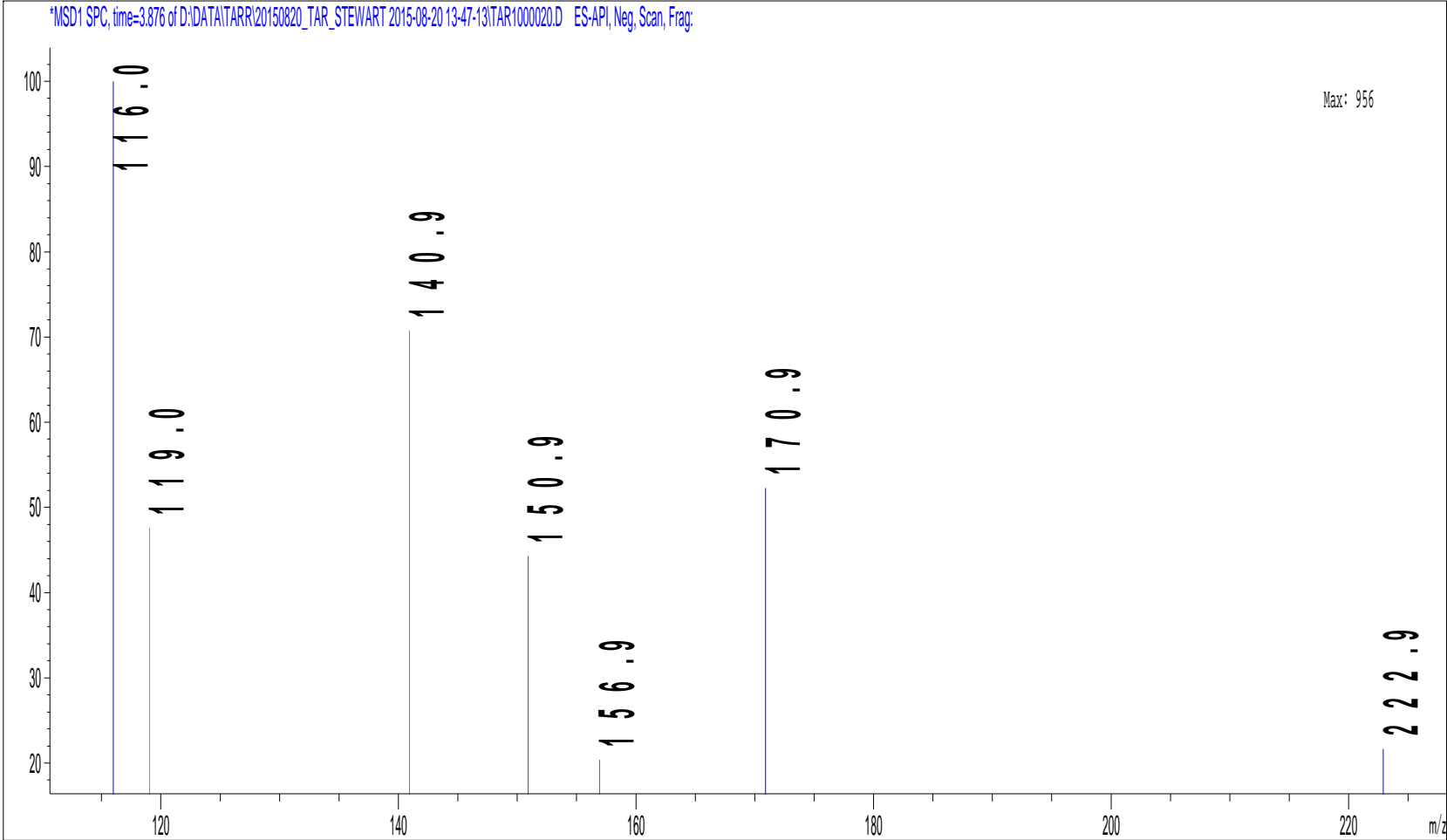
P2-C-02









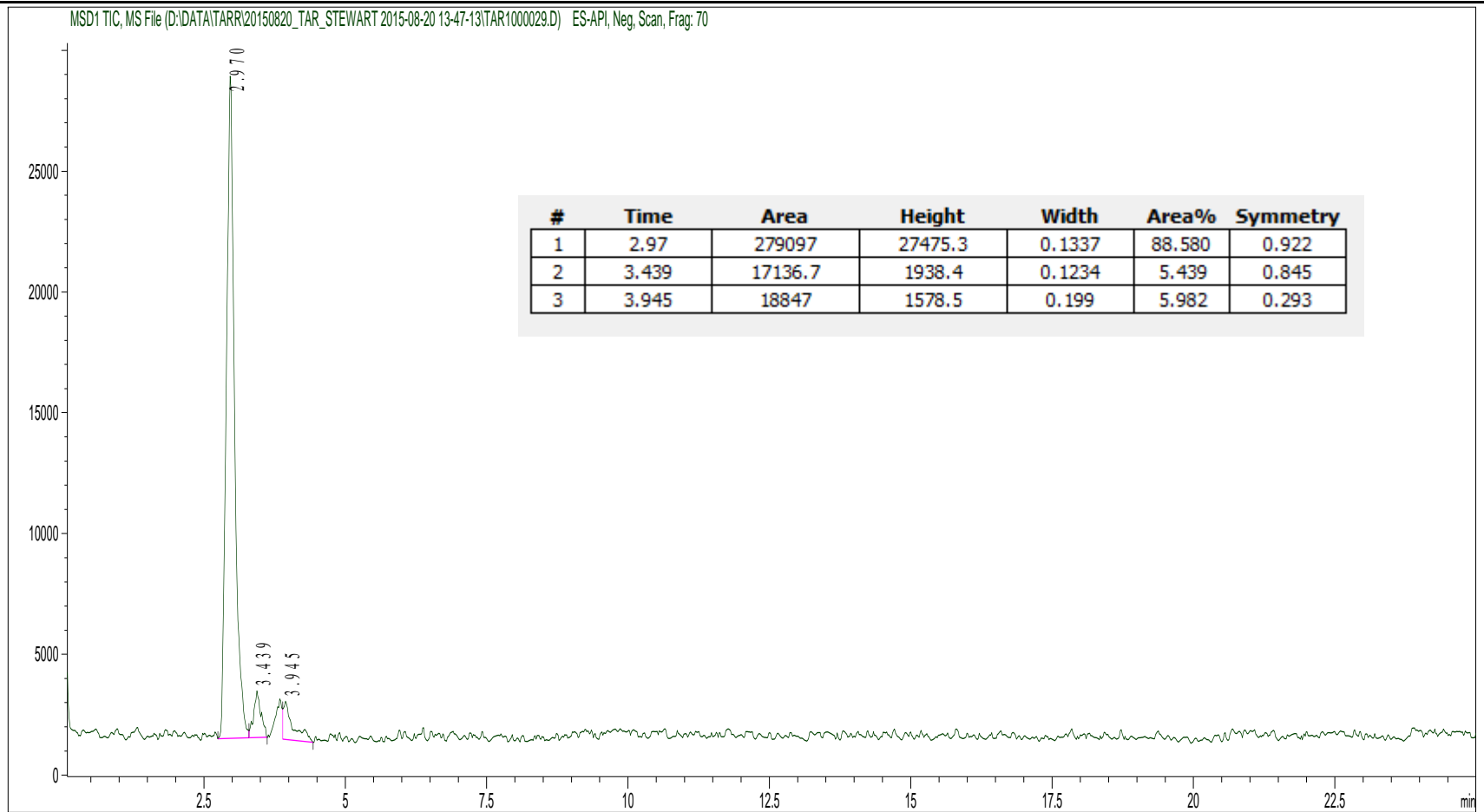


7-Aug-15

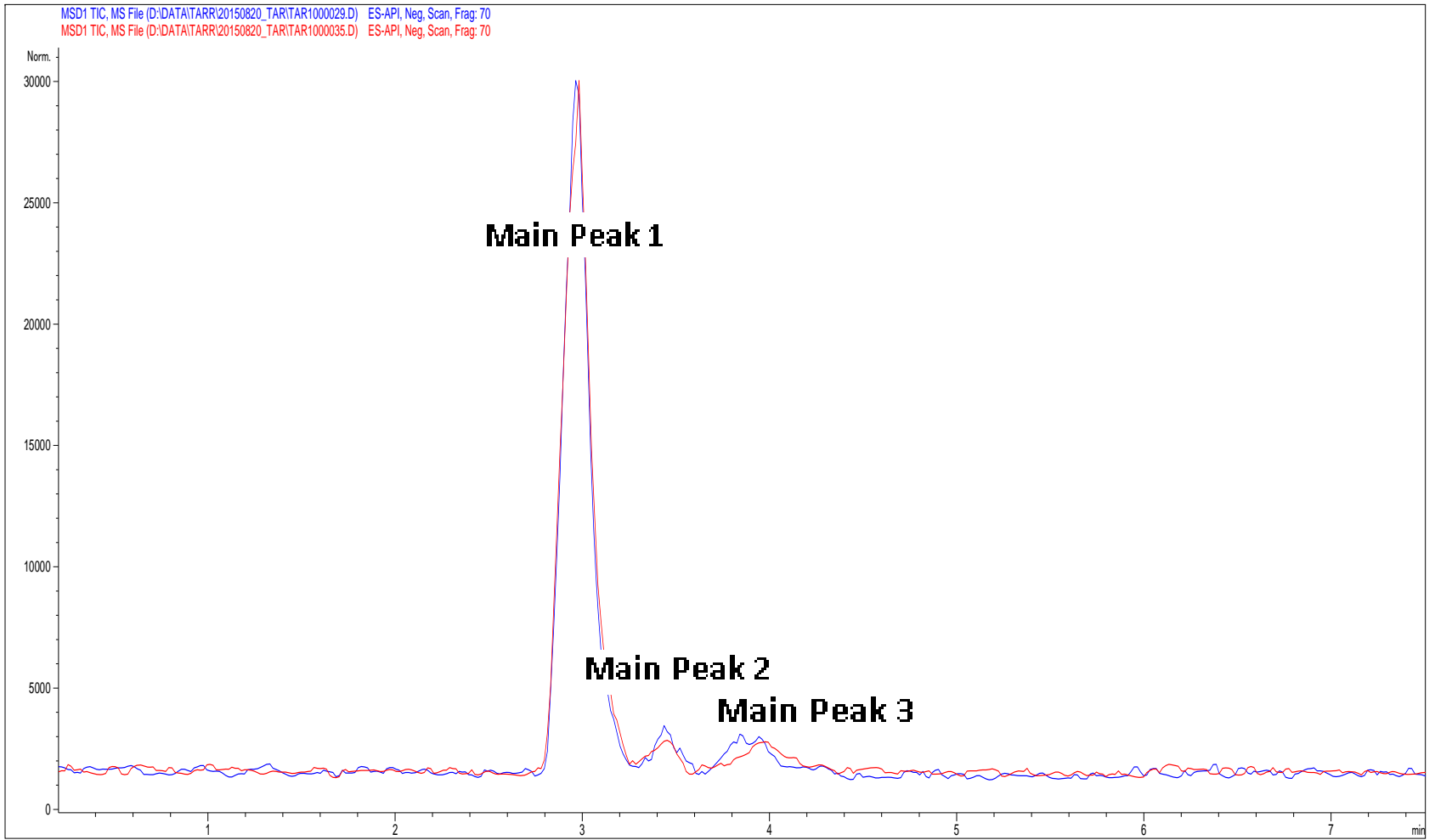
10 DC

6

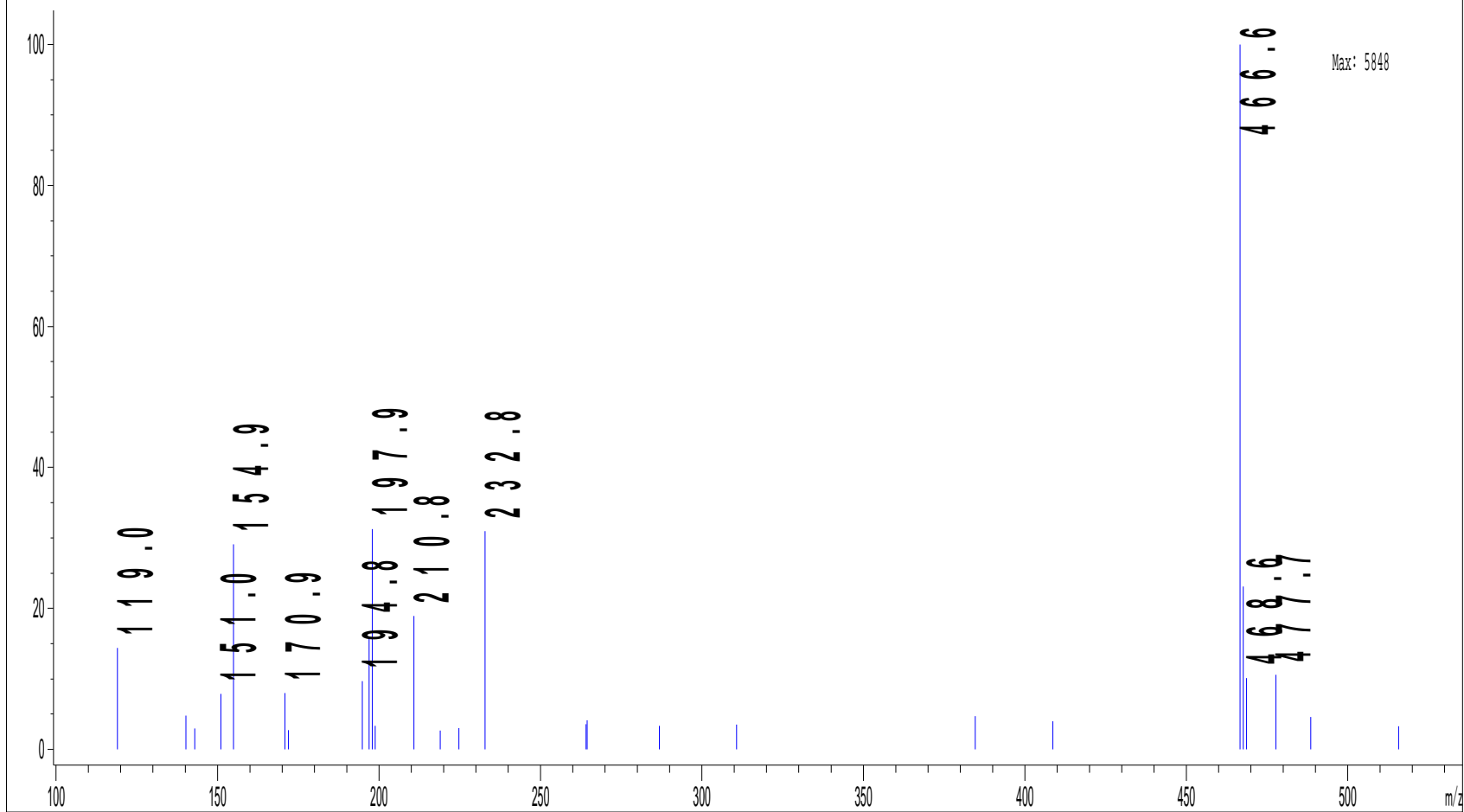
P2-D-08



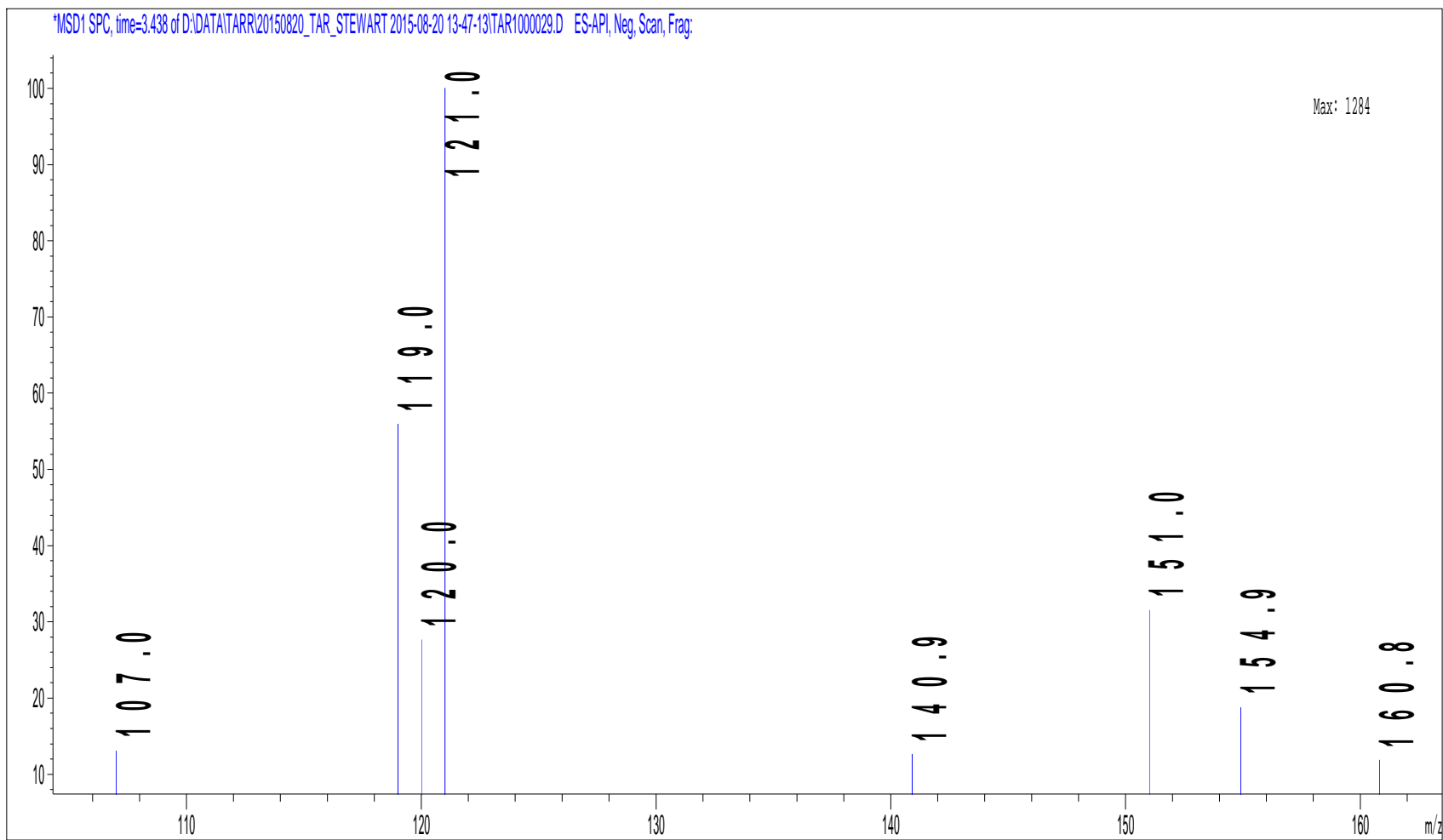




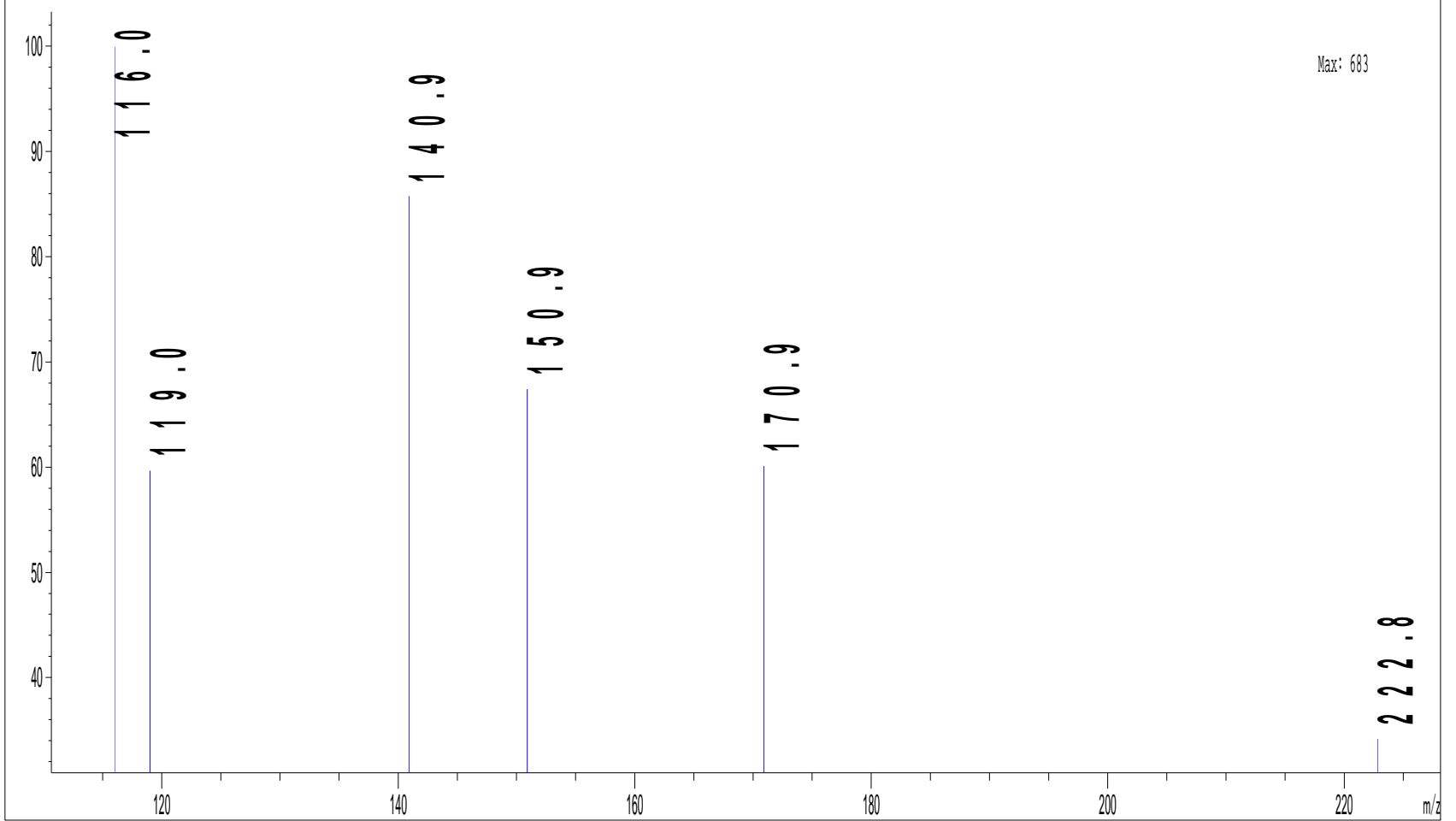
\*MSD1 SPC, time=3.016 of D:\DATA\TARR\20150820\_TAR\_STEWART 2015-08-20 13:47-13\TAR1000029.D ES-API, Neg, Scan, Frag:



\*MSD1 SPC, time=3.438 of D:\DATA\TARR\20150820\_TAR\_STEWART 2015-08-20 13:47:13\TAR1000029.D ES-API, Neg, Scan, Frag:



\*MSD1 SPC, time=3.910 of D:\DATA\TARR\20150820\_TAR\_STEWART 2015-08-20 13:47:13\TAR1000029.D ES-API, Neg. Scan, Frag:

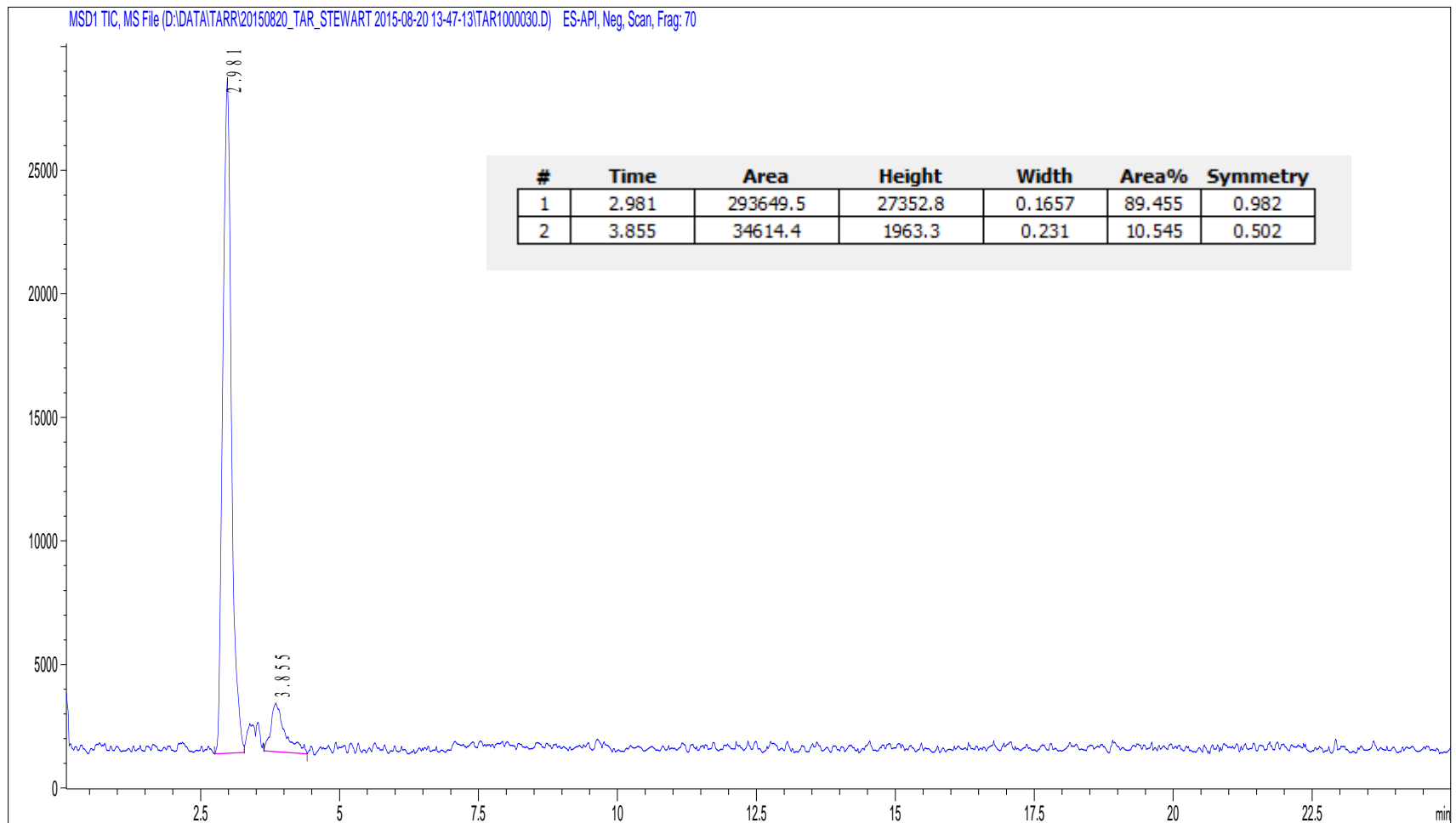


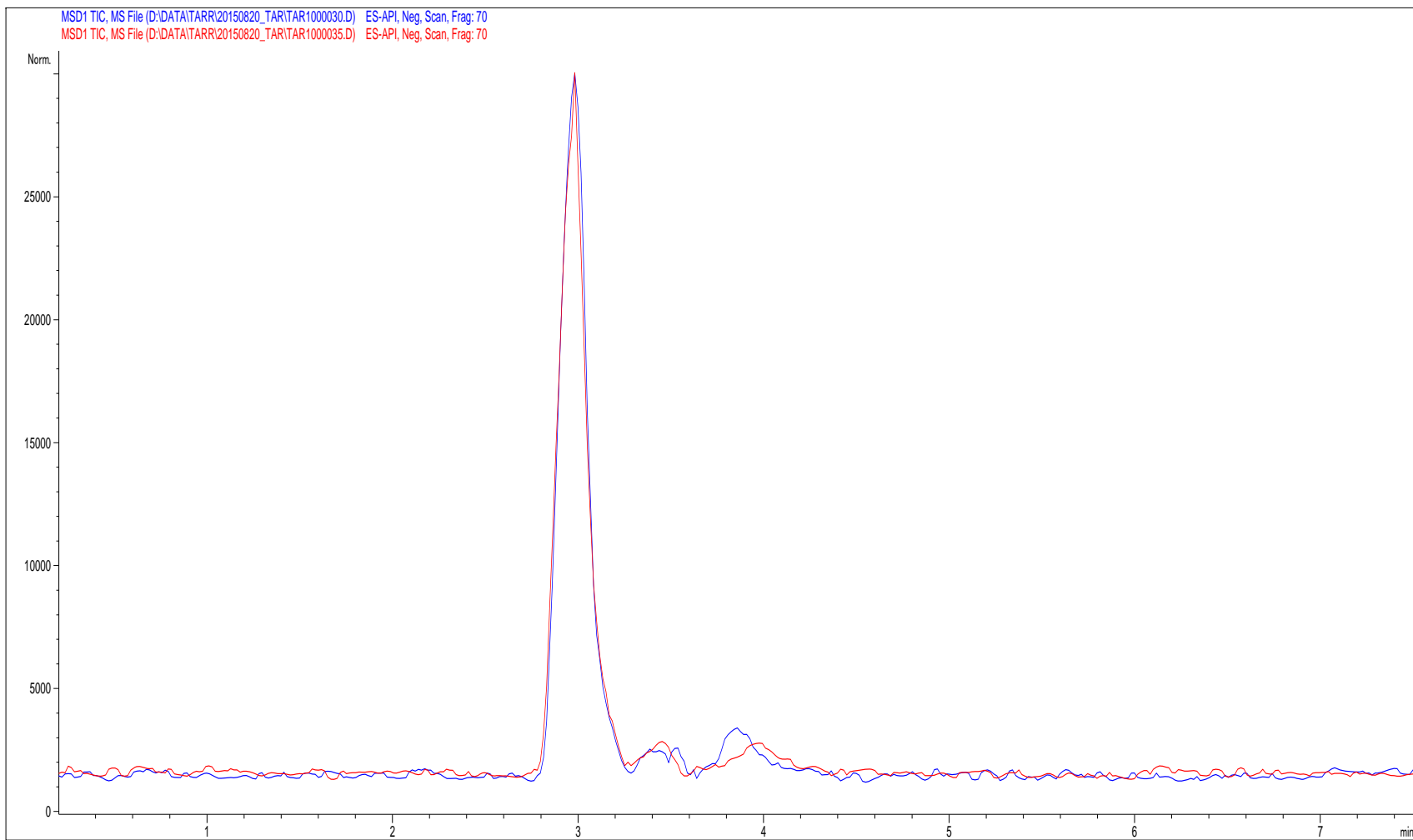
31-Jul-15

10 DC Problem (removal went up)

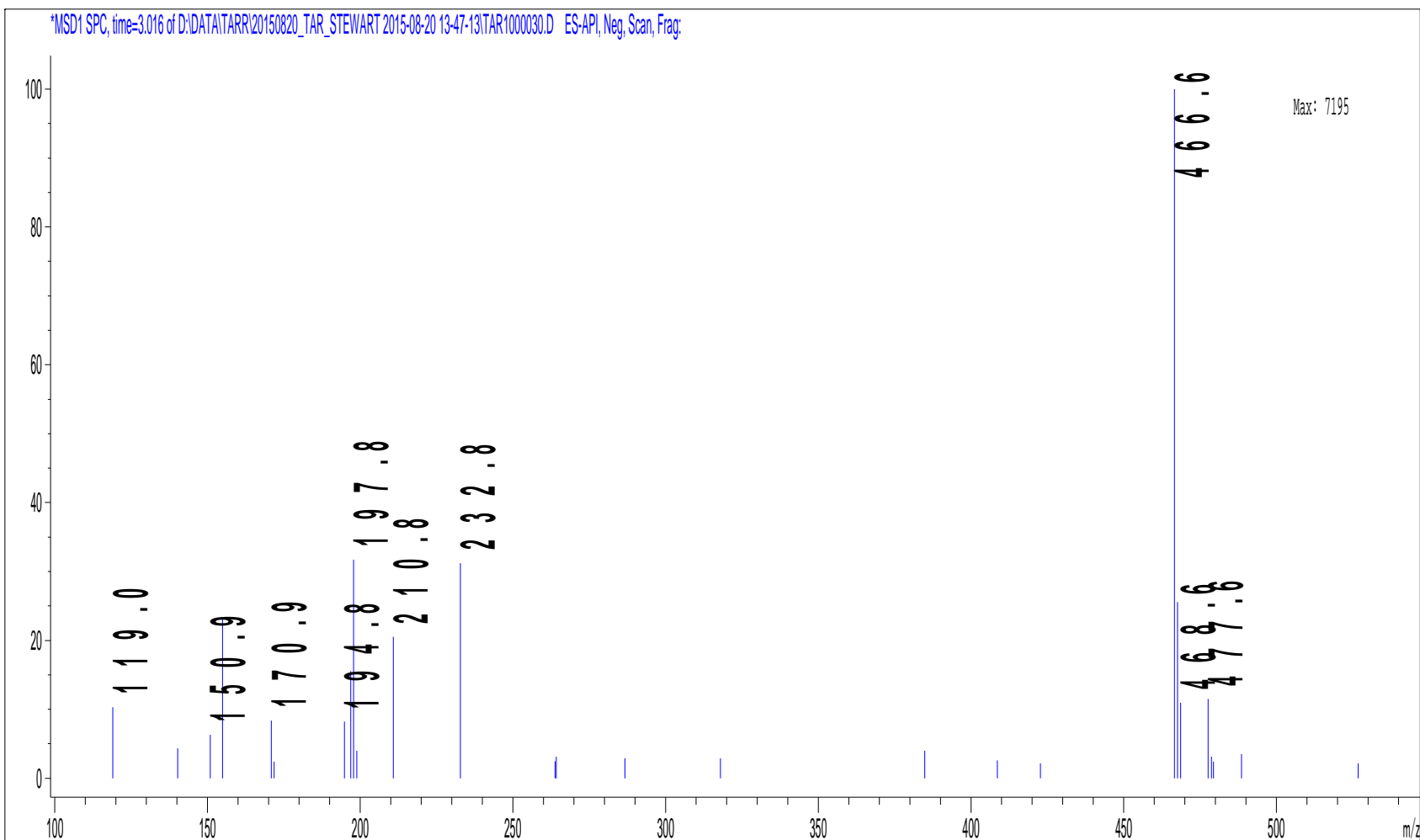
6

P2-D-07

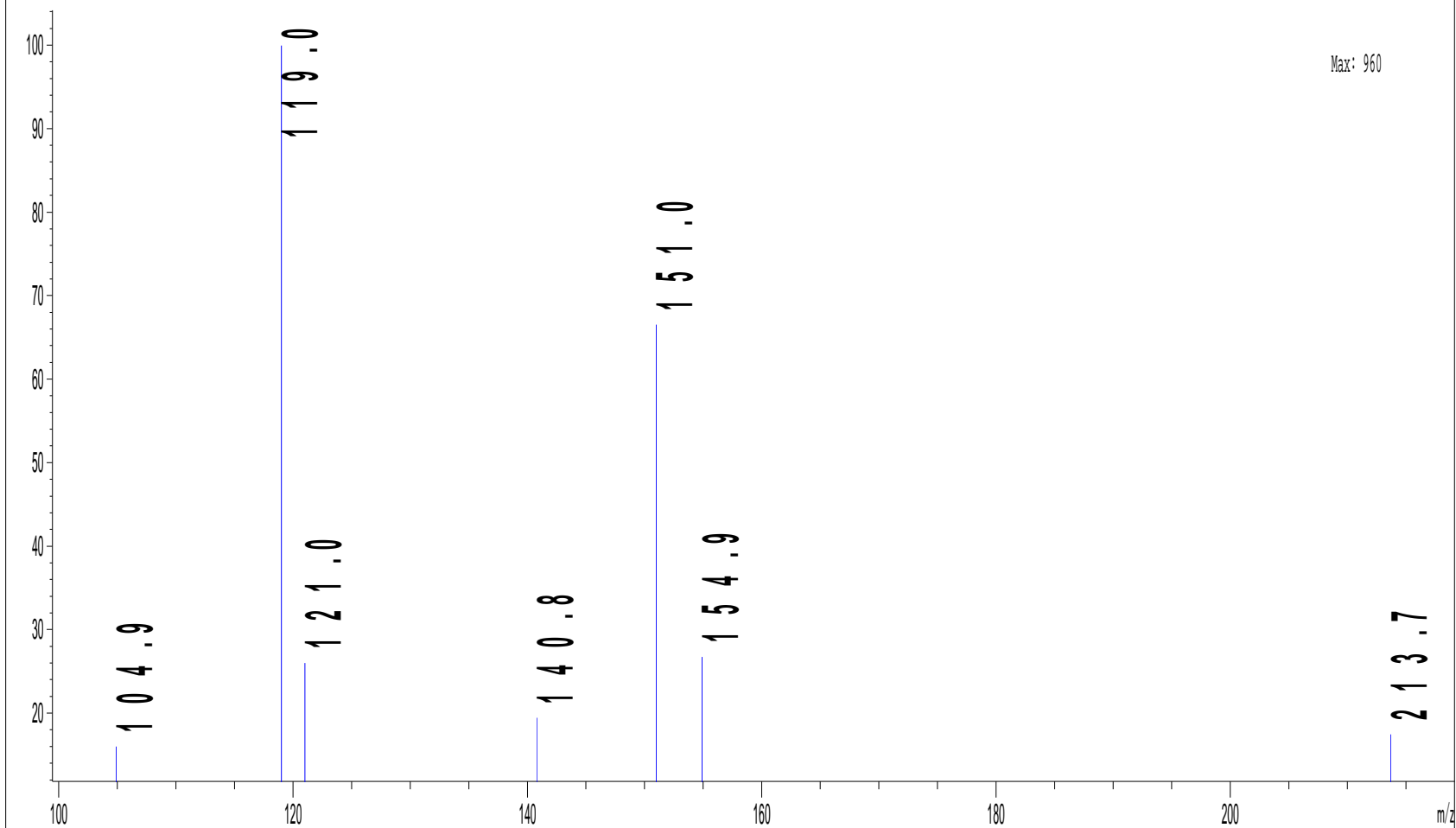




\*MSD1 SPC, time=3.016 of D:\DATA\TARR\20150820\_TAR\_STEWART 2015-08-20 13:47:13\TAR1000030.D ES-API, Neg, Scan, Frag:

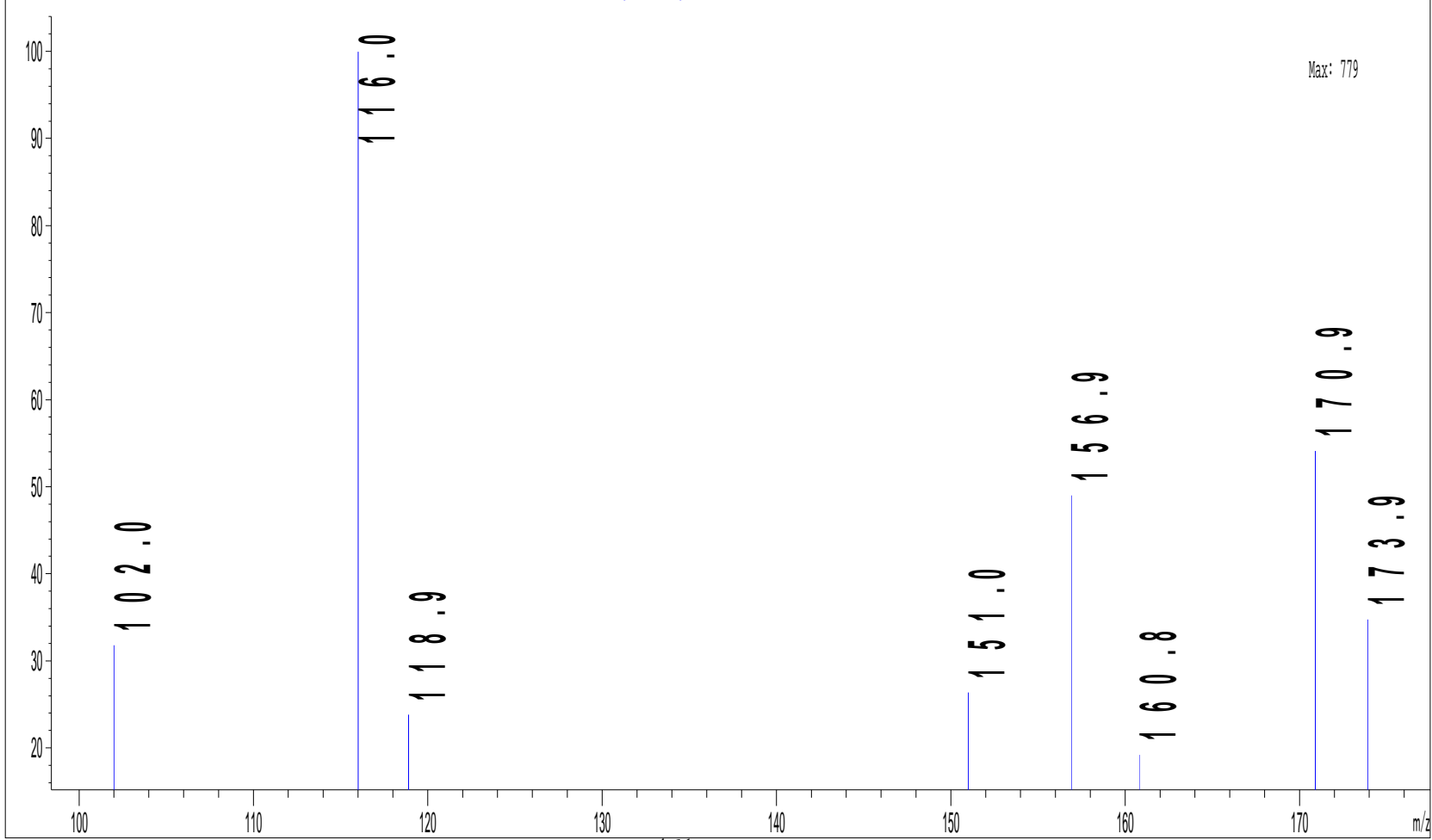


\*MSD1 SPC, time=3.387 of D:\DATA\TARR\20150820\_TAR\_STEWART 2015-08-20 13:47:13\TAR1000030.D ES-API, Neg, Scan, Frag:



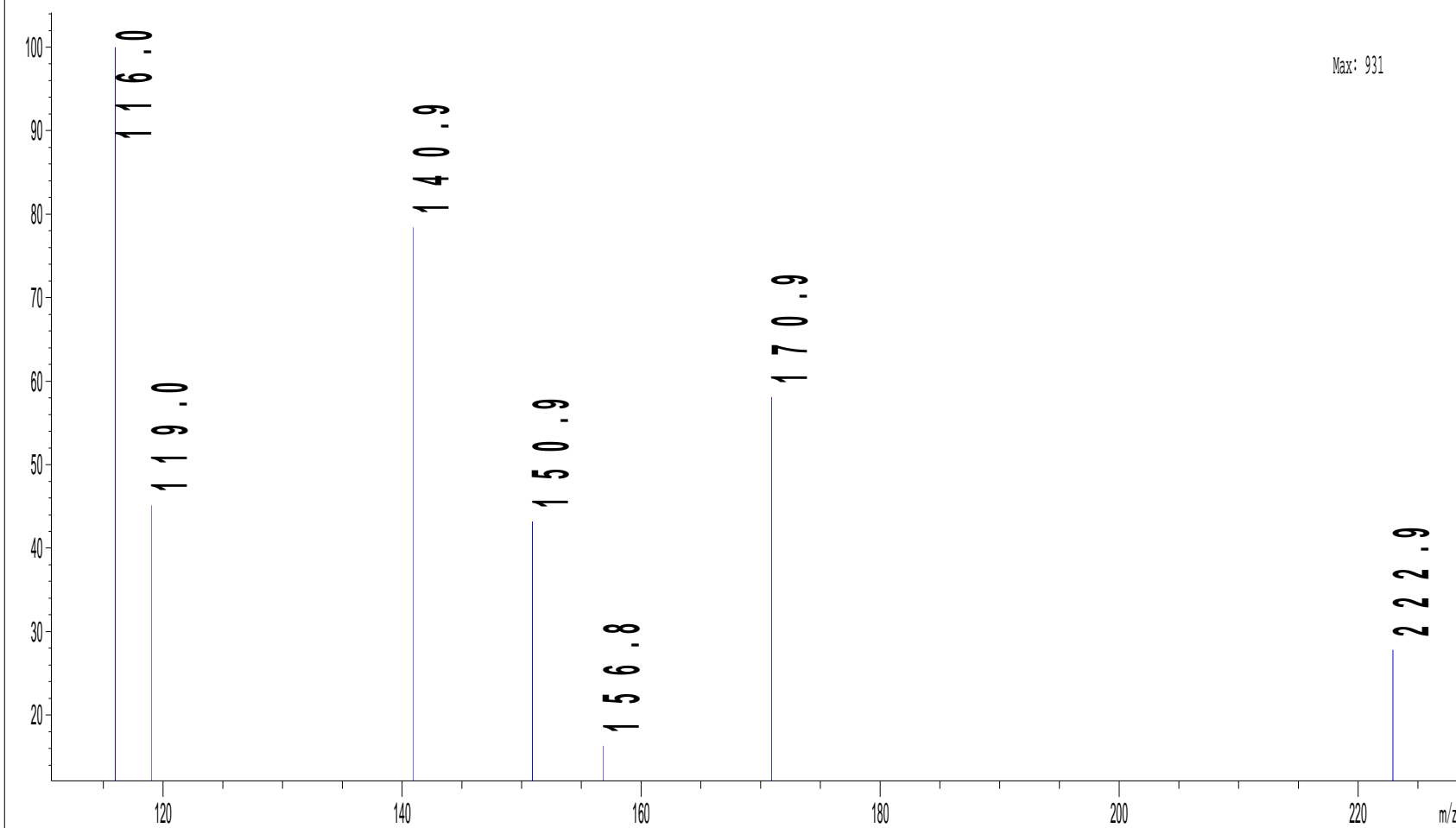


\*MSD1 SPC, time=3.522 of D:\DATA\TARR\20150820\_TAR\_STEWART 2015-08-20 13:47-13\TAR1000030.D ES-API, Neg, Scan, Frag:



Max: 779

\*MSD1 SPC, time=3.859 of D:\DATA\TARR\20150820\_TAR\_STEWART 2015-08-20 13:47-13\TAR1000030.D ES-API, Neg, Scan, Frag:

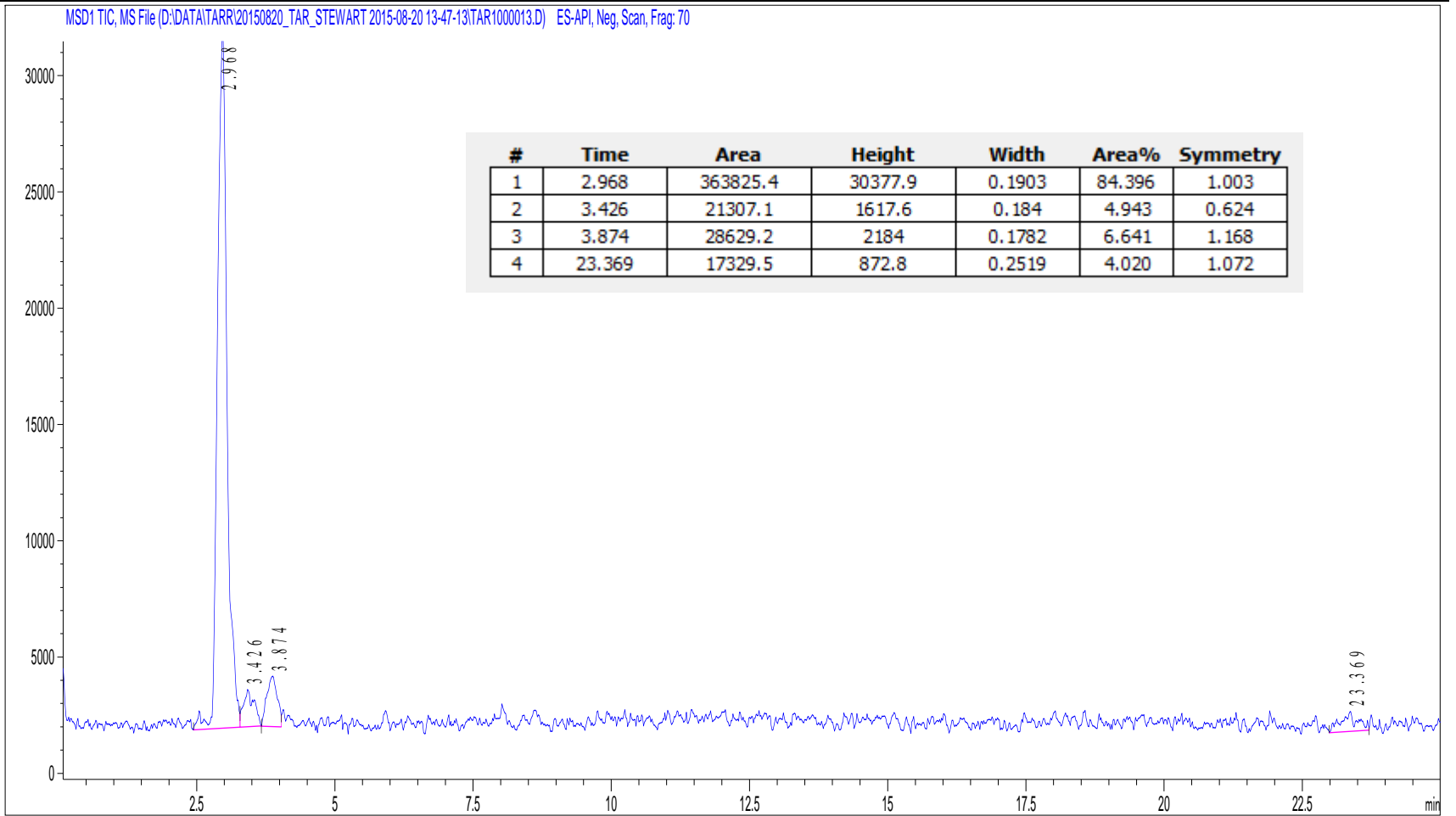


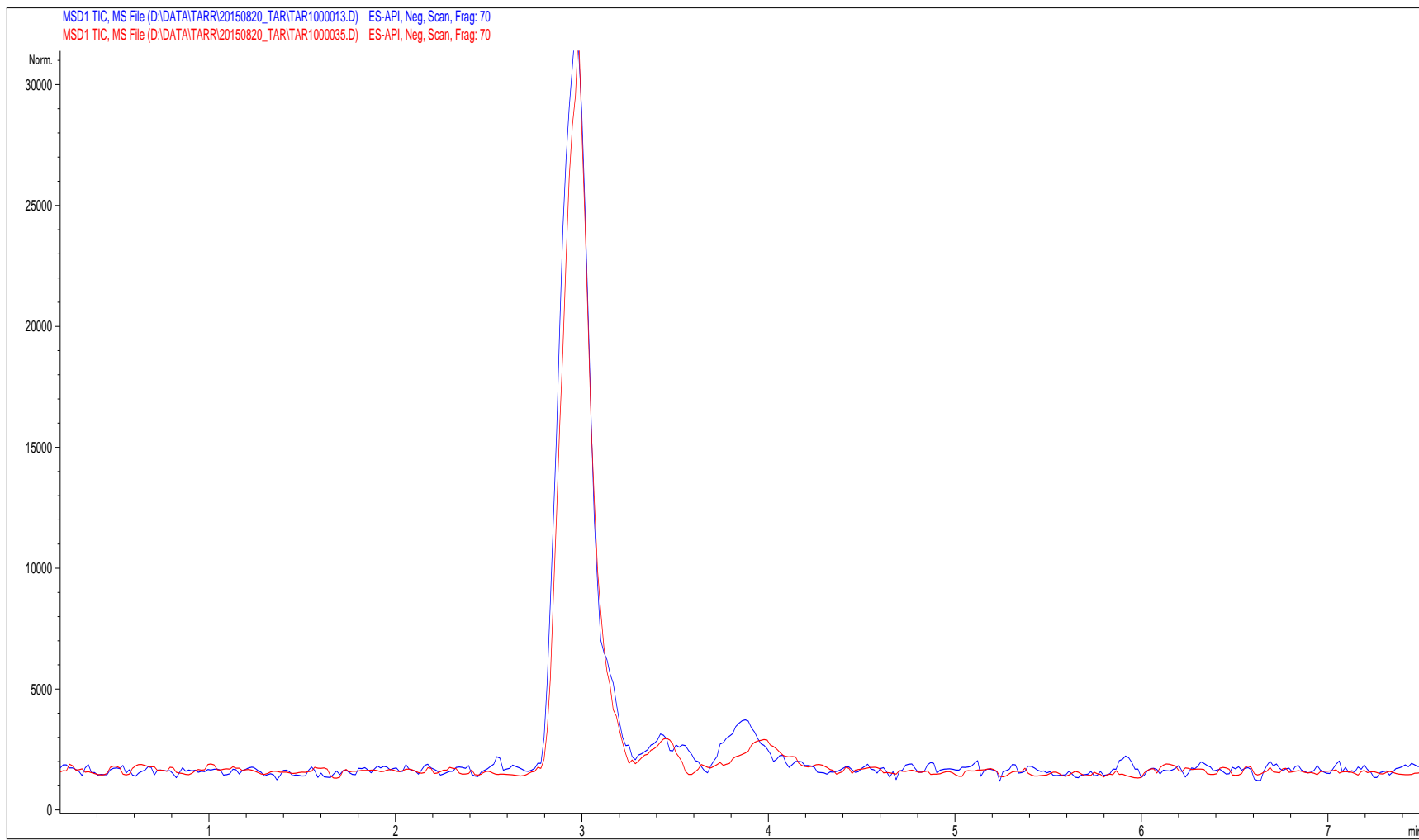
9-Jun-15

20 DC

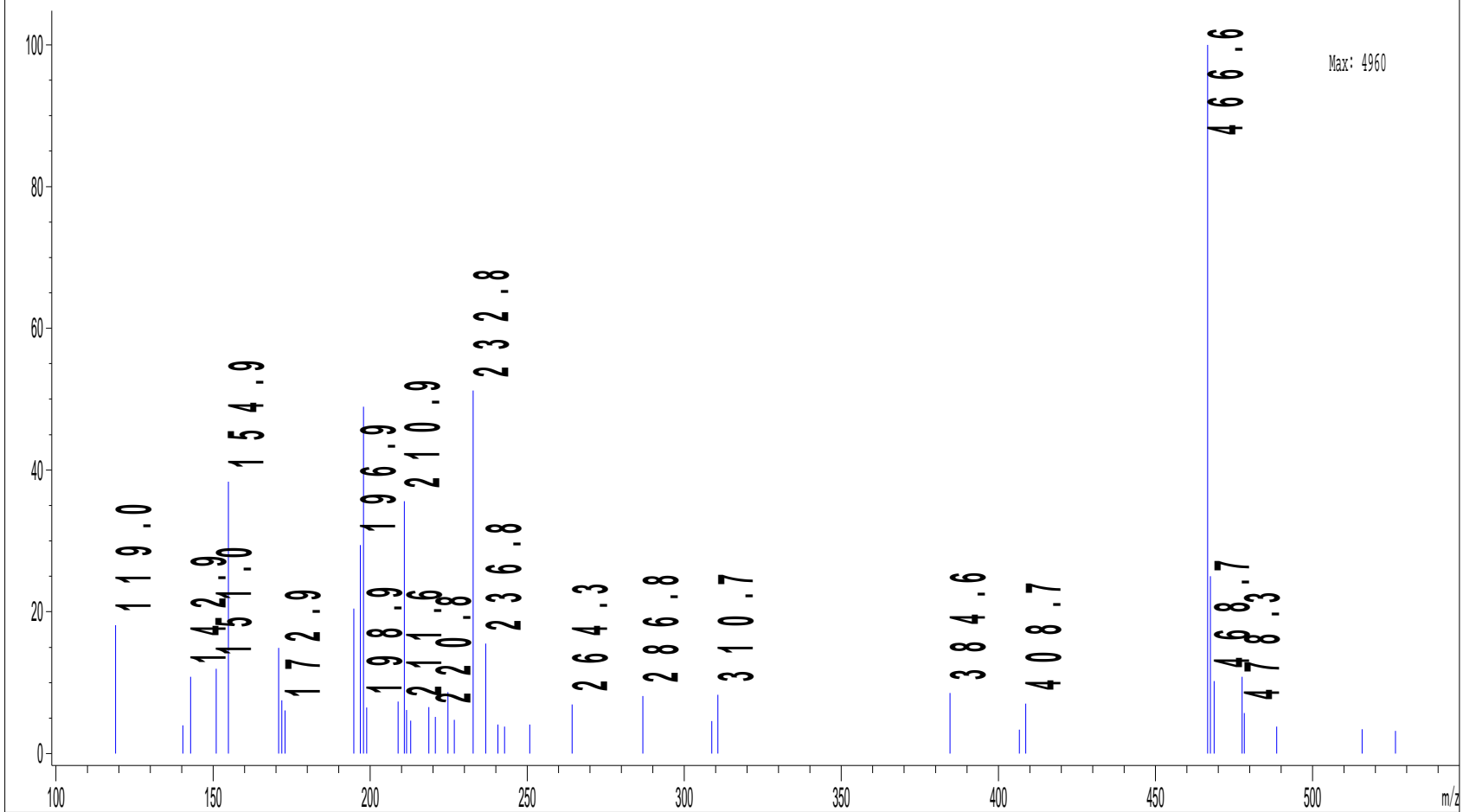
6

P2-B-06

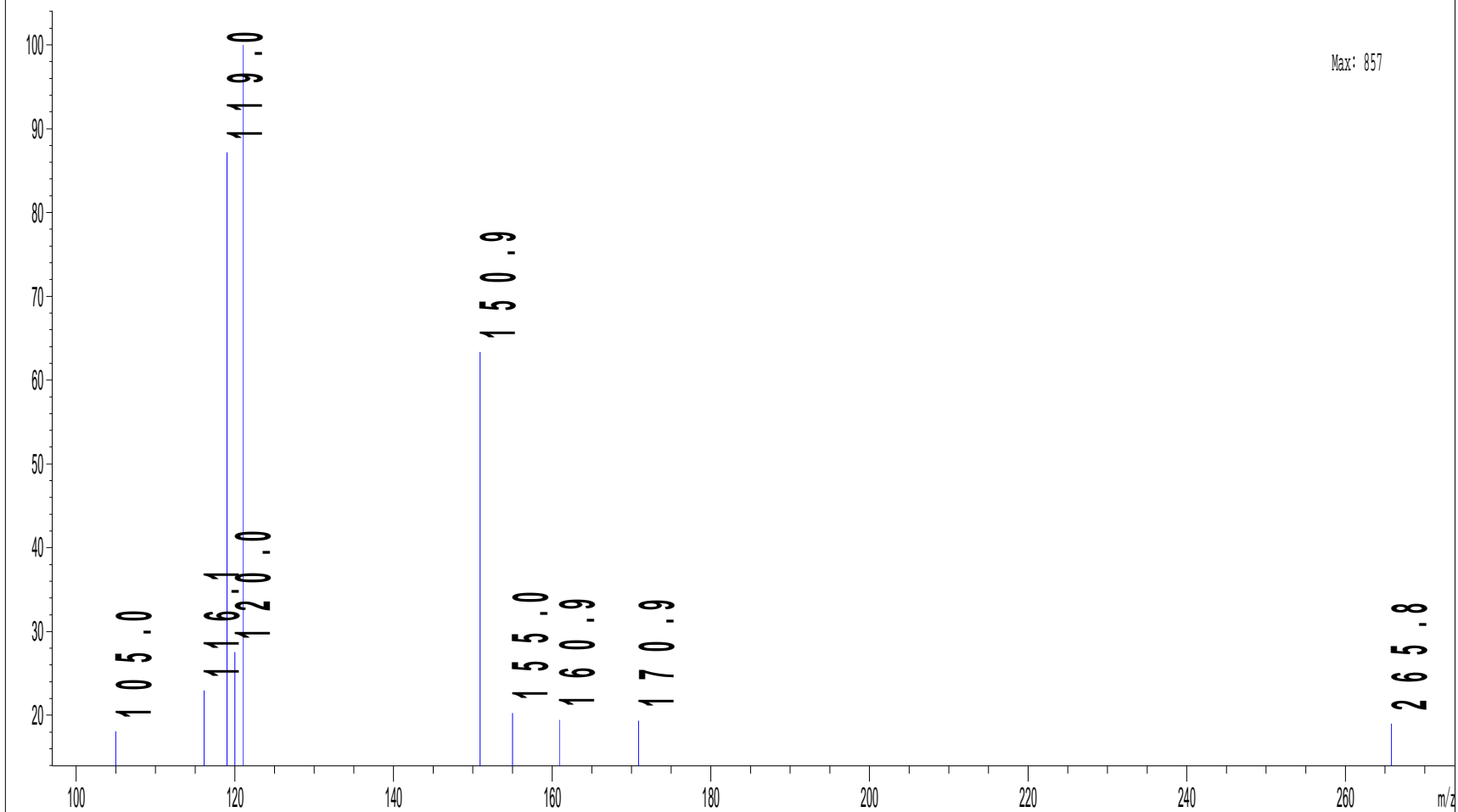




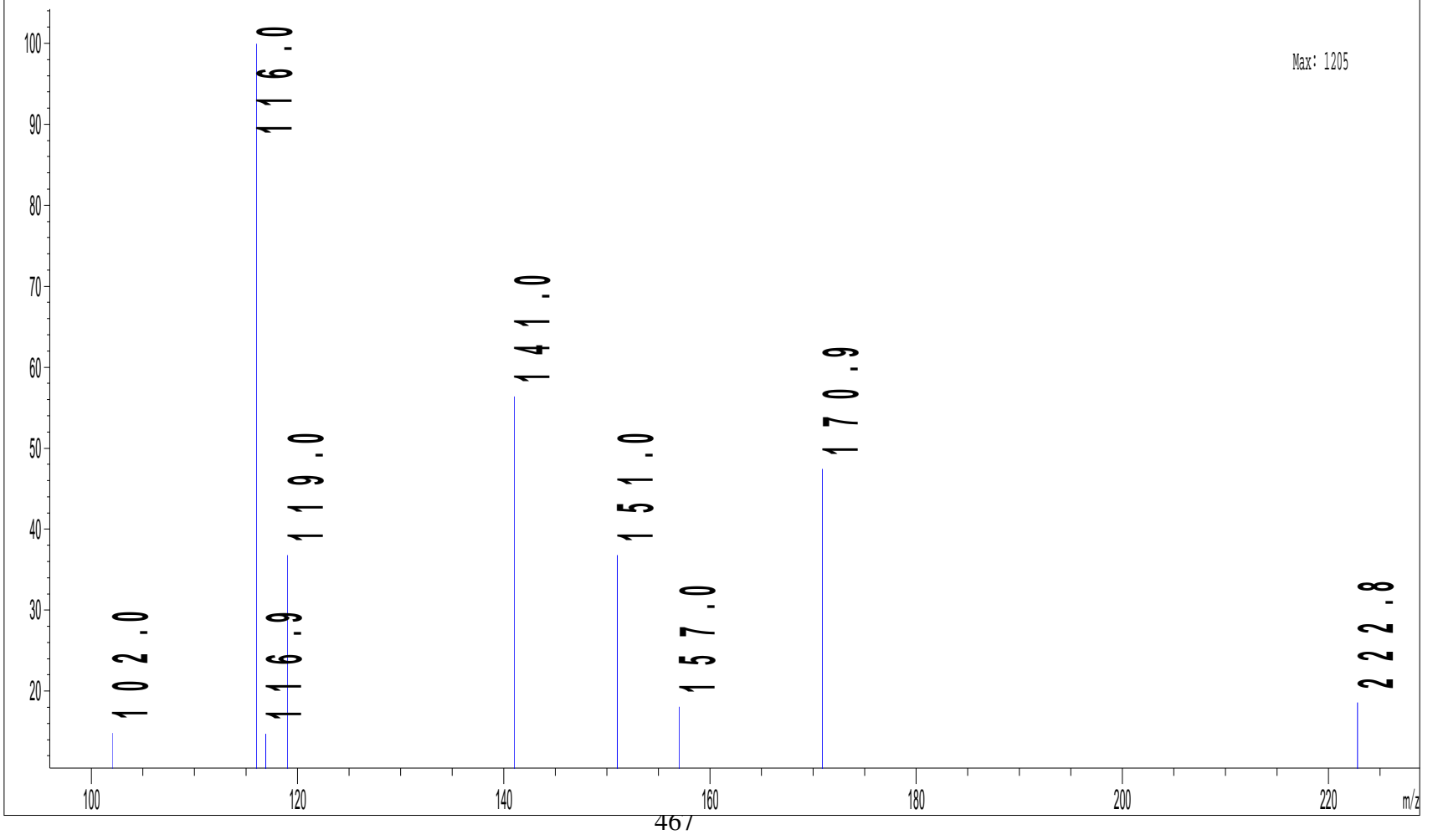
\*MSD1 SPC, time=2.999 of D:\DATA\TARR\20150820\_TAR\_STEWART 2015-08-20 13:47:13\TAR1000013.D ES-API, Neg, Scan, Frag:



\*MSD1 SPC, time=3.454 of D:\DATA\TARR\20150820\_TAR\_STEWART 2015-08-20 13:47:13\TAR1000013.D ES-API, Neg, Scan, Frag:



\*MSD1 SPC, time=3.859 of D:\DATA\TARR\20150820\_TAR\_STEWART 2015-08-20 13:47:13\TAR1000013.D ES-API, Neg. Scan, Frag:



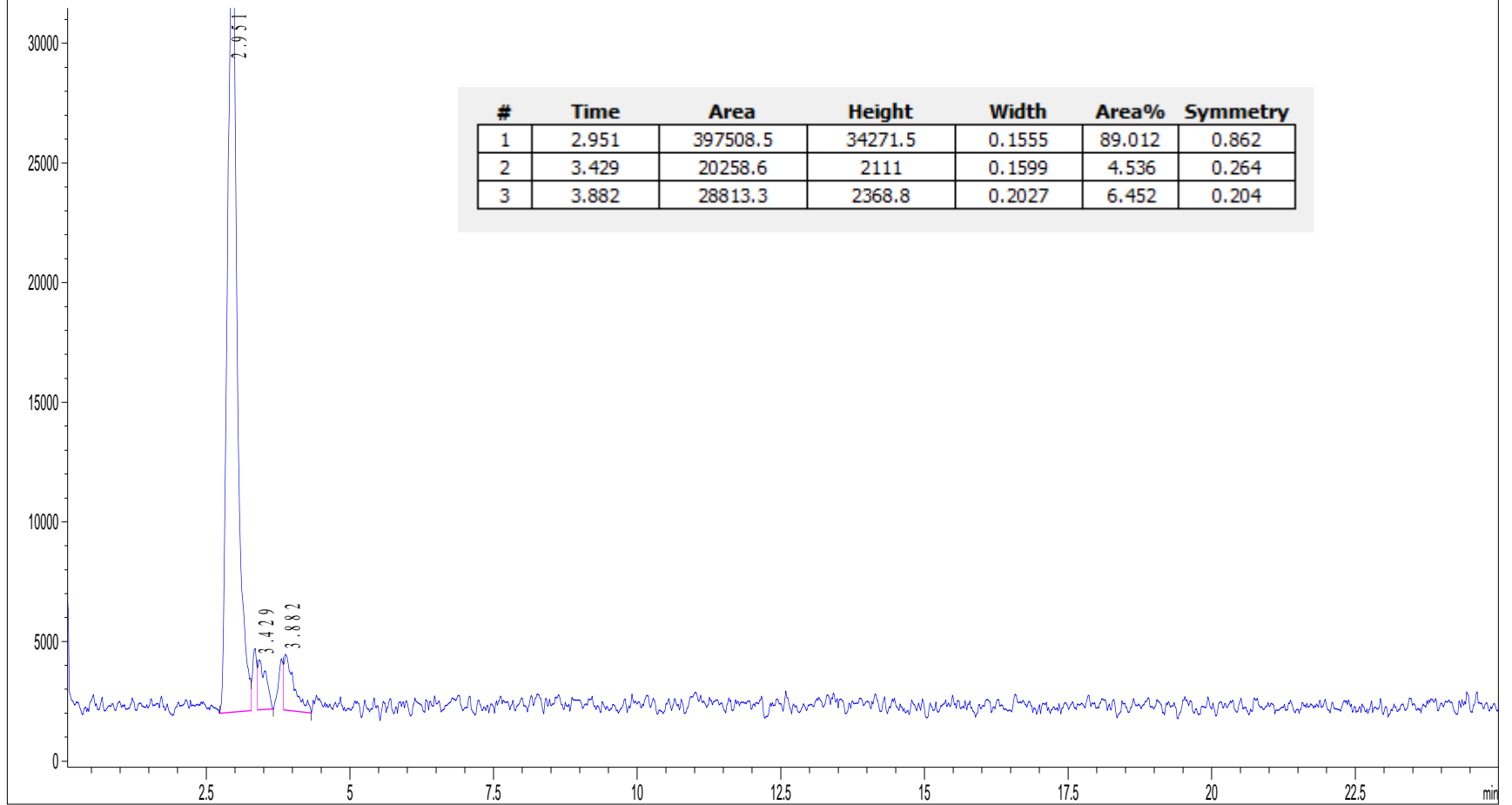
17-Jun-15

30 DC

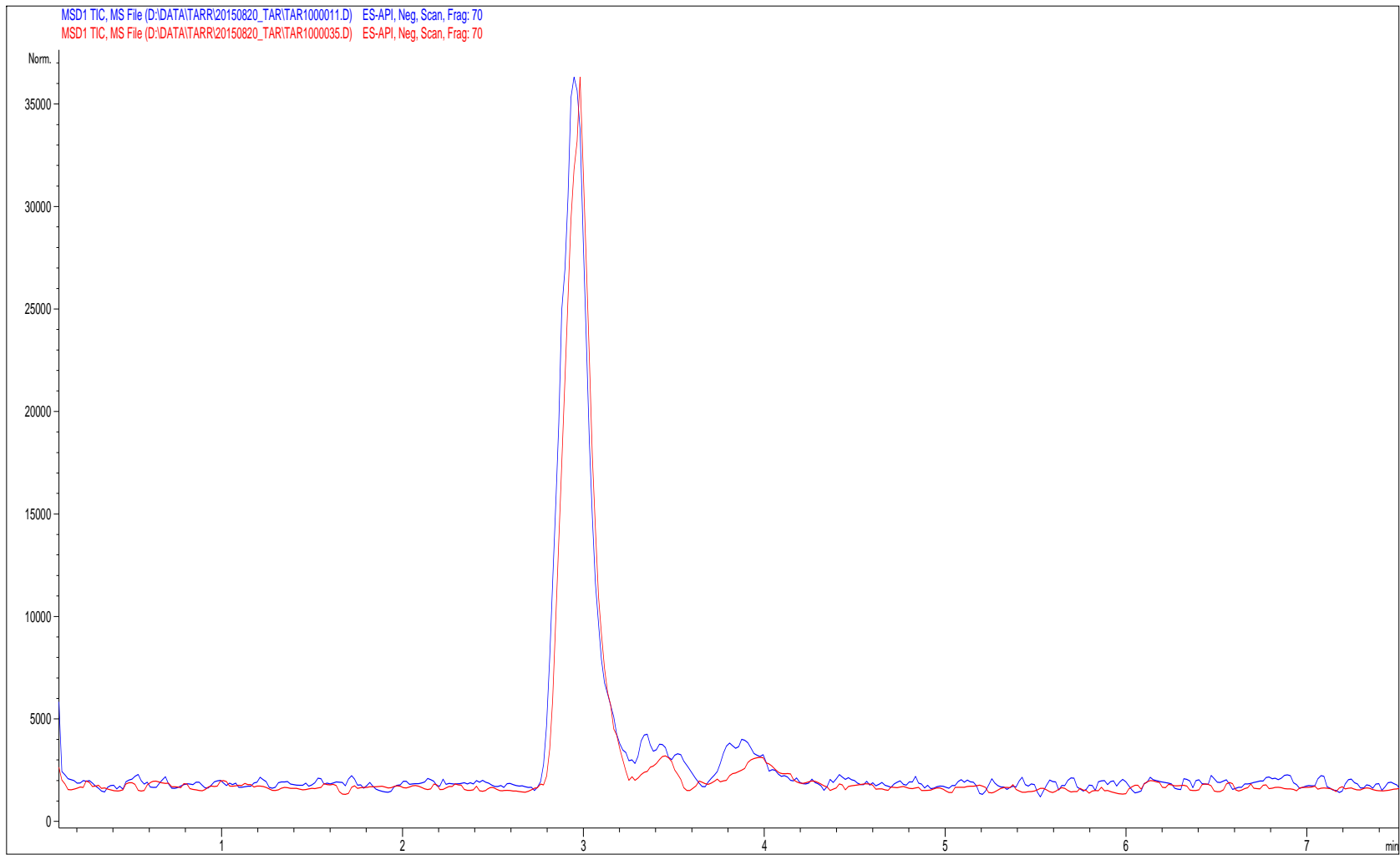
6

P2-B-08

MSD1 TIC, MS File (D:\DATA\TARR\20150820\_TAR\_STEWART 2015-08-20 13-47-13\TAR1000011.D) ES-API, Neg, Scan, Frag: 70

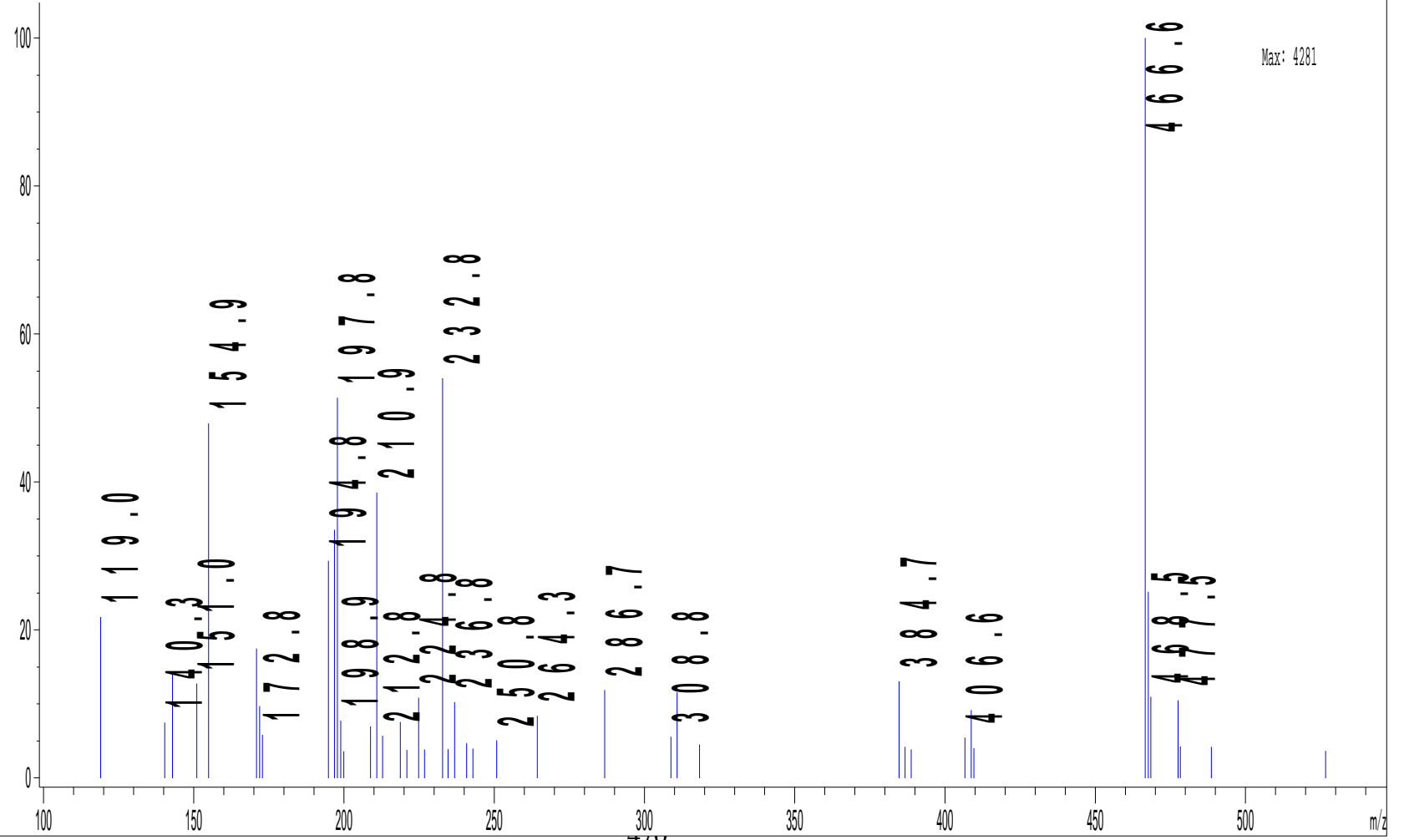




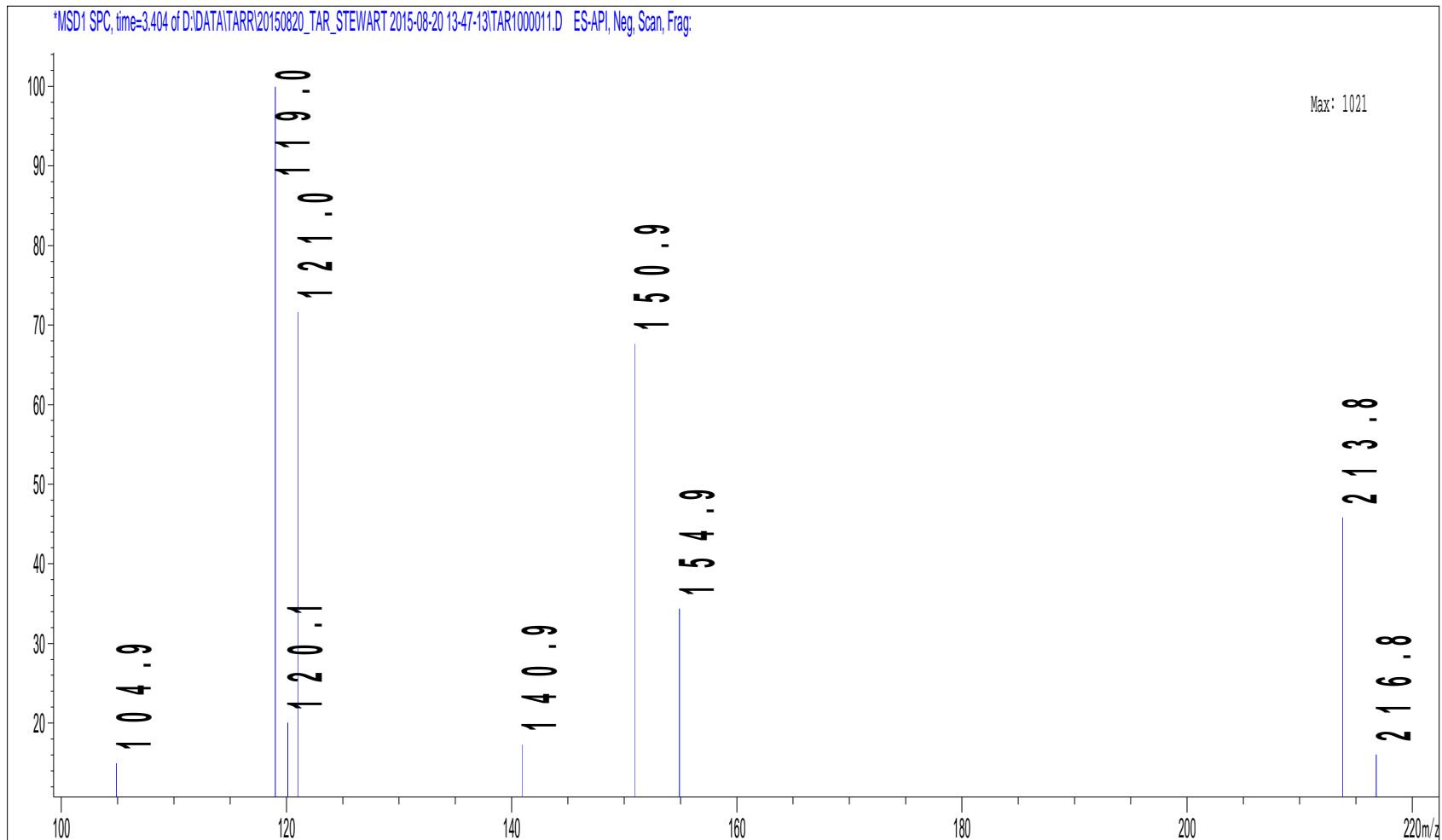


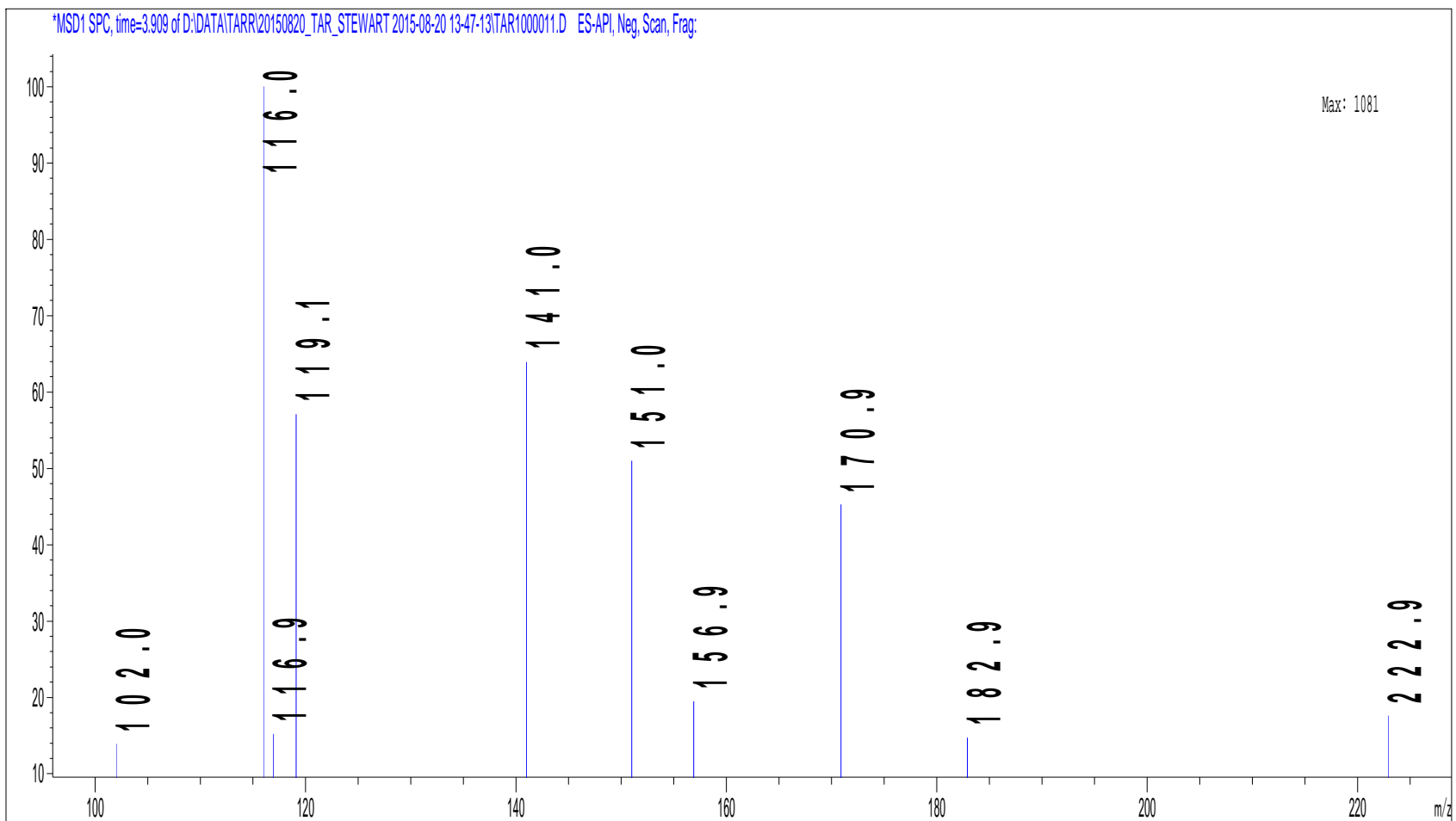
469

\*MSD1 SPC, time=2.999 of D:\DATA\TARR\20150820\_TAR\_STEWART 2015-08-20 13:47:13\TAR1000011.D ES-API, Neg, Scan, Frag:



Max: 4281





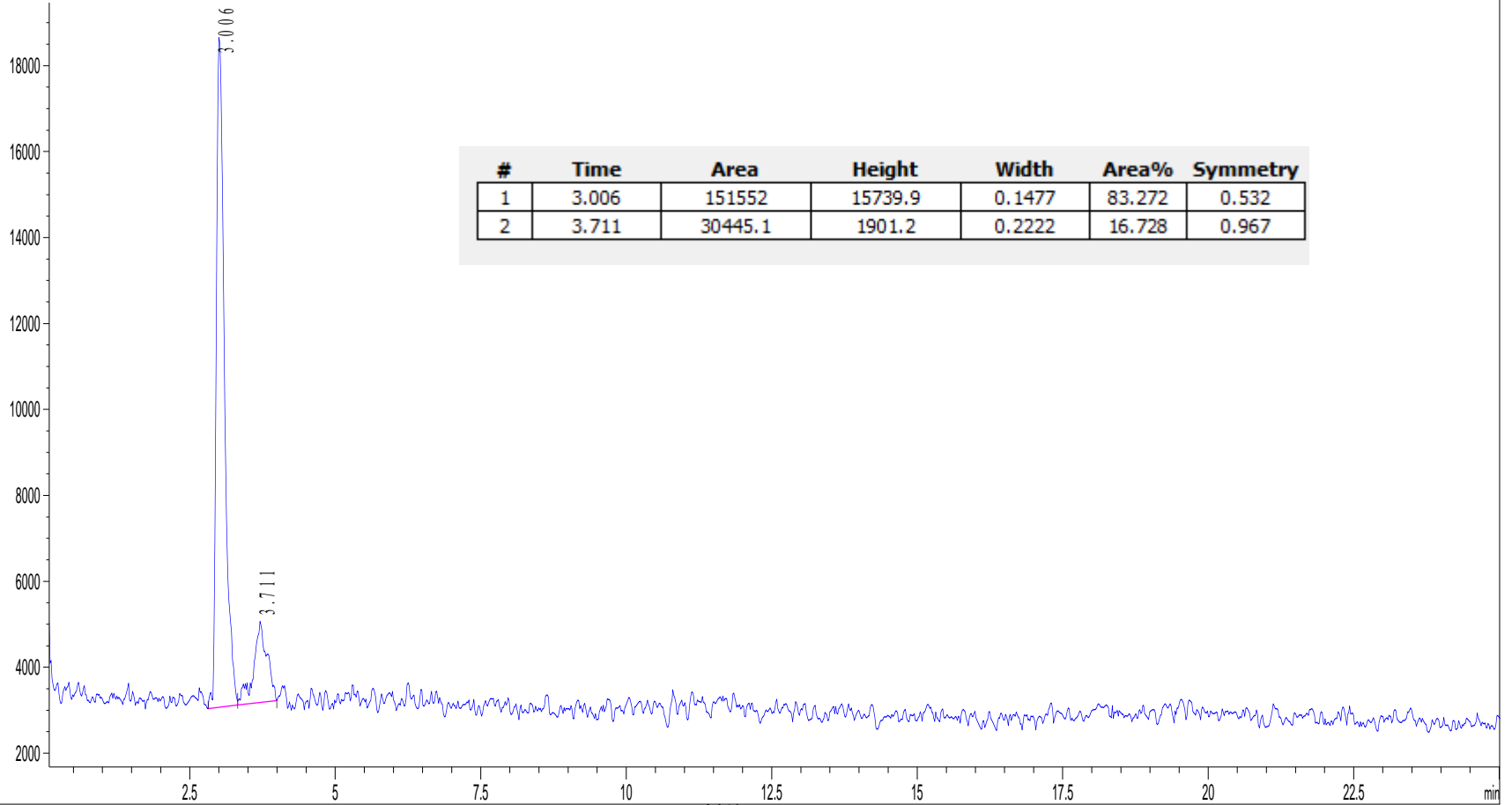
4-Aug-15

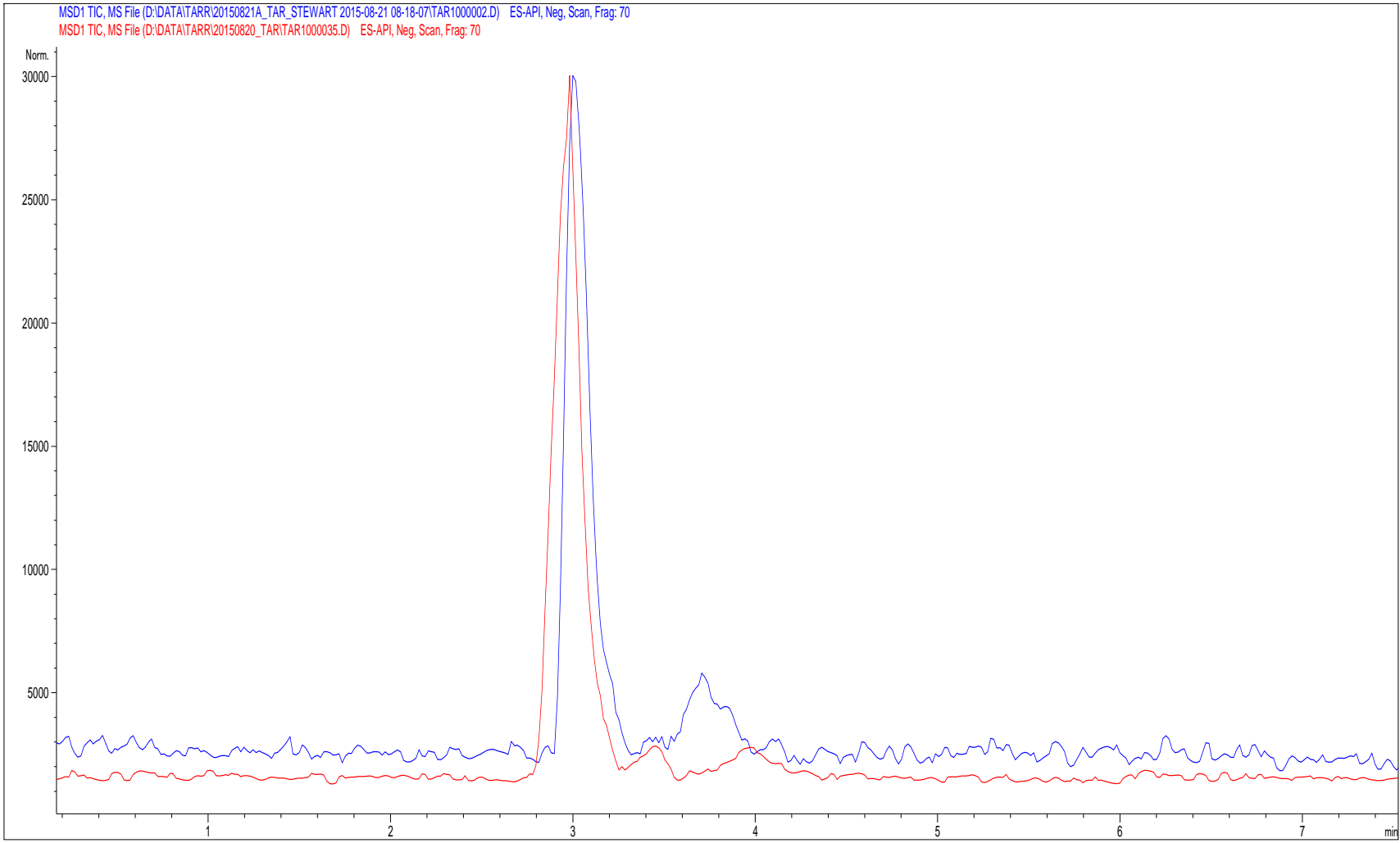
50 DC

6

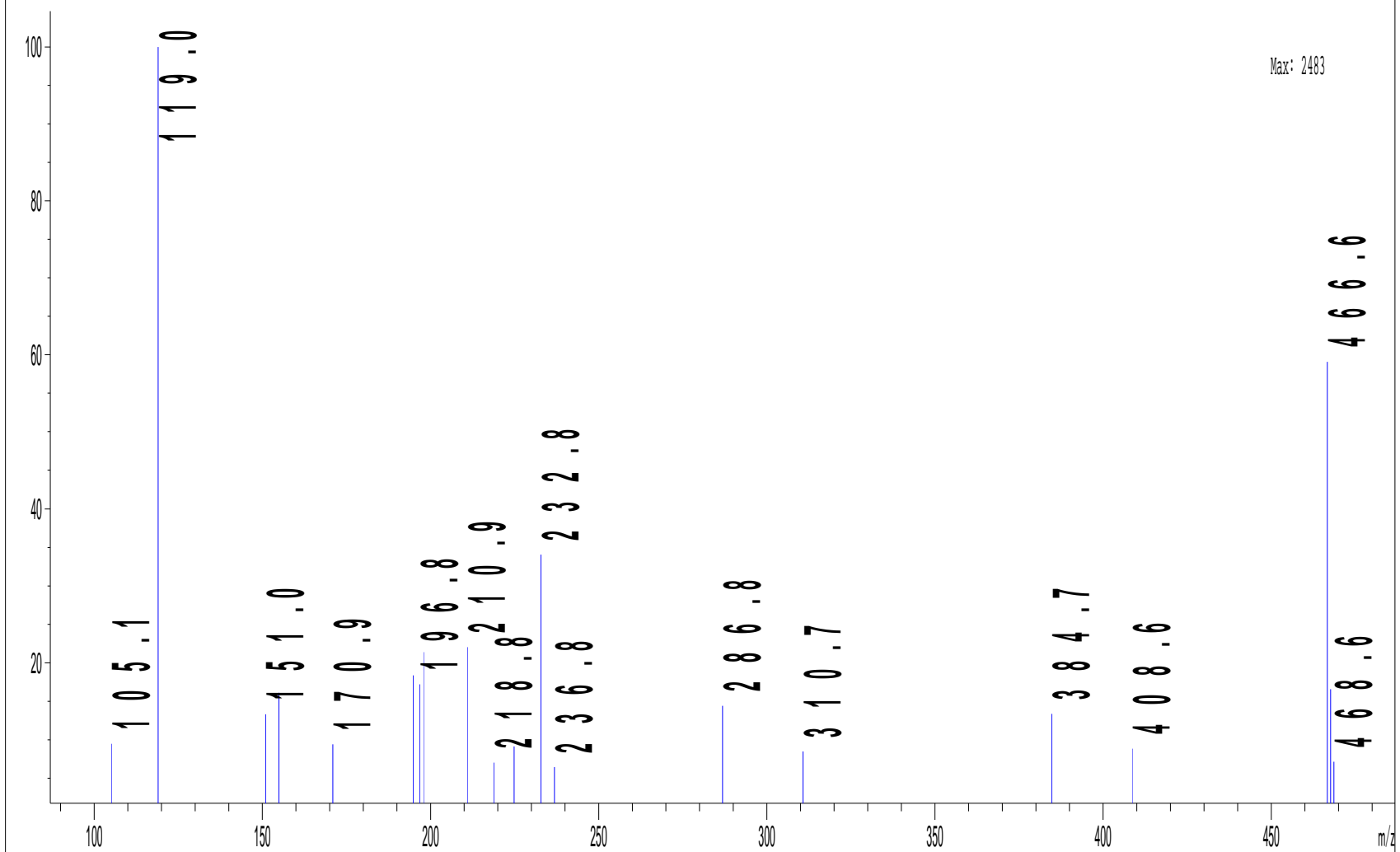
P2-E-01

MSD1 TIC, MS File (D:\DATA\TARR\20150821A\_TAR\_STEWART 2015-08-21 08-18-07\TAR1000002.D) ES-API, Neg, Scan, Frag: 70



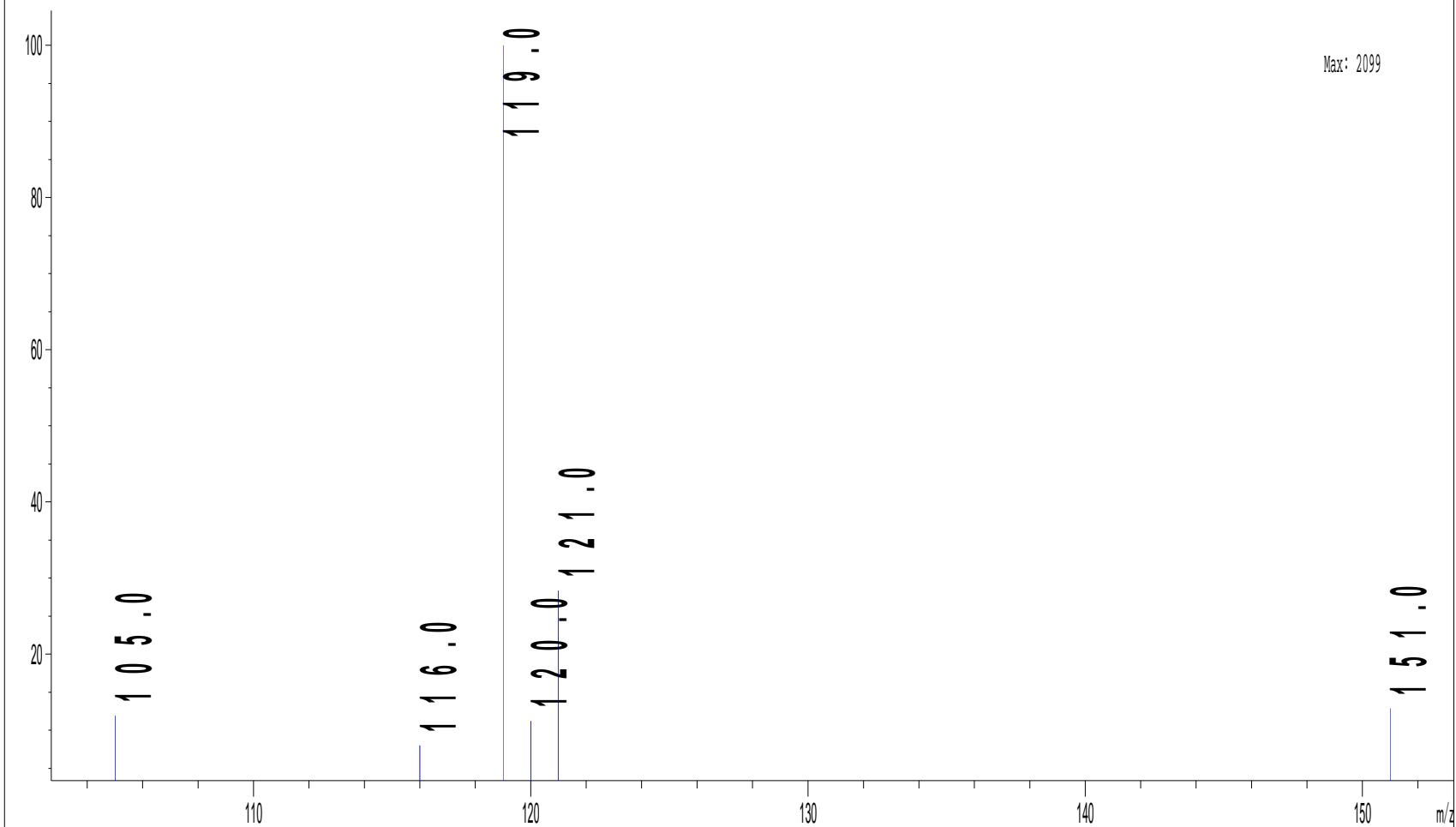


\*MSD1 SPC, time=3.100 of D:\DATA\TARR\20150821A\_TAR\_STEWART 2015-08-21 08-18-07\TAR1000002.D ES-API, Neg, Scan, Frag

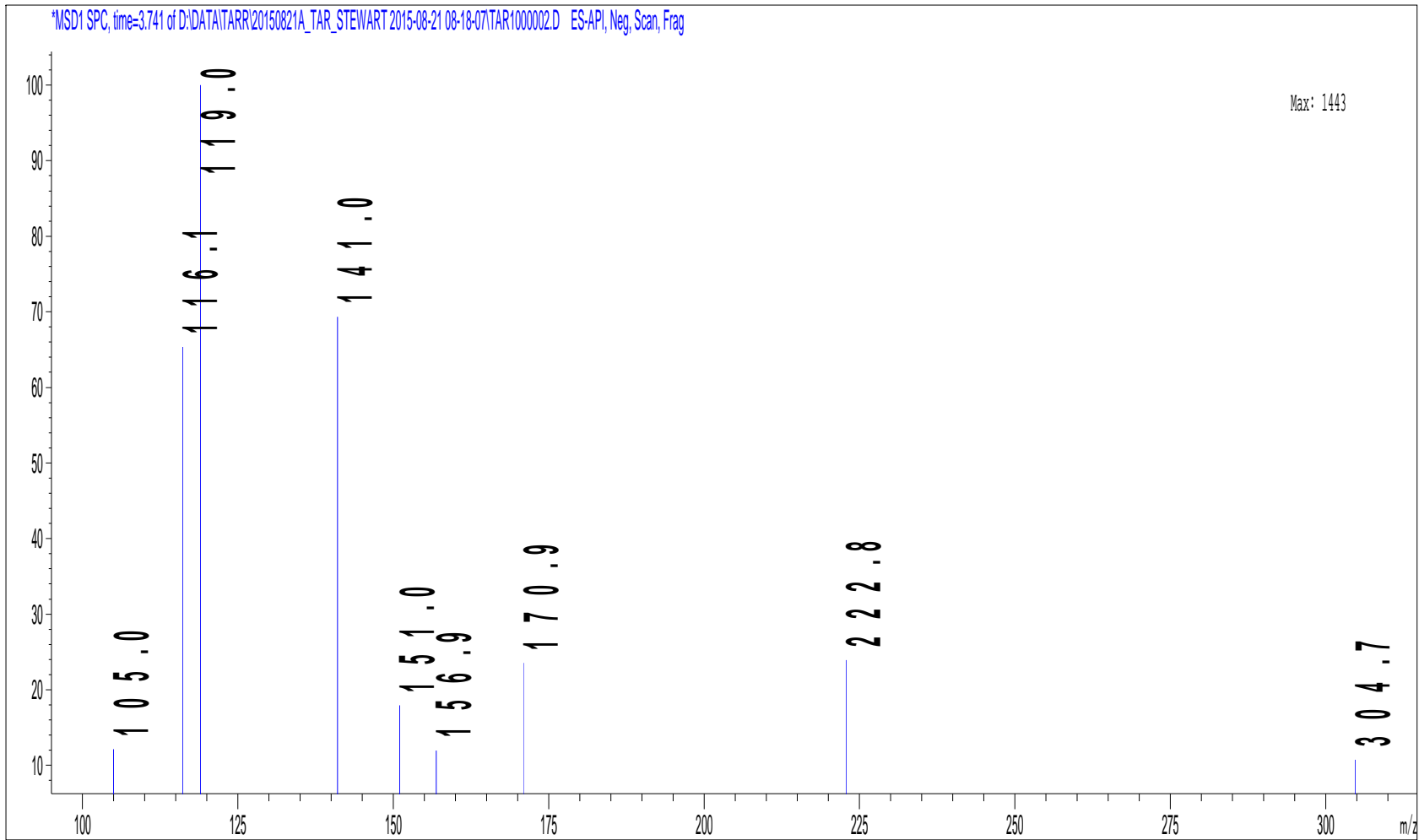


Max: 2483

\*MSD1 SPC, time=3.454 of D:\DATA\TARR\20150821A\_TAR\_STEWART 2015-08-21 08-18-07\TAR1000002.D ES-API, Neg, Scan, Frag







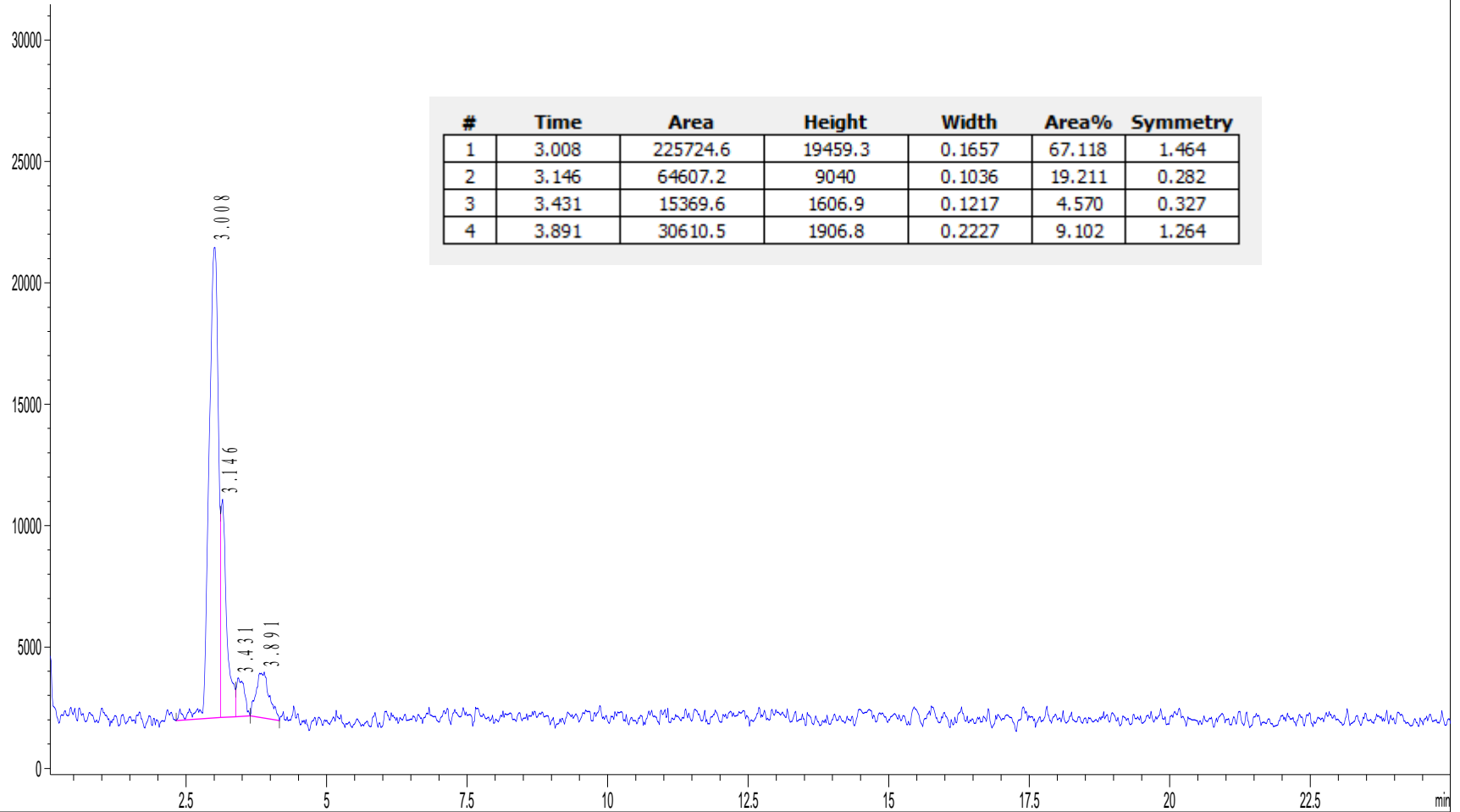
1-Jun-15

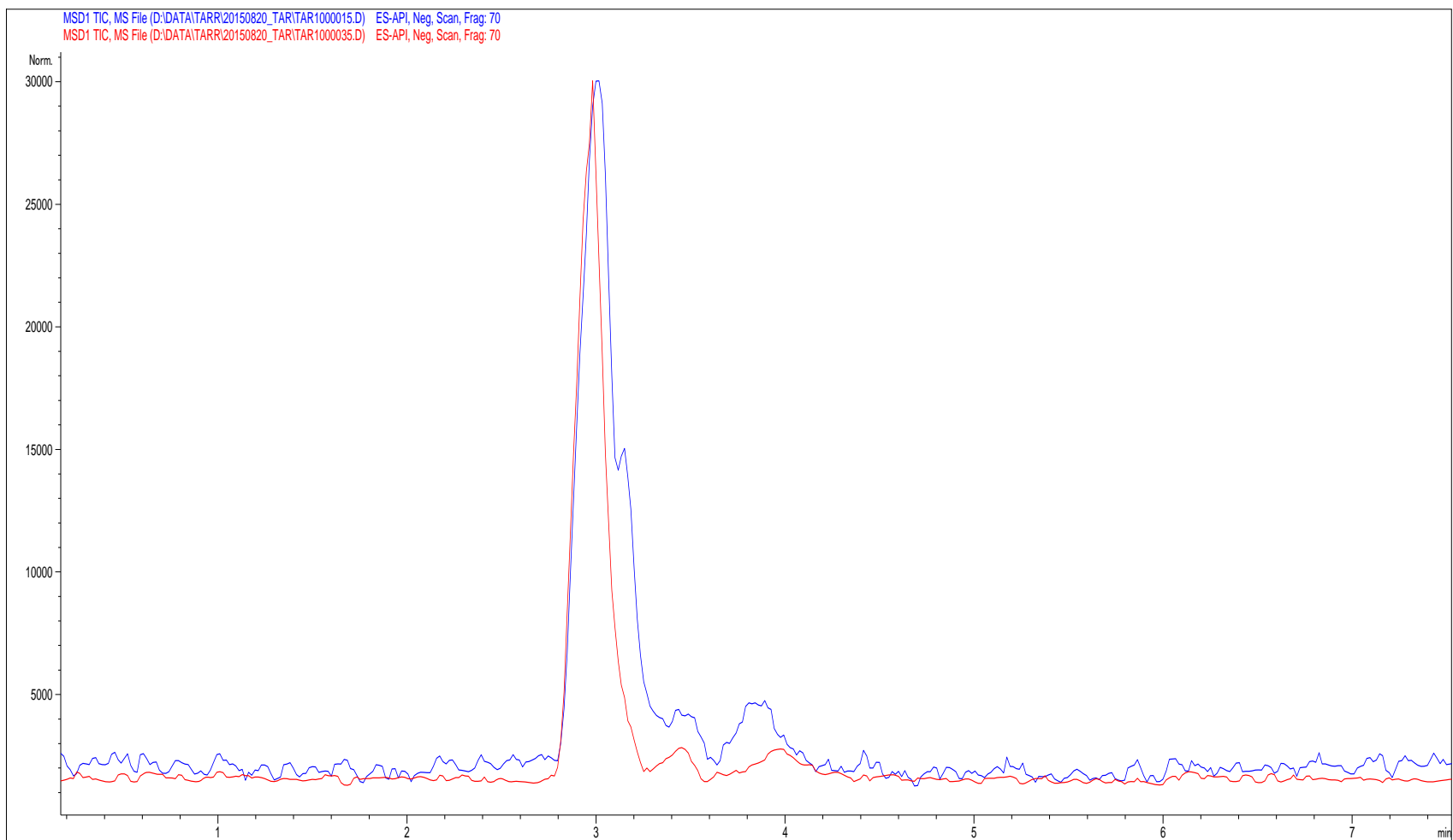
70 DC

6

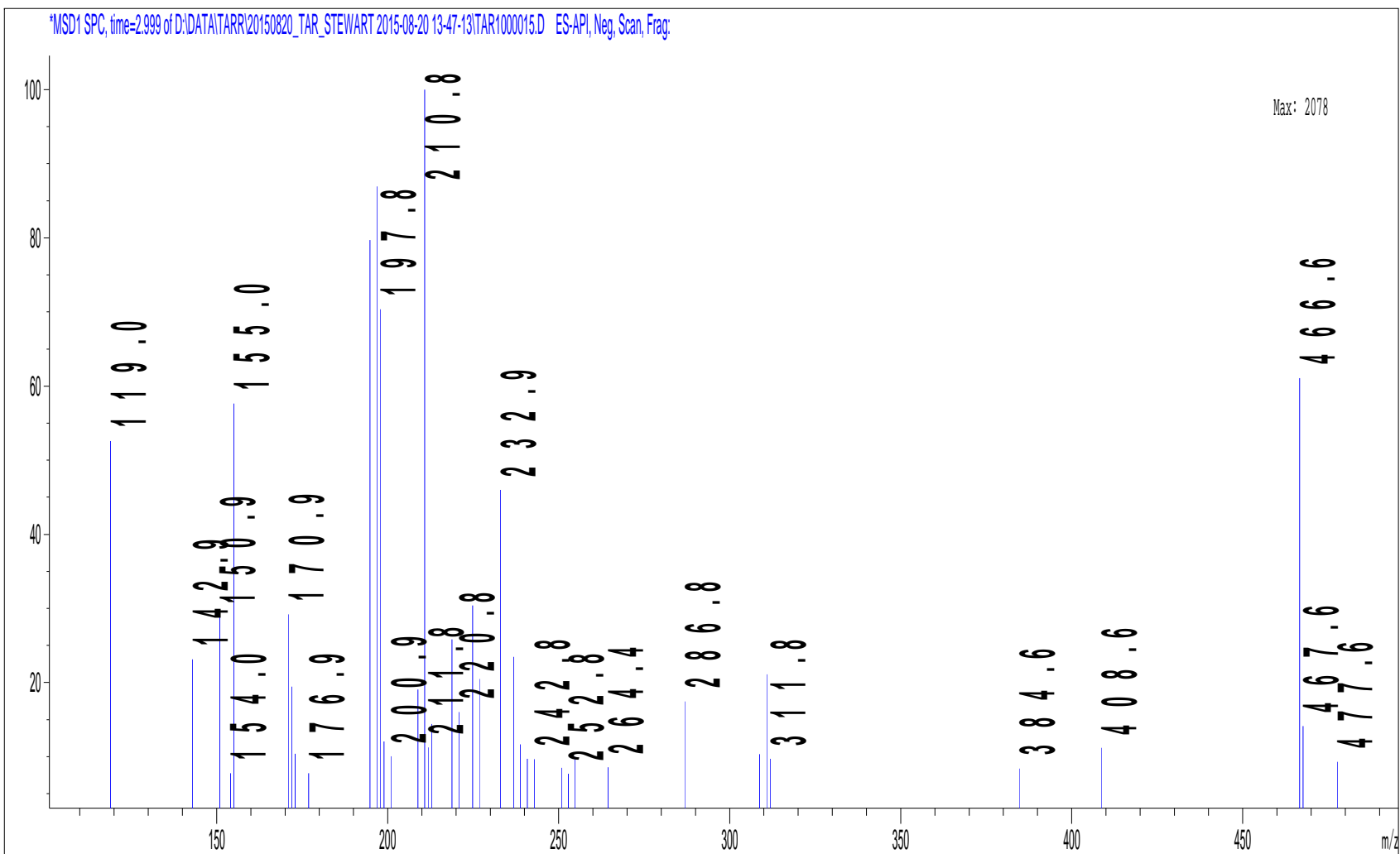
P2-B-04

MSD1 TIC, MS File (D:\DATA\TARR\20150820\_TAR\_STEWART 2015-08-20 13:47:13\TAR1000015.D) ES-API, Neg, Scan, Frag: 70



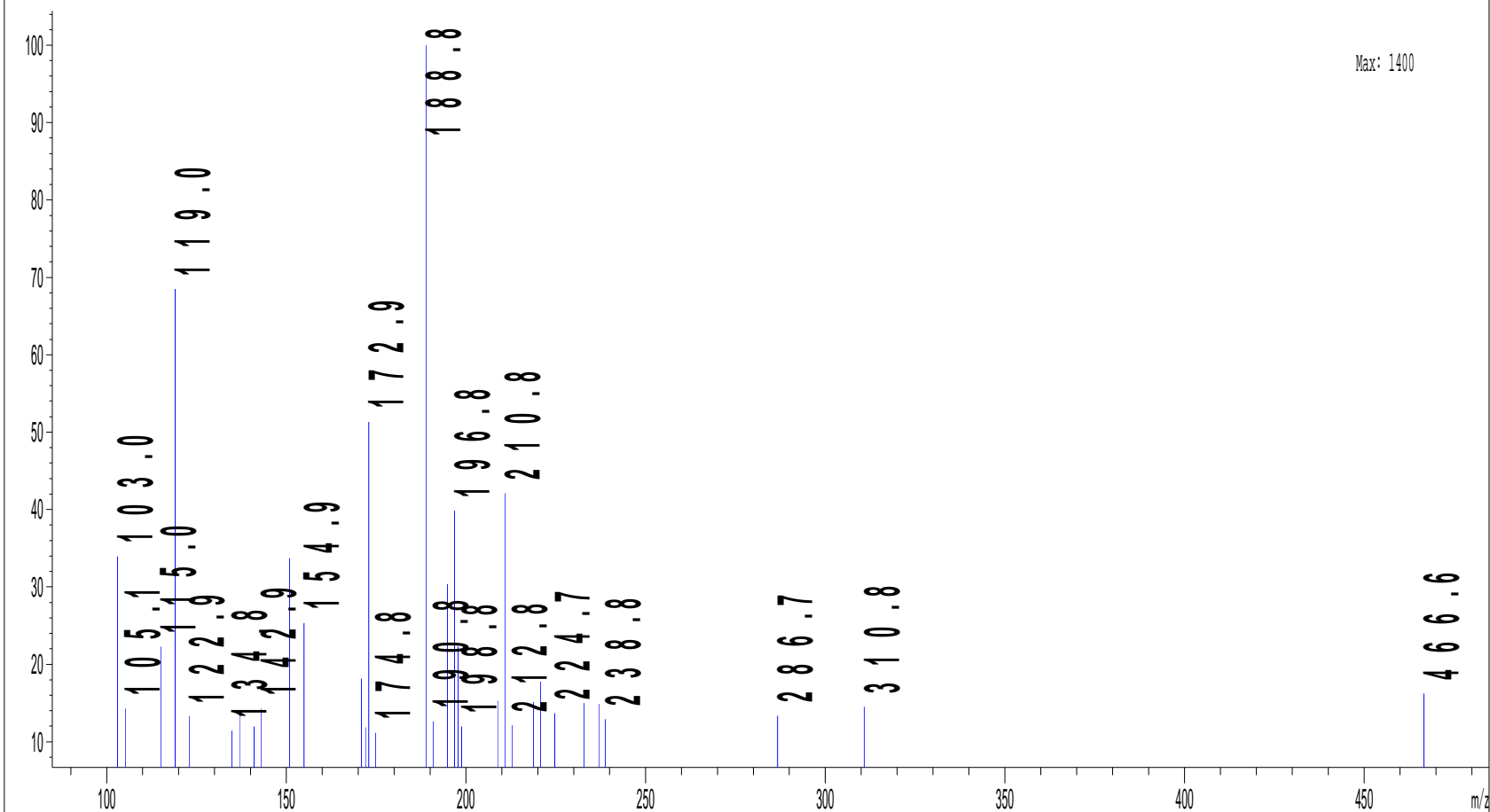


\*MSD1 SPC, time=2.999 of D:\DATA\TARR\20150820\_TAR\_STEWART 2015-08-20 13-47-13\TAR1000015.D ES-API, Neg, Scan, Frag:

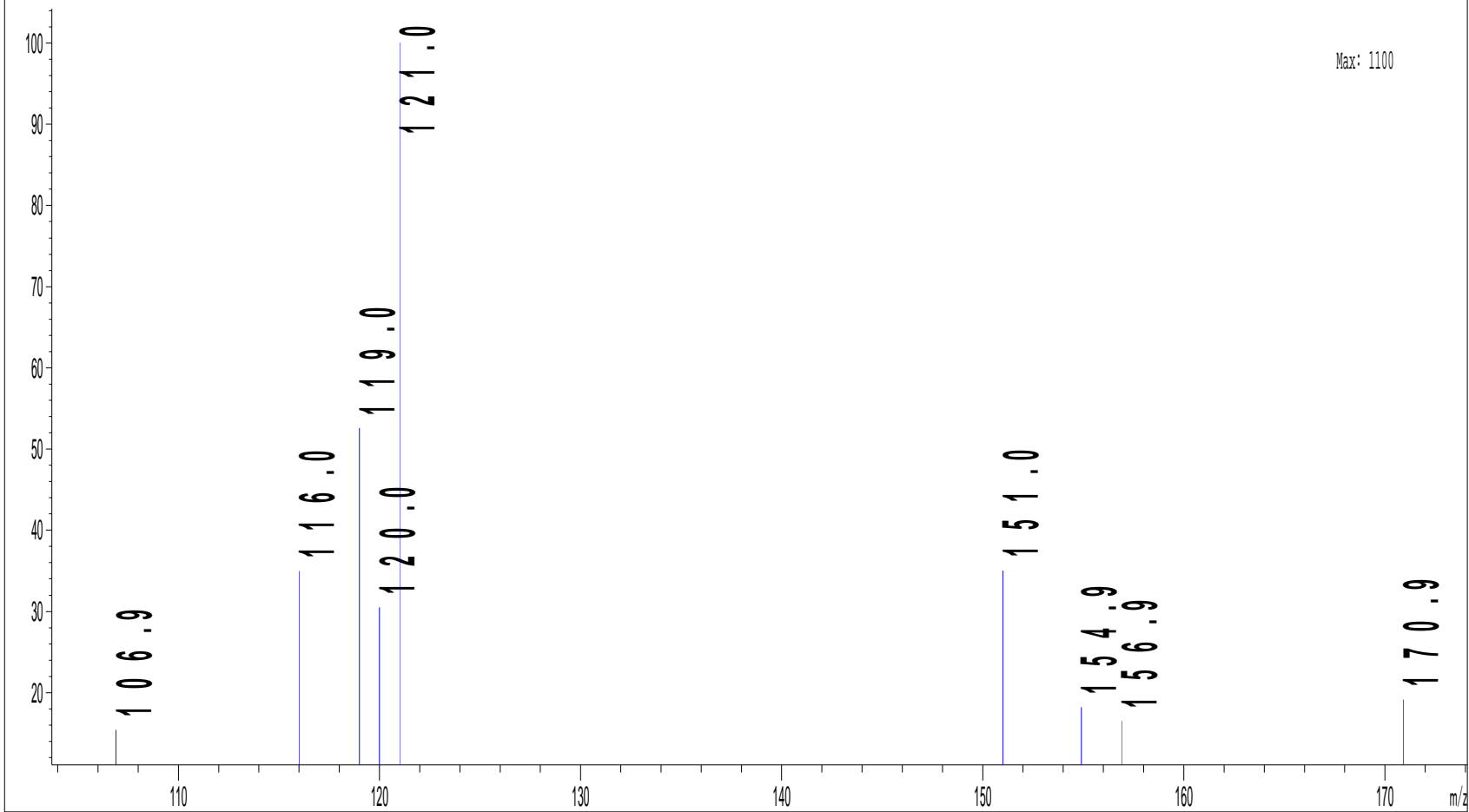


Max: 2078

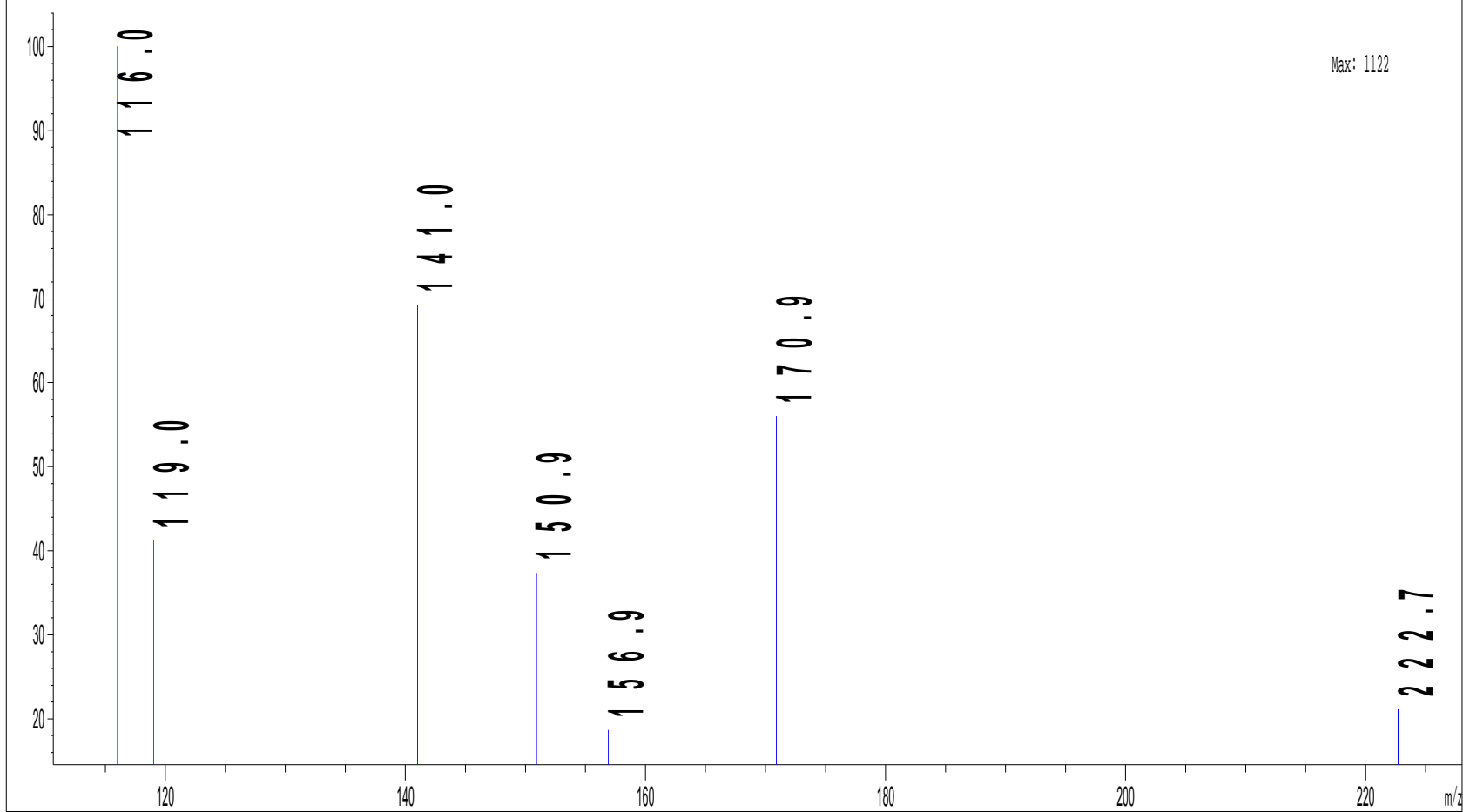
\*MSD1 SPC, time=3.134 of D:\DATA\TARRI\20150820\_TAR\_STEWART 2015-08-20 13:47-13\TAR1000015.D ES-API, Neg, Scan, Frag:



\*MSD1 SPC, time=3.471 of D:\DATA\TARR\20150820\_TAR\_STEWART 2015-08-20 13:47:13\TAR1000015.D ES-API, Neg. Scan, Frag:



\*MSD1 SPC, time=3.859 of D:\DATA\TARR\20150820\_TAR\_STEWART 2015-08-20 13:47:13\TAR1000015.D ES-API, Neg, Scan, Frag:

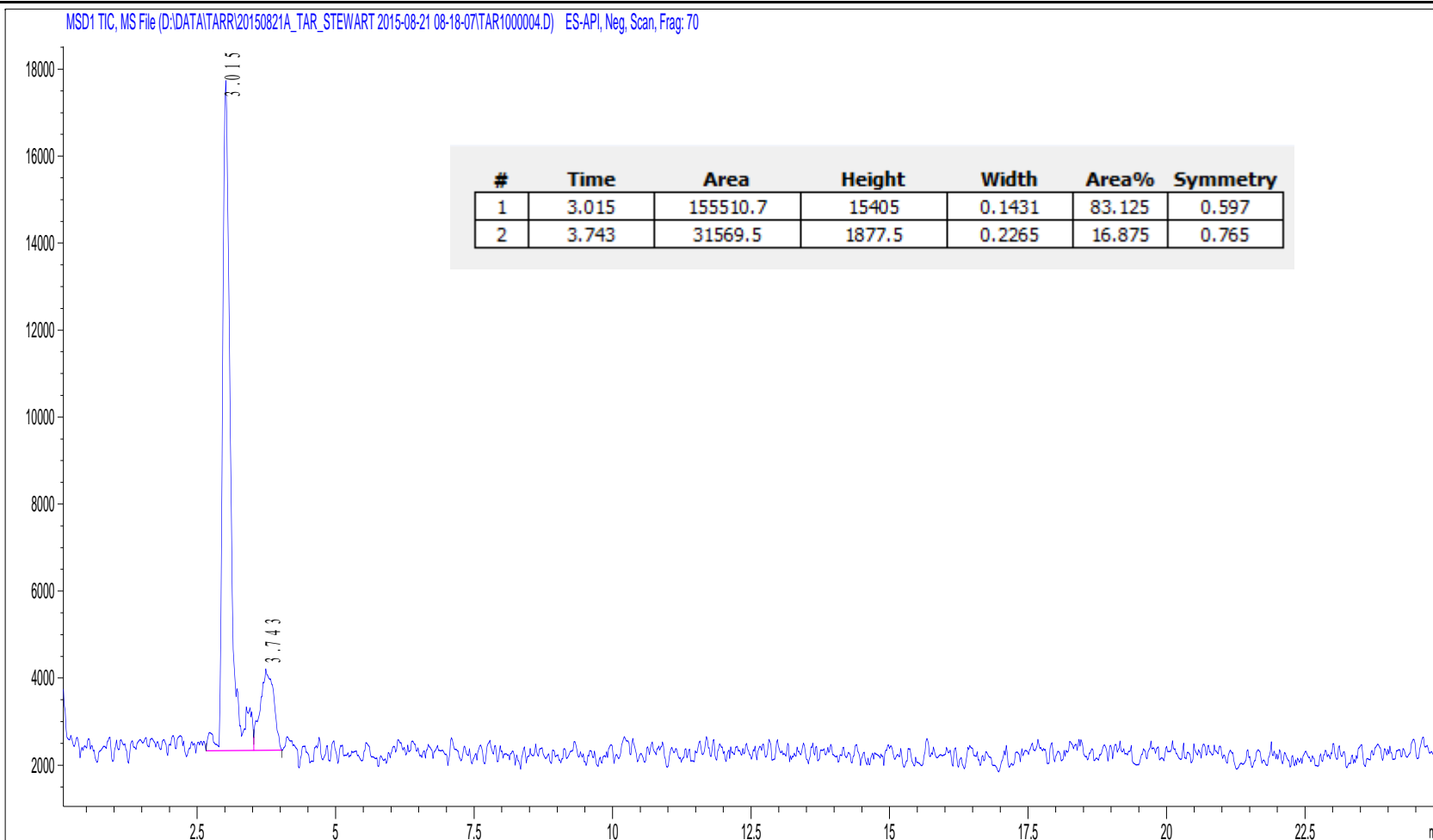


12-Aug-15

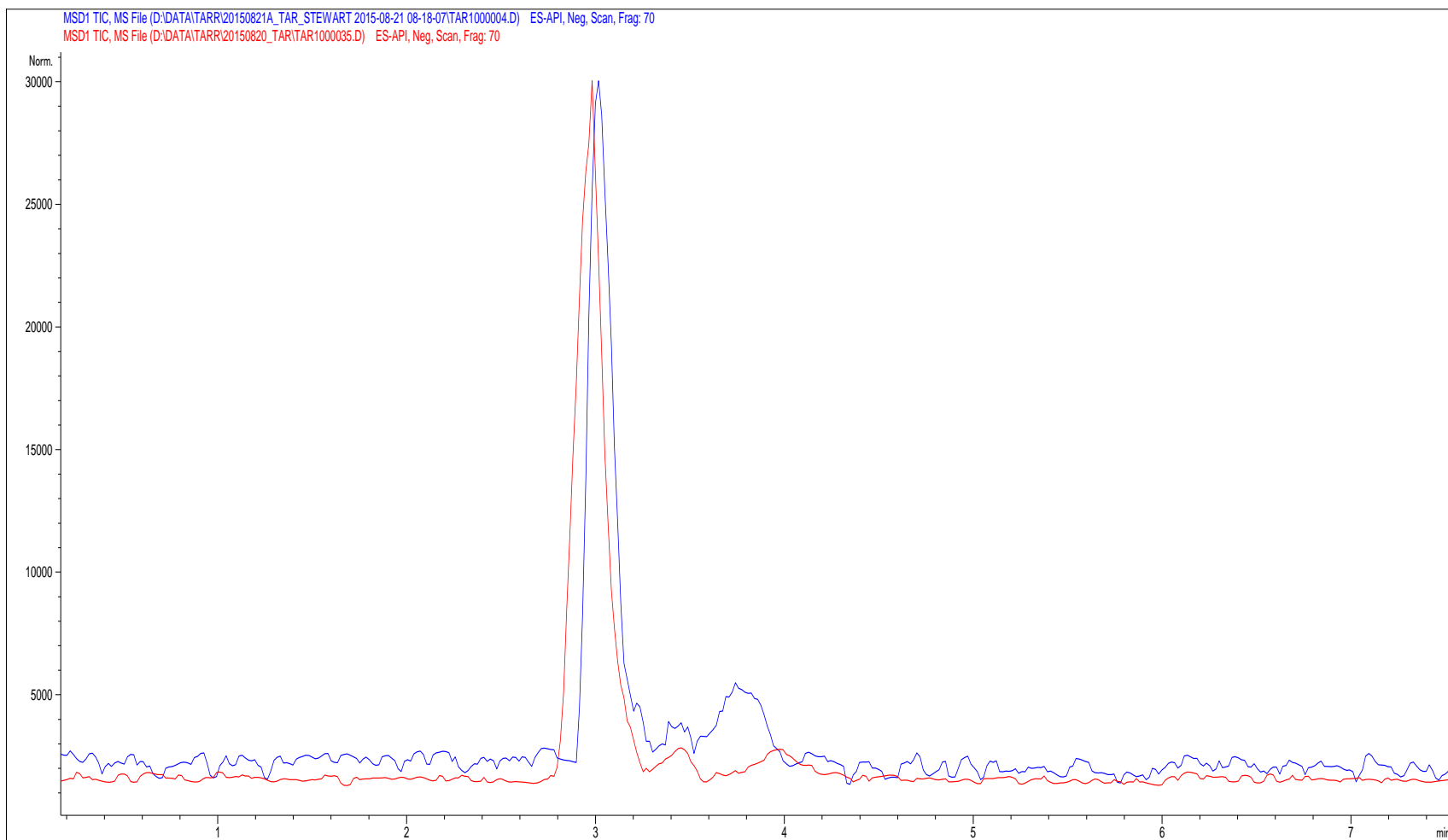
70 DC repeat

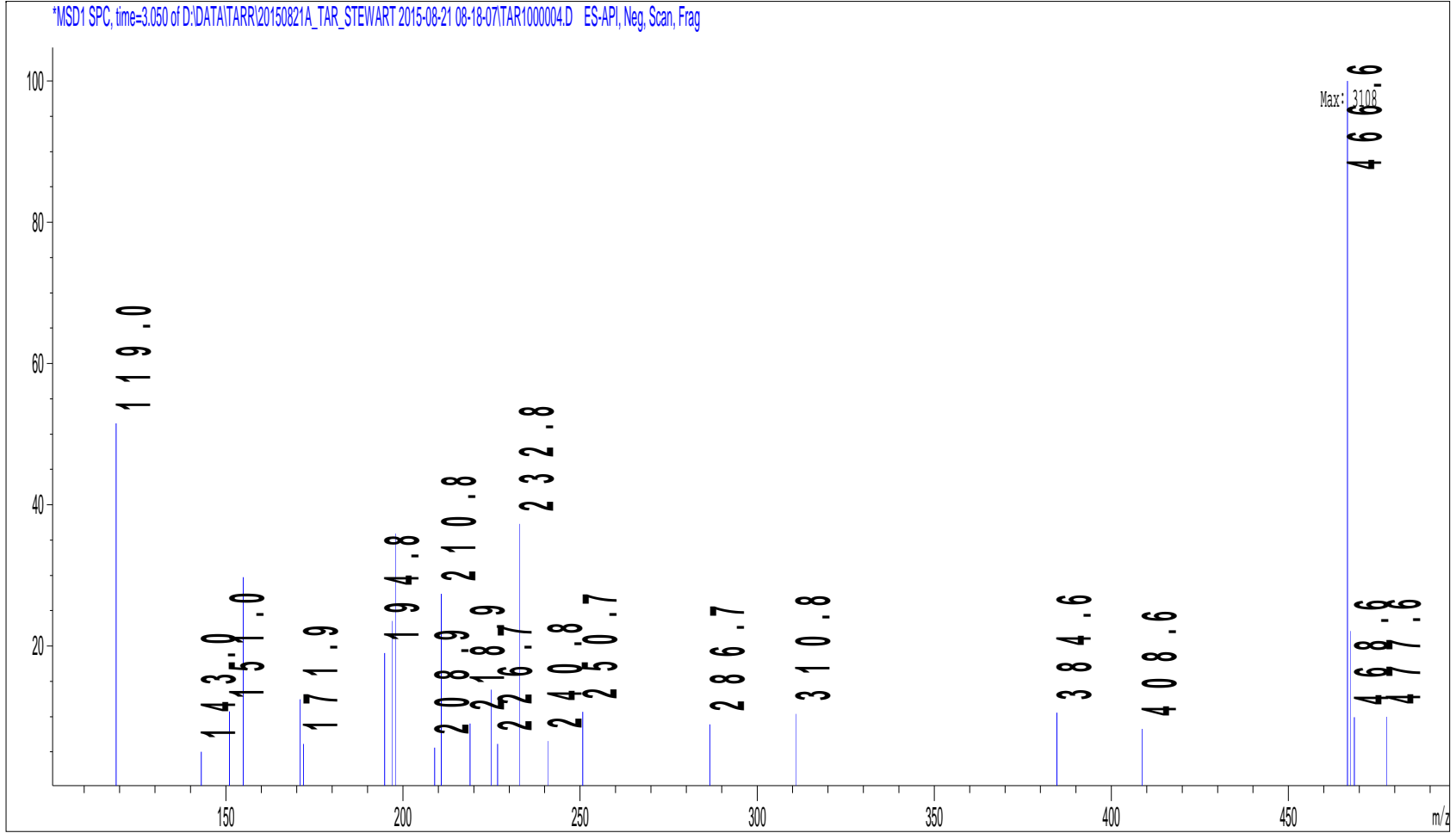
6

P2-E-03

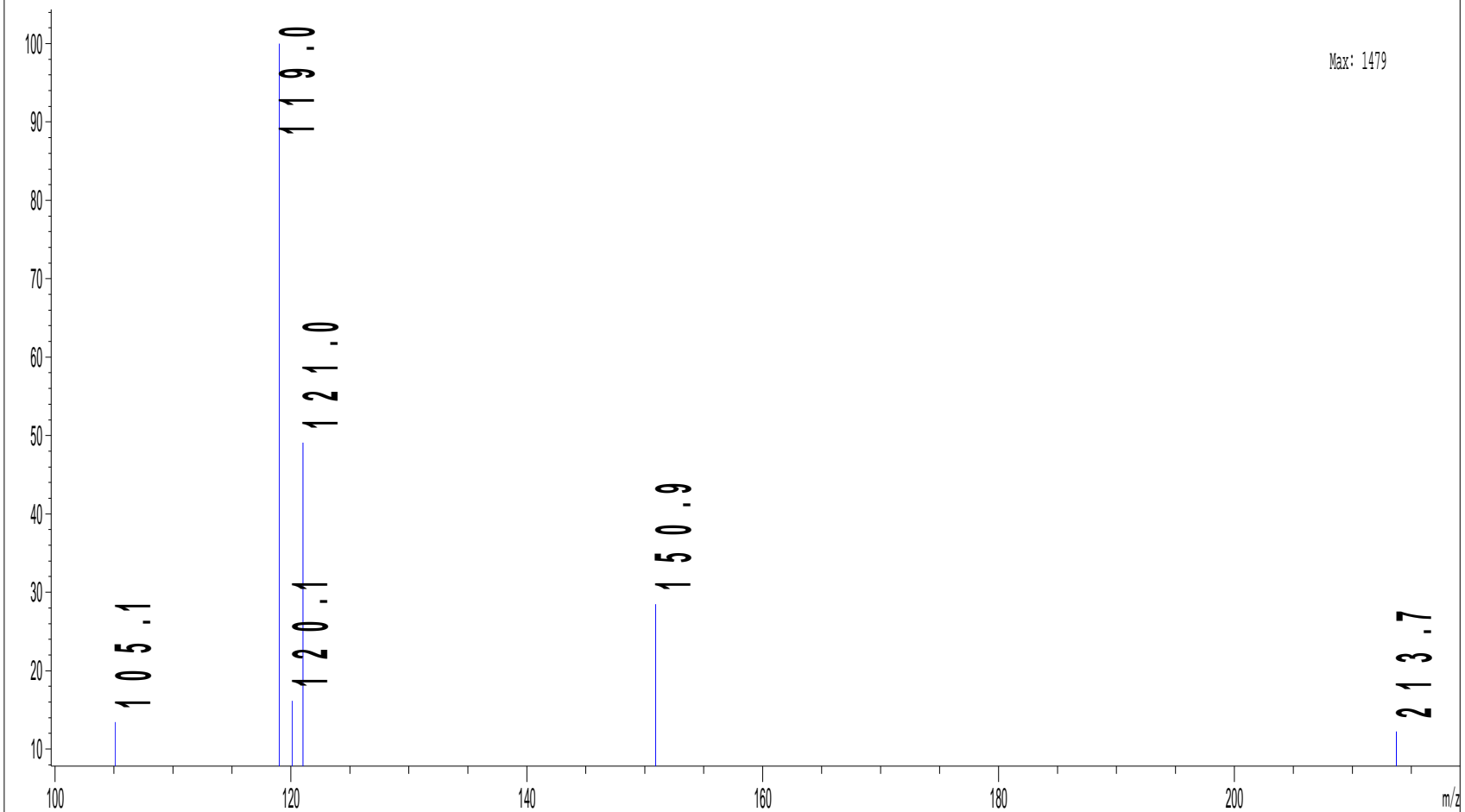


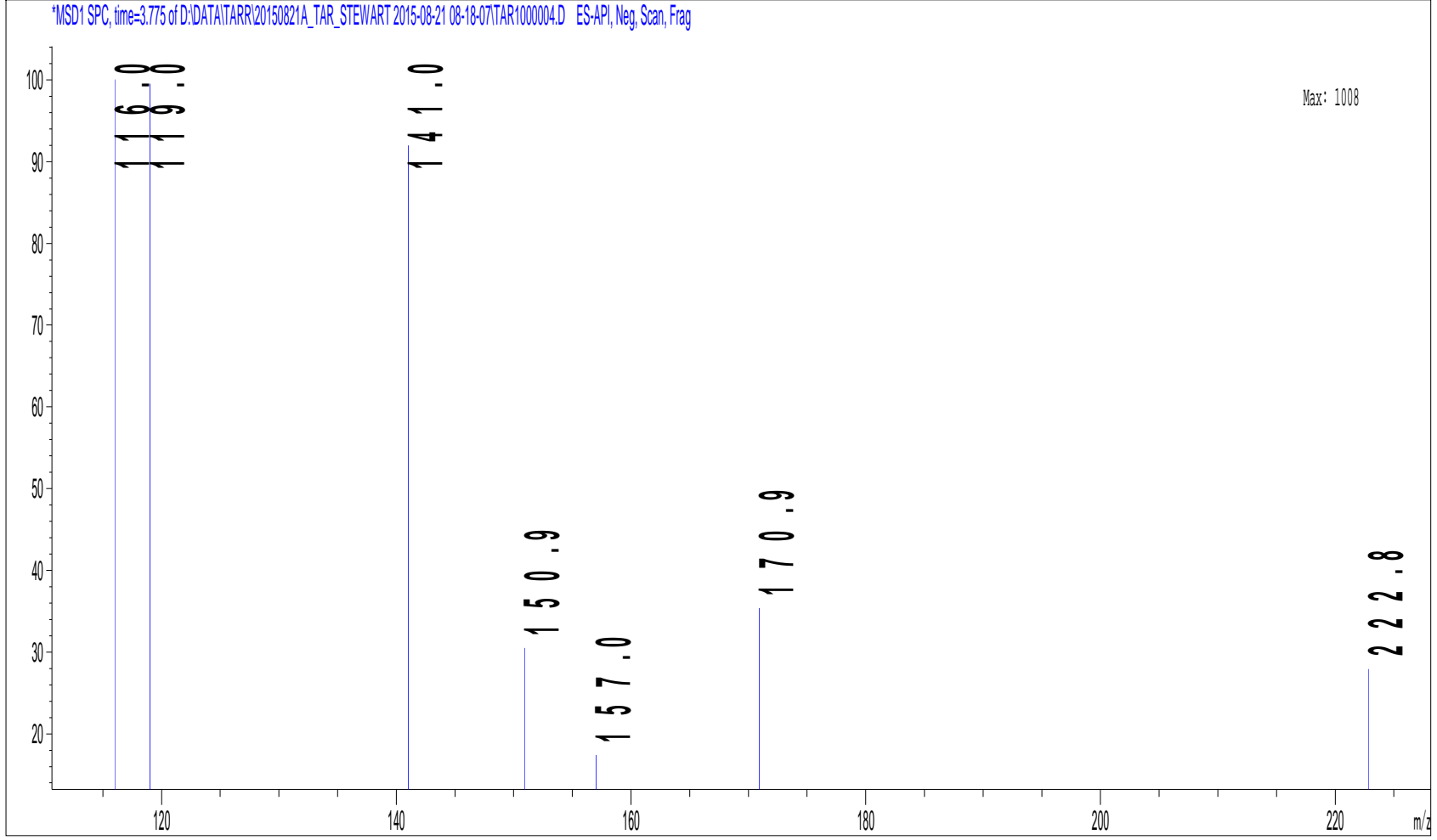






\*MSD1 SPC, time=3.438 of D:\DATA\TARR\20150821A\_TAR\_STEWART 2015-08-21 08-18-07\TAR1000004.D ES-API, Neg. Scan, Frag



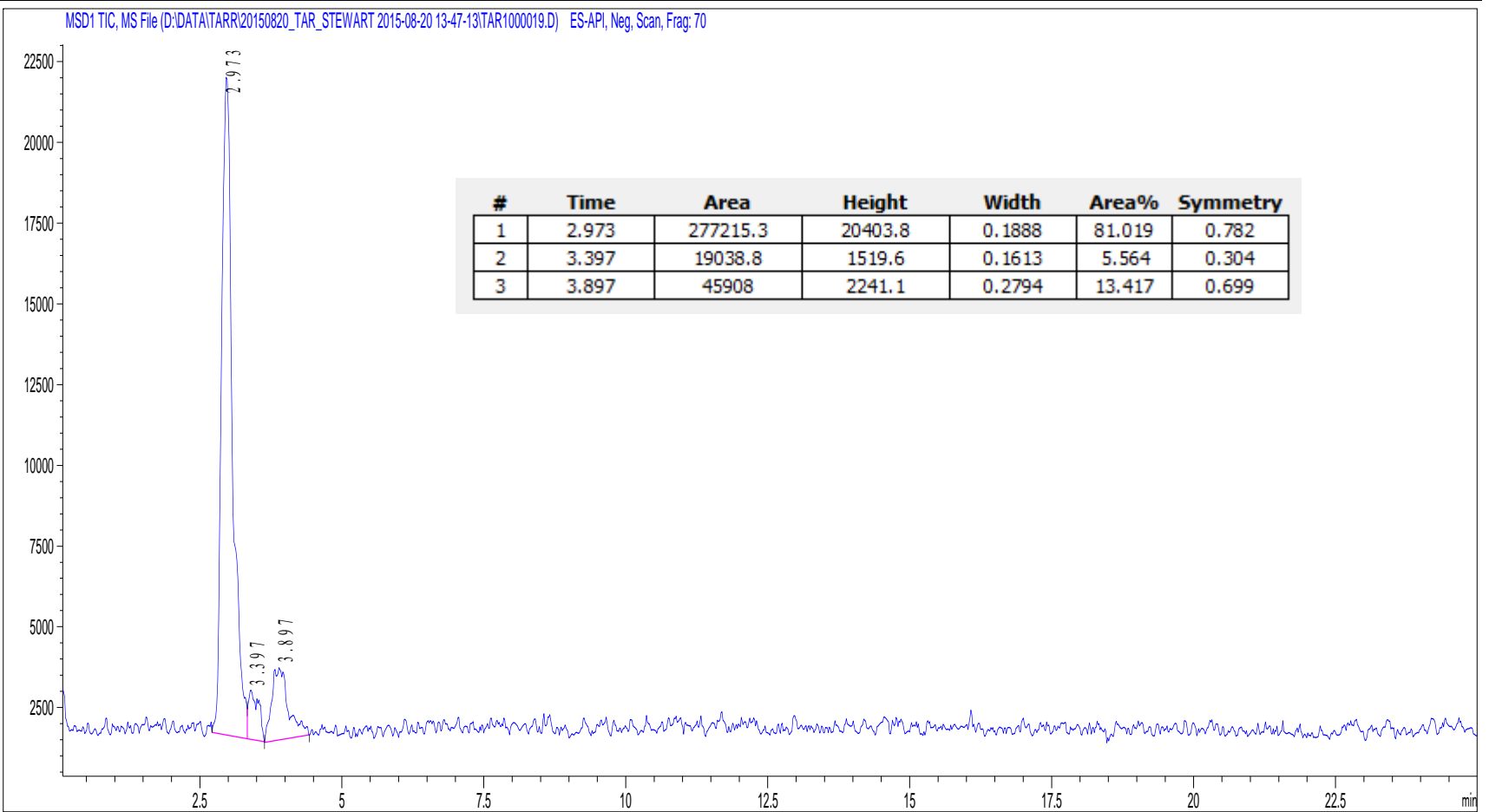


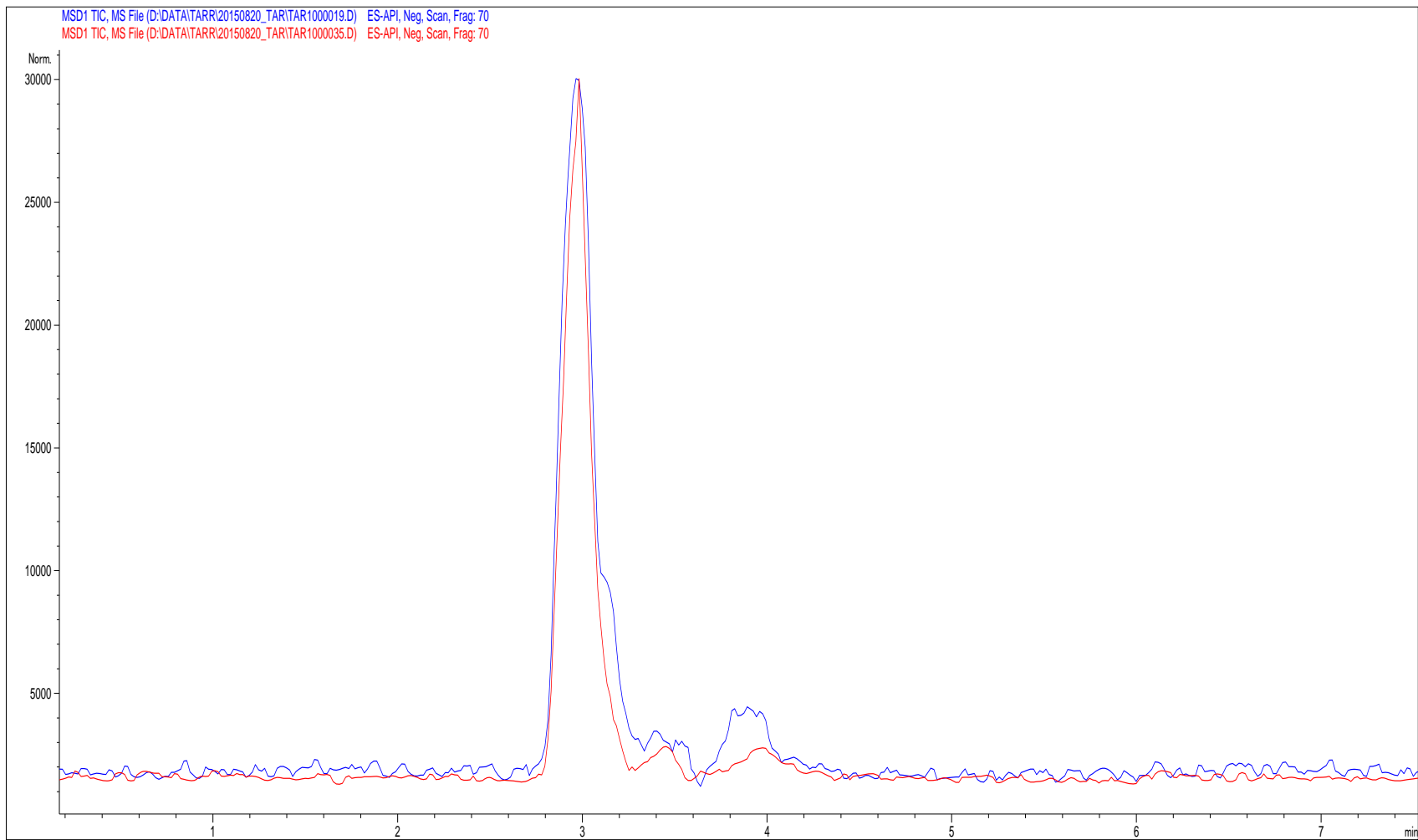
26-Jun-15

100 DC

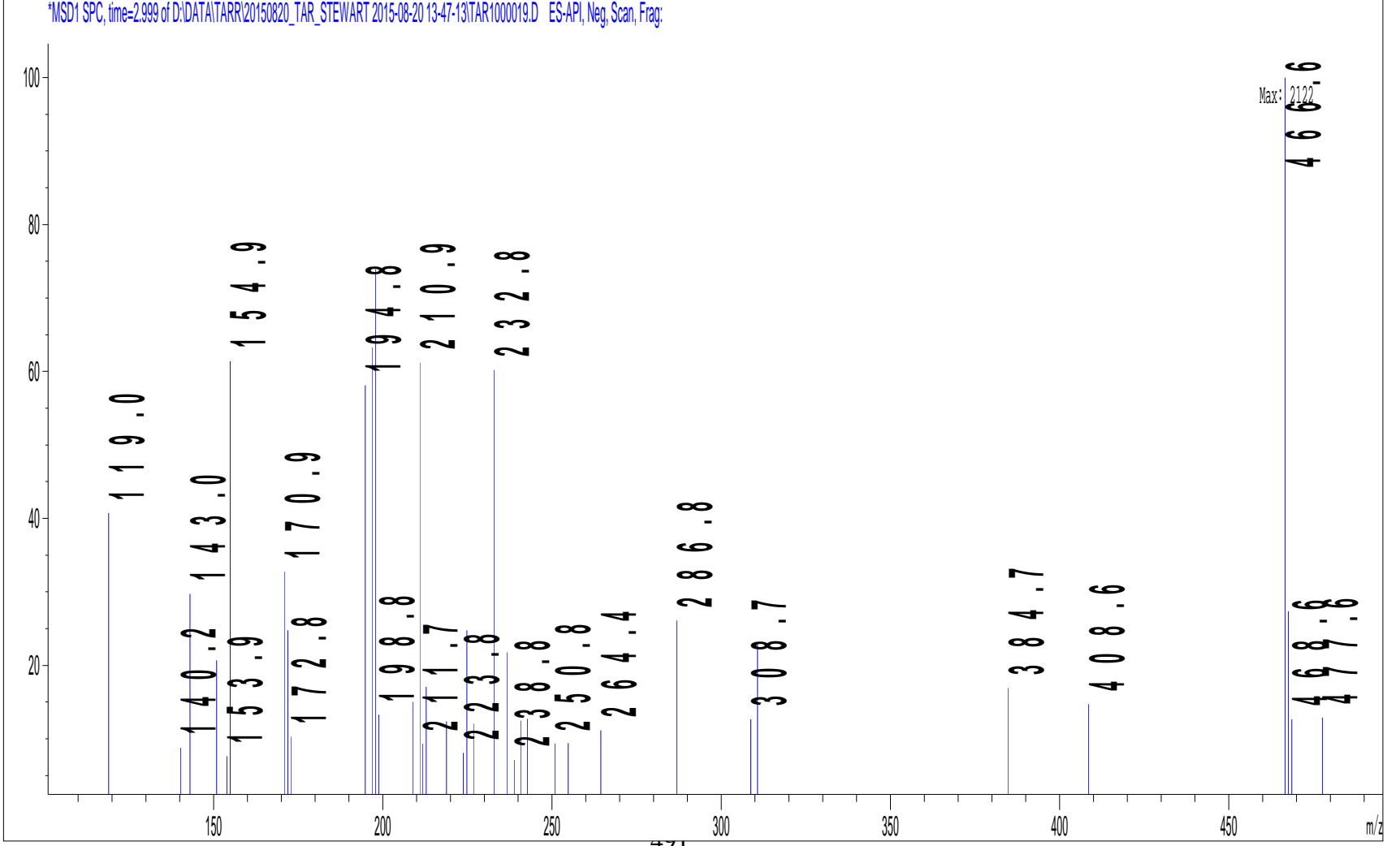
6

P2-C-01

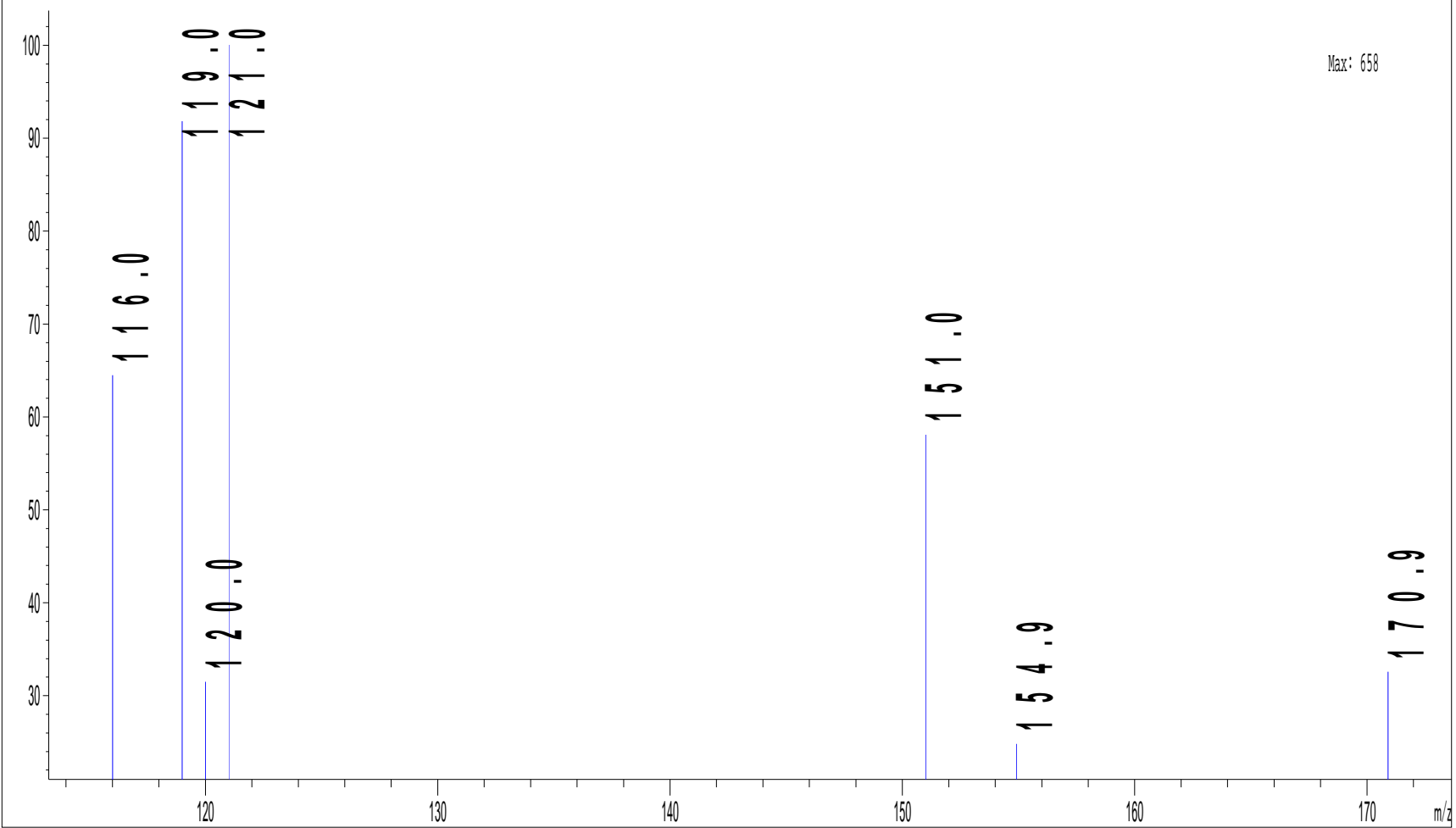




\*MSD1 SPC, time=2.999 of D:\DATA\TARR\20150820\_TAR\_STEWART 2015-08-20 13:47:13\TAR1000019.D ES-API, Neg, Scan, Frag:

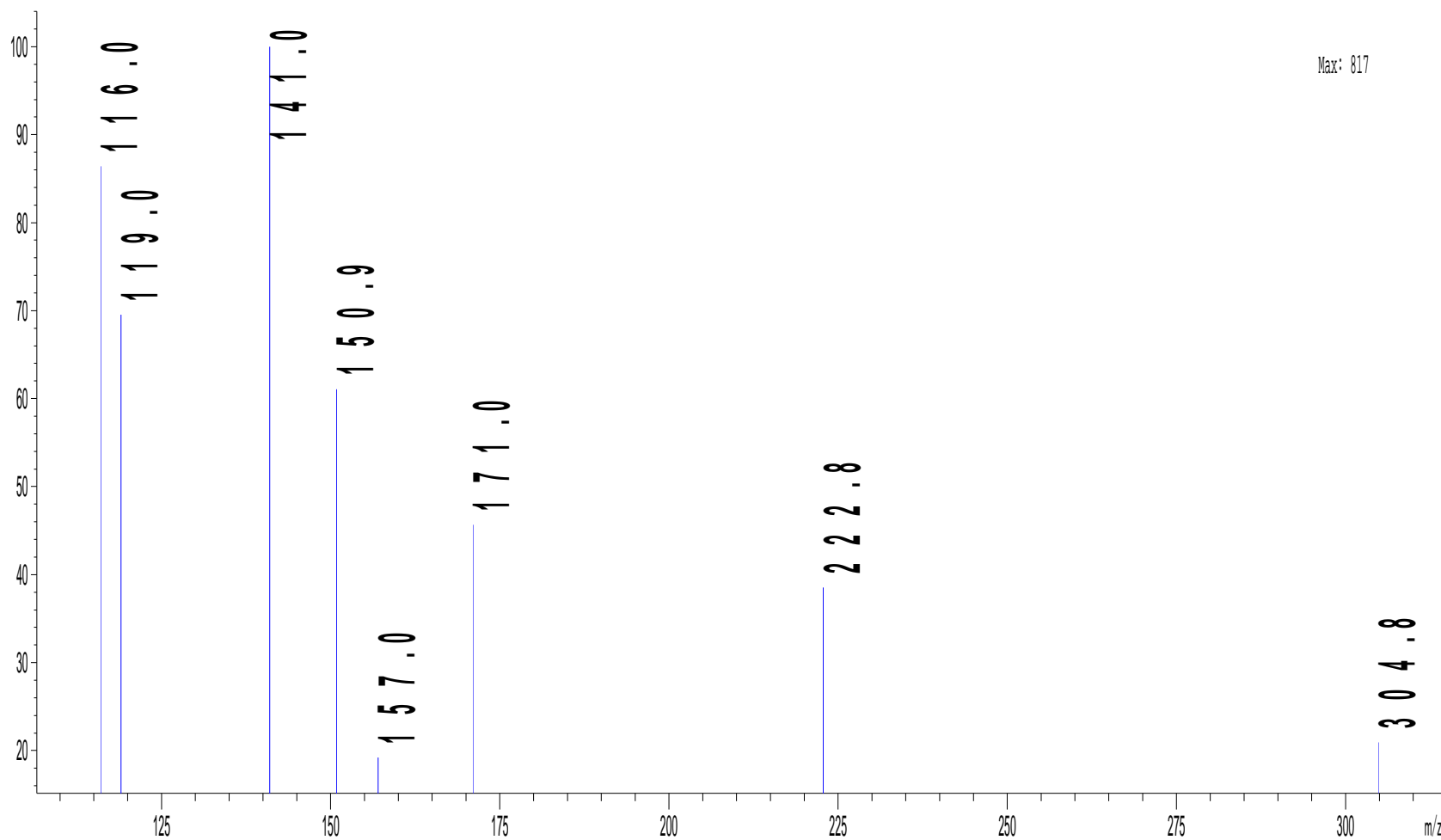


\*MSD1 SPC, time=3.471 of D:\DATA\TARR\20150820\_TAR\_STEWART 2015-08-20 13:47:13\TAR1000019.D ES-API, Neg. Scan, Frag:





\*MSD1 SPC, time=3.926 of D:\DATA\TARR\20150820\_TAR\_STEWART 2015-08-20 13:47:13\TAR1000019.D ES-API, Neg, Scan, Frag:



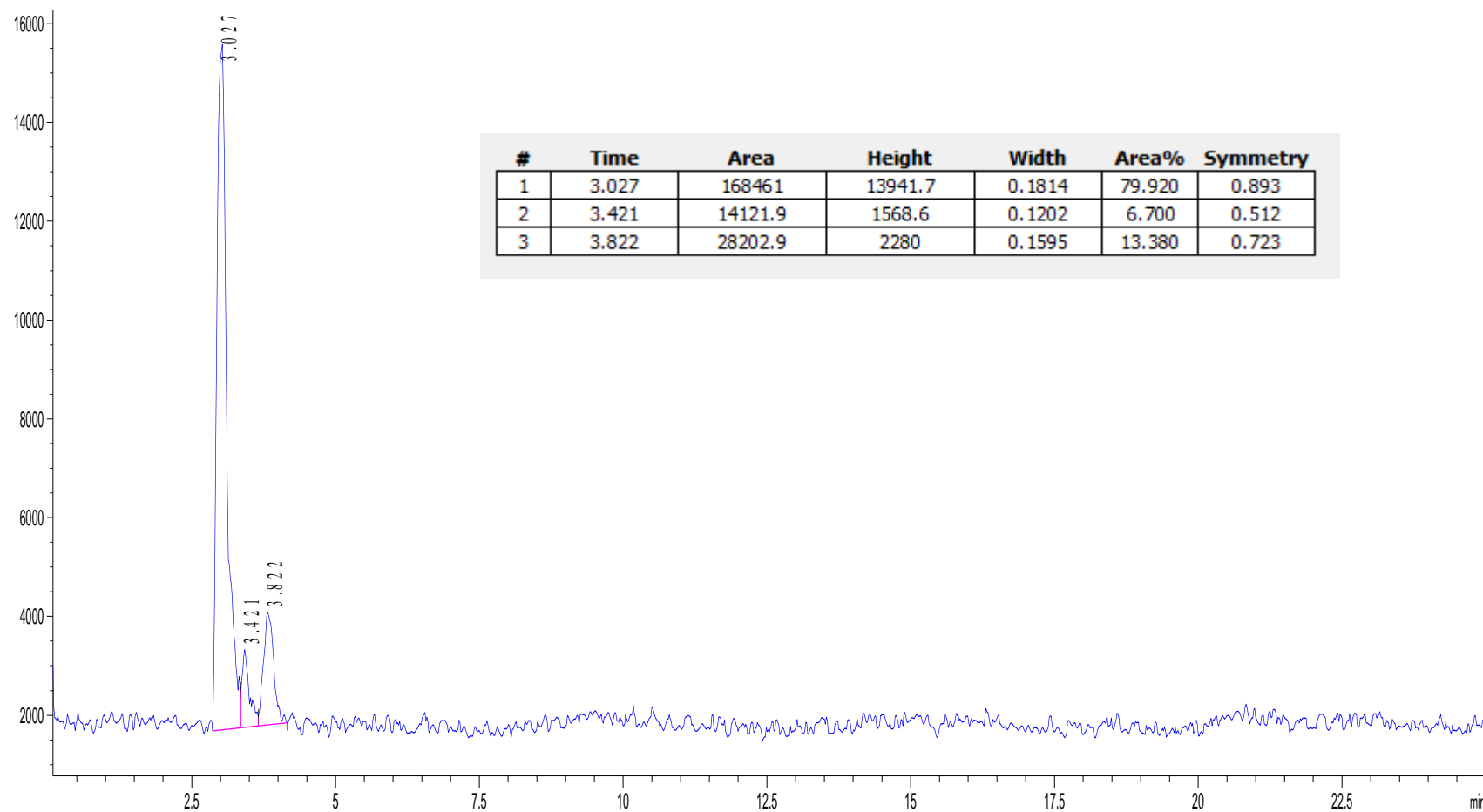
24-Jun-15

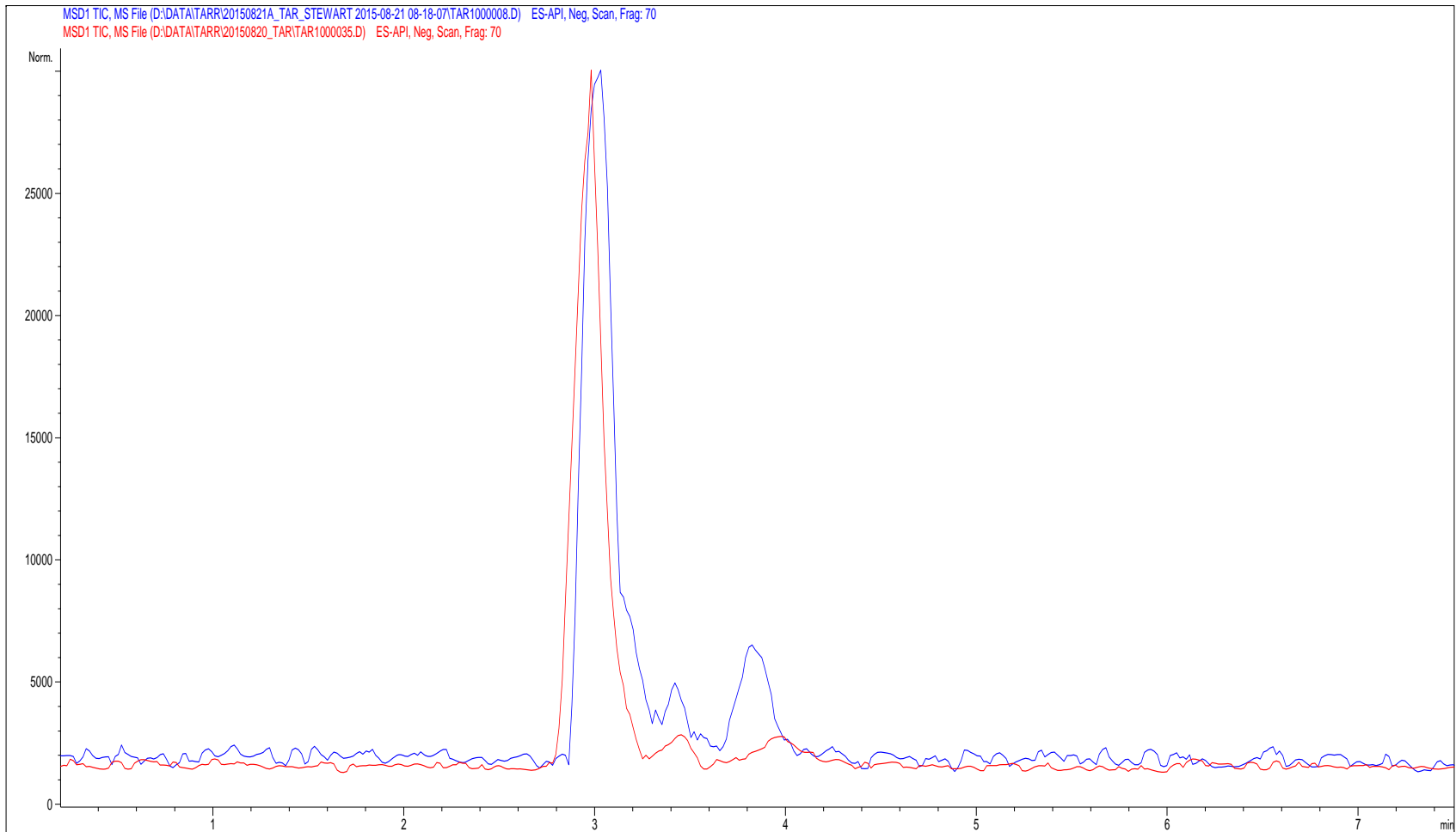
100 DC problem (no removal)

6

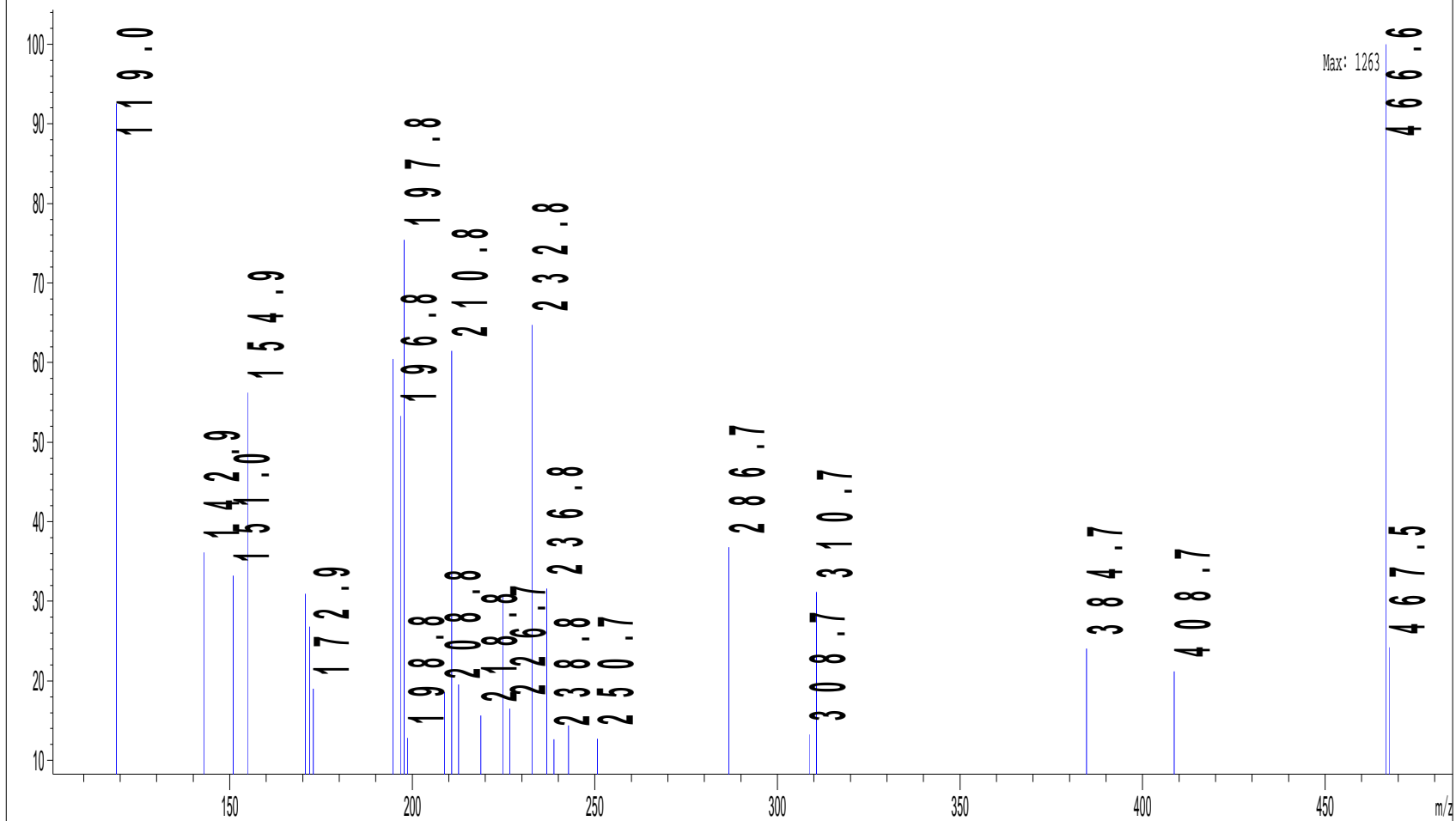
P2-E-07

MSD1 TIC, MS File (D:\DATA\TARR\20150821A\_TAR\_STEWART 2015-08-21 08-18-07\TAR1000008.D) ES-API, Neg, Scan, Frag: 70



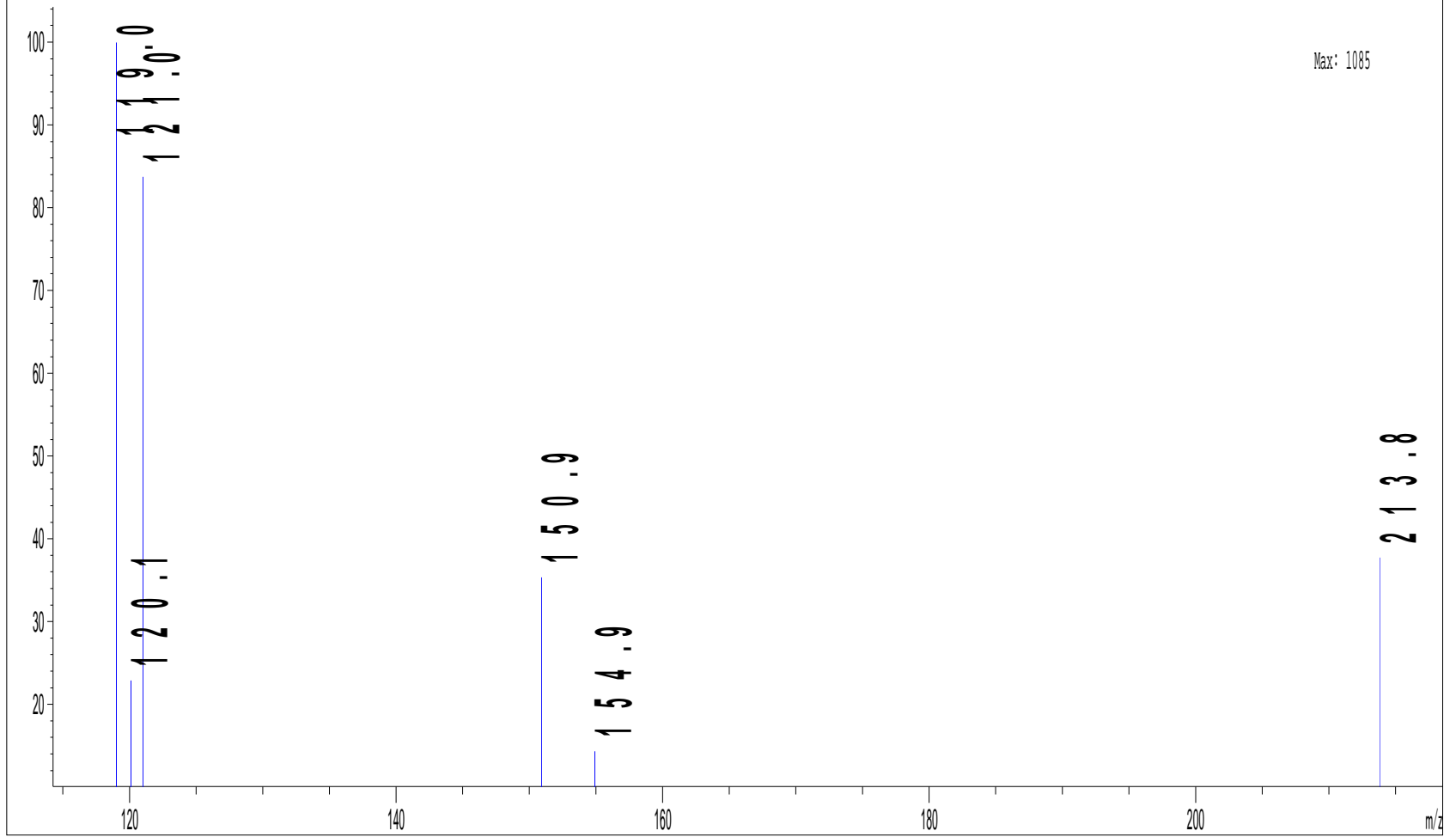


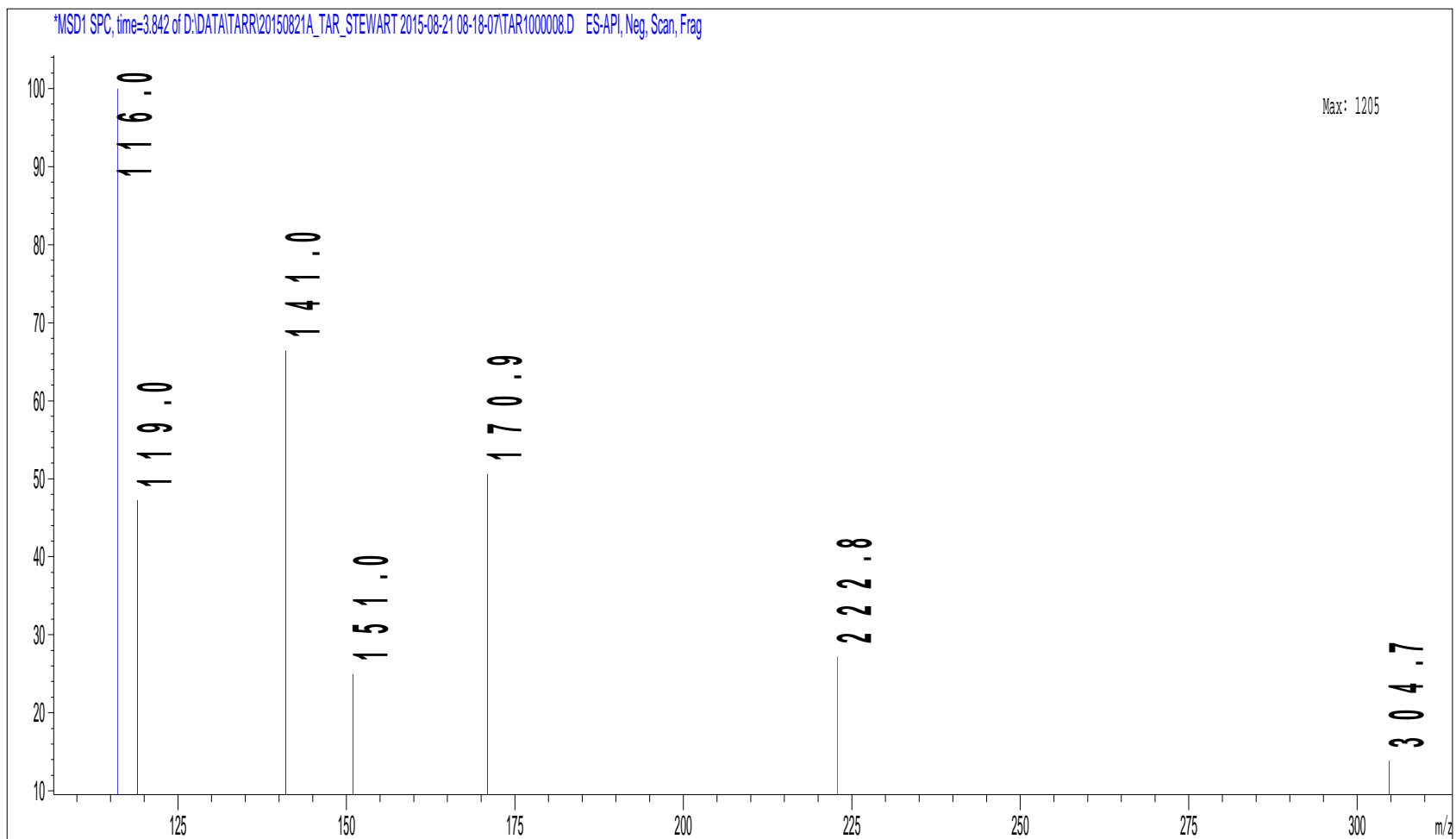
\*MSD1 SPC, time=3.067 of D:\DATA\TARRI\20150821A\_TAR\_STEWART 2015-08-21 08-18-07\TAR1000008.D ES-API, Neg, Scan, Frag



Max: 1263

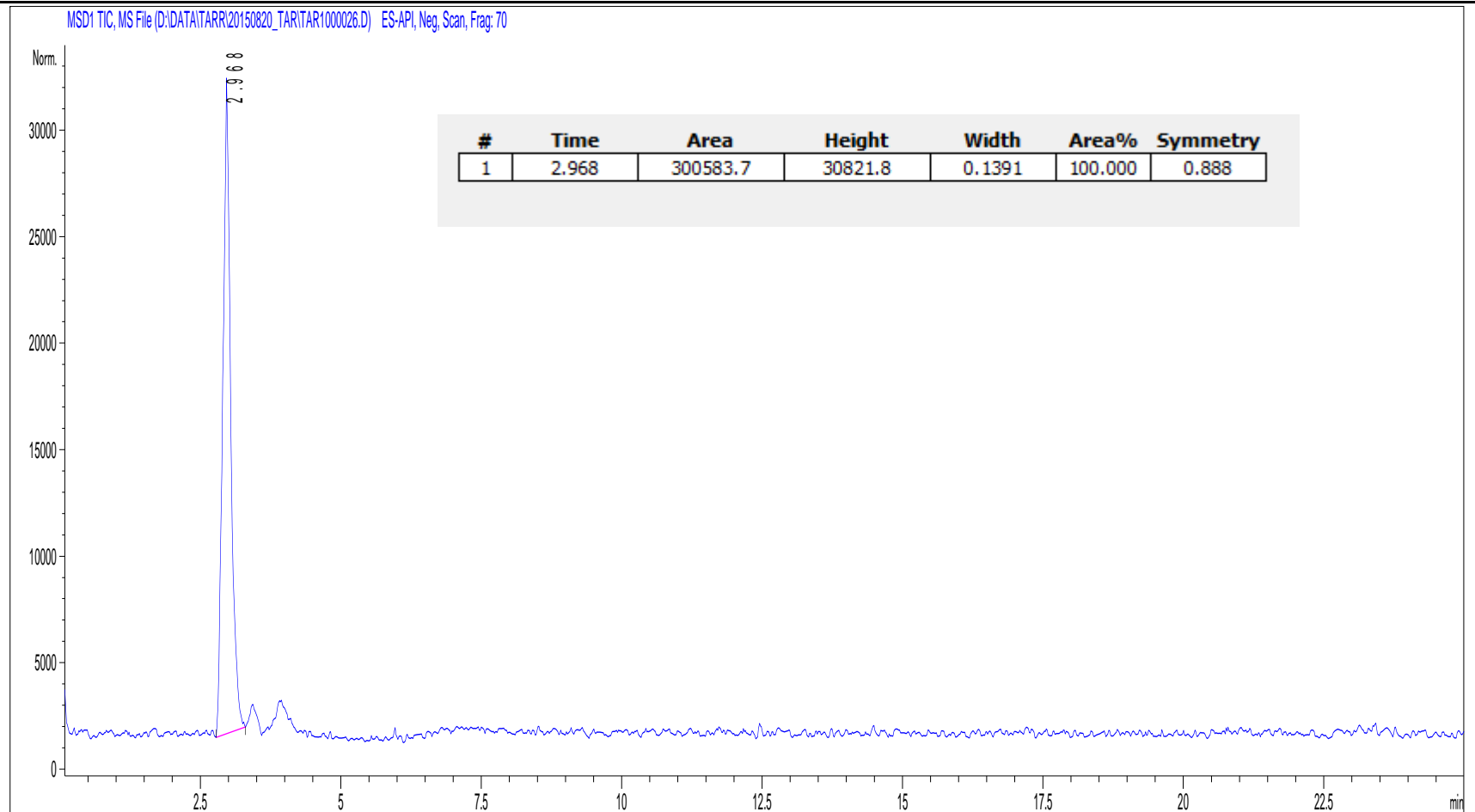
\*MSD1 SPC, time=3.438 of D:\DATA\TARR\20150821A\_TAR\_STEWART 2015-08-21 08-18-07\TAR1000008.D ES-API, Neg, Scan, Frag



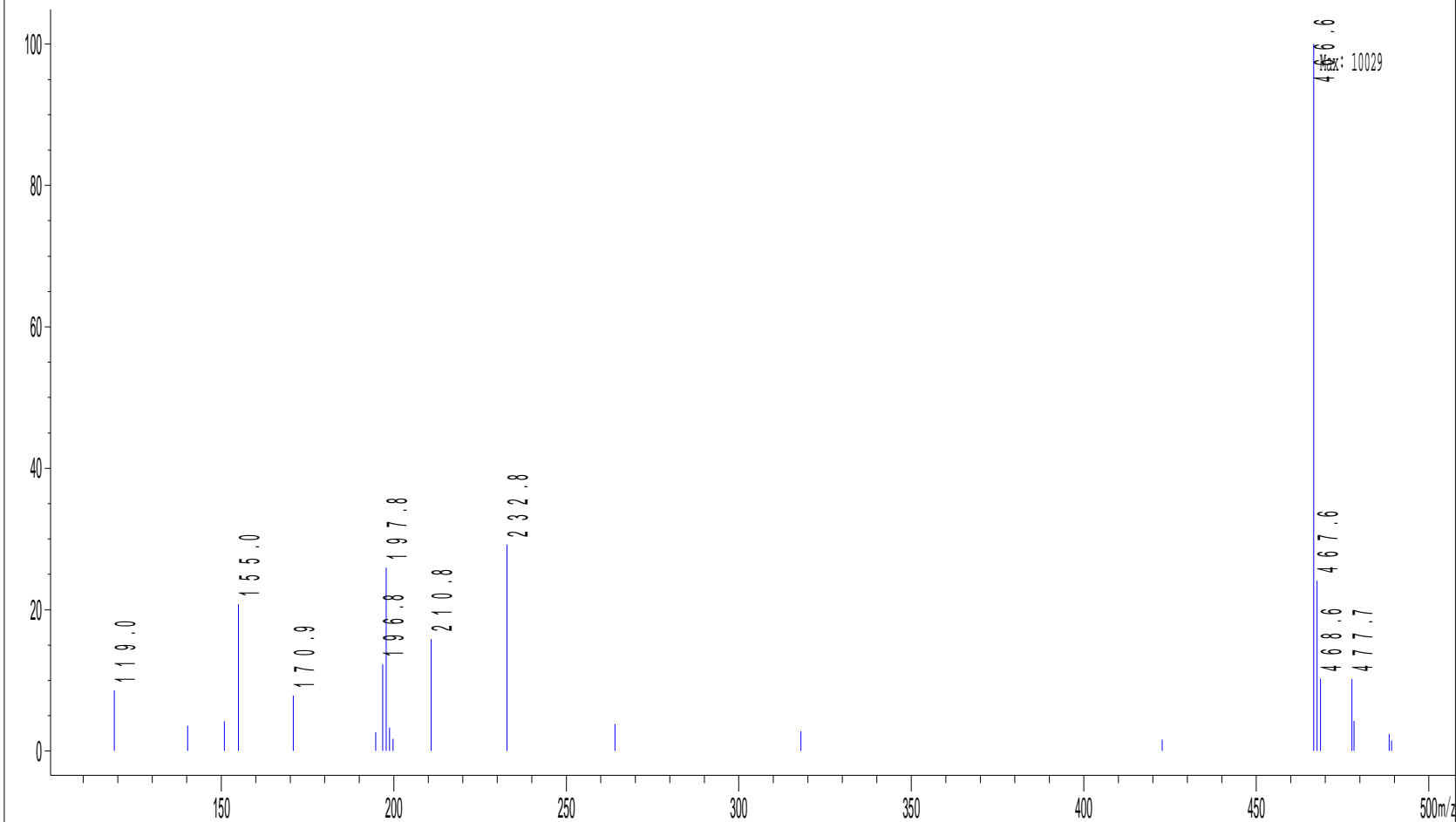


pH 7

14-Jul-15  
H2O2 Ctrl  
7  
P2-C-08

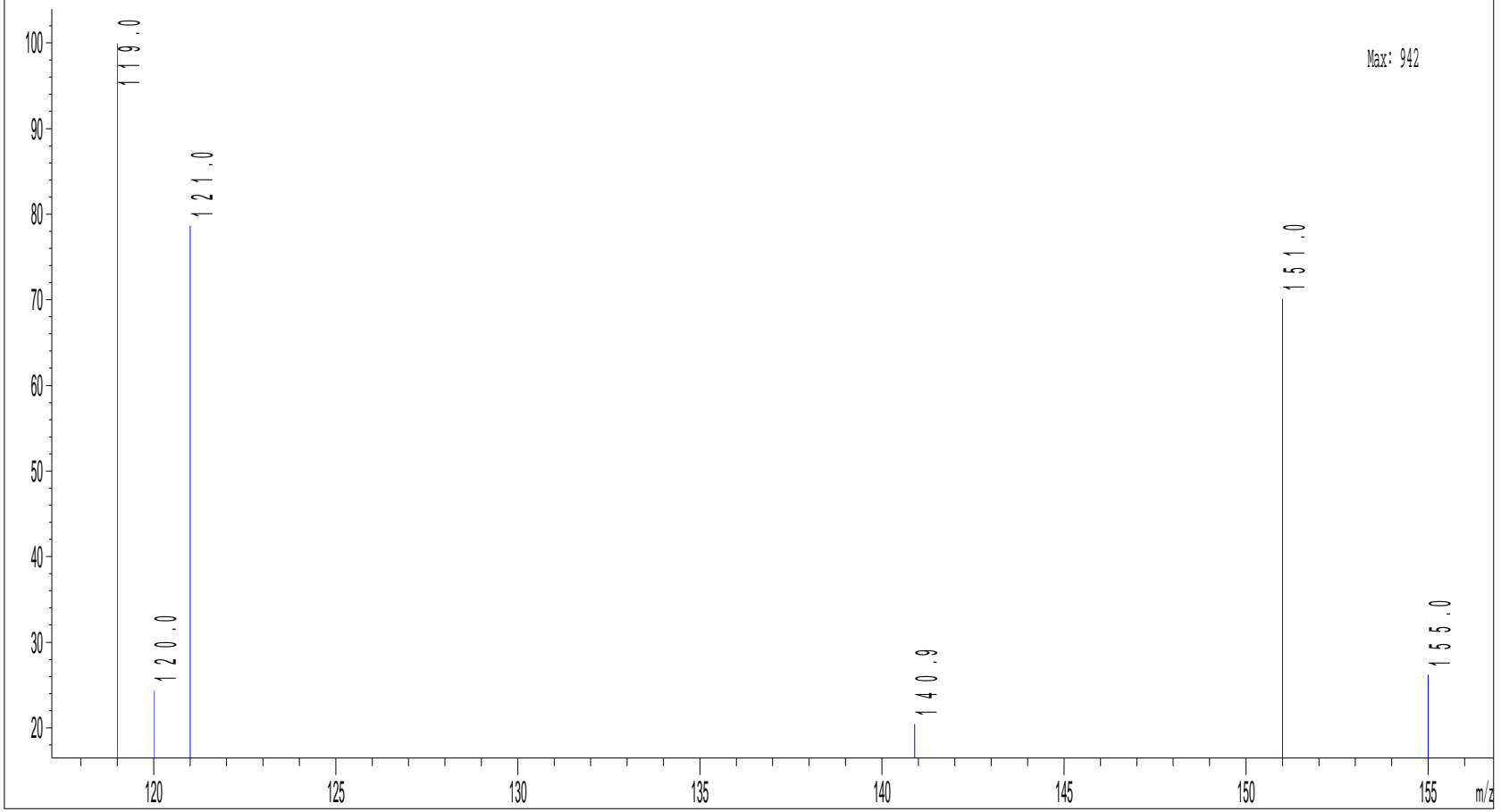


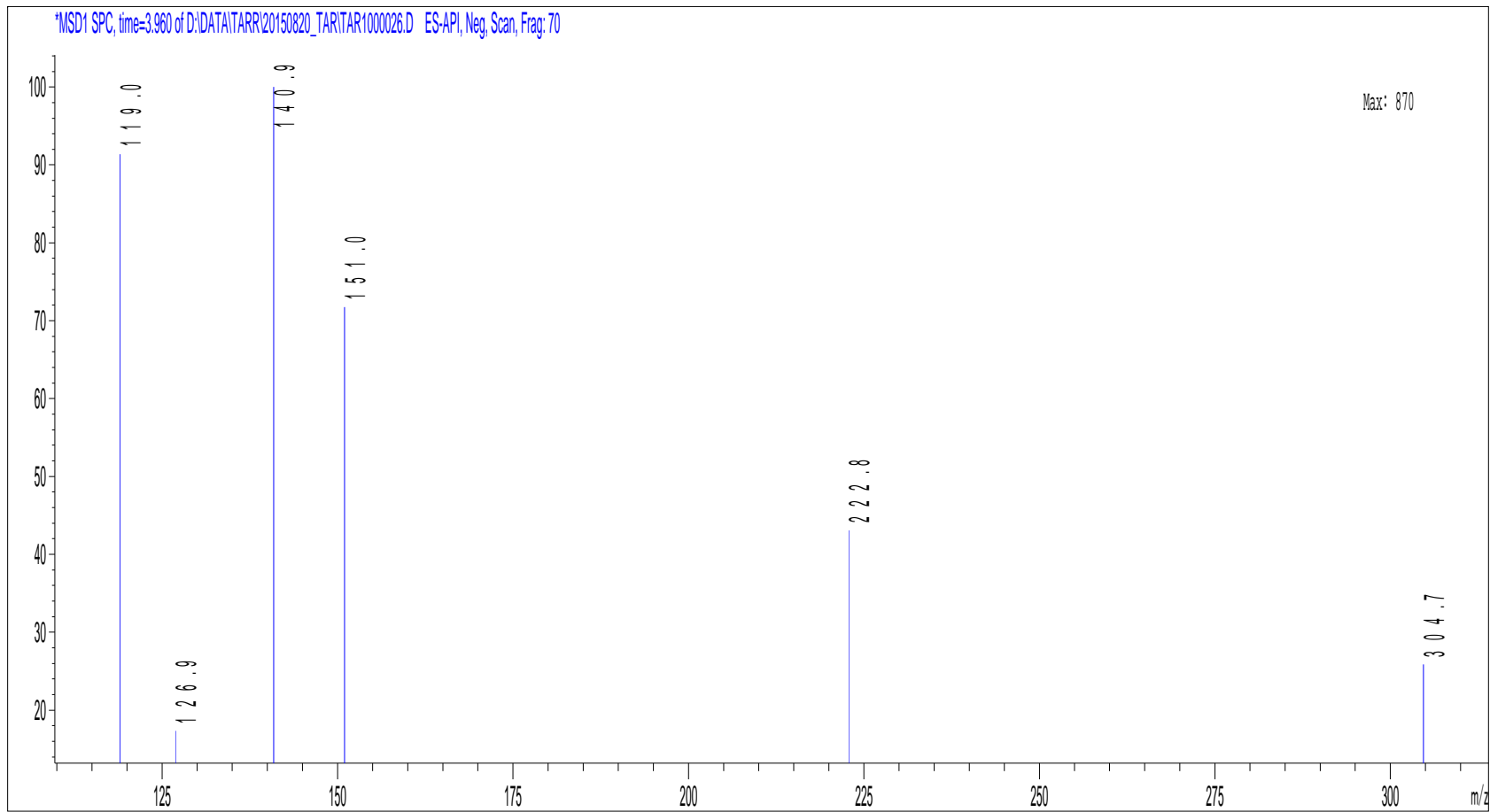
\*MSD1 SPC, time=2.983 of D:\DATA\ARRI20150820\_TARITAR1000026.D ES-API, Neg, Scan, Frag: 70





\*MSD1 SPC, time=3.421 of D:\DATA\ARR\20150820\_TARITAR1000026.D ES-API, Neg, Scan, Frag: 70



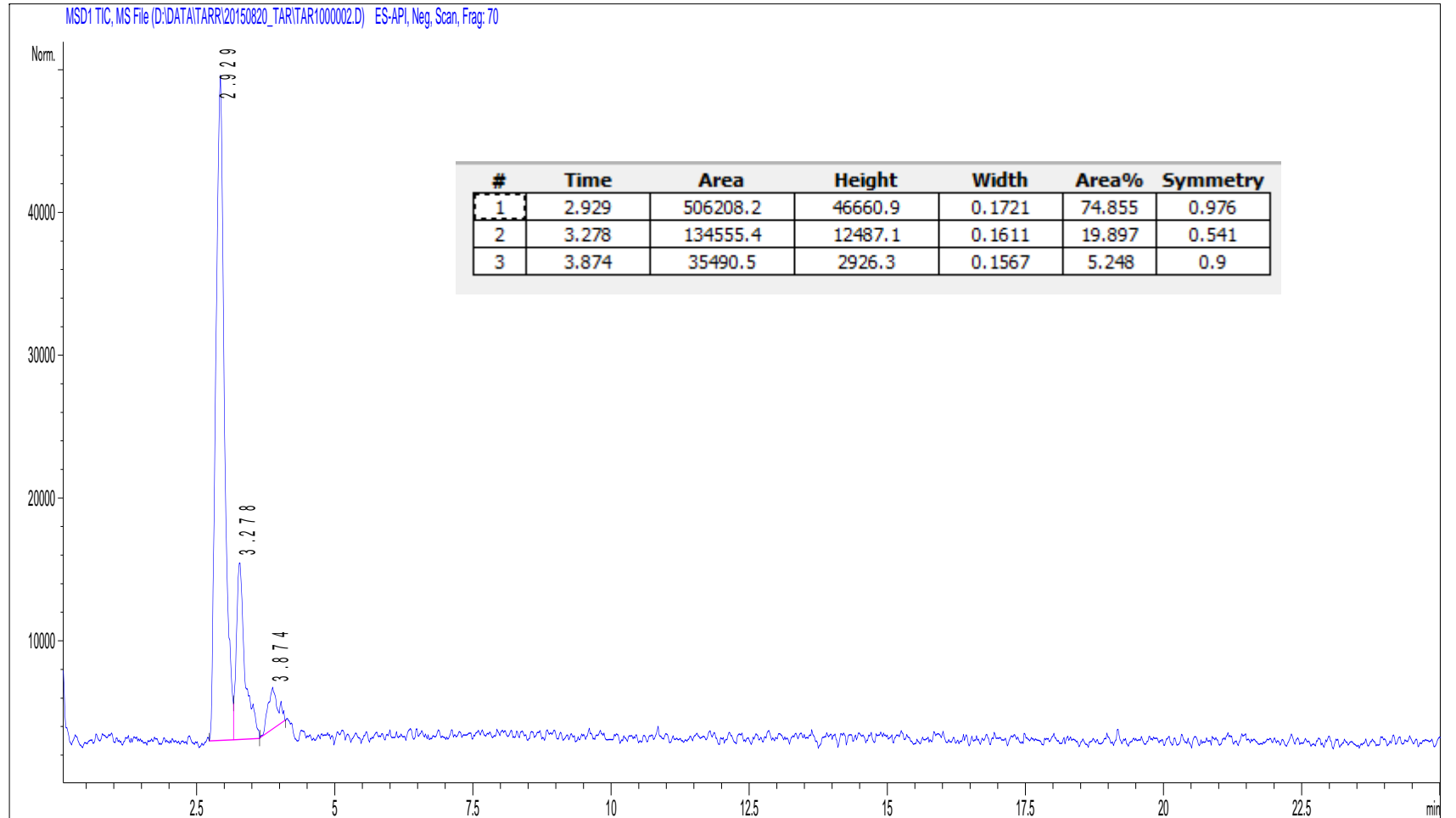


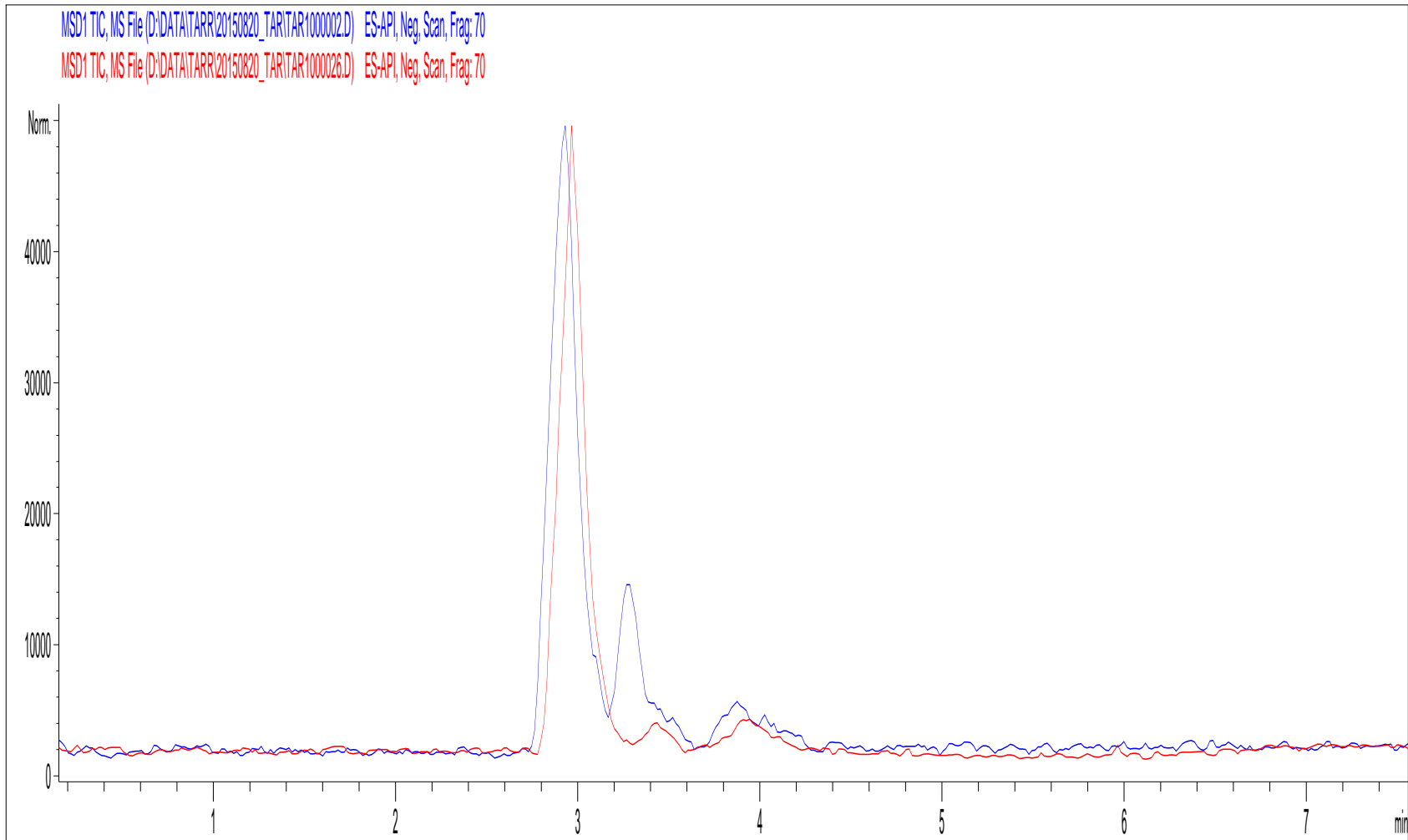
7-Mar-15

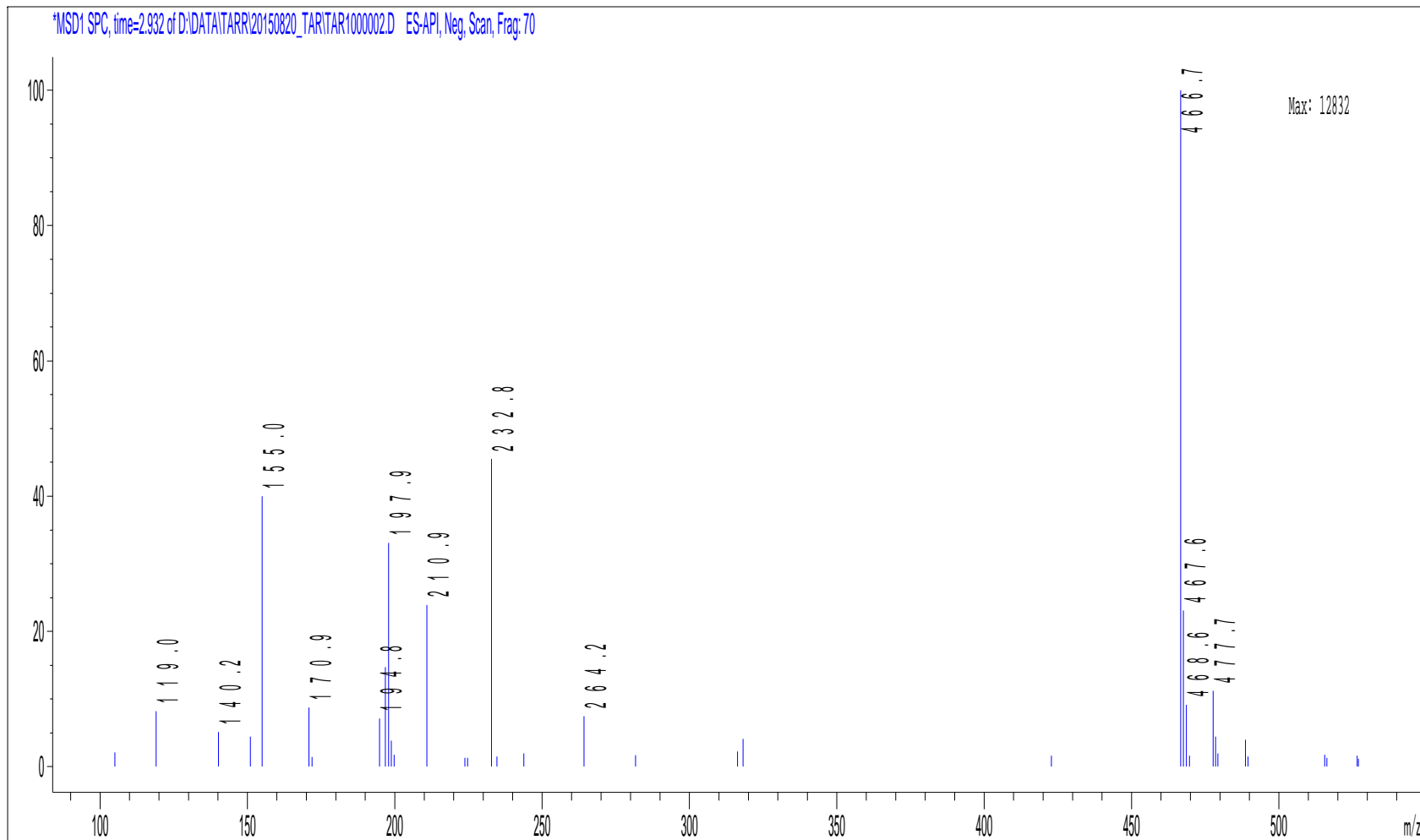
0 DC

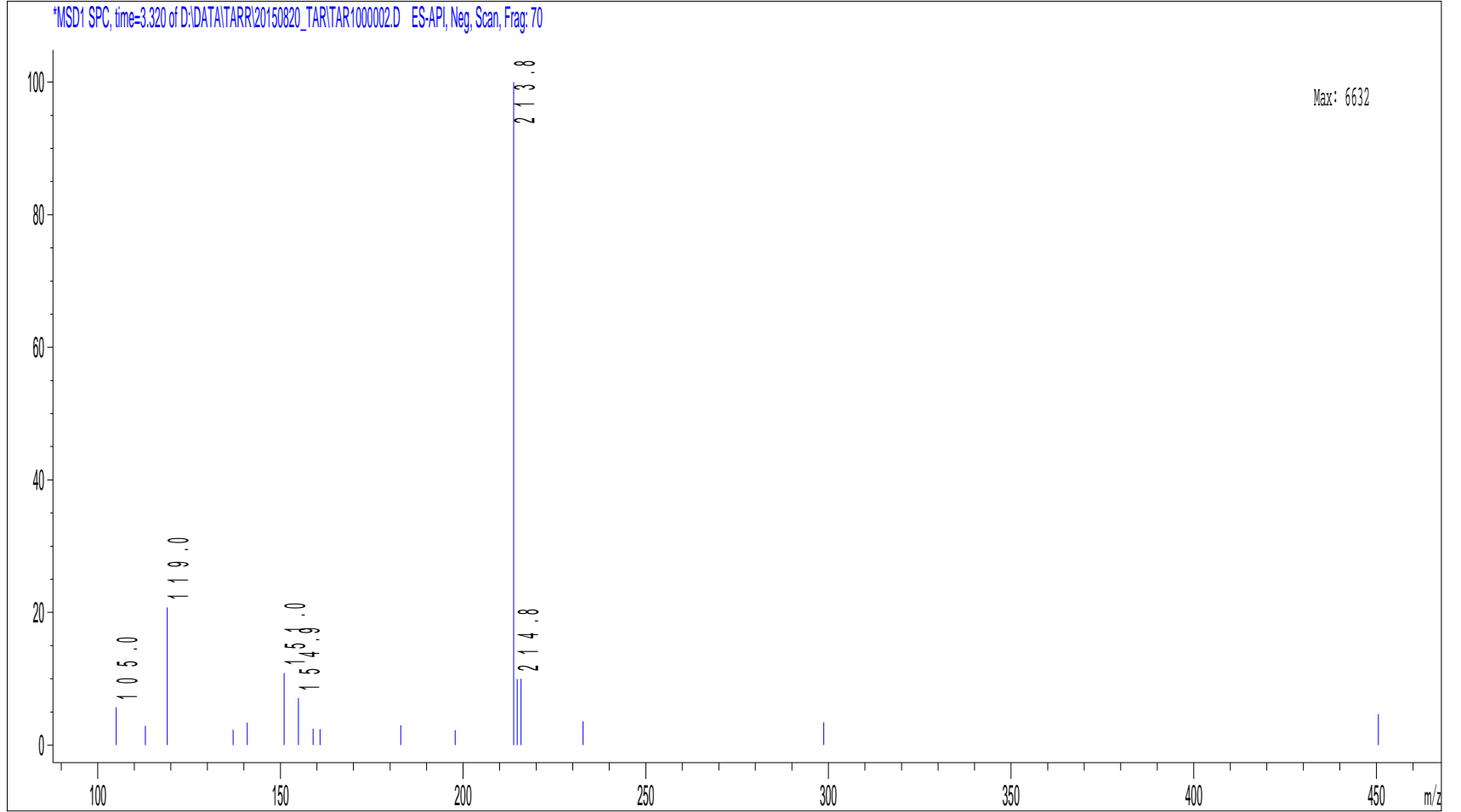
7

P2-A-02

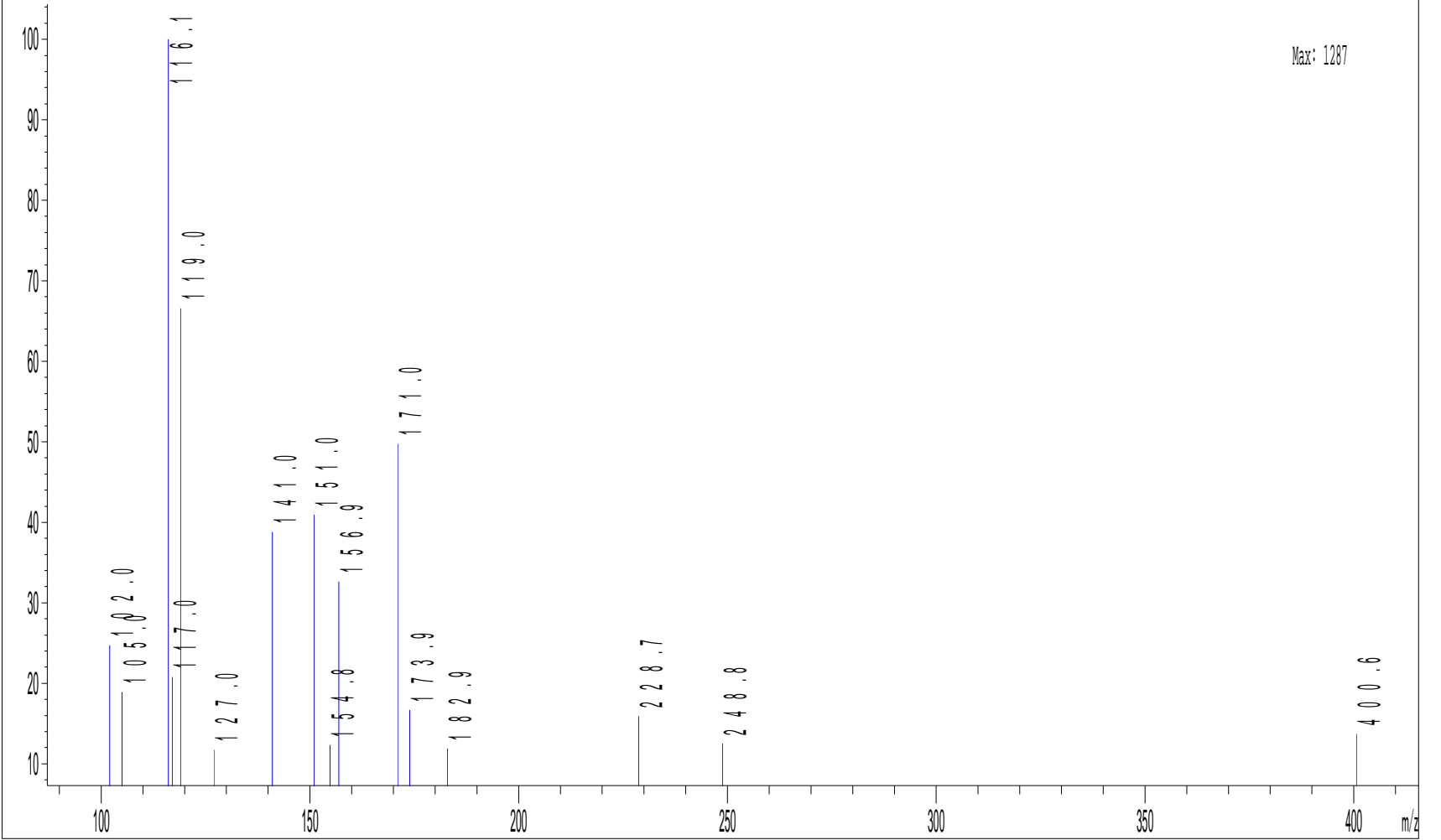








\*MSD1 SPC, time=3.909 of D:\DATA\ARR\20150820\_TARITAR1000002.D ES-API, Neg, Scan, Frag: 70

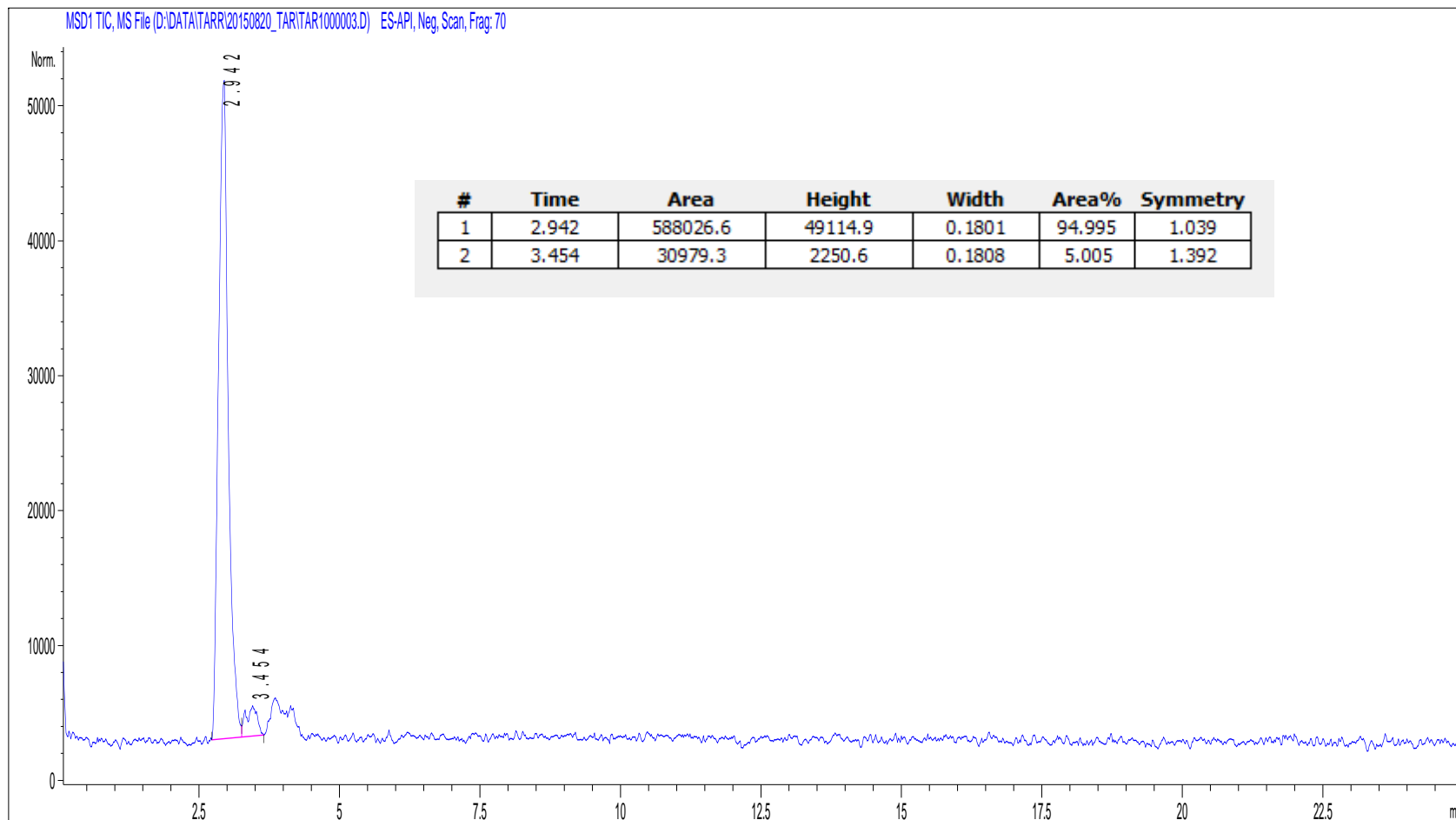


13-Mar-15

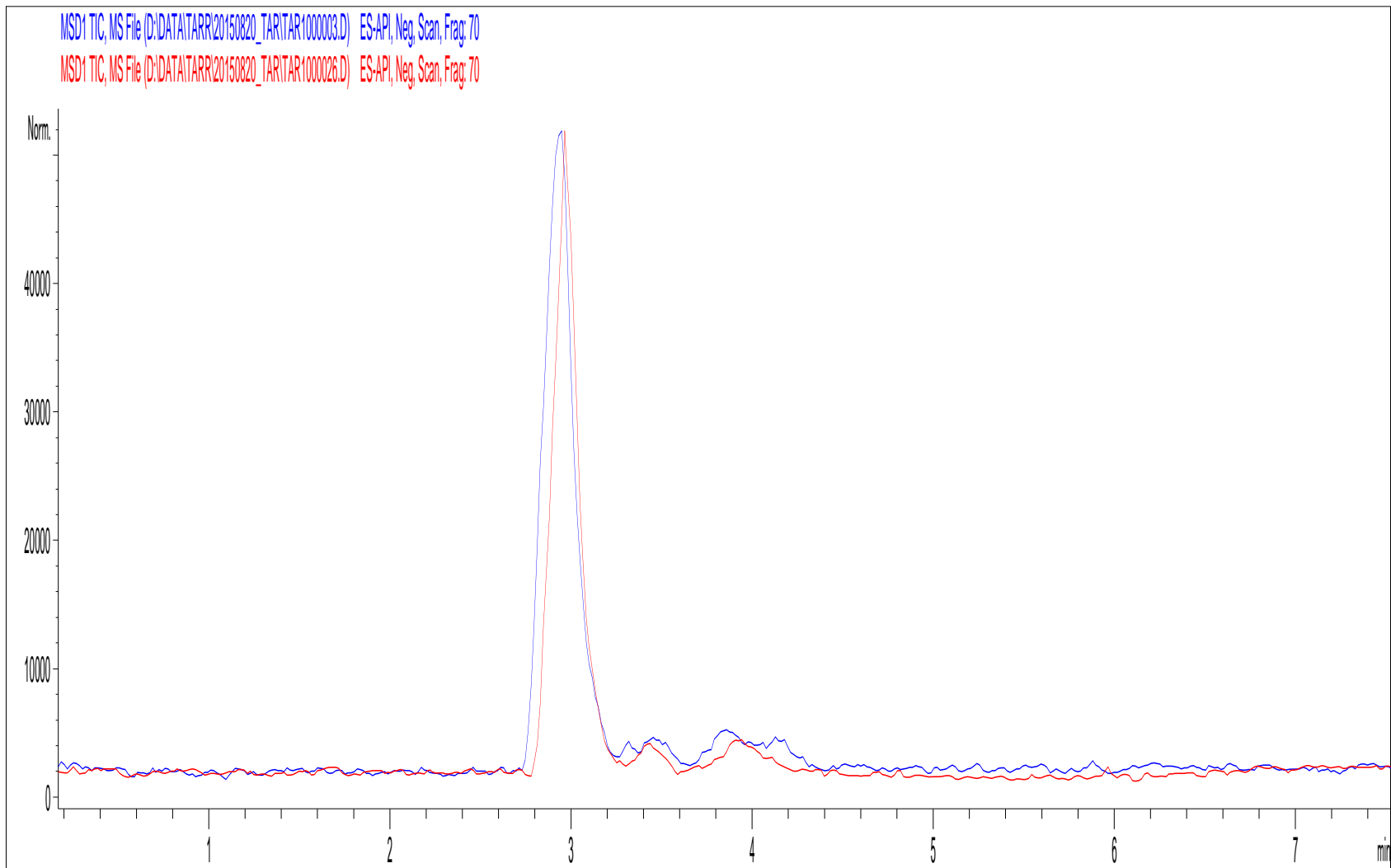
5 DC

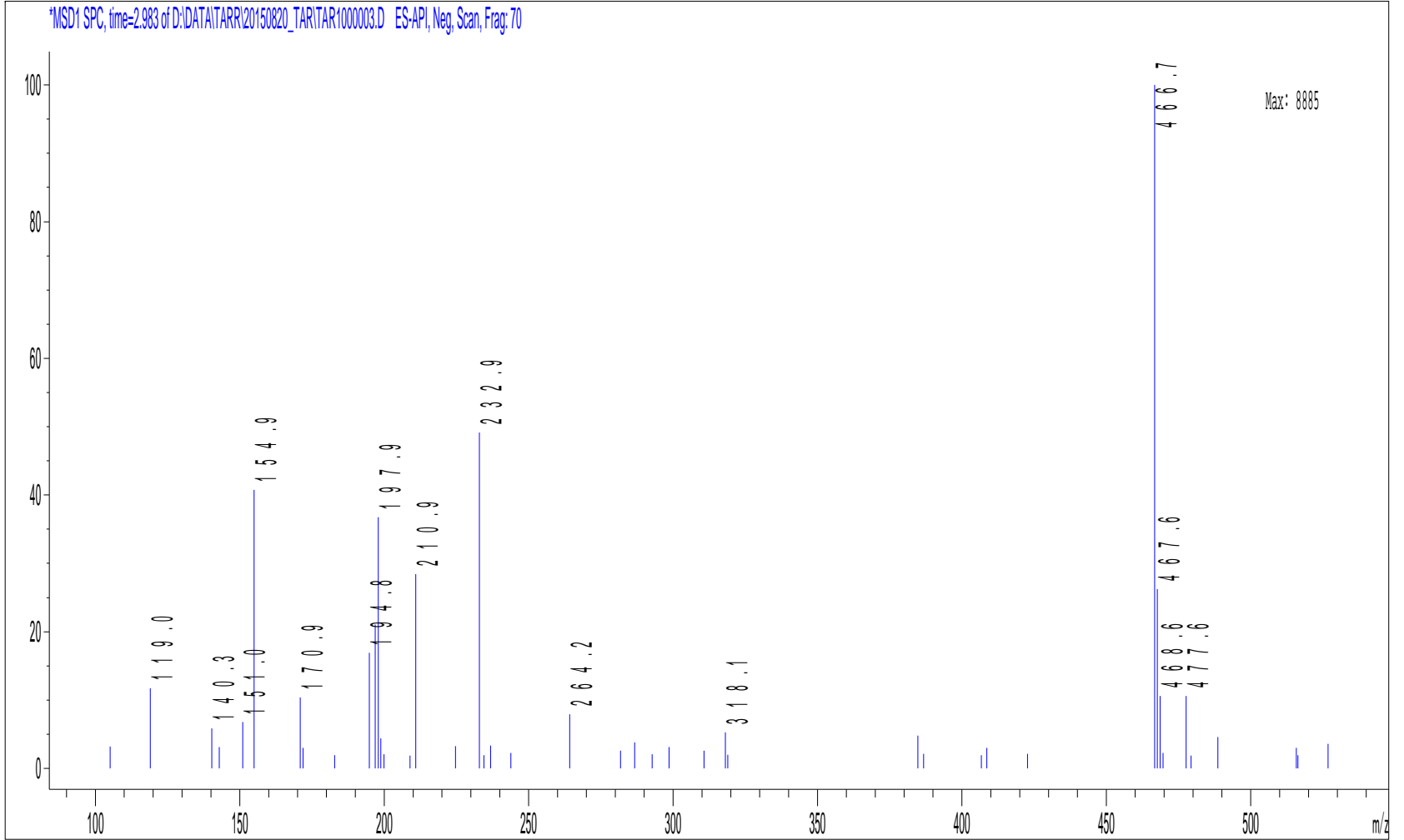
7

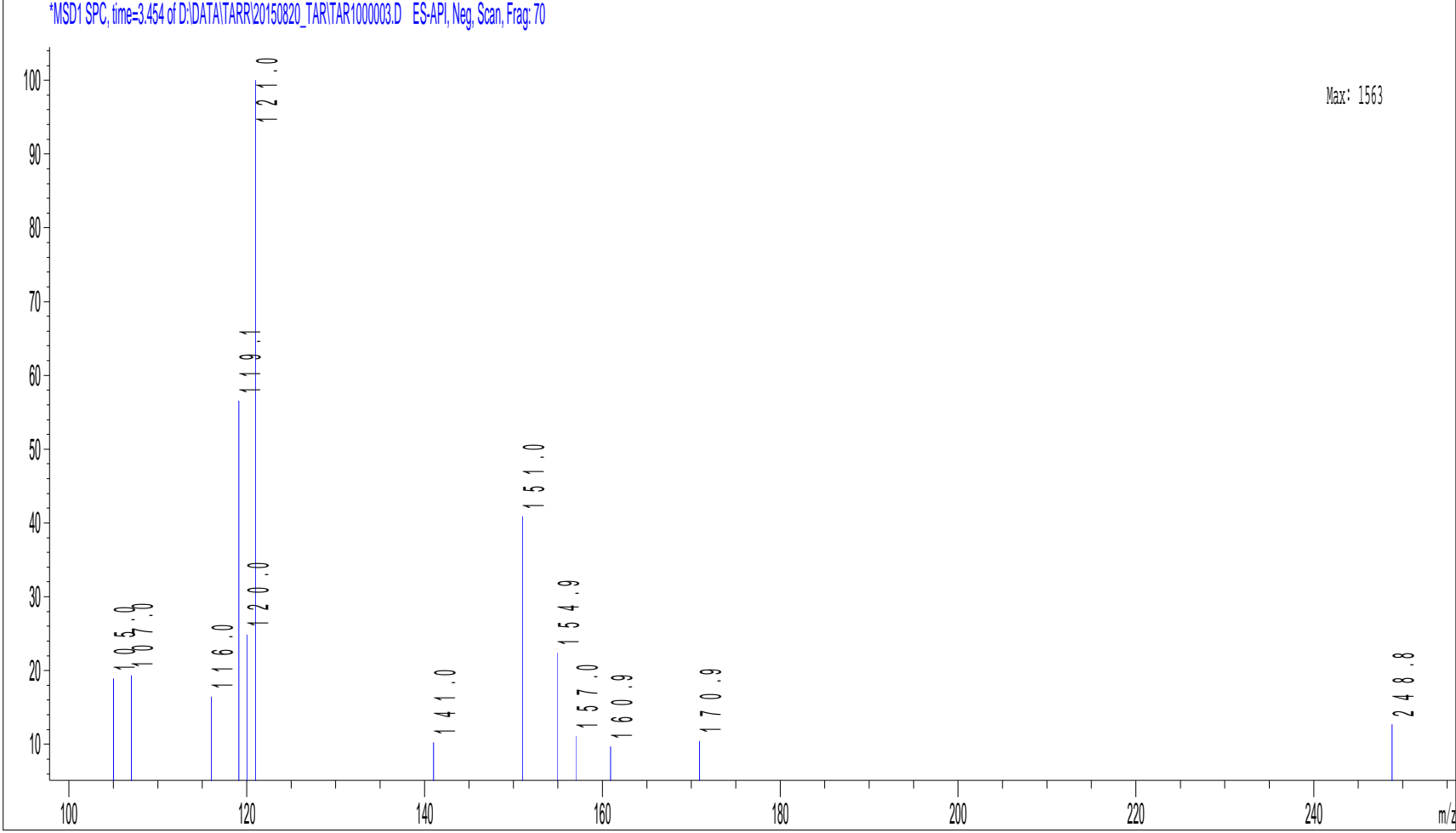
P2-A-03

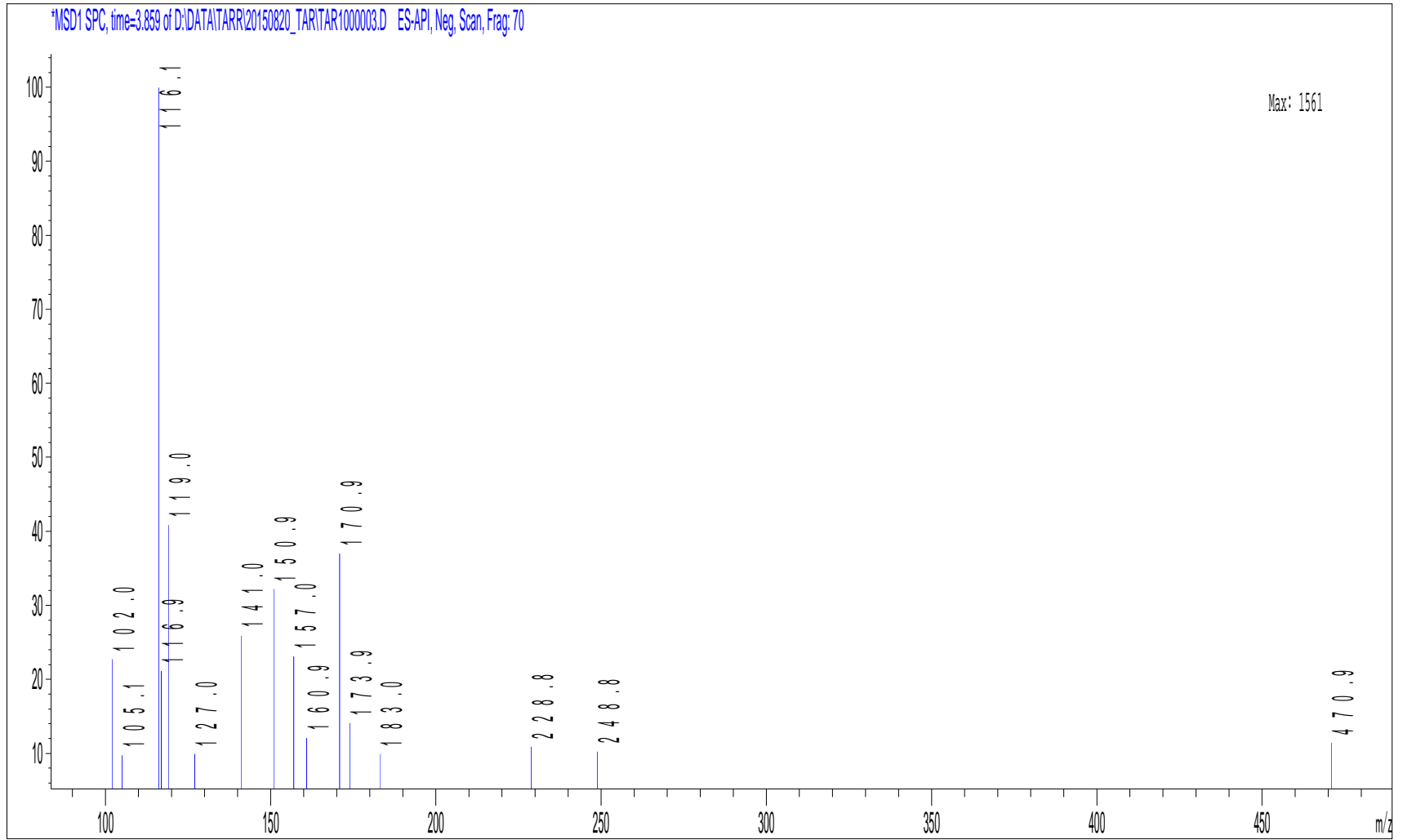


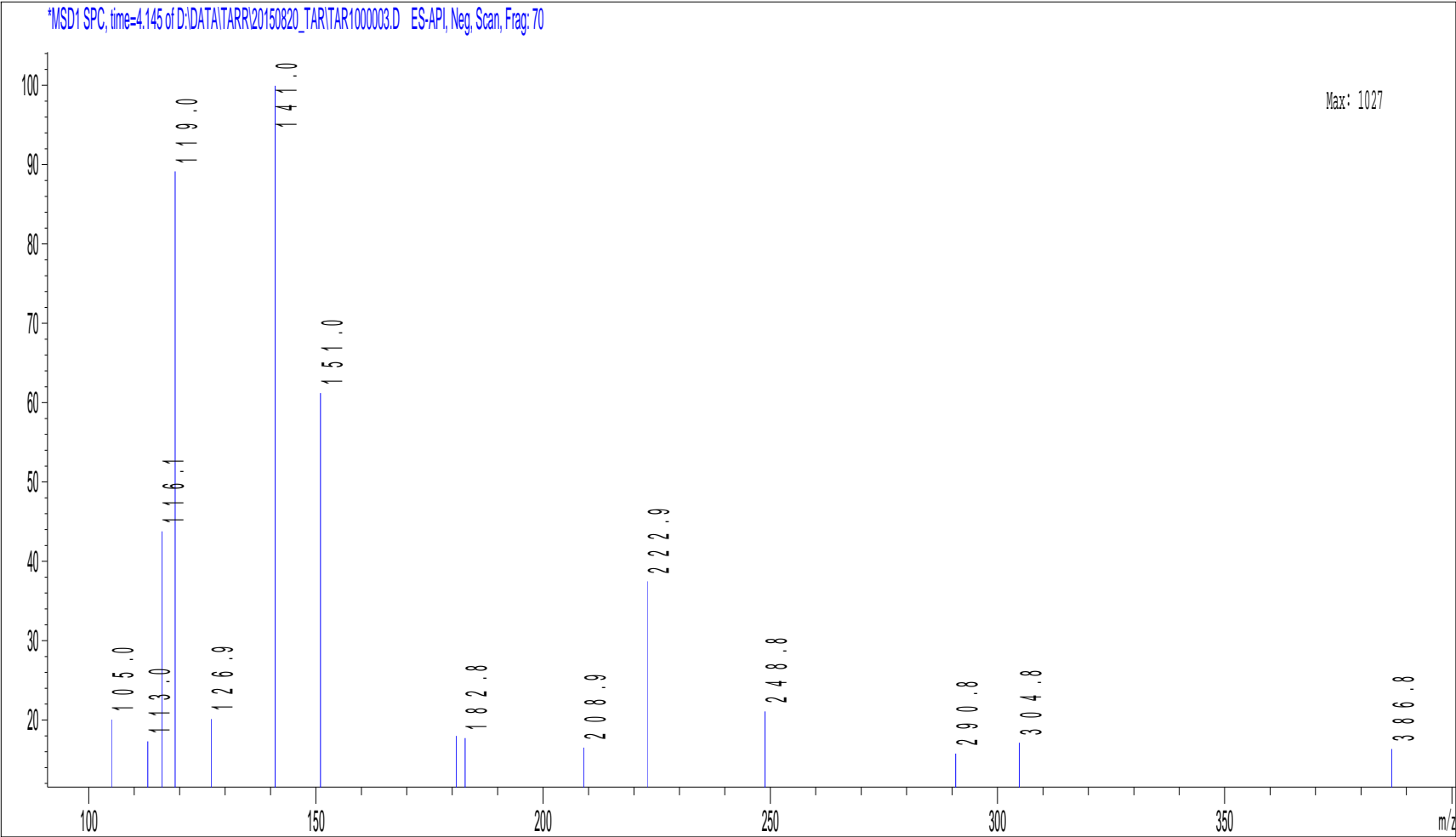










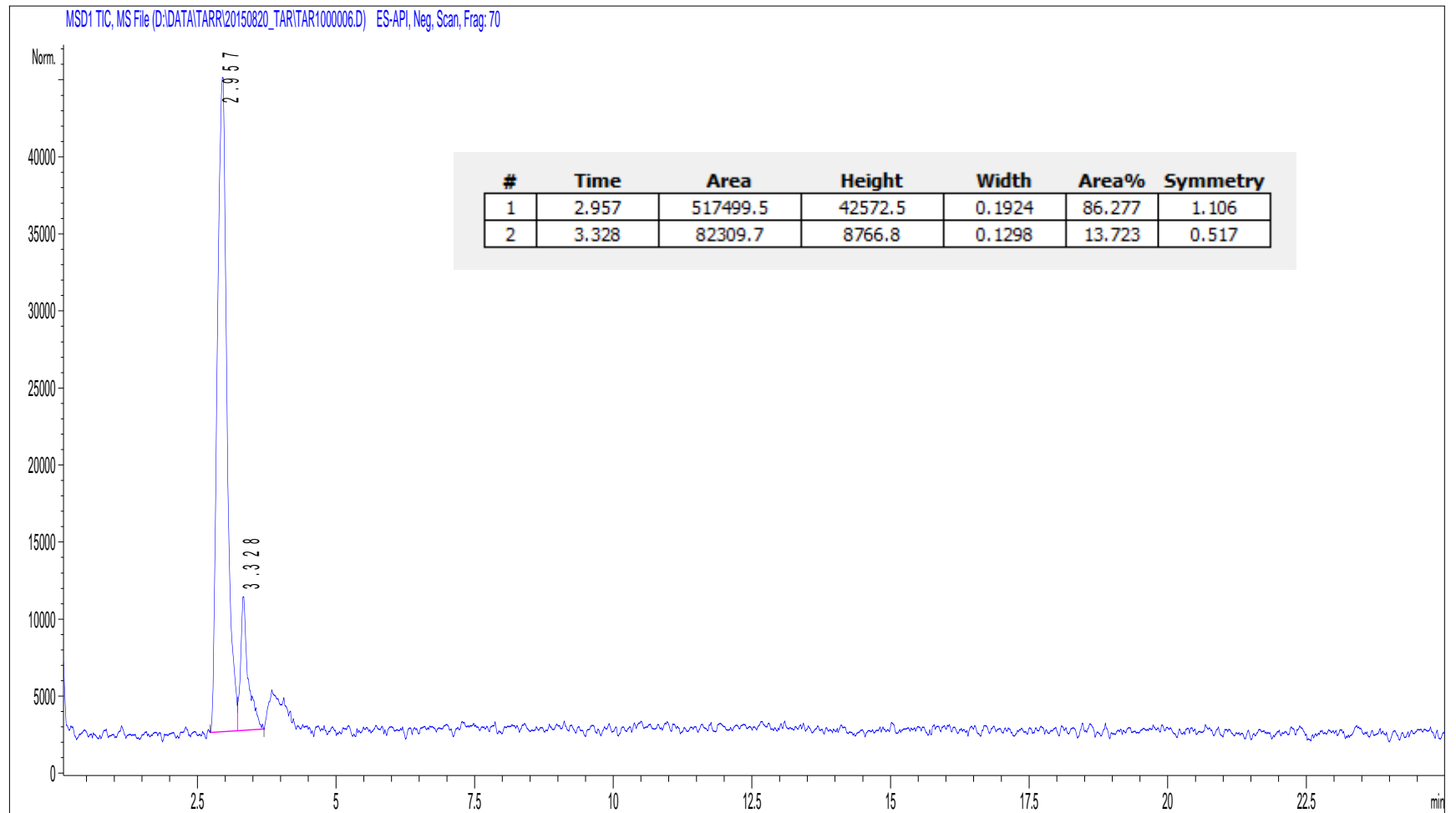


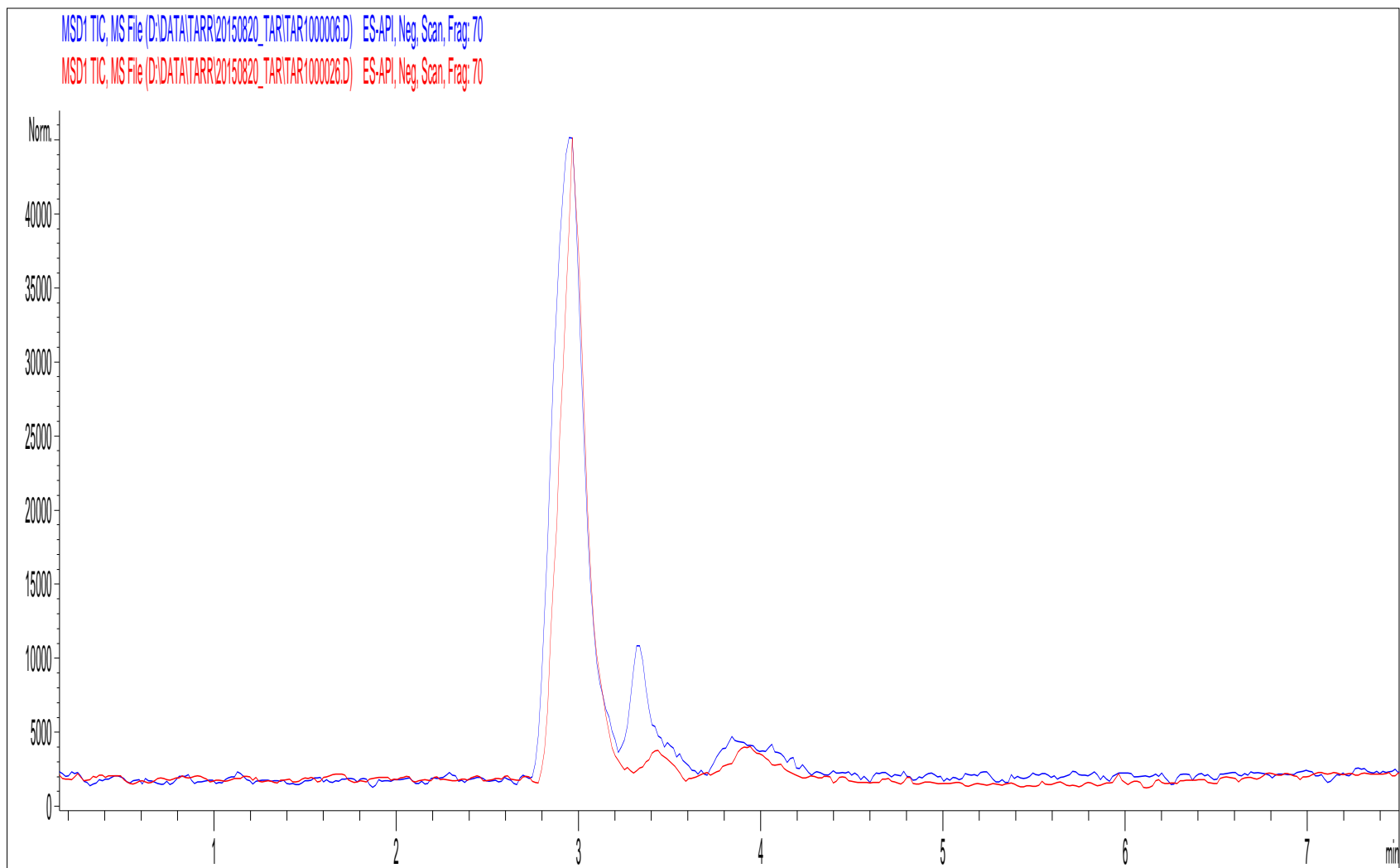
9-Apr-15

10 DC

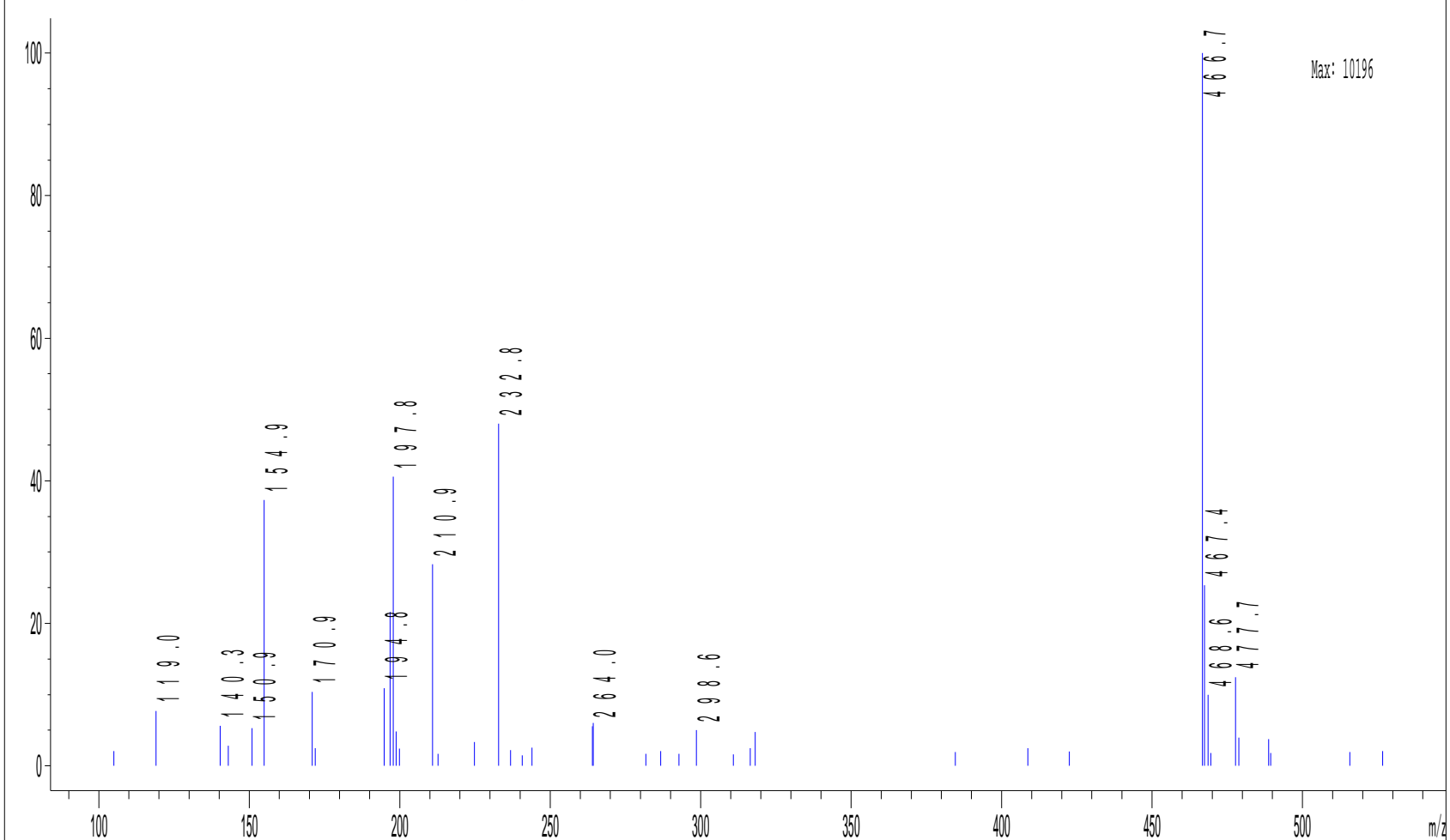
7

P2-A-06

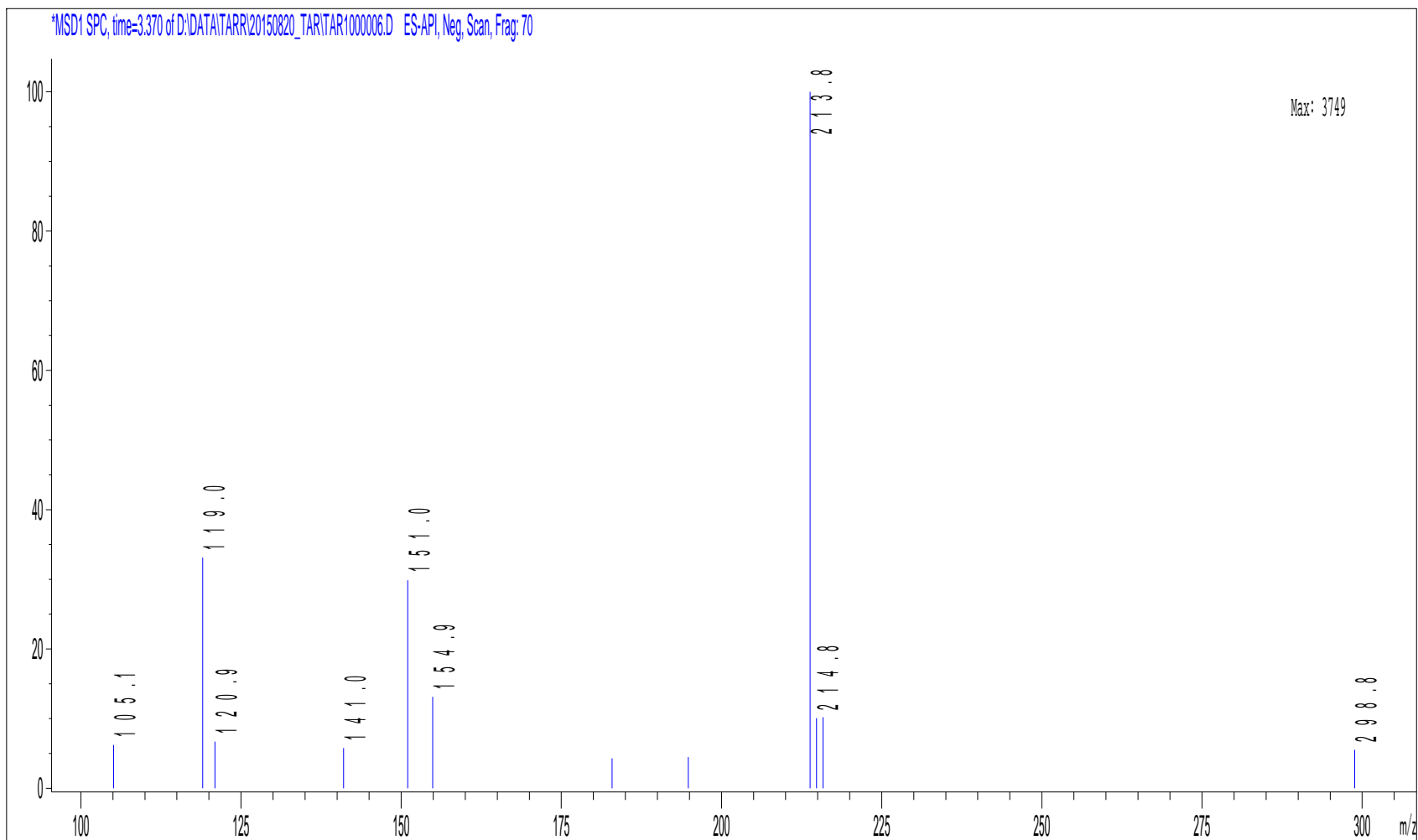


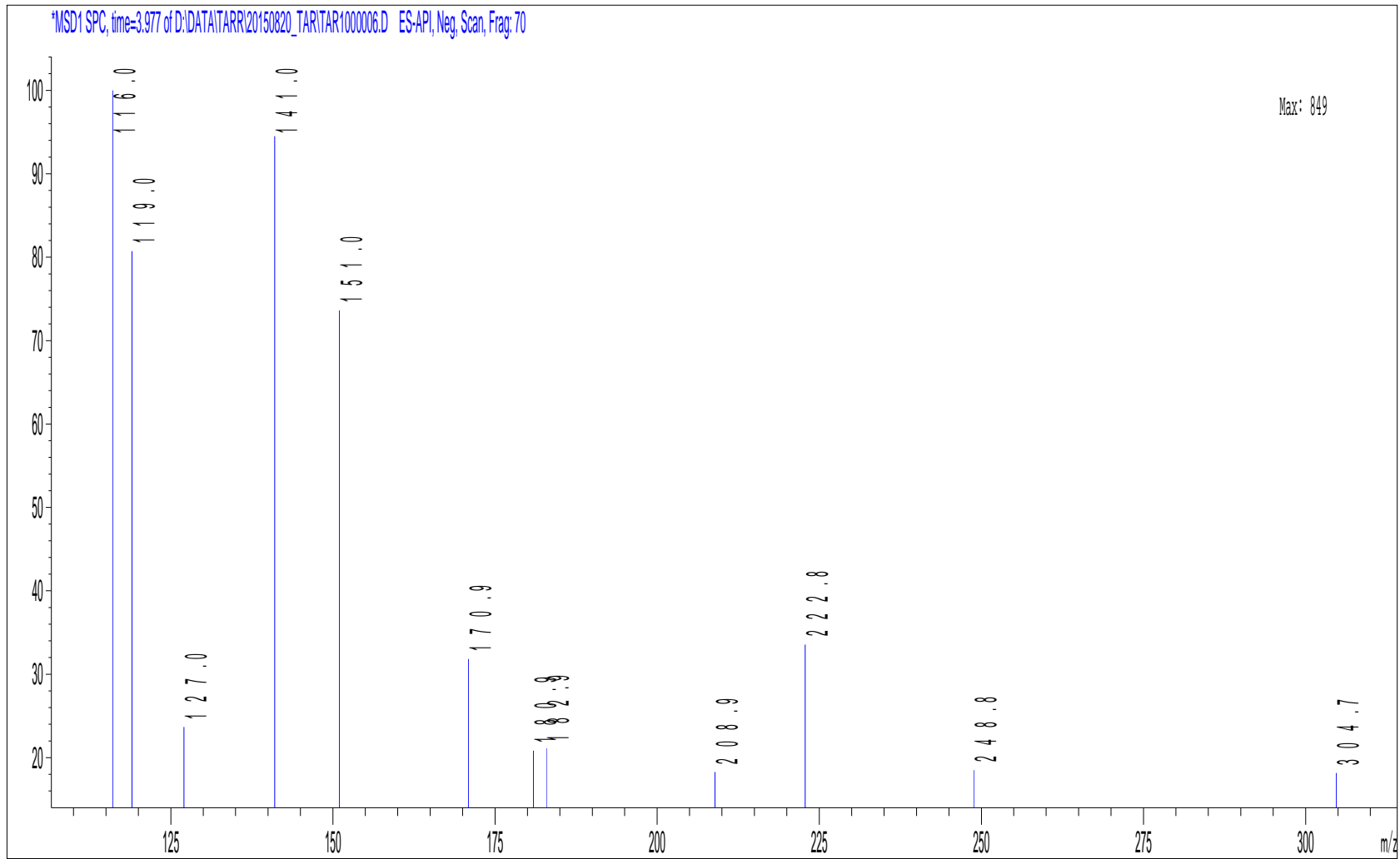


\*MSD1 SPC, time=2.966 of D:\DATA\TARRI\20150820\_TARITAR\1000006.D ES-API, Neg. Scan, Frag: 70







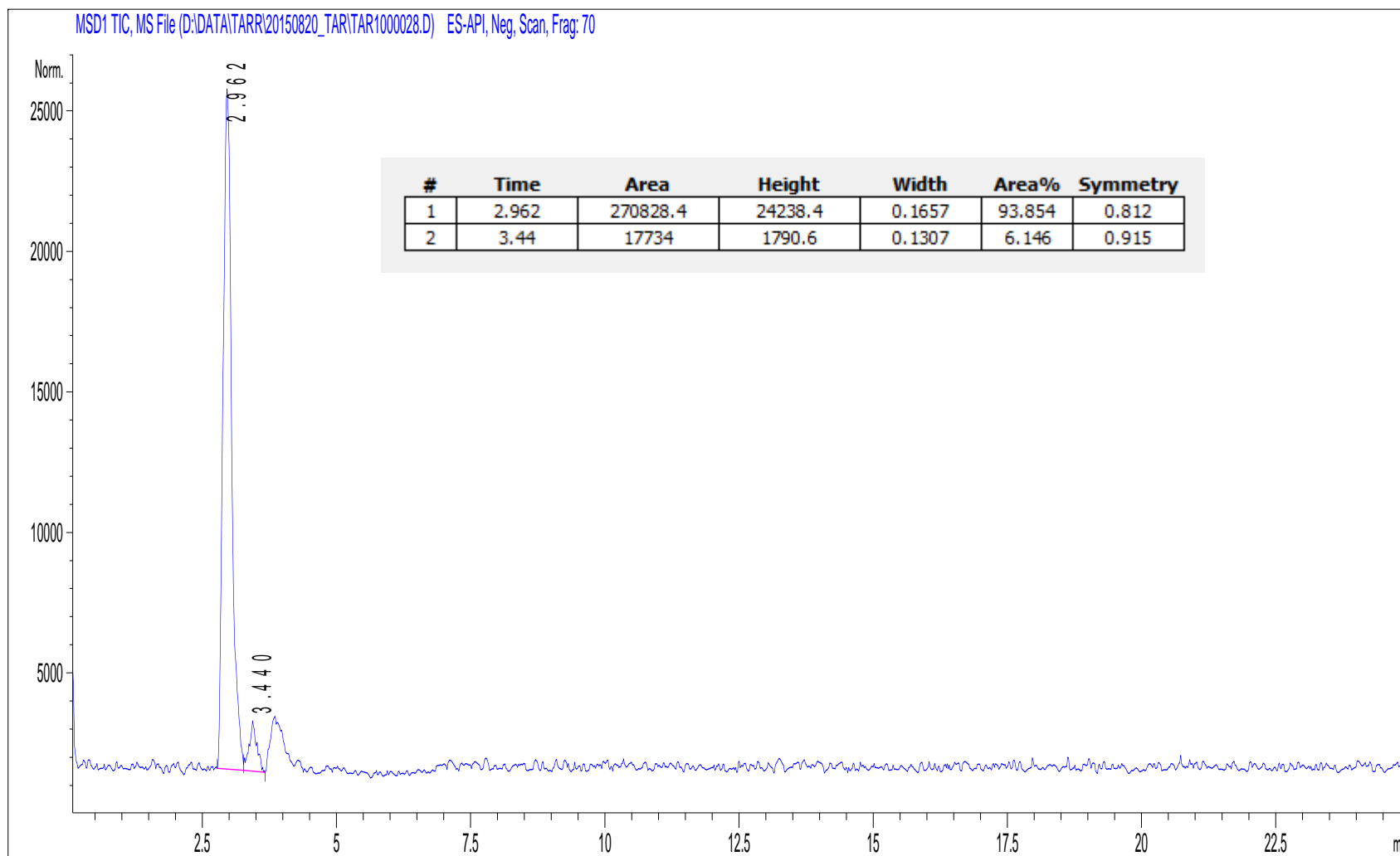


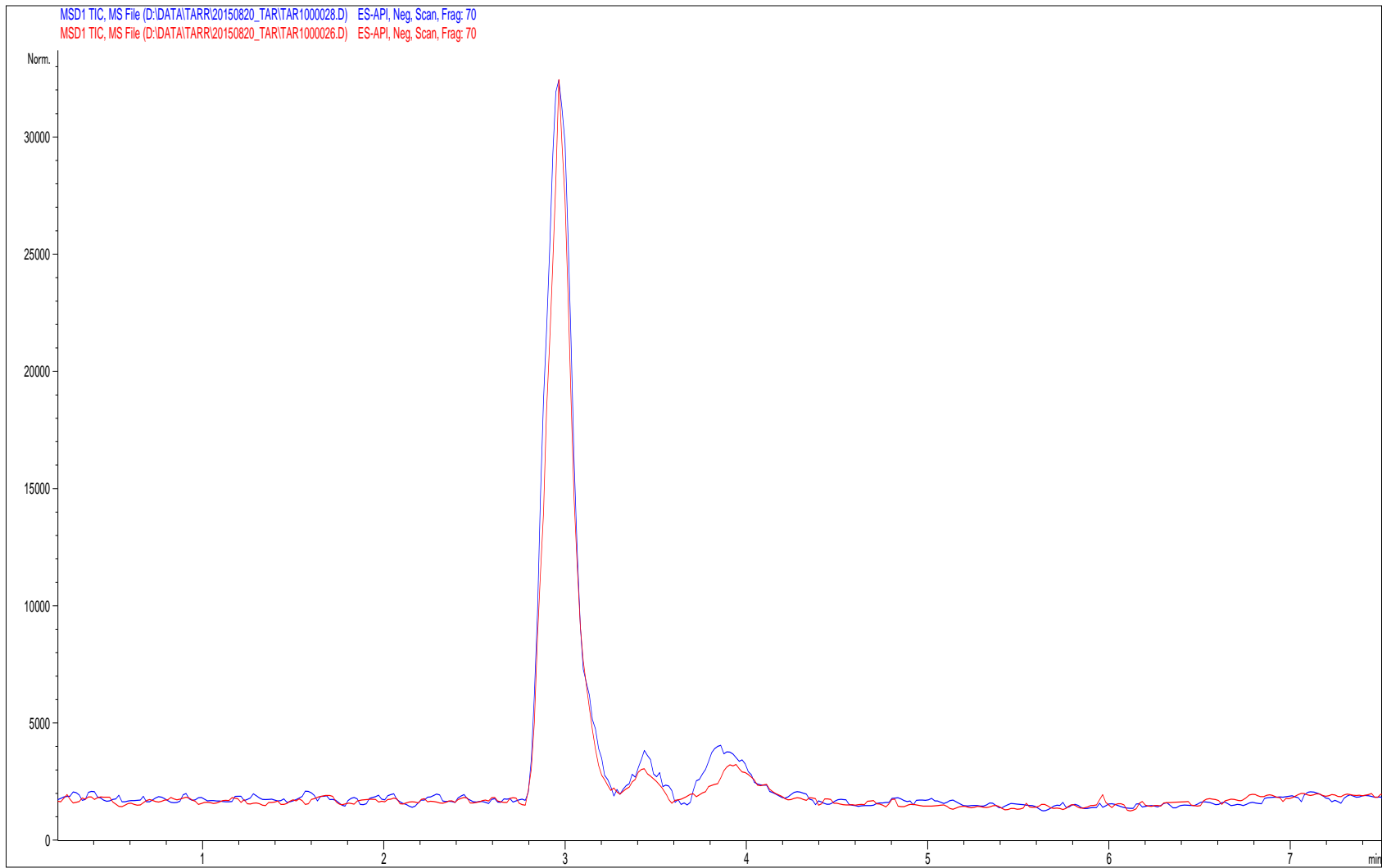
6-Aug-15

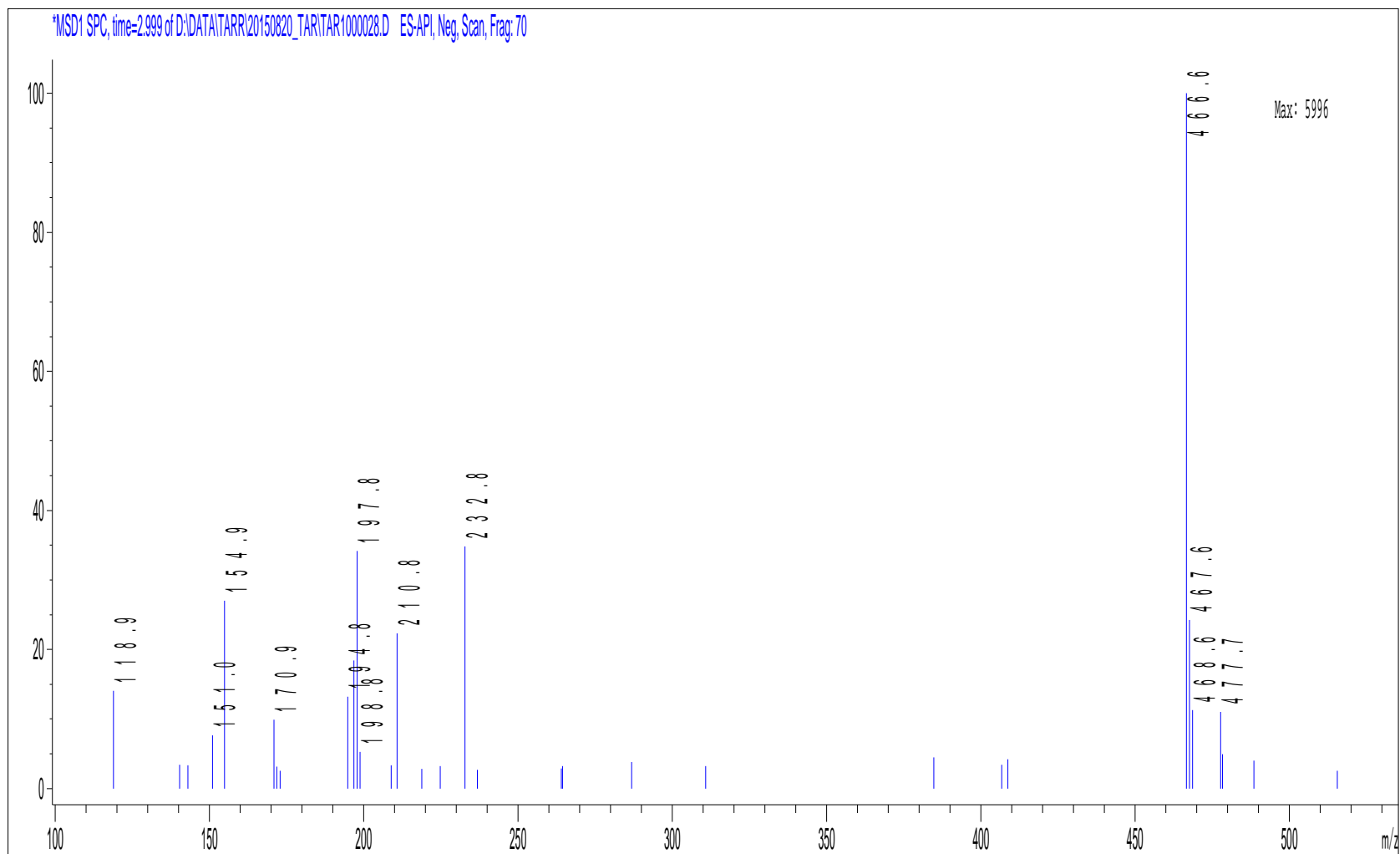
20 DC

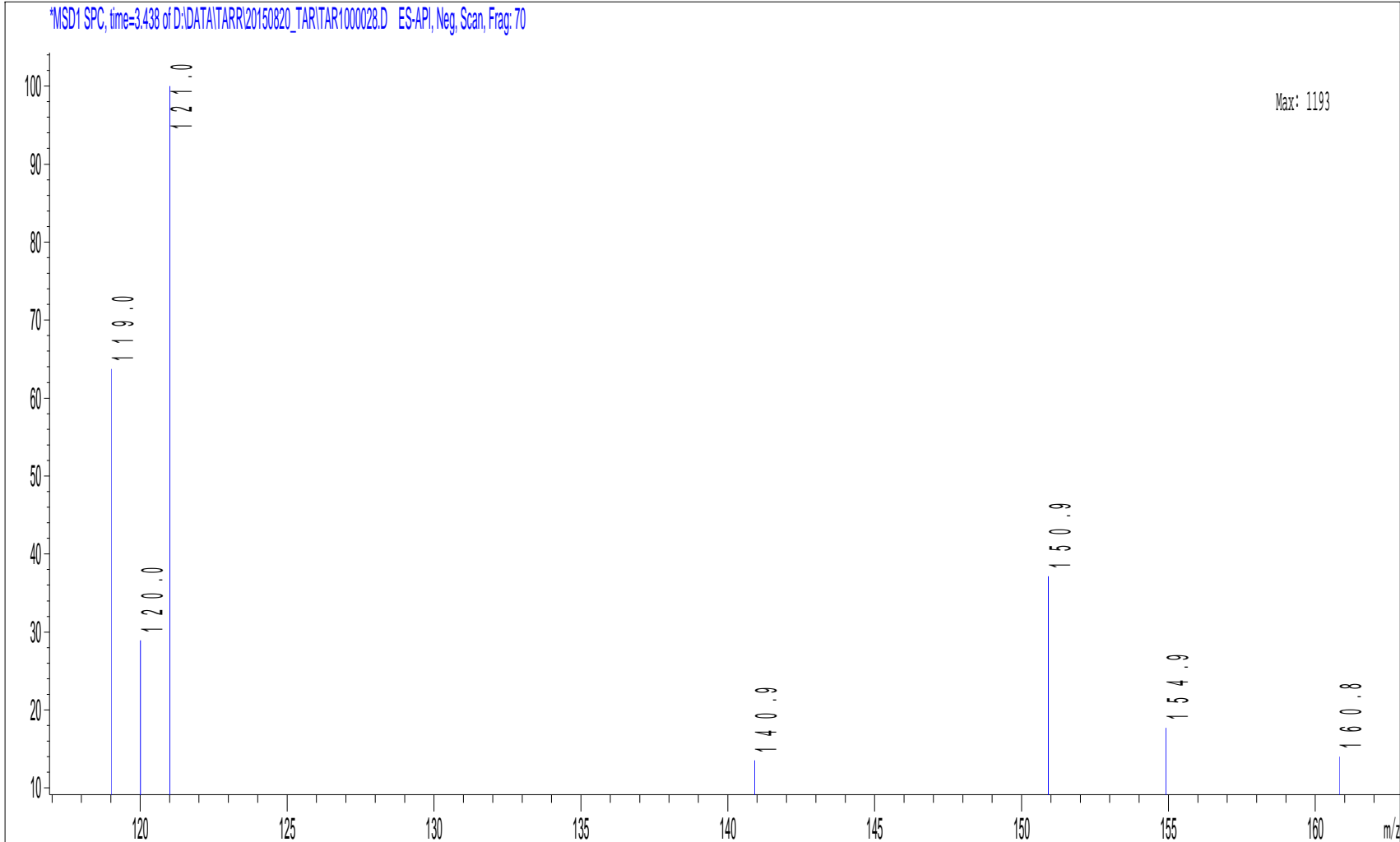
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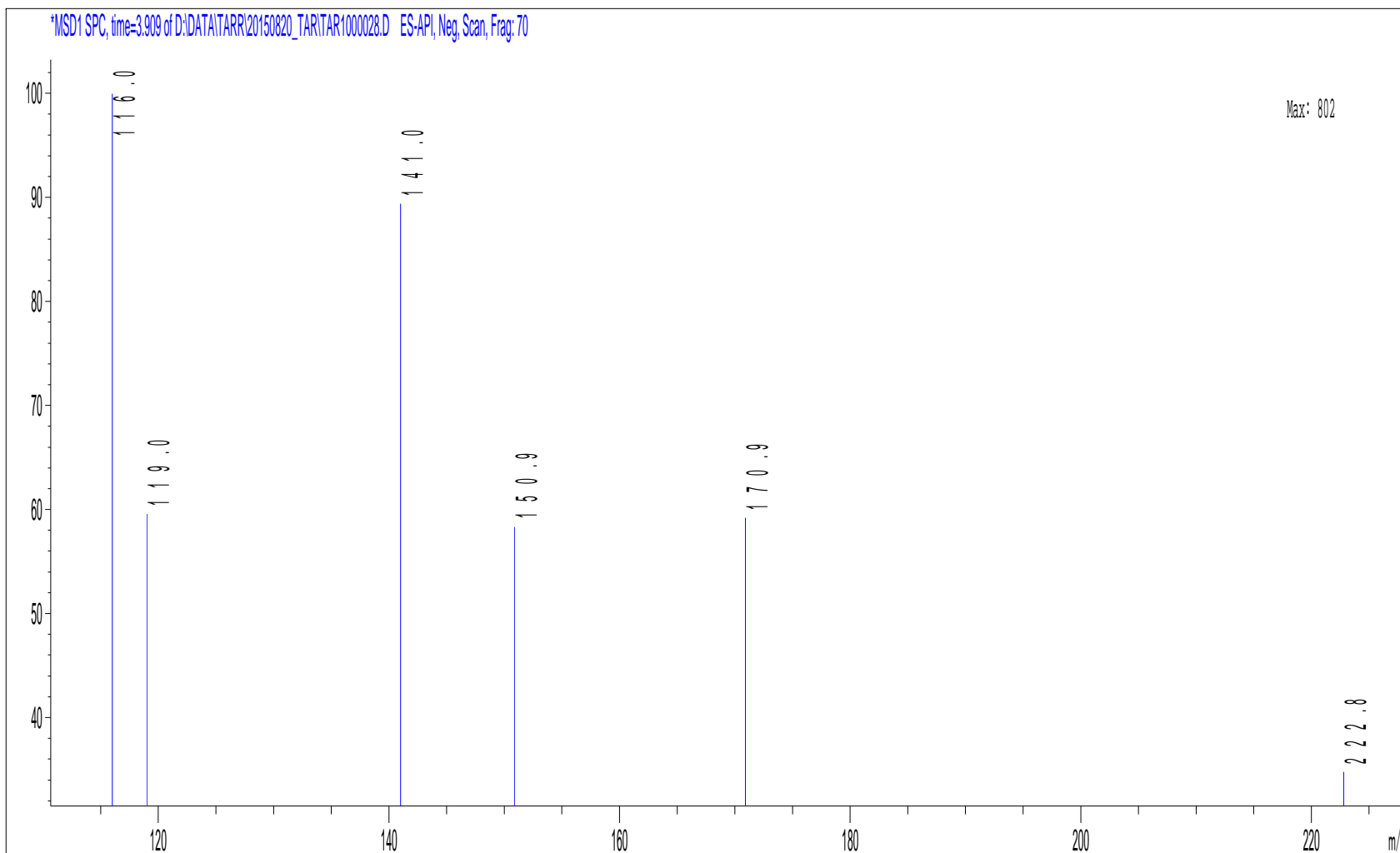
P2-D-09









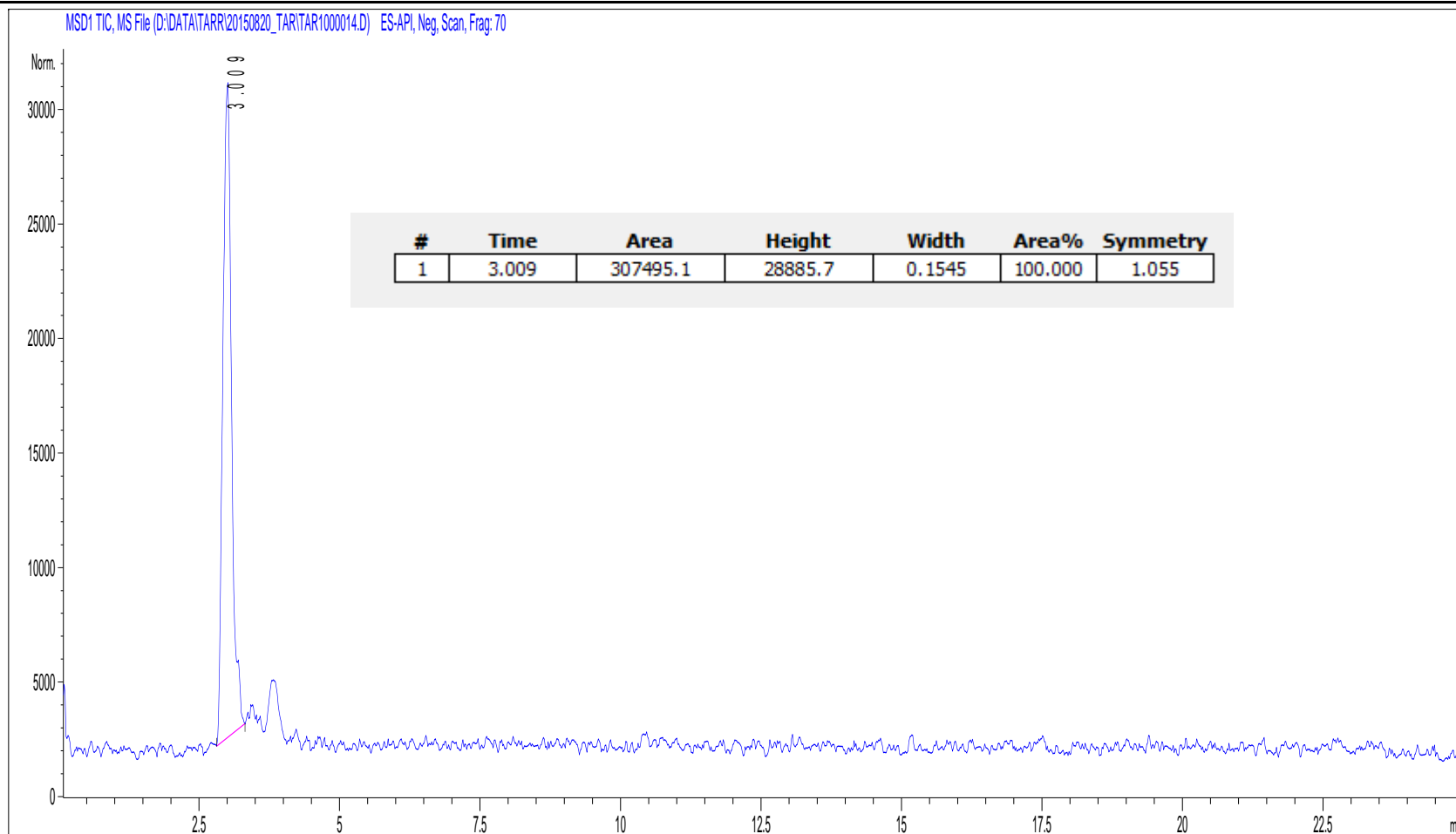


3-Jun-15

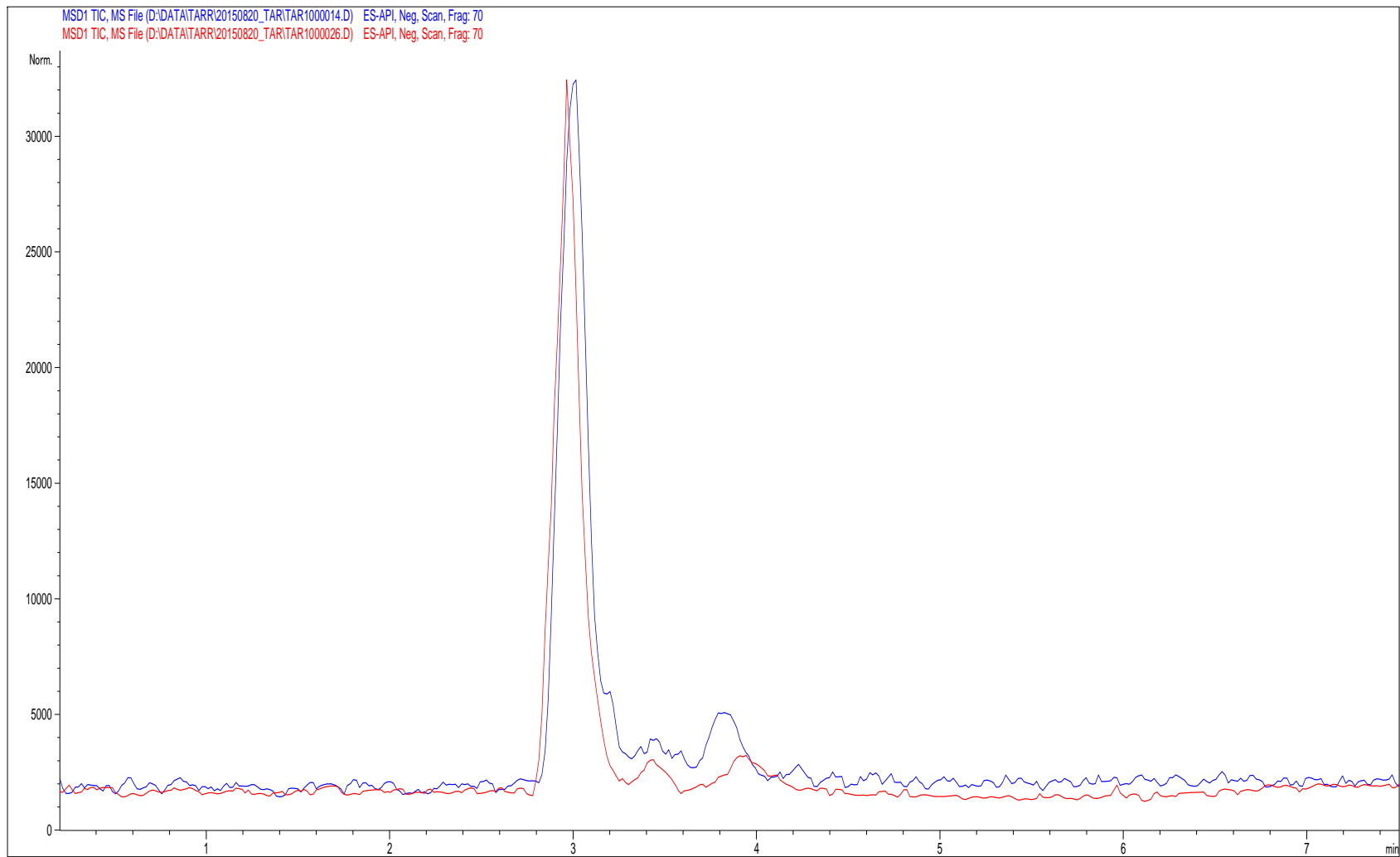
30 DC

7

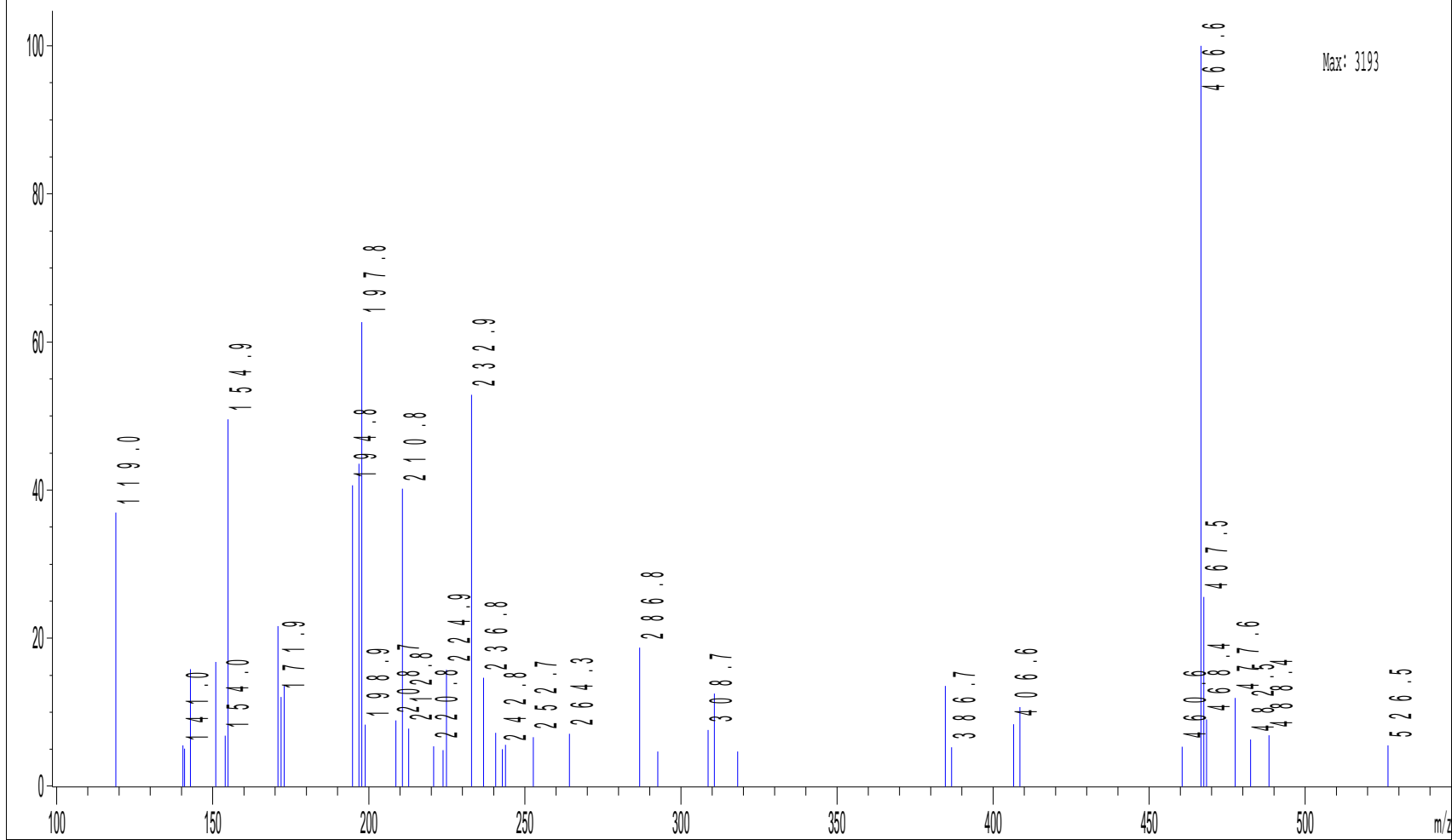
P2-B-05



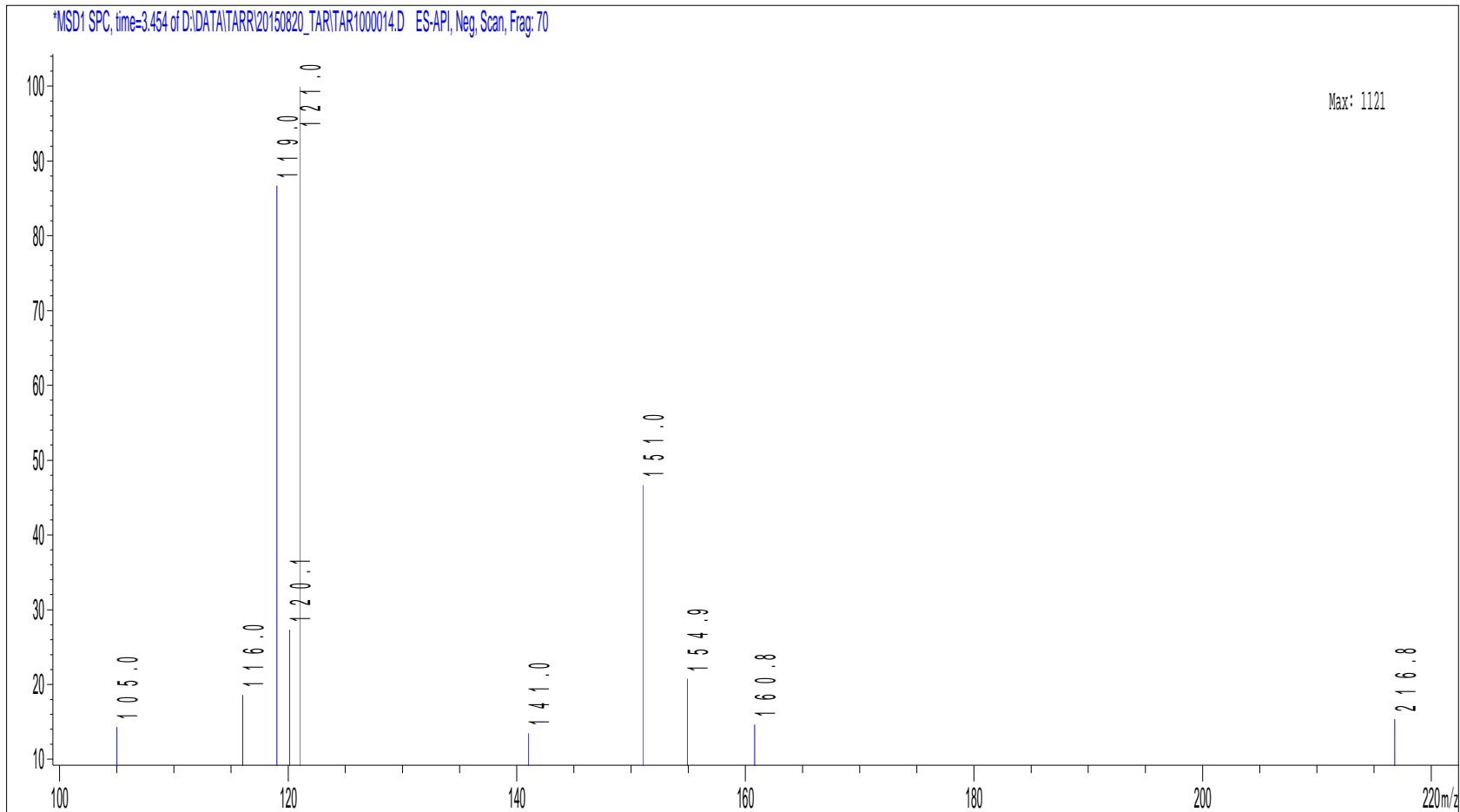




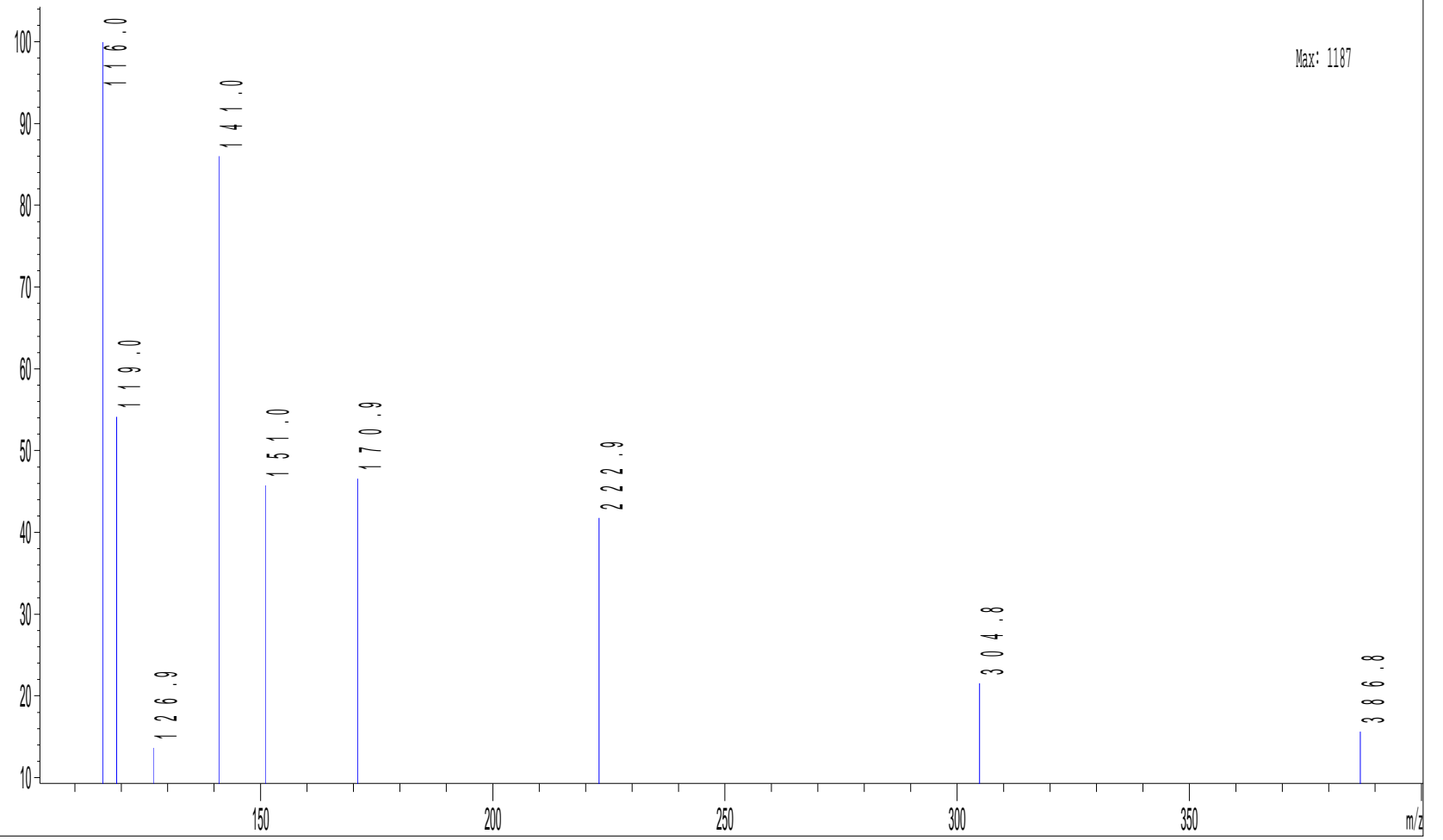
\*MSD1 SPC, time=3.050 of D:\DATA\TARR\20150820\_TARITAR1000014.D ES-API, Neg, Scan, Frag: 70



Max: 3193



\*MSD1 SPC, time=3.842 of D:\DATA\TARR\20150820\_TARITAR1000014.D ES-API, Neg, Scan, Frag: 70

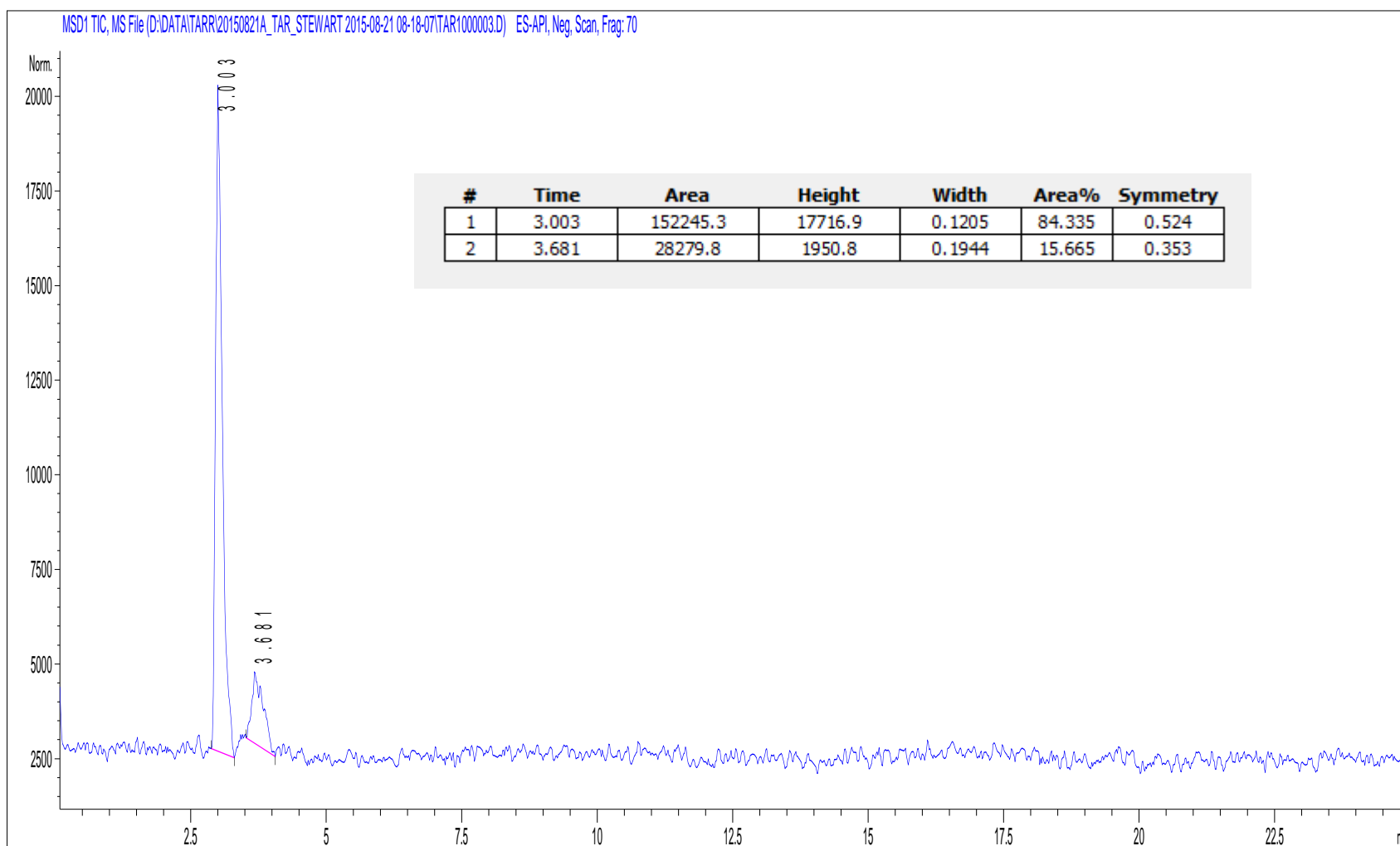


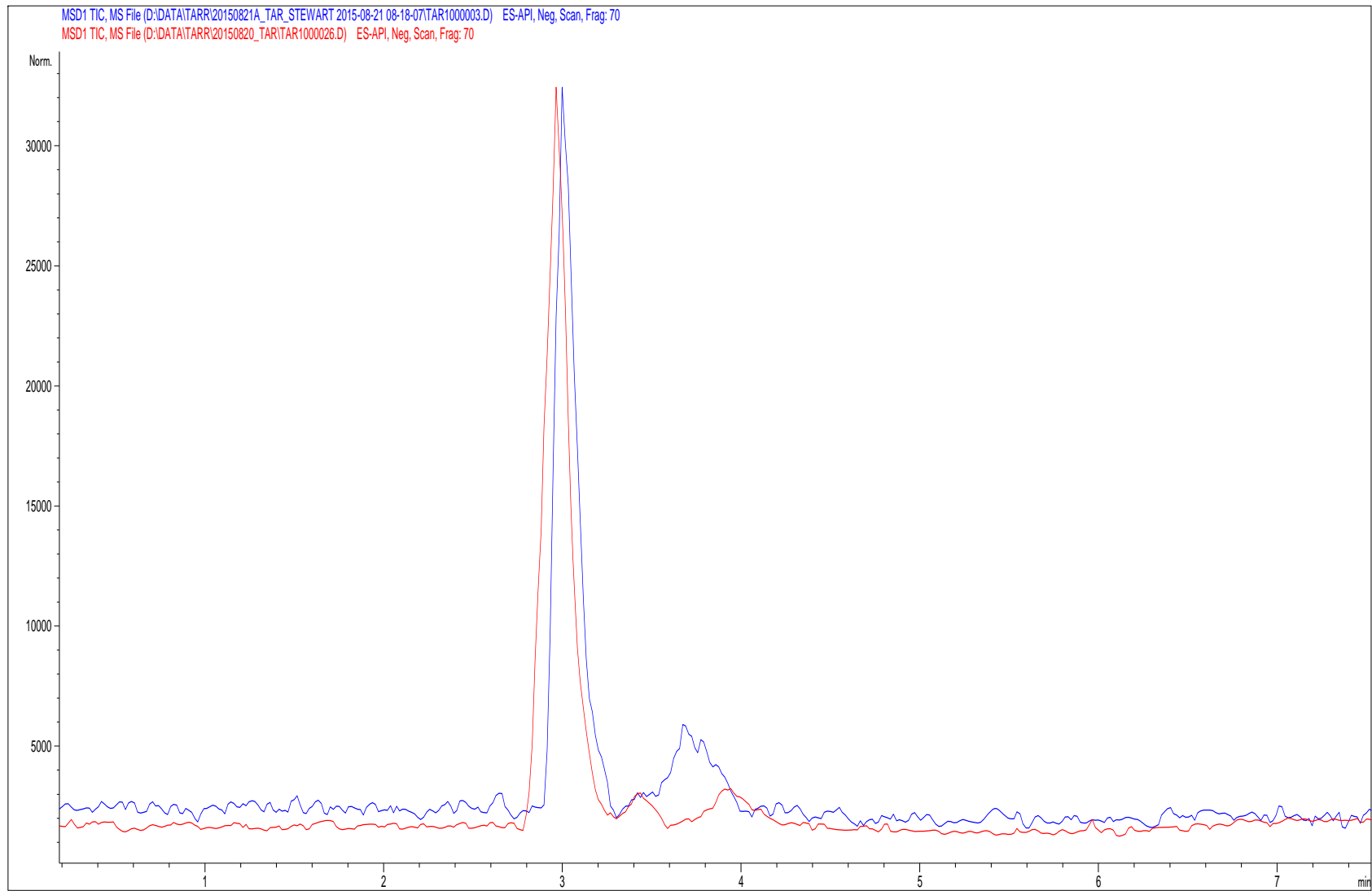
11-Aug-15

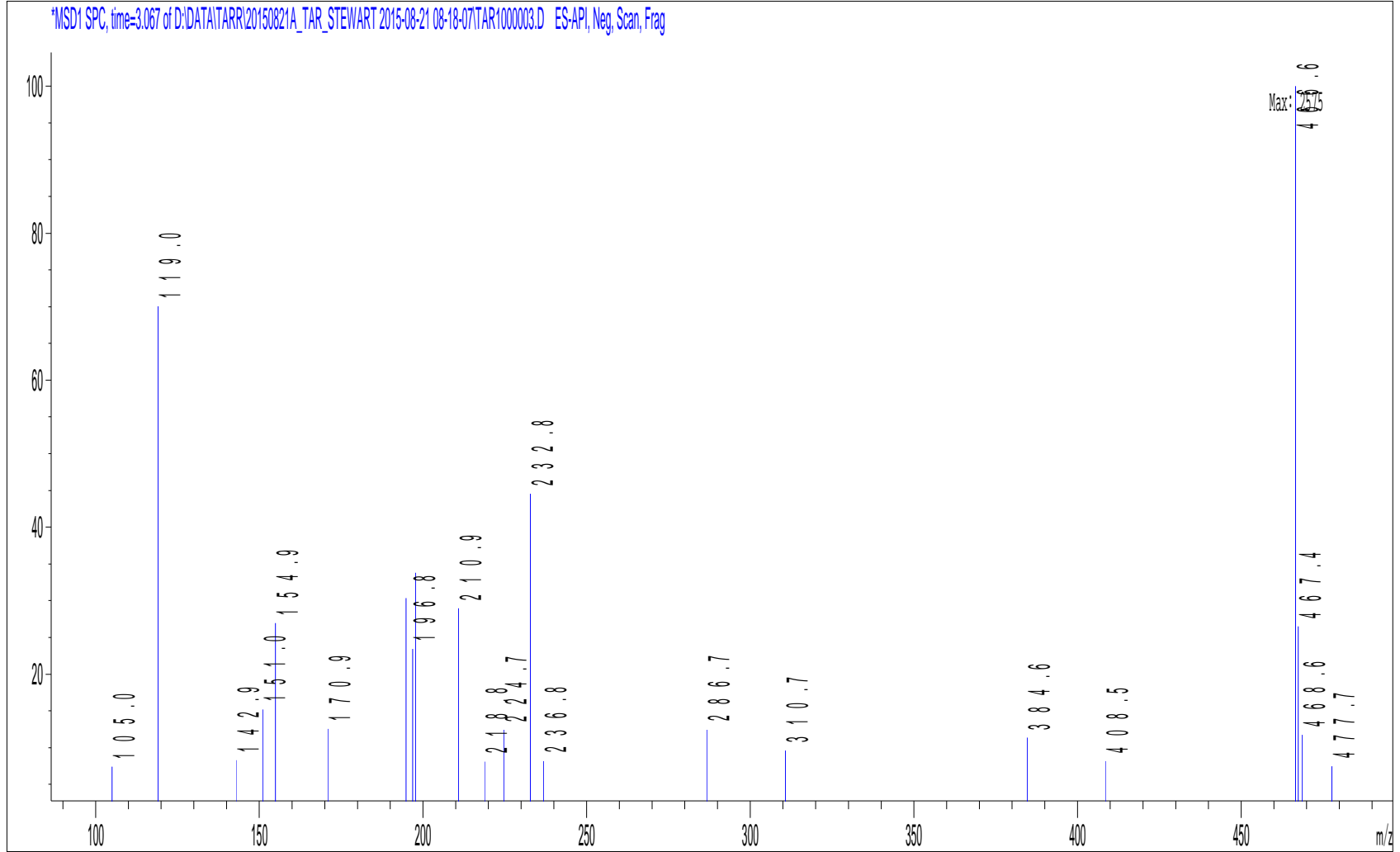
50 DC

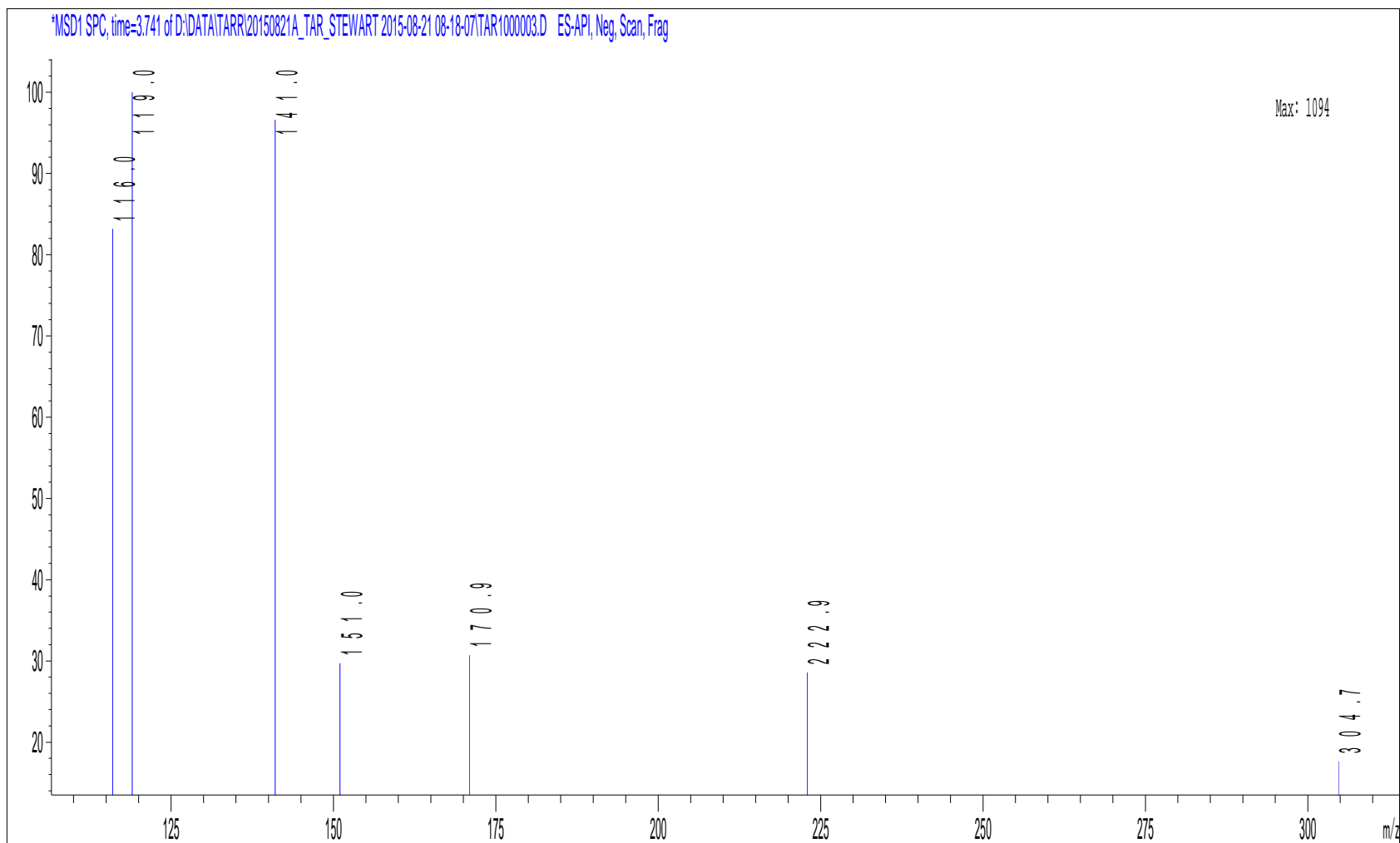
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P2-E-02









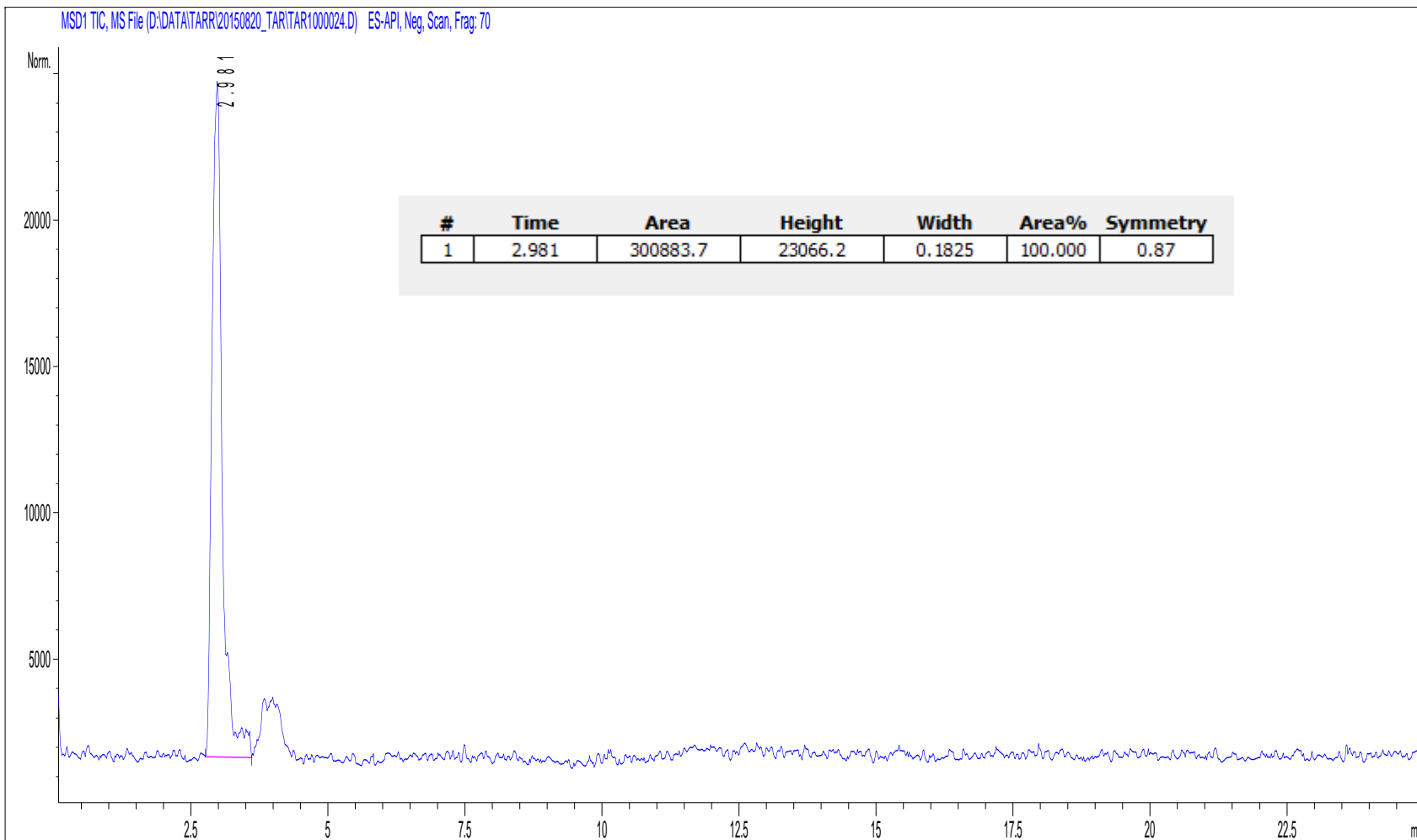


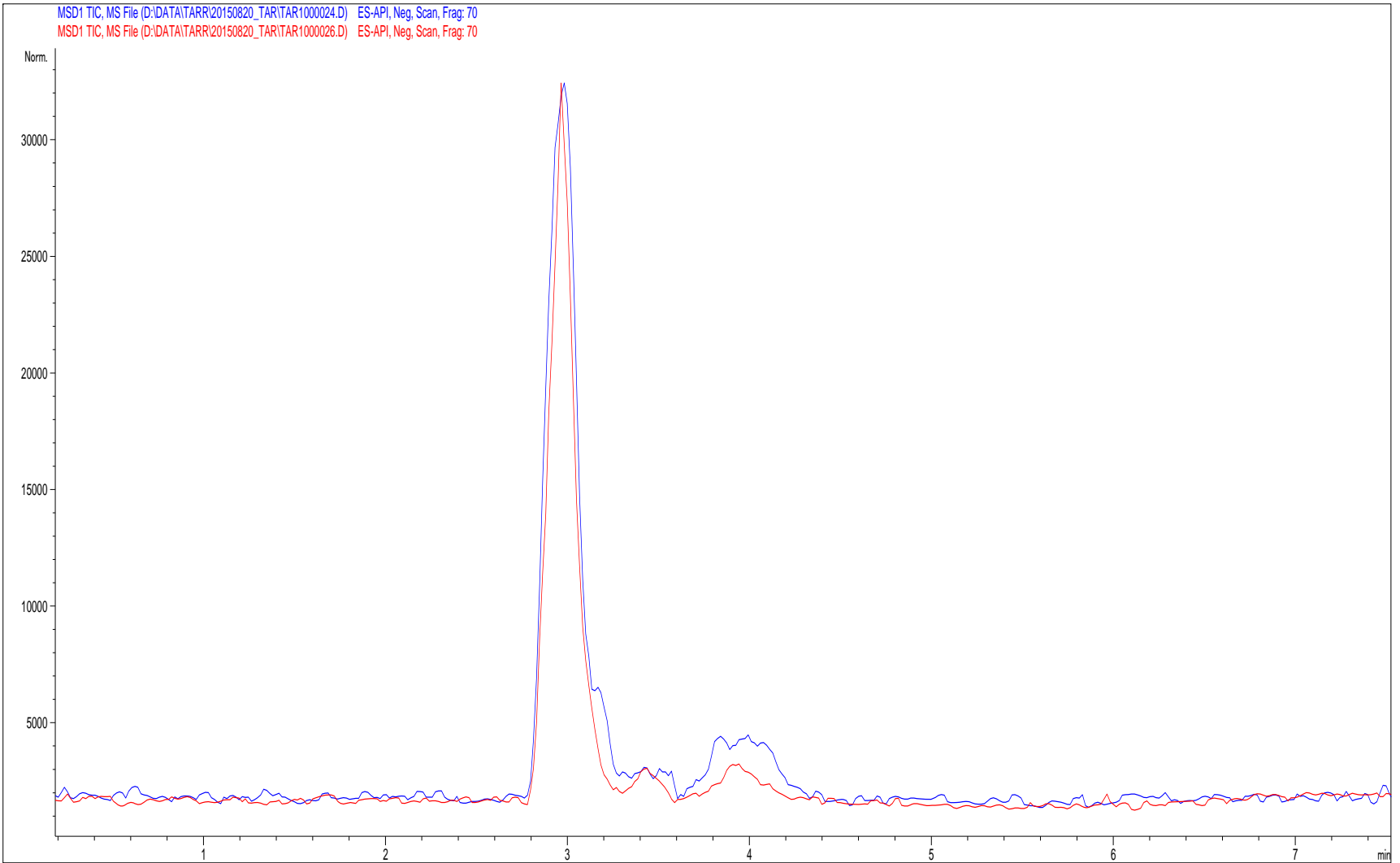
13-Jul-15

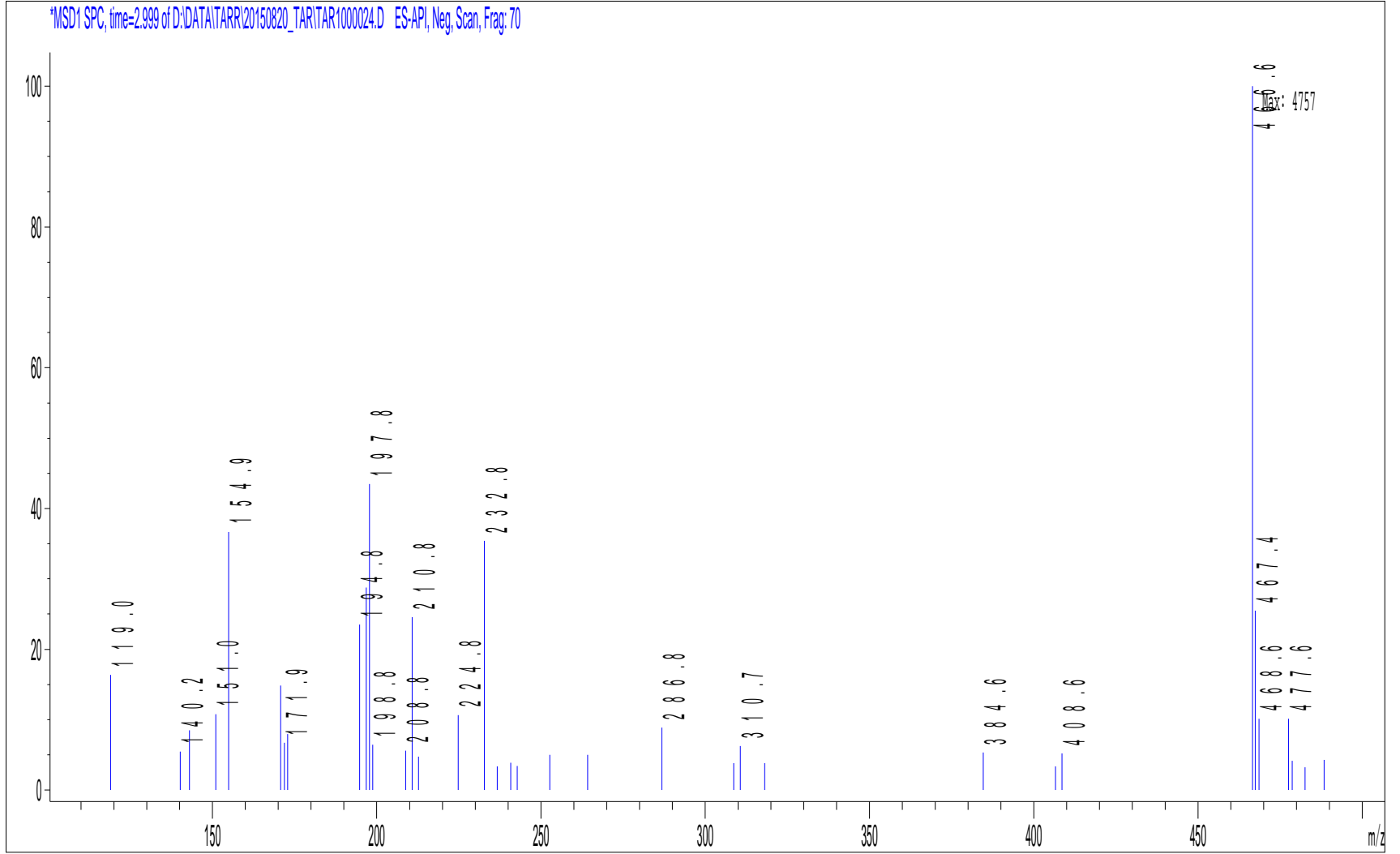
70 DC

7

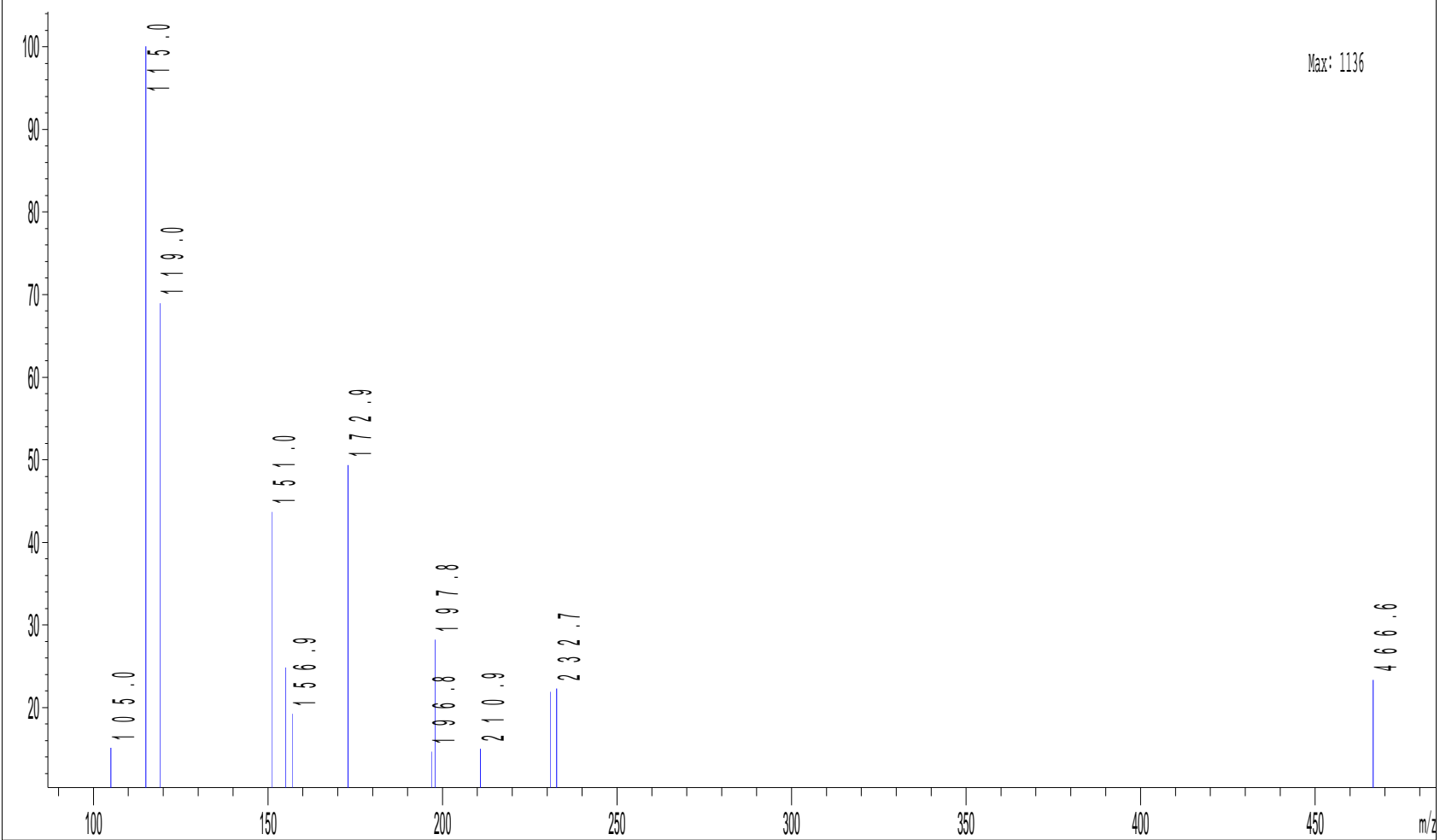
P2-C-06

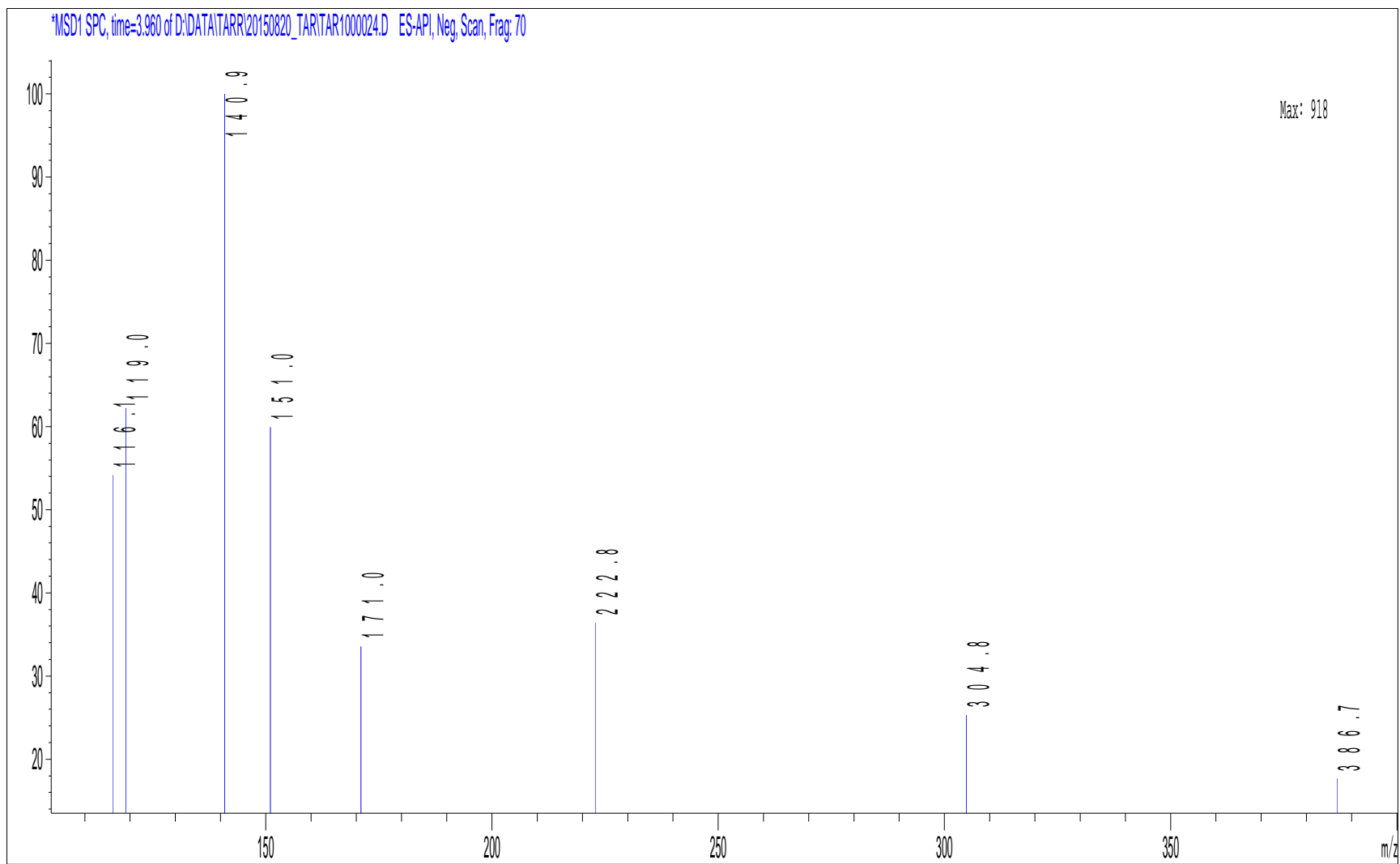






\*MSD1 SPC, time=3.185 of D:\DATA\TARR\20150820\_TARITAR1000024.D ES-API, Neg, Scan, Frag: 70



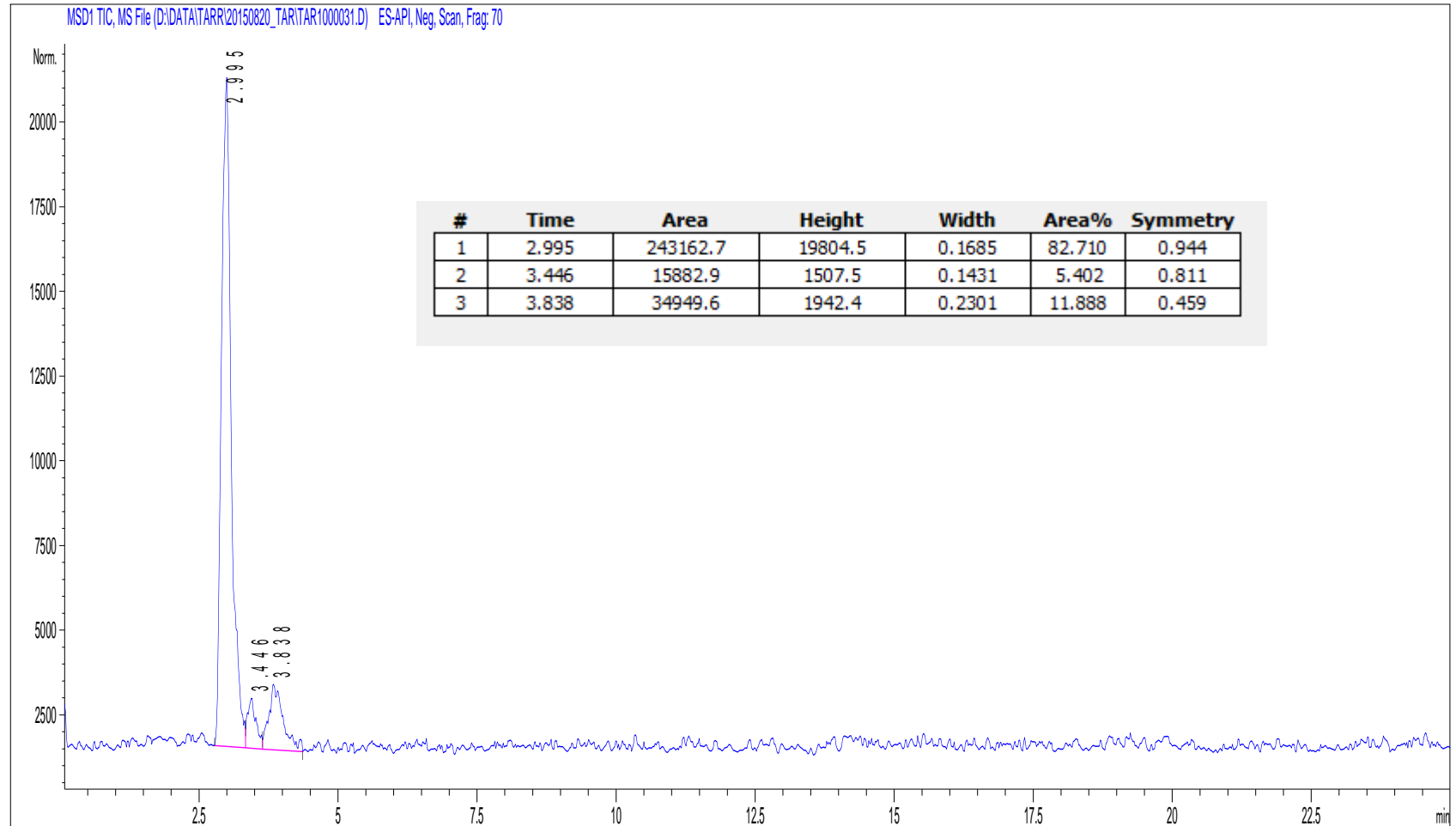


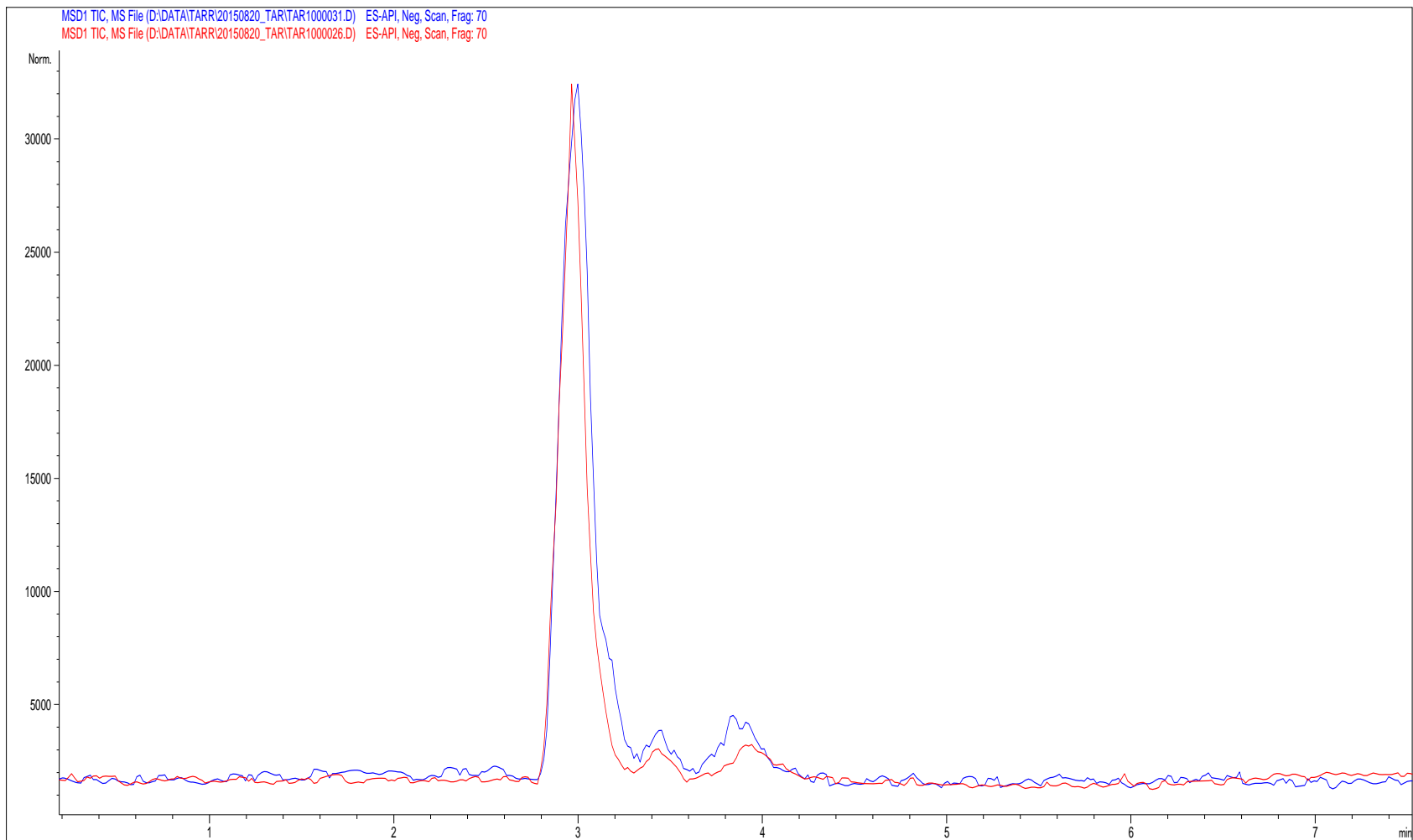
30-Jul-15

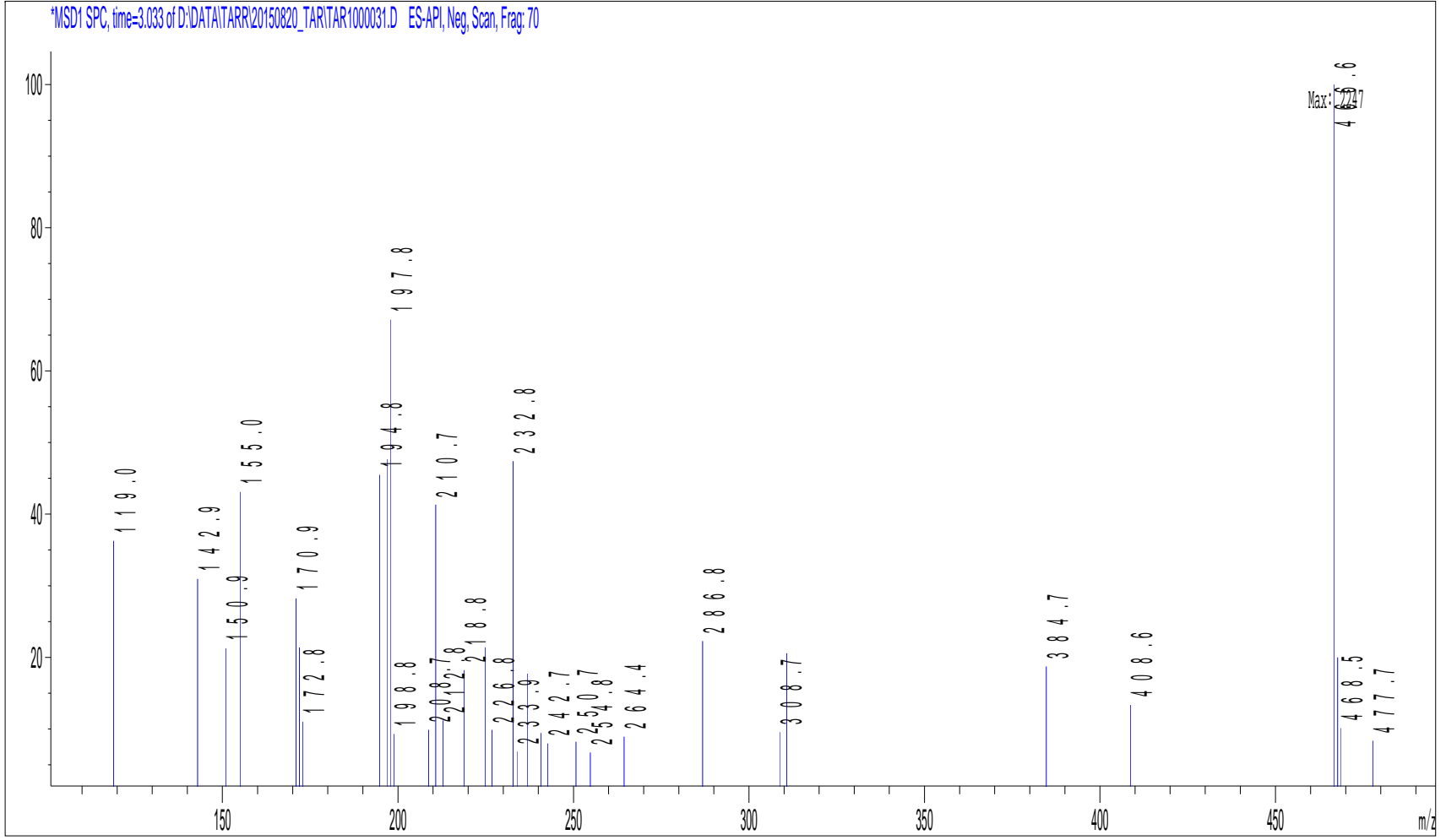
100 DC

7

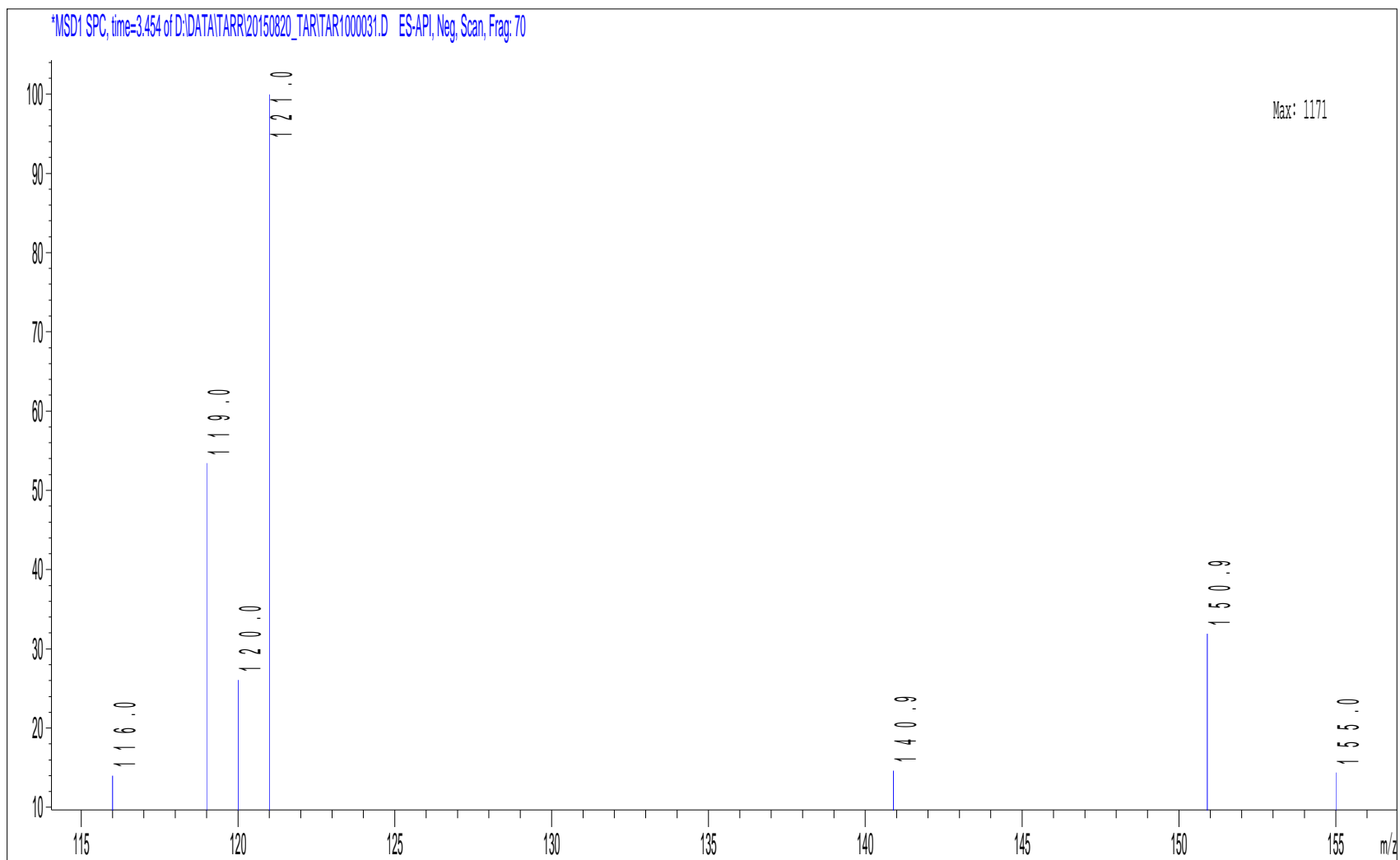
P2-D-06

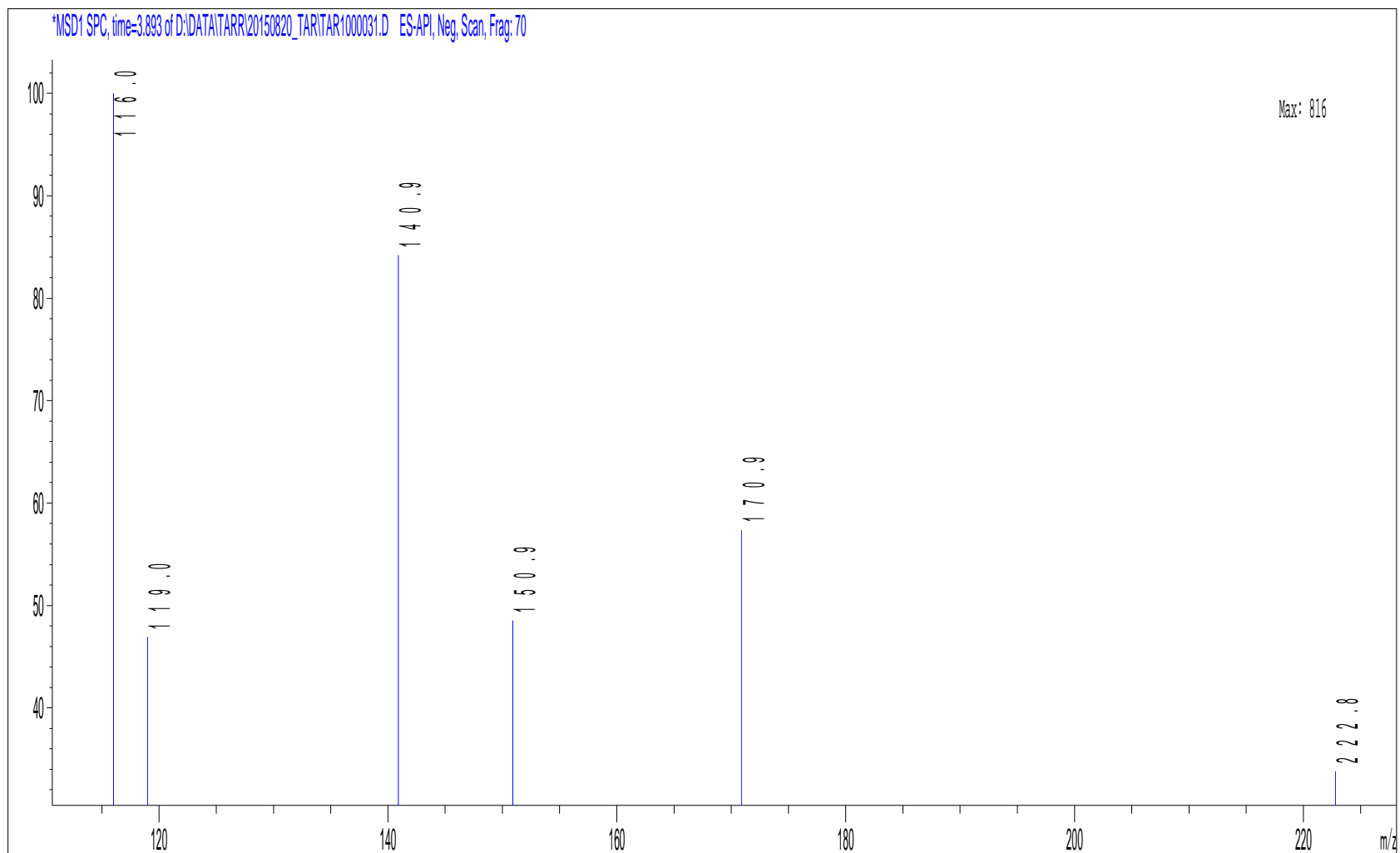










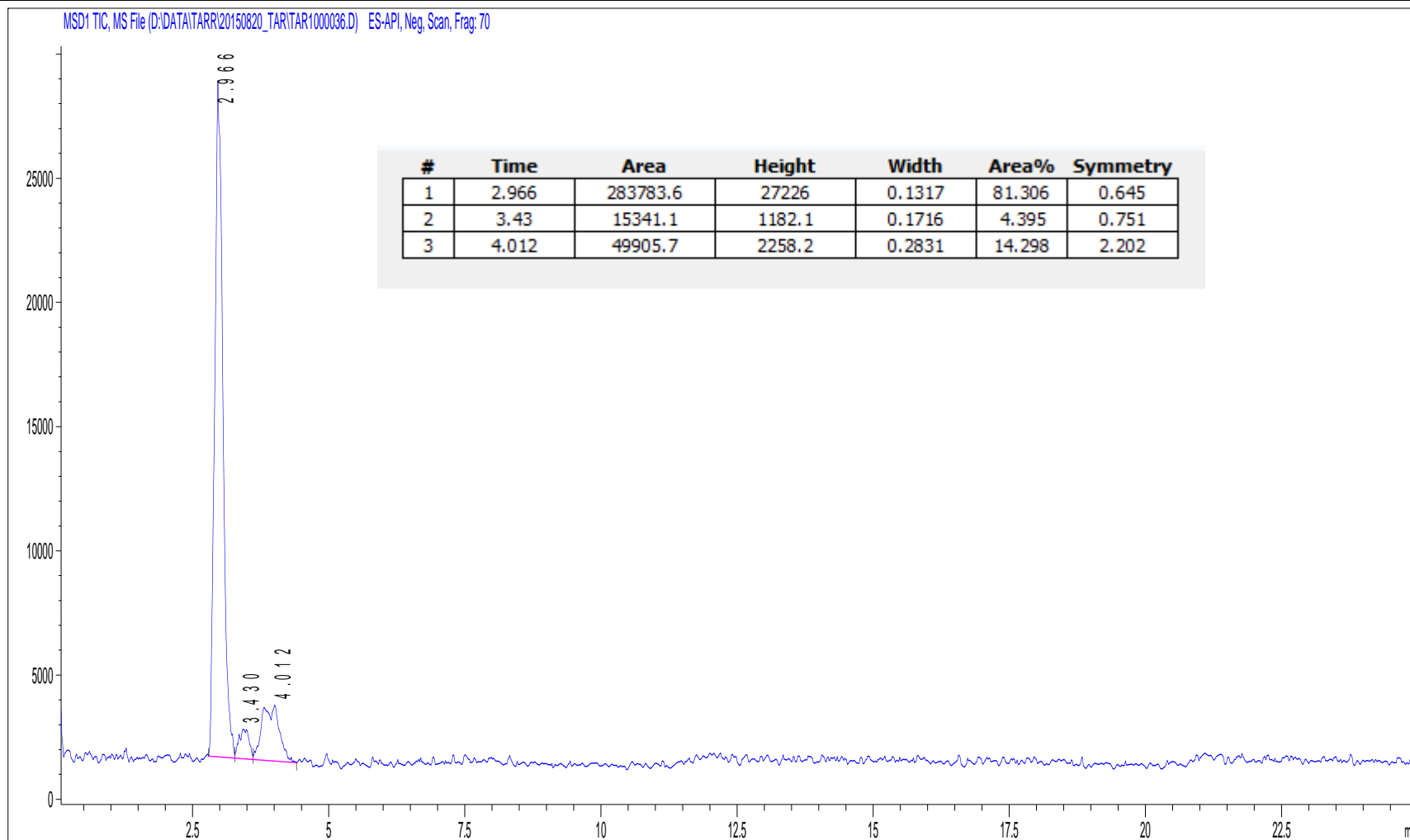


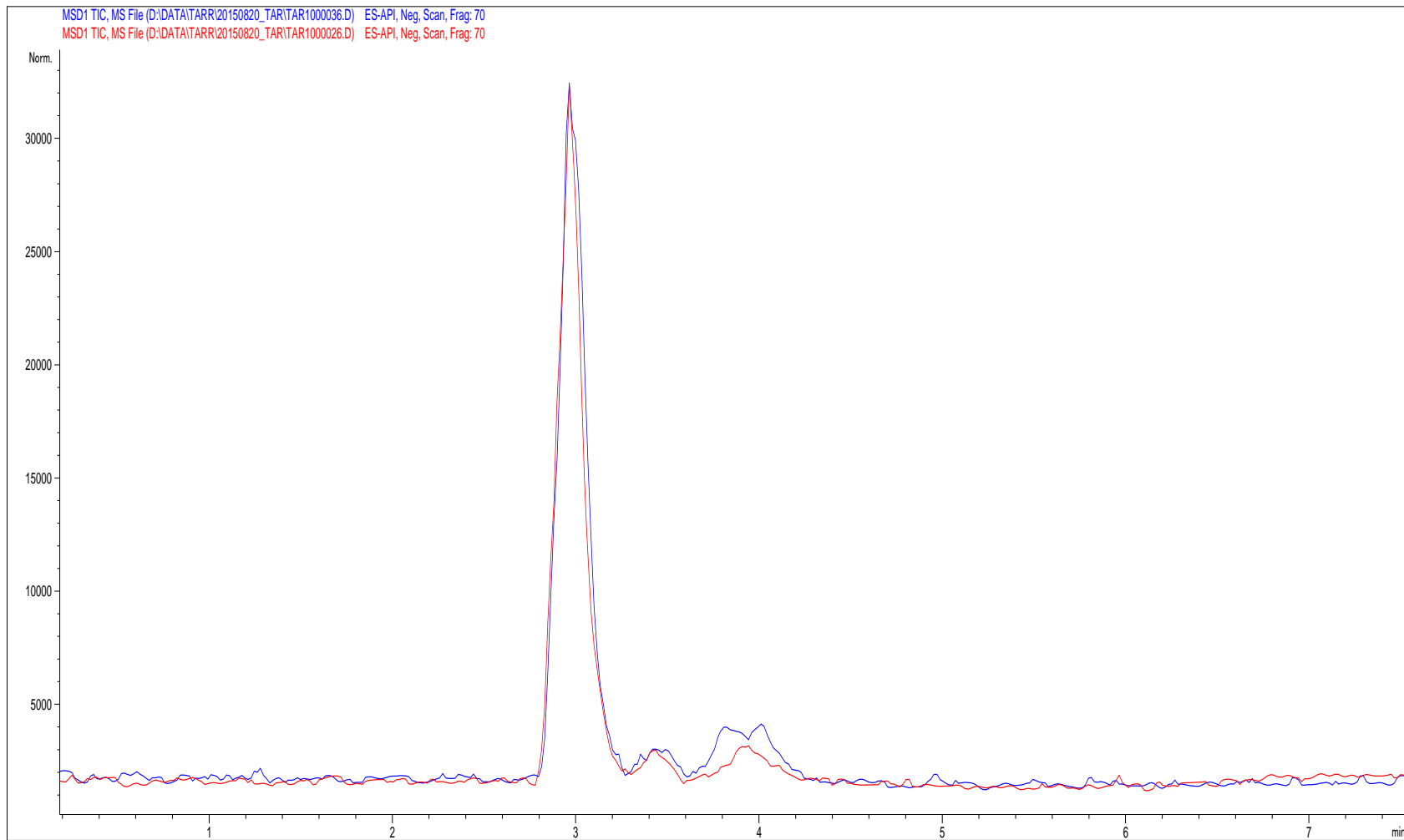
16-Jul-15

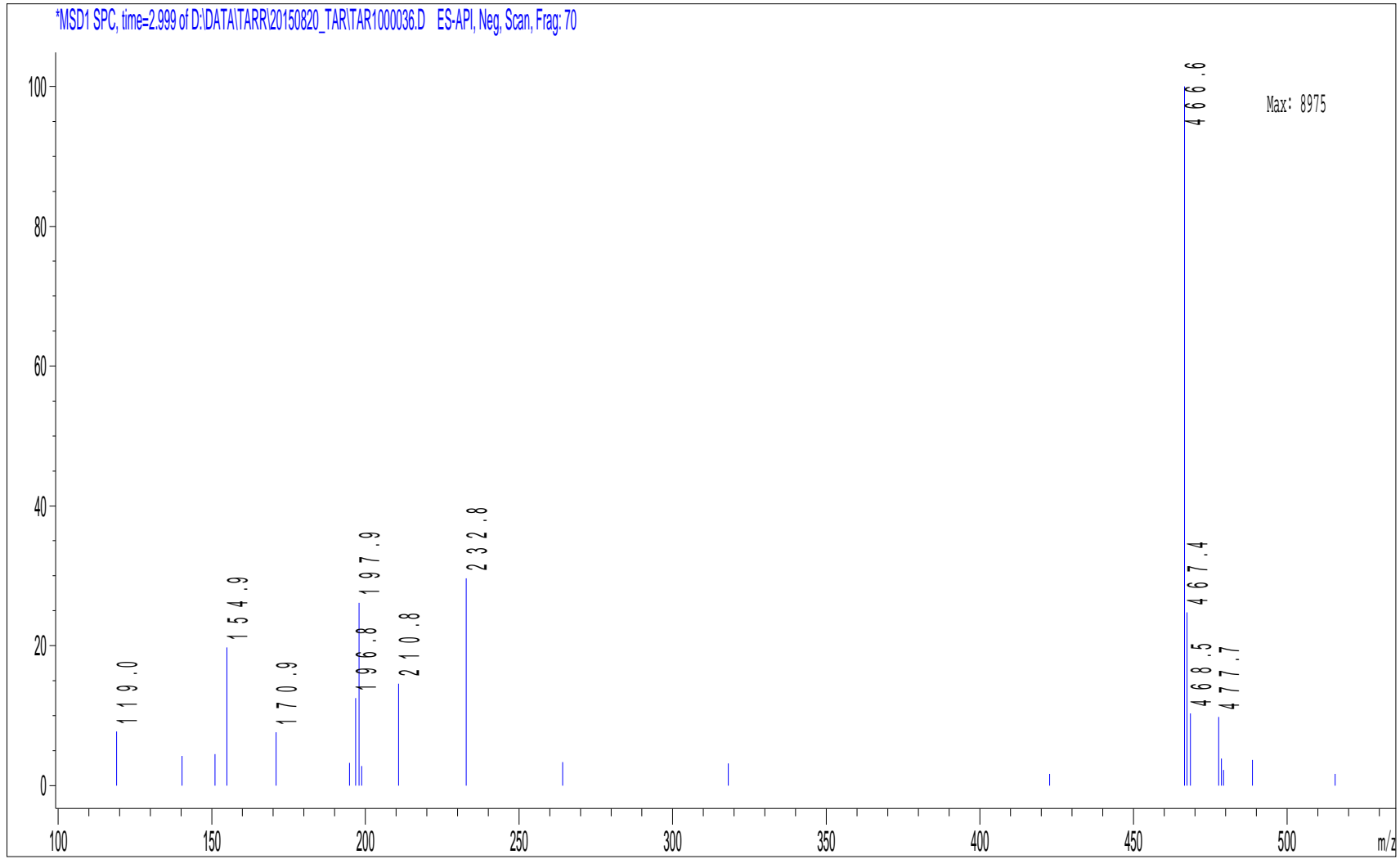
100 DC Problem no removal

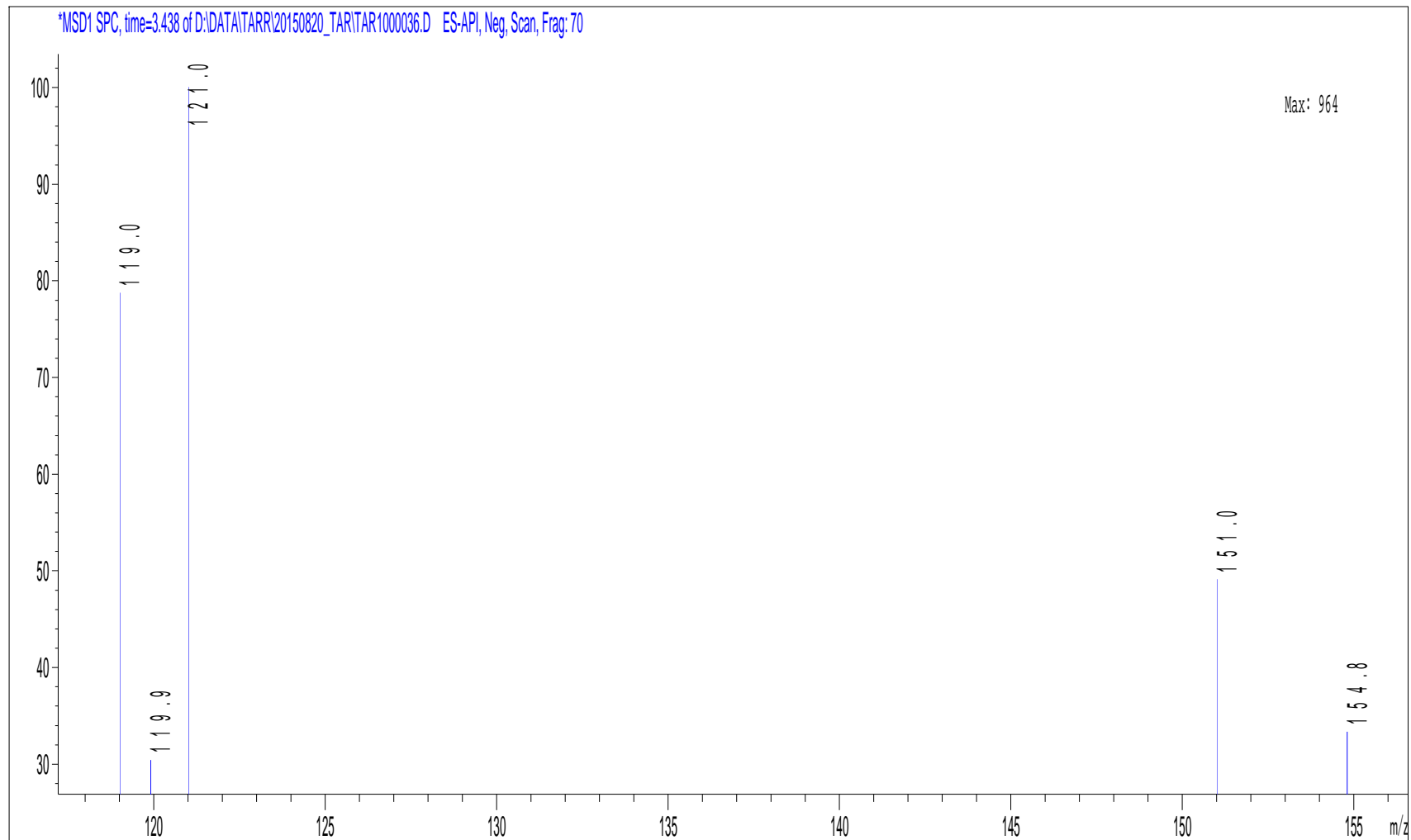
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P2-D-01

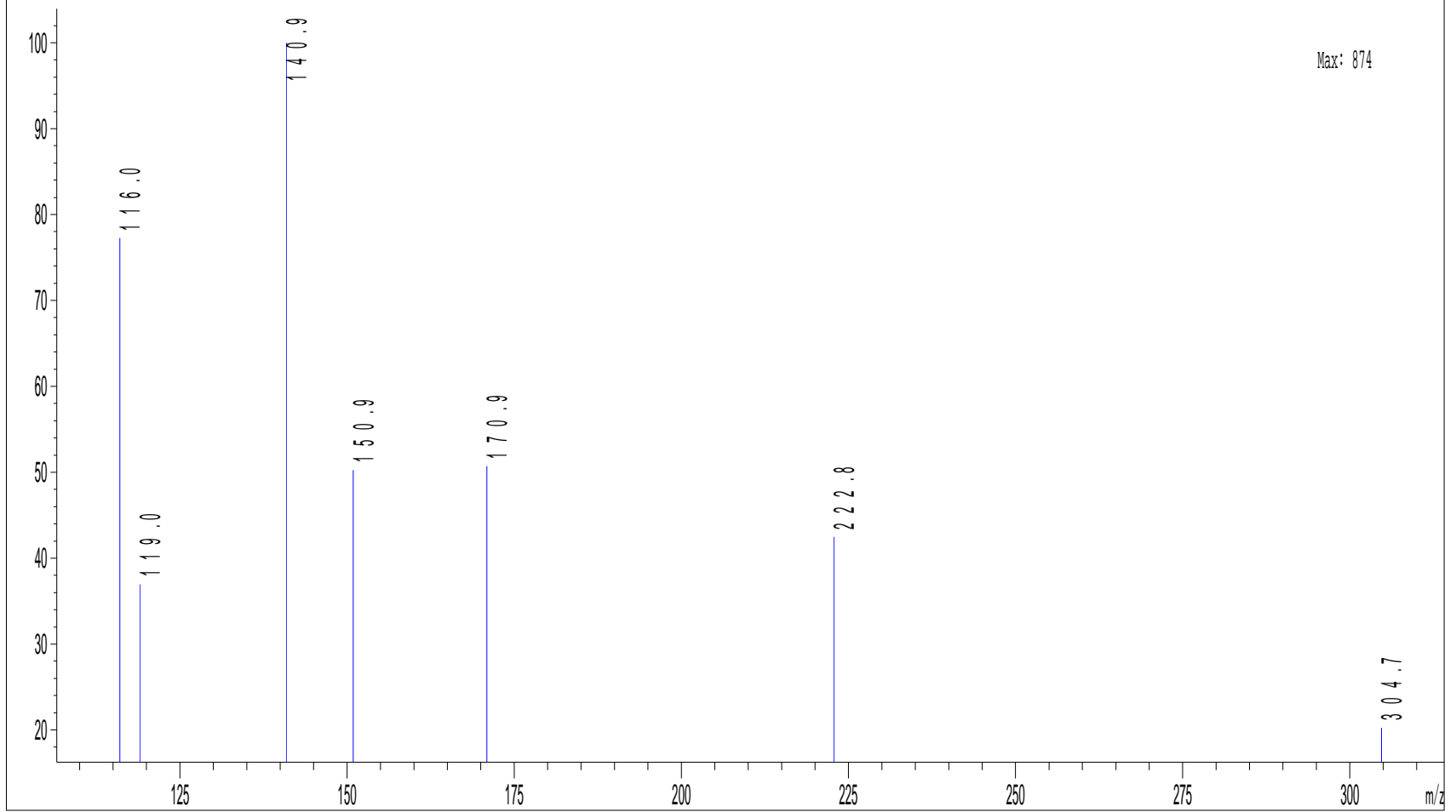






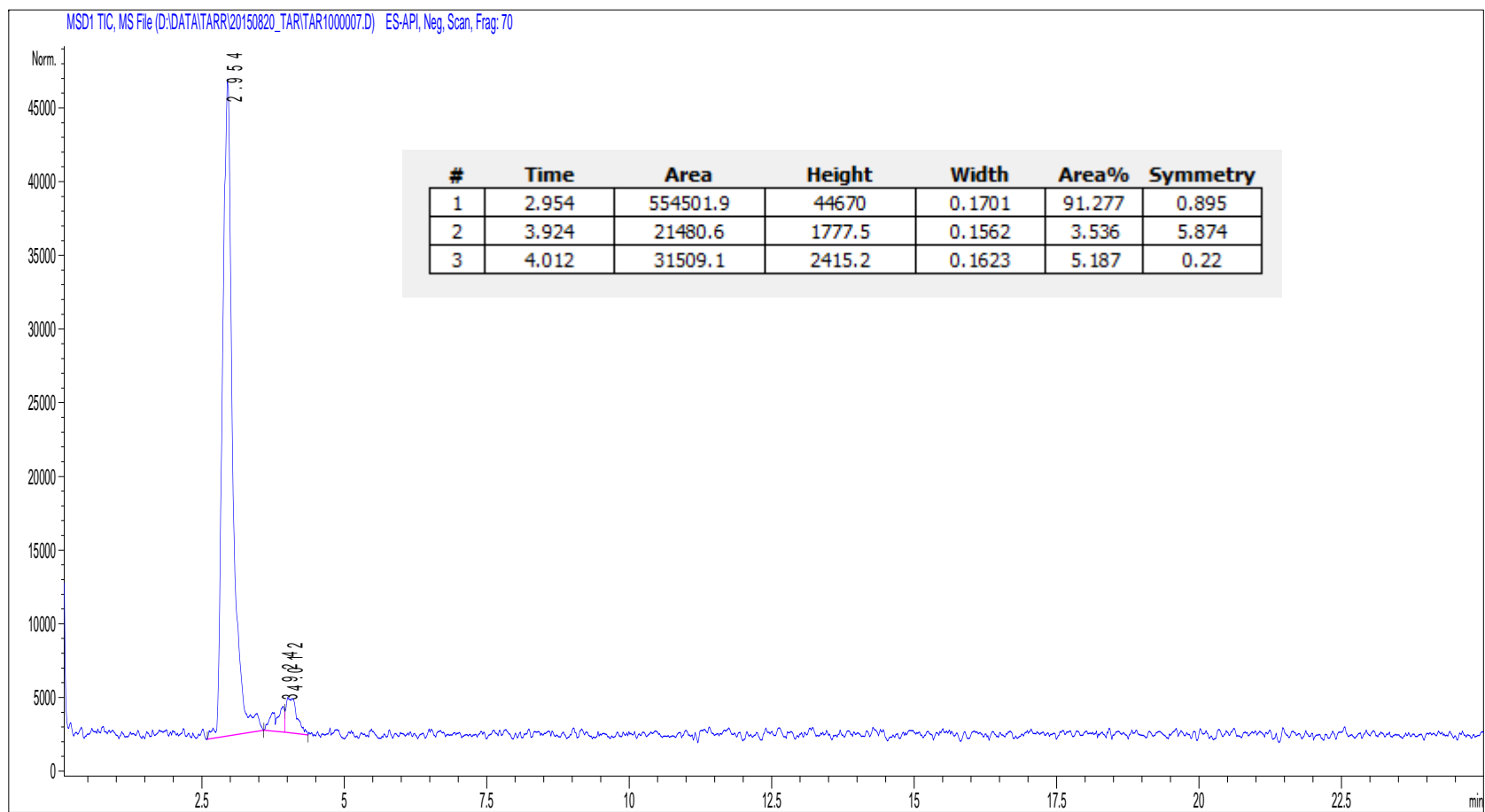


\*MSD1 SPC, time=3.926 of D:\DATA\TARRI\20150820\_TARITAR1000036.D ES-API, Neg, Scan, Frag: 70



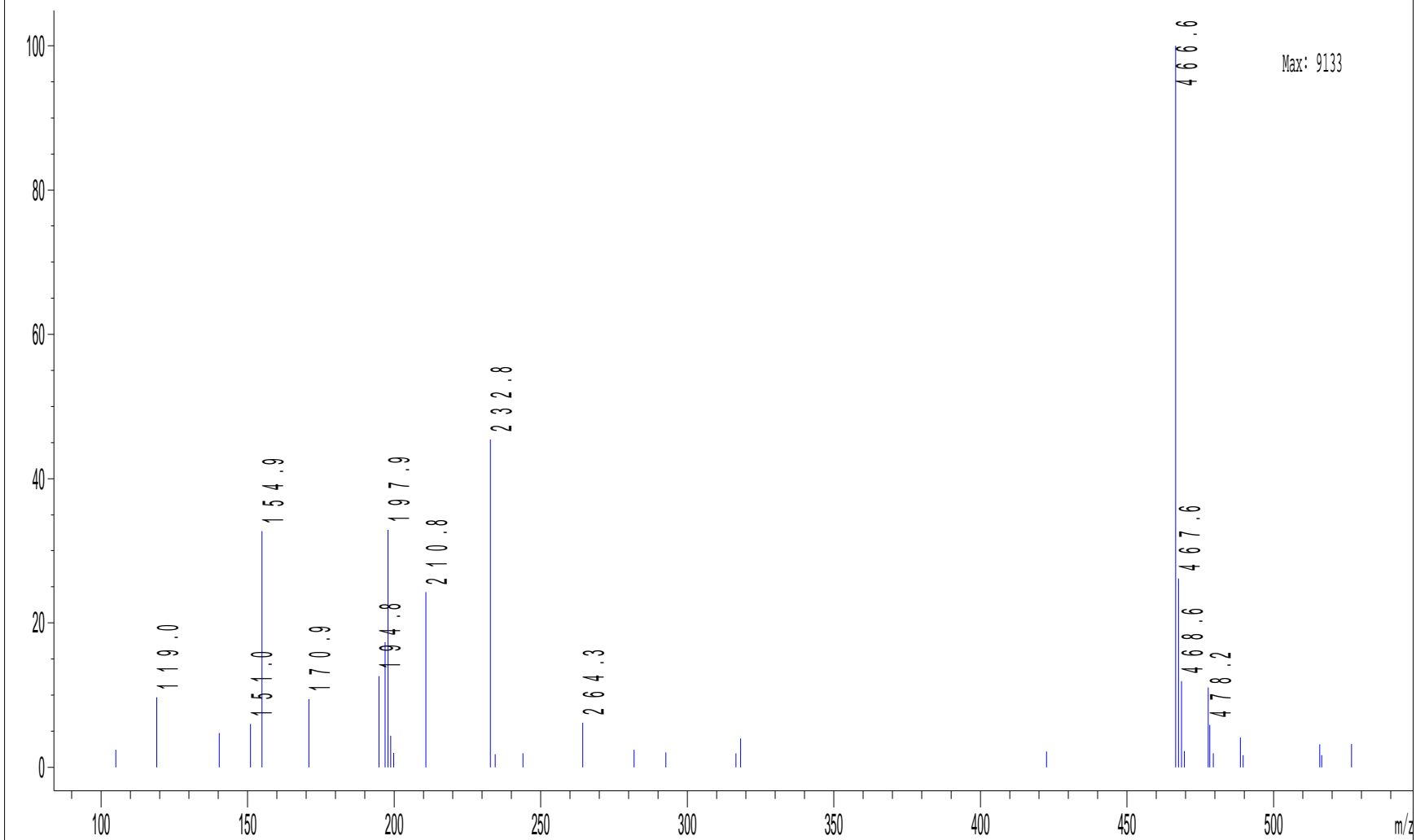
# pH 8

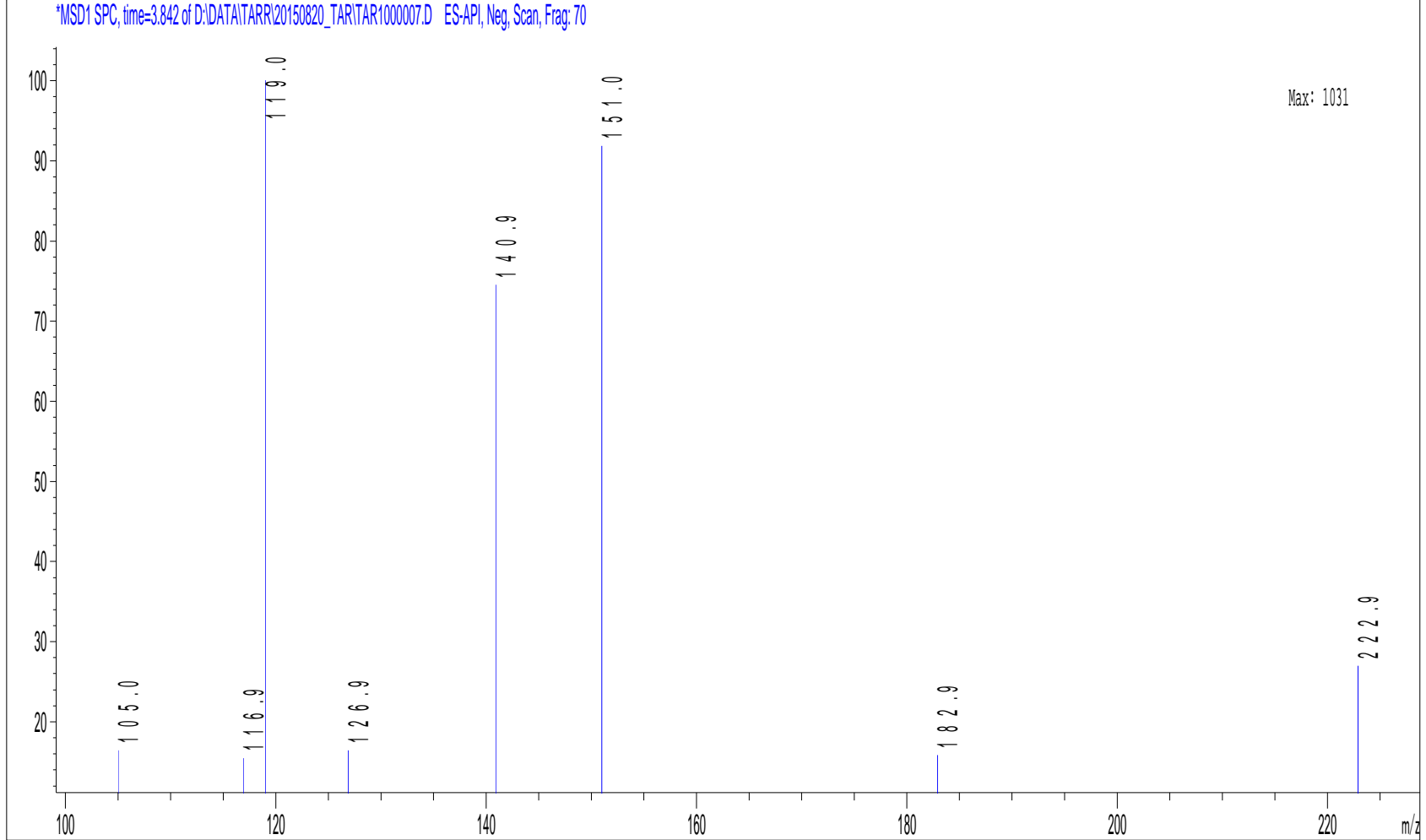
16-Apr-15  
H2O2 Ctrl  
8  
P2-A-07

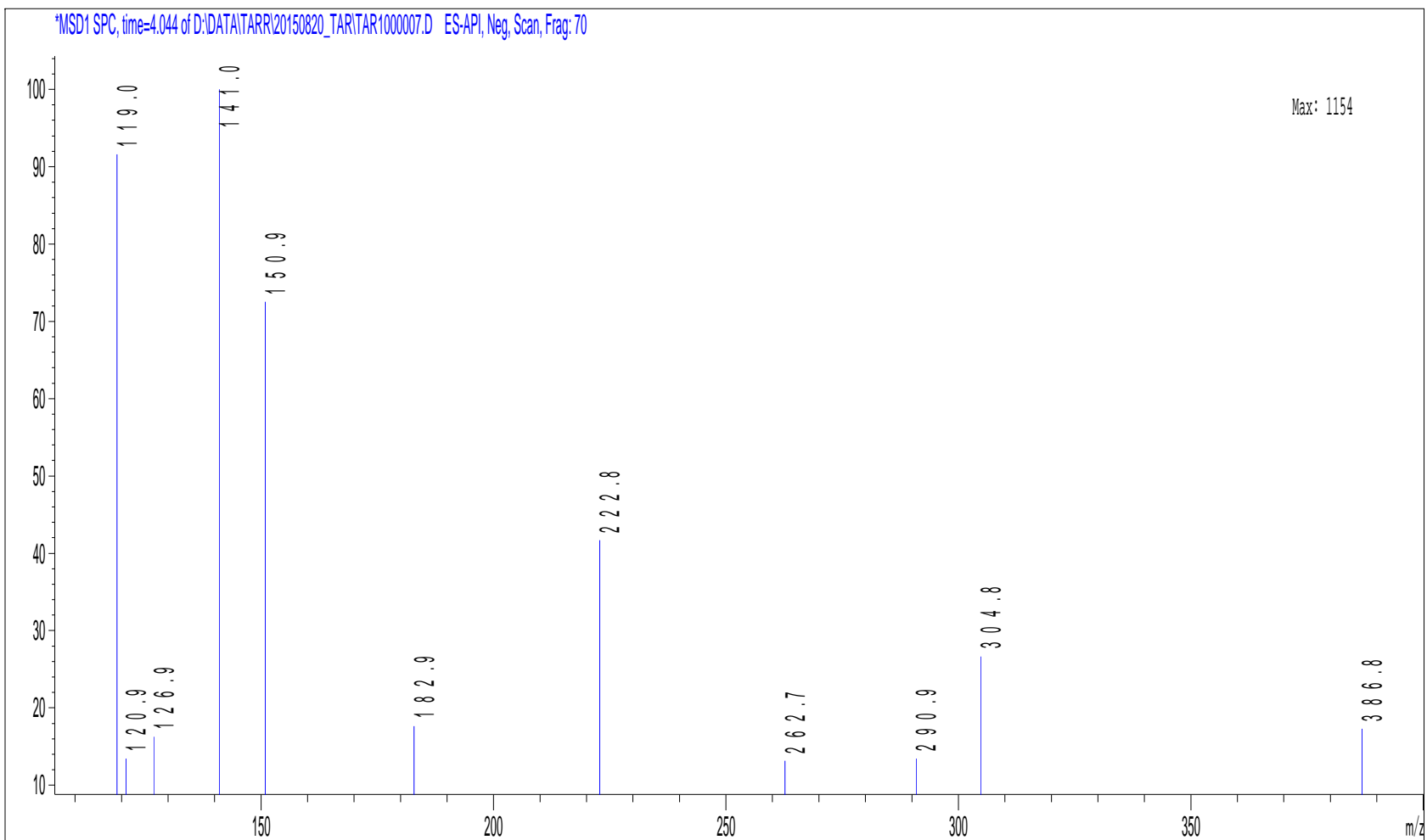




\*MSD1 SPC, time=2.999 of D:\DATA\TARR\20150820\_TARITAR1000007.D ES-API, Neg, Scan, Frag: 70





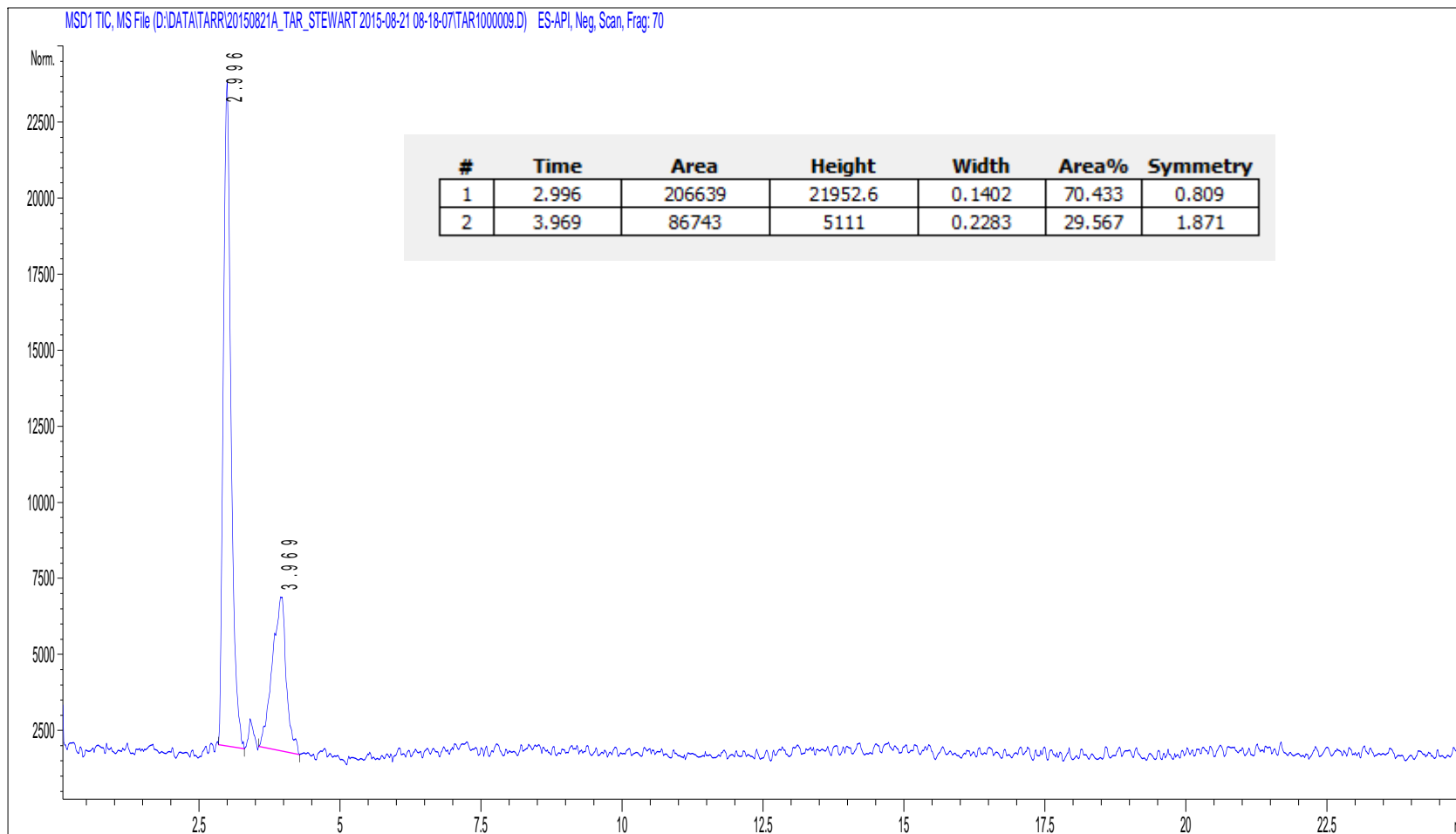


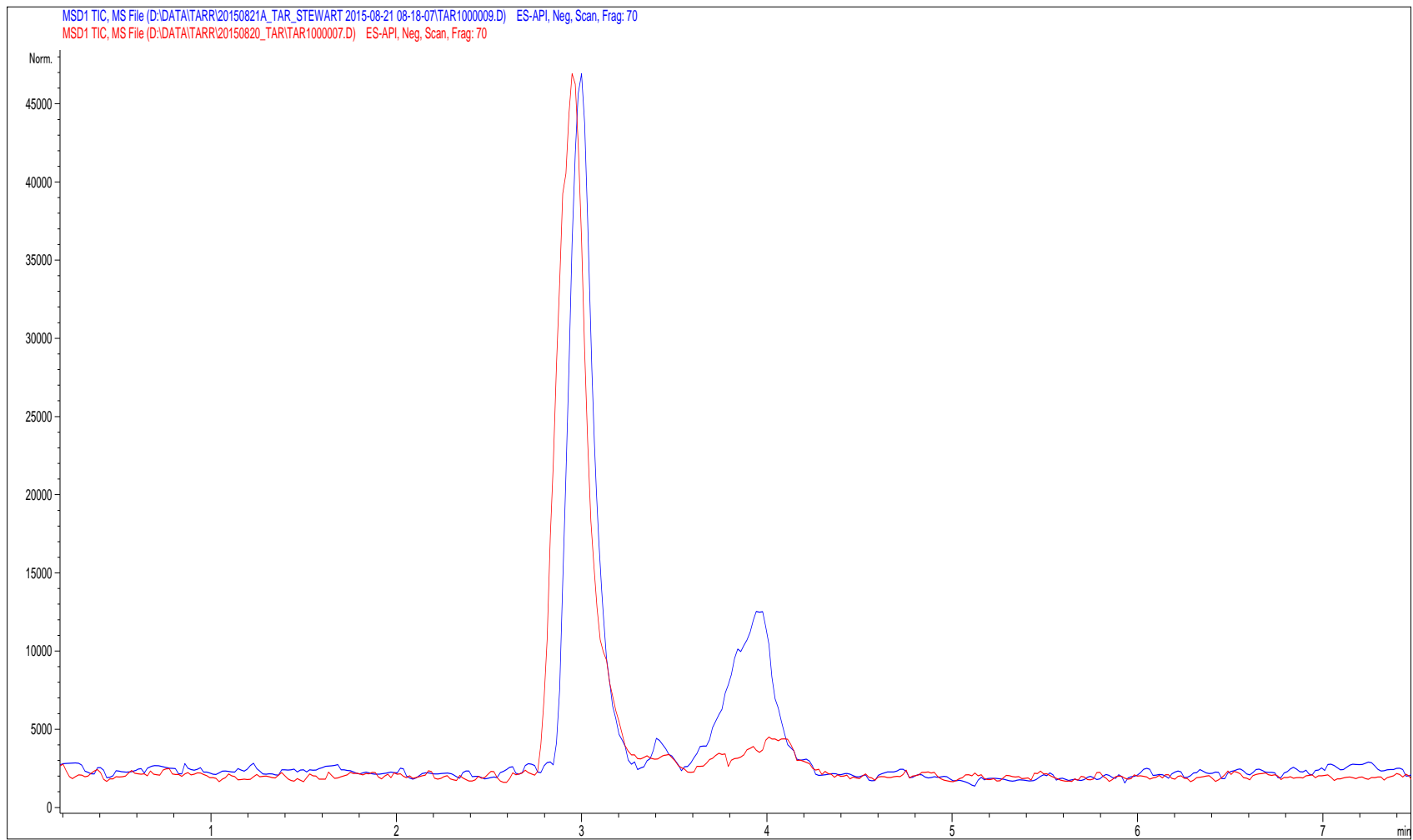
15-Jul-15

0 DC

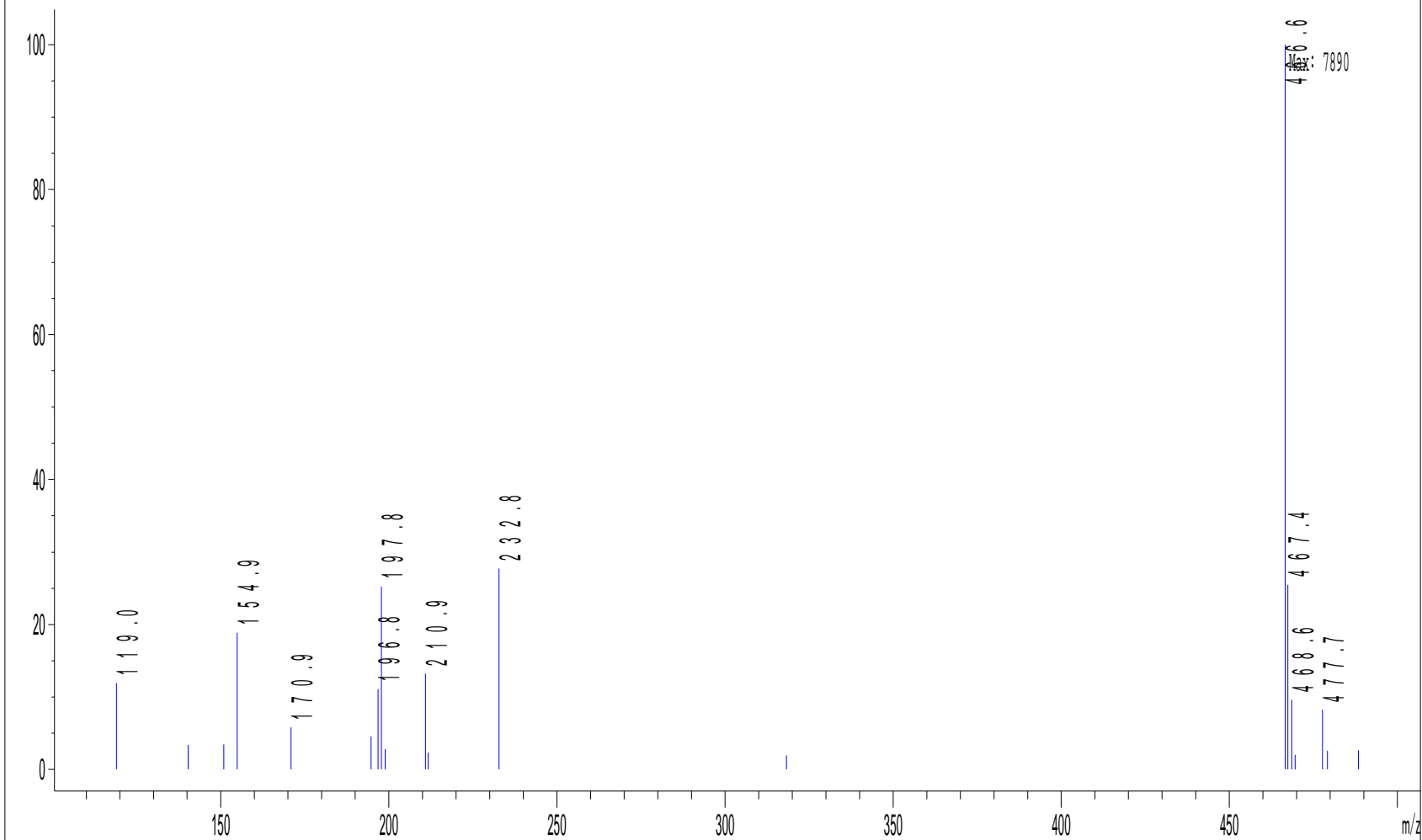
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P2-E-08

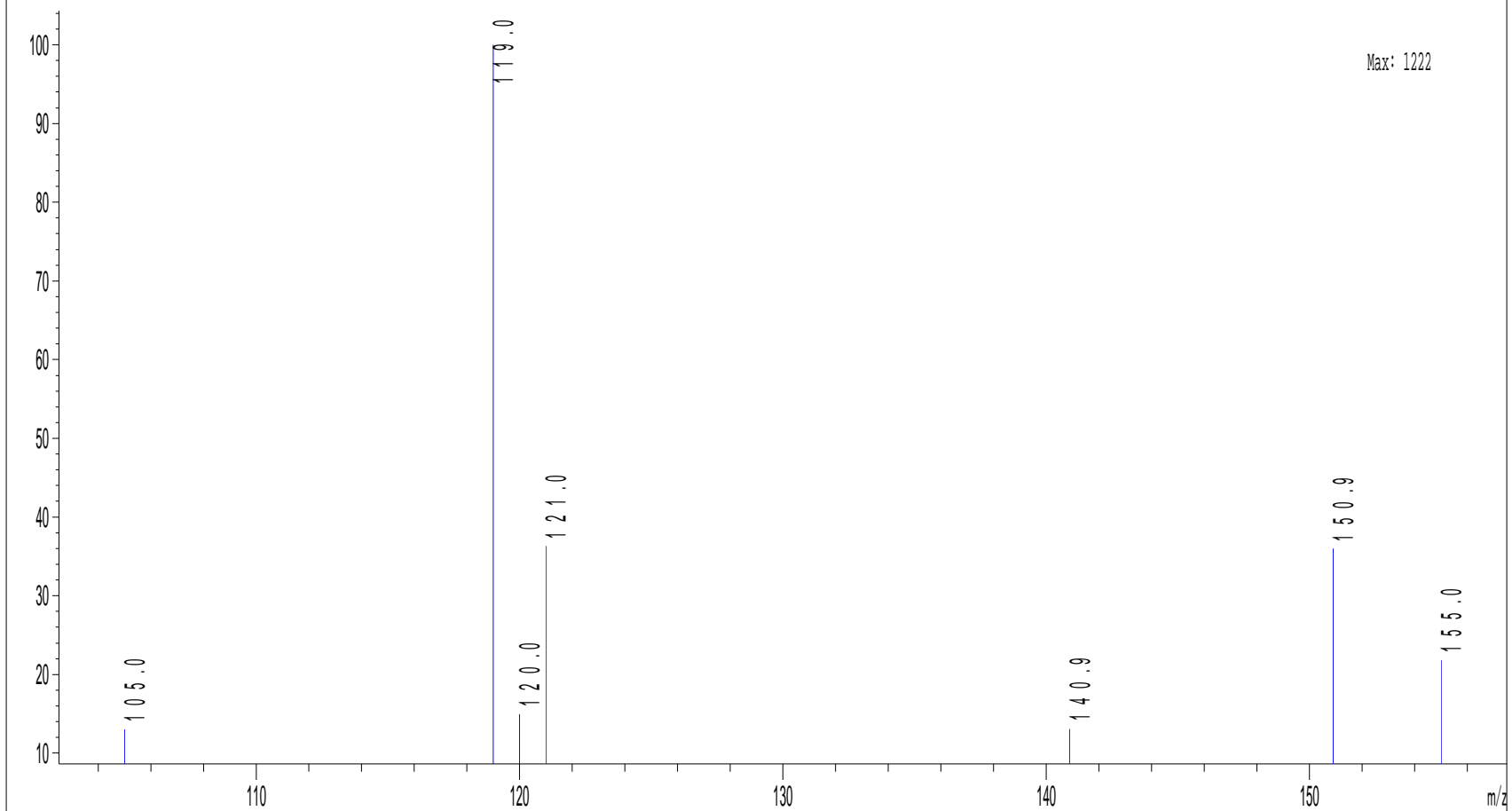


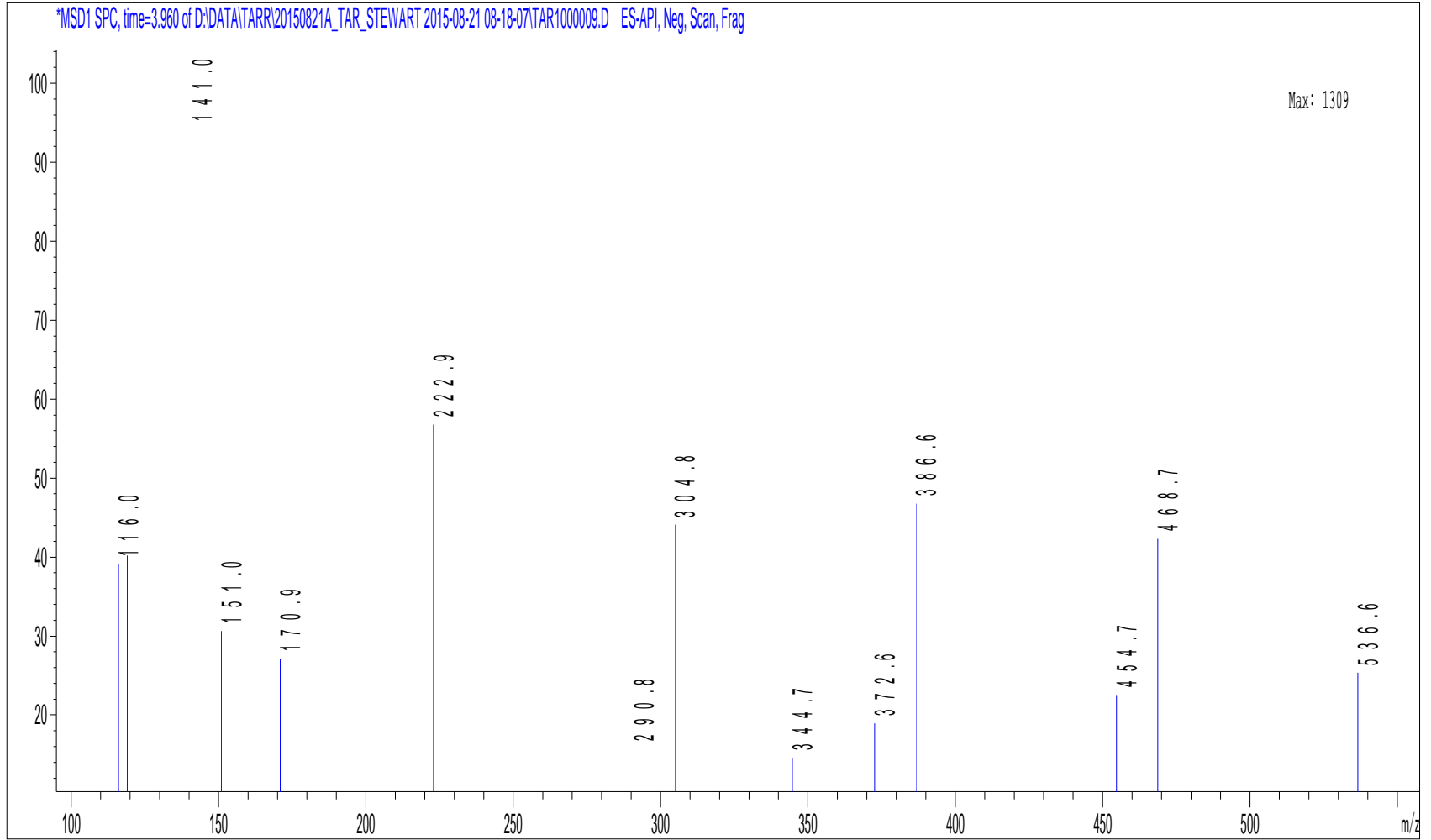


\*MSD1 SPC, time=3.016 of D:\DATA\TARR\20150821A\_TAR\_STEWART 2015-08-21 08-18-07\TAR1000009.D ES-API, Neg, Scan, Frag



\*MSD1 SPC, time=3.404 of D:\DATA\TARR\20150821A\_TAR\_STEWART 2015-08-21 08-18-07\TAR1000009.D ES-API, Neg. Scan, Frag





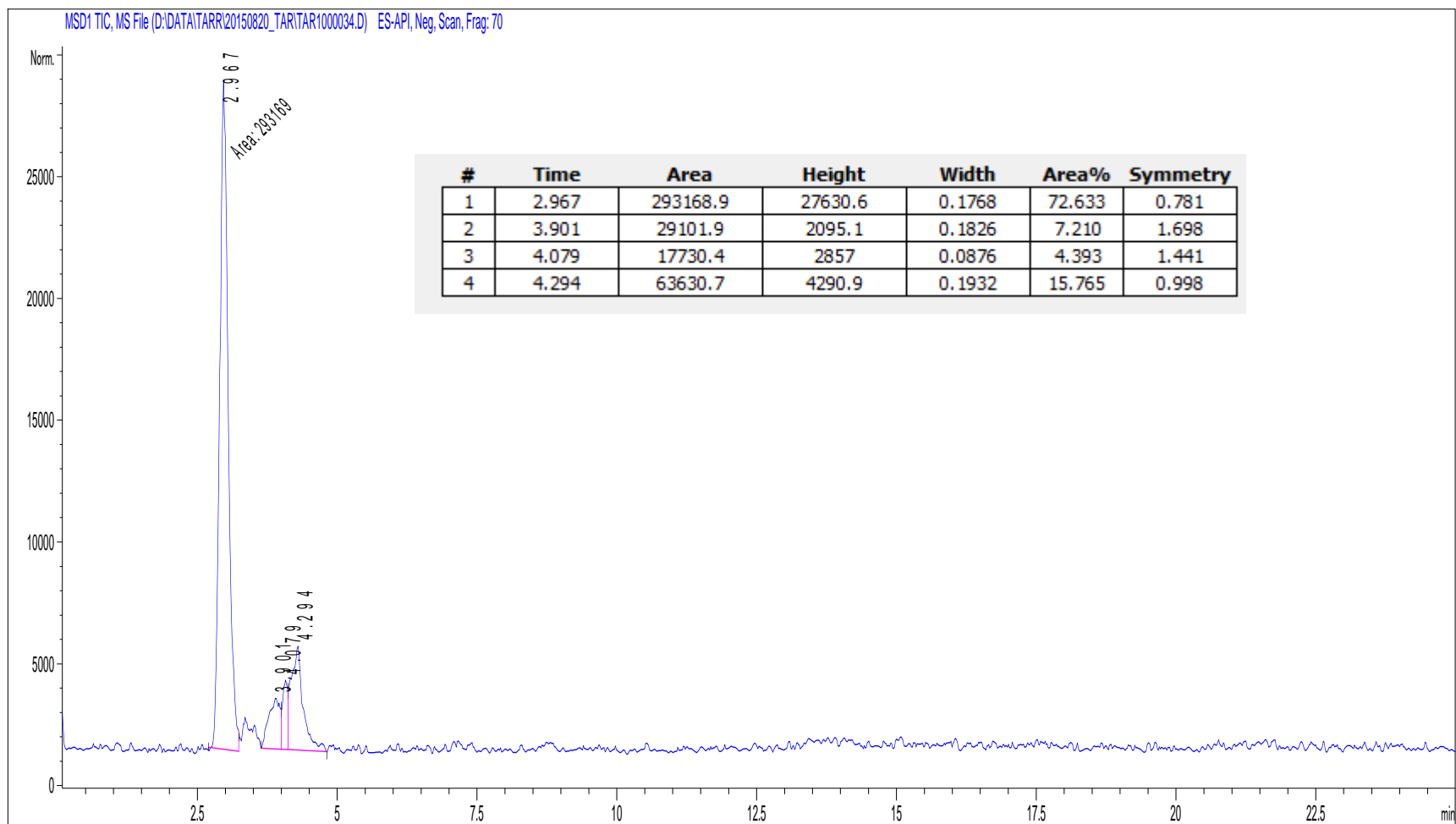


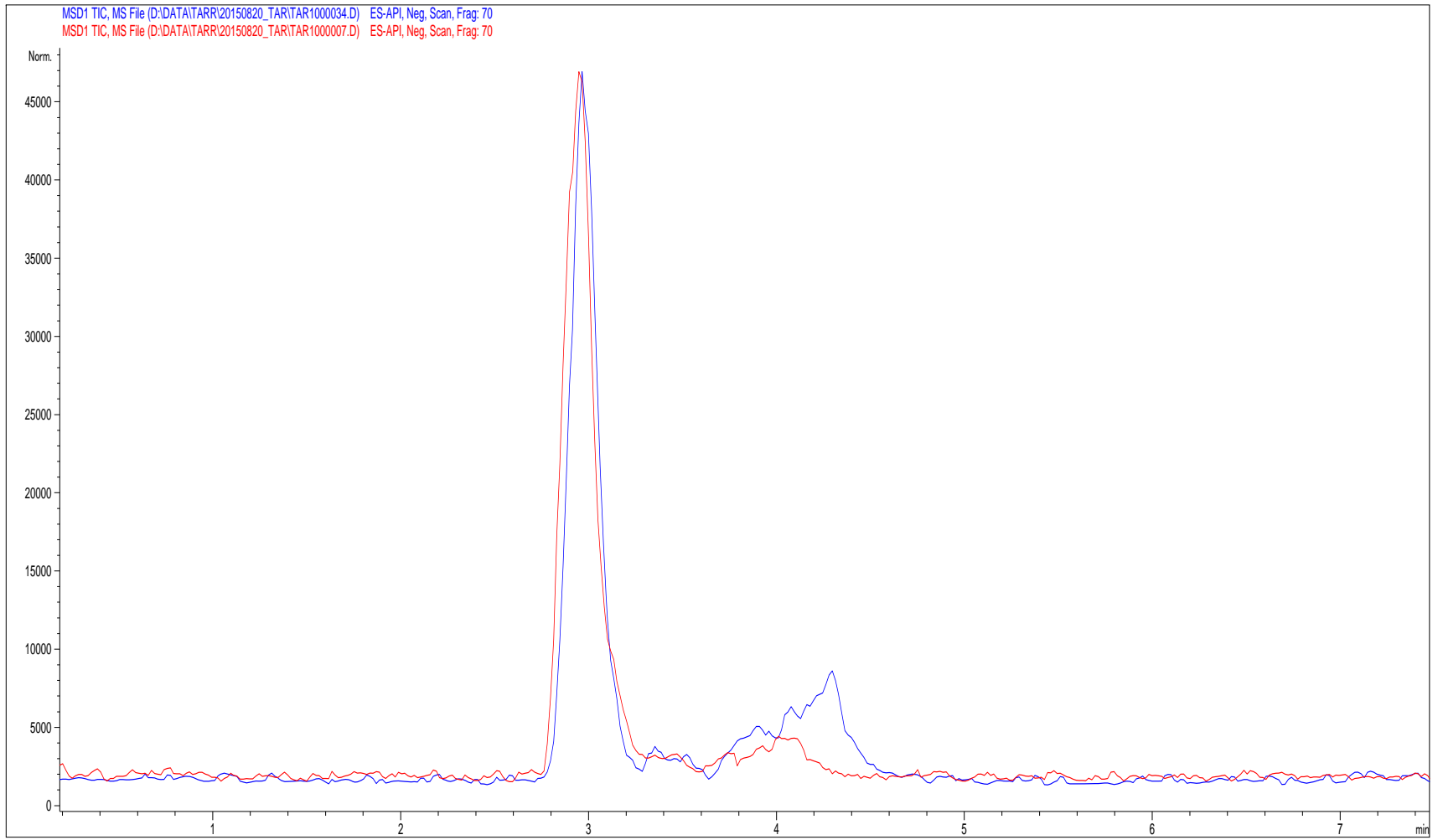
21-Jul-15

5 DC

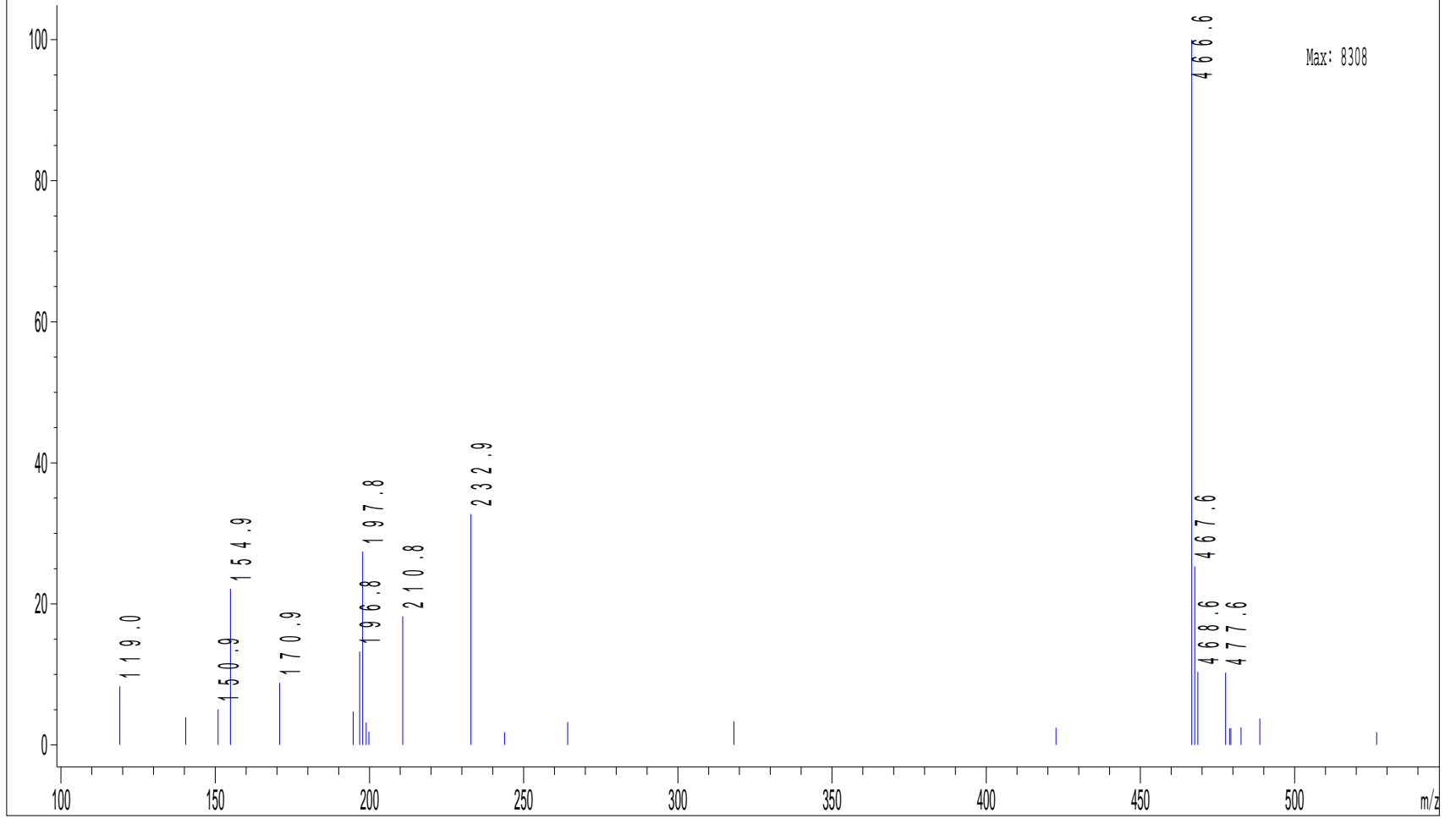
8

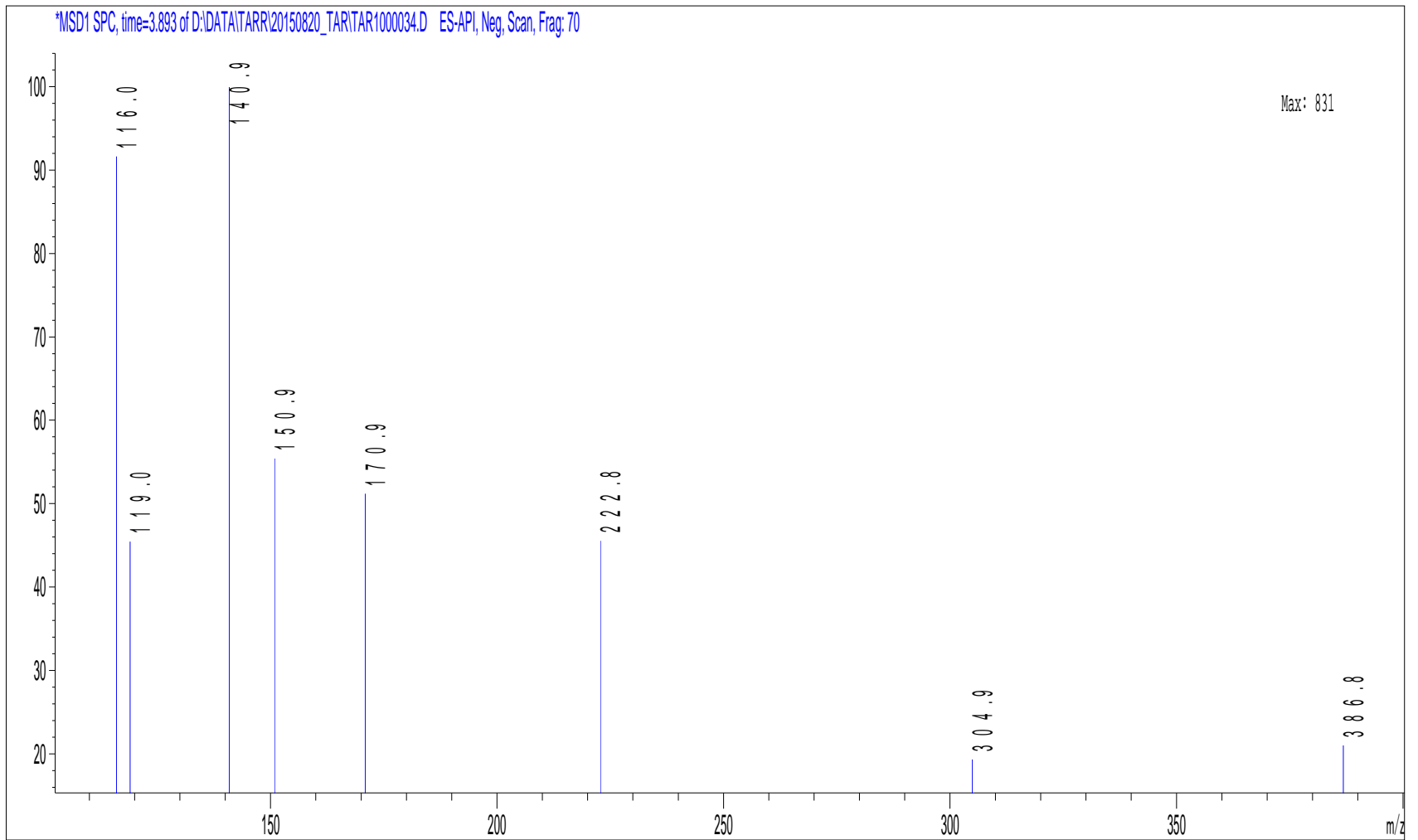
P2-D-03

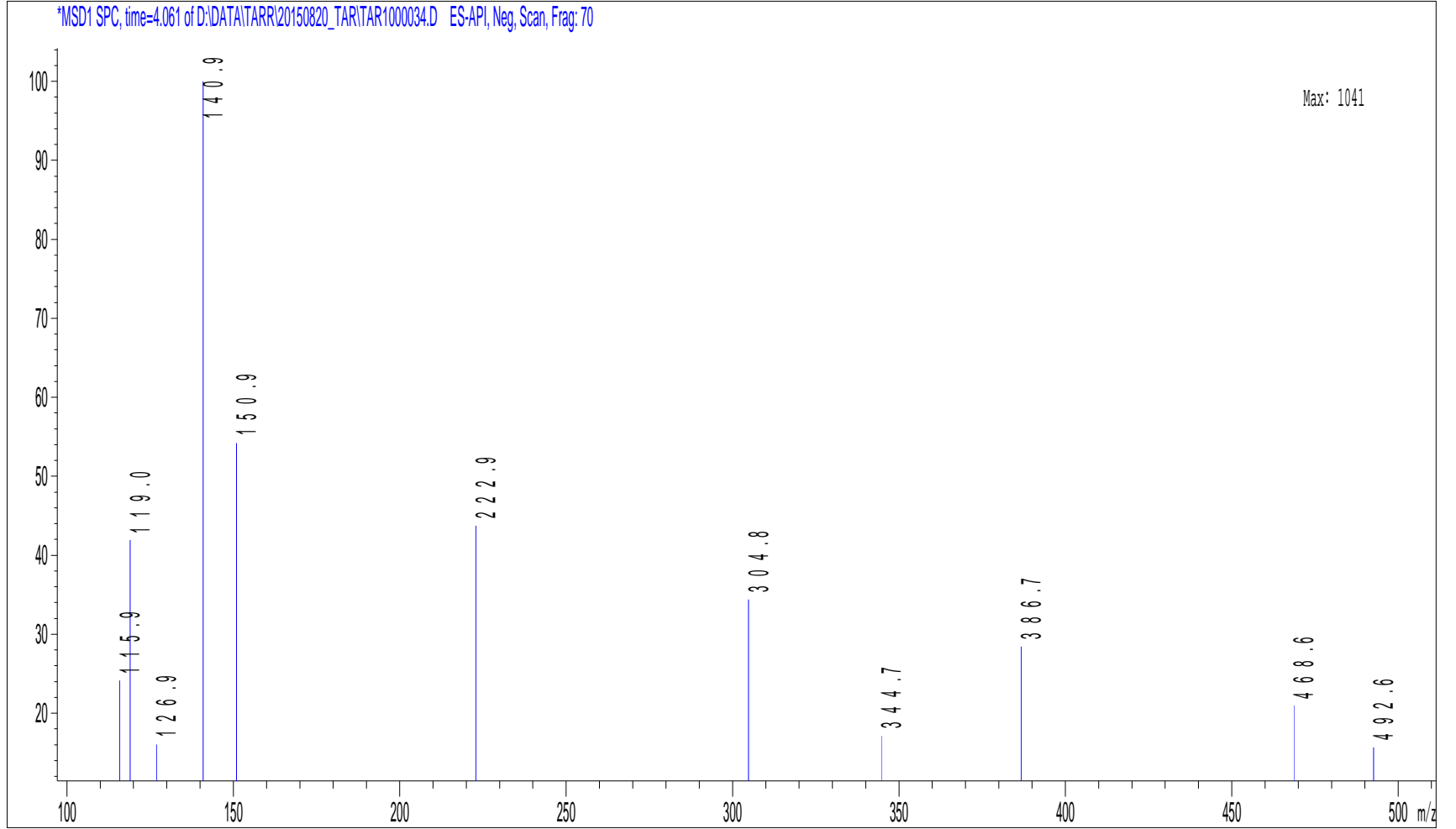


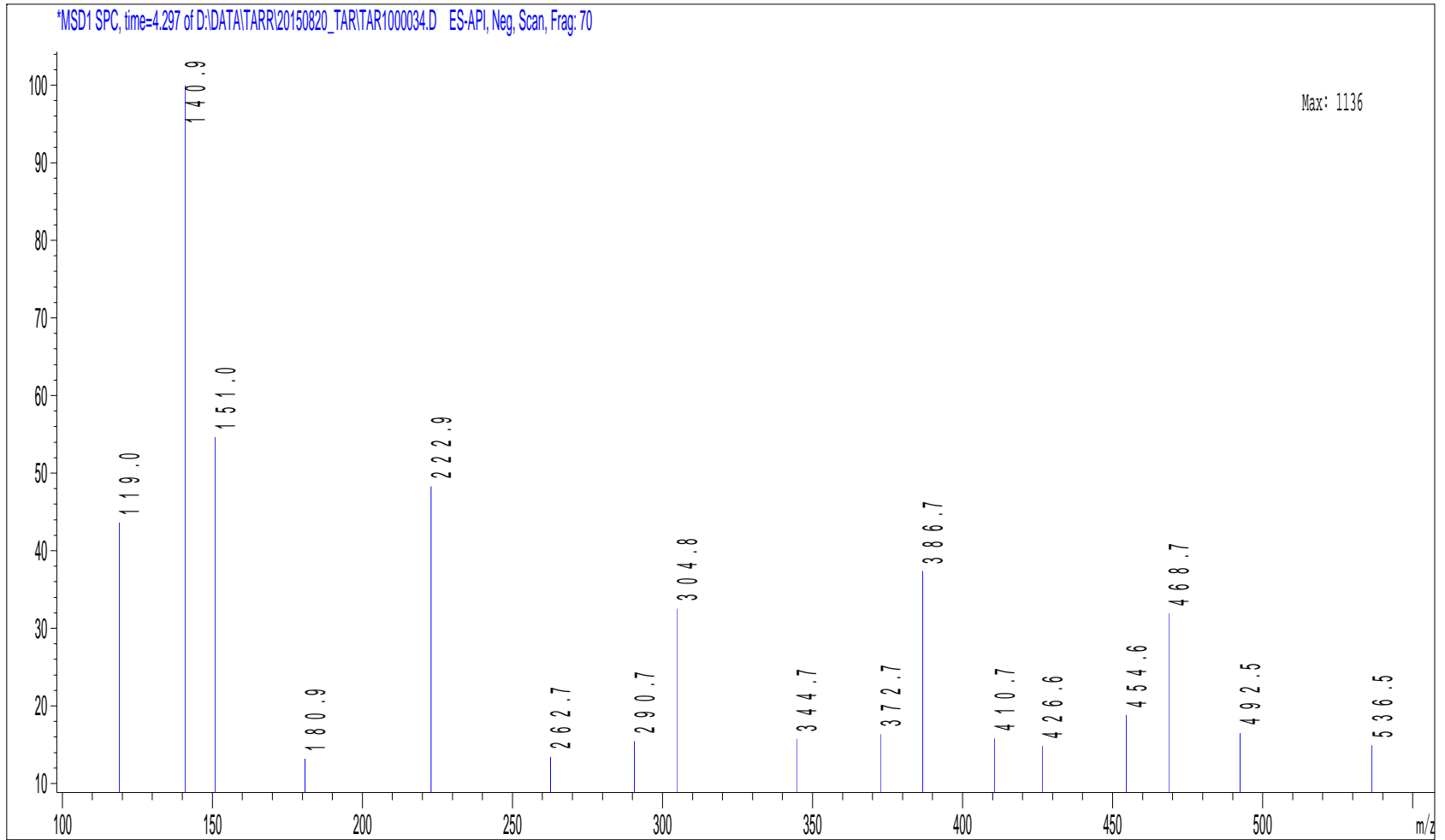


\*MSD1 SPC, time=2.999 of D:\DATA\TARR\20150820\_TARITAR1000034.D ES-API, Neg, Scan, Frag: 70







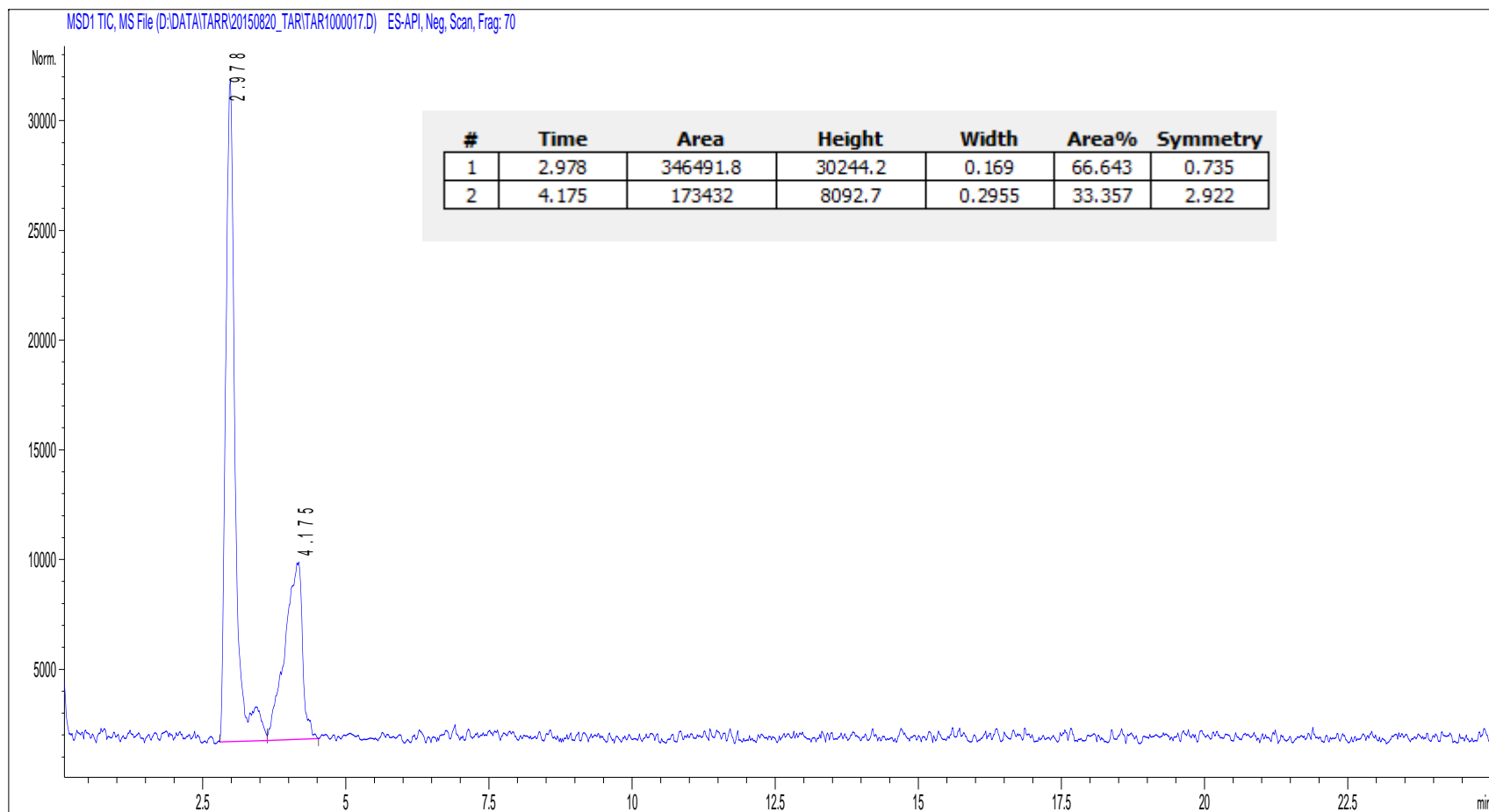


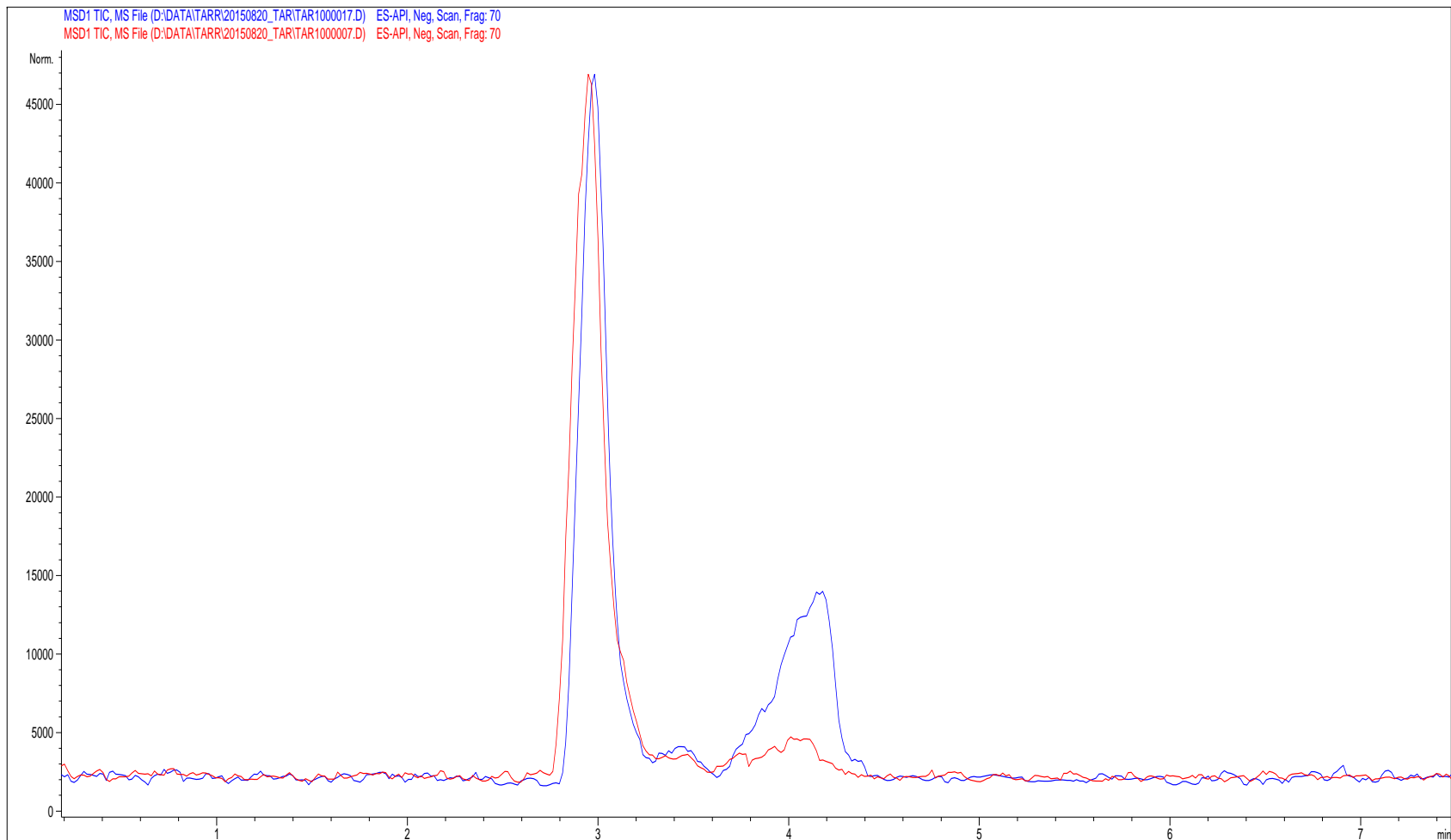
27-May-15

10 DC

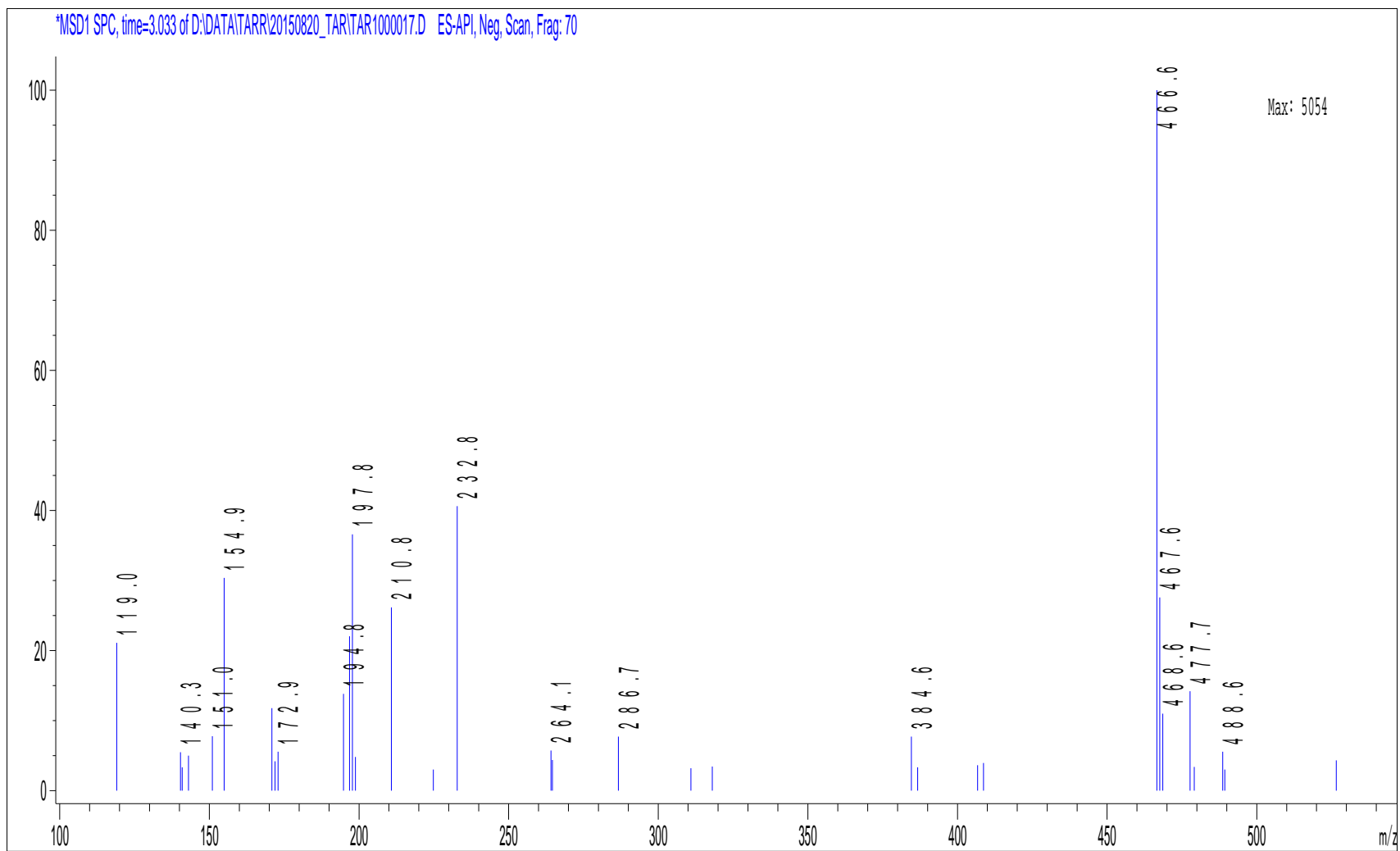
8

P2-B-02

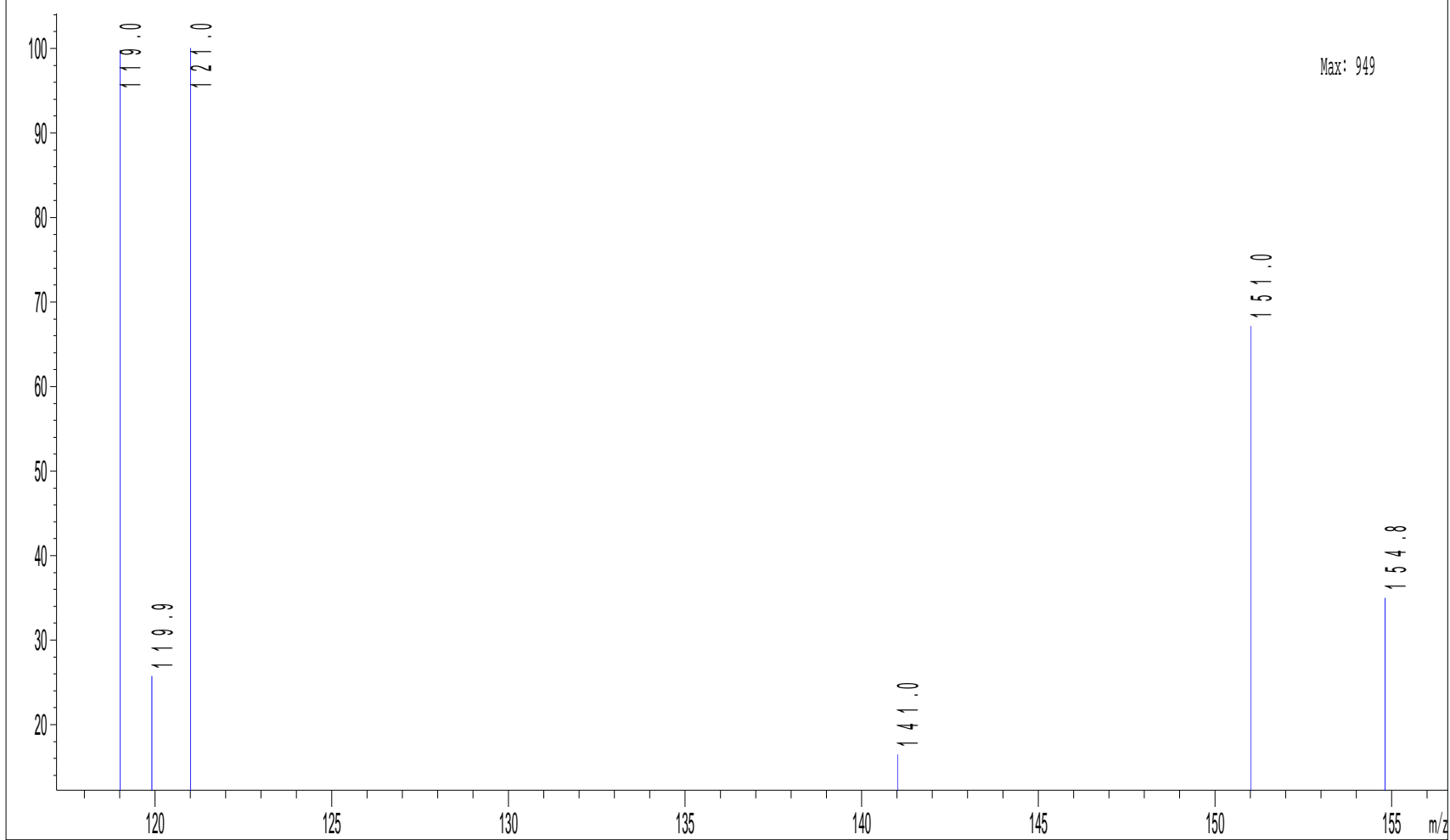


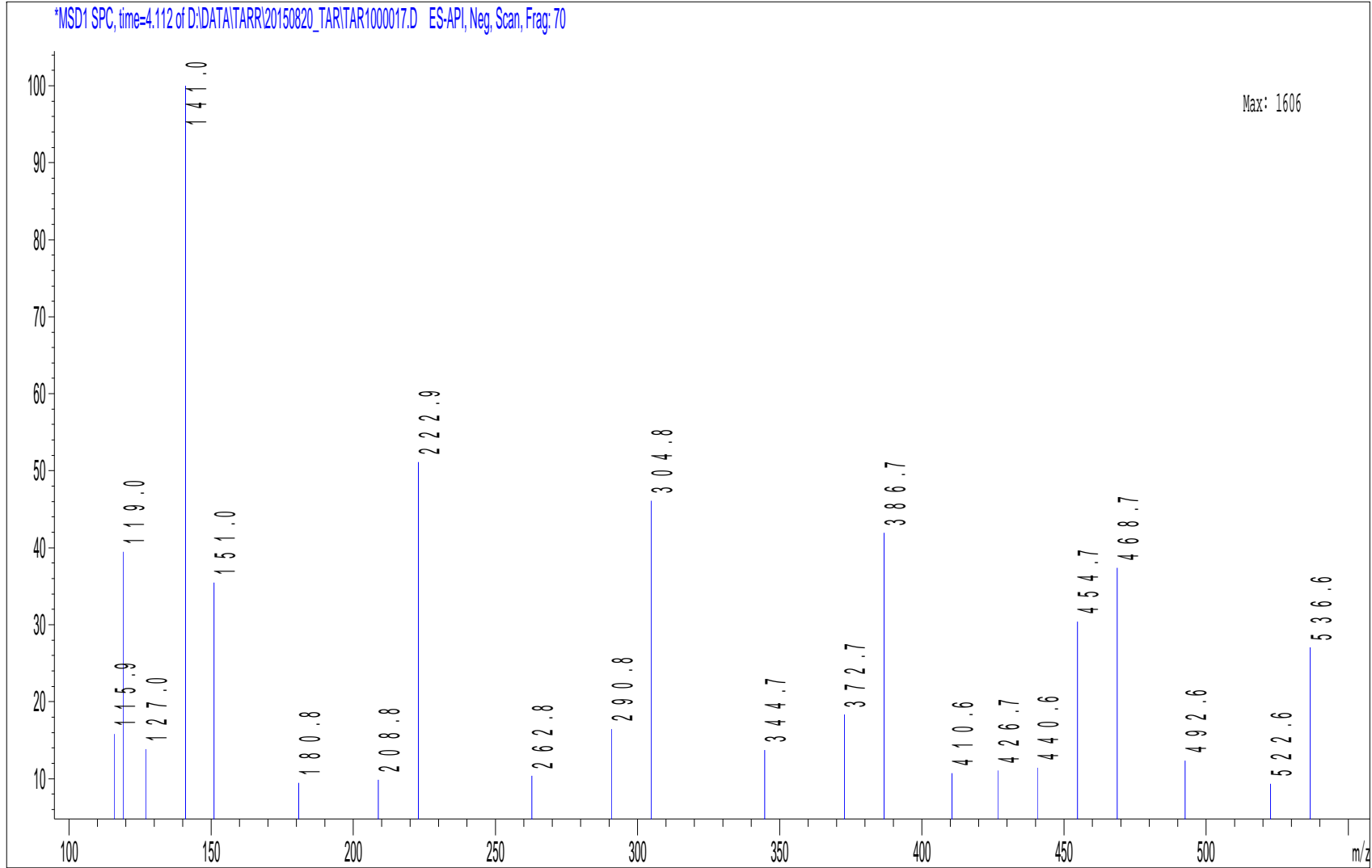






\*MSD1 SPC, time=3.421 of D:\DATA\TARRI20150820\_TARITAR1000017.D ES-API, Neg, Scan, Frag: 70



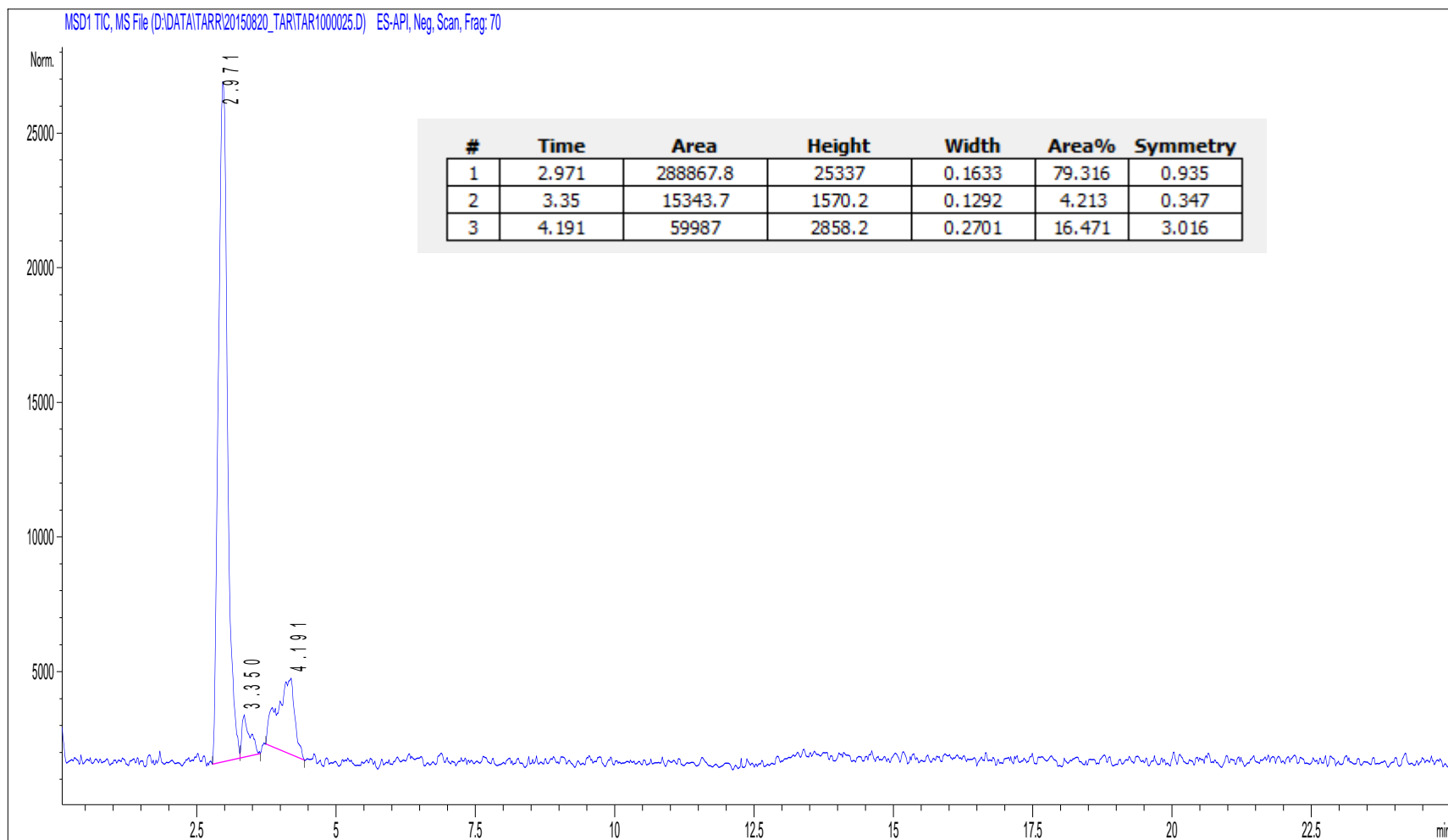


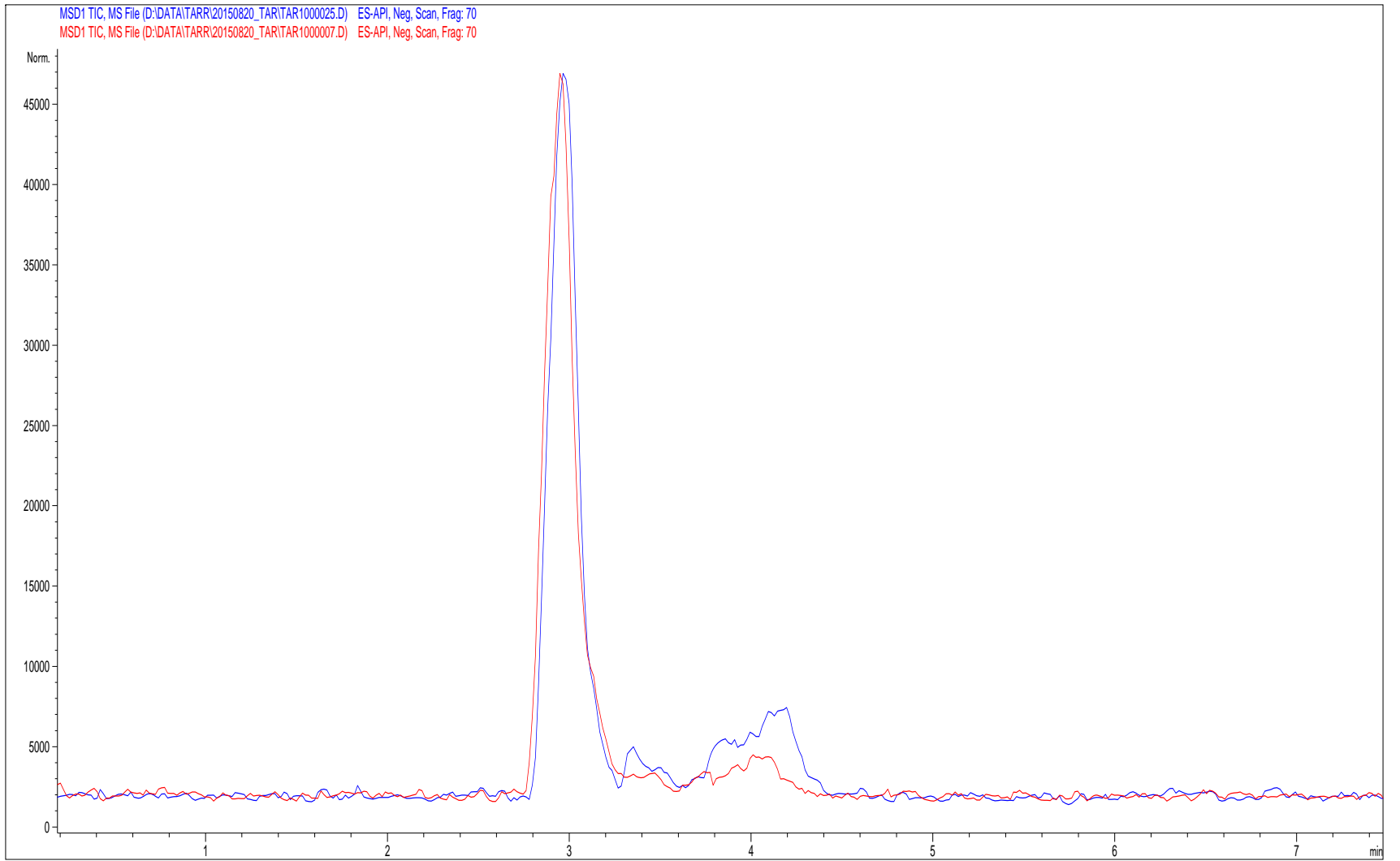
10-Jul-15

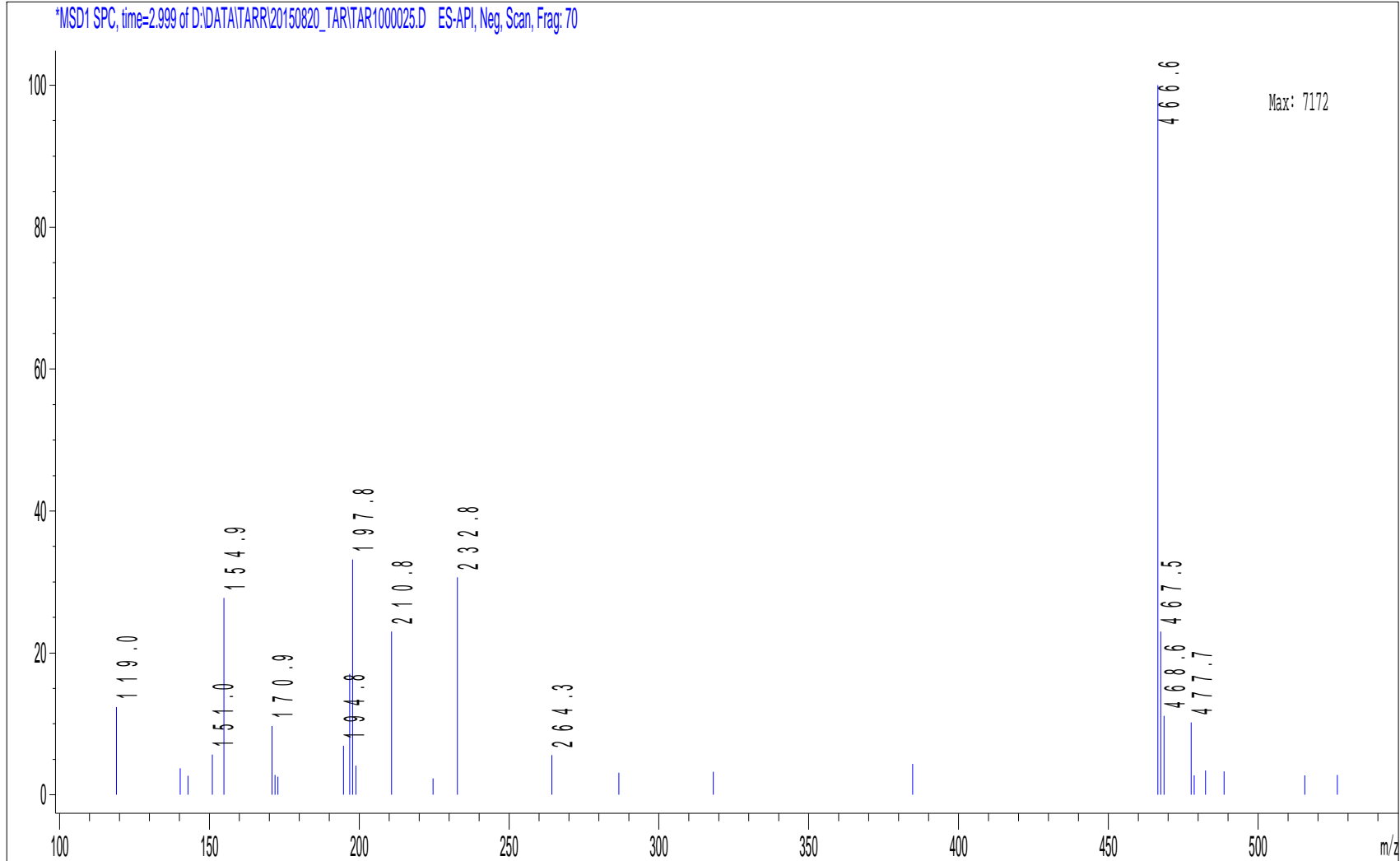
20 DC

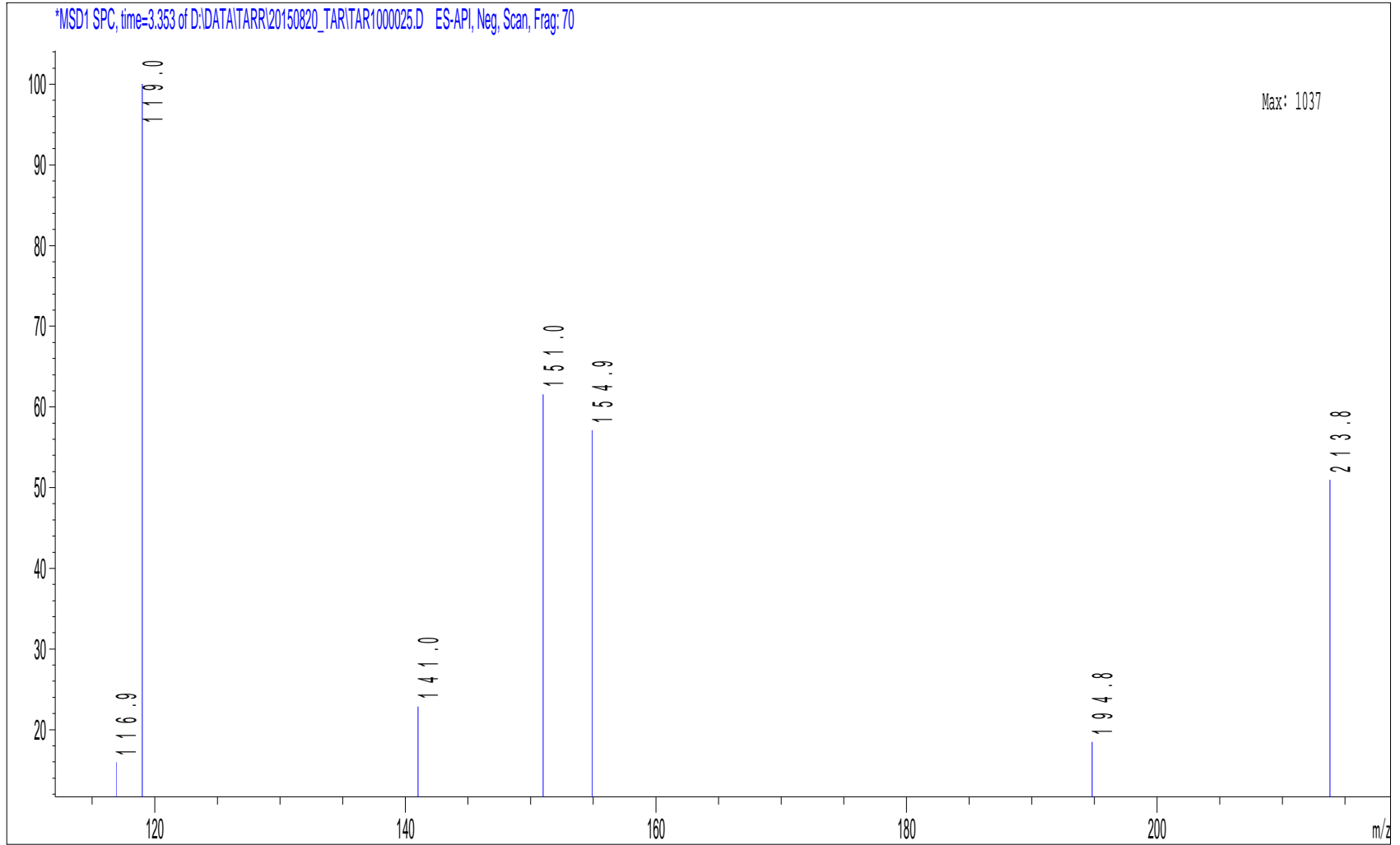
8

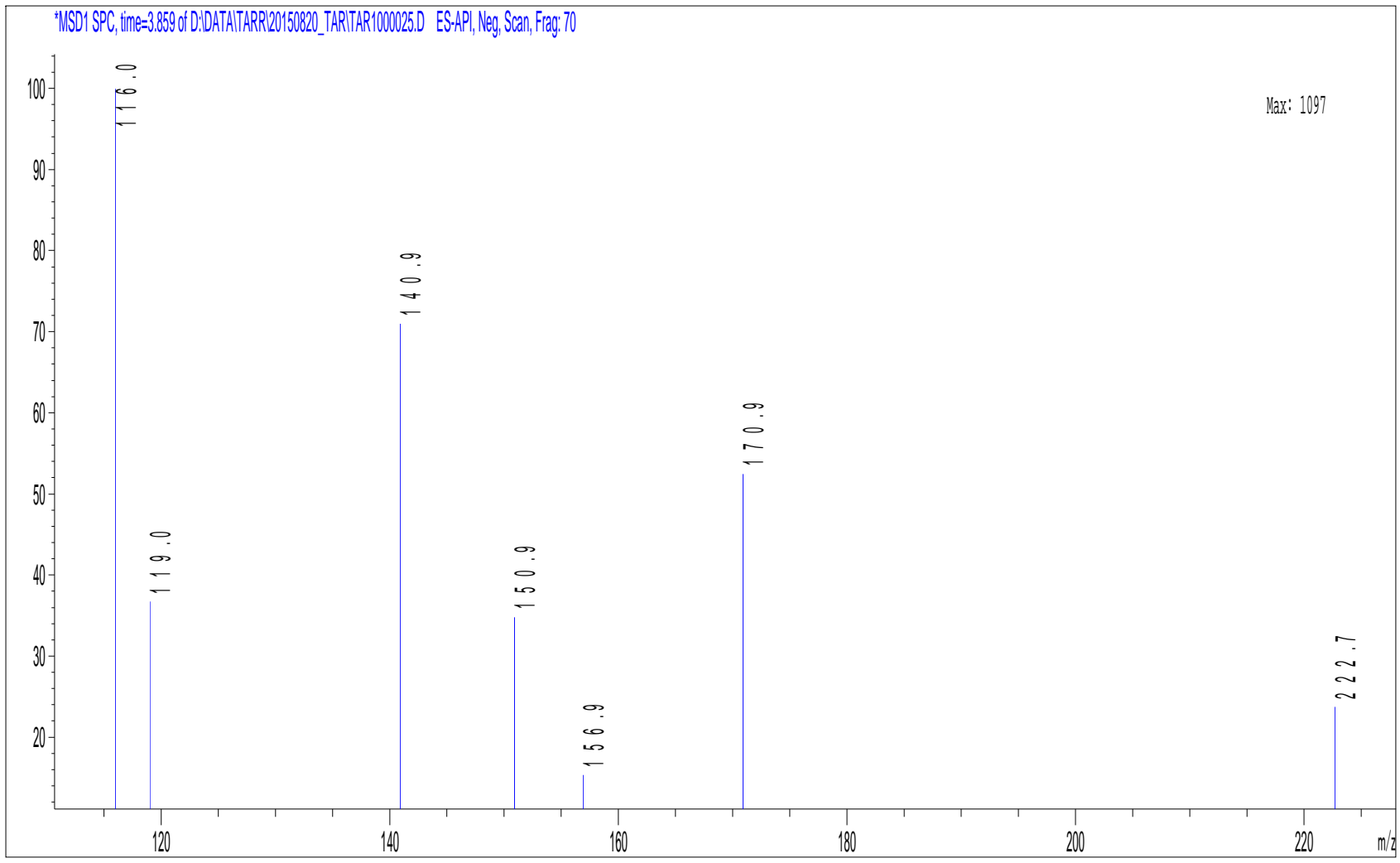
P2-C-07



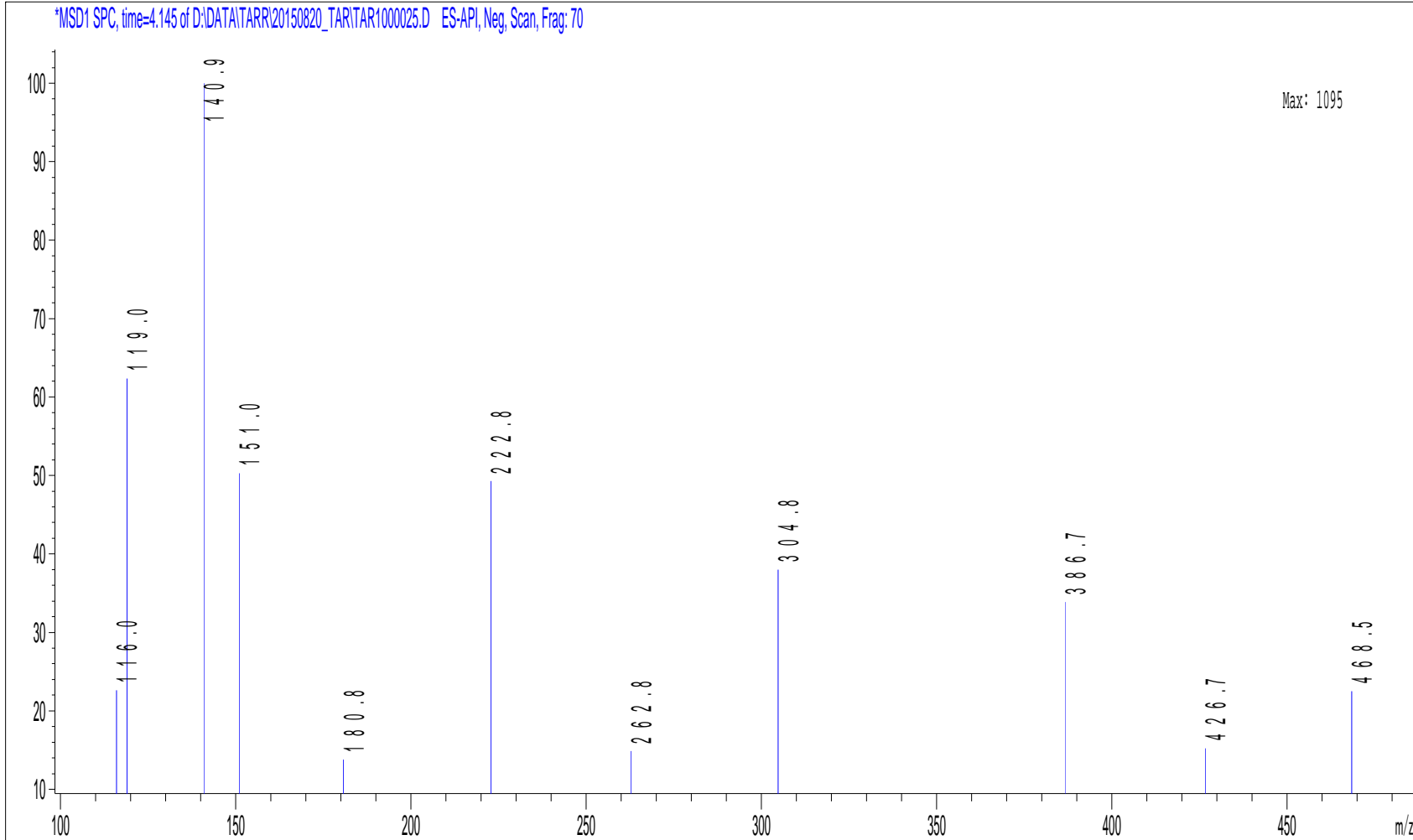










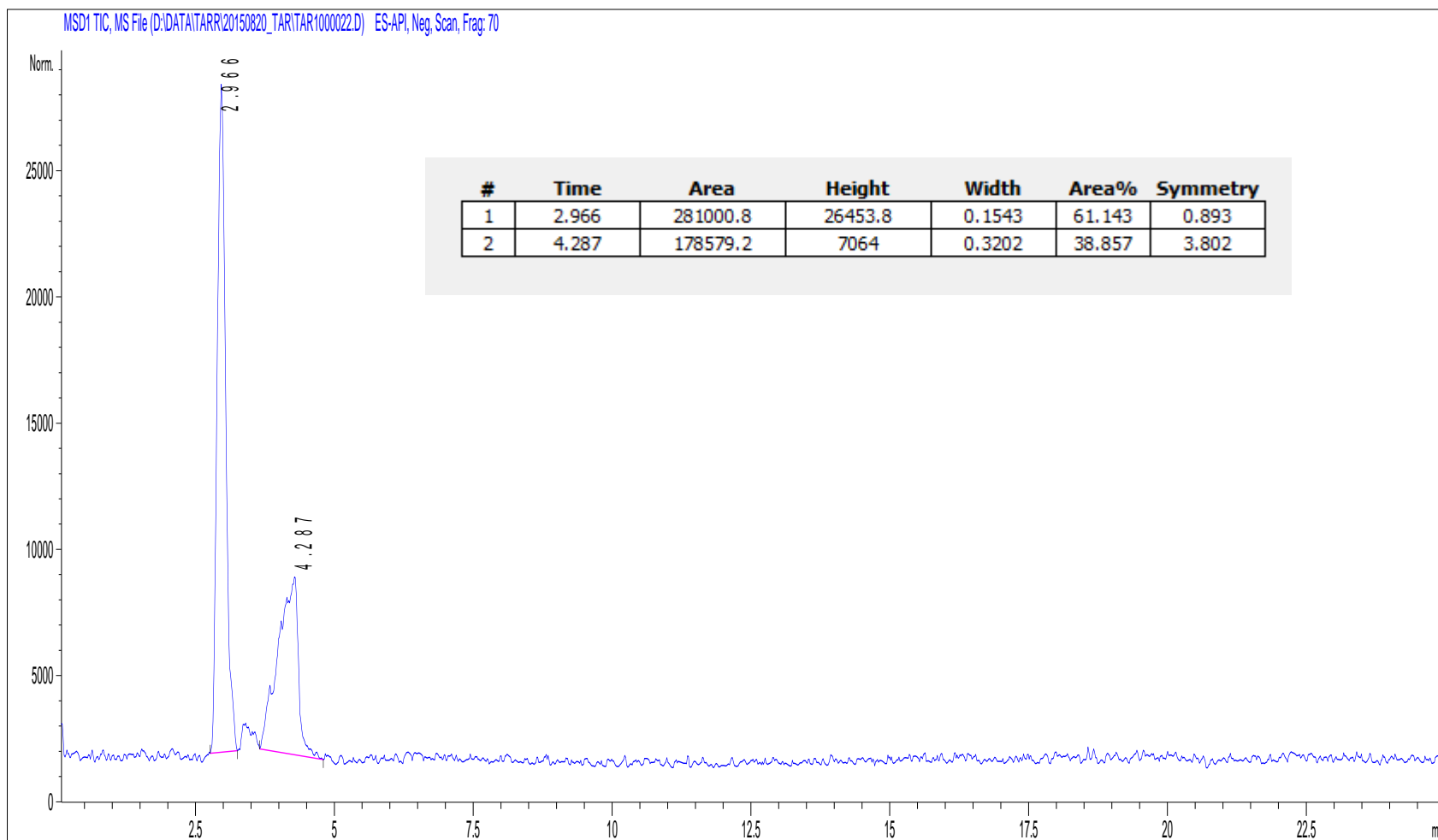


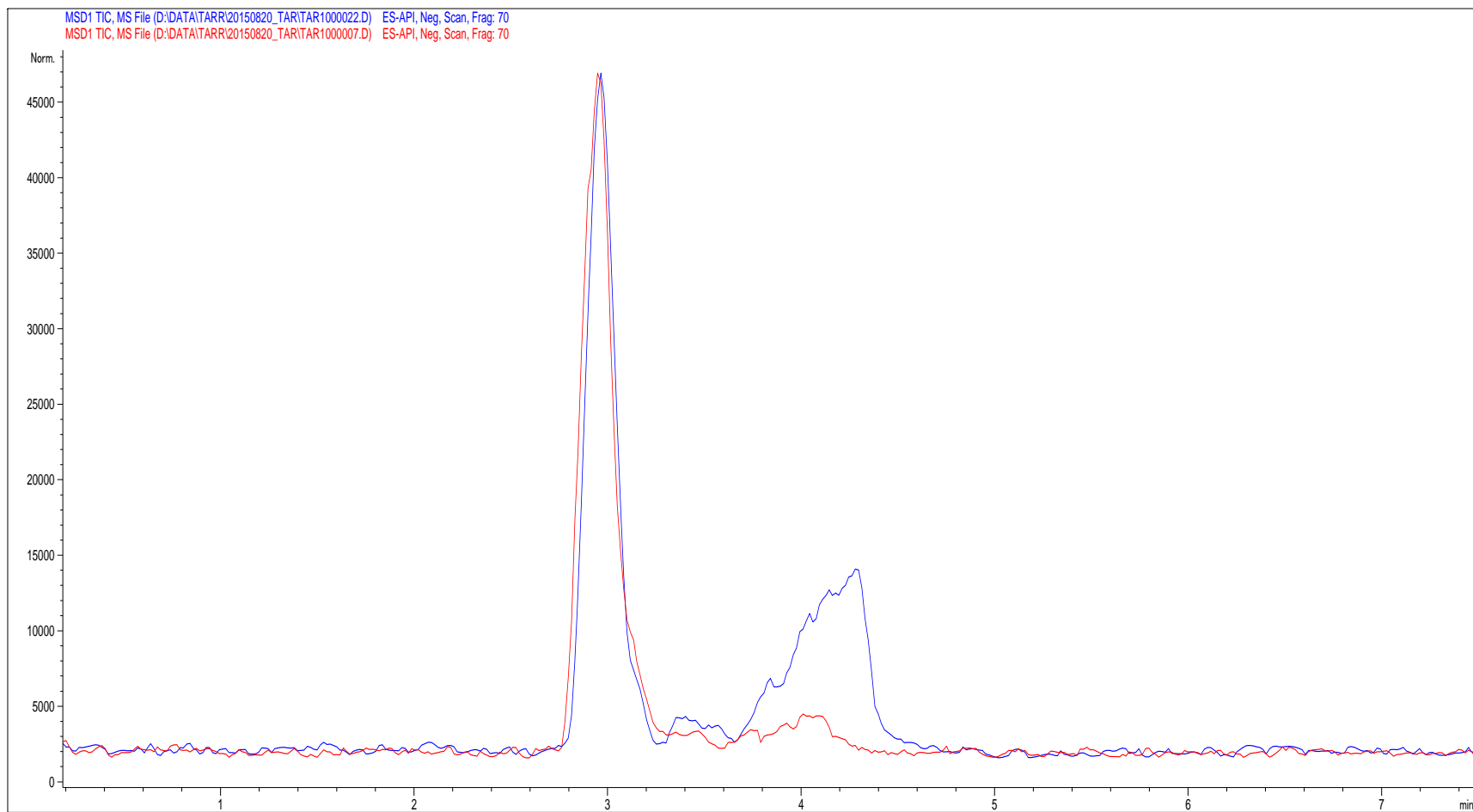
2-Jul-15

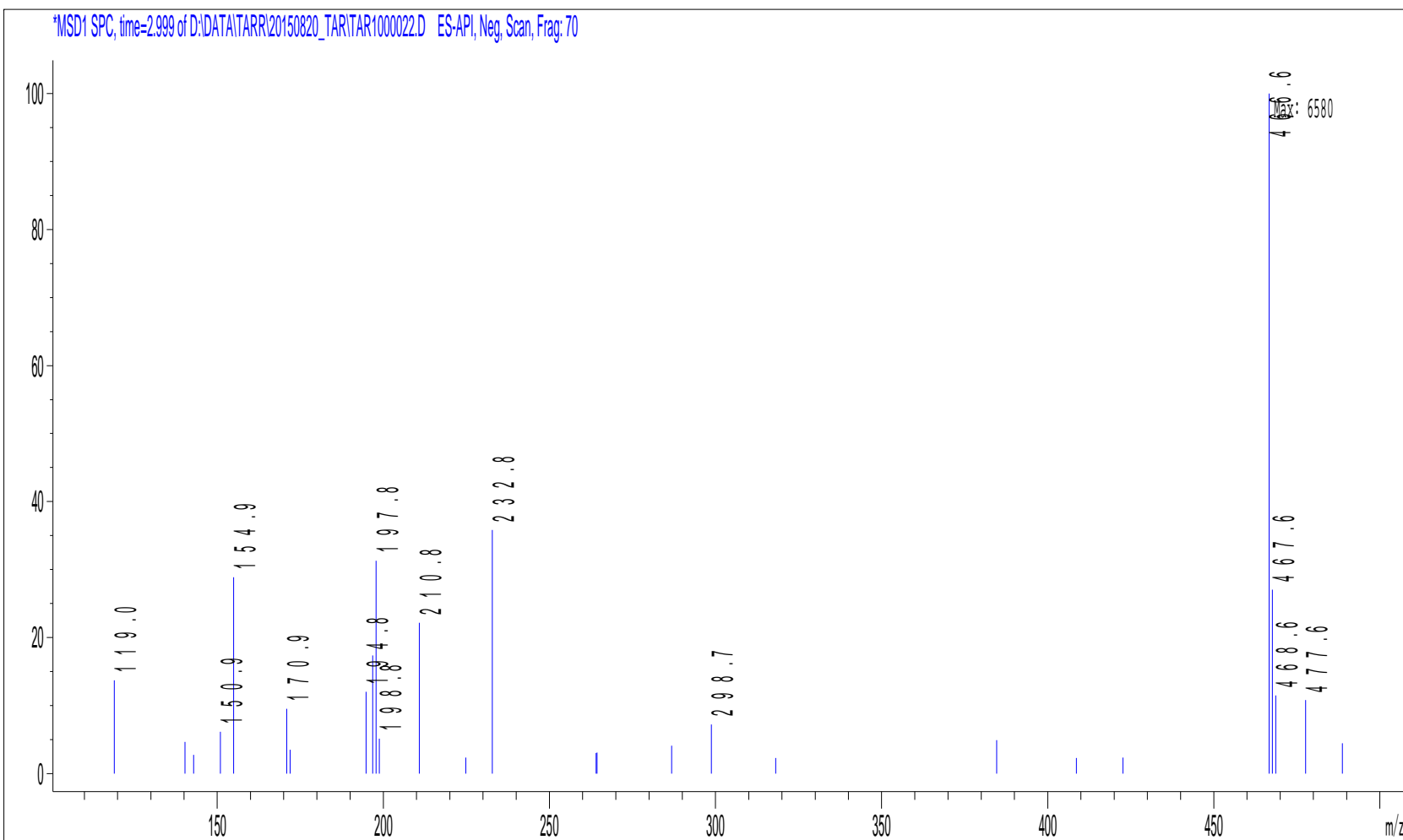
30 DC

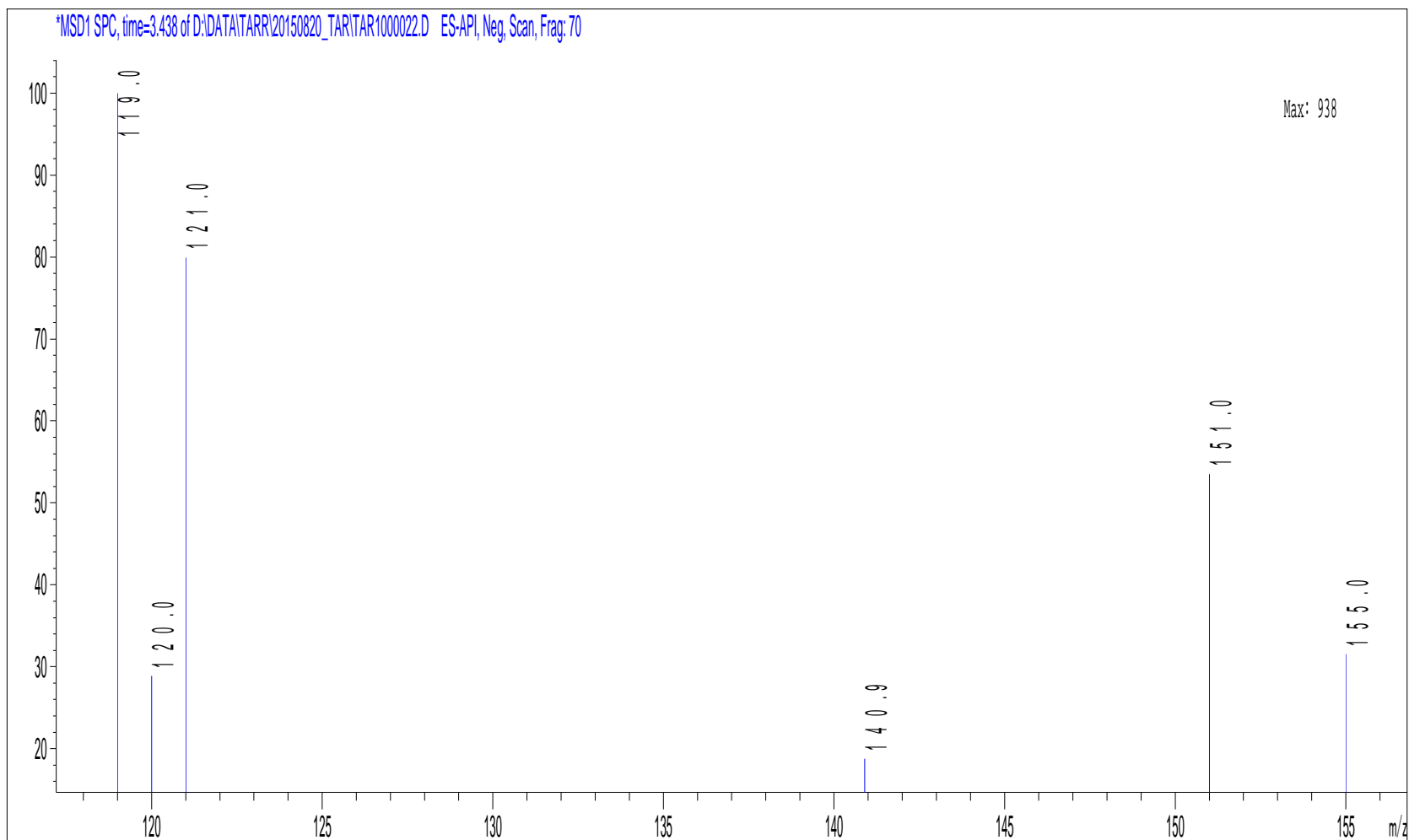
8

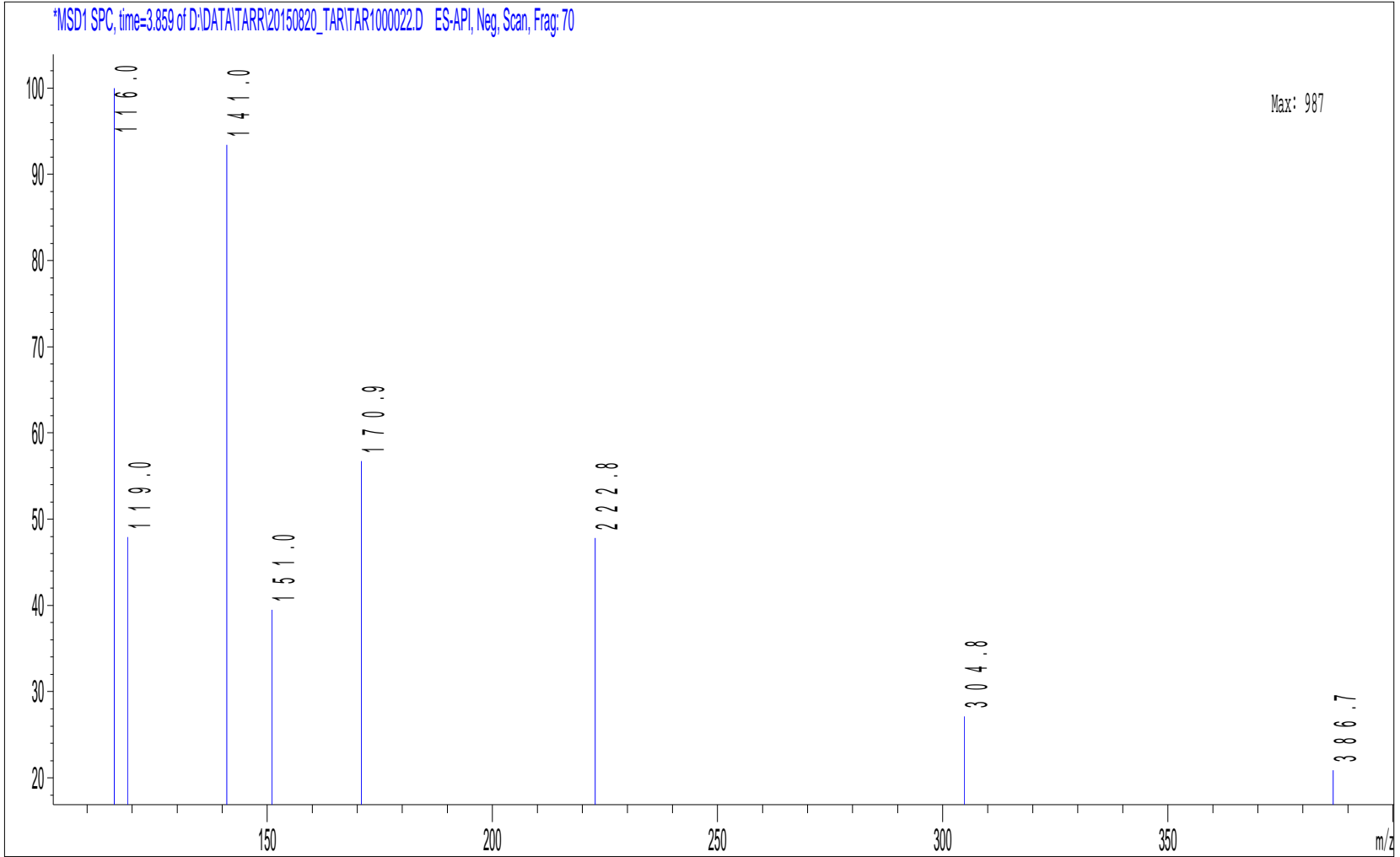
P2-C-04

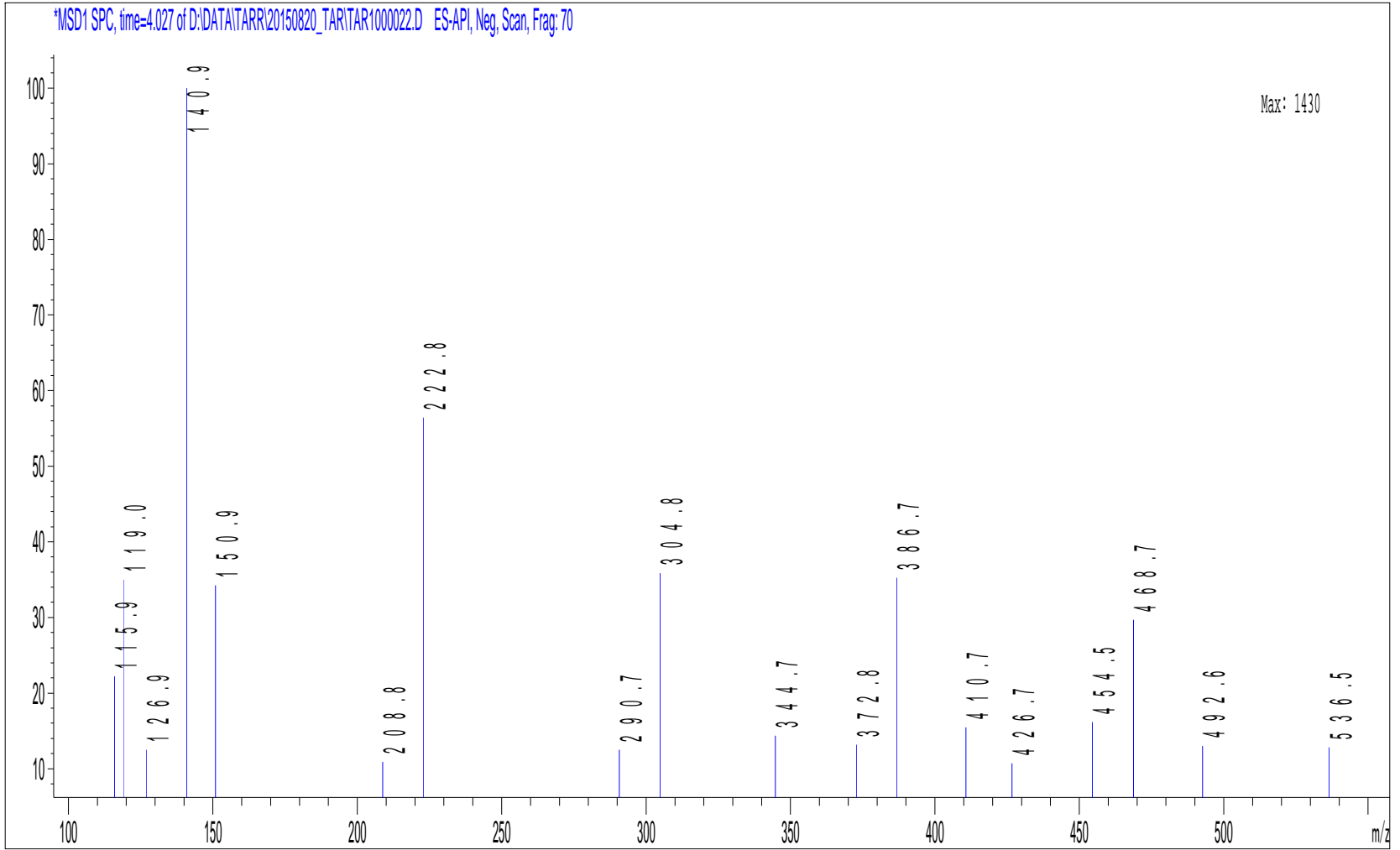




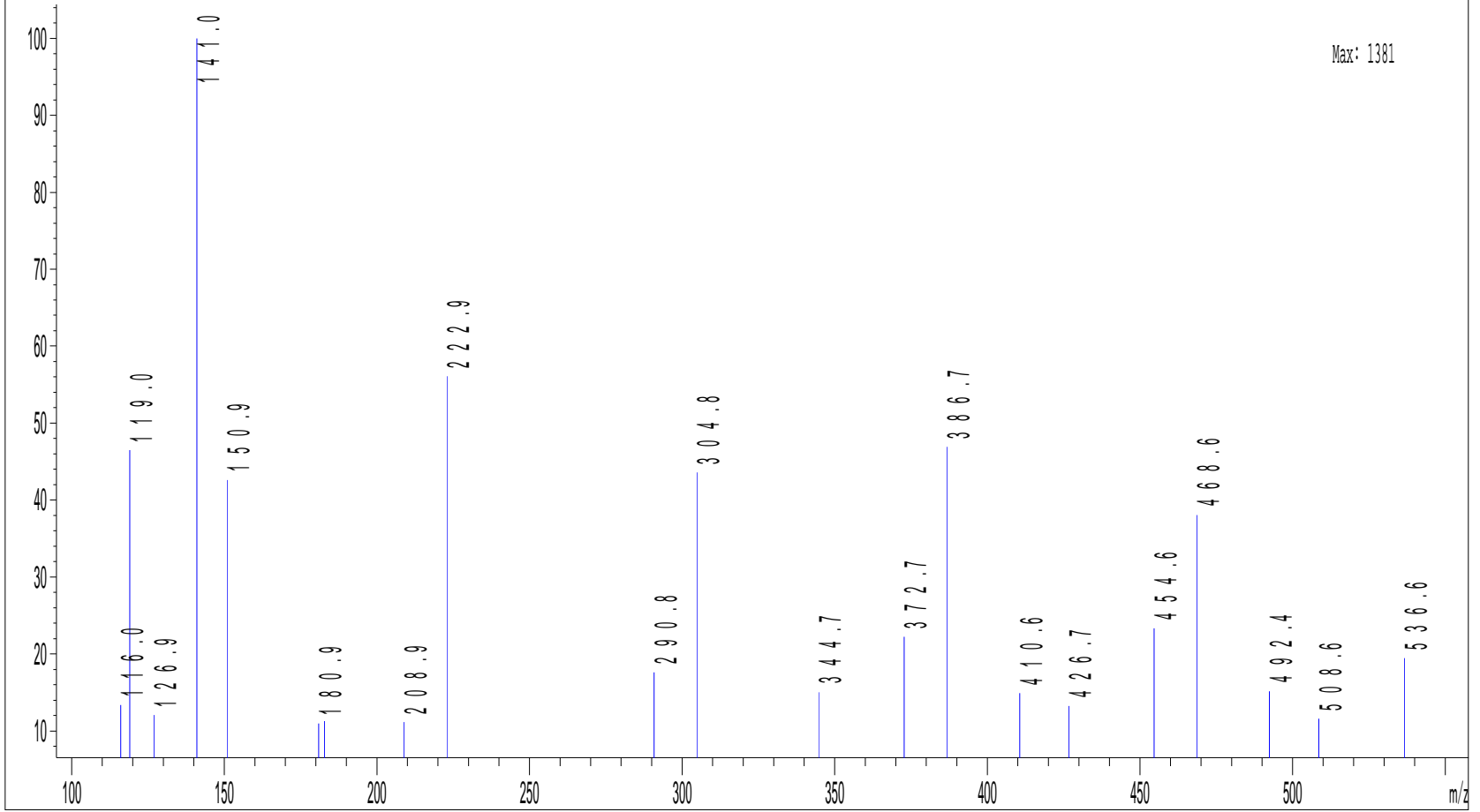






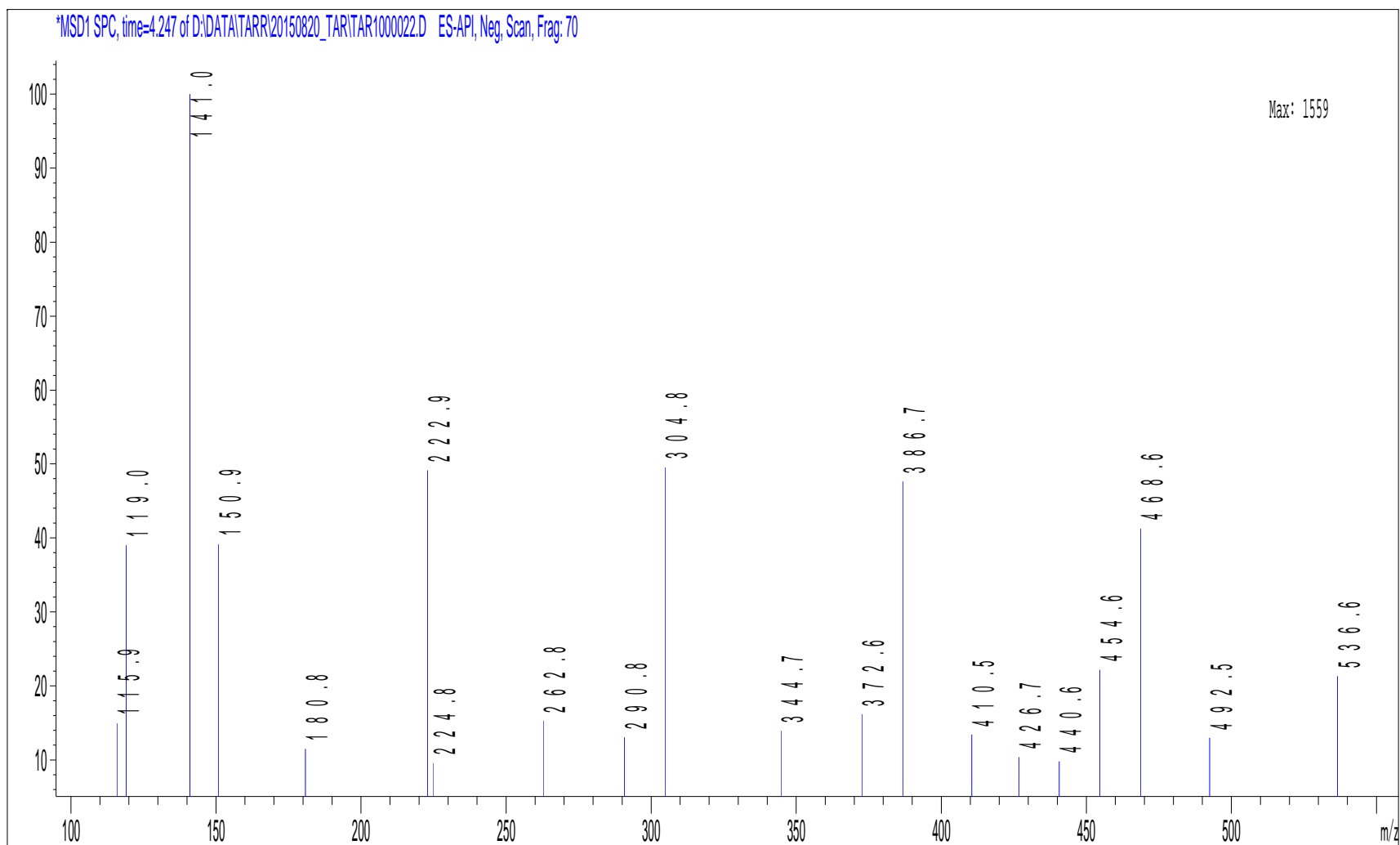


\*MSD1 SPC, time=4.145 of D:\DATA\TARR\20150820\_TARITAR1000022.D ES-API, Neg, Scan, Frag: 70





\*MSD1 SPC, time=4.247 of D:\DATA\TARR\20150820\_TARITAR1000022.D ES-API, Neg. Scan, Frag: 70

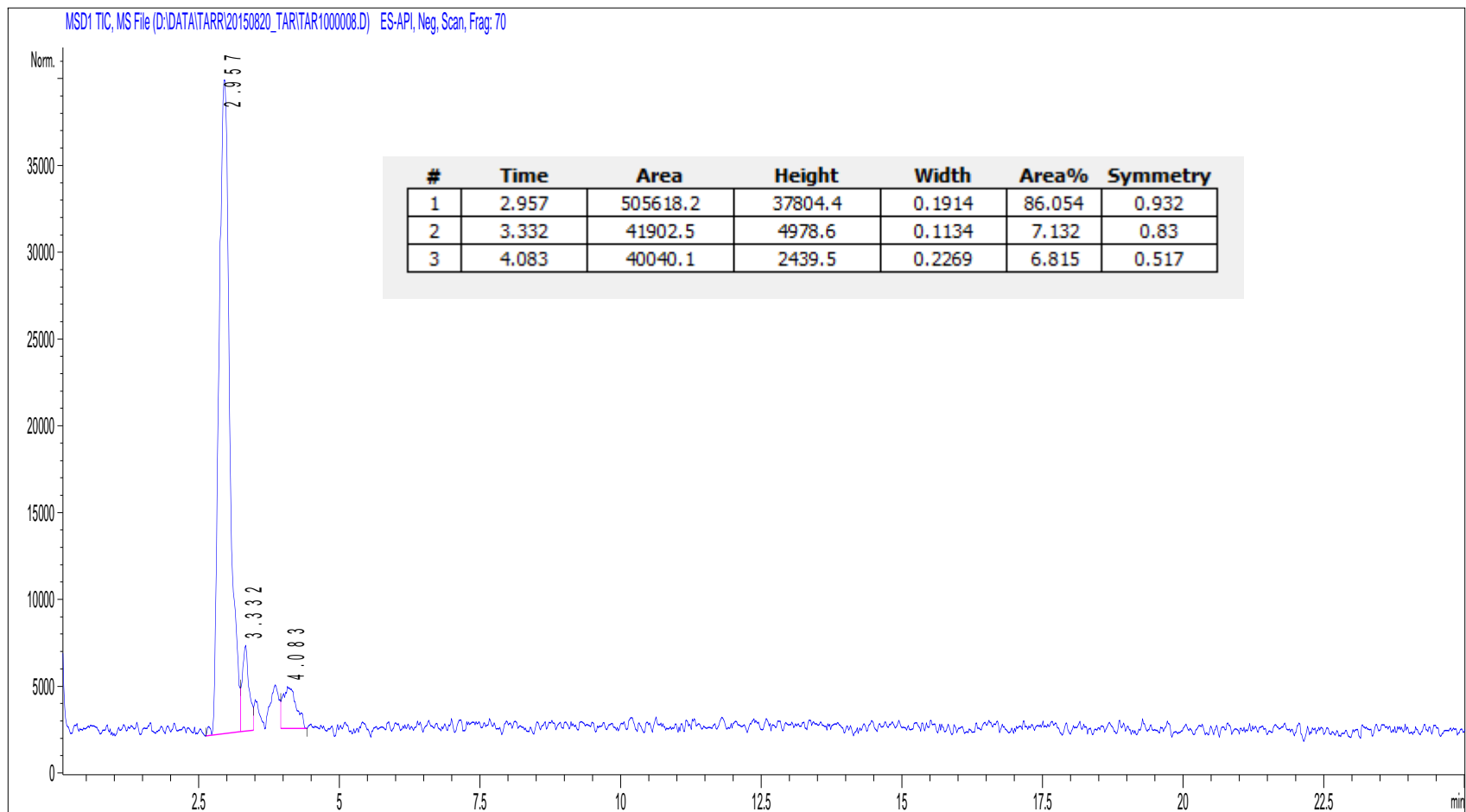


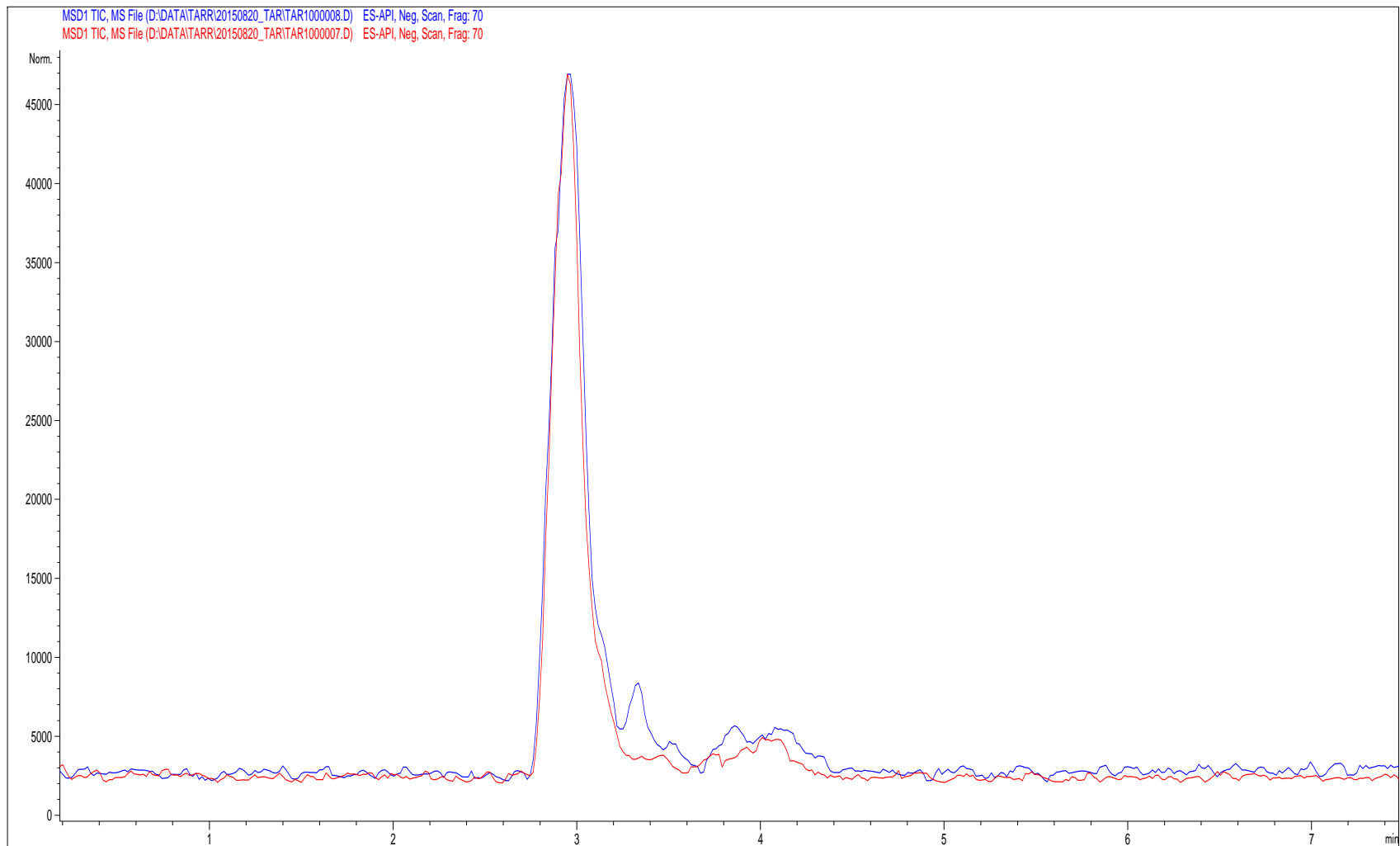
23-Apr-15

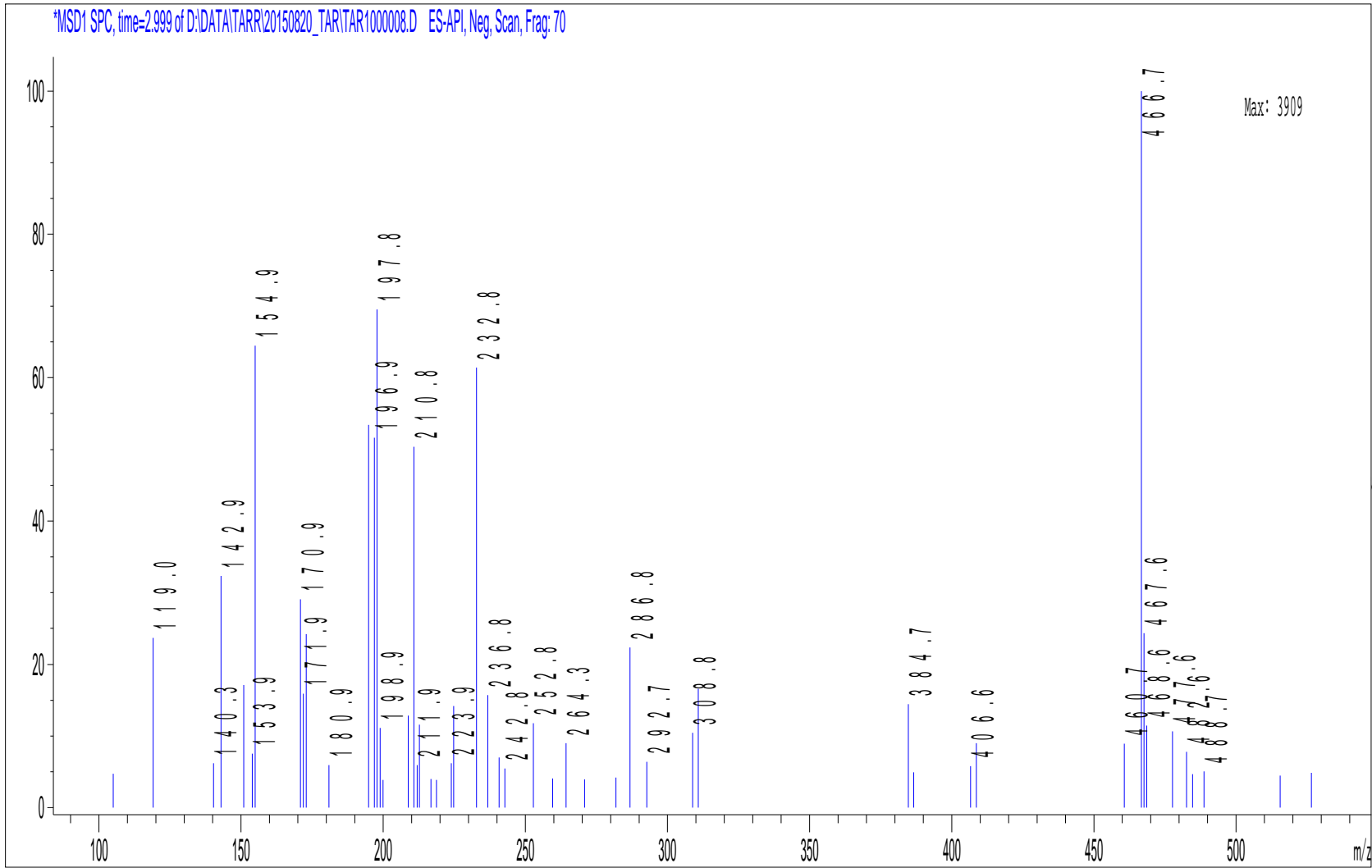
50 DC

8

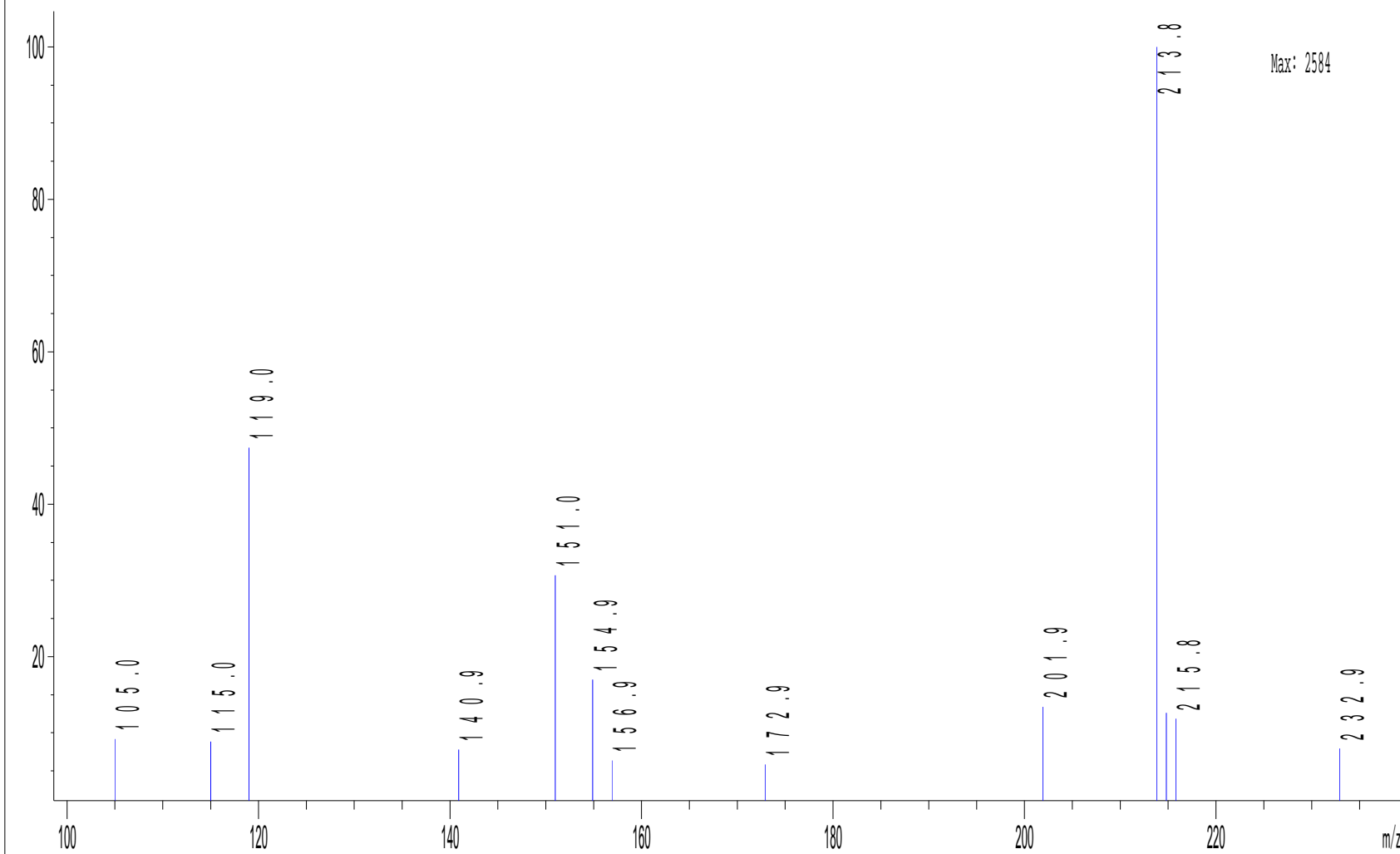
P2-A-08



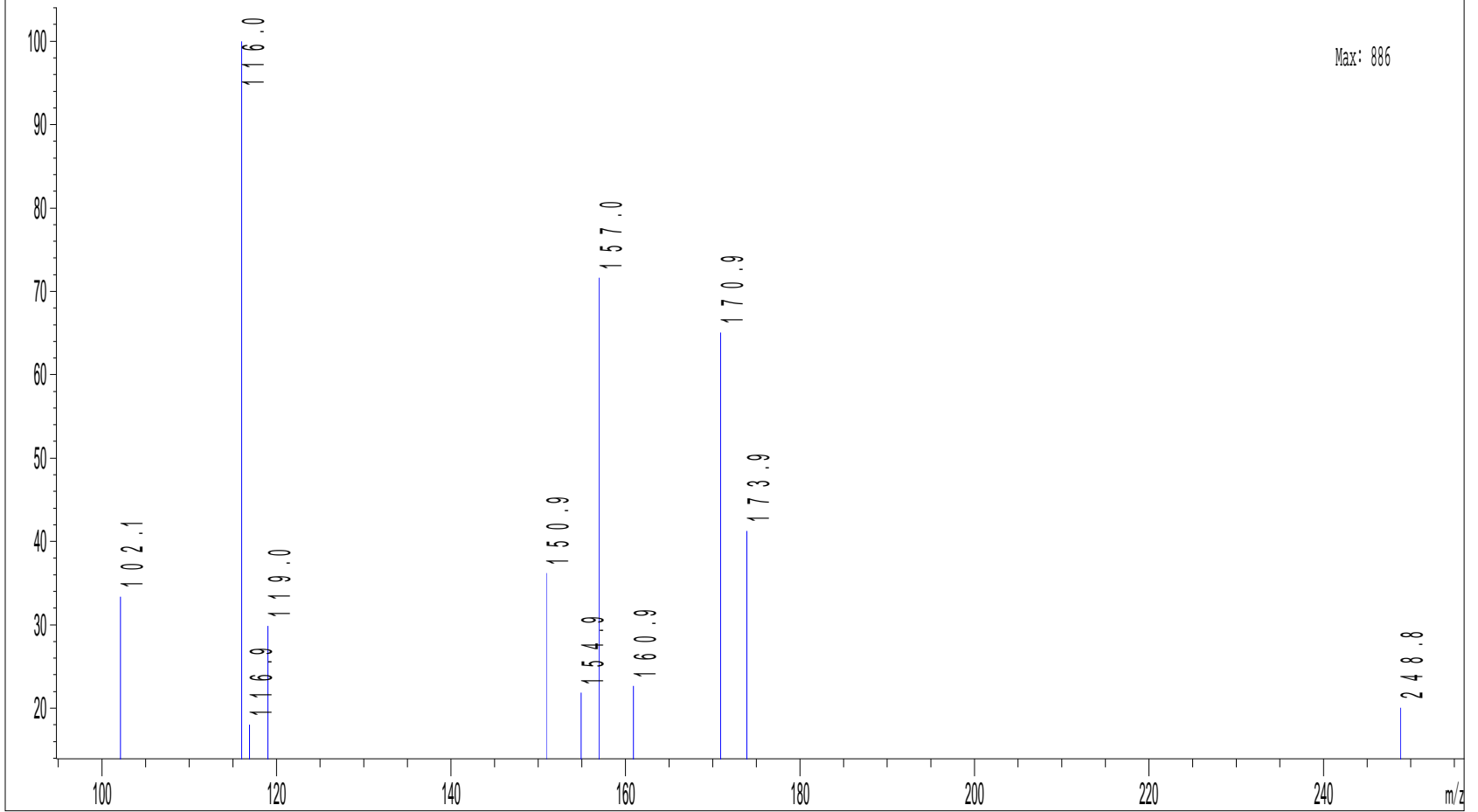




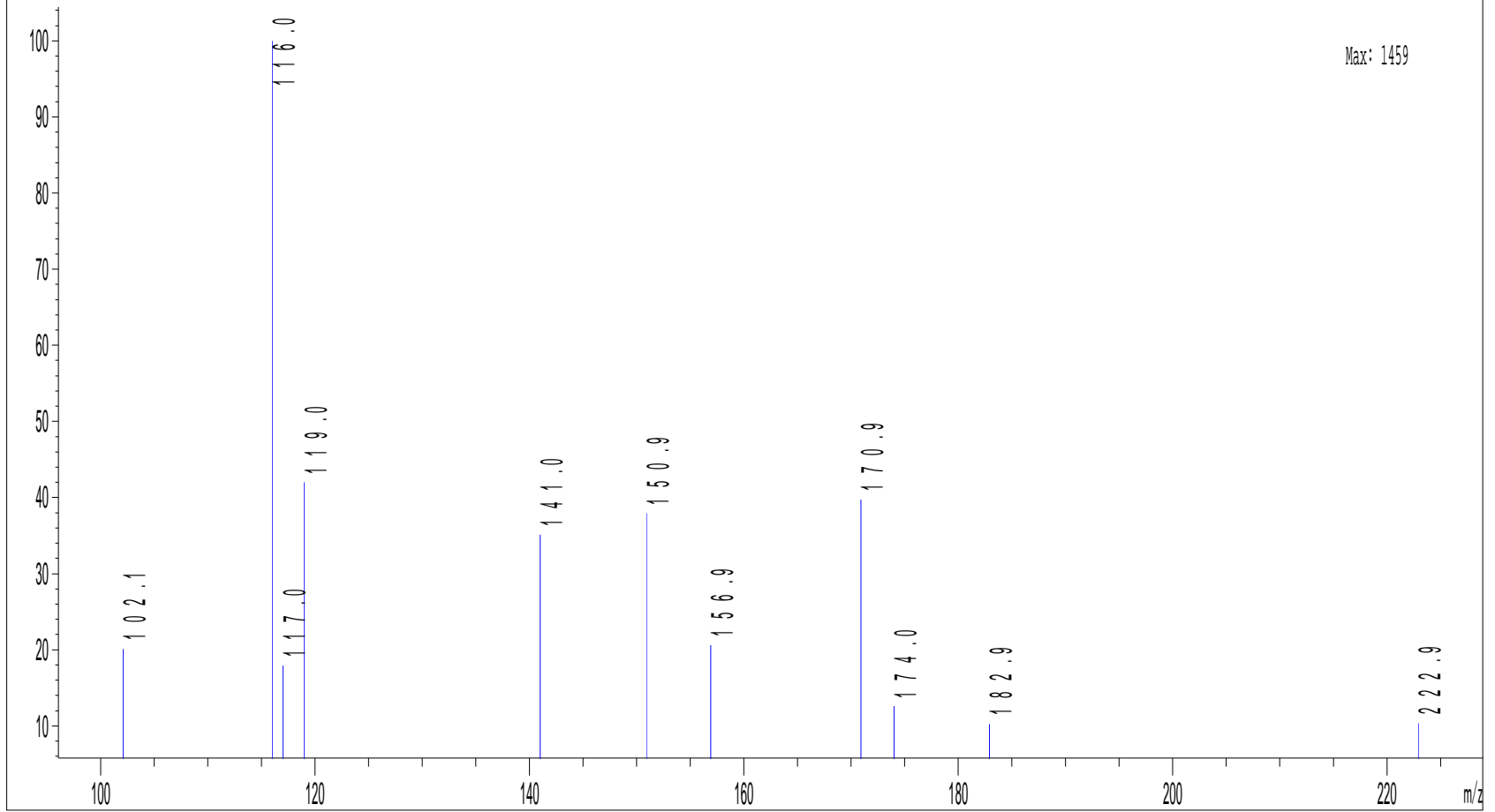
\*MSD1 SPC, time=3.320 of D:\DATA\TARR\20150820\_TARITAR1000008.D ES-API, Neg, Scan, Frag: 70



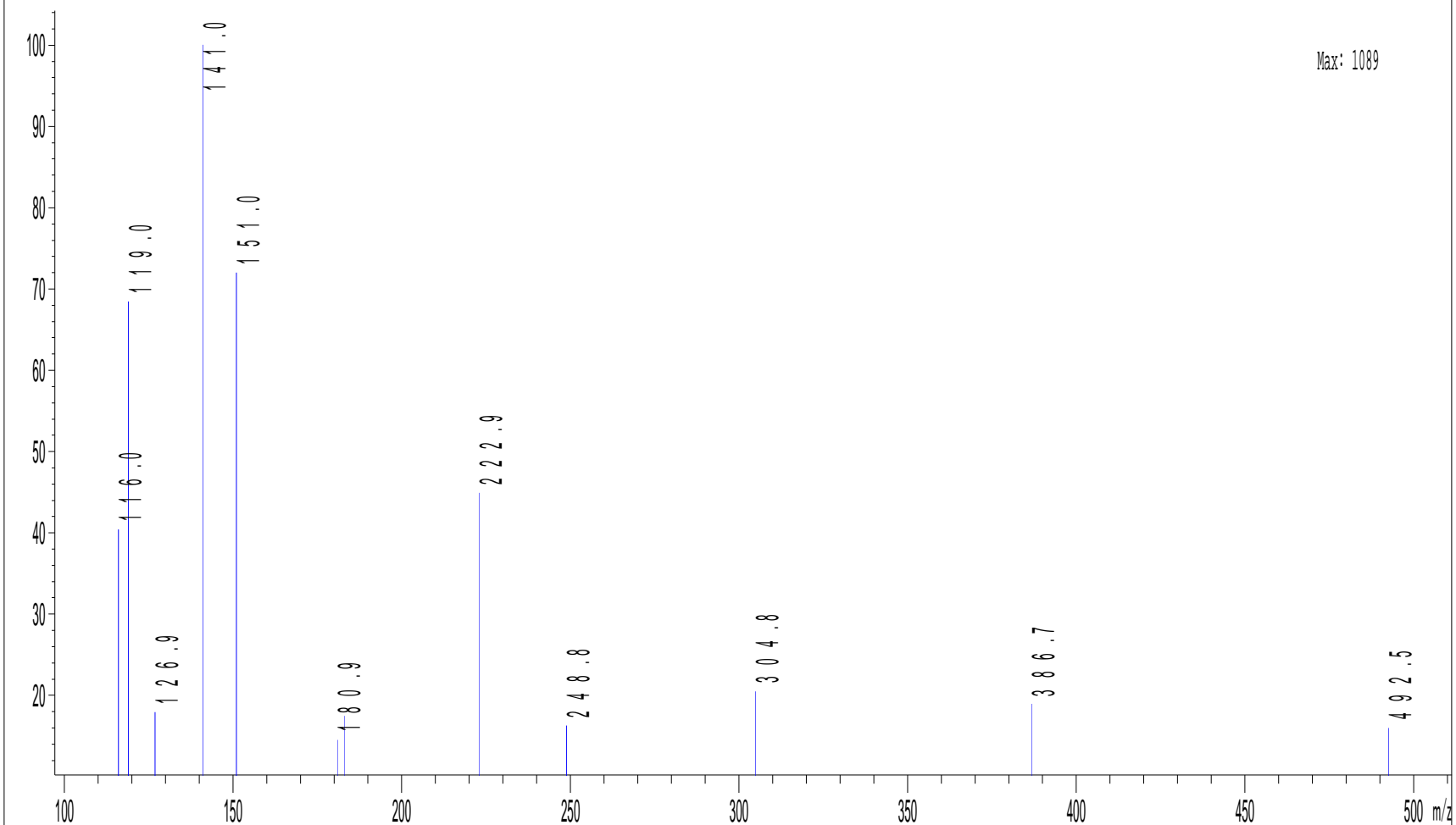
\*MSD1 SPC, time=3.522 of D:\DATA\TARR\20150820\_TARITAR1000008.D ES-API, Neg, Scan, Frag: 70



\*MSD1 SPC, time=3.859 of D:\DATA\TARR\20150820\_TARITAR1000008.D ES-API, Neg, Scan, Frag: 70



\*MSD1 SPC, time=4.095 of D:\DATA\ARR\20150820\_TARITAR1000008.D ES-API, Neg, Scan, Frag: 70



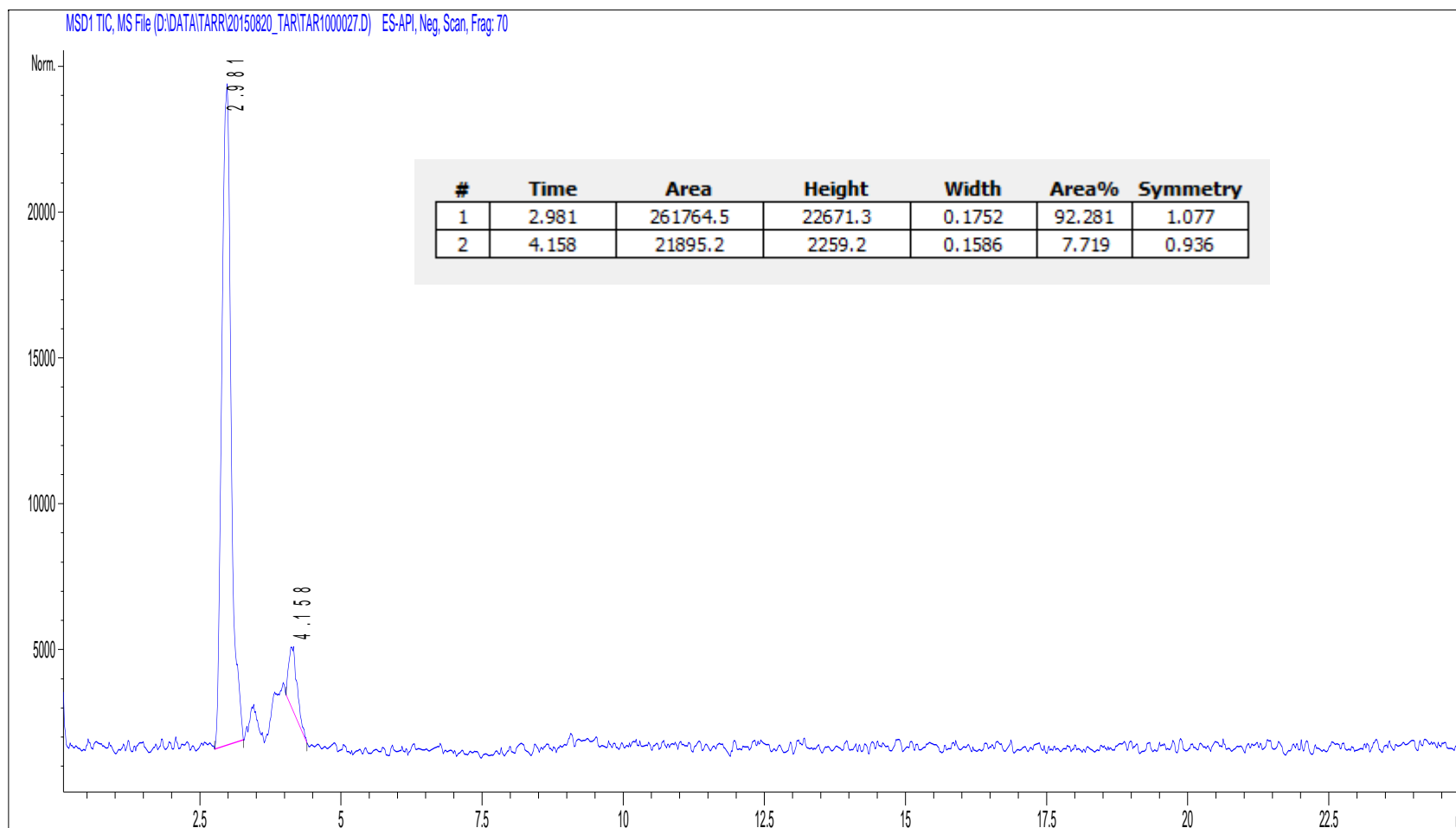


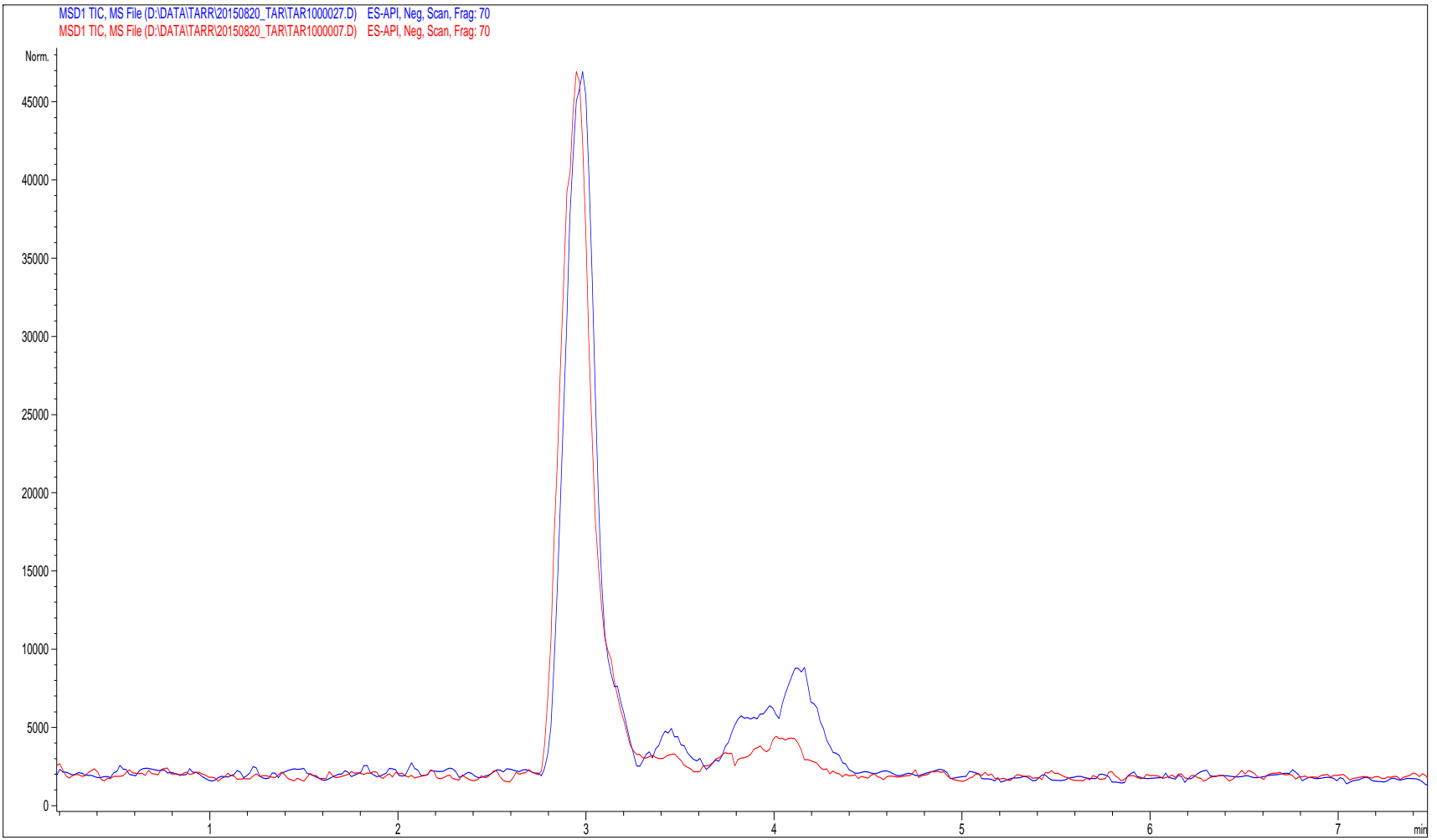
9-Jul-15

70 DC

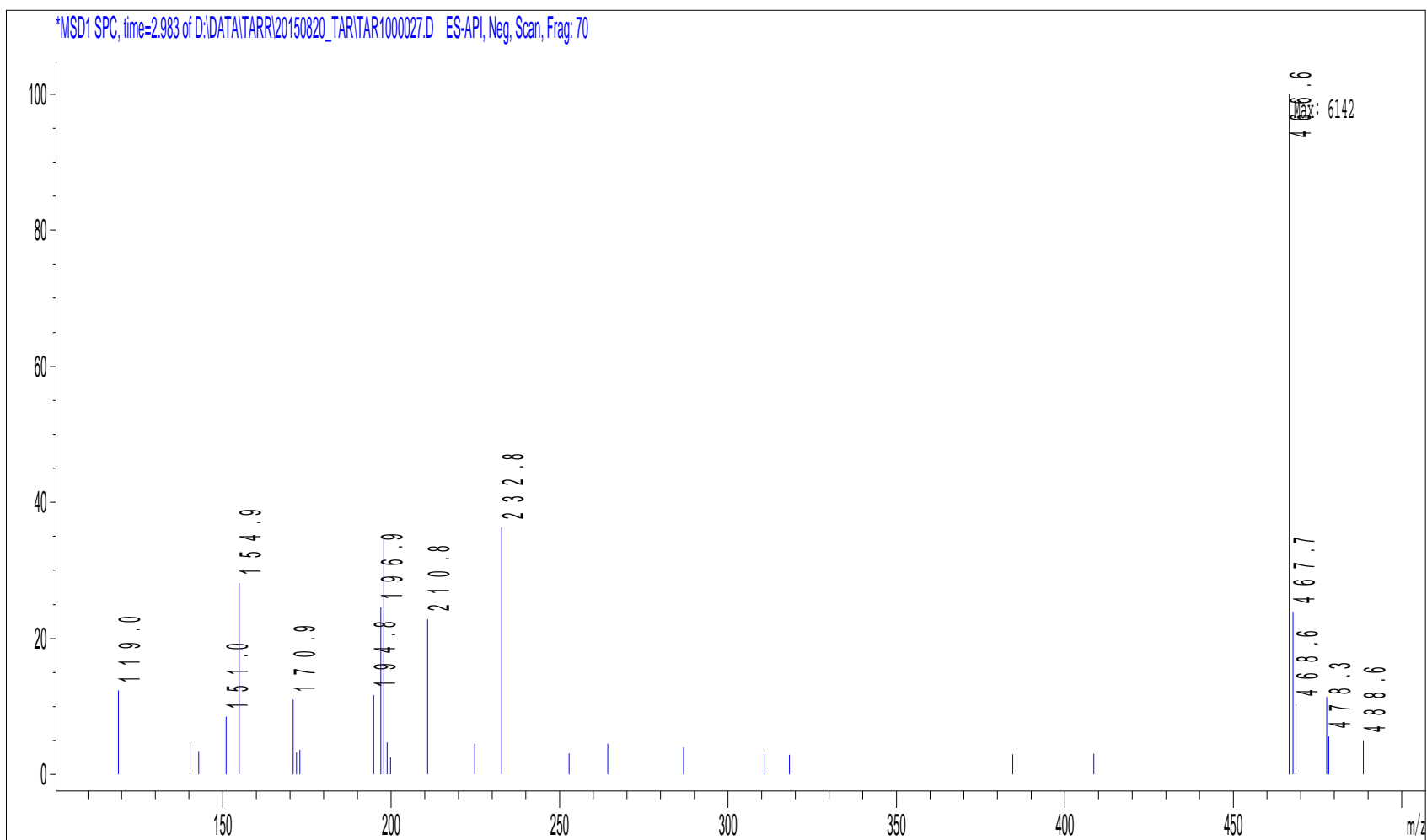
8

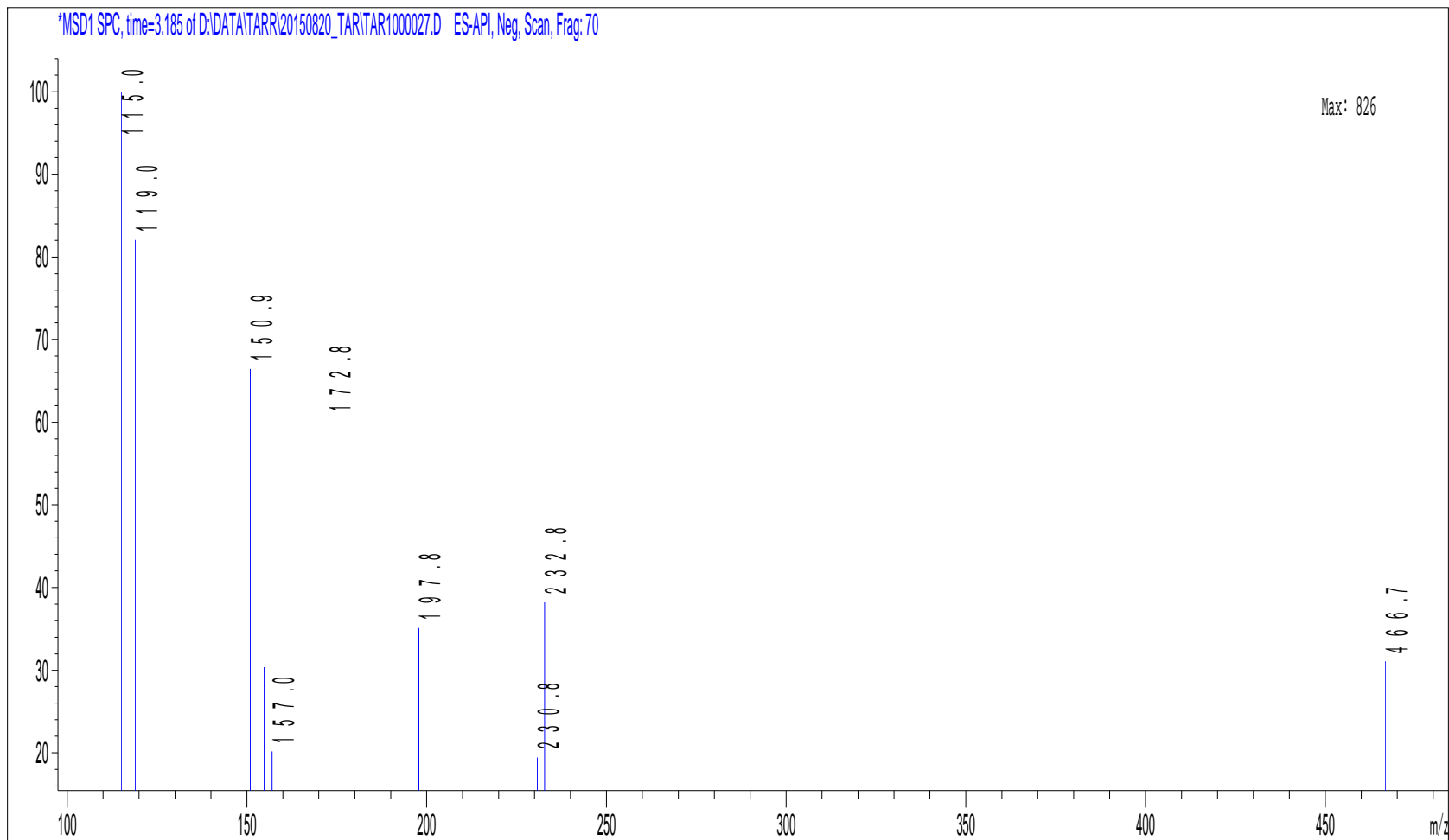
P2-C-09

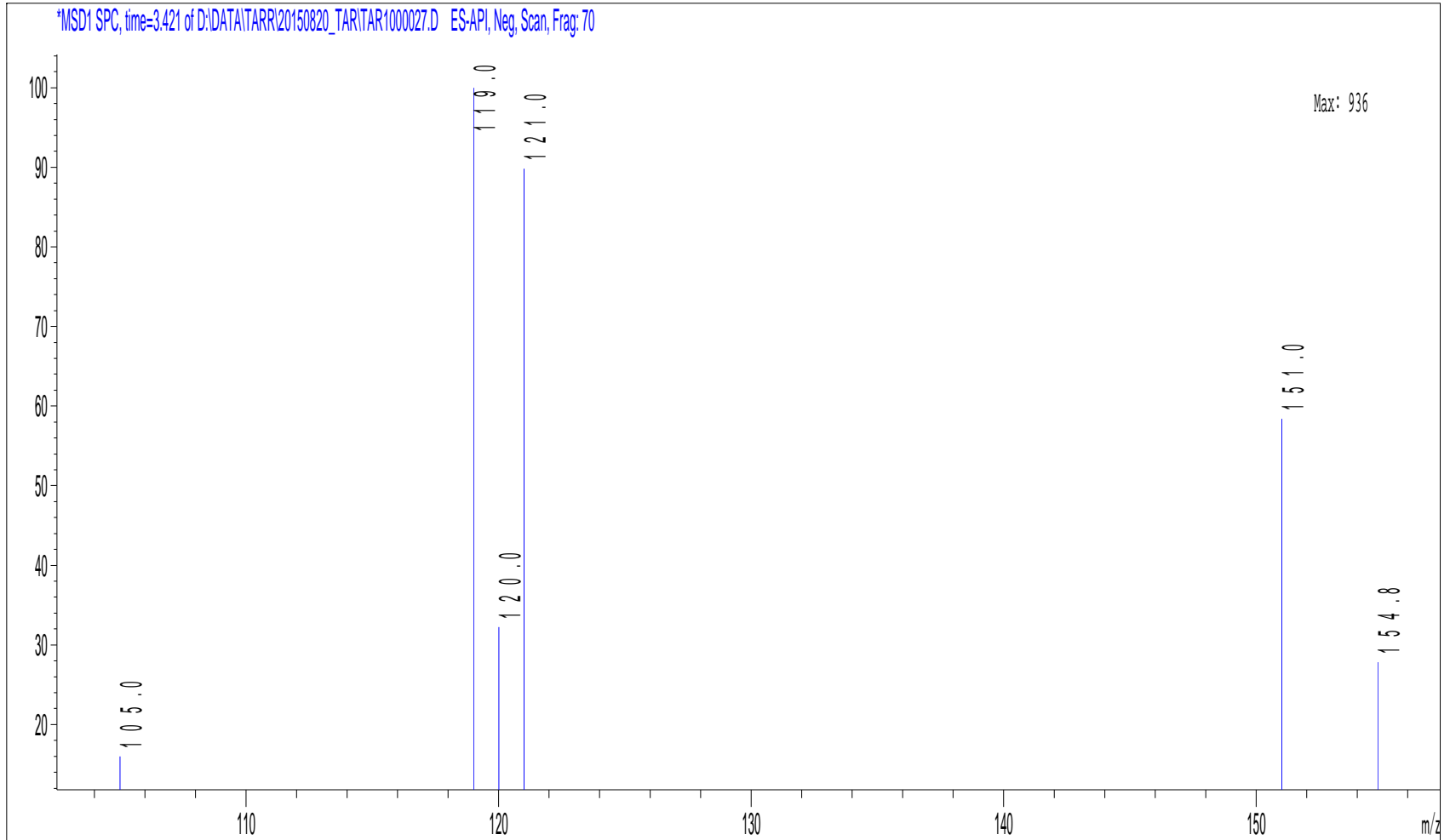


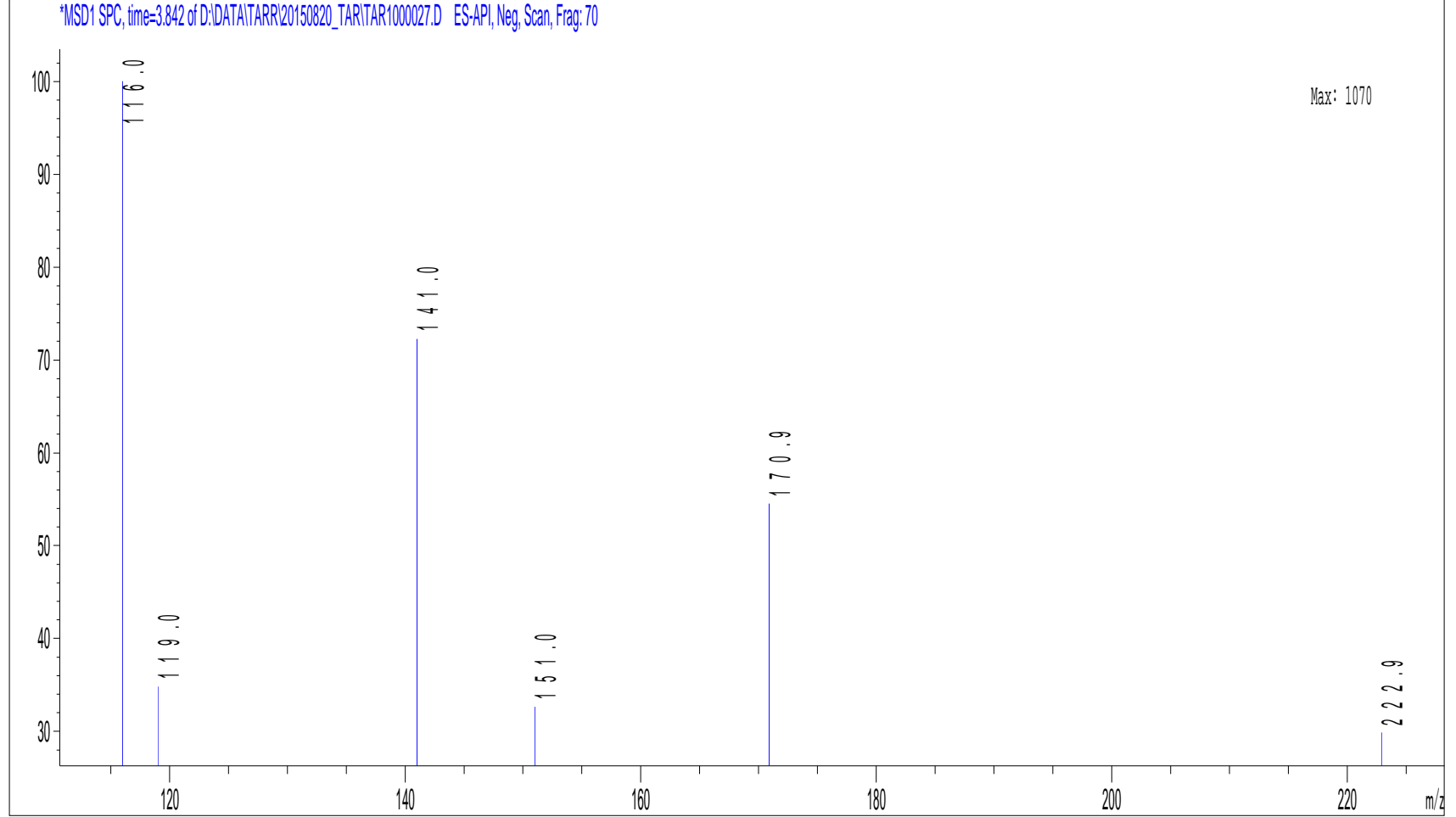


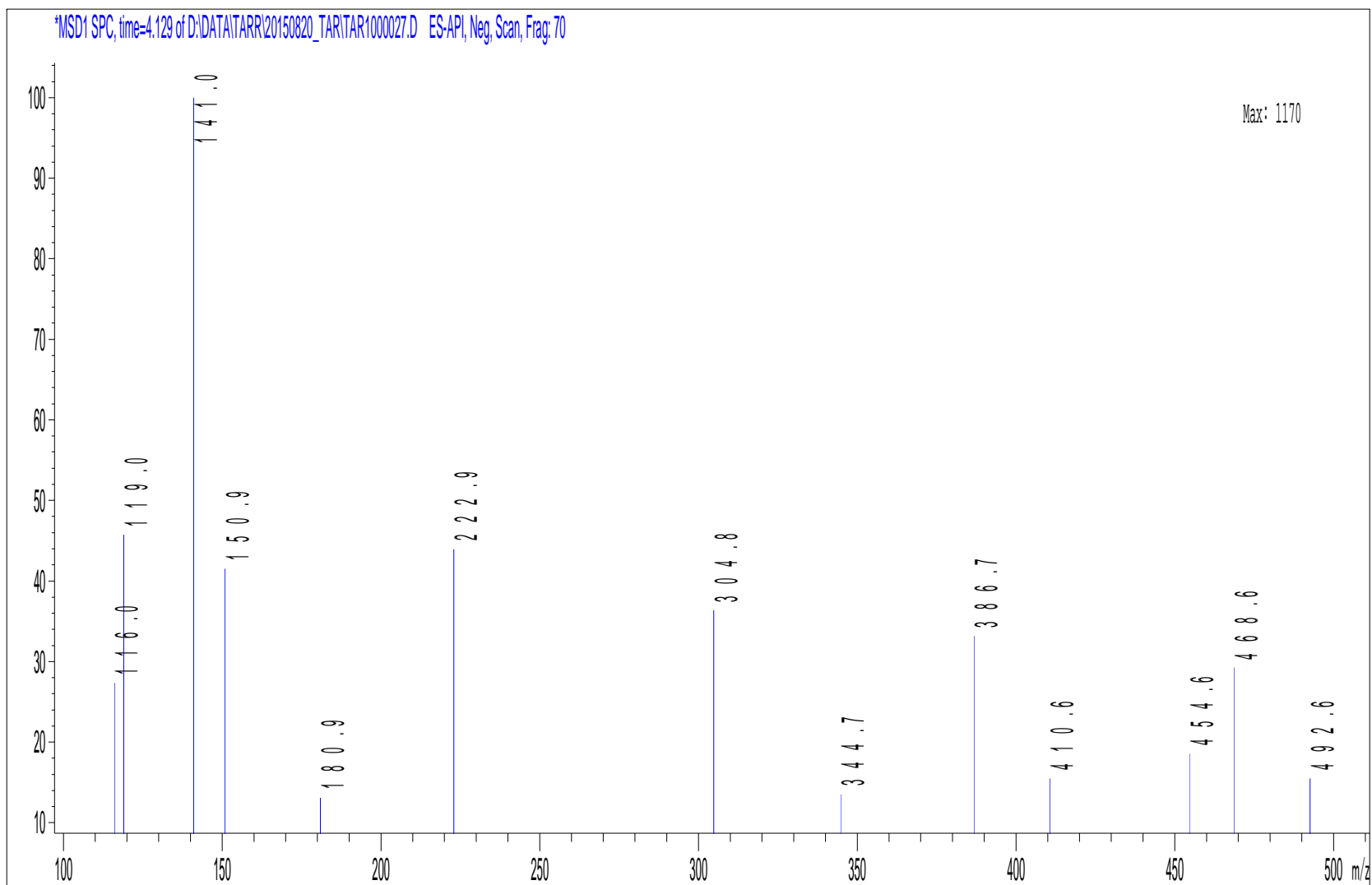
\*MSD1 SPC, time=2.983 of D:\DATA\TARRI\20150820\_TARITAR1000027.D ES-API, Neg, Scan, Frag: 70











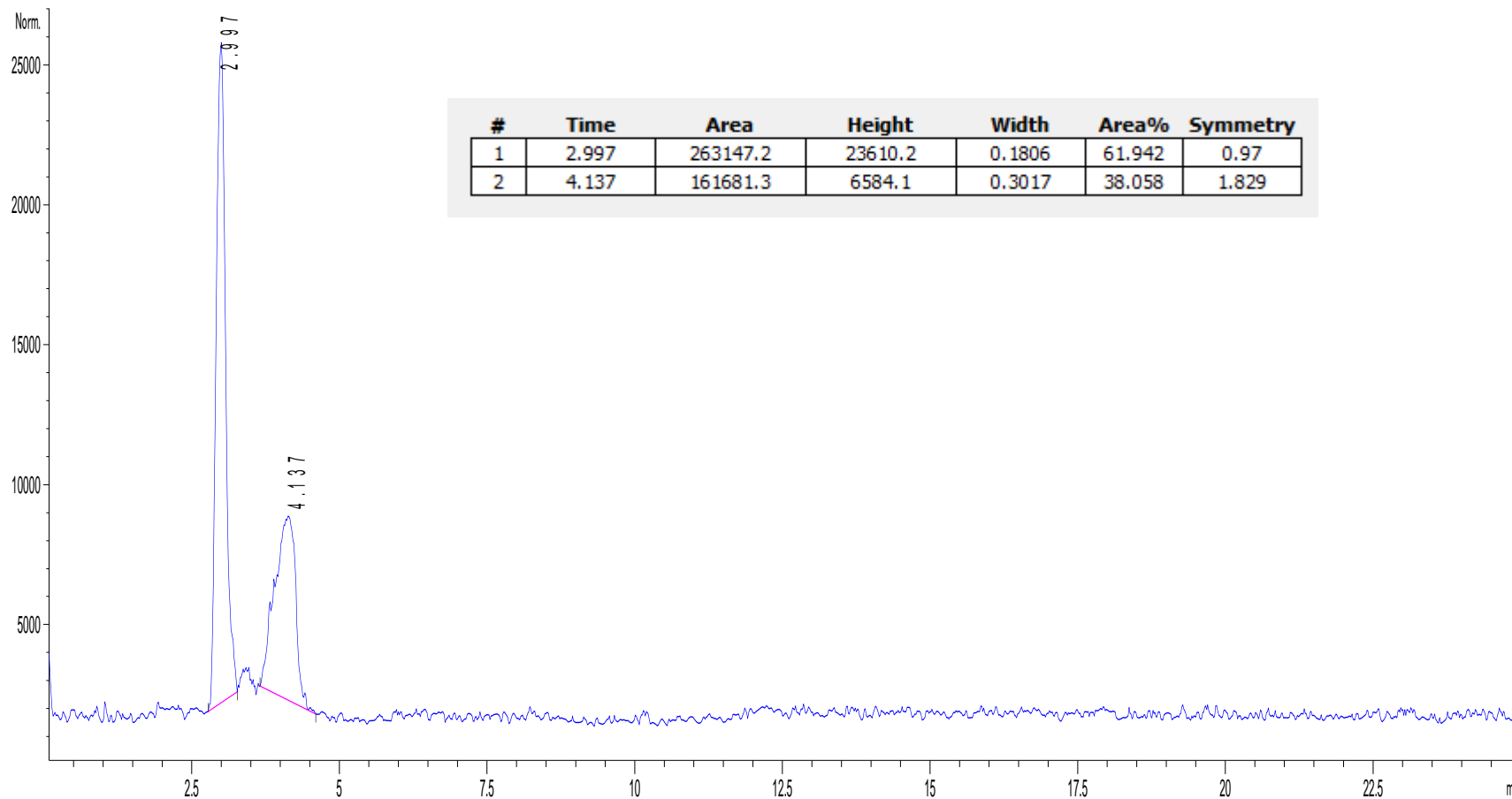
6-Jul-15

100 DC

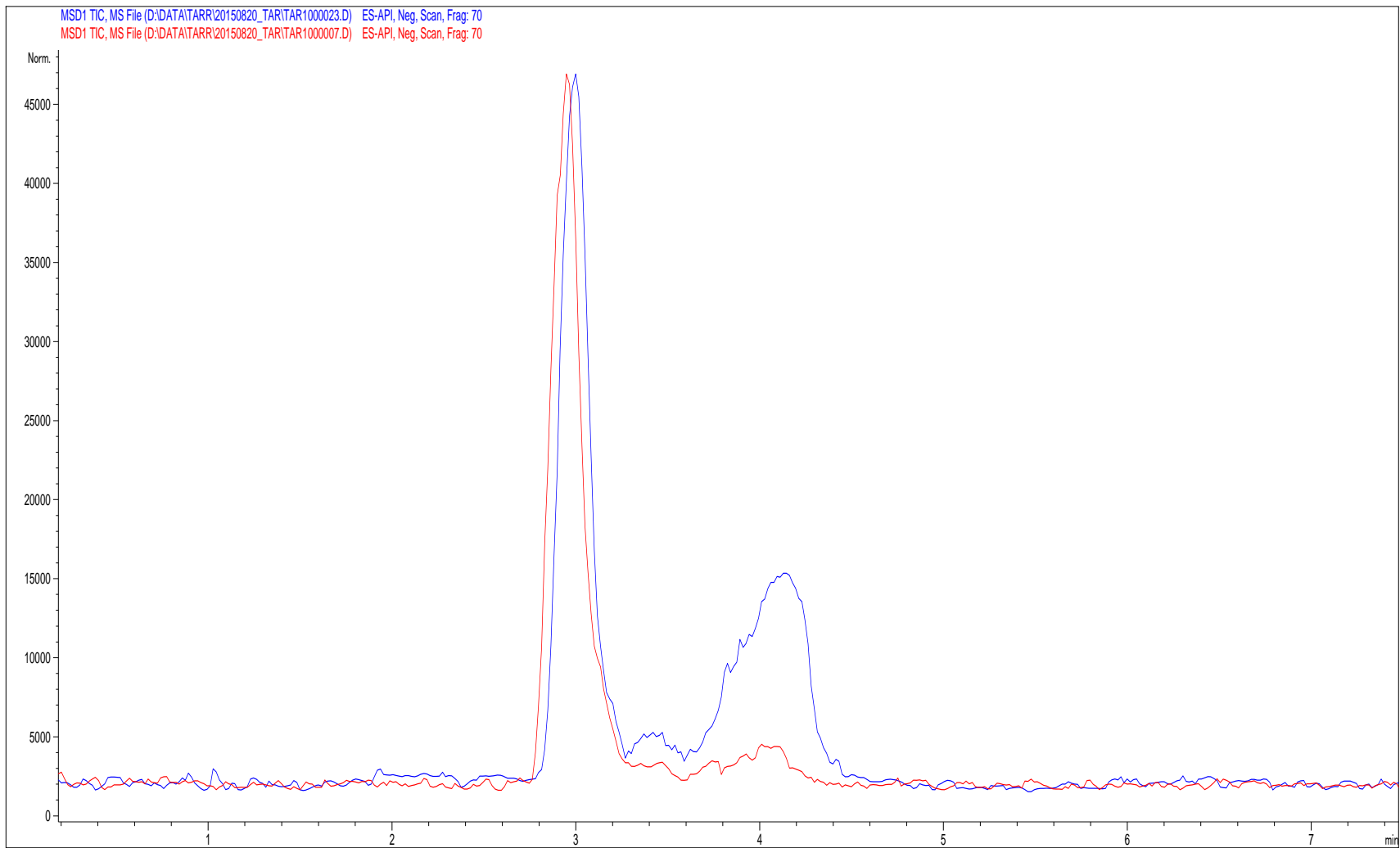
8

P2-C-05

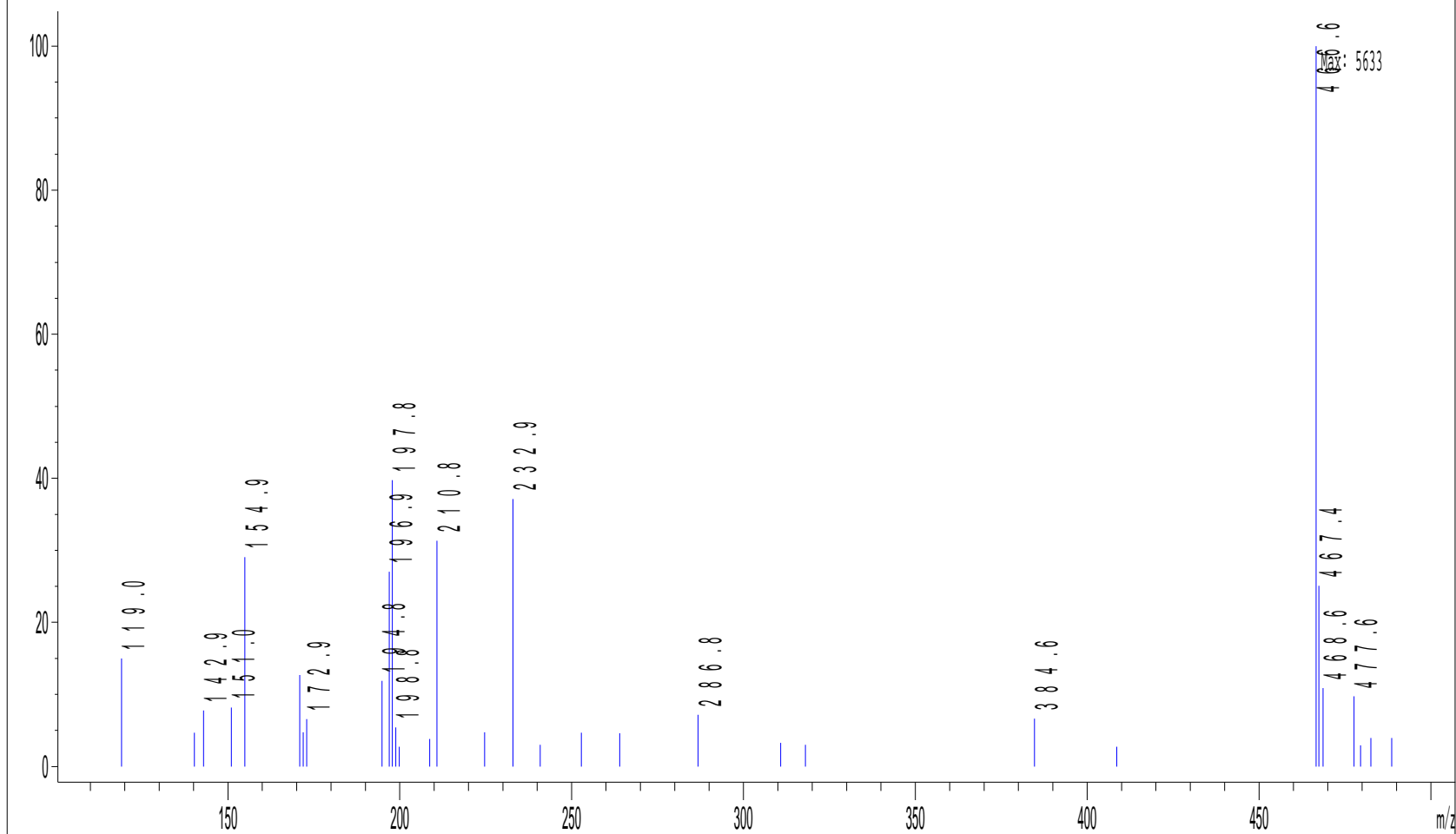
MSD1 TIC, MS File (D:\DATA\TARRI\20150820\_TAR\TAR1000023.D) ES-API, Neg, Scan, Frag: 70



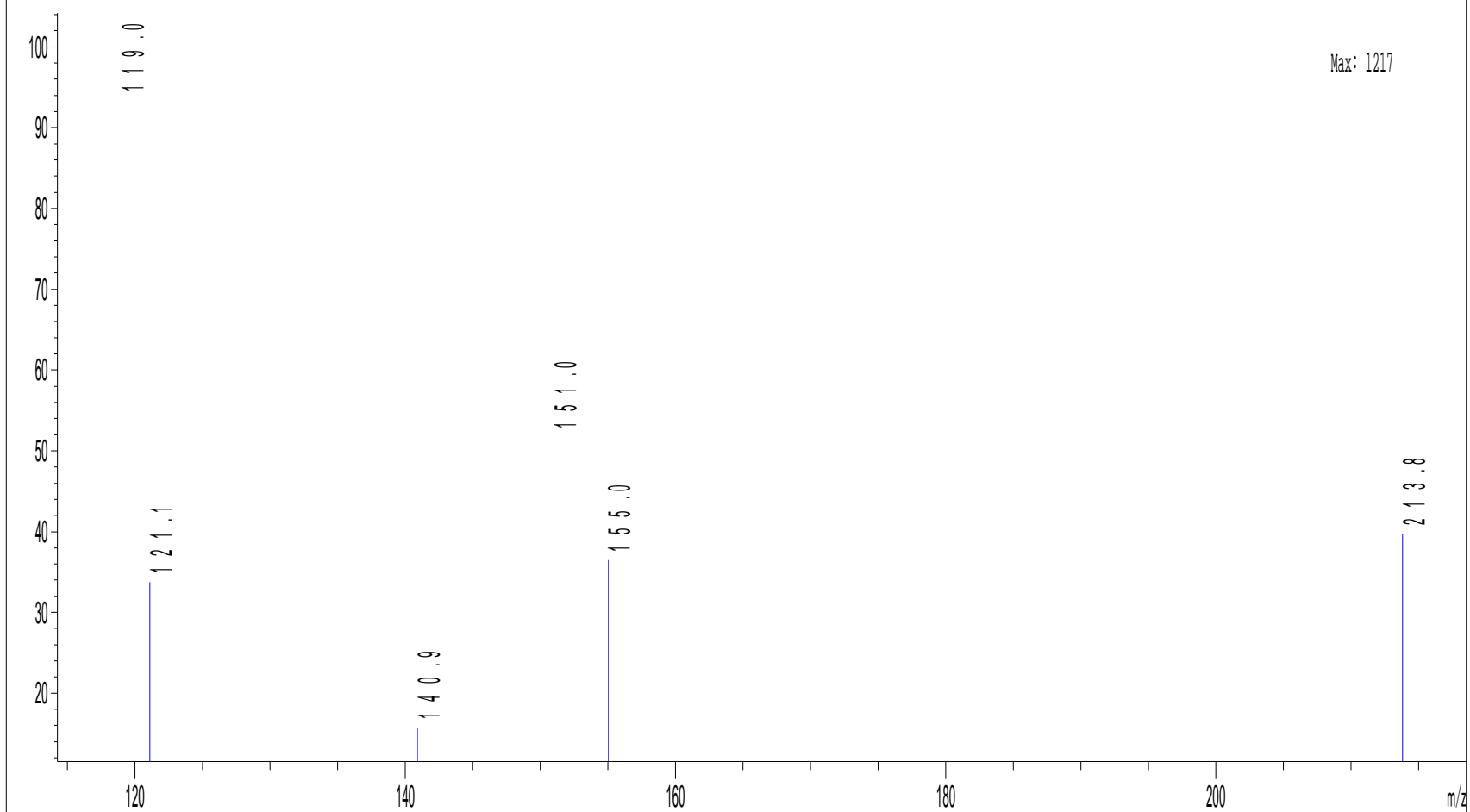


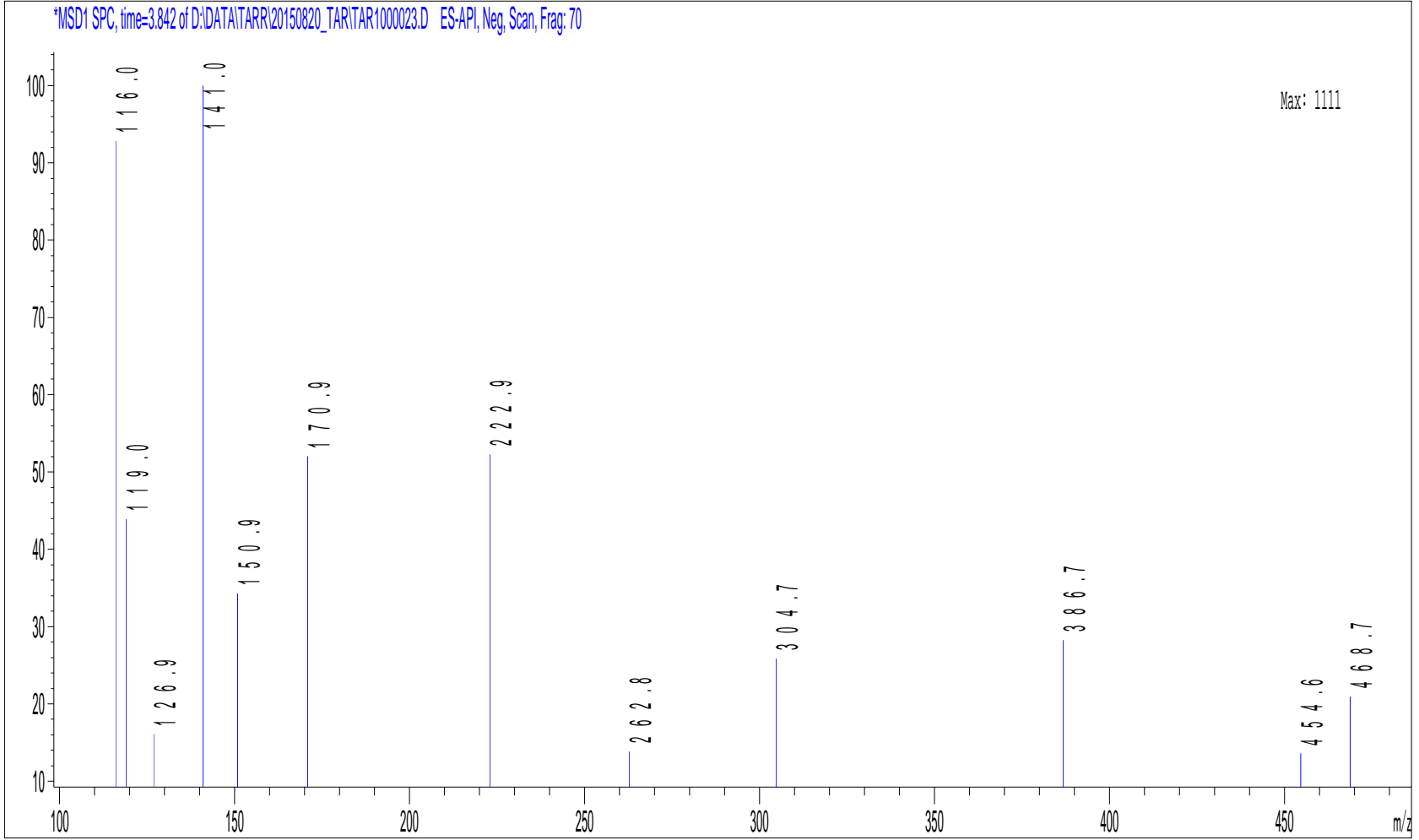


\*MSD1 SPC, time=3.016 of D:\DATA\TARR\20150820\_TARITAR1000023.D ES-API, Neg, Scan, Frag: 70

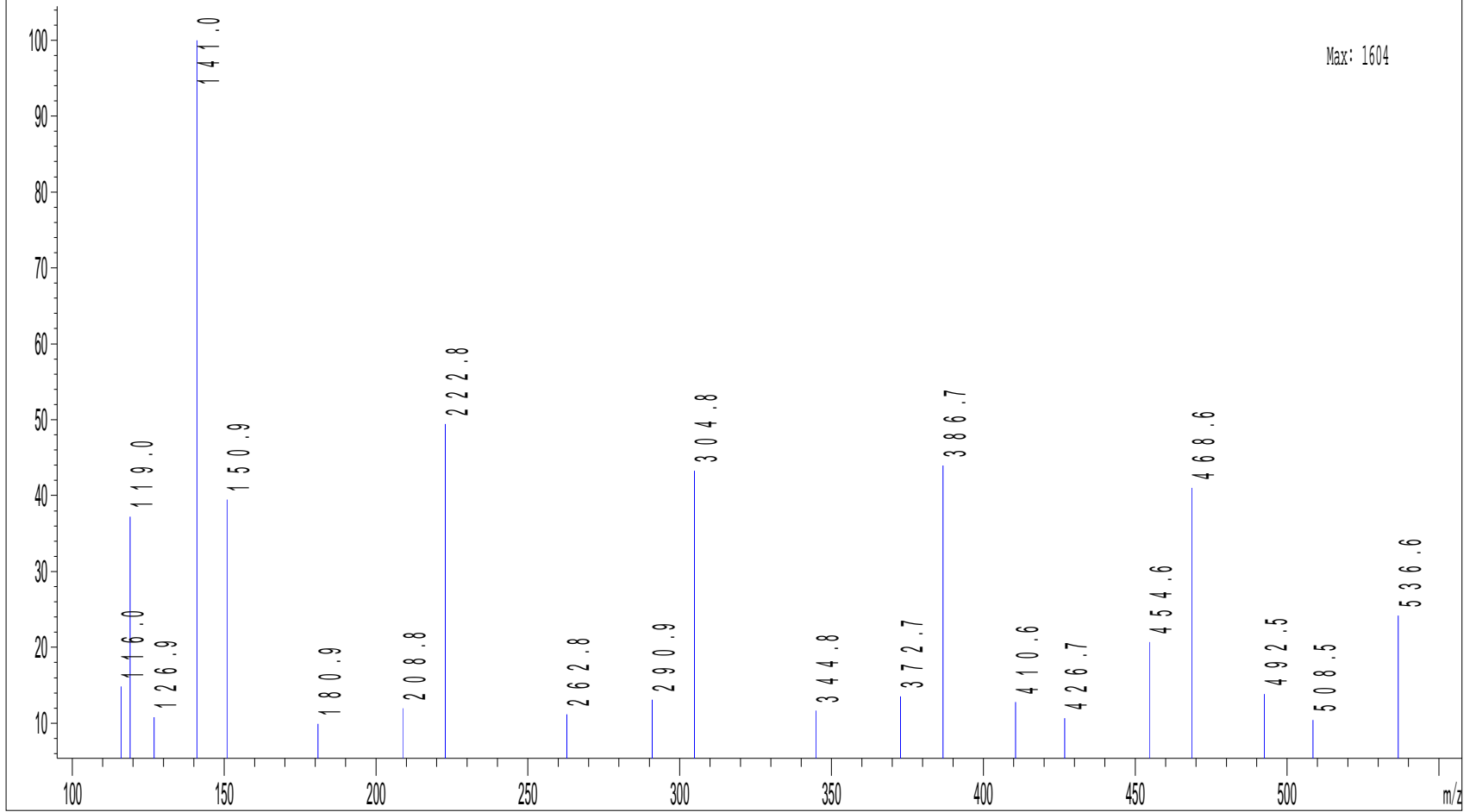


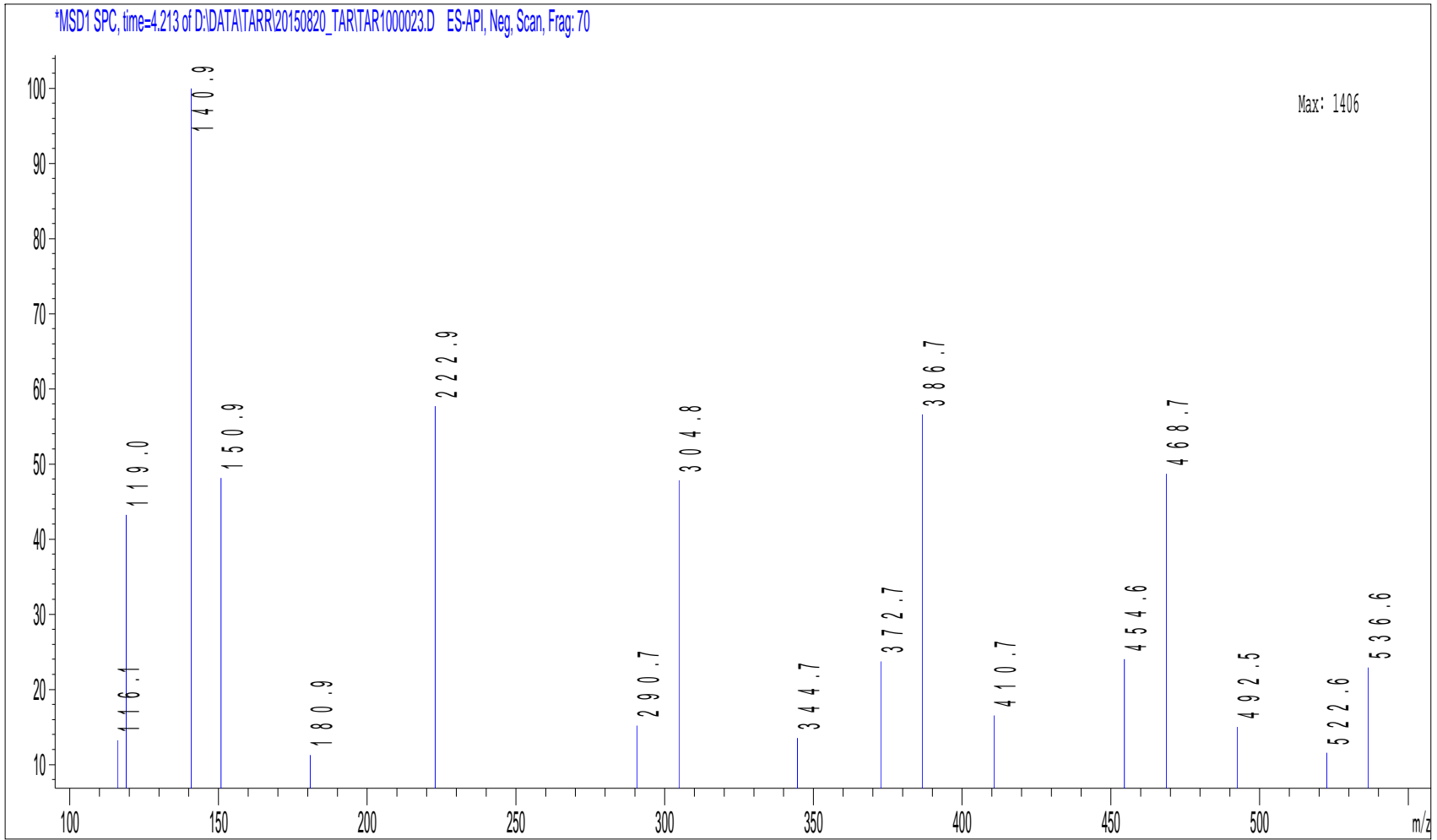
\*MSD1 SPC, time=3.404 of D:\DATA\TARR\20150820\_TARITAR1000023.D ES-API, Neg, Scan, Frag: 70





\*MSD1 SPC, time=4.112 of D:\DATA\TARR\20150820\_TARITAR1000023.D ES-API, Neg, Scan, Frag: 70



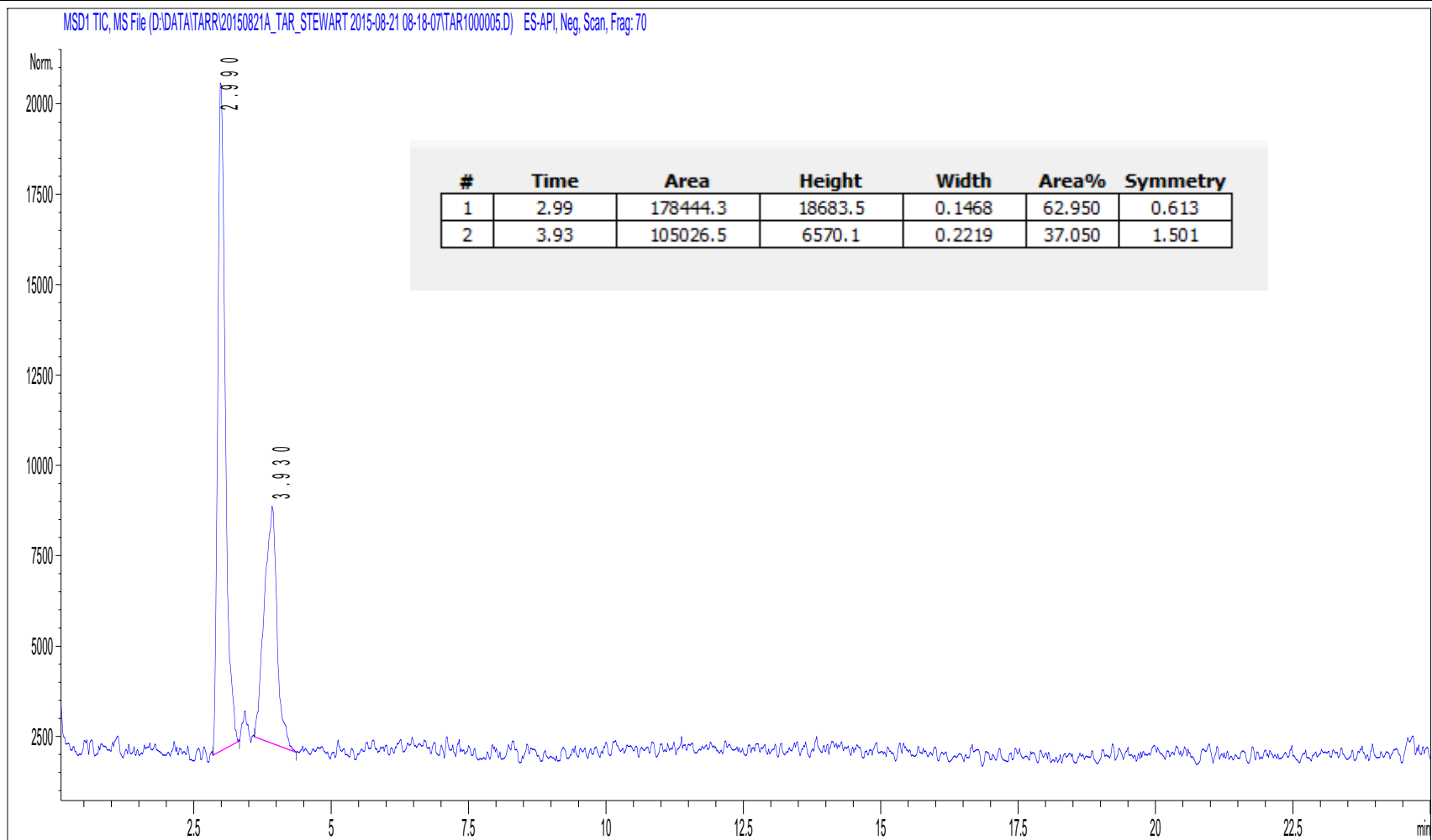


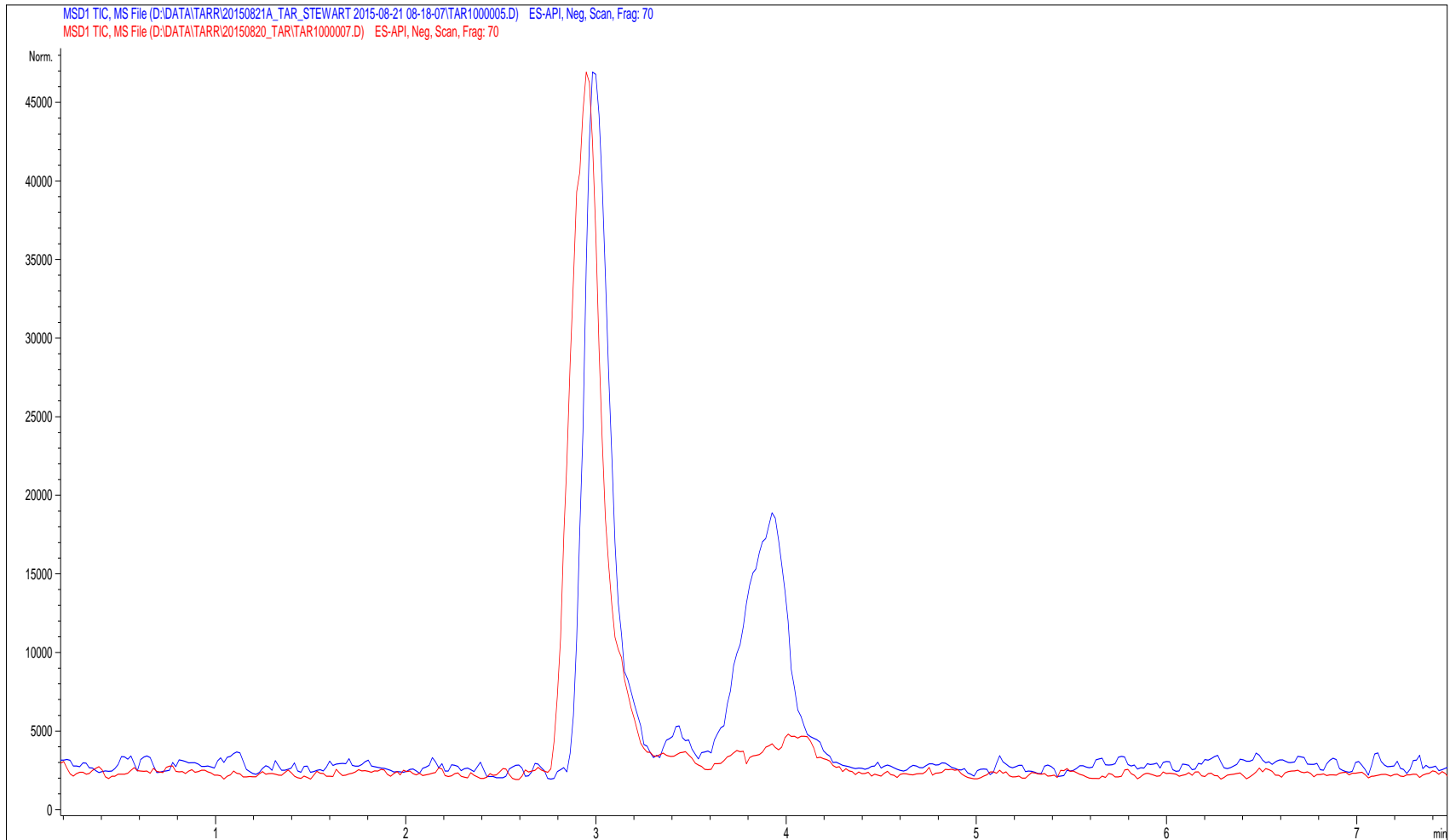
13-Aug-15

100 DC Repeat

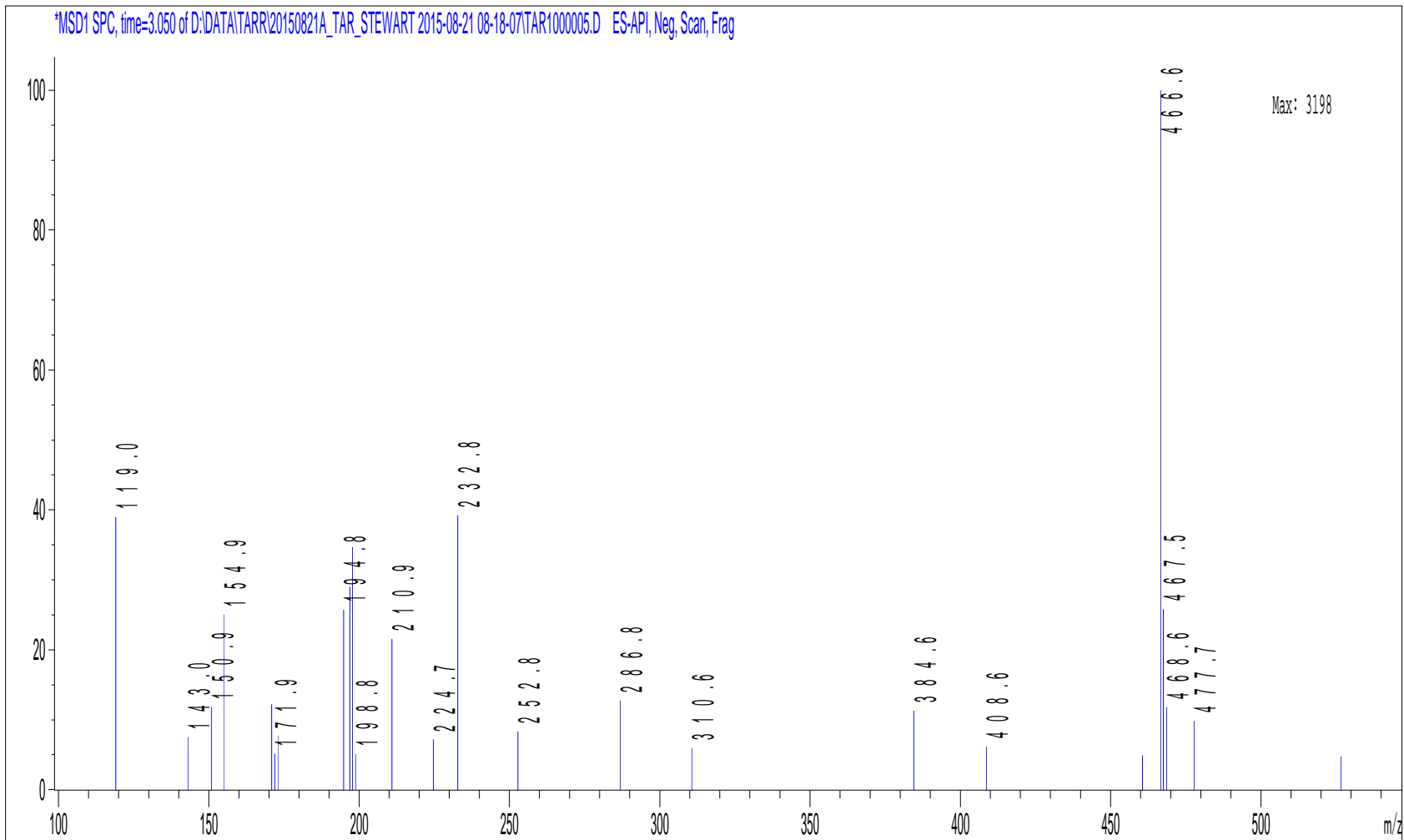
8

P2-E-04

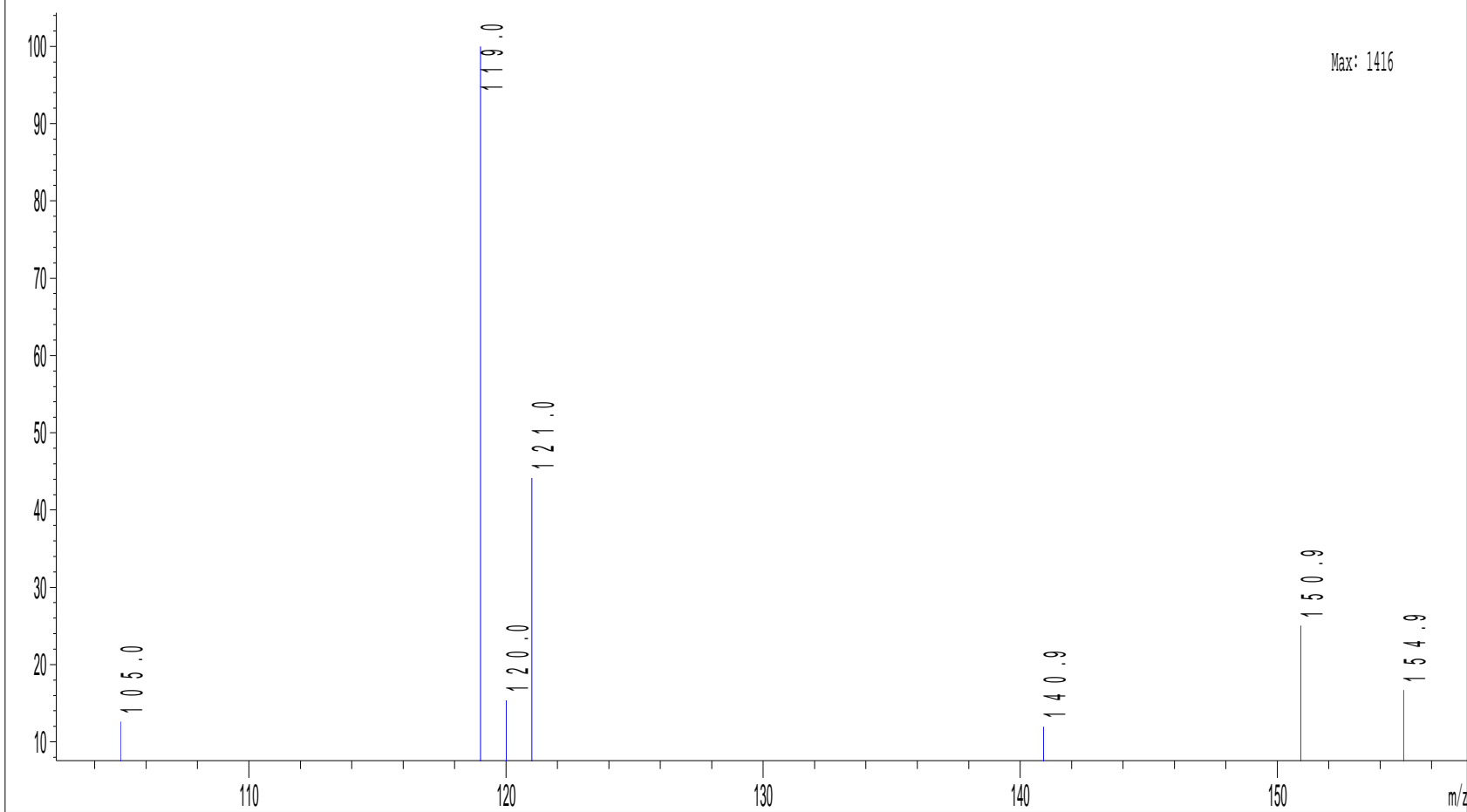




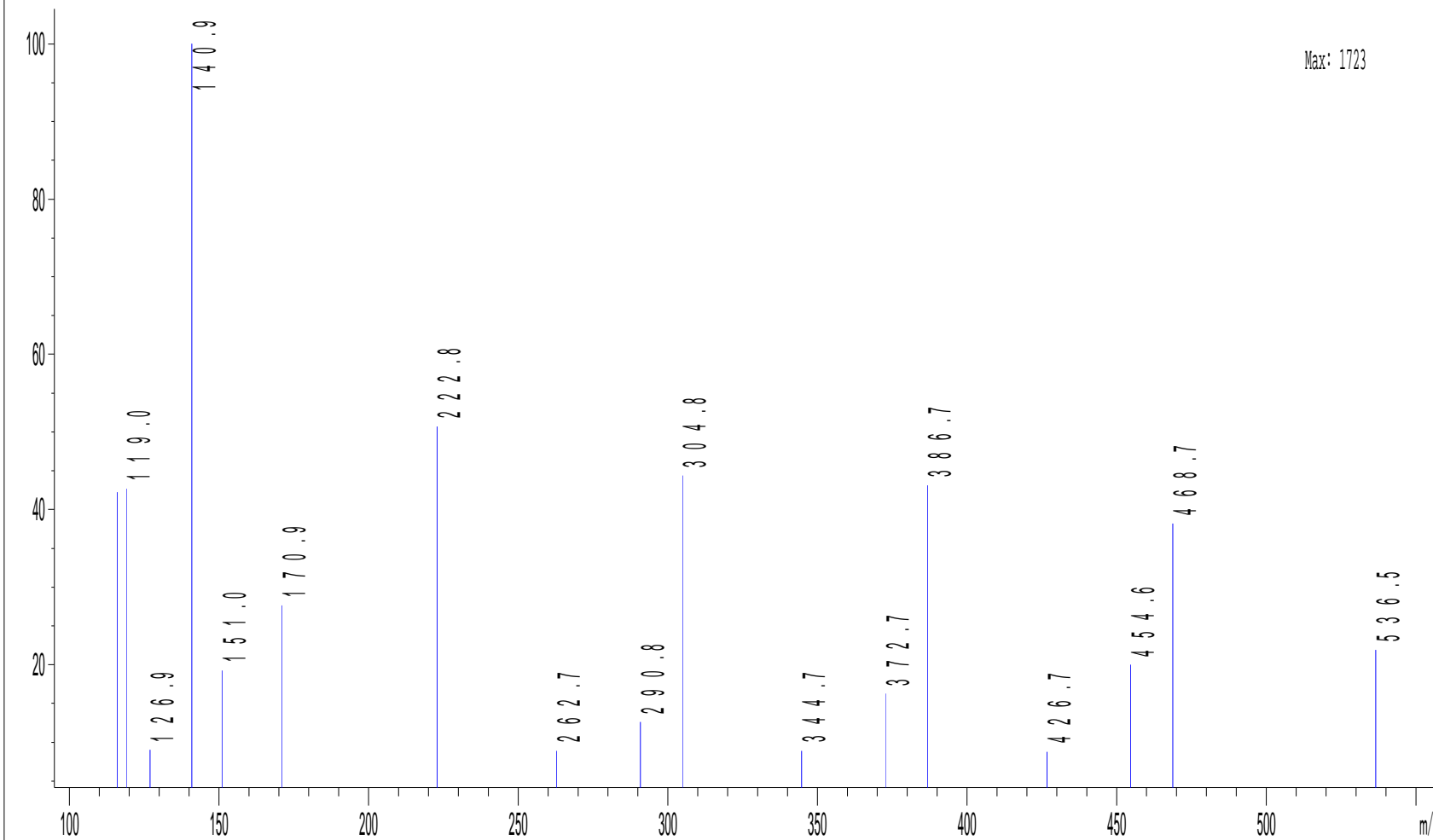




\*MSD1 SPC, time=3.438 of D:\DATA\TARR\20150821A\_TAR\_STEWART 2015-08-21 08-18-07\TAR1000005.D ES-API, Neg, Scan, Frag

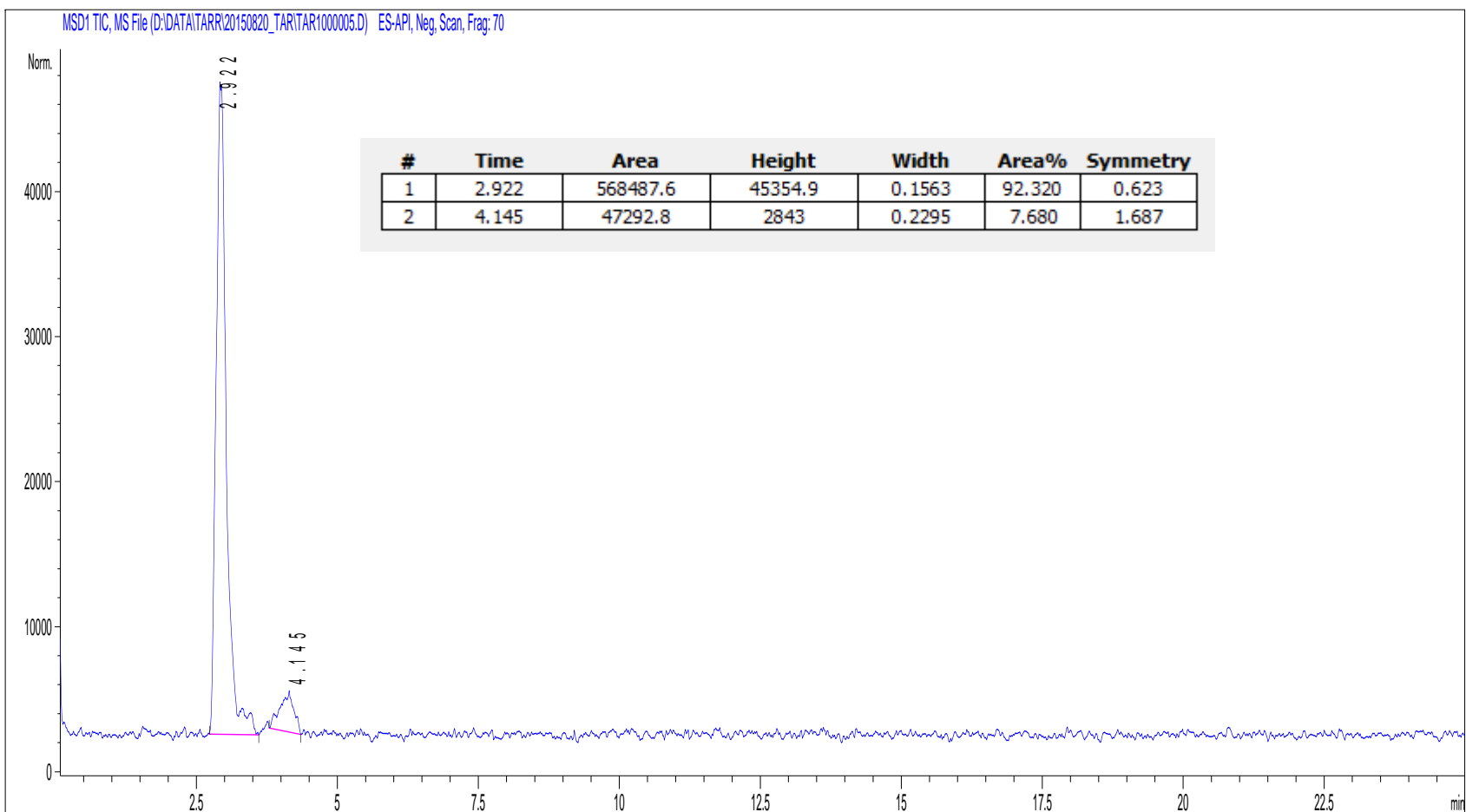


\*MSD1 SPC, time=3.926 of D:\DATA\TARR\20150821A\_TAR\_STEWART 2015-08-21 08-18-07\TAR1000005.D ES-API, Neg, Scan, Frag

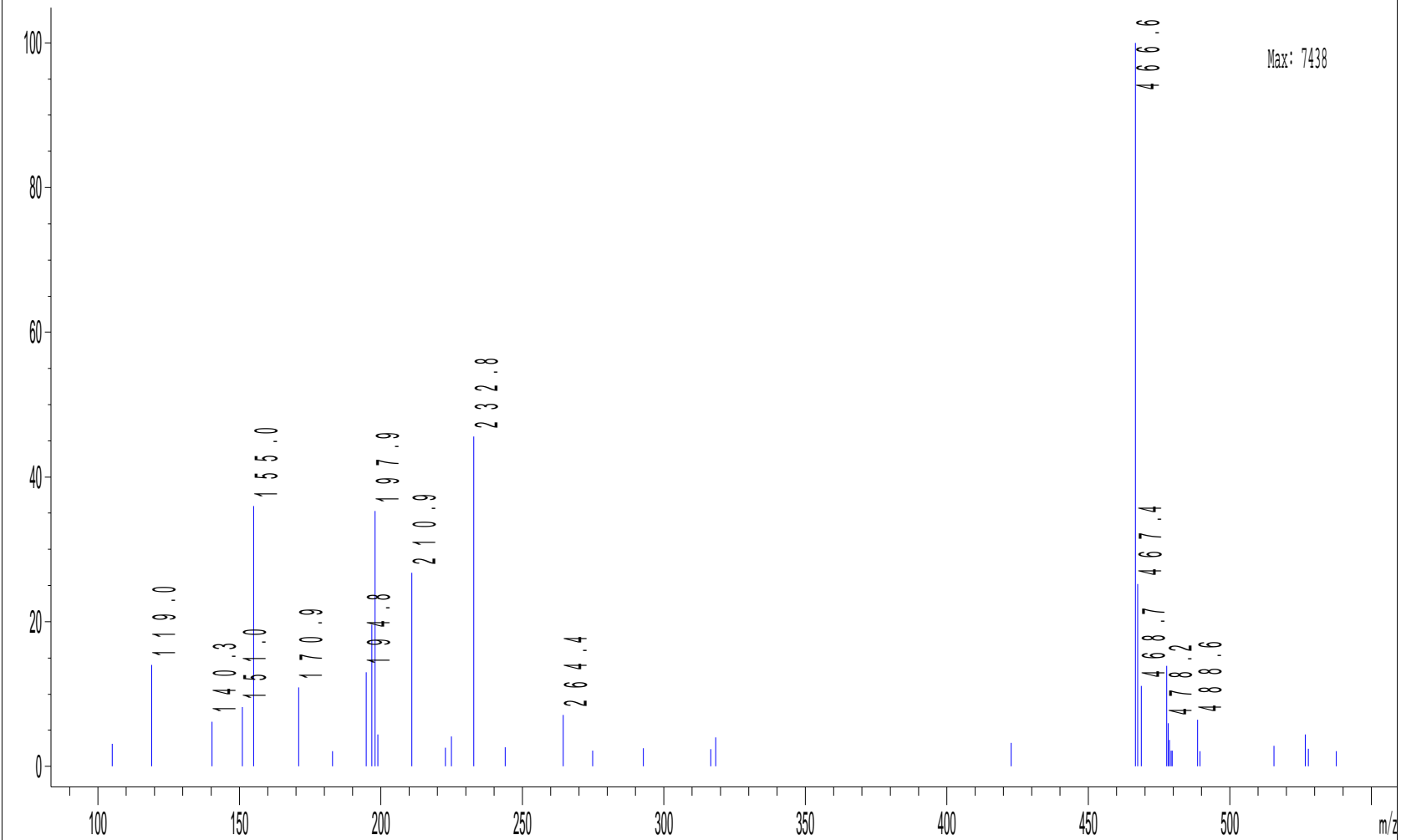


pH 9

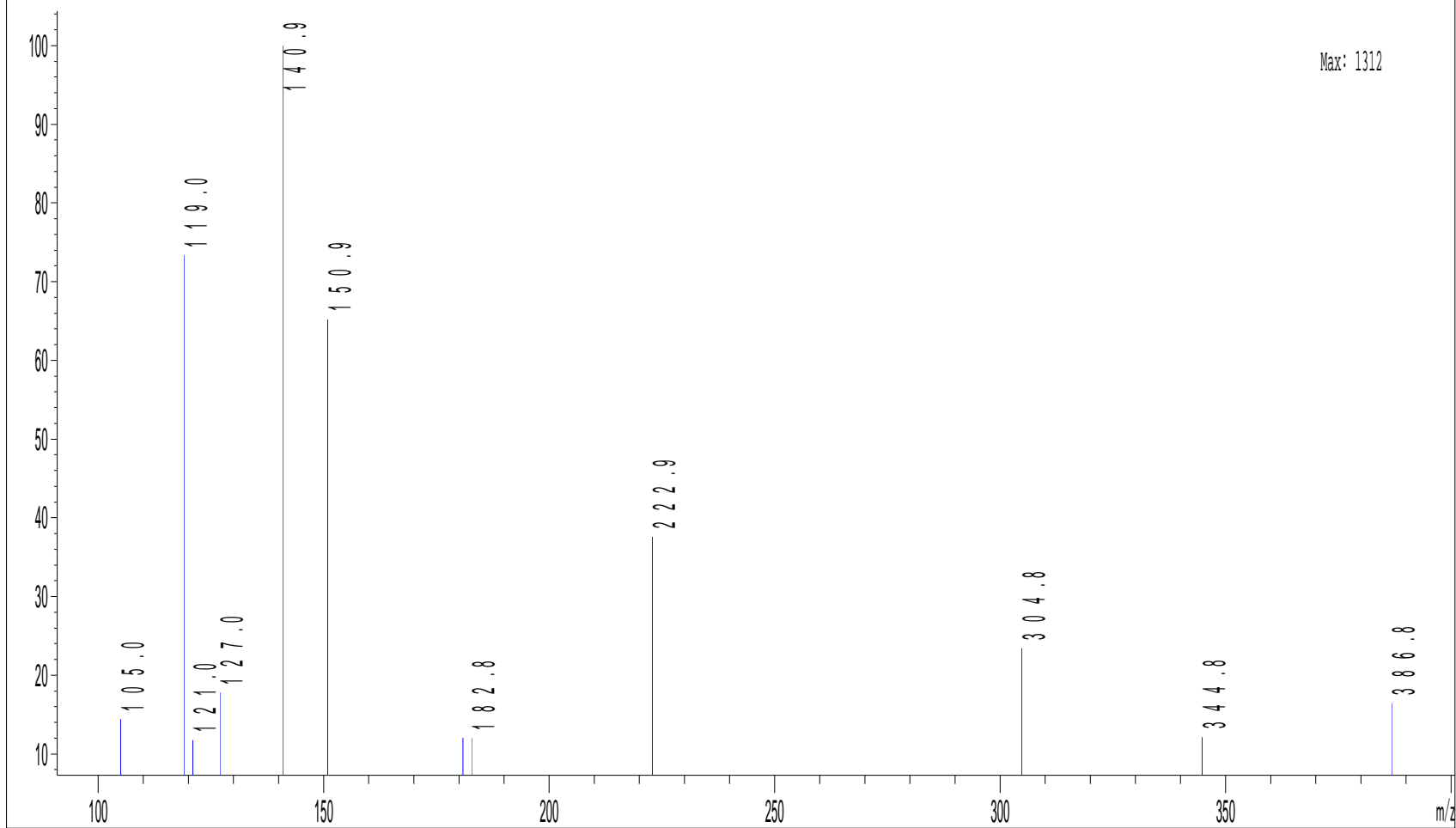
8-Apr-15  
H2O2 Ctrl  
9  
P2-A-05



\*MSD1 SPC, time=2.999 of D:\DATA\TARR\20150820\_TARITAR1000005.D ES-API, Neg. Scan, Frag: 70



\*MSD1 SPC, time=4.129 of D:\DATA\TARR\20150820\_TARITAR1000005.D ES-API, Neg, Scan, Frag: 70

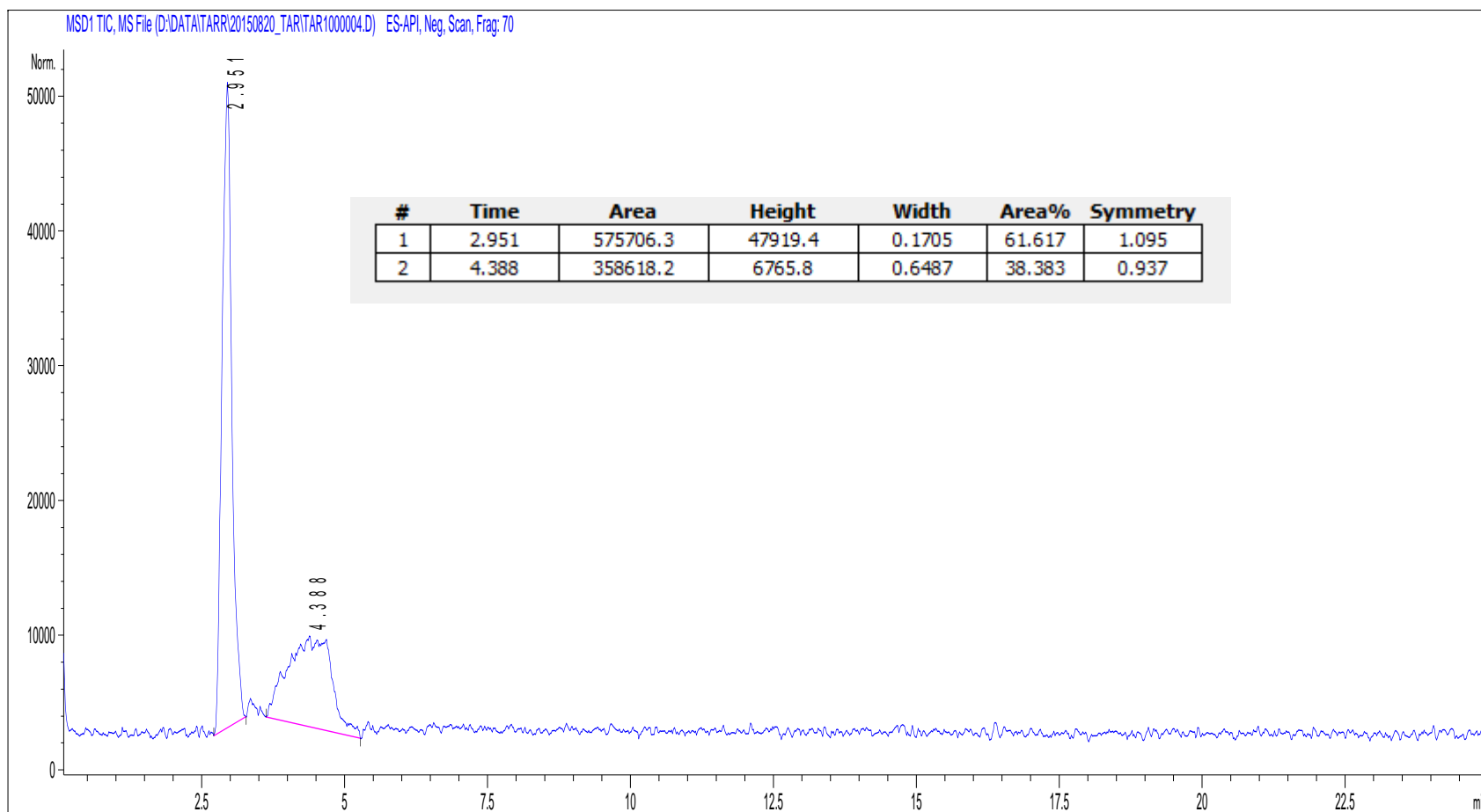


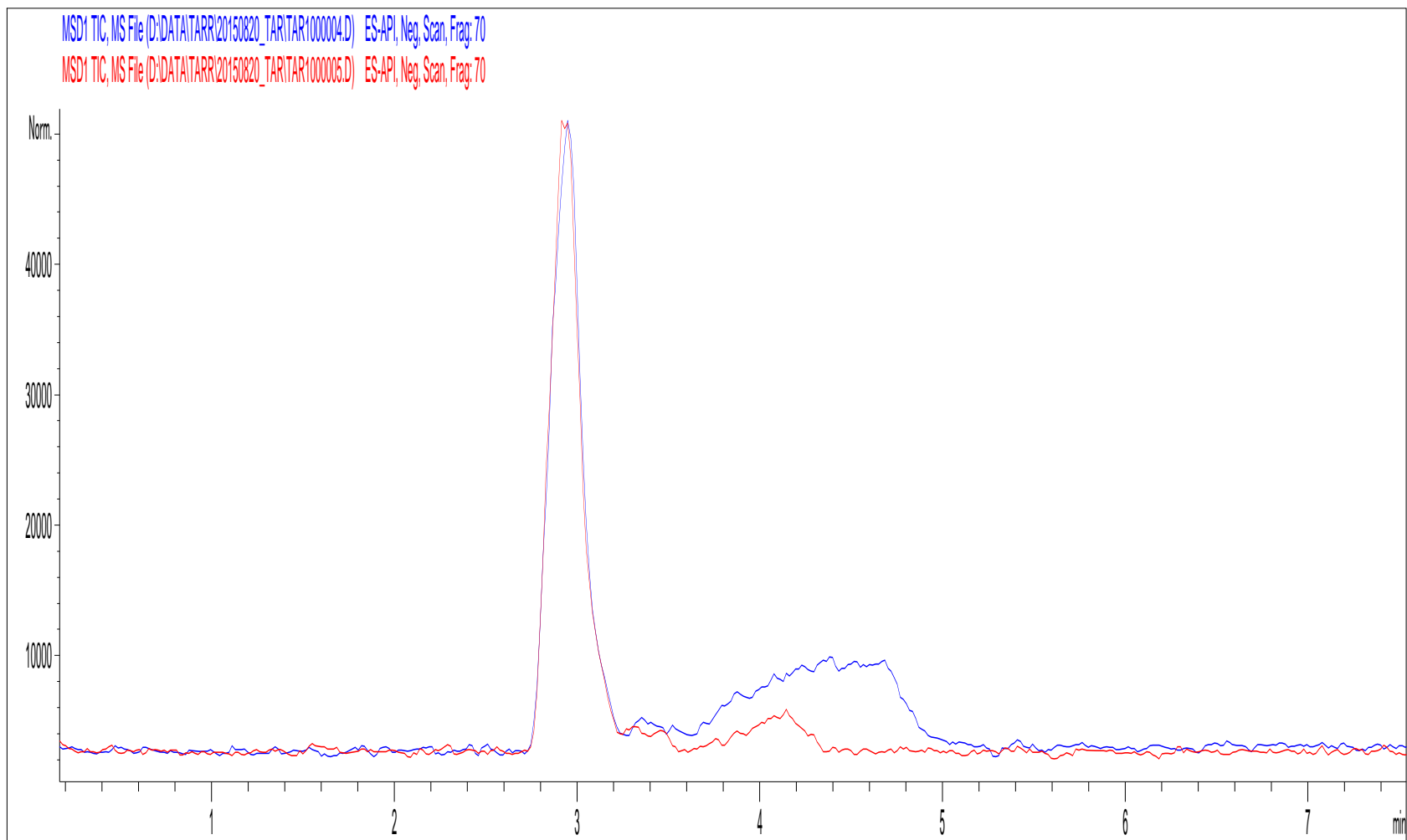
16-Mar-15

0 DC

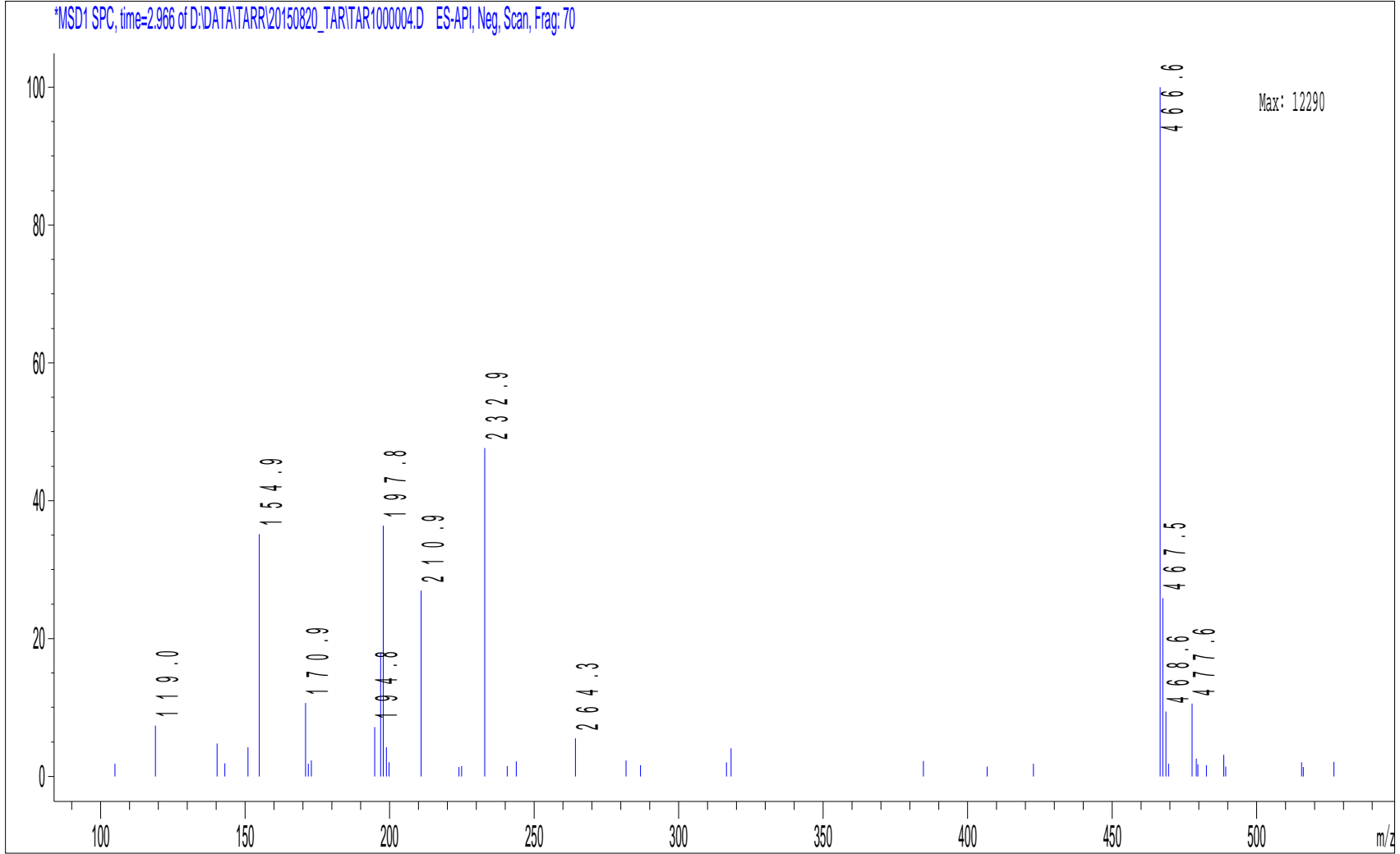
9

P2-A-04

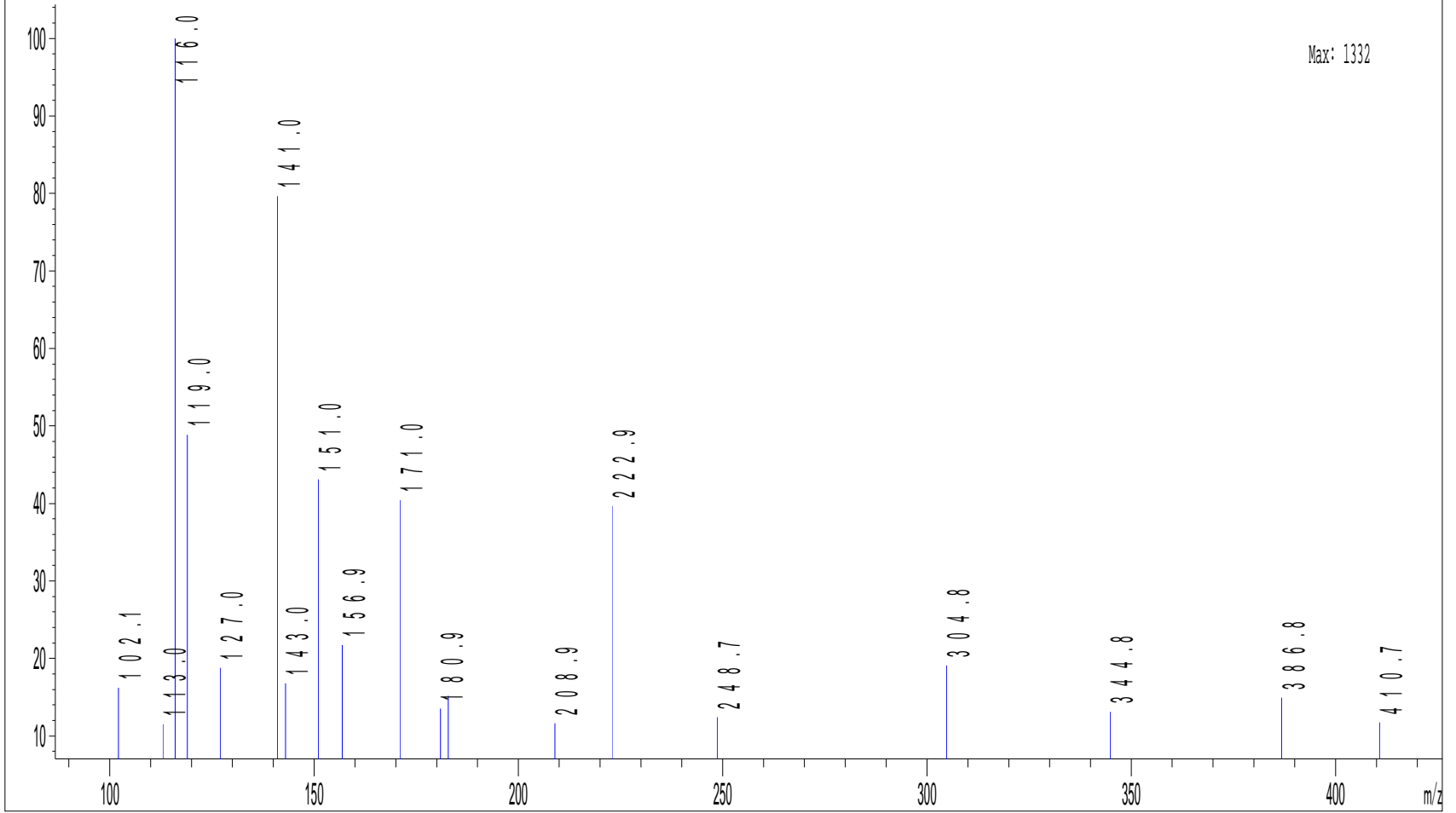




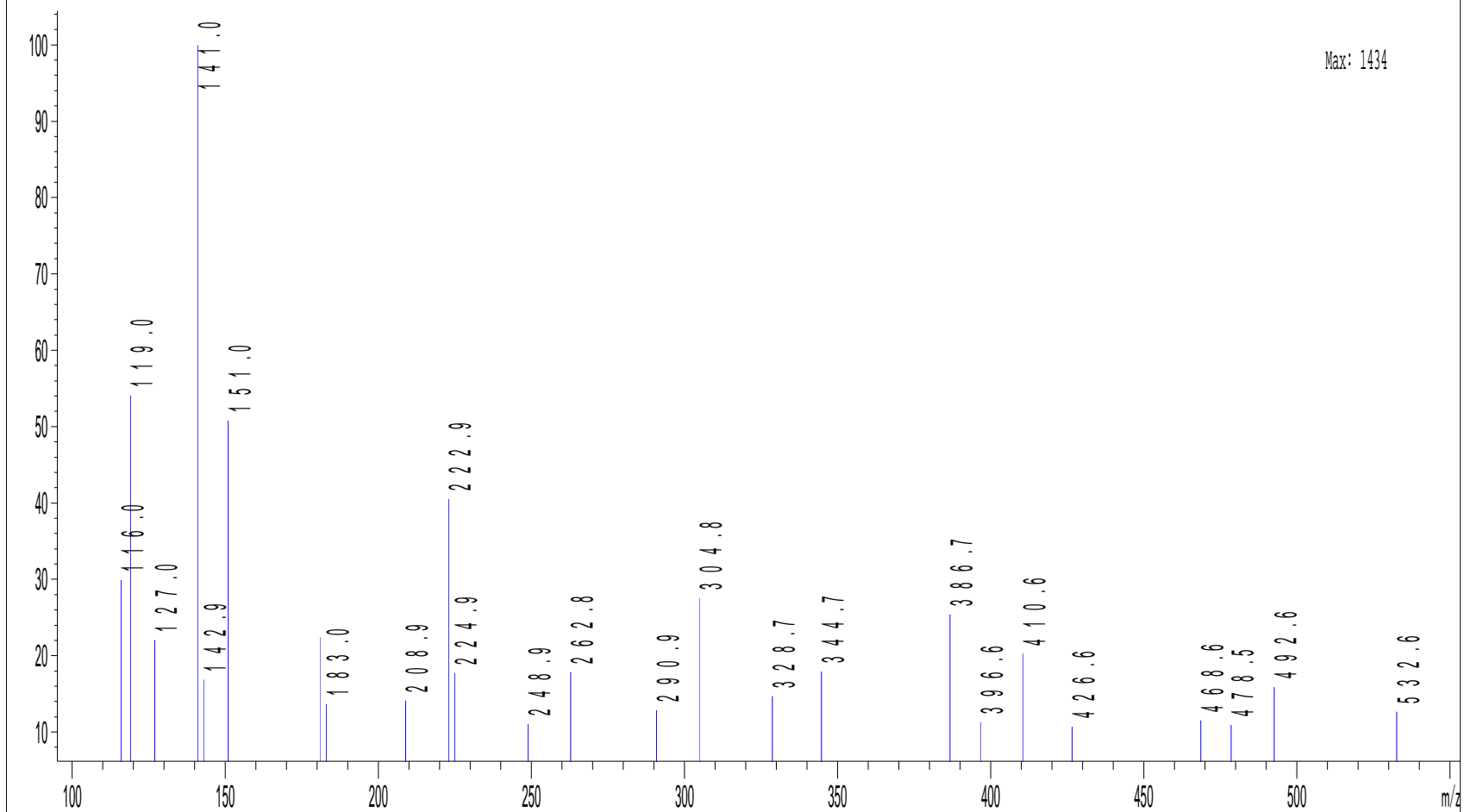




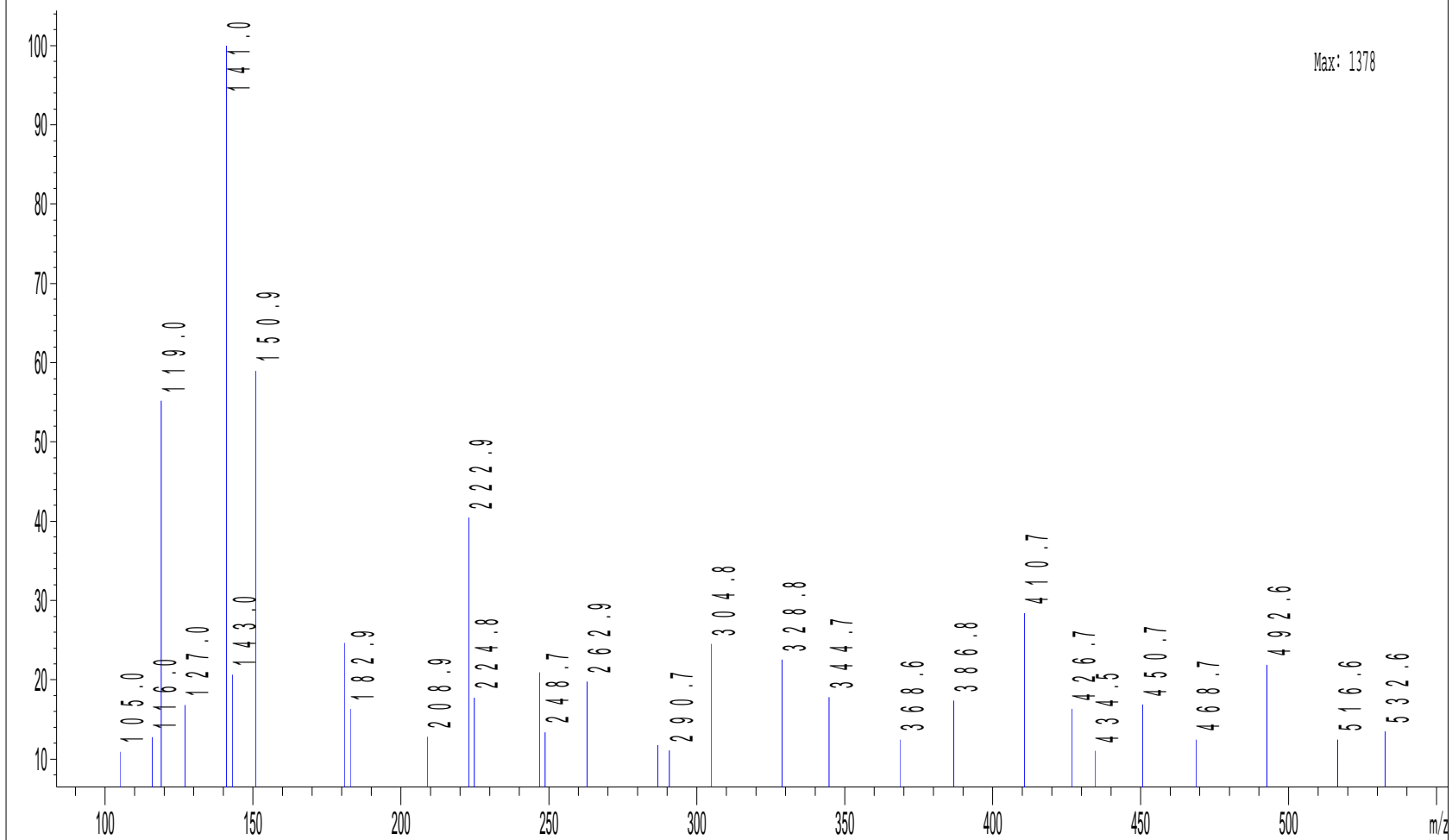
\*MSD1 SPC, time=3.876 of D:\DATA\TARR\20150820\_TARITAR1000004.D ES-API, Neg, Scan, Frag: 70



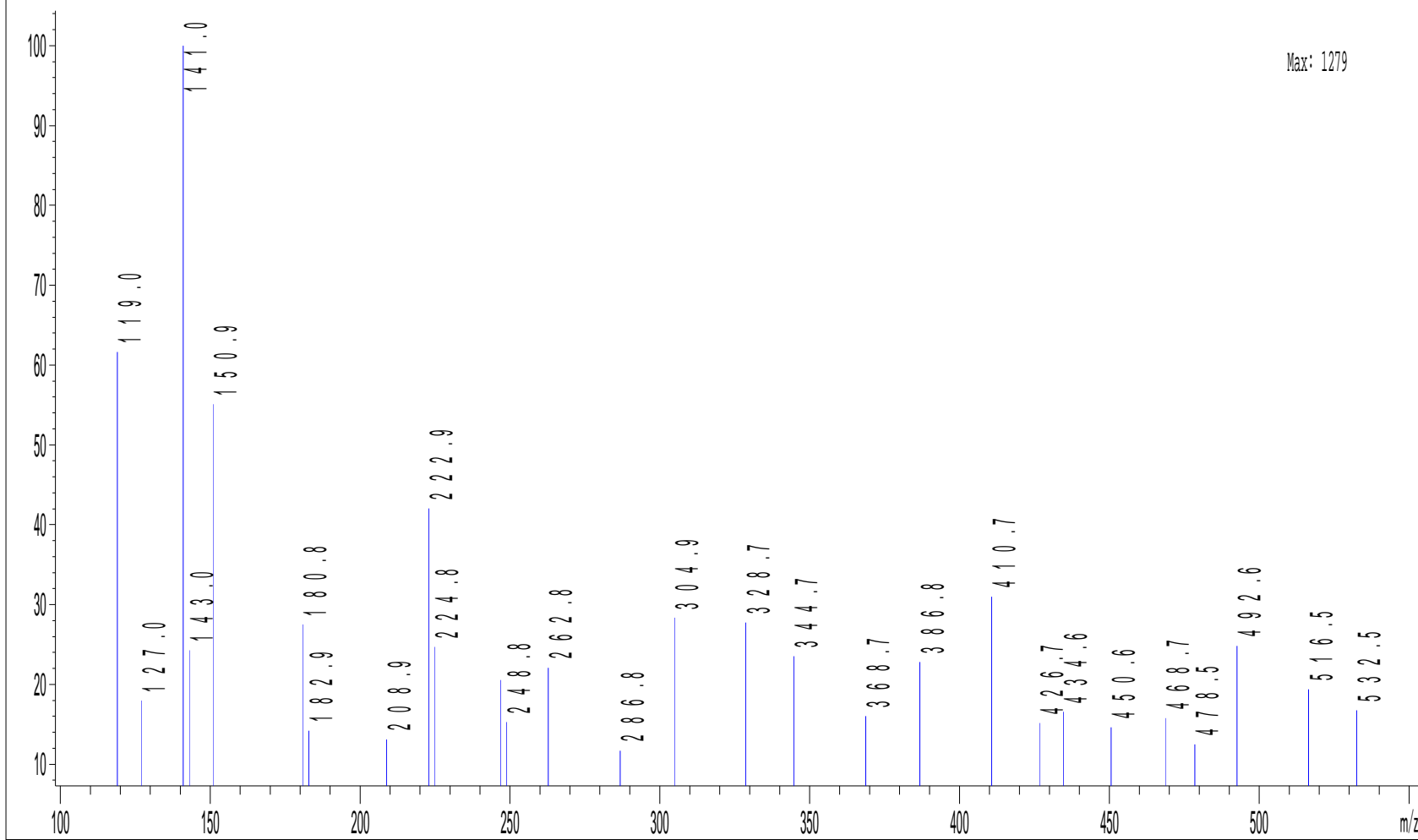
\*MSD1 SPC, time=4.078 of D:\DATA\TARR\20150820\_TARITAR1000004.D ES-API, Neg. Scan, Frag: 70



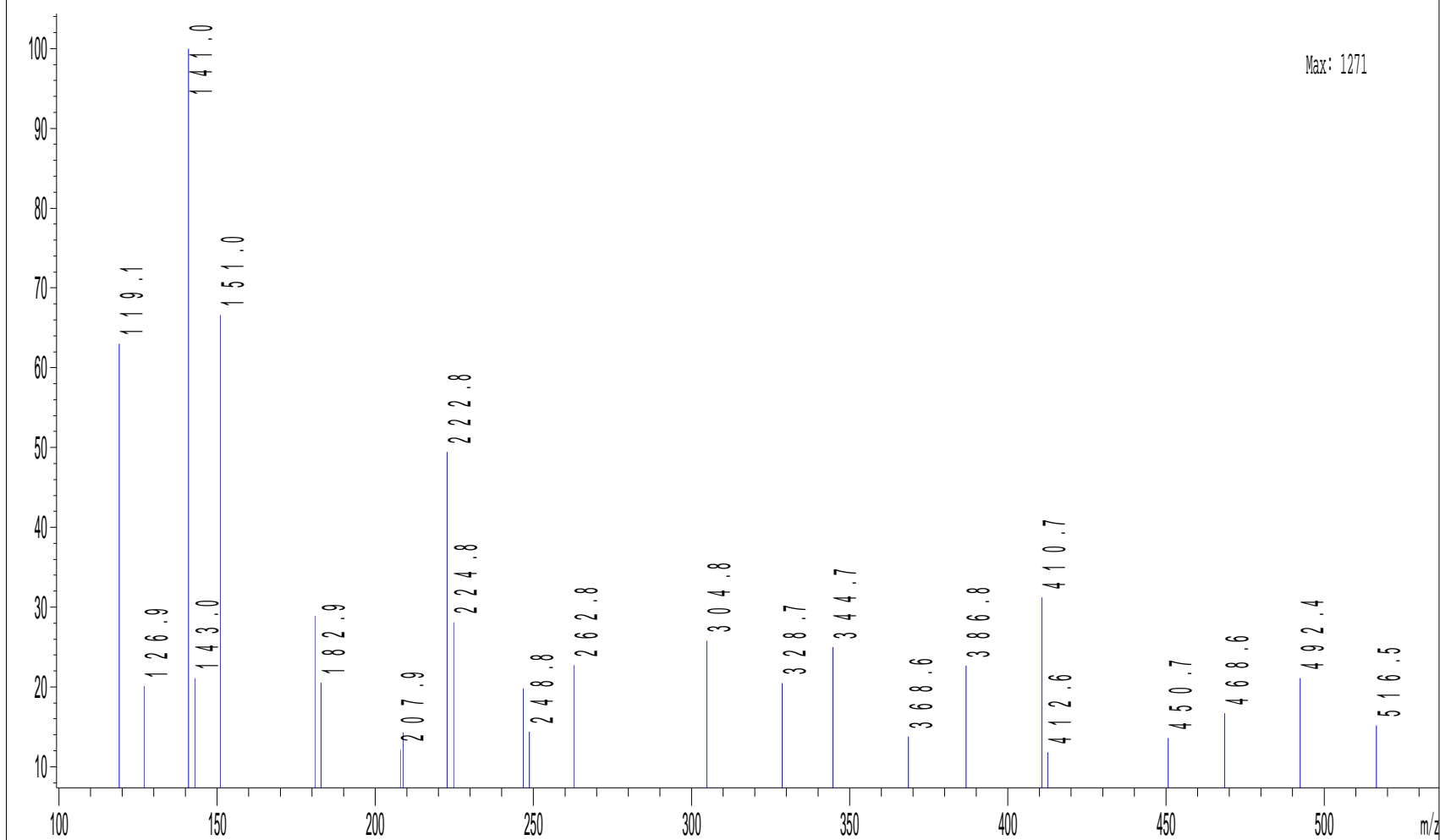
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\*MSD1 SPC, time=4.500 of D:\DATA\TARR\20150820\_TARITAR1000004.D ES-API, Neg, Scan, Frag: 70



\*MSD1 SPC, time=4.719 of D:\DATA\TARRI20150820\_TARITAR1000004.D ES-API, Neg, Scan, Frag: 70

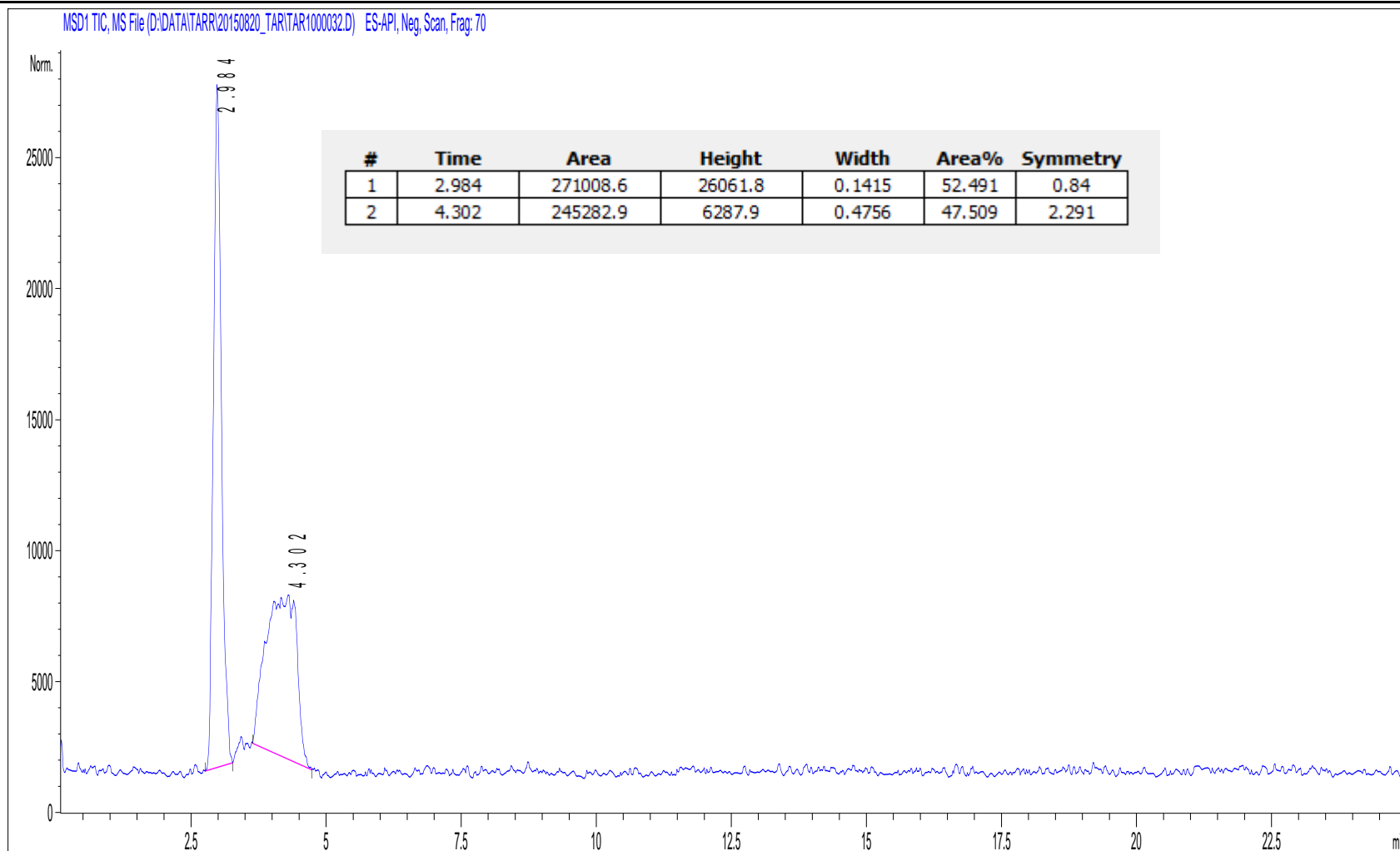


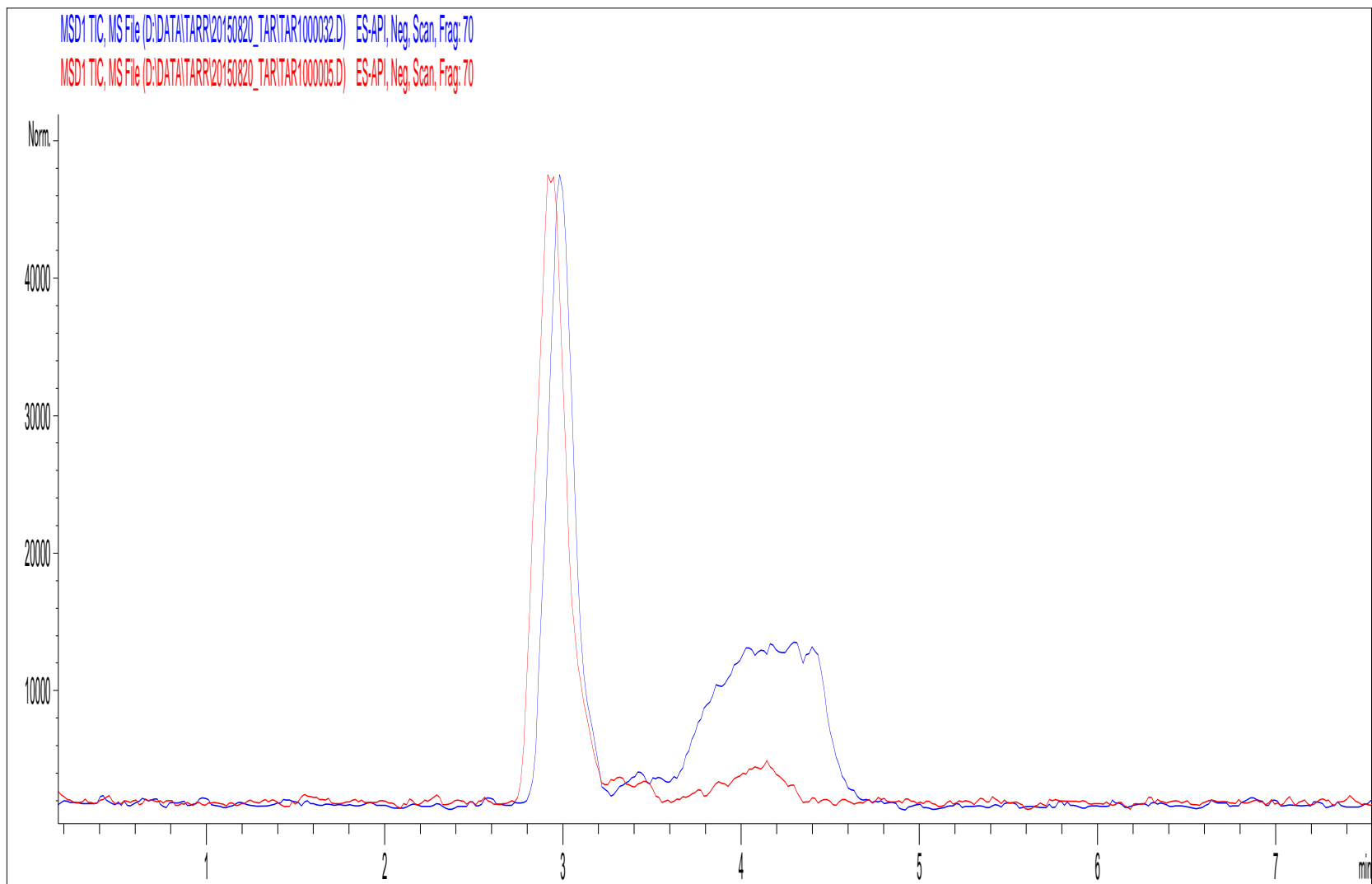
28-Jul-15

5 DC

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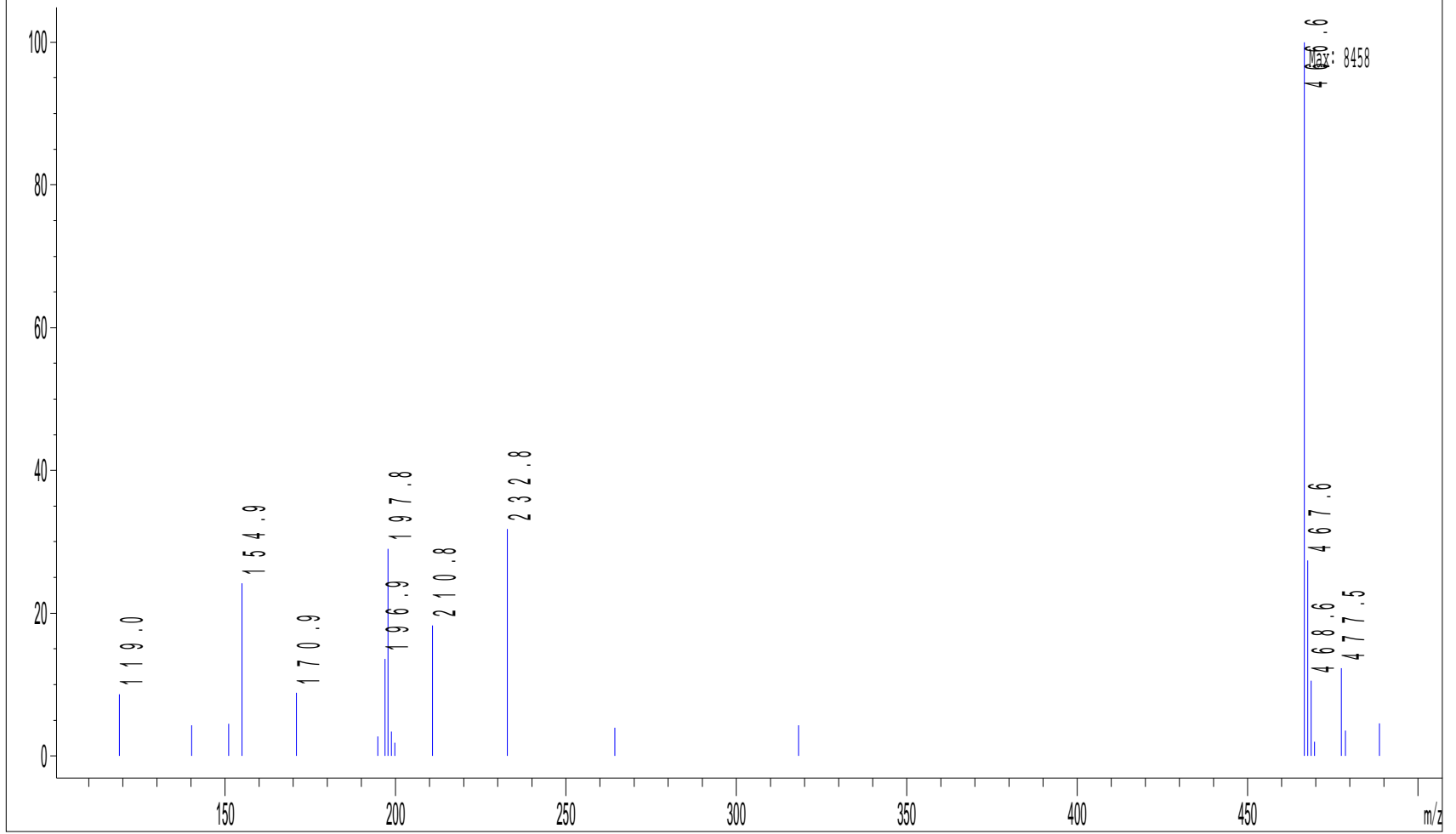
P2-D-05

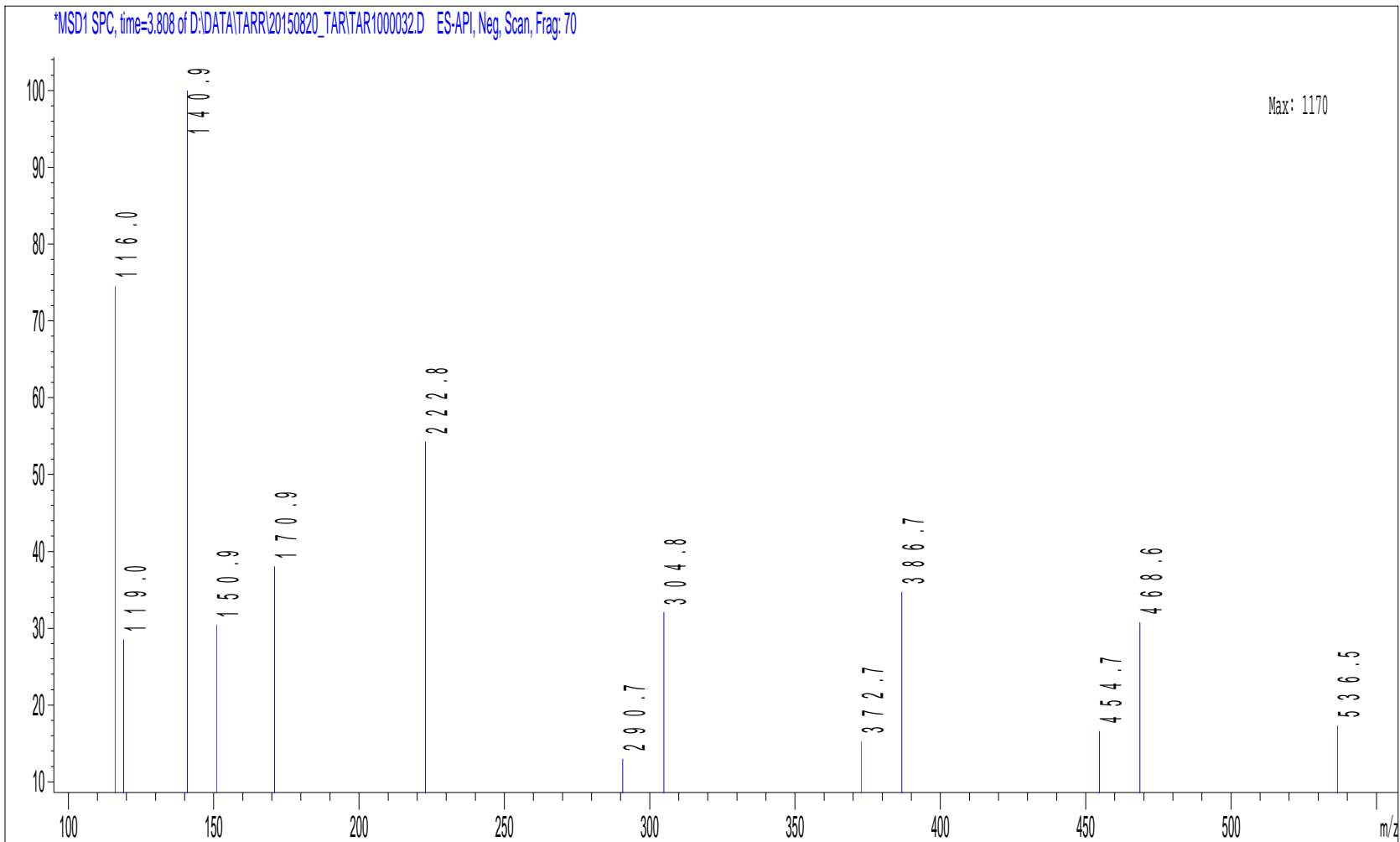


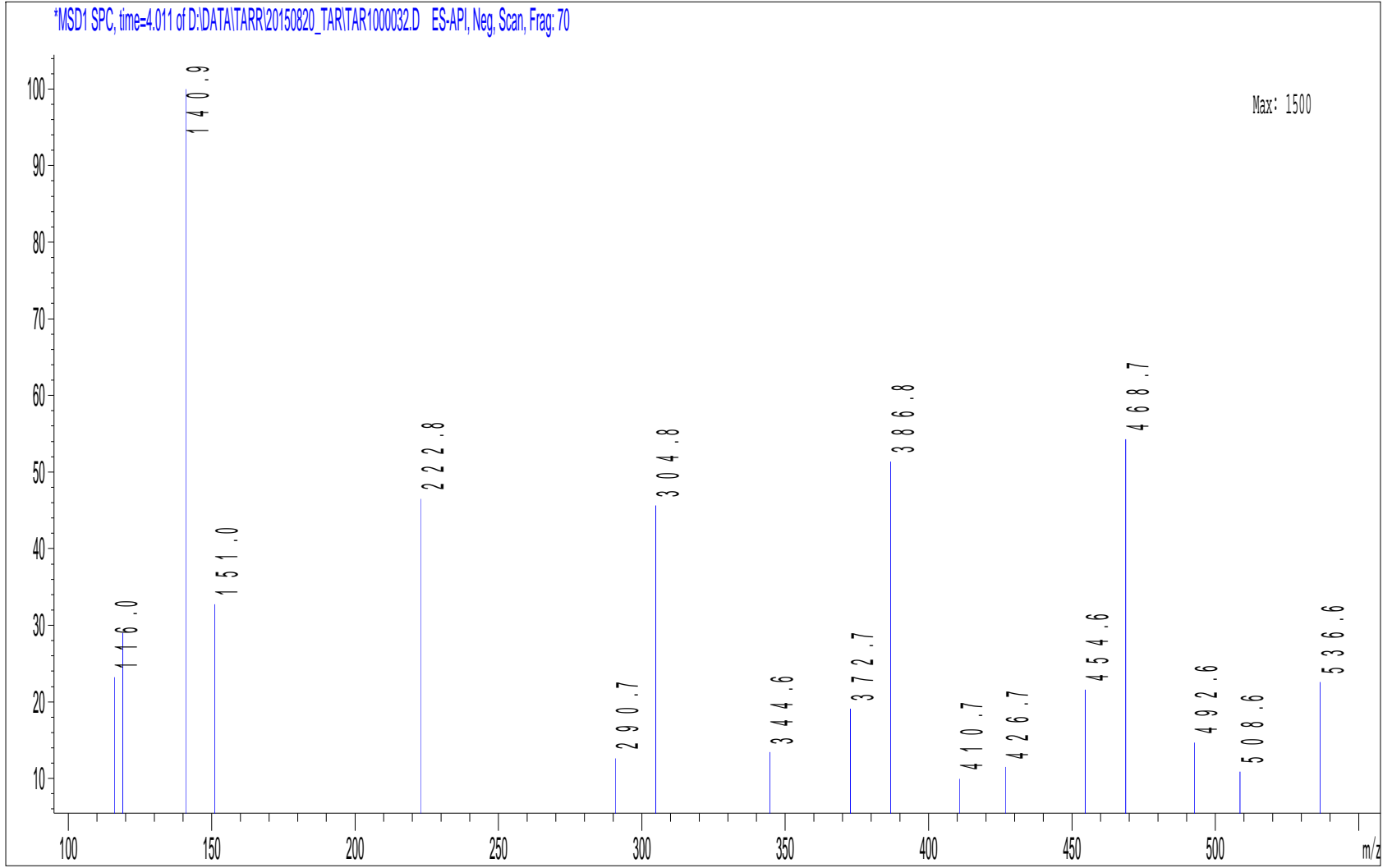


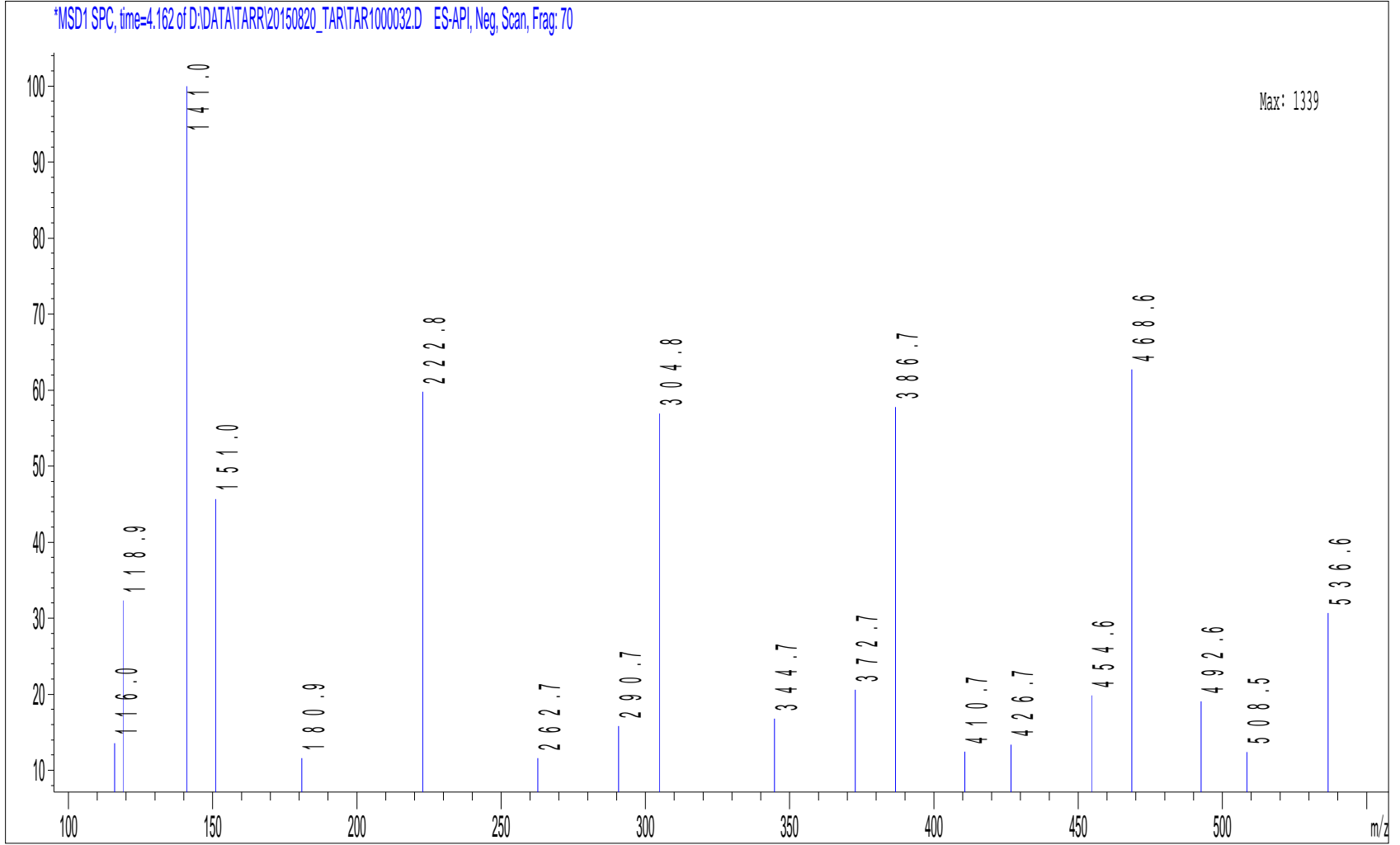


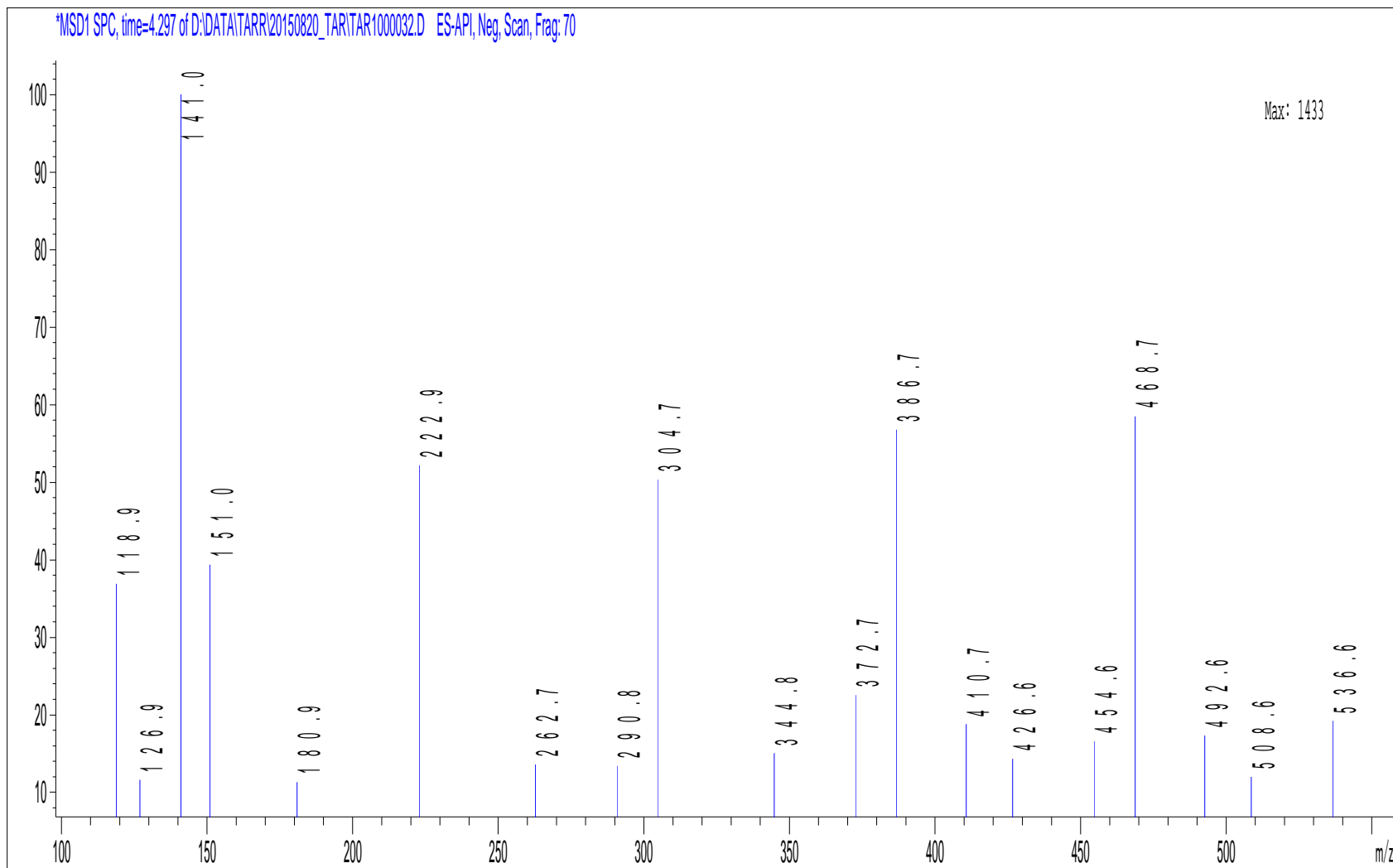
\*MSD1 SPC, time=2.999 of D:\DATA\TARR\20150820\_TARITAR1000032.D ES-API, Neg, Scan, Frag: 70



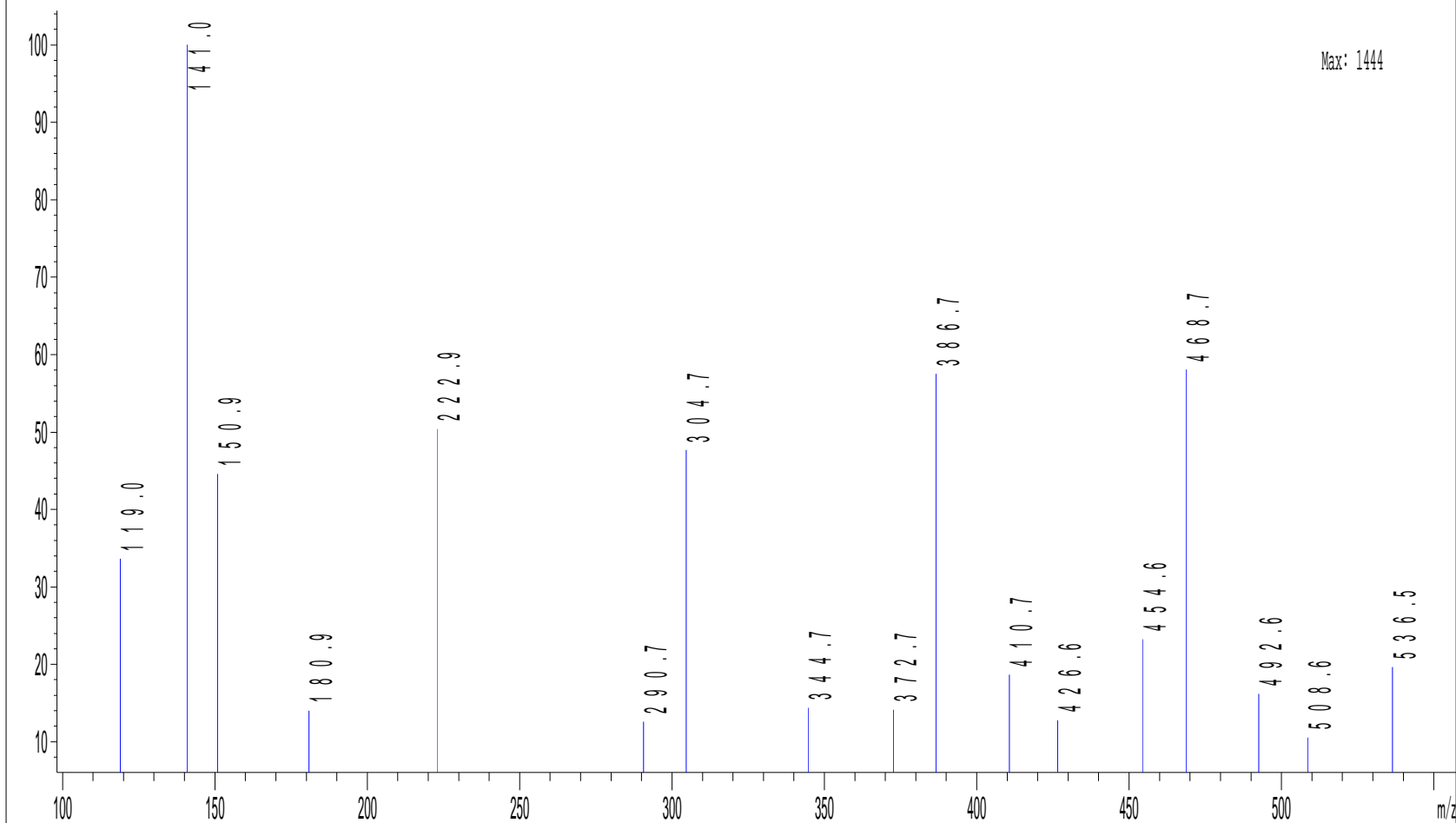








\*MSD1 SPC, time=4.415 of D:\DATA\TARR\20150820\_TARITAR1000032.D ES-API, Neg, Scan, Frag: 70

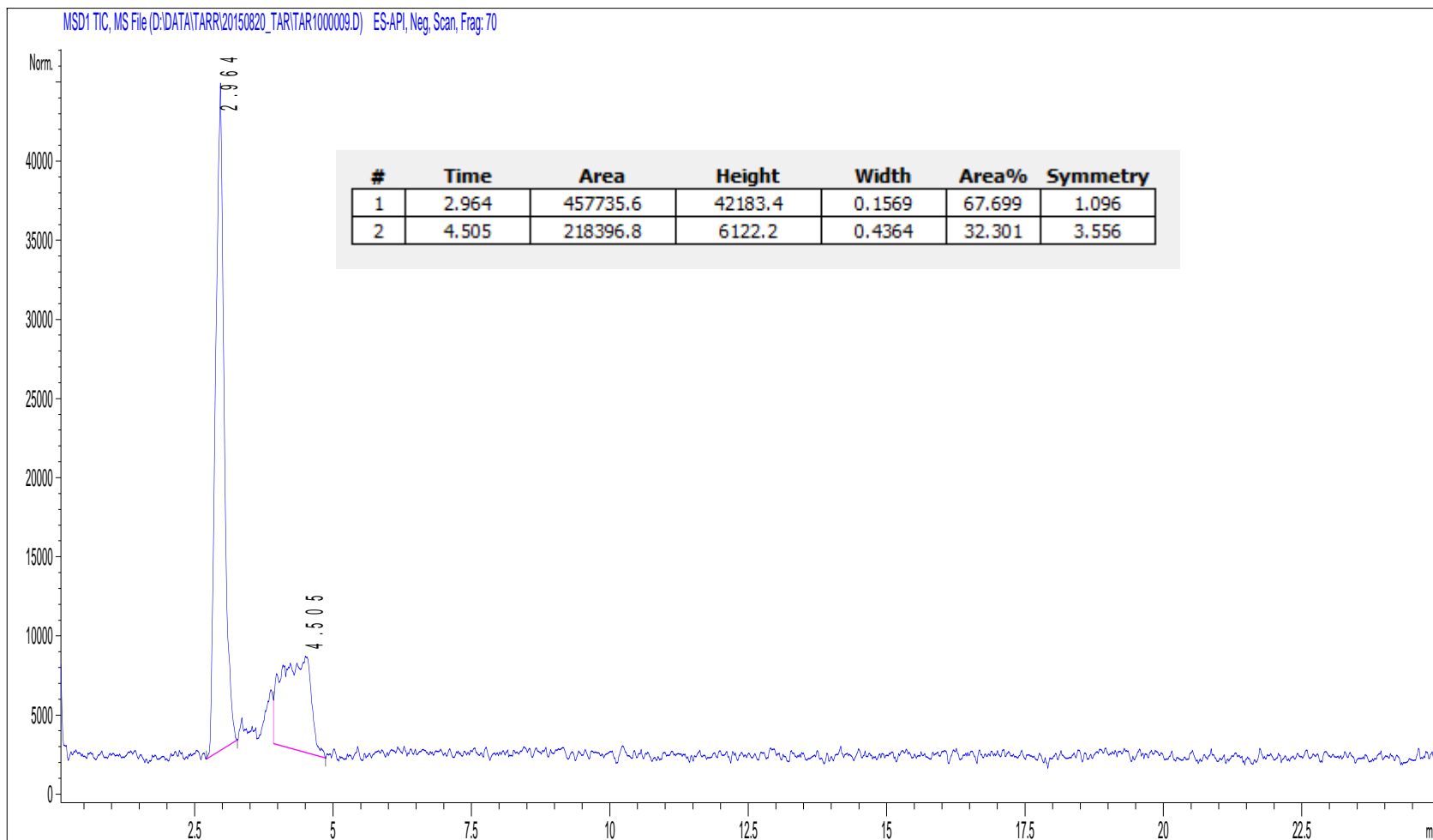


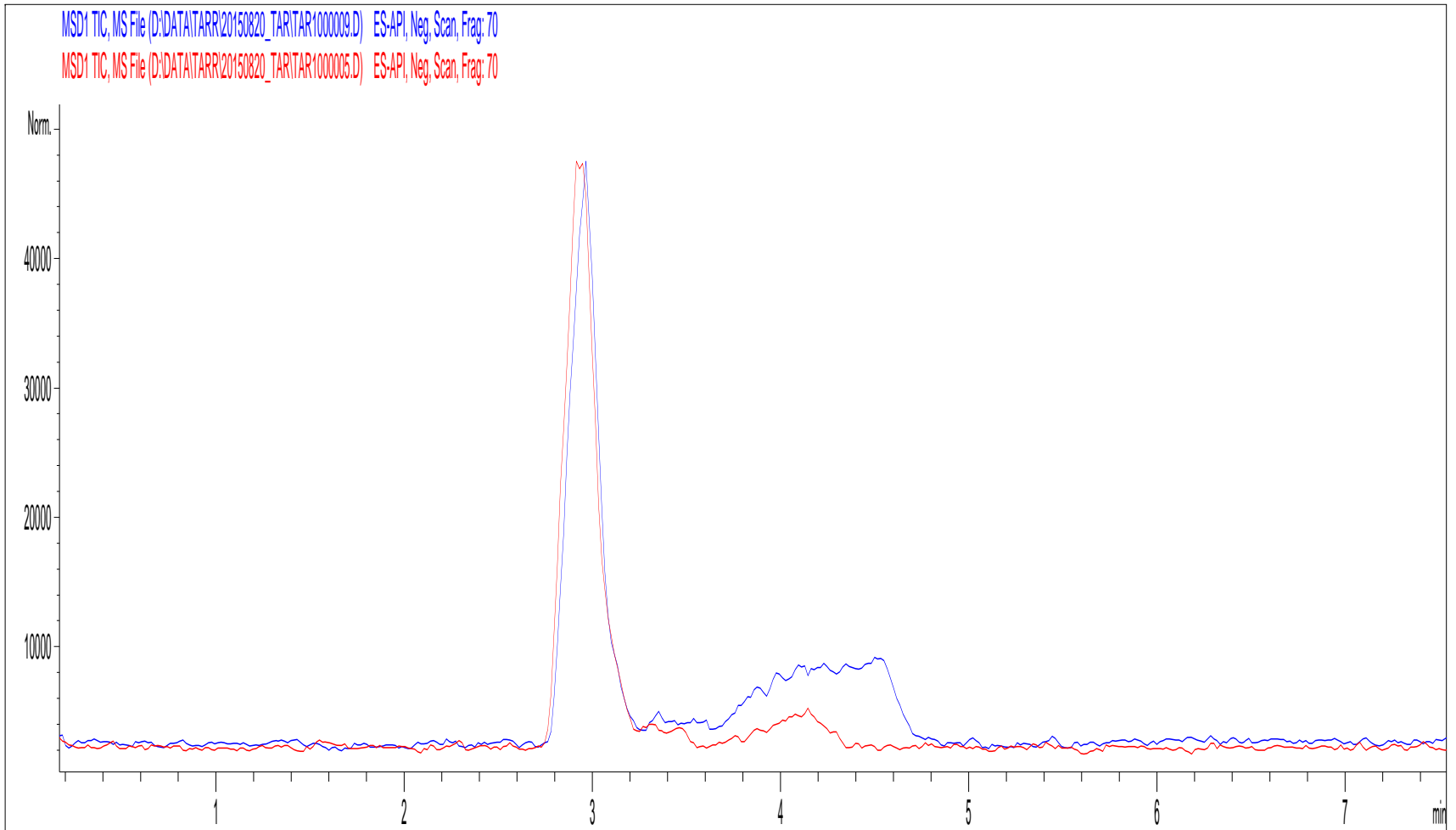
30-Apr-15

10 DC

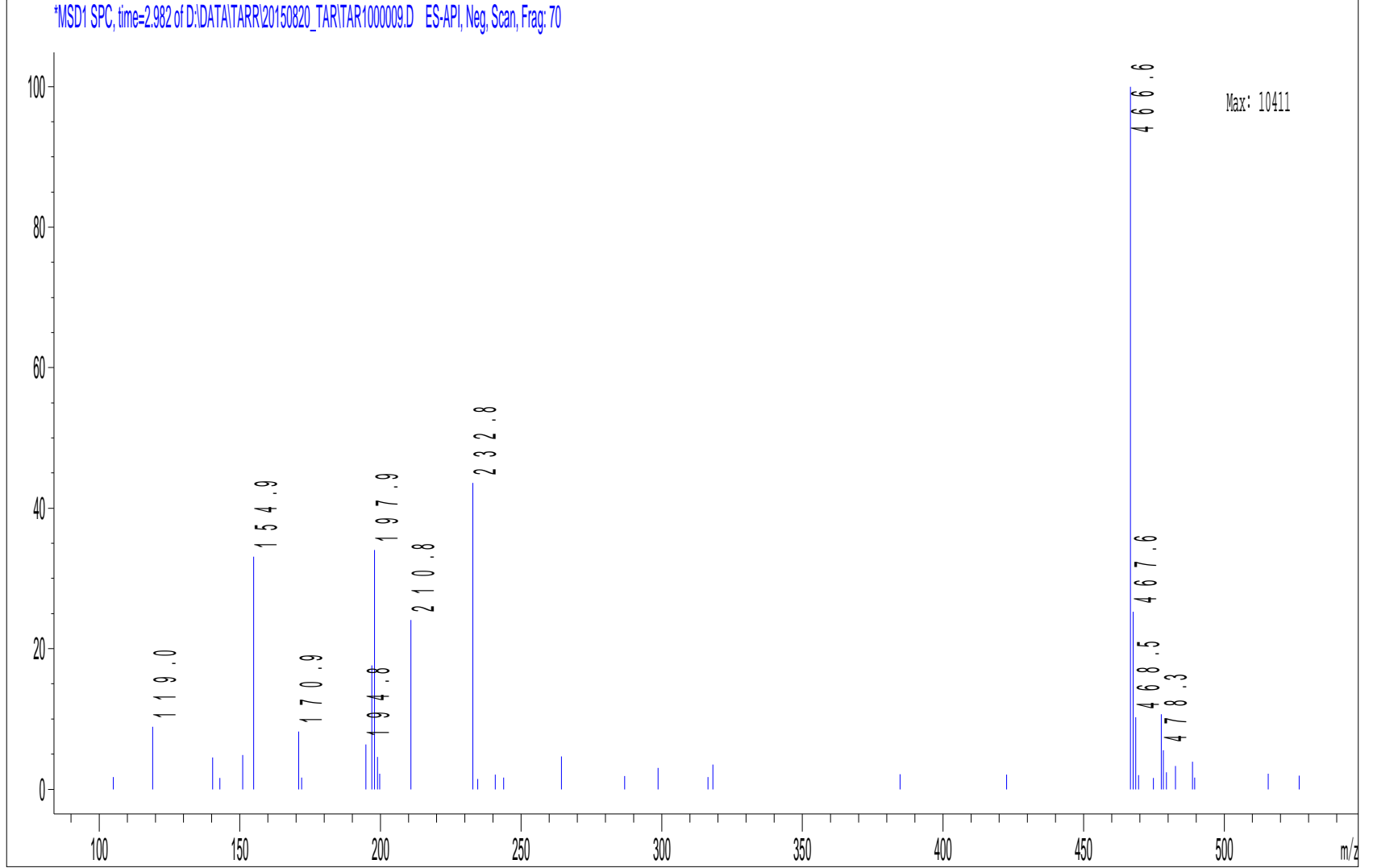
9

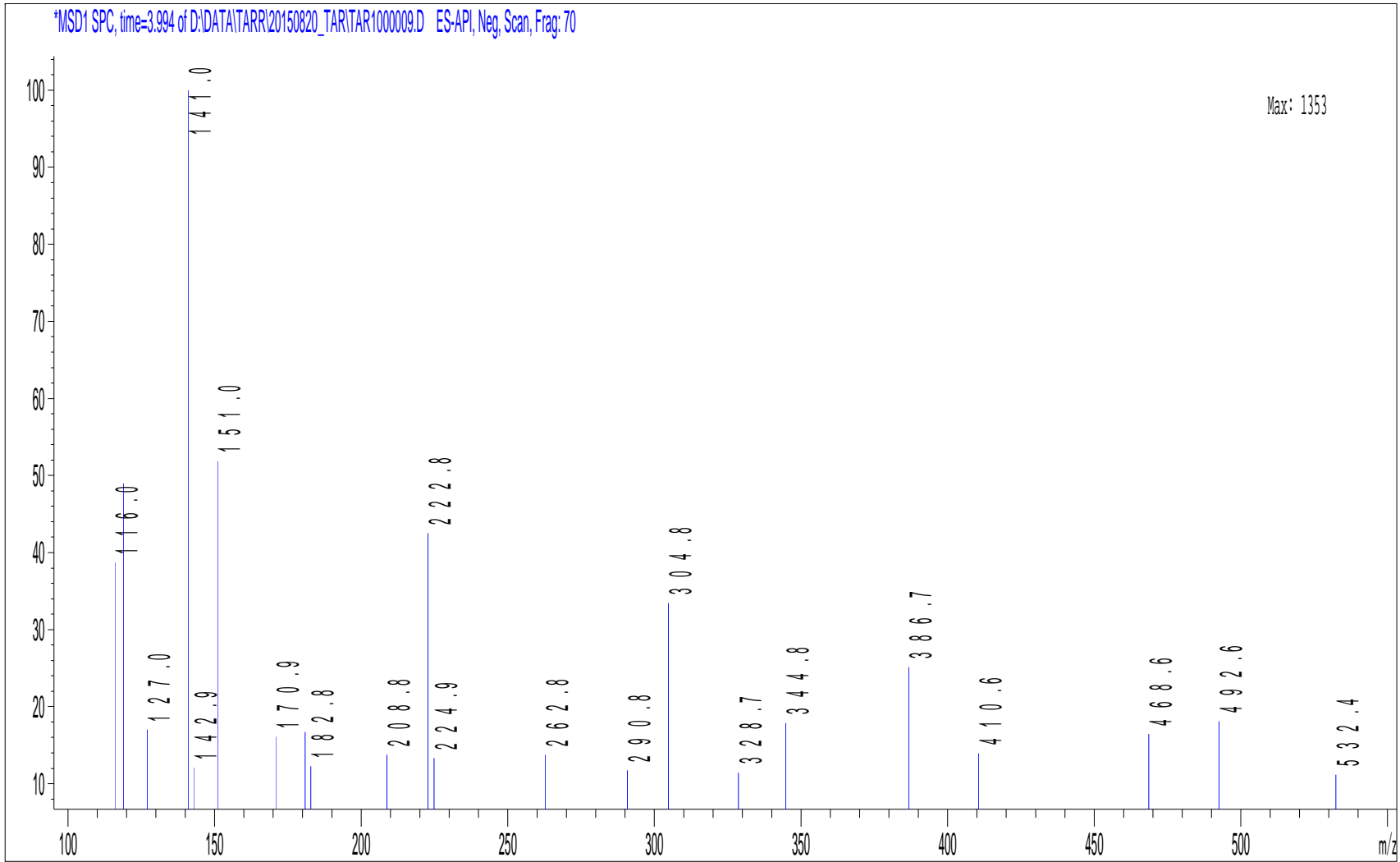
P2-A-09

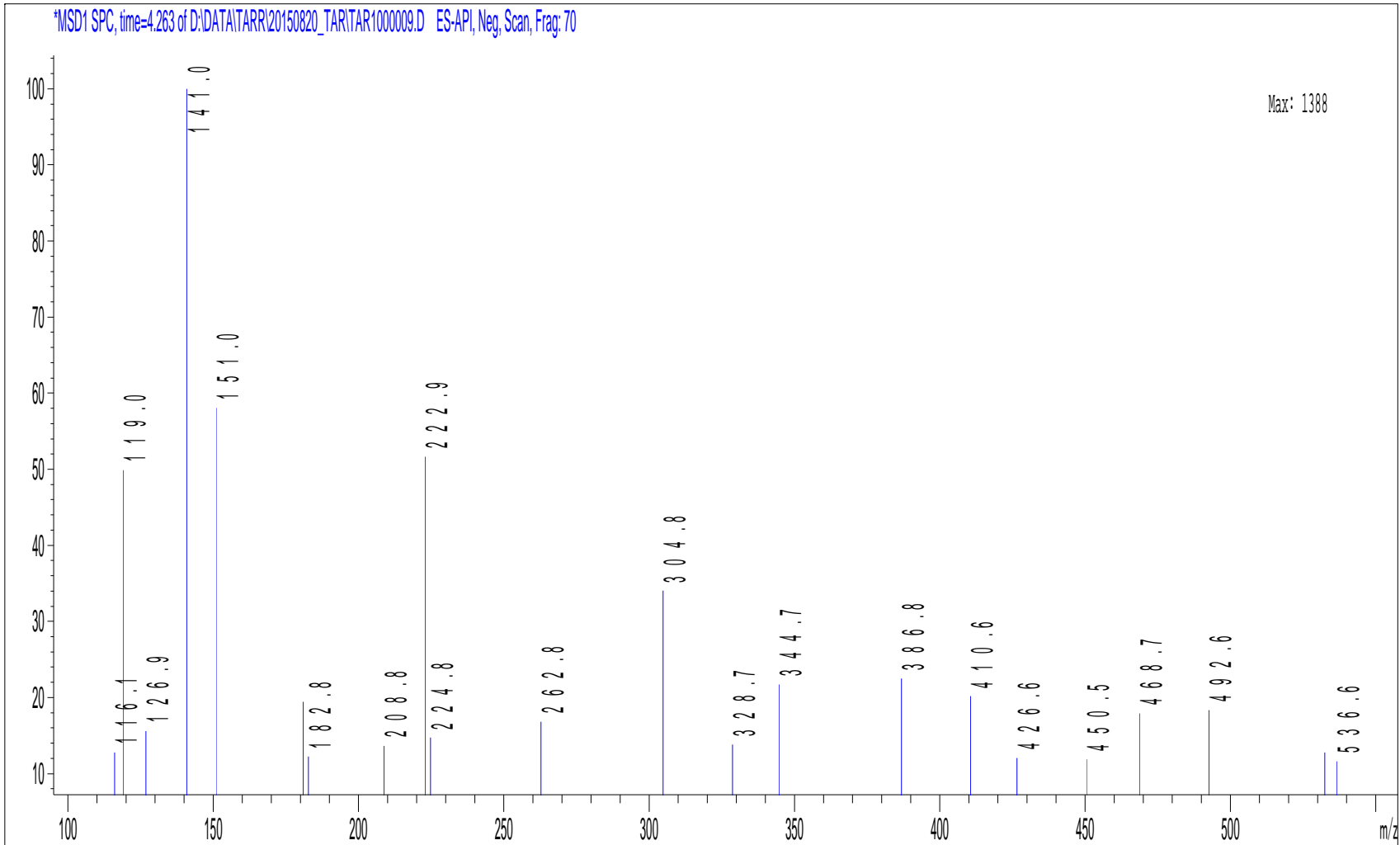




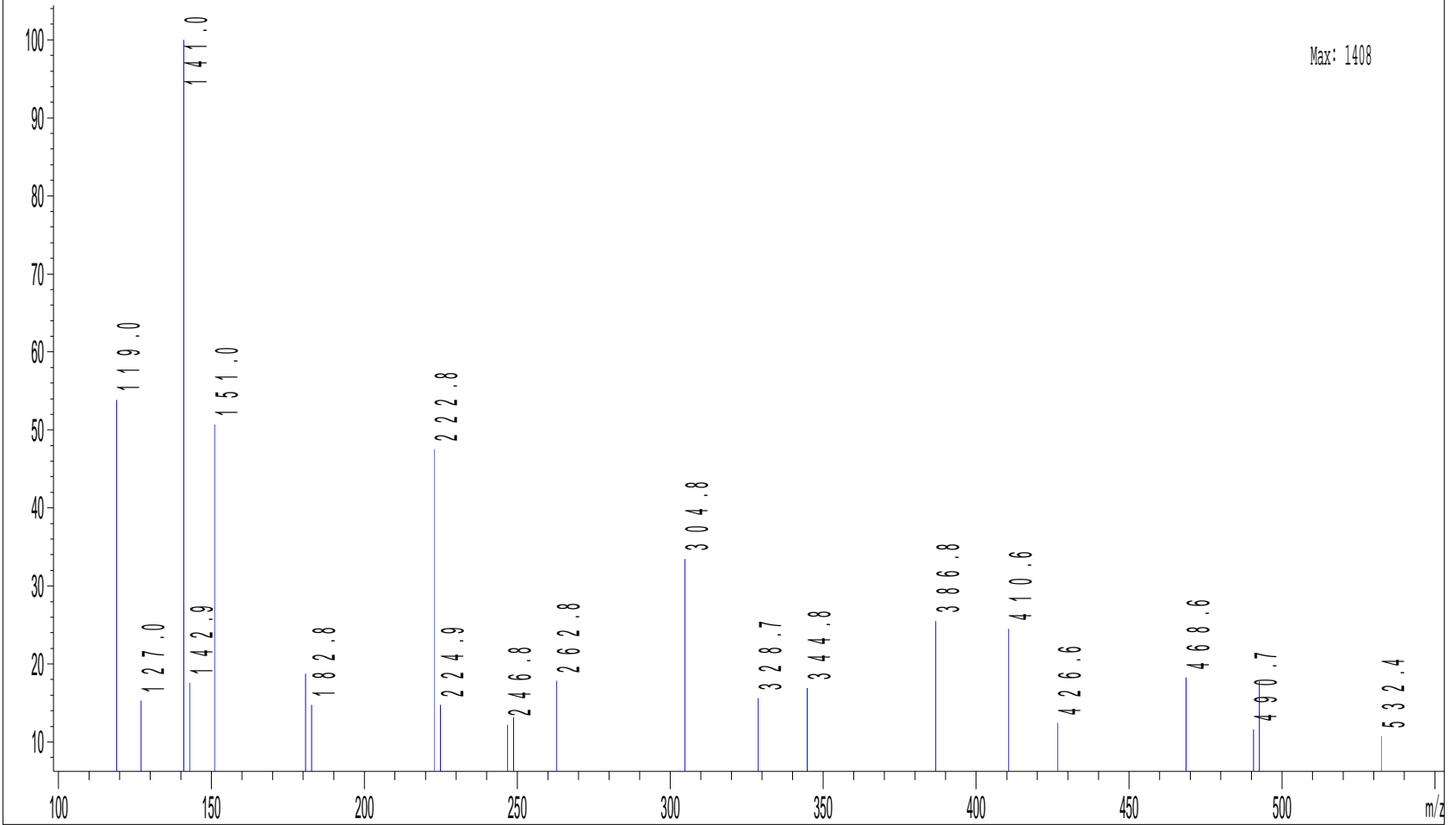




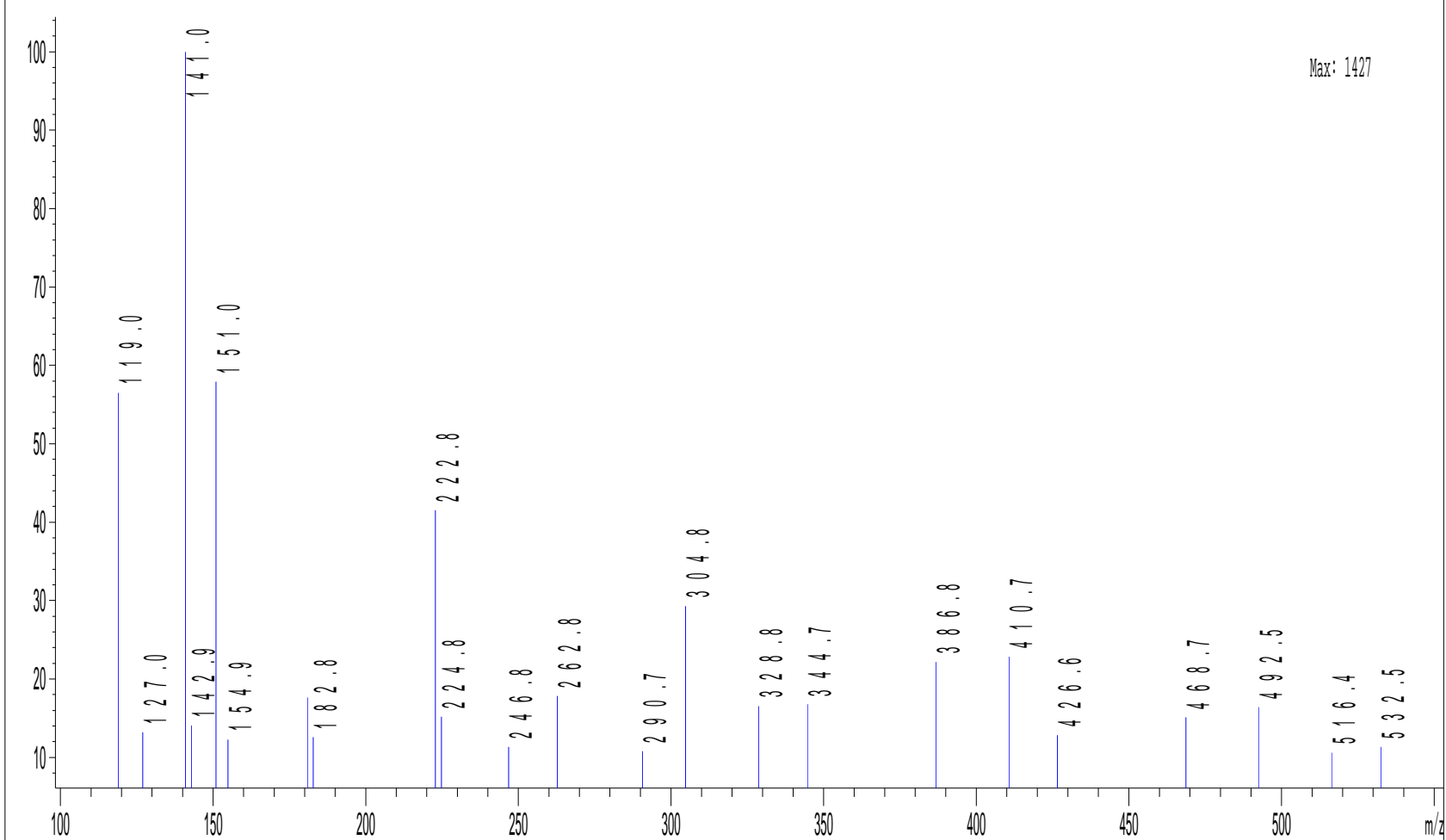




\*MSD1 SPC, time=4.432 of D:\DATA\TARR\20150820\_TARITAR1000009.D ES-API, Neg, Scan, Frag: 70



\*MSD1 SPC, time=4.567 of D:\DATA\TARR\20150820\_TAR\TAR1000009.D ES-API, Neg, Scan, Frag: 70



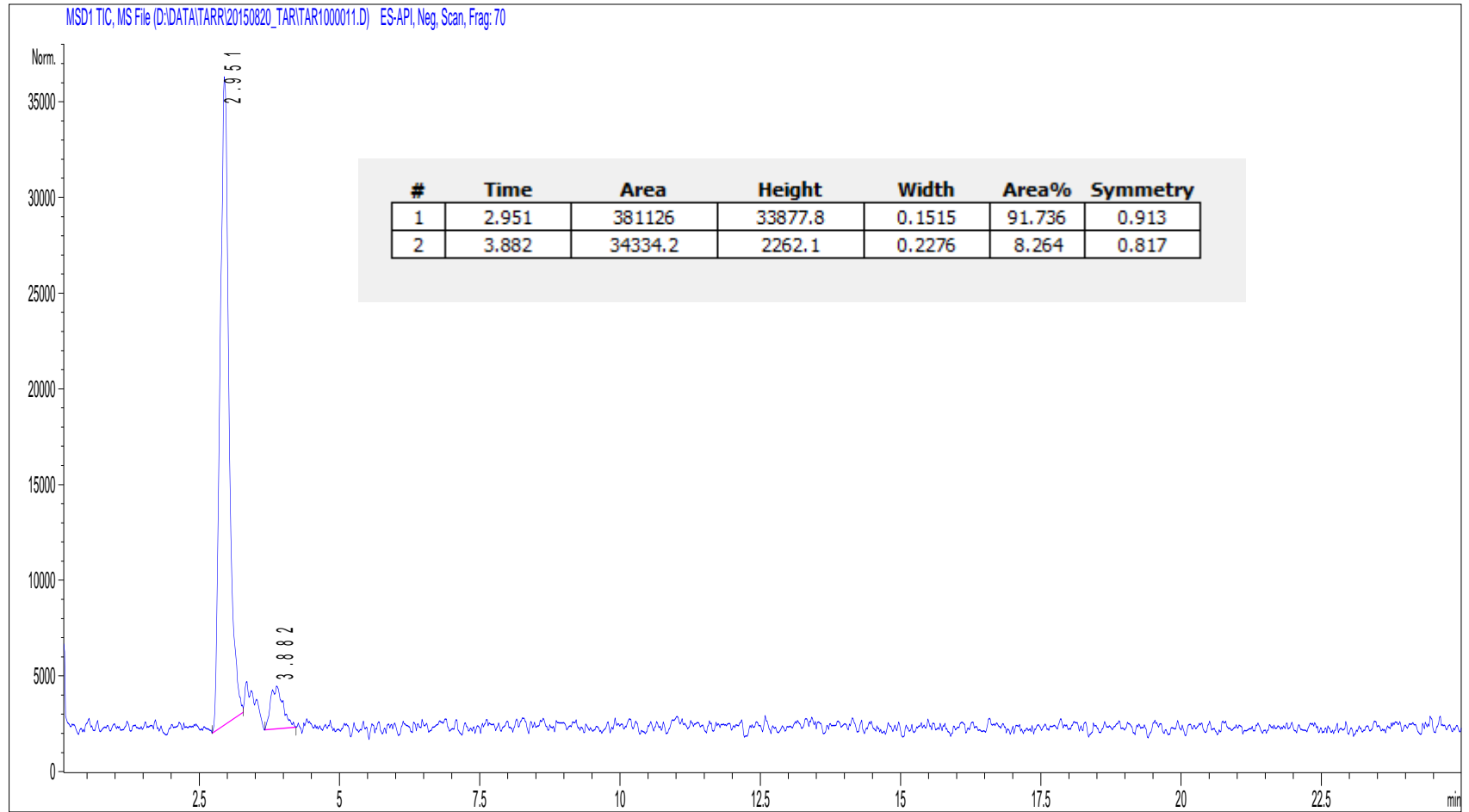
Max: 1427

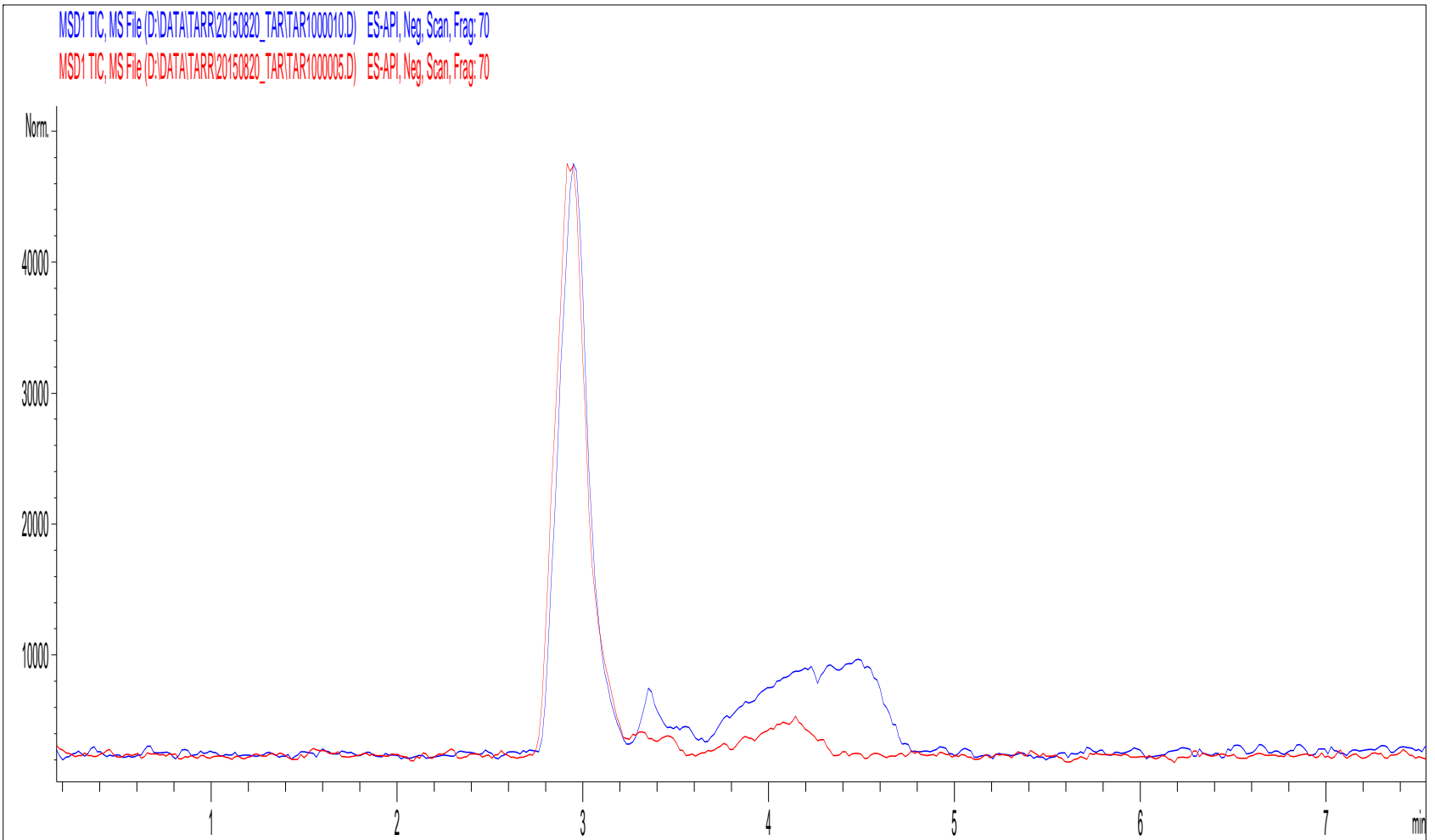
22-Jun-15

20 DC

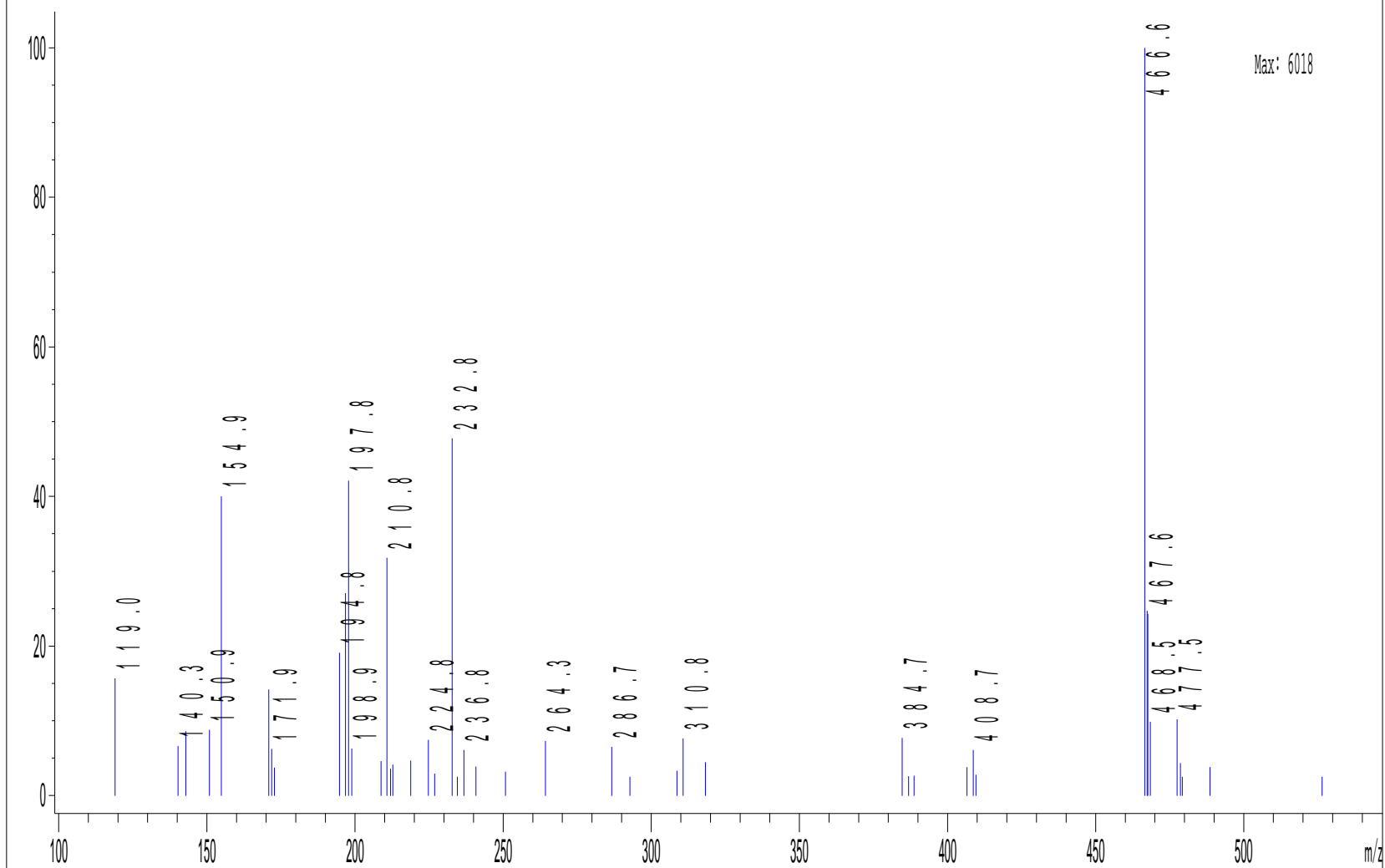
9

P2-B-09

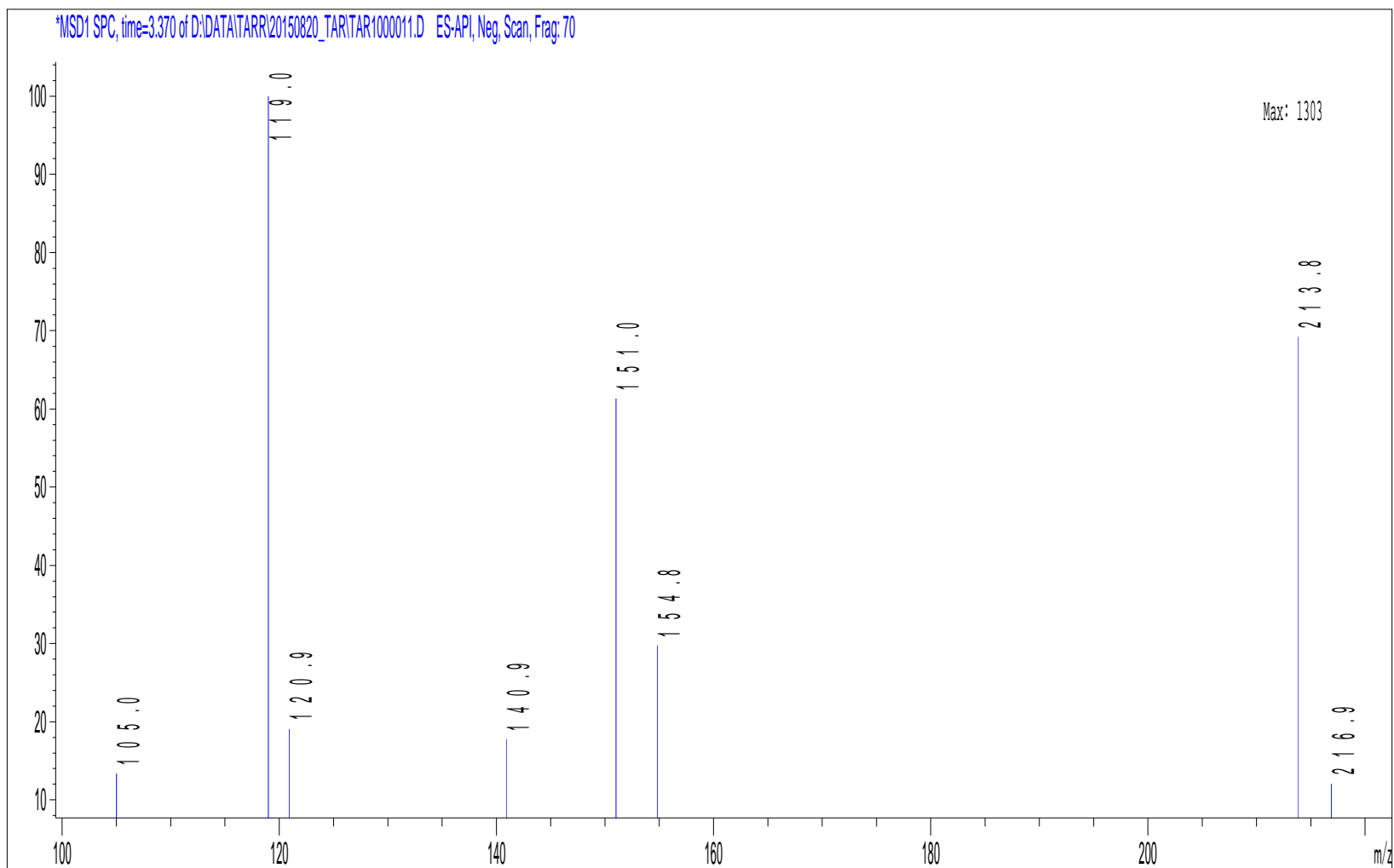




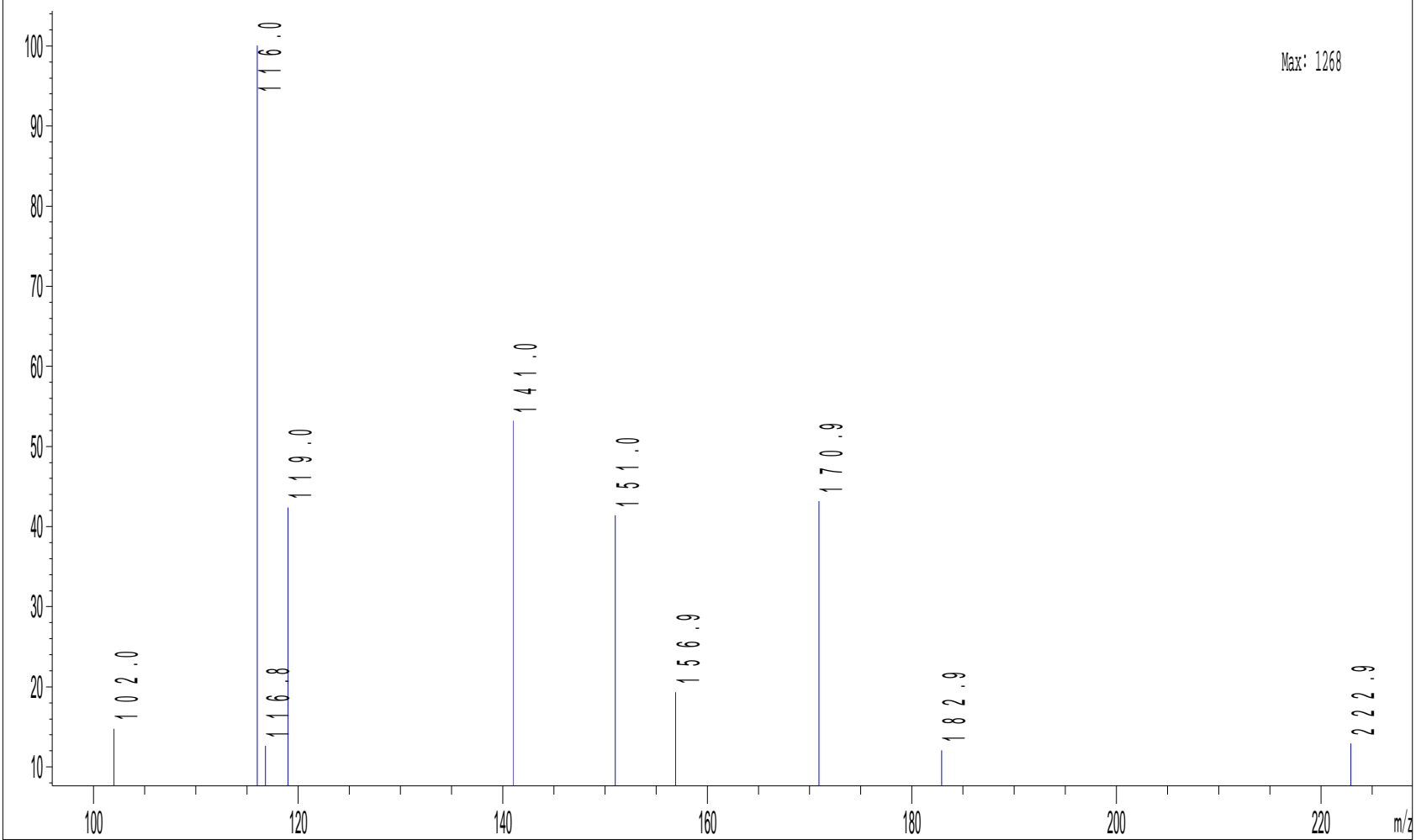
\*MSD1 SPC, time=2.982 of D:\DATA\TARRI20150820\_TARITAR1000011.D ES-API, Neg, Scan, Frag: 70







\*MSD1 SPC, time=3.876 of D:\DATA\TARR\20150820\_TARITAR1000011.D ES-API, Neg, Scan, Frag: 70

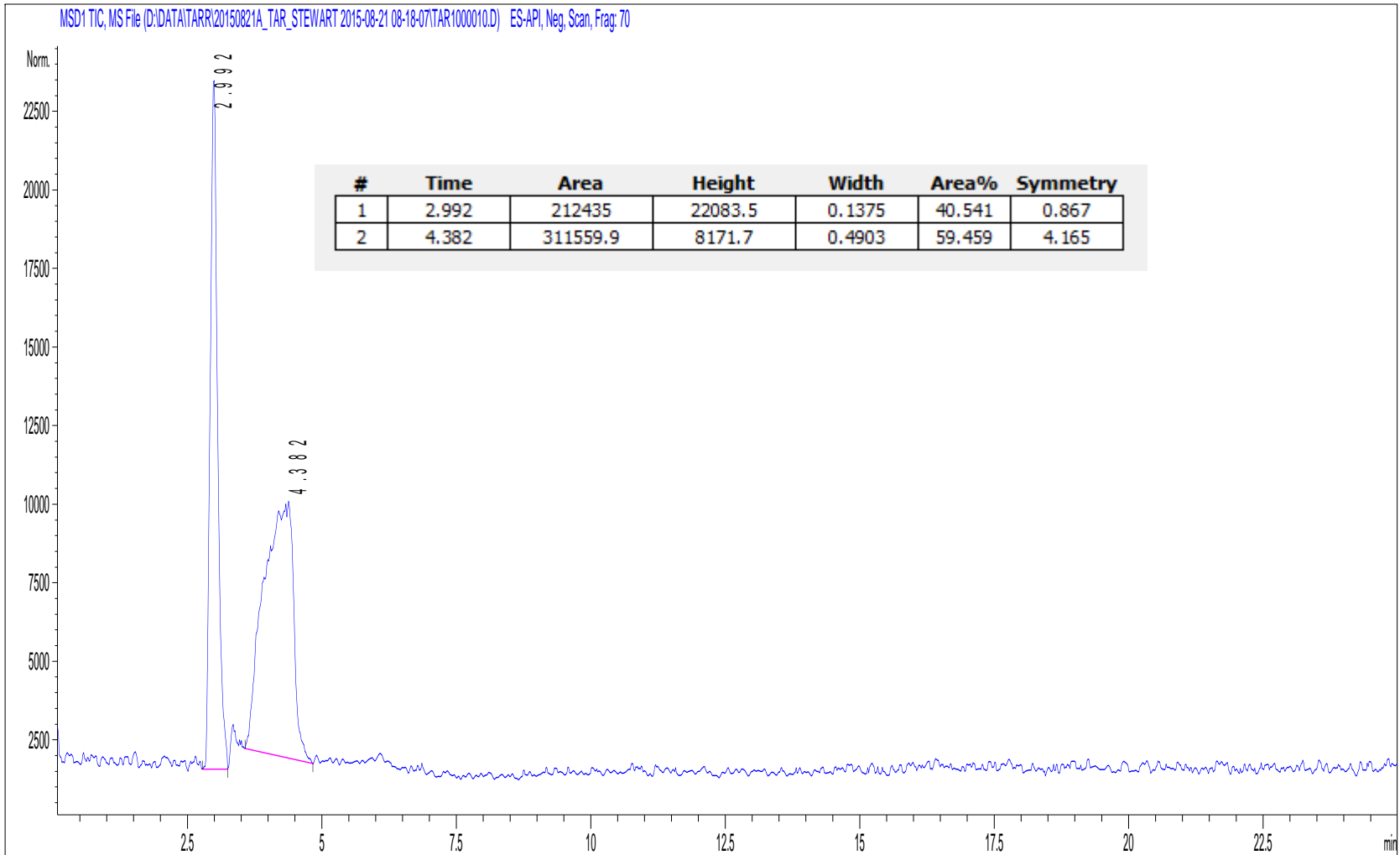


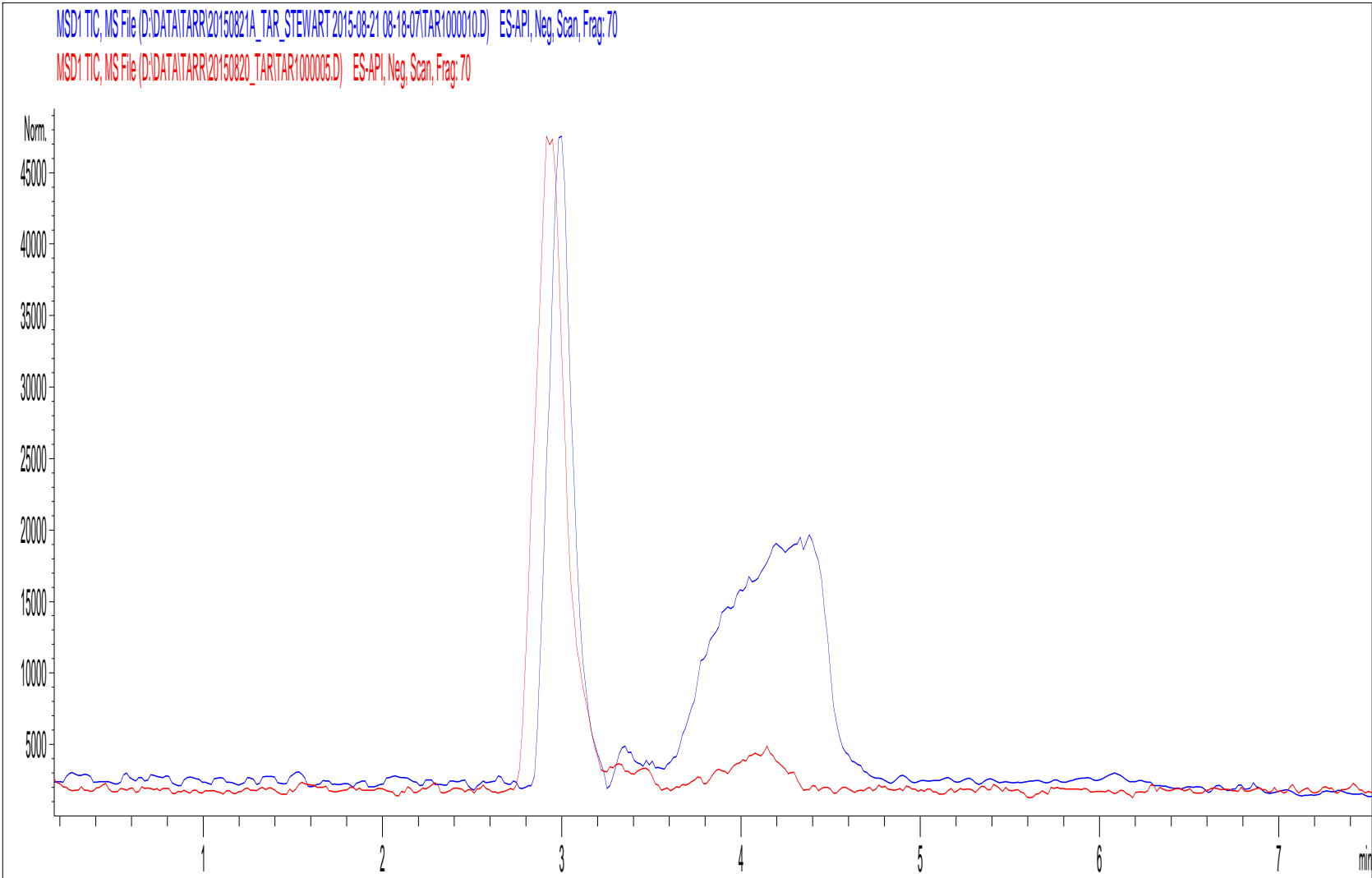
5-Aug-15

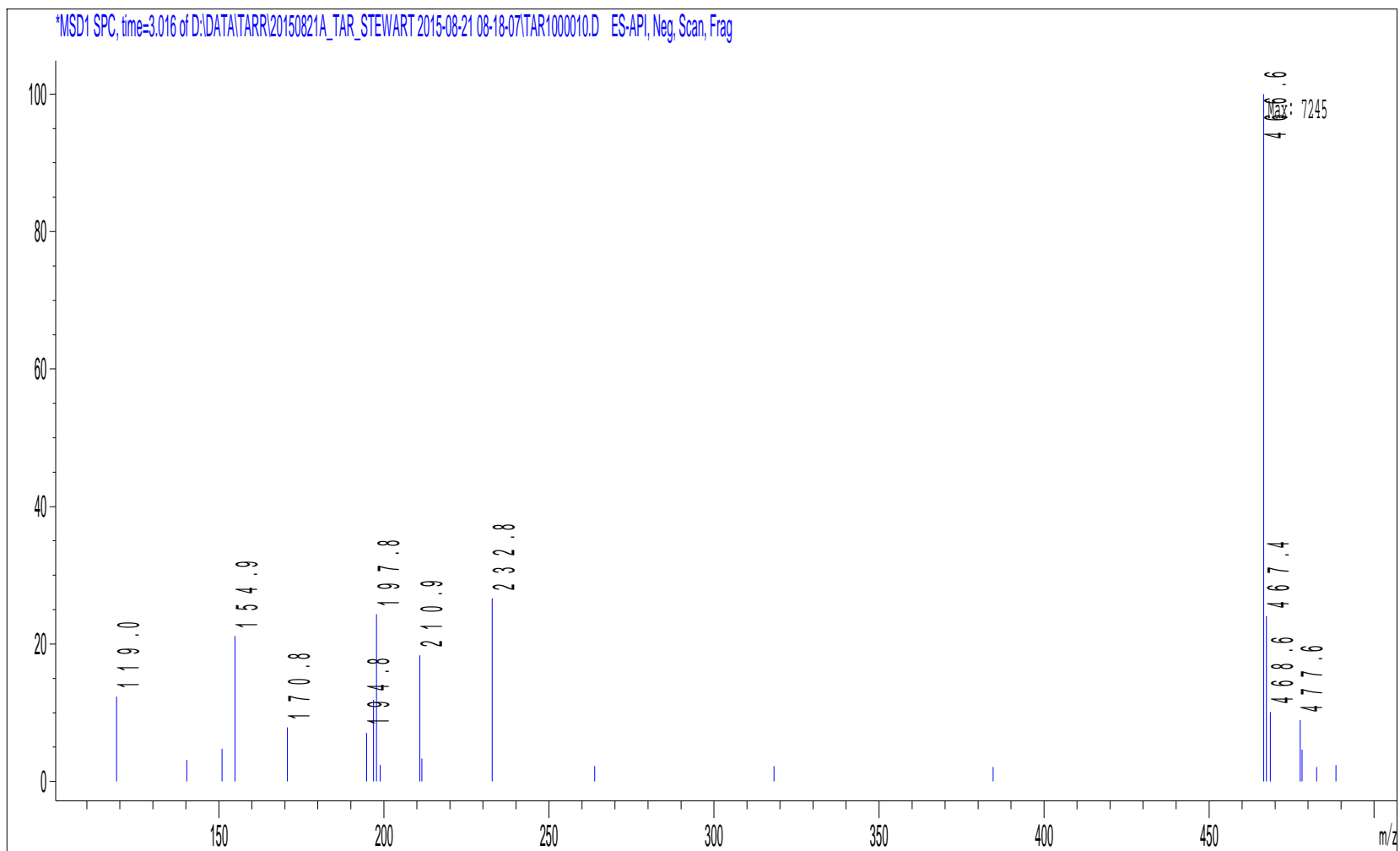
30 DC

9

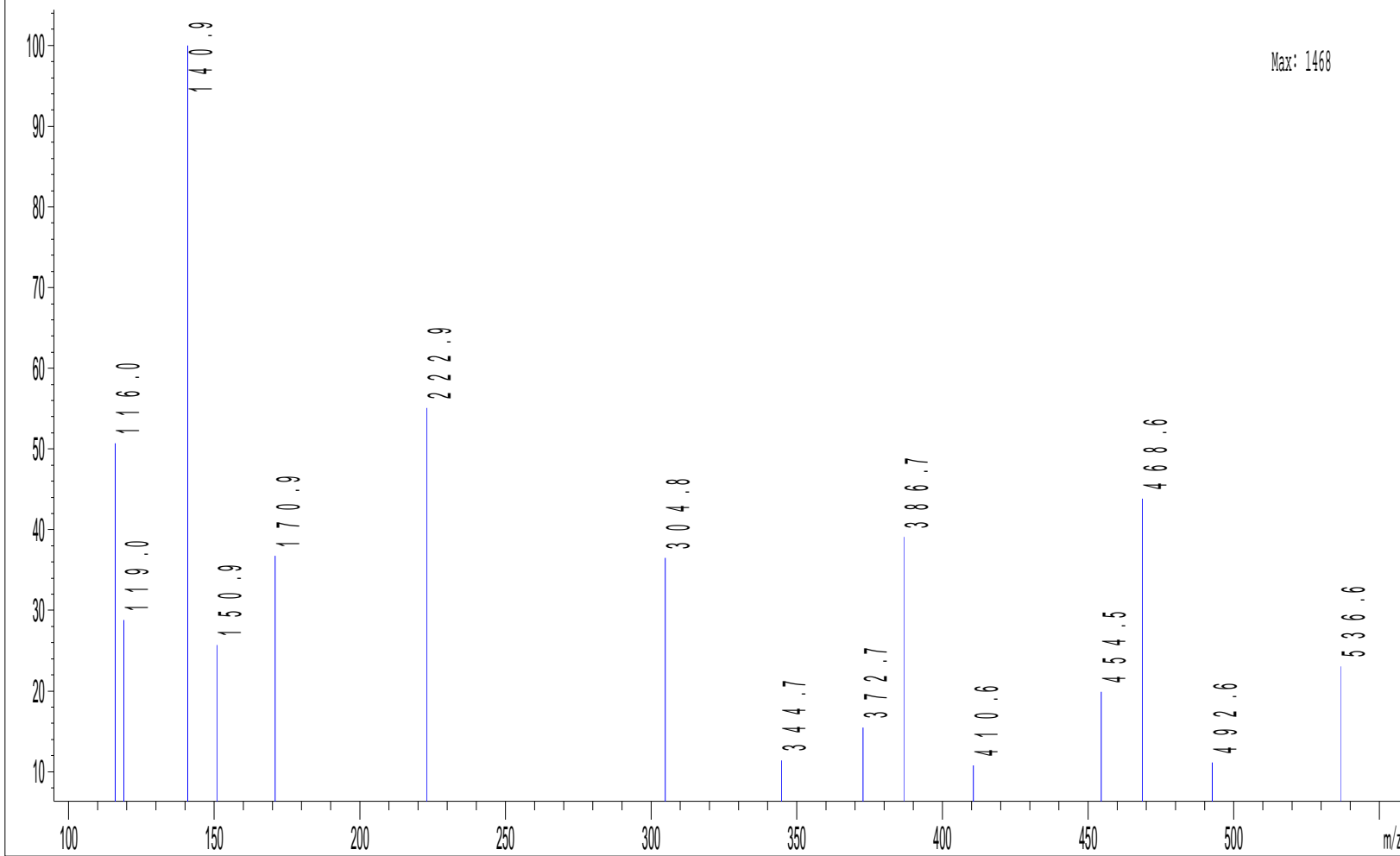
P2-E-09

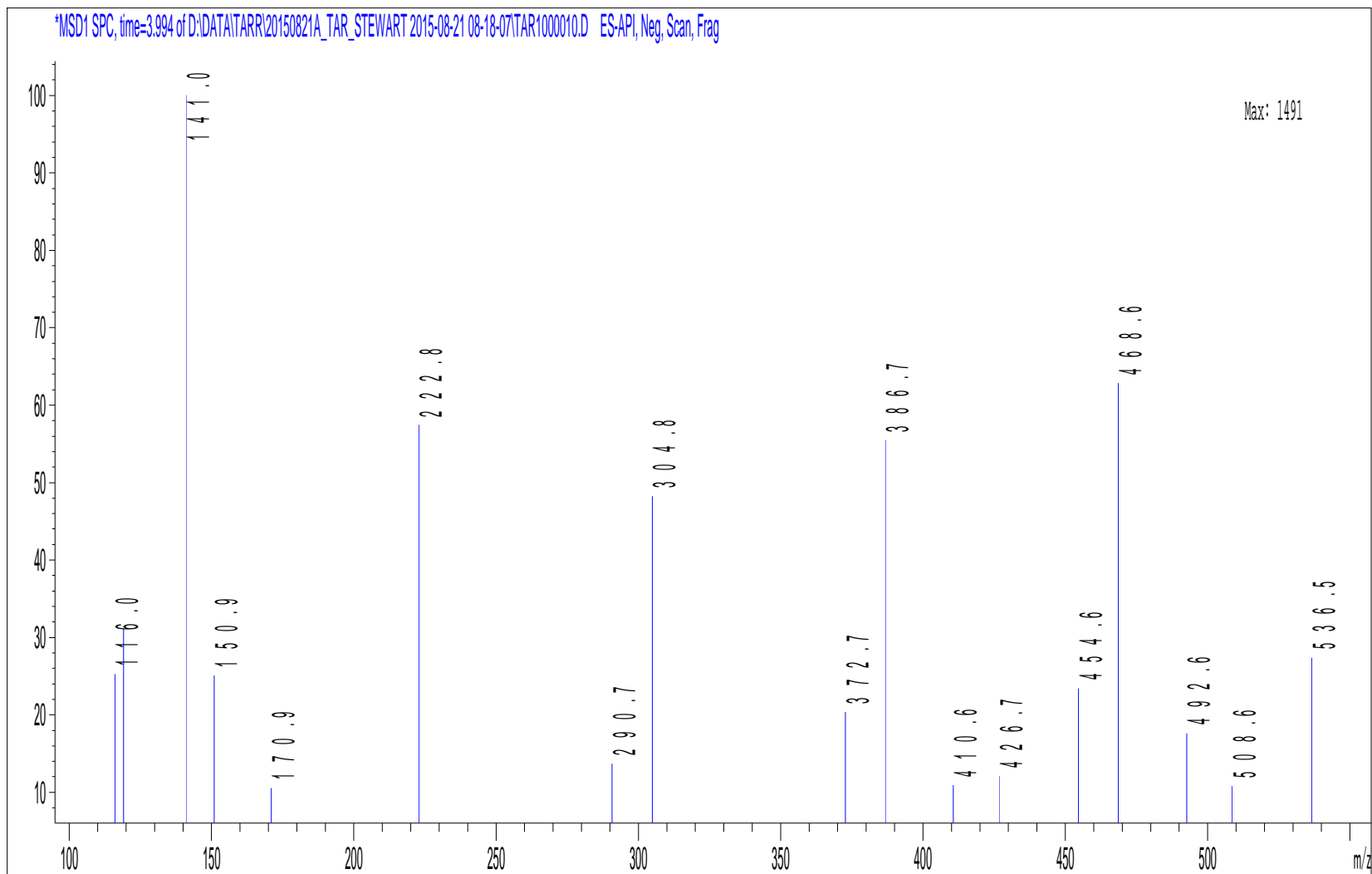


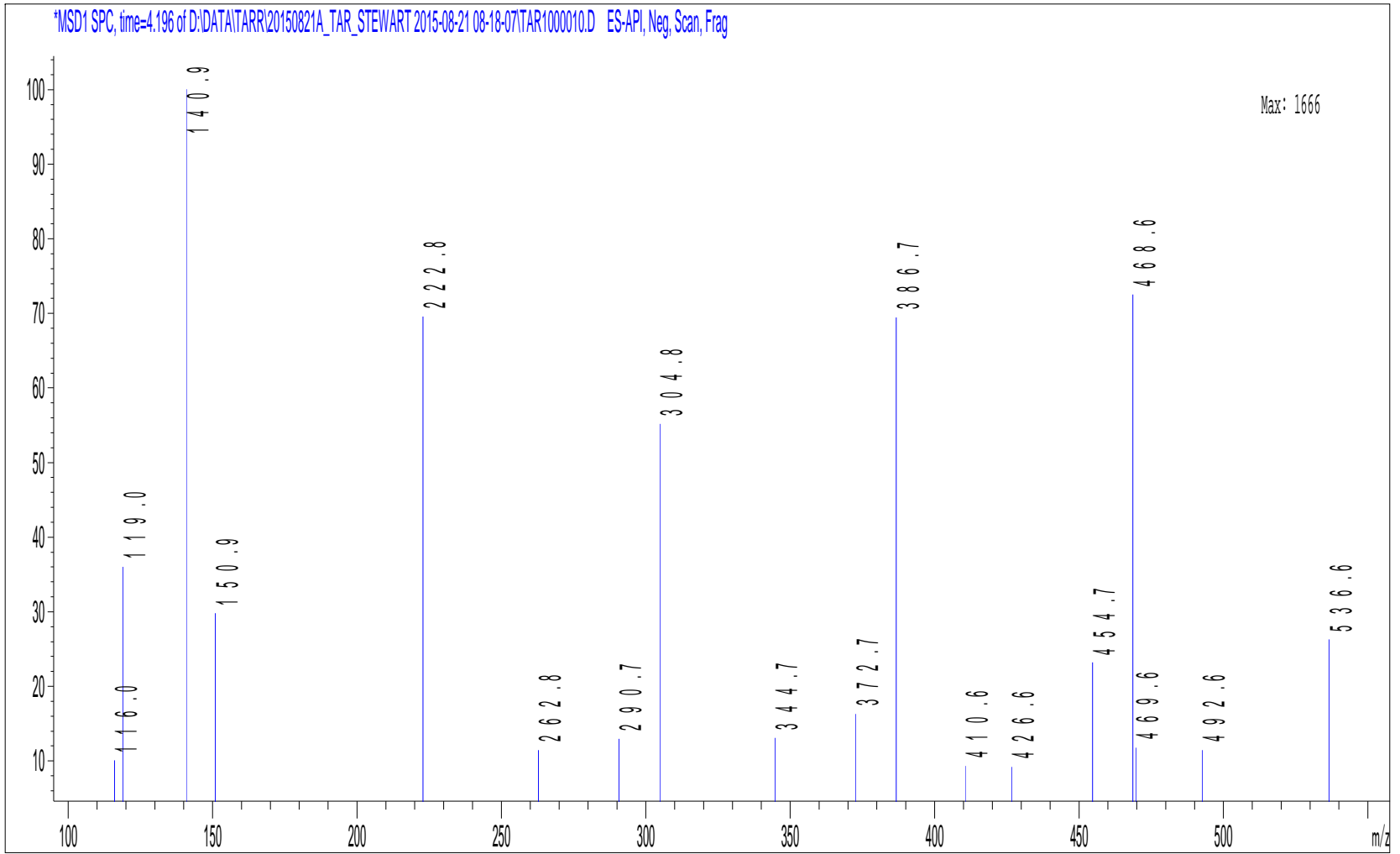




\*MSD1 SPC, time=3.893 of D:\DATA\TARR\20150821A\_TAR\_STEWART 2015-08-21 08-18-07\TAR1000010.D ES-API, Neg, Scan, Frag

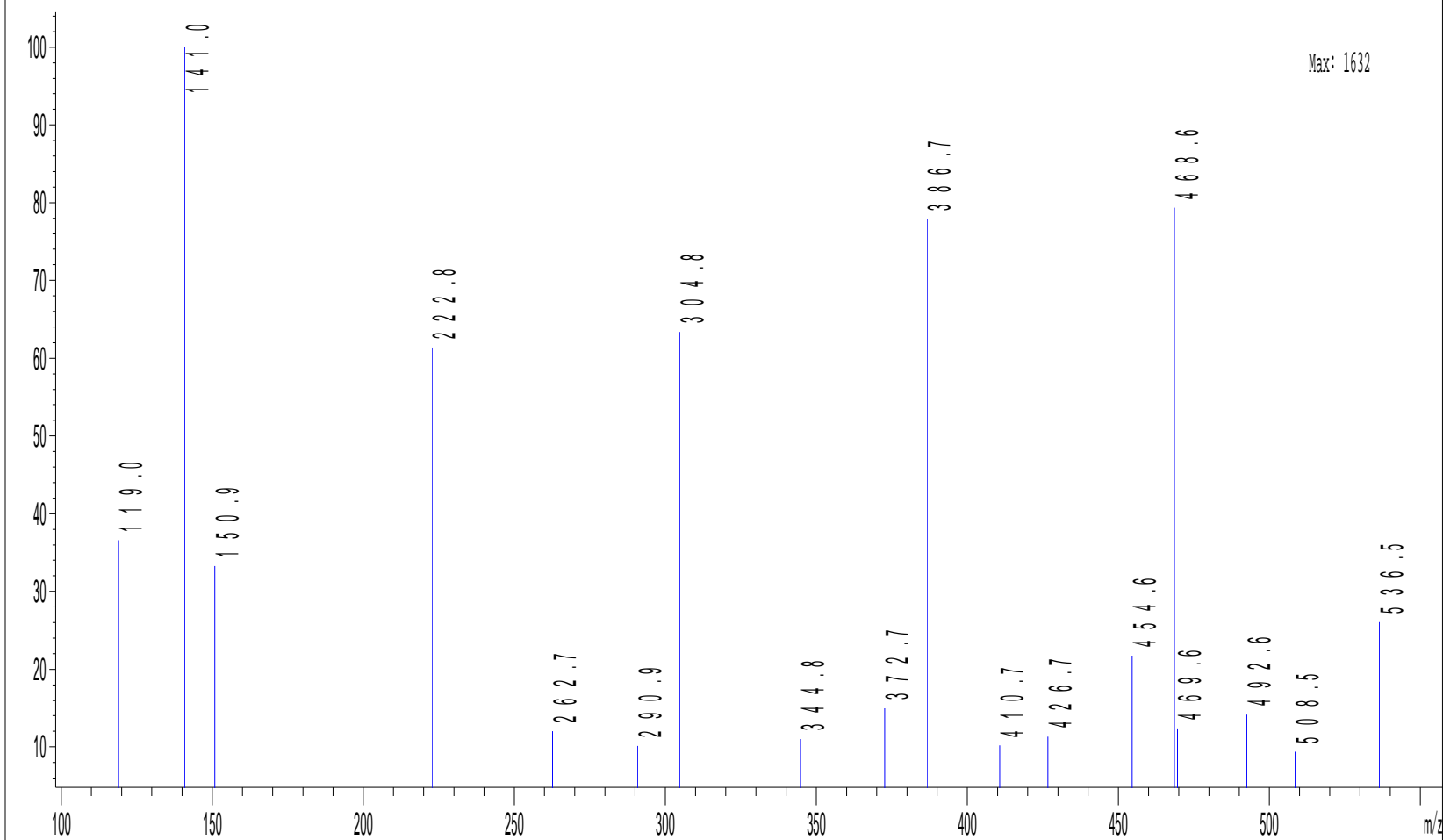


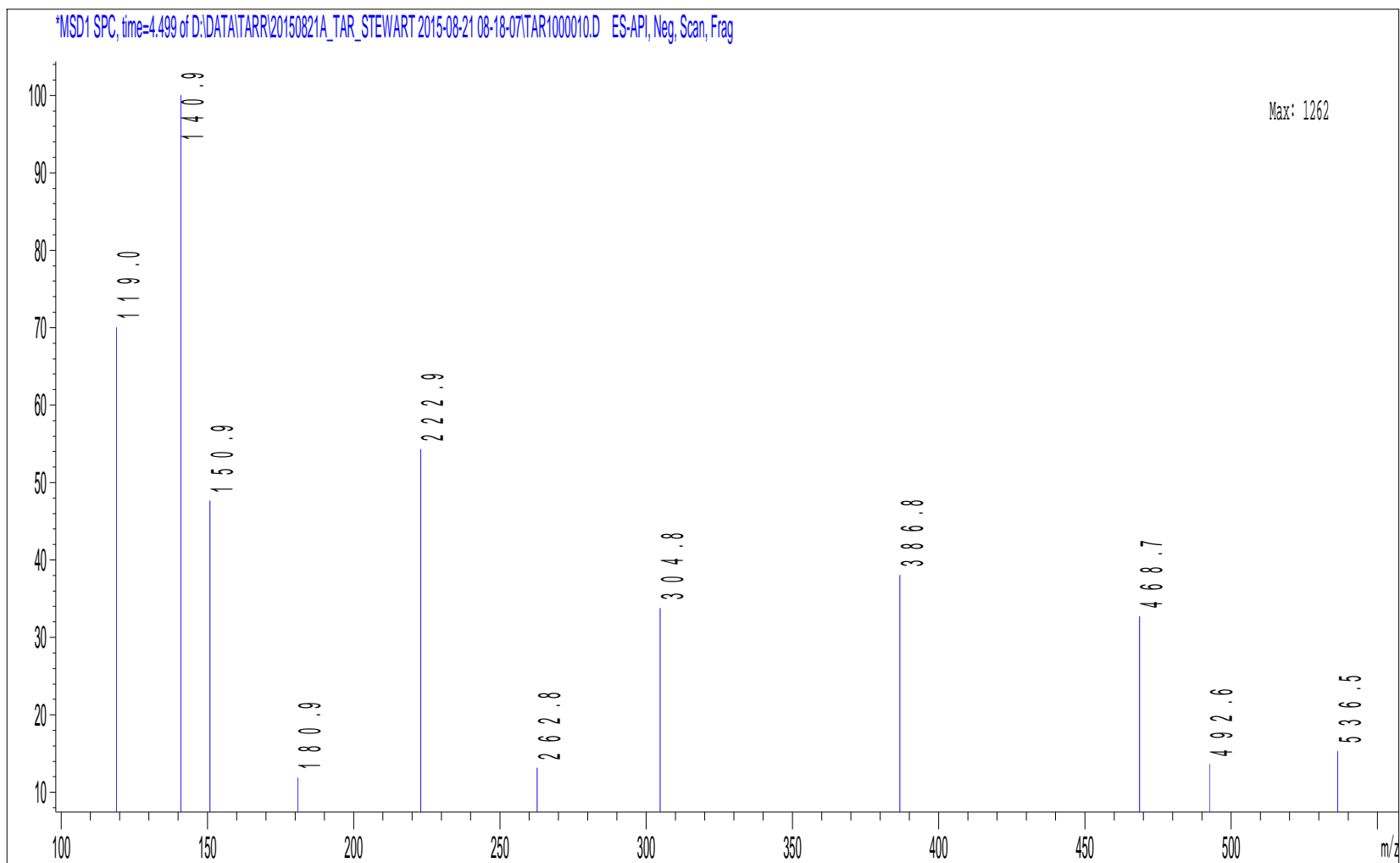






\*MSD1 SPC, time=4.398 of D:\DATA\TARR\20150821A\_TAR\_STEWART 2015-08-21 08-18-07\TAR1000010.D ES-API, Neg, Scan, Frag



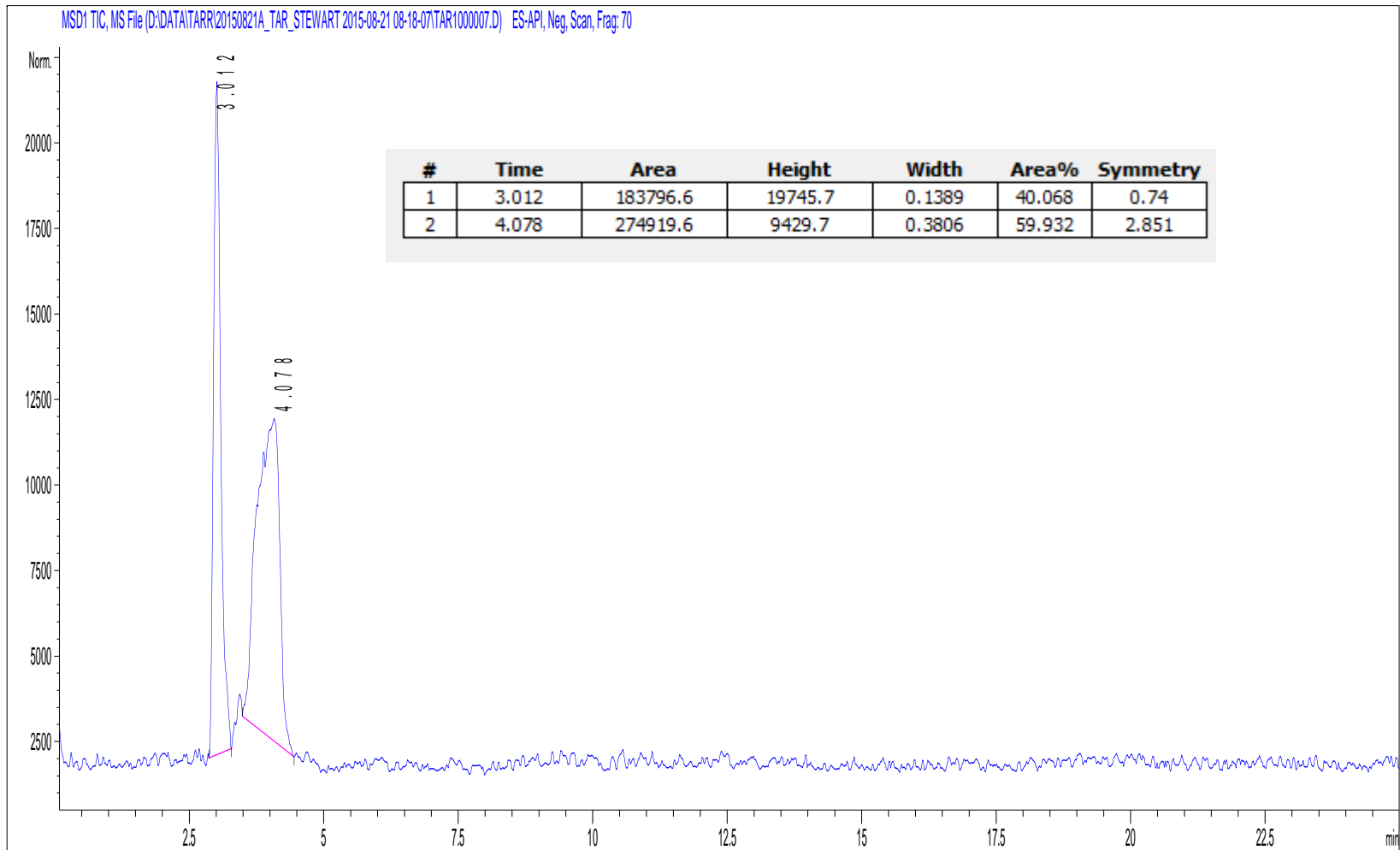


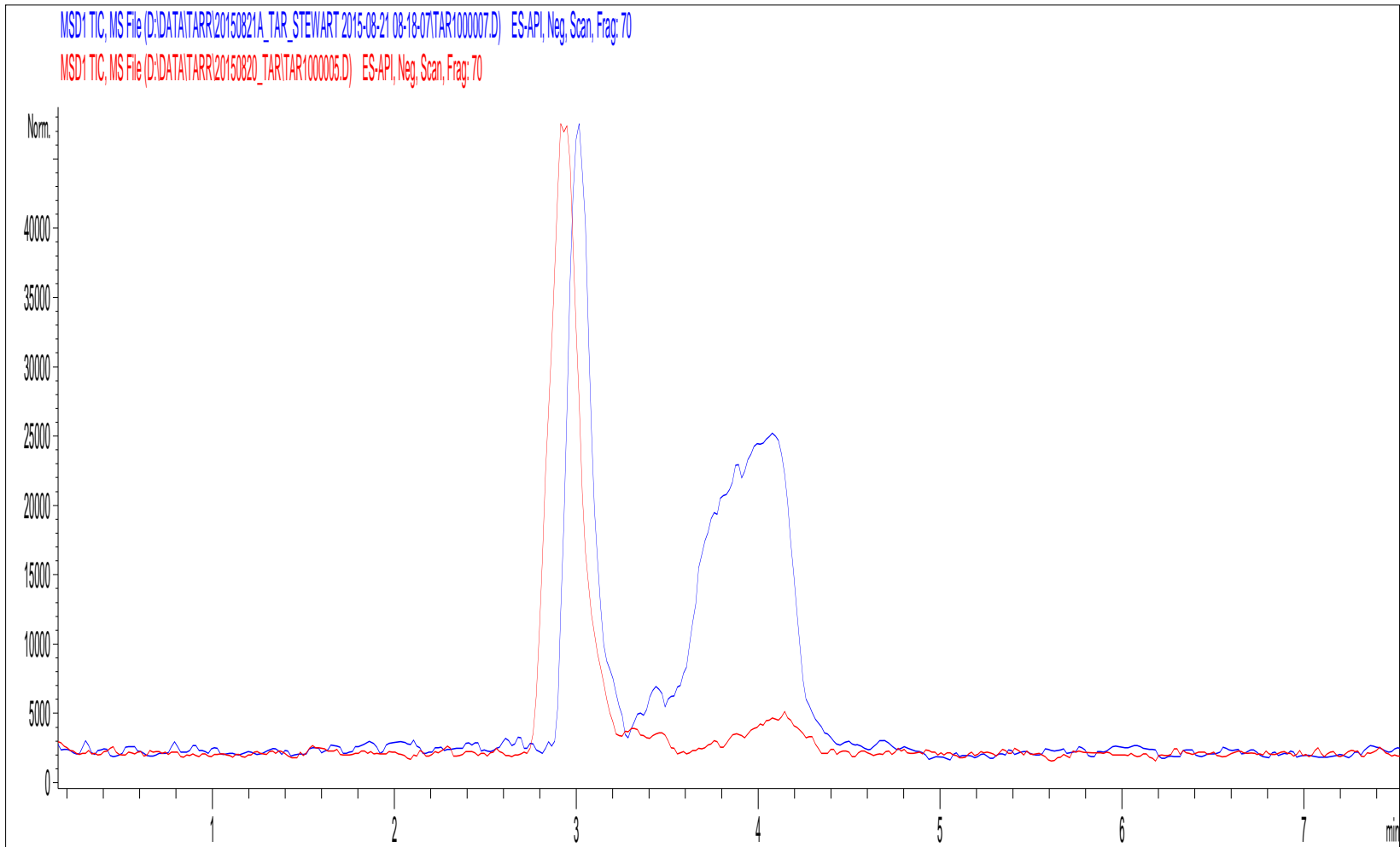
7-May-15

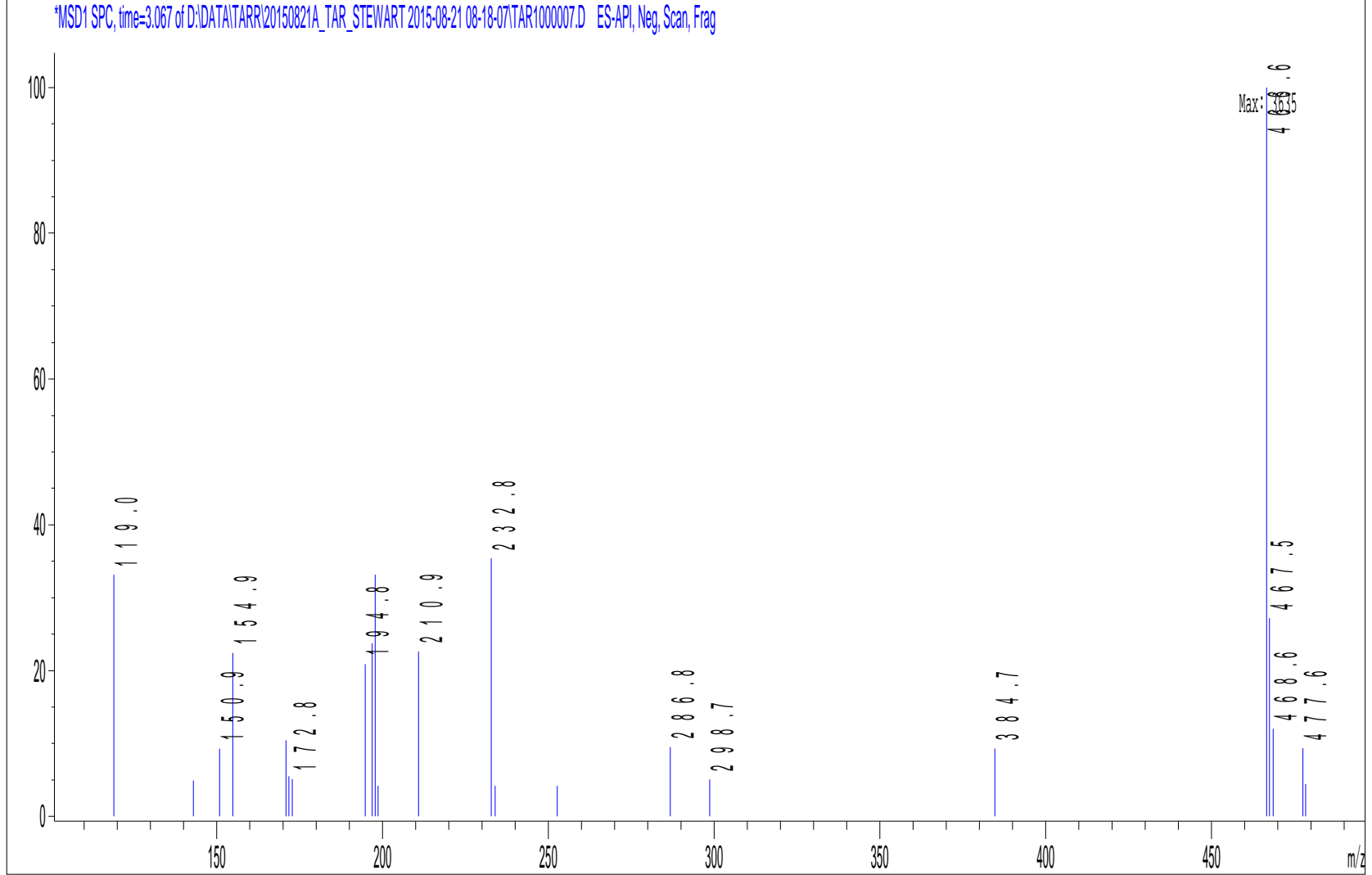
50 DC

9

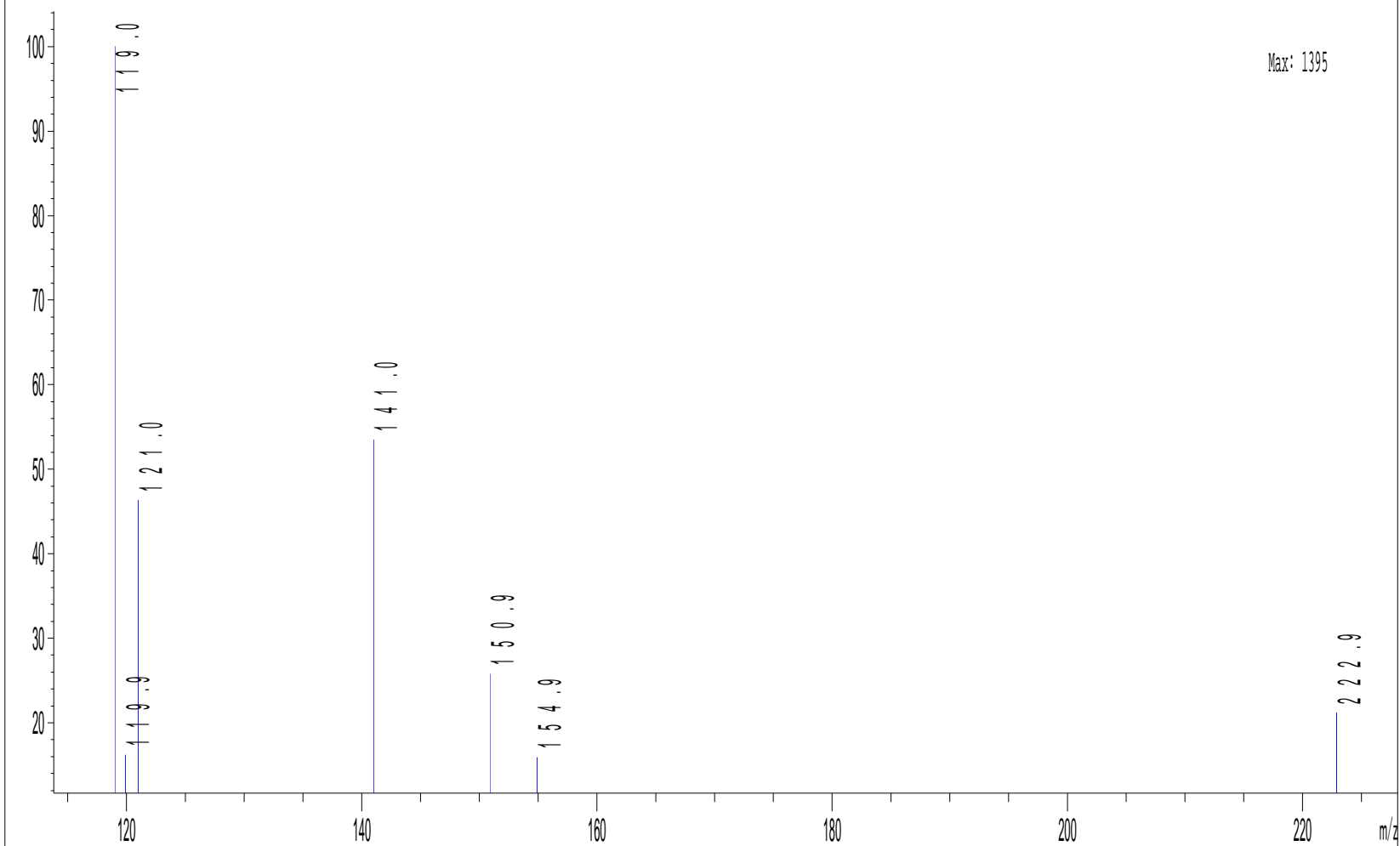
P2-E-06

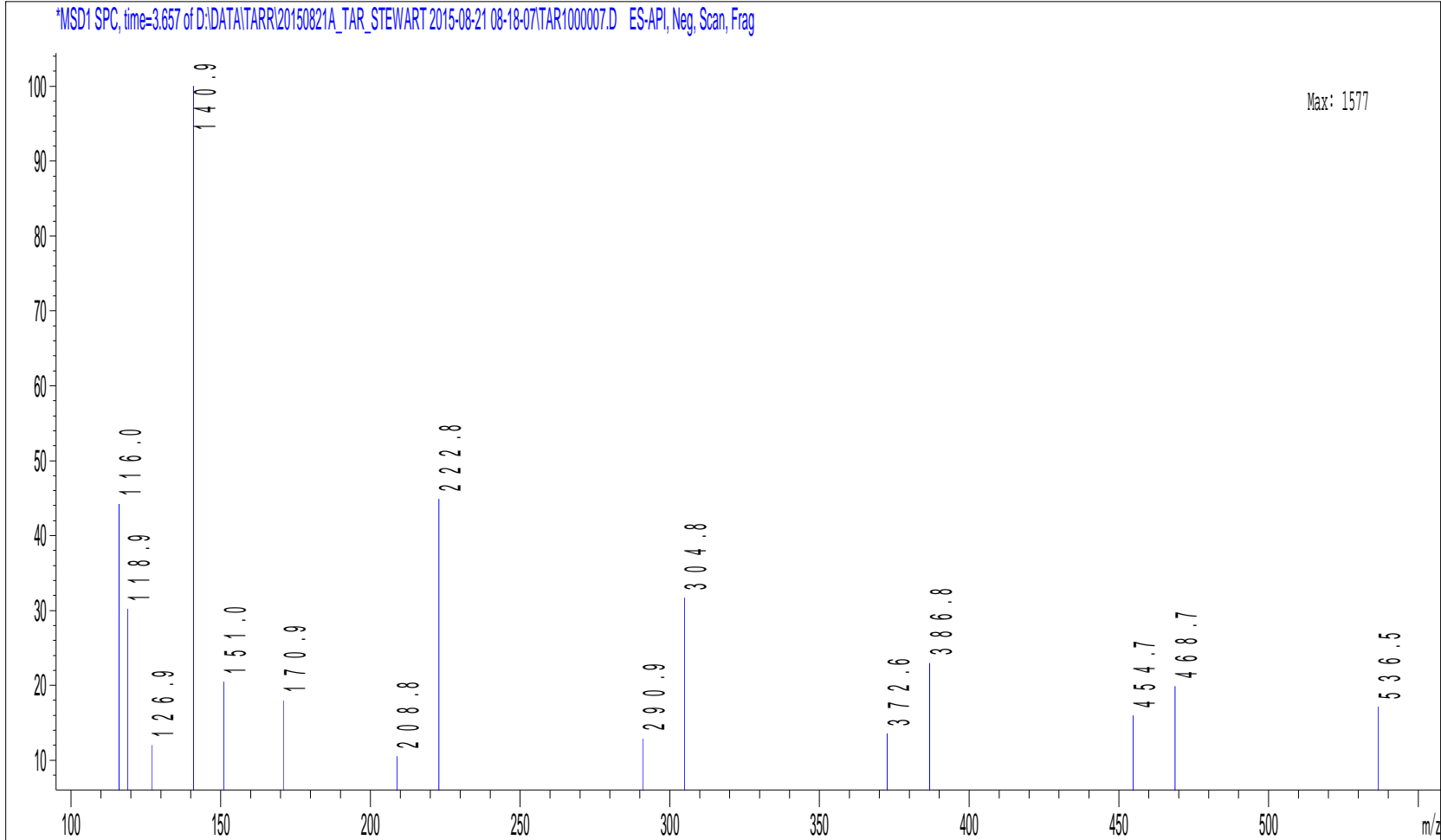




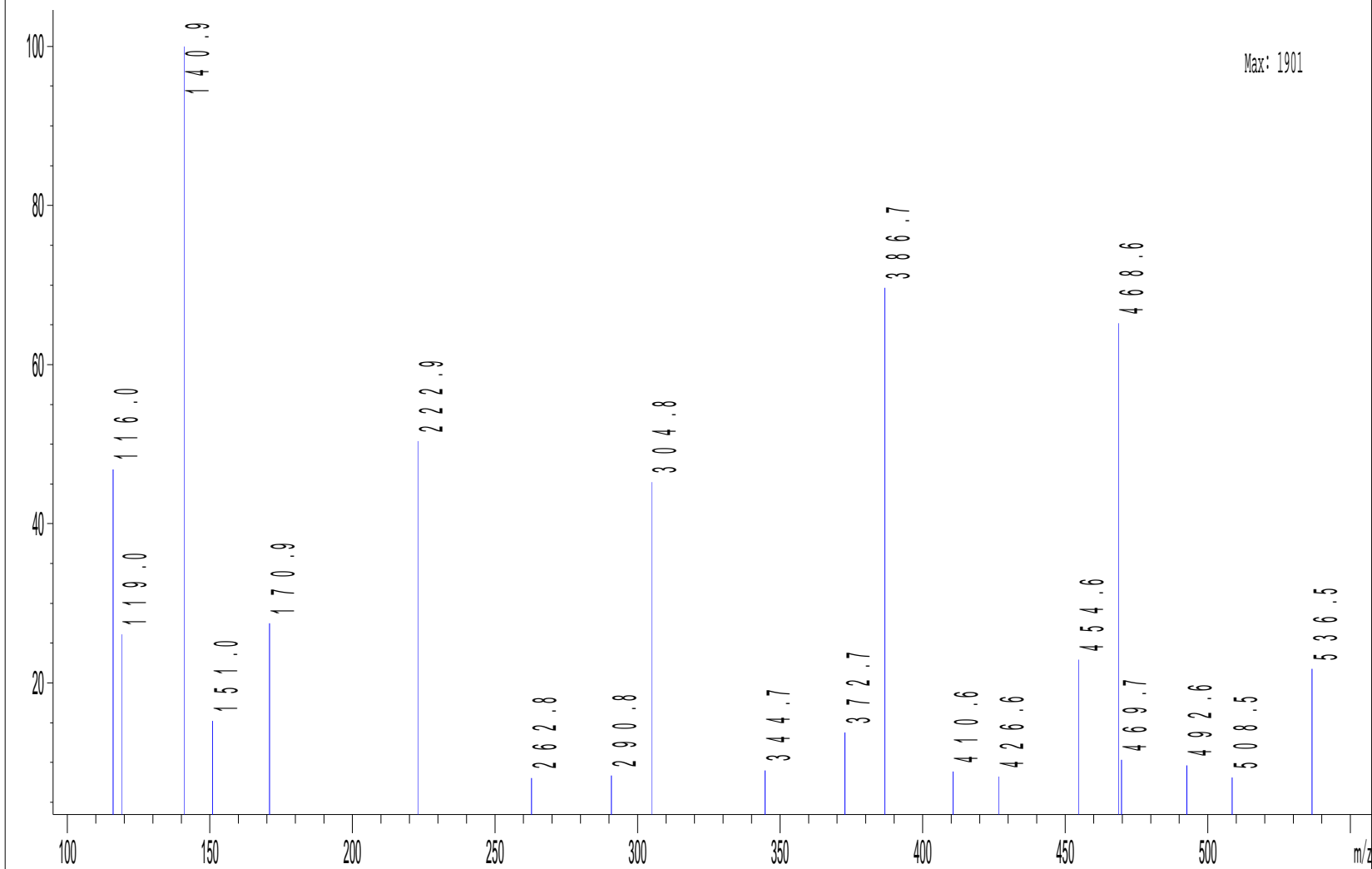


\*MSD1 SPC, time=3.438 of D:\DATA\TARR\20150821A\_TAR\_STEWART 2015-08-21 08-18-07\TAR1000007.D ES-API, Neg, Scan, Frag





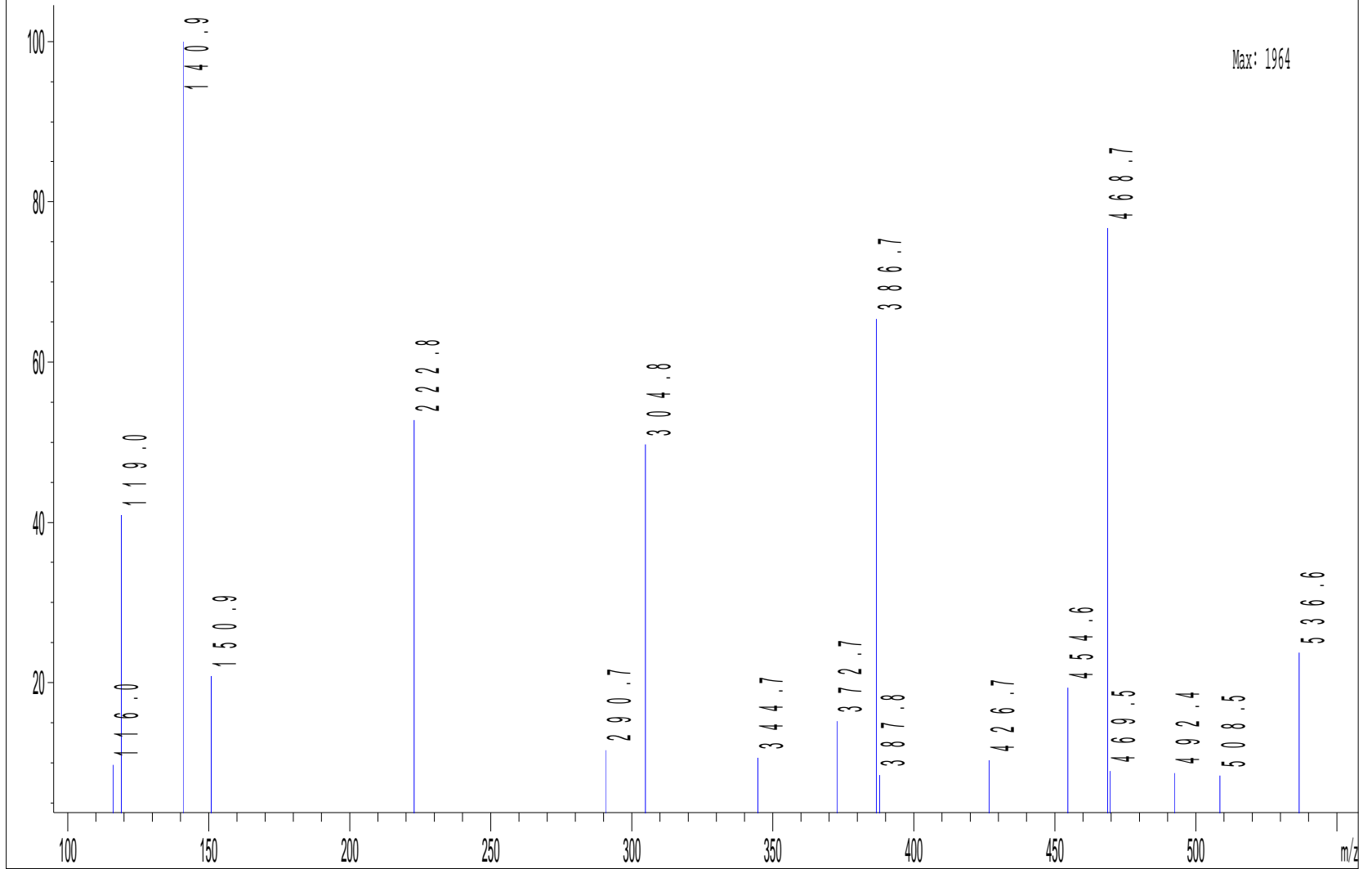
\*MSD1 SPC, time=3.893 of D:\DATA\TARR\20150821A\_TAR\_STEWART 2015-08-21 08-18-07\TAR1000007.D ES-API, Neg, Scan, Frag



Max: 1901



\*MSD1 SPC, time=4.145 of D:\DATA\TARR\20150821A\_TAR\_STEWART 2015-08-21 08-18-07\TAR1000007.D ES-API, Neg, Scan, Frag



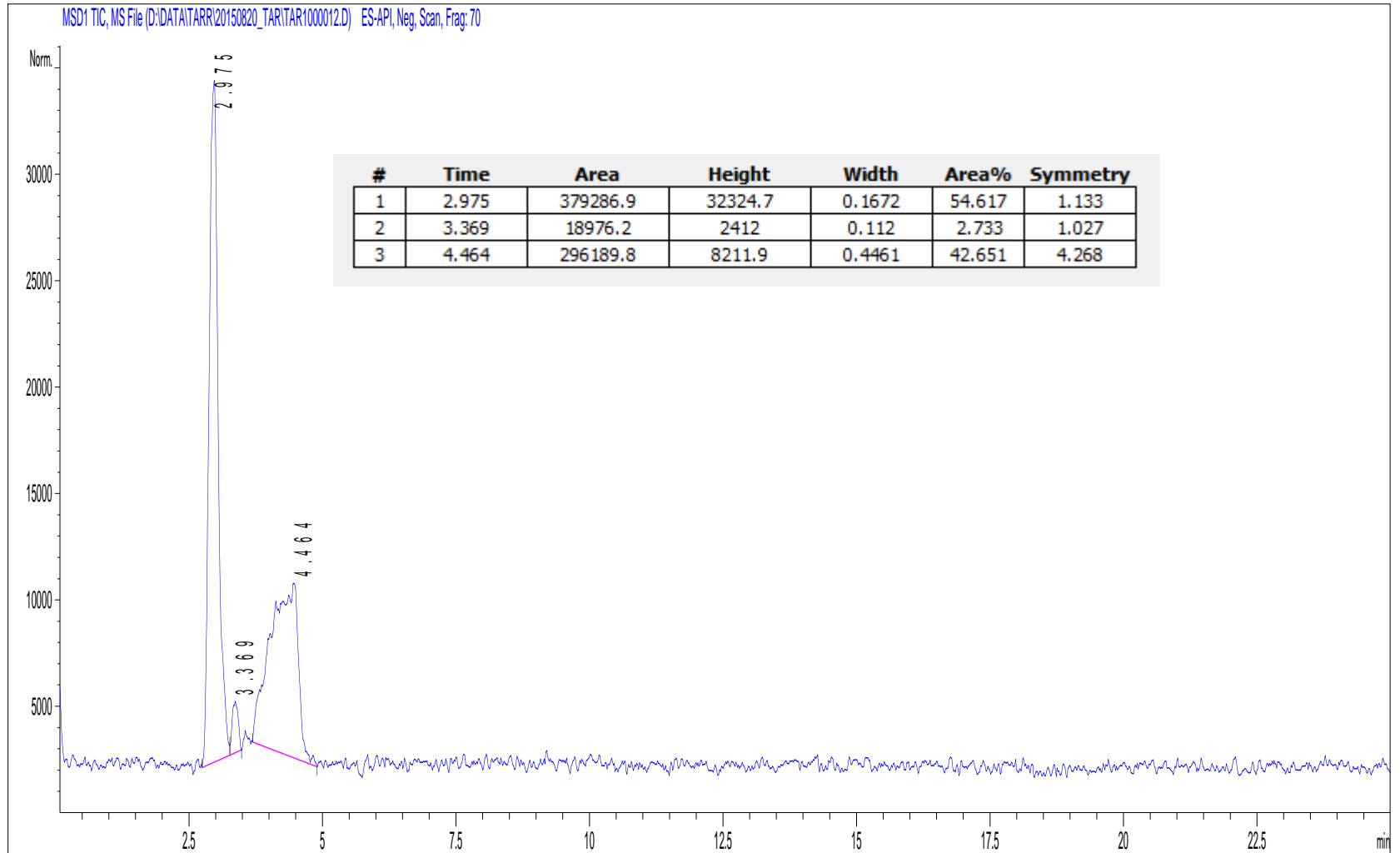
Max: 1964

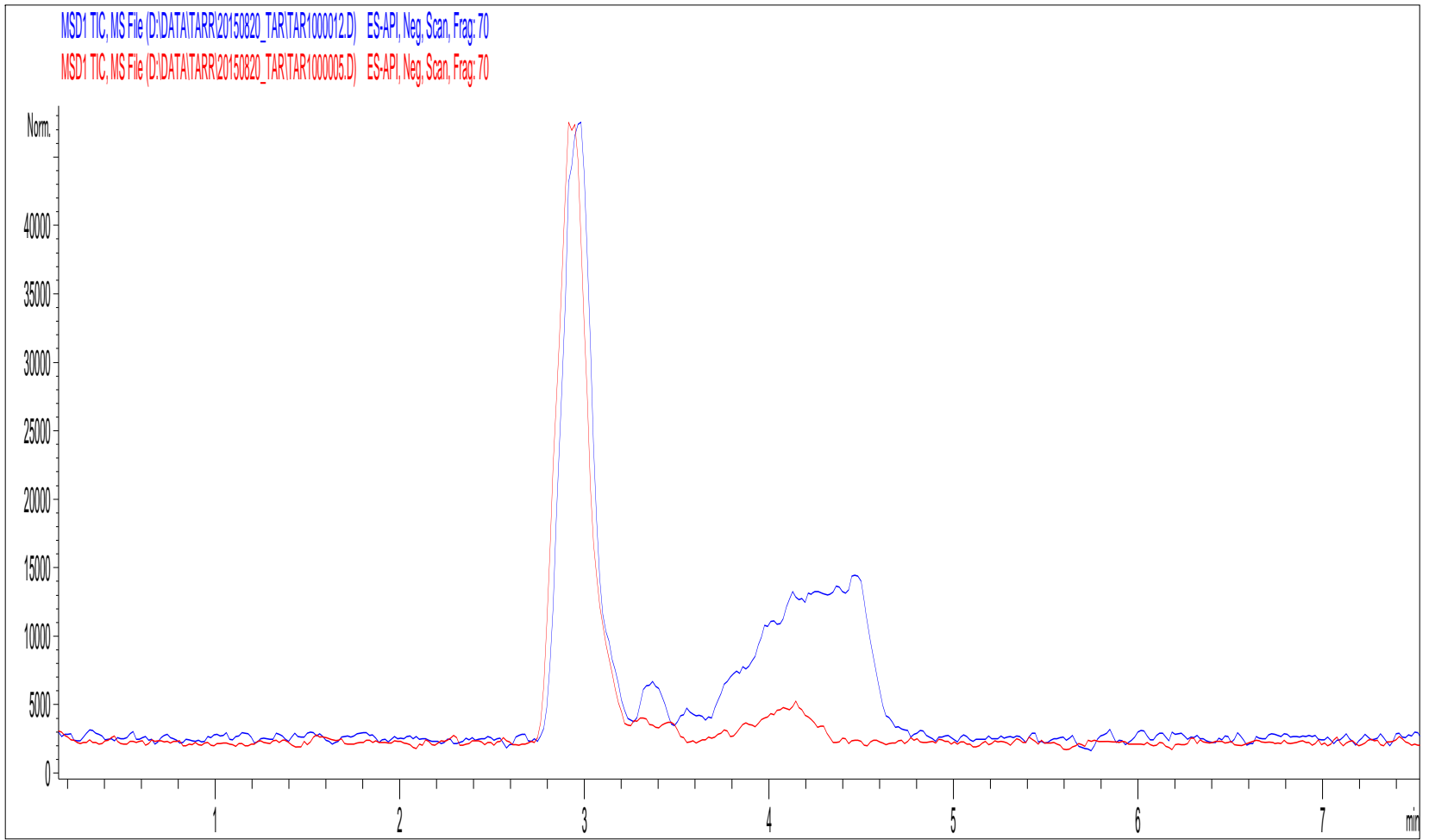
15-Jun-15

50 DC Repeat

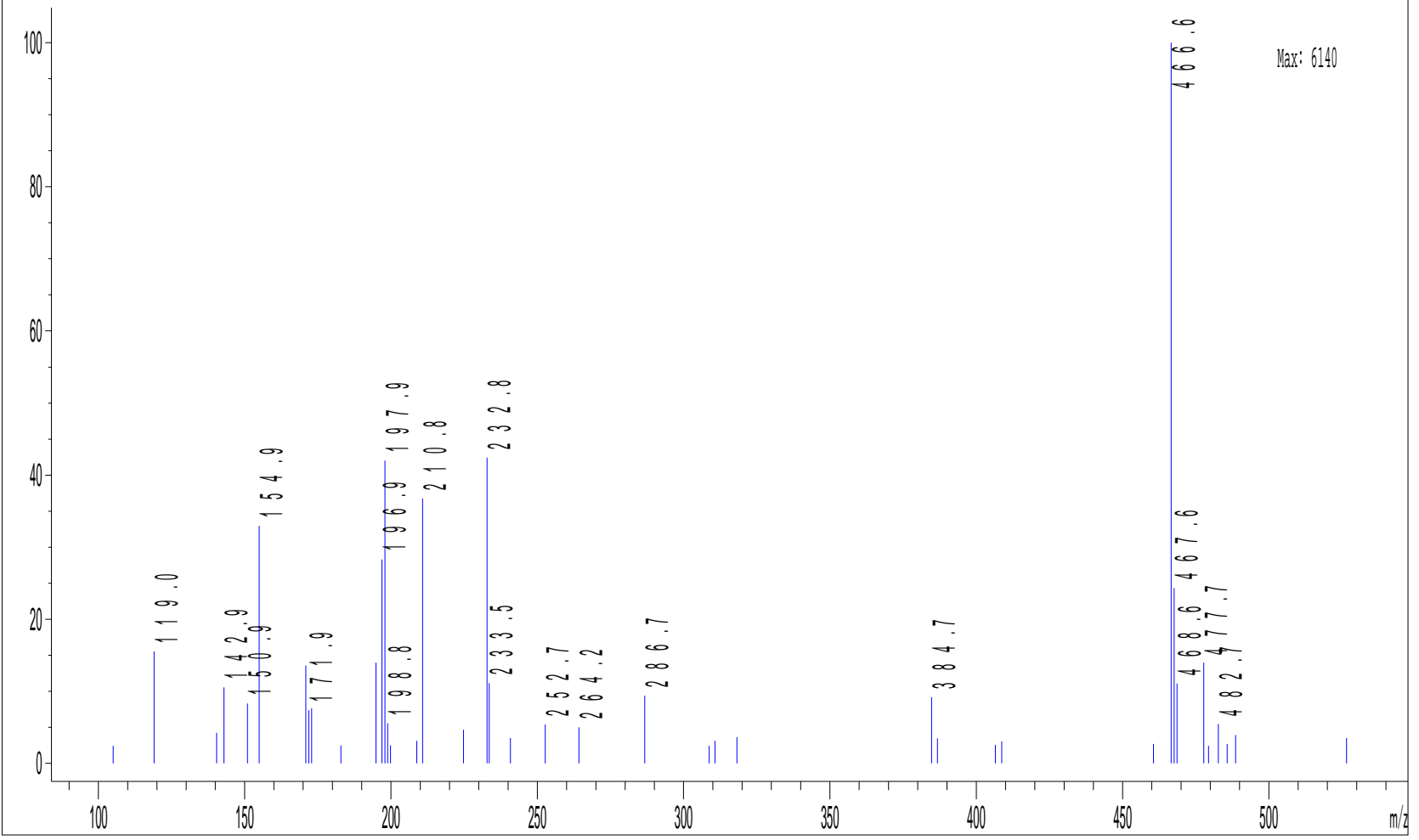
9

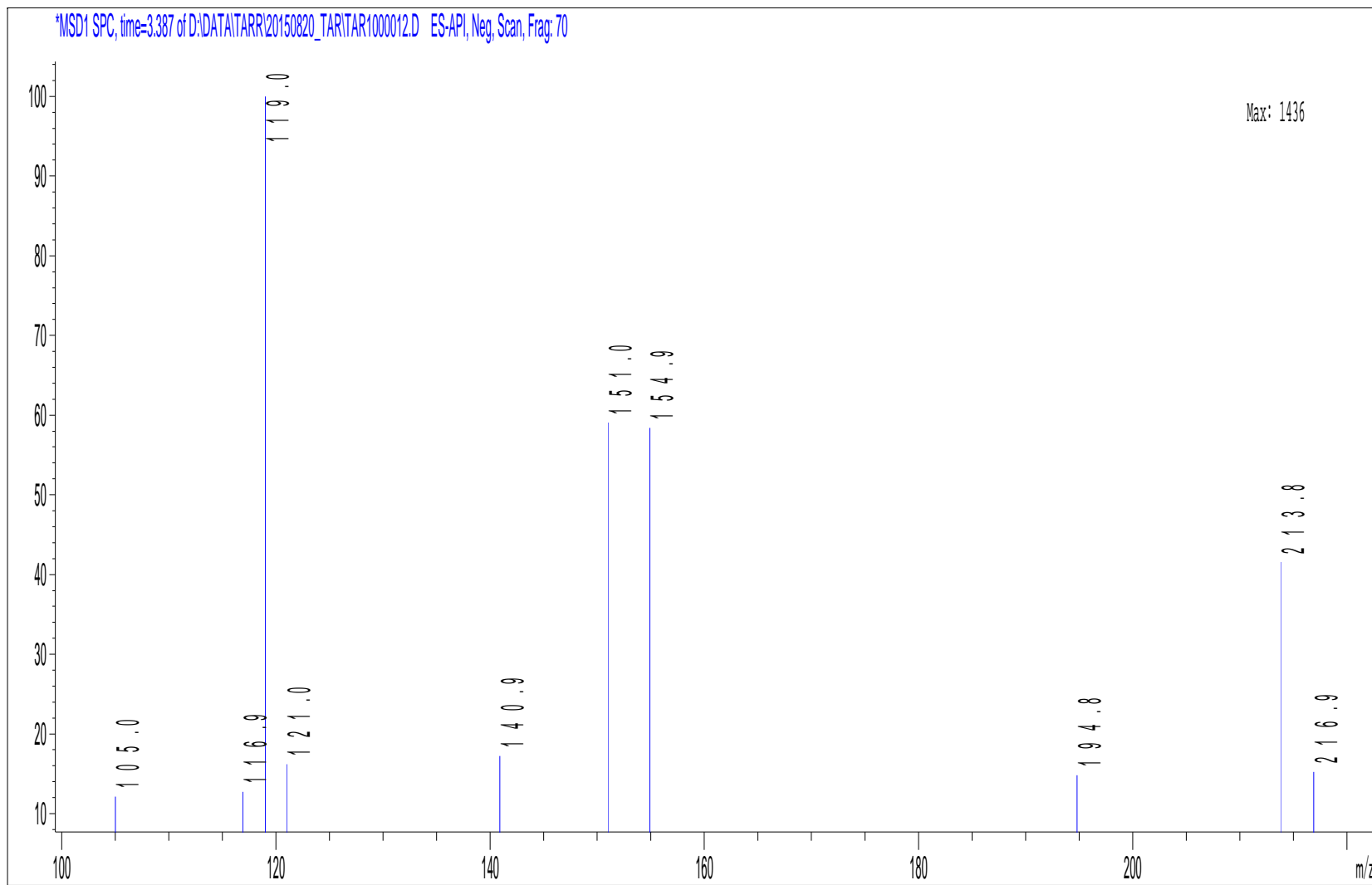
P2-B-07



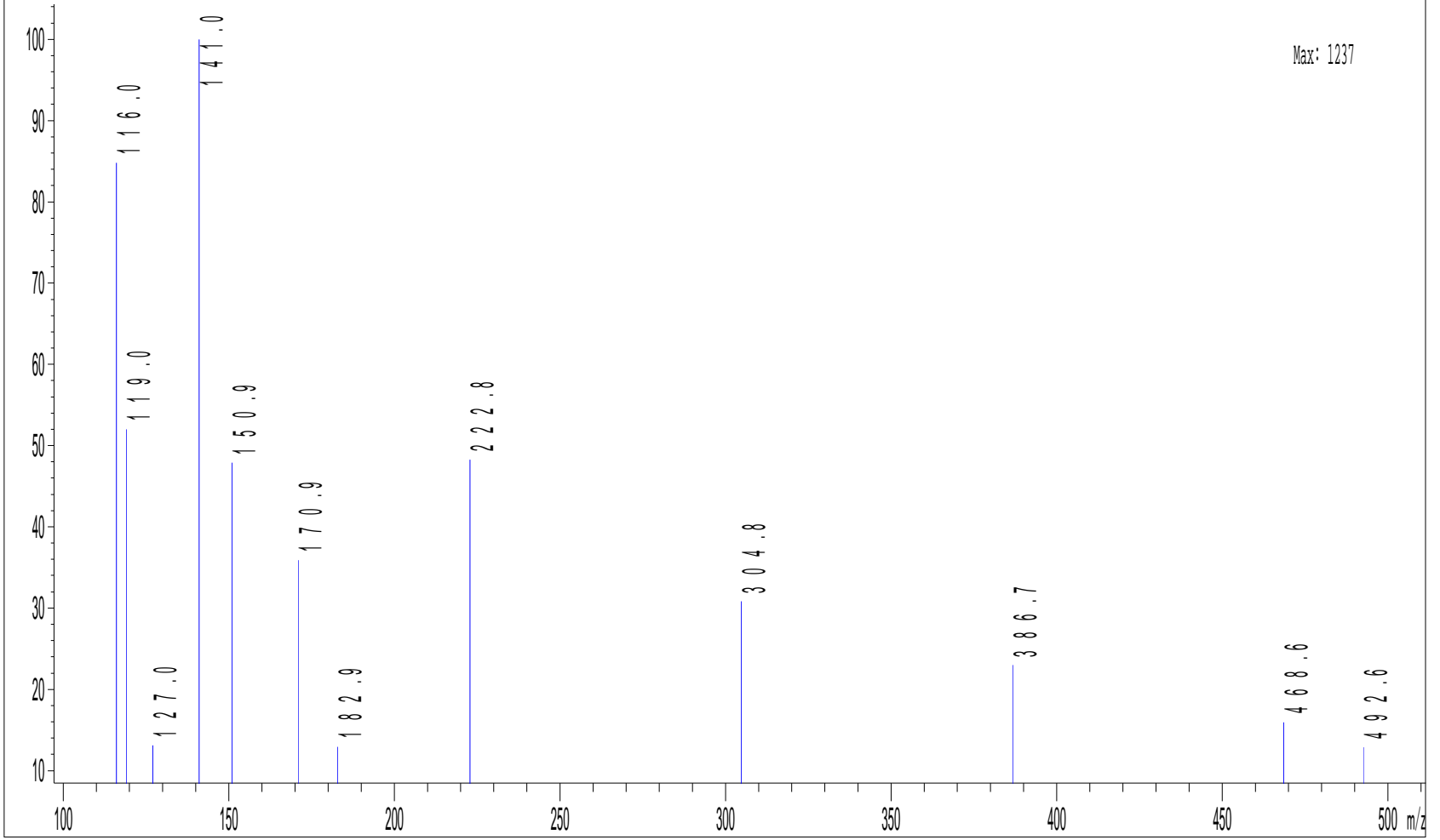


\*MSD1 SPC, time=2.999 of D:\DATA\TARR\20150820\_TARITAR1000012.D ES-API, Neg, Scan, Frag: 70

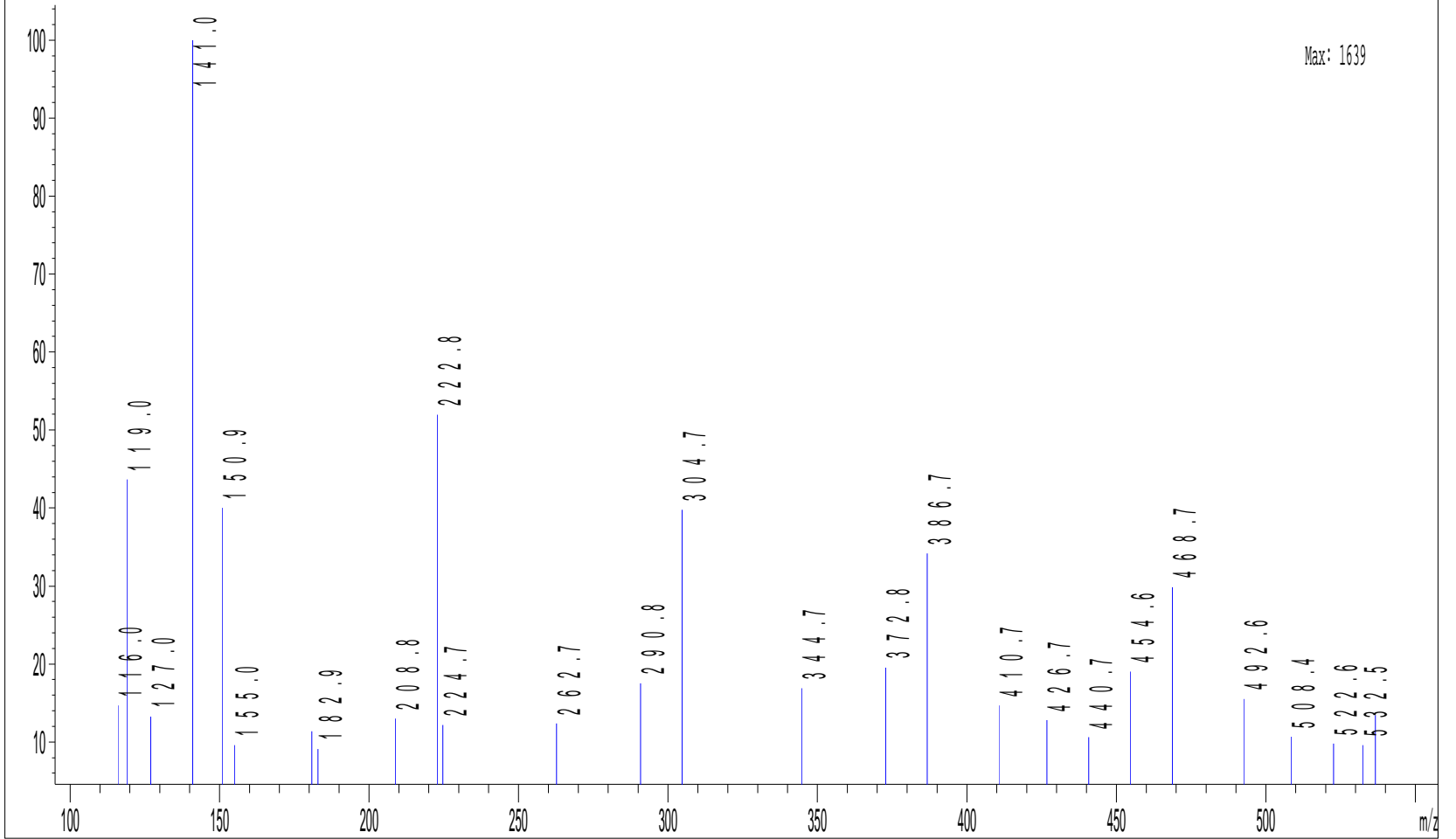




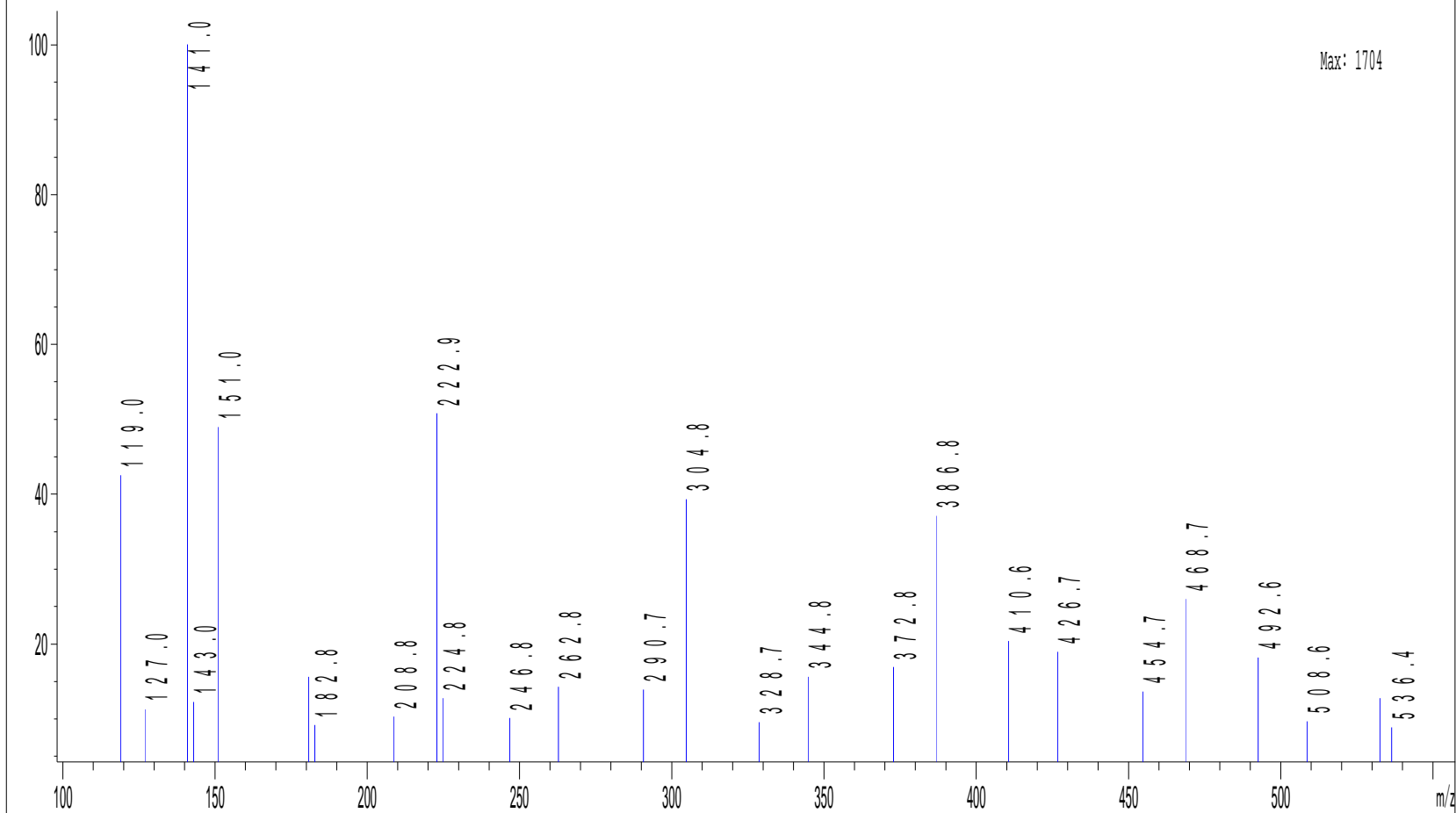
\*MSD1 SPC, time=3.876 of D:\DATA\TARR\20150820\_TARITAR1000012.D ES-API, Neg, Scan, Frag: 70



\*MSD1 SPC, time=4.129 of D:\DATA\TARR\20150820\_TARITAR1000012.D ES-API, Neg, Scan, Frag: 70



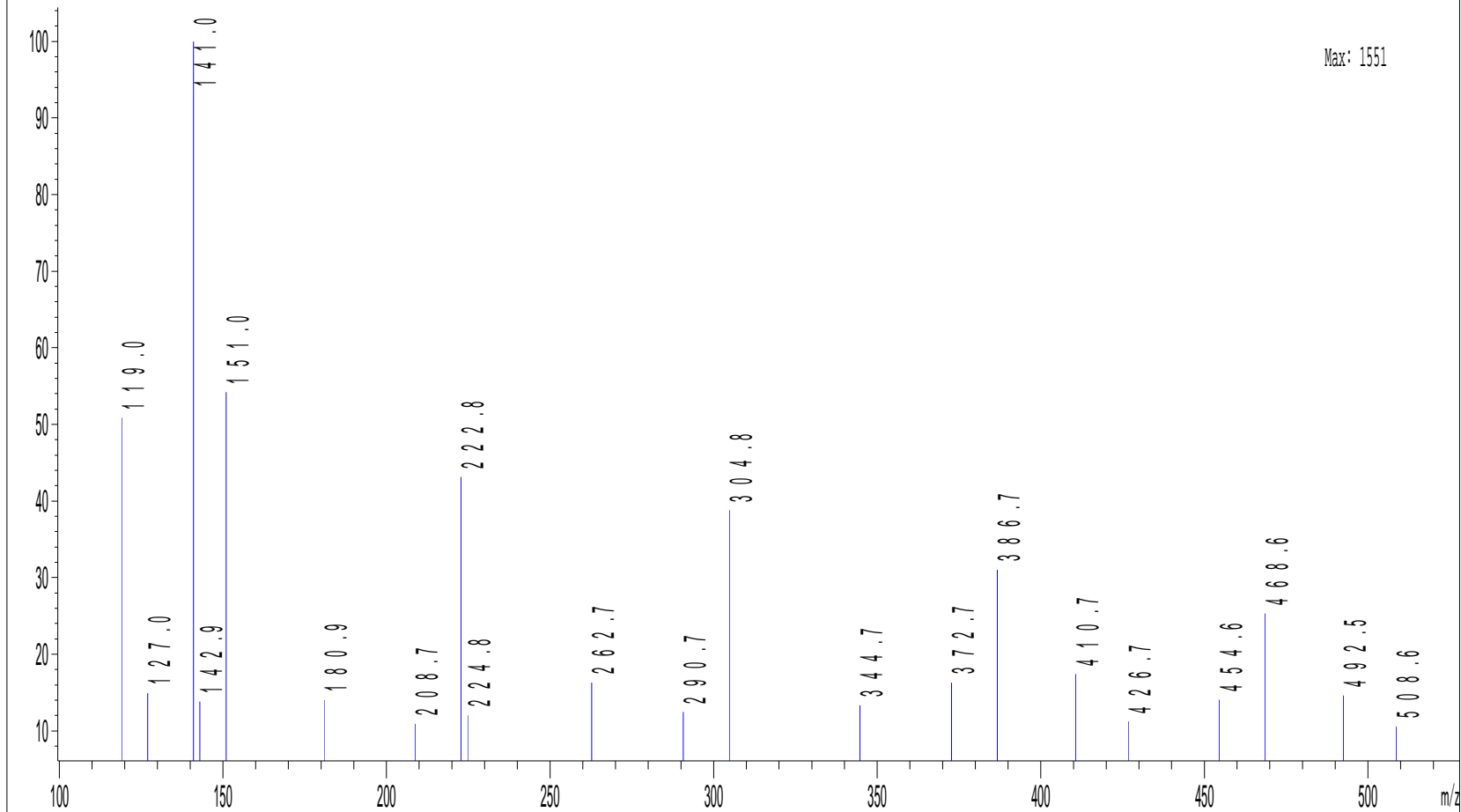
\*MSD1 SPC, time=4.364 of D:\DATA\TARR\20150820\_TAR\TAR1000012.D ES-API, Neg, Scan, Frag: 70



Max: 1704



\*MSD1 SPC, time=4.533 of D:\DATA\TARR\20150820\_TARITAR1000012.D ES-API, Neg, Scan, Frag: 70

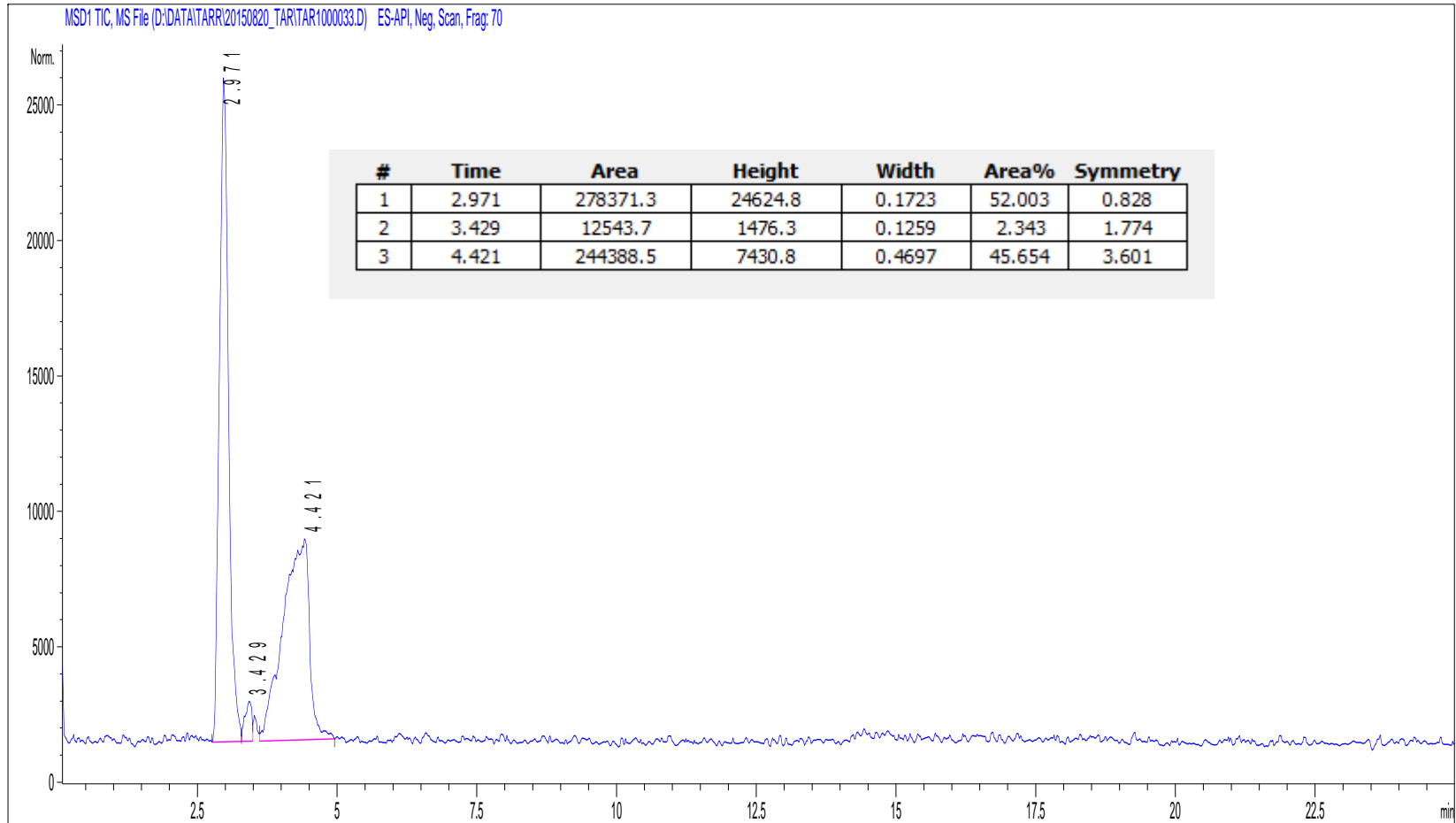


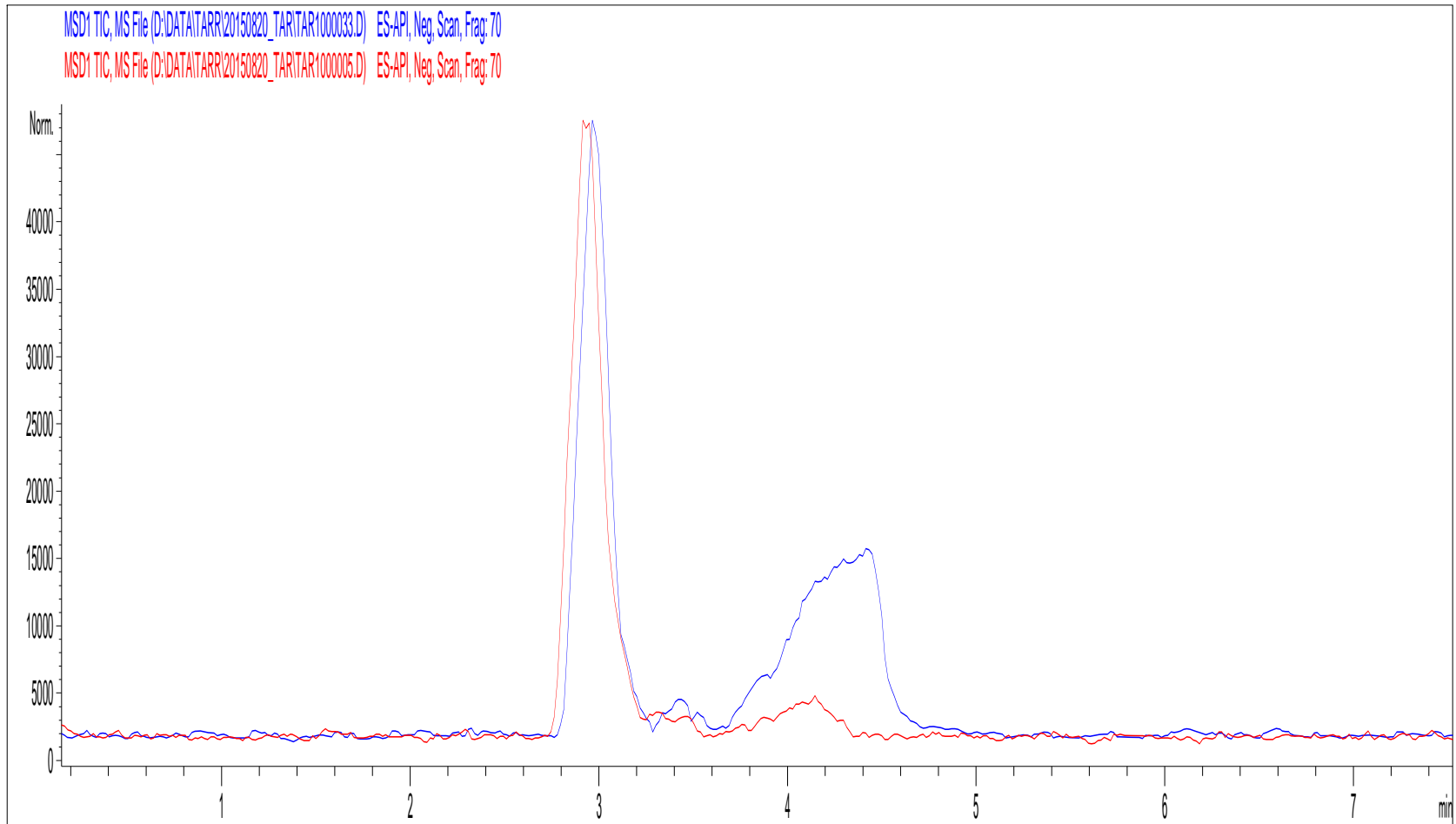
23-Jul-15

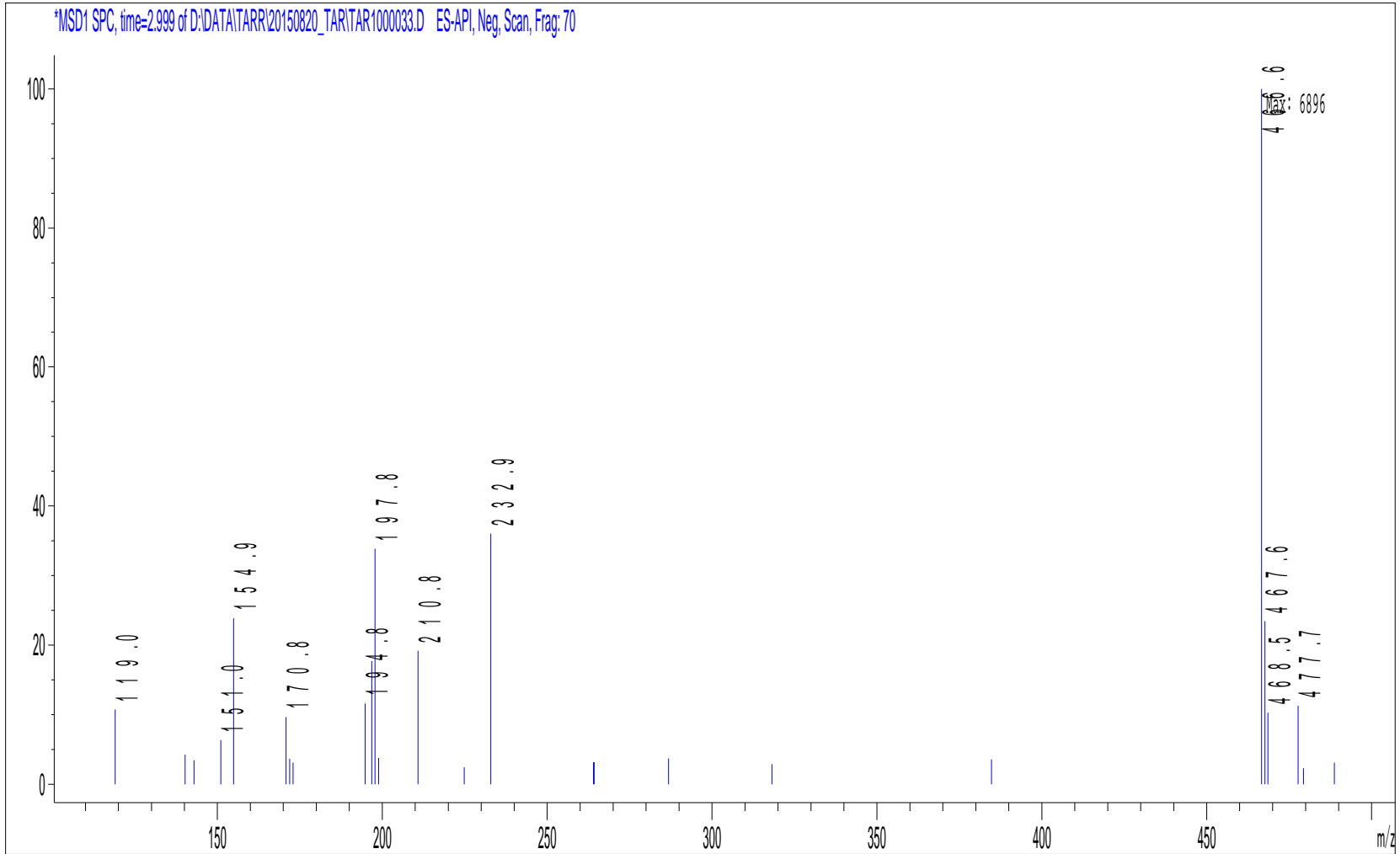
70 DC

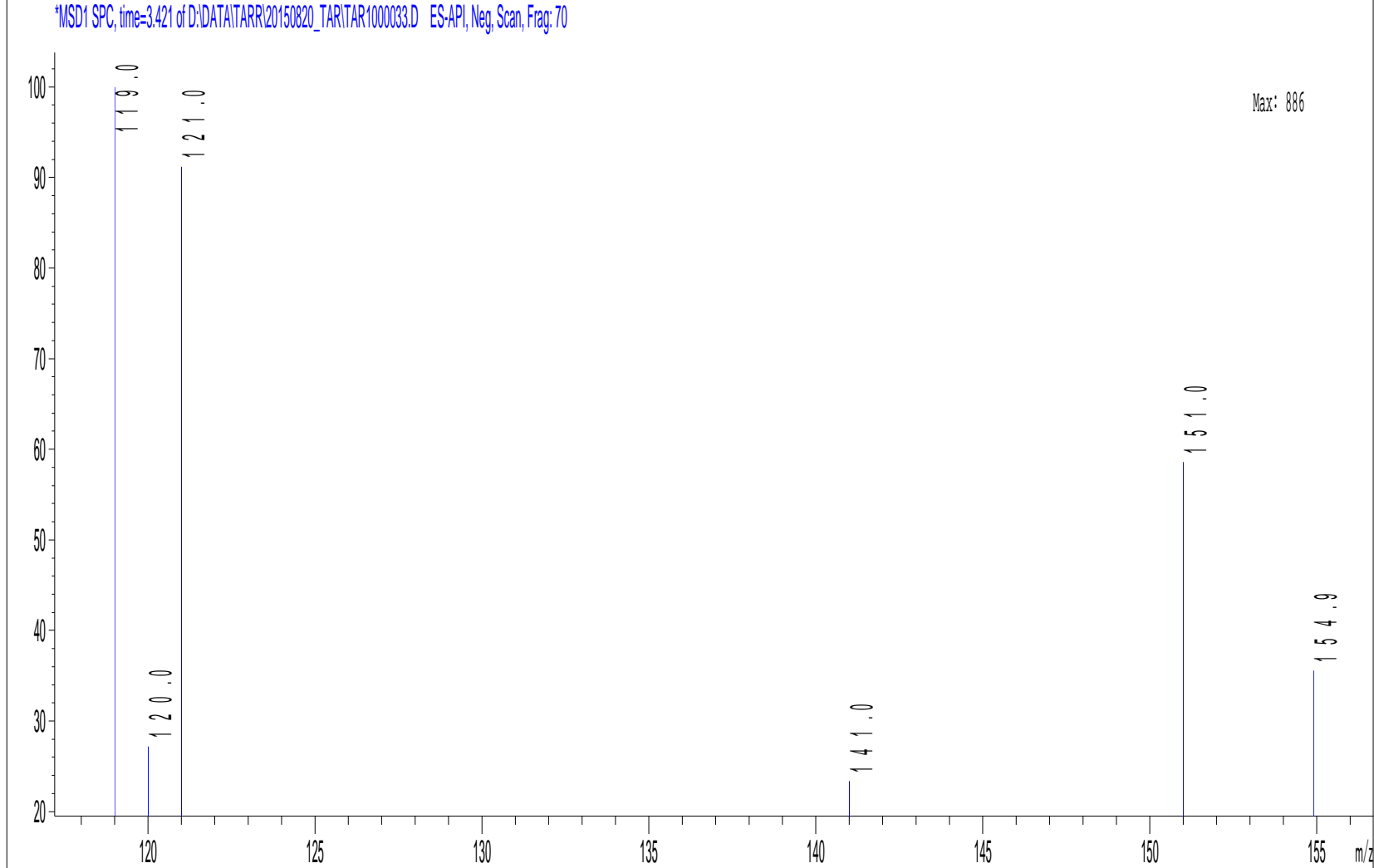
9

P2-D-04

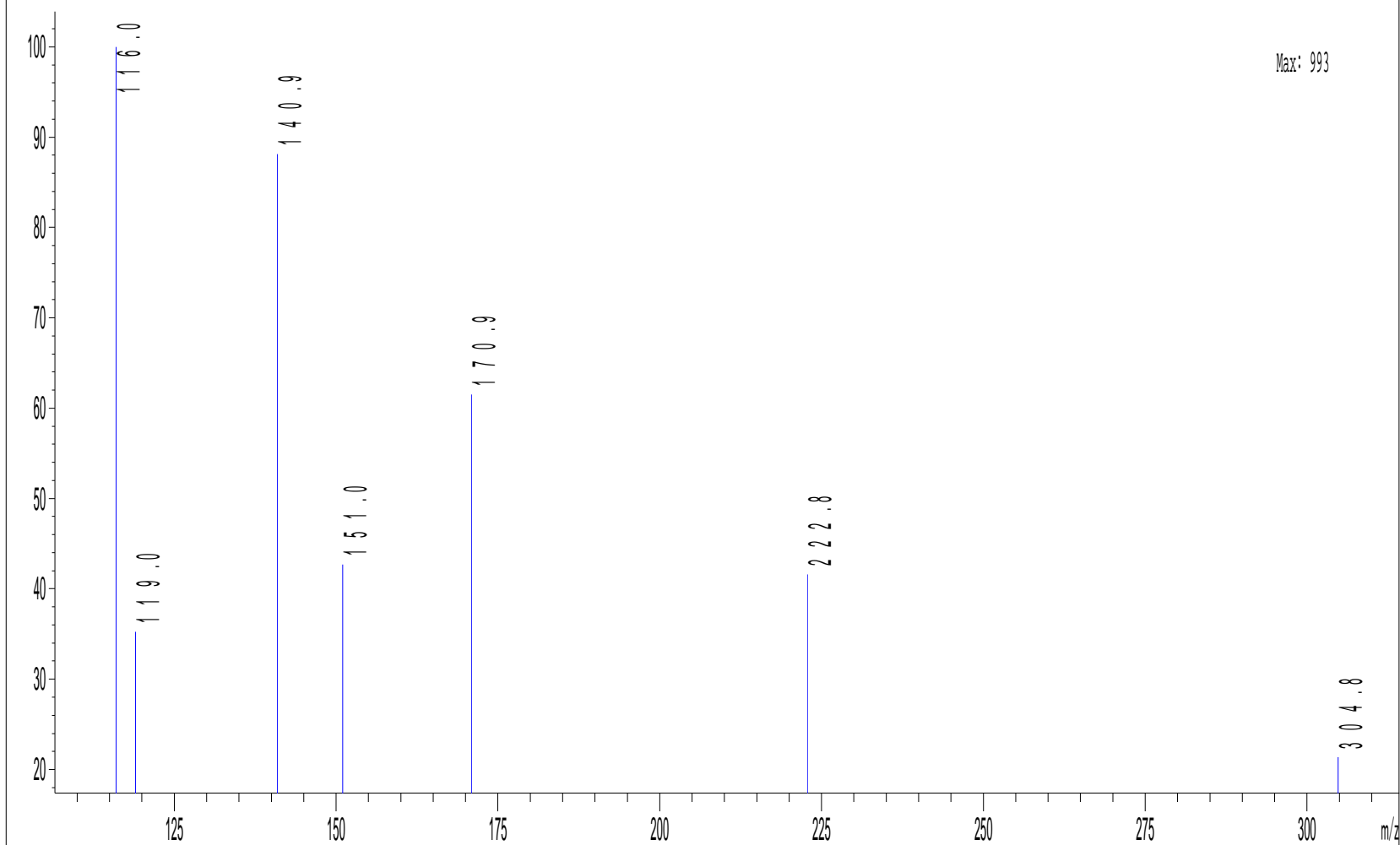




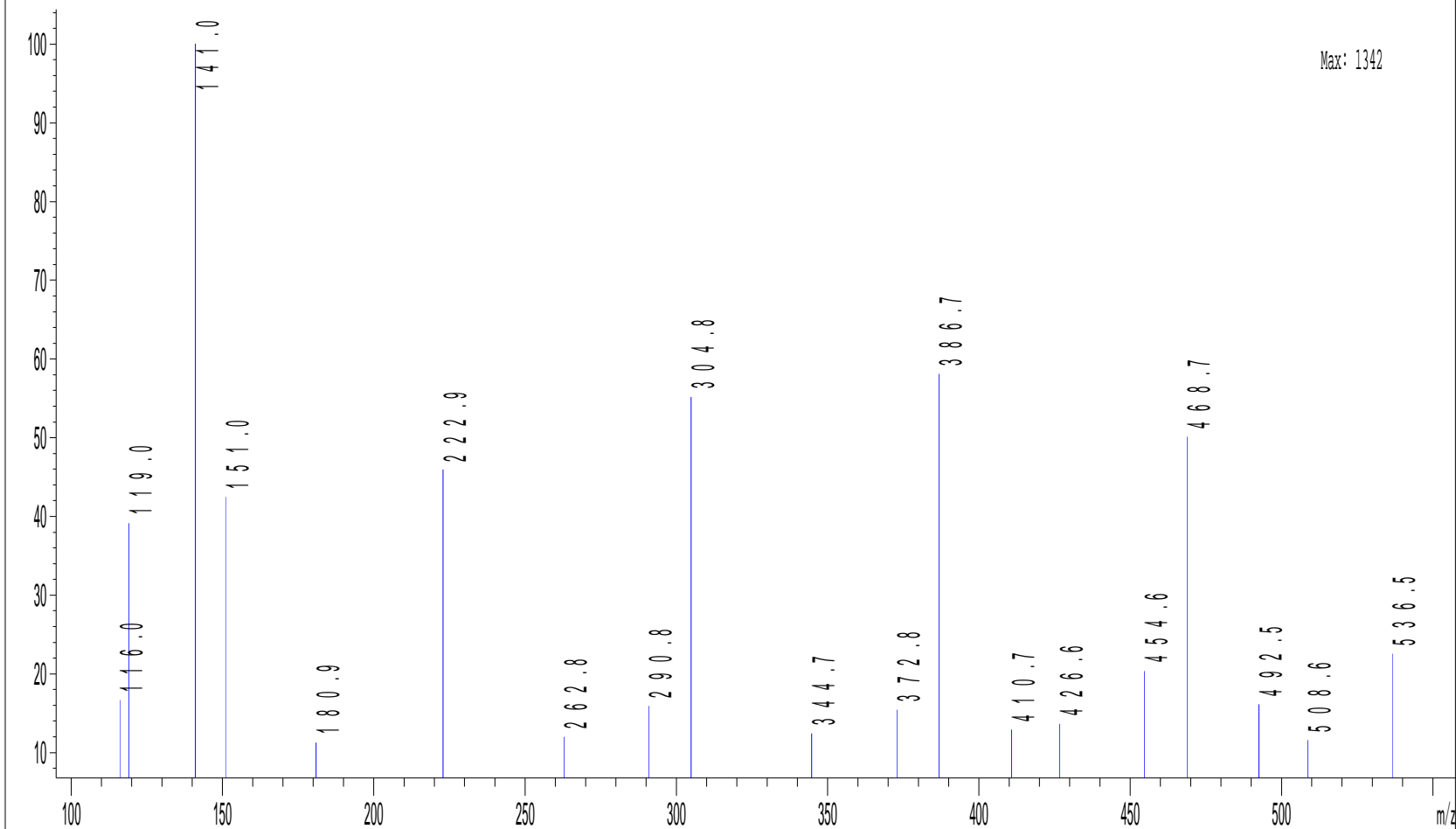




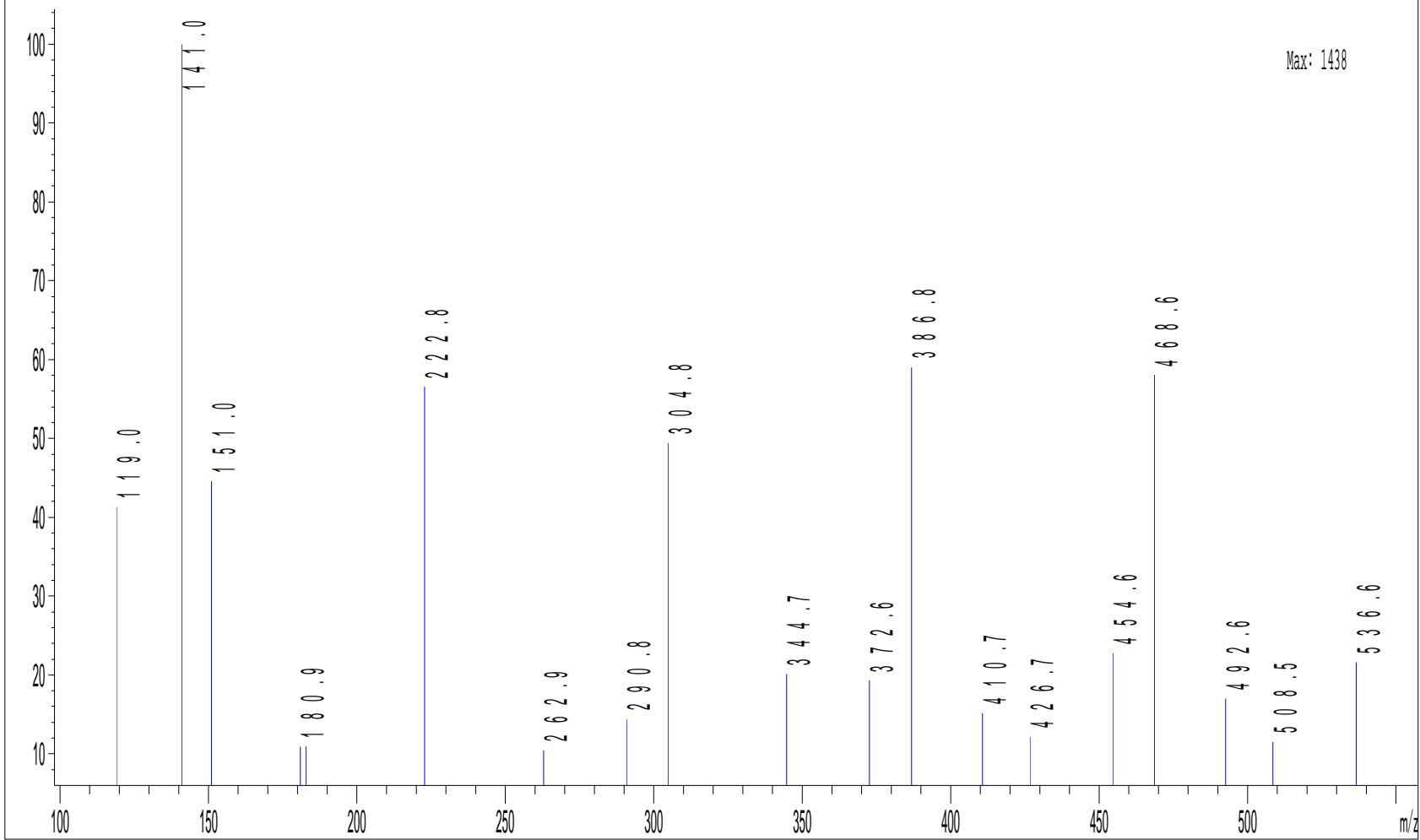
\*MSD1 SPC, time=3.859 of D:\DATA\TARR\20150820\_TARITAR1000033.D ES-API, Neg, Scan, Frag: 70



\*MSD1 SPC, time=4.145 of D:\DATA\TARR\20150820\_TAR\TAR1000033.D ES-API, Neg, Scan, Frag: 70

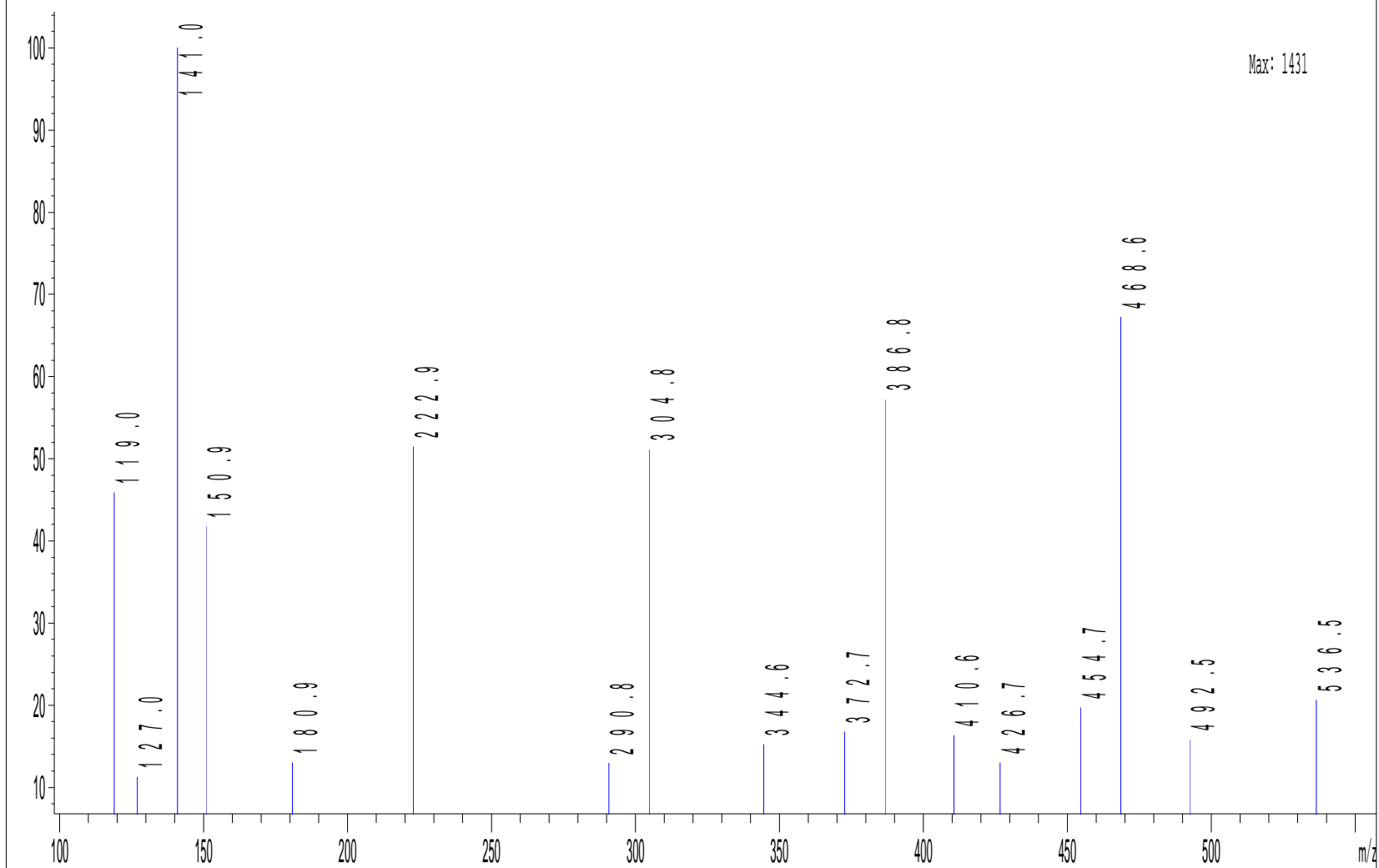


\*MSD1 SPC, time=4.297 of D:\DATA\TARR\20150820\_TARITAR1000033.D ES-API, Neg, Scan, Frag: 70





\*MSD1 SPC, time=4.466 of D:\DATA\ARR\20150820\_TARITAR1000033.D ES-API, Neg, Scan, Frag: 70



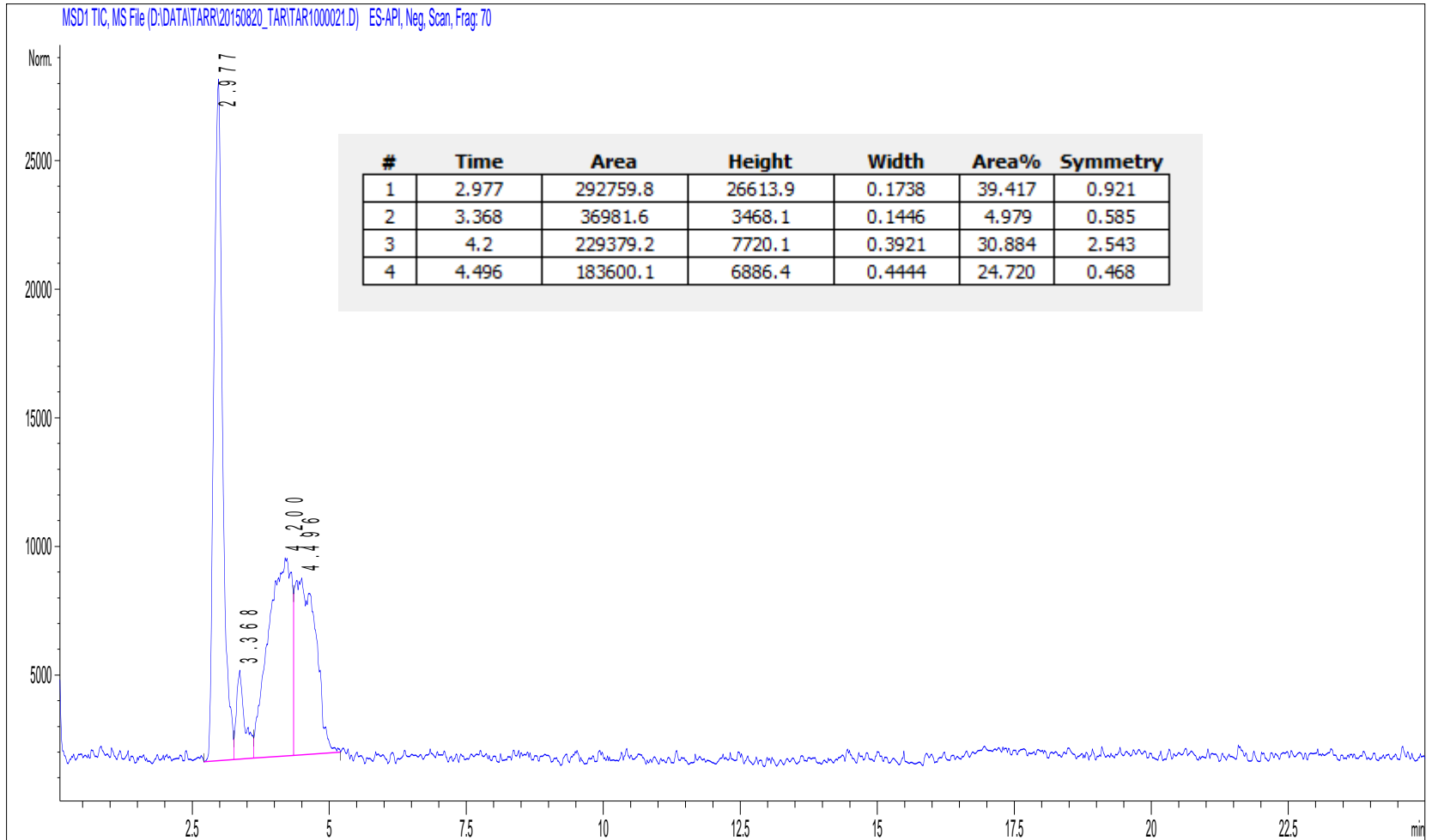
Max: 1431

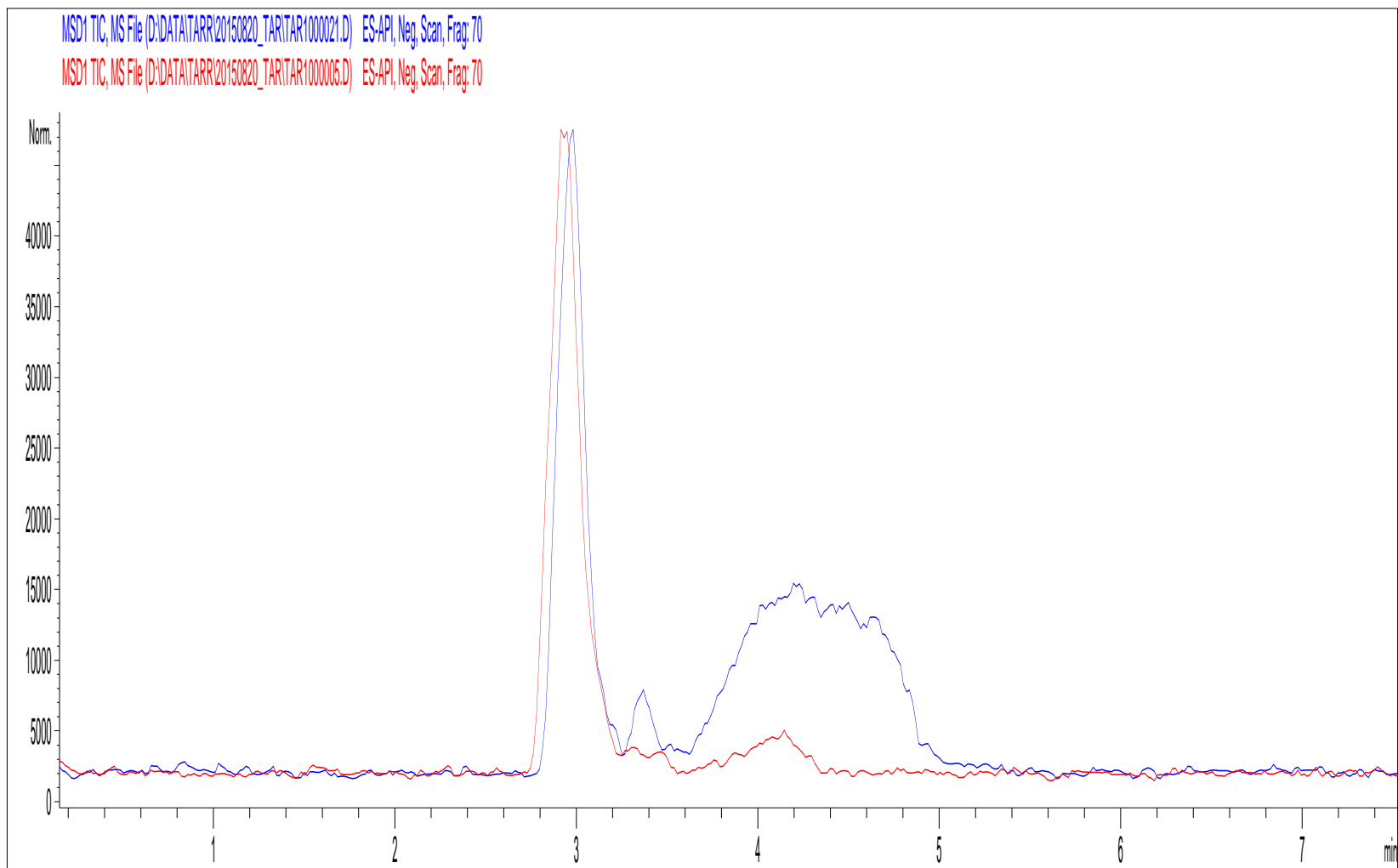
1-Jul-15

100 DC

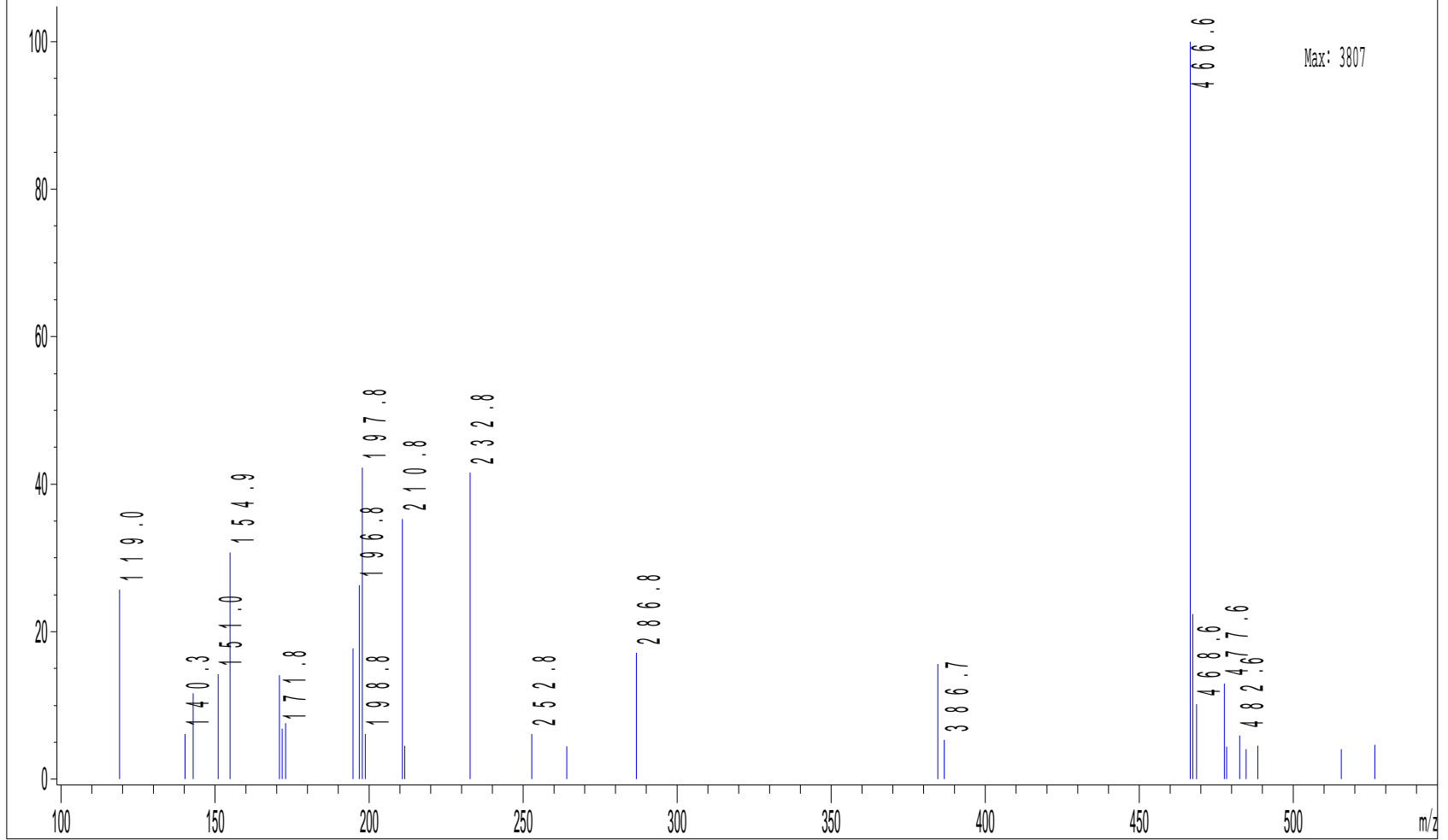
9

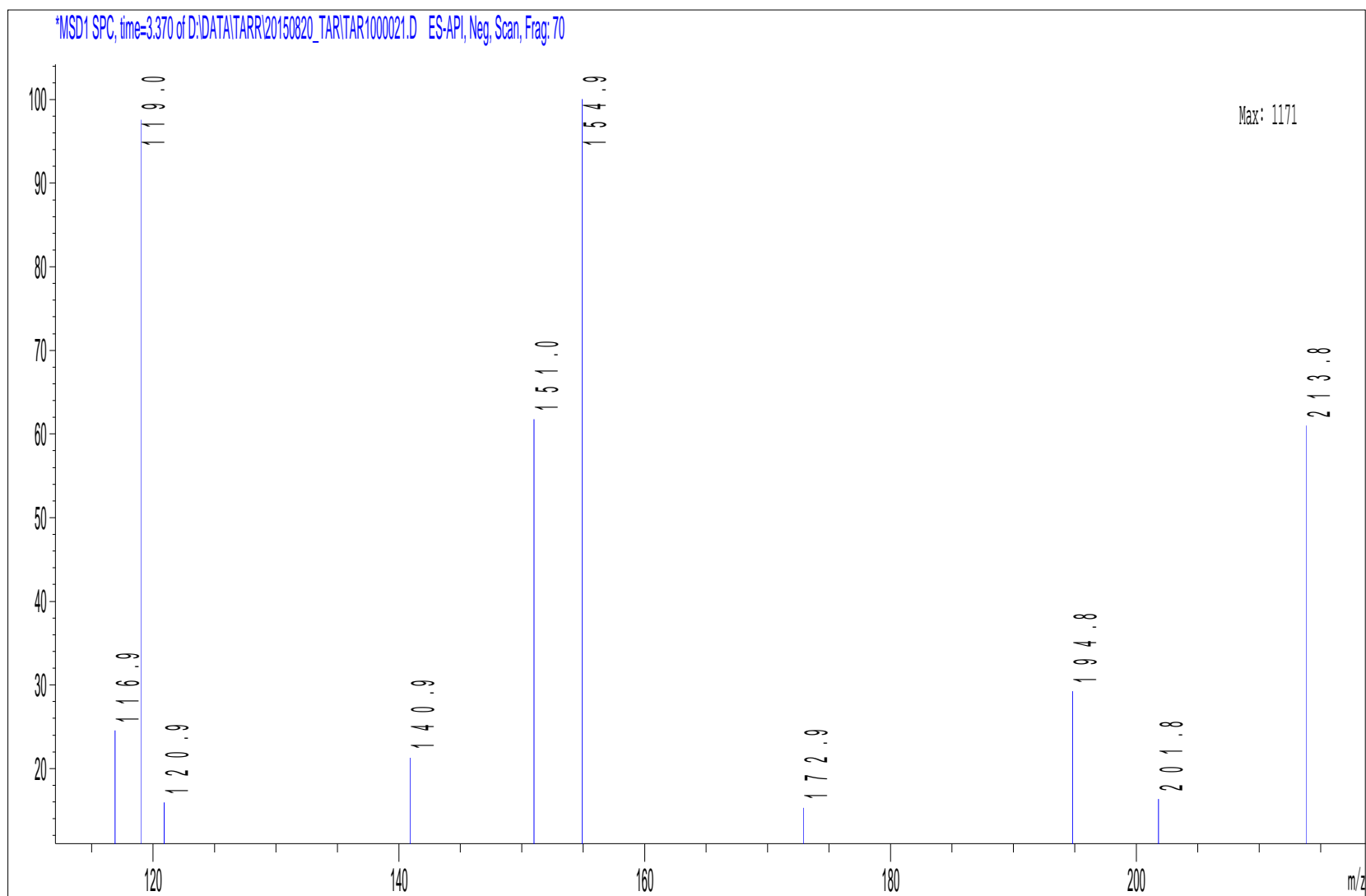
P2-C-03

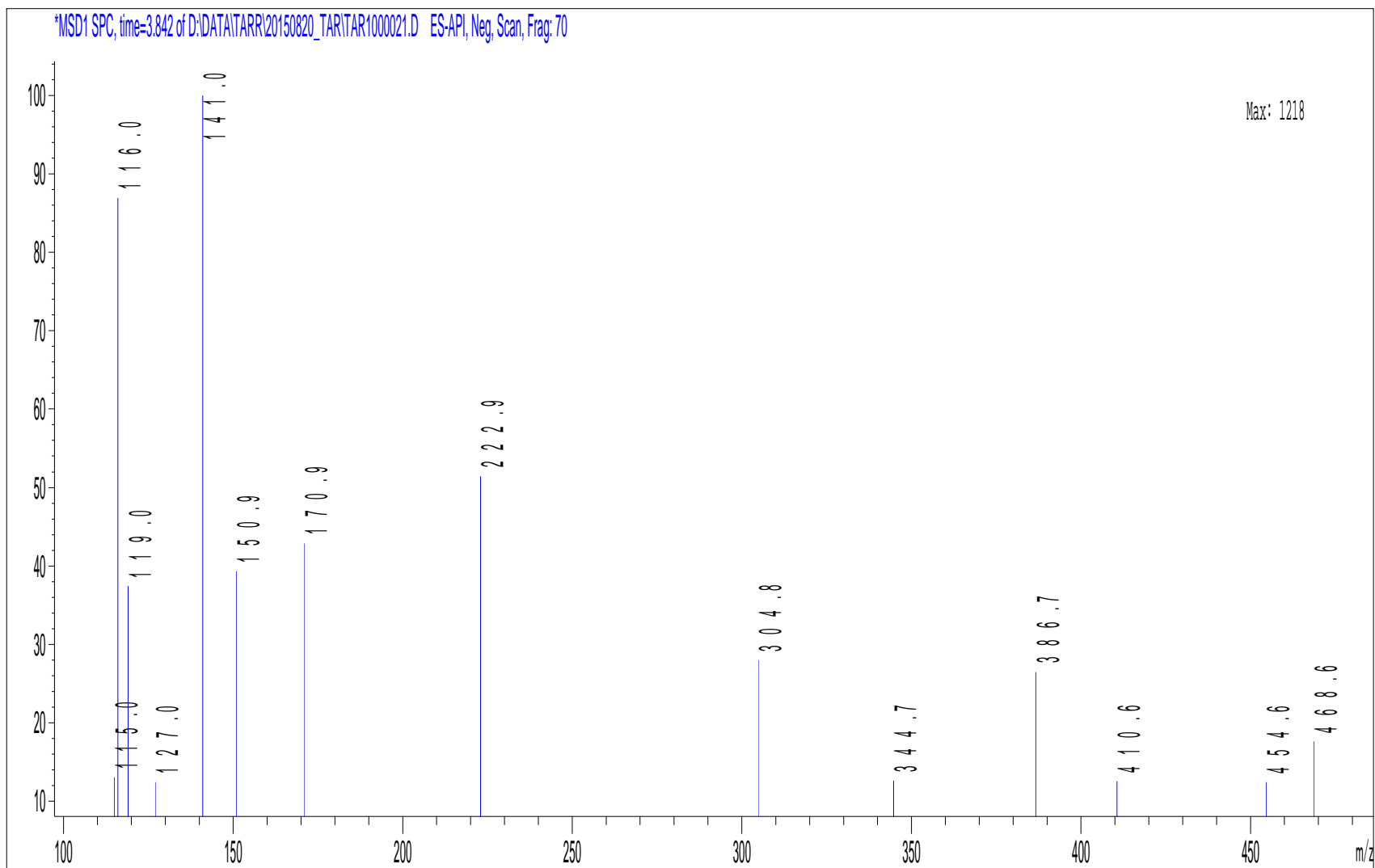


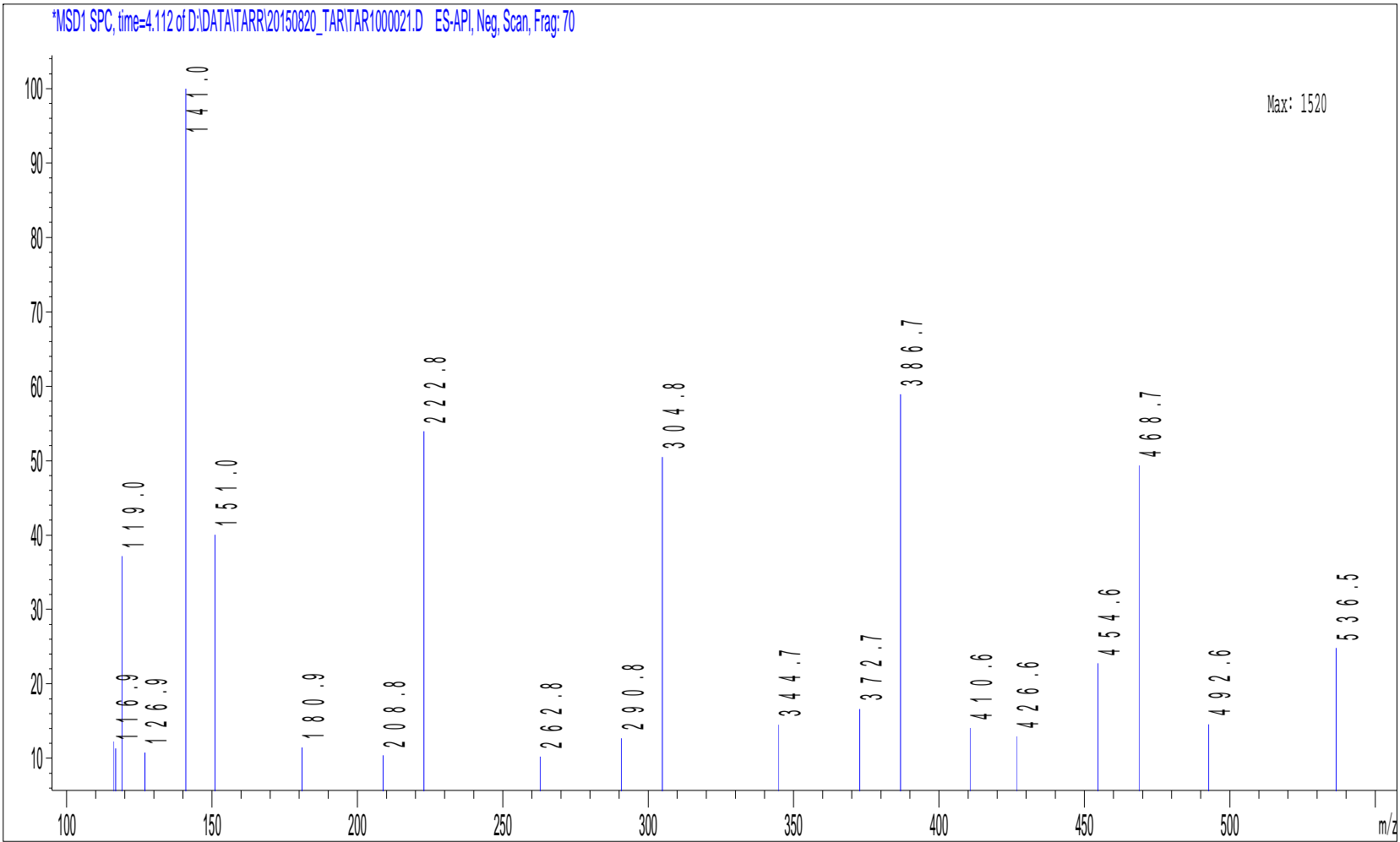


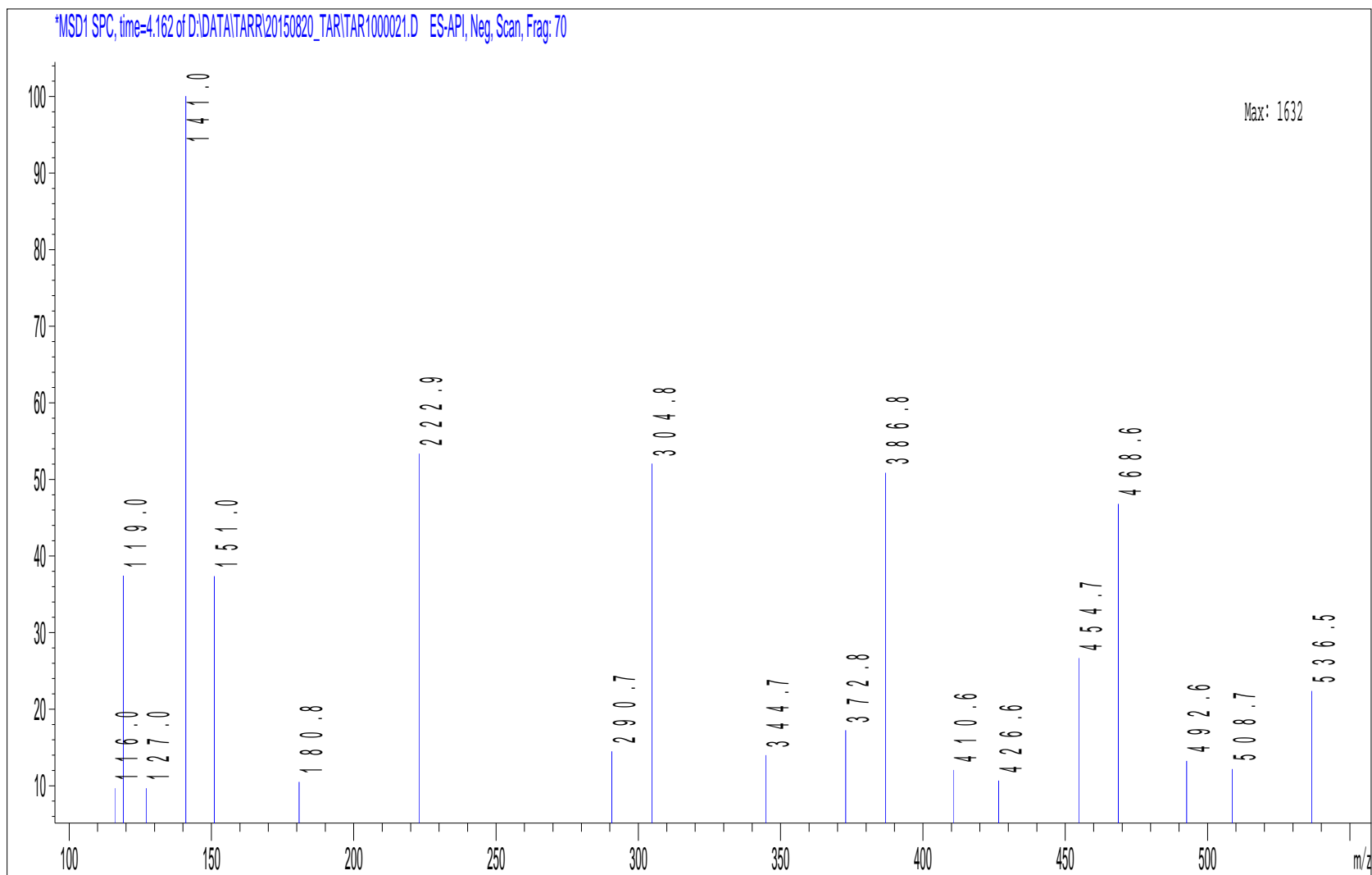
\*MSD1 SPC, time=3.033 of D:\DATA\TARR\20150820\_TARITAR1000021.D ES-API, Neg, Scan, Frag: 70





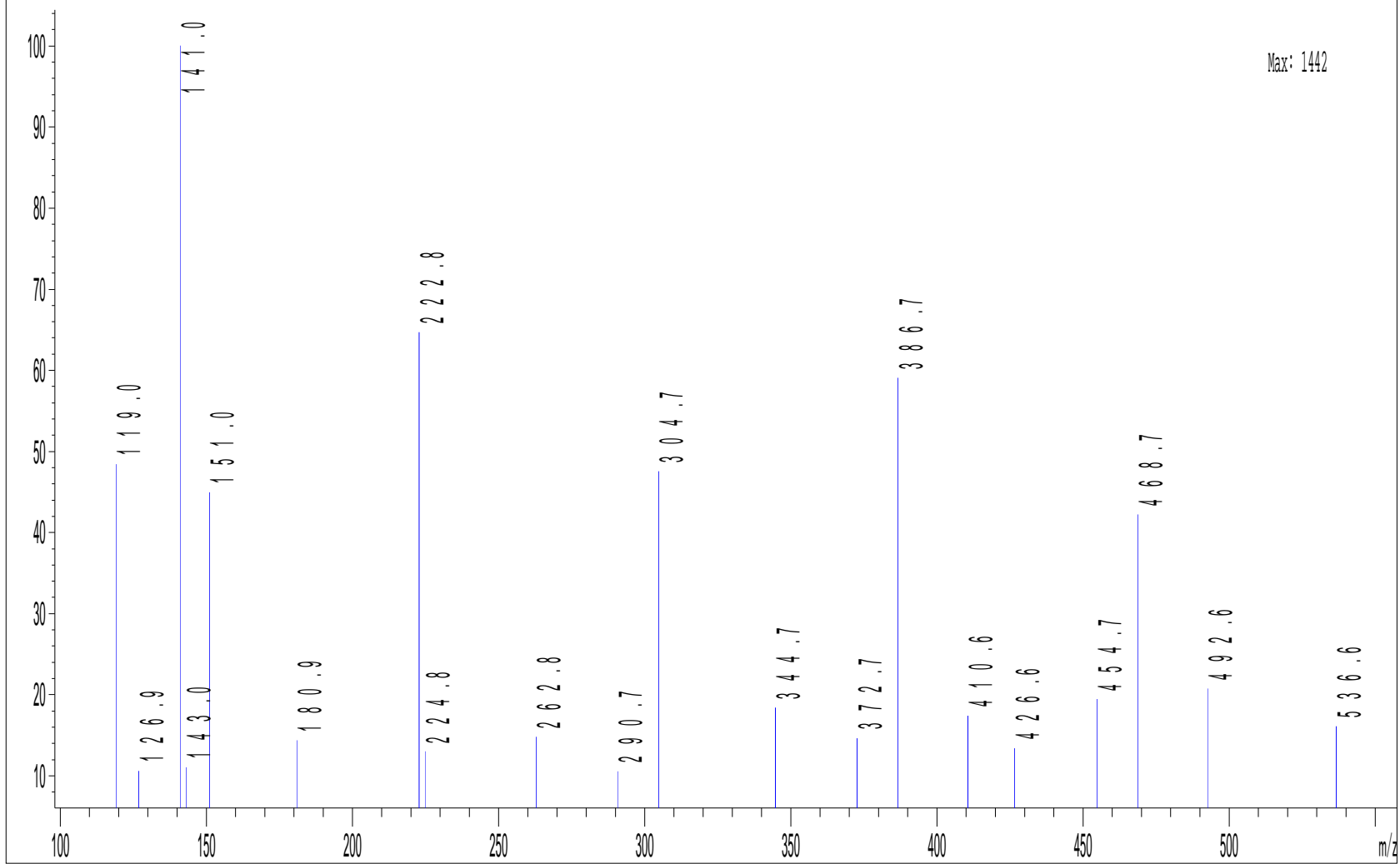






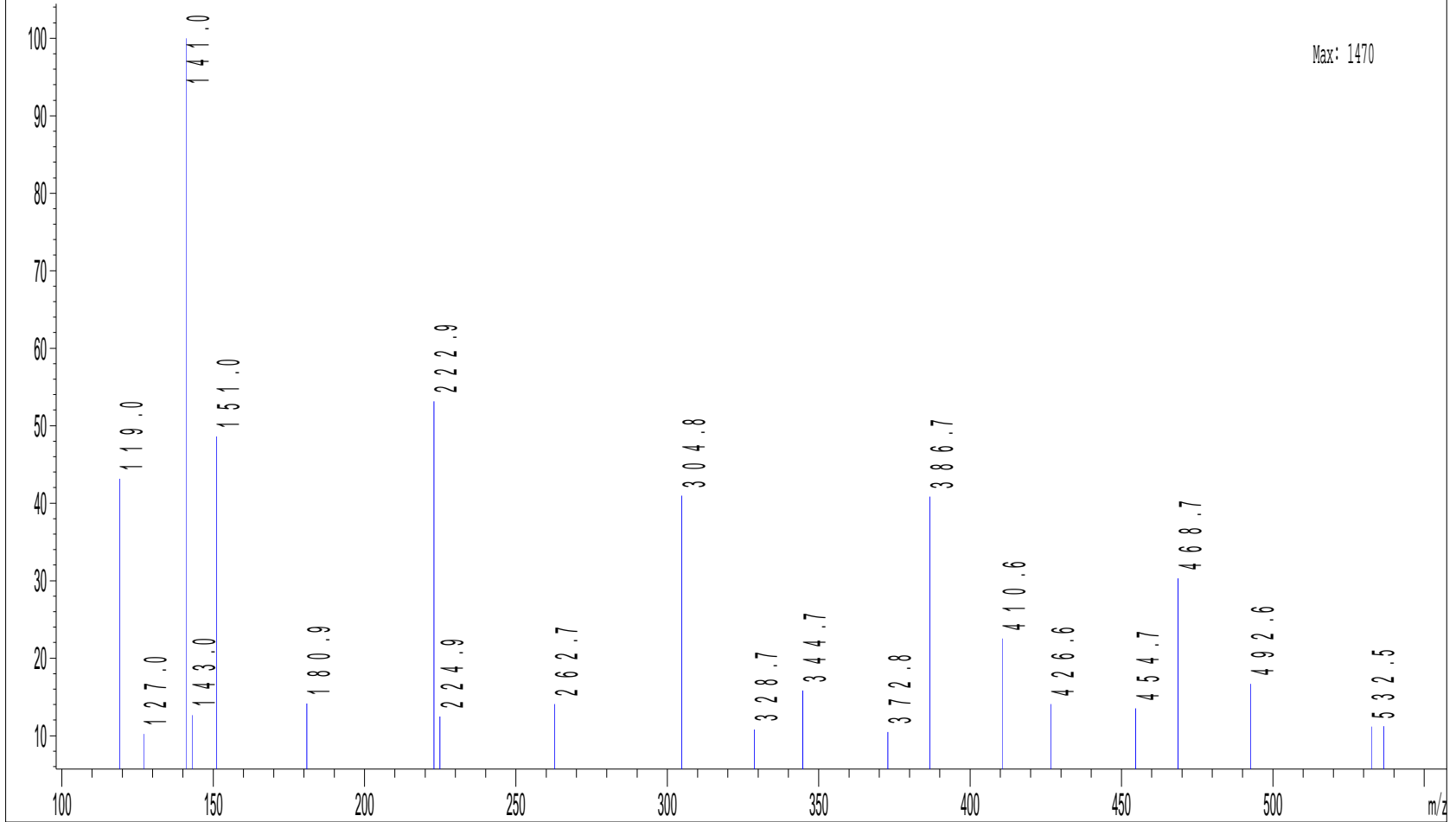


\*MSD1 SPC, time=4.415 of D:\DATA\TARR\20150820\_TARITAR1000021.D ES-API, Neg, Scan, Frag: 70



Max: 1442

\*MSD1 SPC, time=4.668 of D:\DATA\TARR\20150820\_TARITAR1000021.D ES-API, Neg. Scan, Frag: 70



## Appendix L: Chromatographic Contrast Angle Summaries

Positive		
0% DC	Theta (Deg) Whole	Theta (Deg) 2.5-4.5
pH6 Comp w pH8	3.375918422	6.723188691
pH6 Comp w pH9	3.42610567	7.907831248
pH8 Comp w pH9	5.245054624	11.18602854
pH6 Comp w pH7	11.48356239	24.03847461
pH7 Comp w pH8	11.06561411	24.66379254
pH7 Comp w pH9	12.22613449	24.92113008
H <sub>2</sub> O <sub>2</sub> Ctrl	Theta (Deg)	Theta (Deg) 2.5-4.5
pH8 Comp w pH9	1.780189654	2.894453995
pH6 Comp w pH8	3.783486646	5.159573841
pH6 Comp w pH9	3.872725509	6.913180549
pH6 Comp w pH7	3.043401804	7.078502639
pH7 Comp w pH8	4.692746649	9.244153793
pH7 Comp w pH9	4.305227895	9.407799531

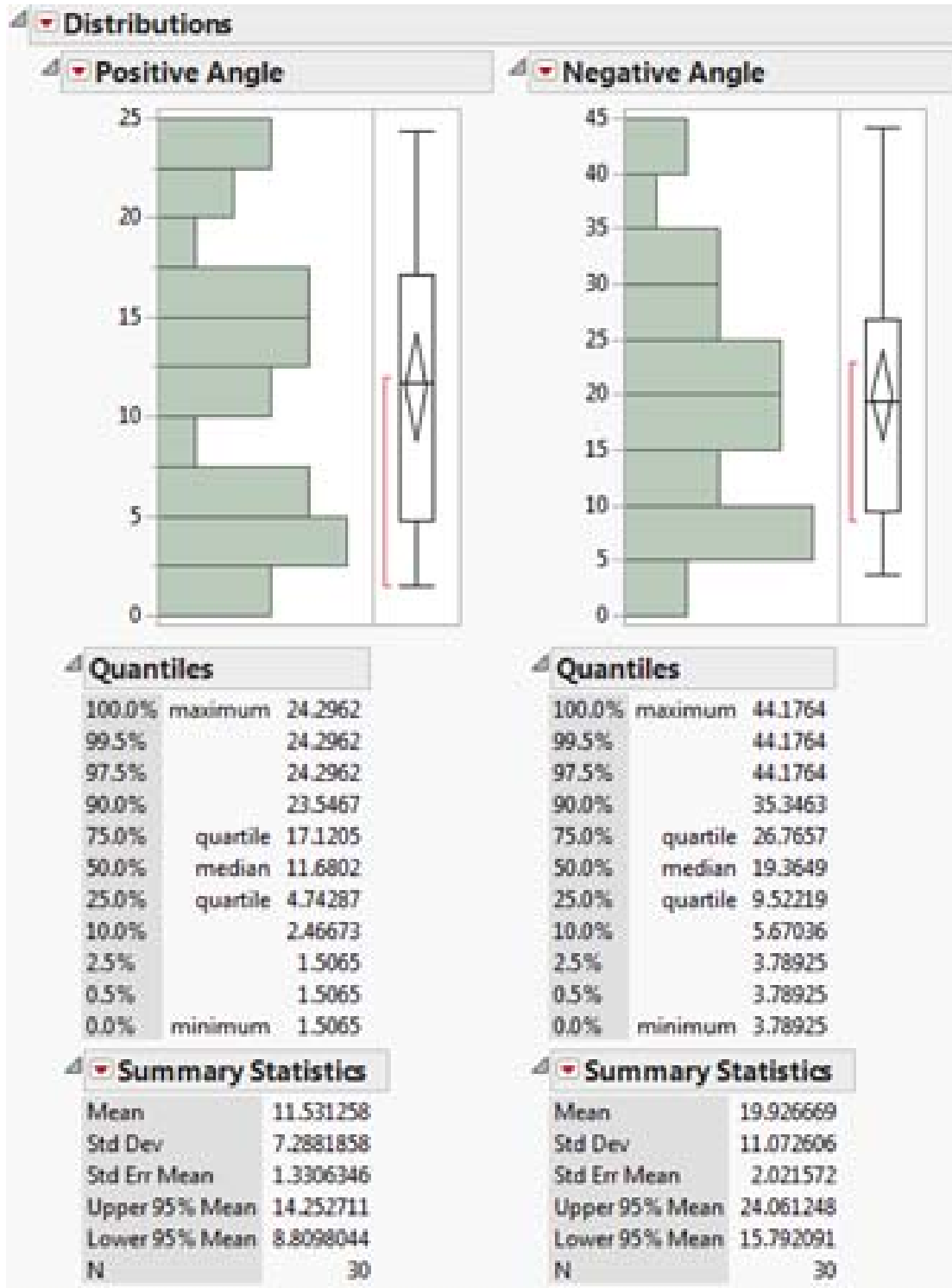
	Duty Cycle	pH 6	pH 7	pH 8	pH 9
0 DC Comp w H2O2 Ctrl	H2O2 Ctrl	19.84760124	30.06175819	23.32015516	21.96194288
0 DC Comp w 5 DC	5	1.506501447	23.96279159	3.056264052	16.44890953
0 DC Comp w 10 DC	10	5.639061308	14.57841327	2.701092136	11.41825989
0 DC Comp w 20 DC	20	2.44069513	21.24374485	6.73941897	11.94213319
0 DC Comp w 30 DC	30	7.508182612	24.2961799	4.97775981	17.87267424
0 DC Comp w 50 DC	50	4.038199613	10.85555459	12.55758574	17.37739471
0 DC Comp w 70 DC	70	14.23321809	23.80256933	3.379406247	15.41170405
0 DC Comp w 100 DC	100	1.506501447	21.23052869	6.852131469	17.03485288
0 DC Comp w 70 DC (2)	Repeat 70	14.23321809			
0 DC Comp w 100 DC (2)	Repeat 100			7.09280342	

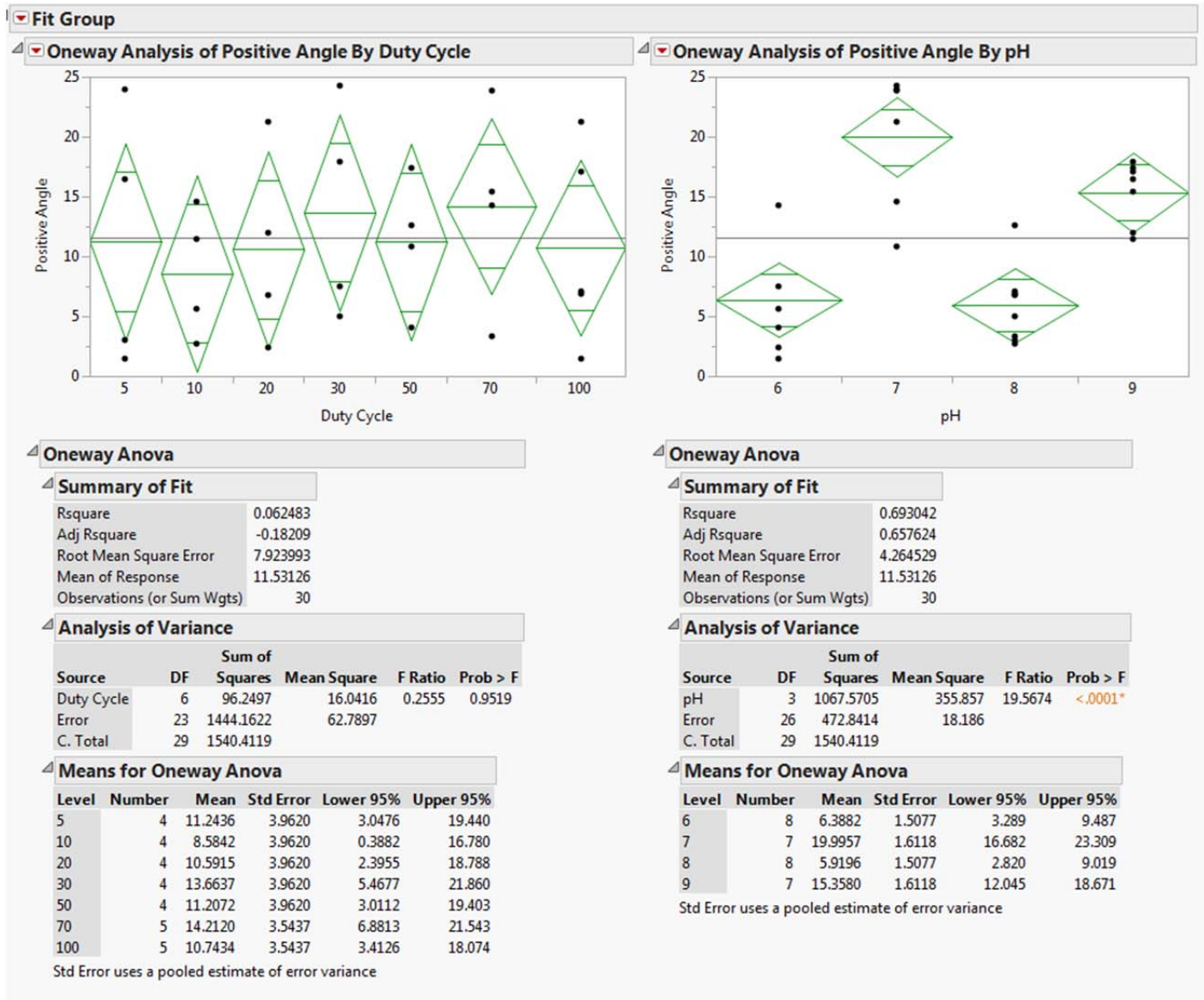
Negative

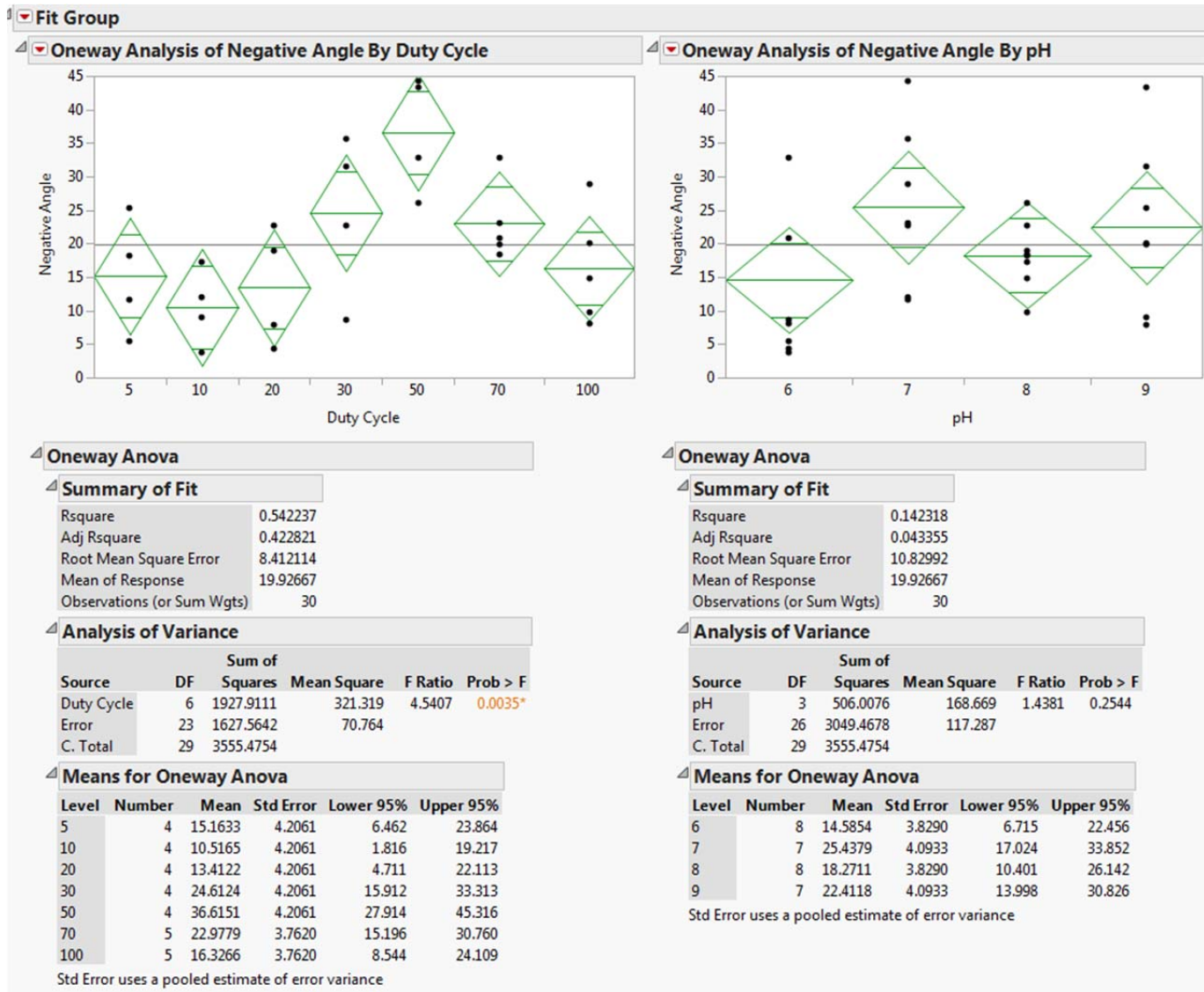
0% DC	Theta (Deg) 2.5-4.5
pH7 Comp w pH9	16.57104377
pH6 Comp w pH9	16.72608901
pH6 Comp w pH8	20.61519241
pH6 Comp w pH7	23.09971409
pH8 Comp w pH9	30.19031693
pH7 Comp w pH8	37.8272853
H <sub>2</sub> O <sub>2</sub> Ctrl	Theta (Deg) 2.5-4.5
pH6 Comp w pH7	3.574156638
pH8 Comp w pH9	6.27061759
pH6 Comp w pH8	12.11077217
pH7 Comp w pH8	12.49426866
pH6 Comp w pH9	17.47102257
pH7 Comp w pH9	17.9140816

	Duty Cycle	pH 6	pH 7	pH 8	pH 9
0 DC Comp w H2O2 Ctrl	H <sub>2</sub> O <sub>2</sub> Ctrl	4.287375869	25.39208308	29.21614692	13.98393889
0 DC Comp w 5 DC	5	5.435667548	11.60653237	18.27342076	25.3374457
0 DC Comp w 10 DC	10	3.789254145	12.06138548	17.3084023	8.906979859
0 DC Comp w 20 DC	20	4.236908762	22.6824843	18.94669199	7.782610468
0 DC Comp w 30 DC	30	8.60704675	35.62249185	22.66396489	31.55611185
0 DC Comp w 50 DC	50	32.84861223	44.17639494	26.04684018	43.38847849
0 DC Comp w 70 DC	70	20.80601967	22.9937655	18.44558516	19.78317349
0 DC Comp w 100 DC	100	8.098637143	28.92238094	14.75679853	20.12767796
0 DC Comp w 70 DC (2)	Repeat 70	32.86106106			
0 DC Comp w 100 DC (2)	Repeat 100			9.727257579	

## Appendix M: CCA Summary Statistics, ANOVA, and Tukey Analyses







## Positive Ionization CCA Tukey Analysis

### Response Y1 Positive Angle

#### Whole Model

#### Effect Summary

Source	LogWorth	PValue
X2 pH	4.423	0.00004
X1 Duty Cycle*X2 pH	3.124	0.00075
X1 Duty Cycle	3.014	0.00097 <sup>^</sup>

#### Summary of Fit

RSquare	0.999981
RSquare Adj	0.999727
Root Mean Square Error	0.120336
Mean of Response	11.53126
Observations (or Sum Wgts)	30

#### Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	27	1540.3830	57.0512	3939.798
Error	2	0.0290	0.0145	Prob > F
C. Total	29	1540.4119		0.0003*

#### Effect Tests

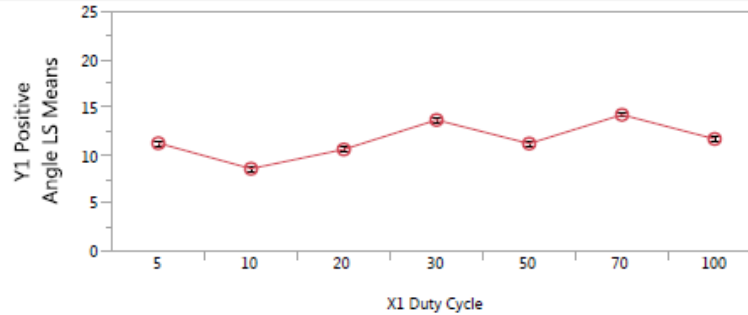
Source	Nparm	DF	Sum of Squares	F Ratio	Prob > F
X1 Duty Cycle	6	6	89.6315	1031.617	0.0010*
X2 pH	3	3	1149.3616	26457.23	<.0001*
X1 Duty Cycle*X2 pH	18	18	346.3756	1328.874	0.0008*

### X1 Duty Cycle

#### Least Squares Means Table

Level	Least Sq Mean	Std Error	Mean
5	11.243617	0.06016799	11.2436
10	8.584207	0.06016799	8.5842
20	10.591497	0.06016799	10.5915
30	13.663698	0.06016799	13.6637
50	11.207182	0.06016799	11.2072
70	14.206723	0.05628200	14.2120
100	11.686087	0.05628200	10.7434

#### LS Means Plot



#### LSMeans Differences Tukey HSD

$\alpha = 0.050$   $Q = 8.79249$



**Response Y1 Positive Angle**

**X1 Duty Cycle**

**LSMeans Differences Tukey HSD**

		LSMean[j]						
Mean[i]-Mean[j]	5	10	20	30	50	70	100	
Std Err Dif								
Lower CL Dif								
Upper CL Dif								
LSMean[i]	5	0	2.65941	0.65212	-2.4201	0.03643	-2.9631	-0.4425
		0	0.08509	0.08509	0.08509	0.08509	0.08239	0.08239
		0	1.91125	-0.096	-3.1682	-0.7117	-3.6875	-1.1669
		0	3.40757	1.40028	-1.6719	0.78459	-2.2387	0.28193
	10	-2.6594	0	-2.0073	-5.0795	-2.623	-5.6225	-3.1019
		0.08509	0	0.08509	0.08509	0.08509	0.08239	0.08239
		-3.4076	0	-2.7554	-5.8276	-3.3711	-6.3469	-3.8263
		-1.9113	0	-1.2591	-4.3313	-1.8748	-4.8981	-2.3775
	20	-0.6521	2.00729	0	-3.0722	-0.6157	-3.6152	-1.0946
		0.08509	0.08509	0	0.08509	0.08509	0.08239	0.08239
		-1.4003	1.25913	0	-3.8204	-1.3638	-4.3396	-1.819
		0.09604	2.75545	0	-2.324	0.13247	-2.8908	-0.3702
30	2.42008	5.07949	3.0722	0	2.45652	-0.543	1.97761	
	0.08509	0.08509	0.08509	0	0.08509	0.08239	0.08239	
	1.67192	4.33134	2.32404	0	1.70836	-1.2674	1.25321	
	3.16824	5.82765	3.82036	0	3.20467	0.18137	2.70201	
50	-0.0364	2.62298	0.61569	-2.4565	0	-2.9995	-0.4789	
	0.08509	0.08509	0.08509	0.08509	0	0.08239	0.08239	
	-0.7846	1.87482	-0.1325	-3.2047	0	-3.7239	-1.2033	
	0.71172	3.37113	1.36384	-1.7084	0	-2.2751	0.24549	
70	2.96311	5.62252	3.61523	0.54303	2.99954	0	2.52064	
	0.08239	0.08239	0.08239	0.08239	0.08239	0	0.07959	
	2.23871	4.89812	2.89083	-0.1814	2.27514	0	1.8208	
	3.68751	6.34692	4.33963	1.26742	3.72394	0	3.22047	
100	0.44247	3.10188	1.09459	-1.9776	0.4789	-2.5206	0	
	0.08239	0.08239	0.08239	0.08239	0.08239	0.07959	0	
	-0.2819	2.37748	0.37019	-2.702	-0.2455	-3.2205	0	
	1.16687	3.82628	1.81899	-1.2532	1.2033	-1.8208	0	

Level		Least Sq Mean
70	A	14.206723
30	A	13.663698
100	B	11.686087
5	B C	11.243617
50	B C	11.207182
20	C	10.591497
10	D	8.584207

Levels not connected by same letter are significantly different.

**X2 pH**

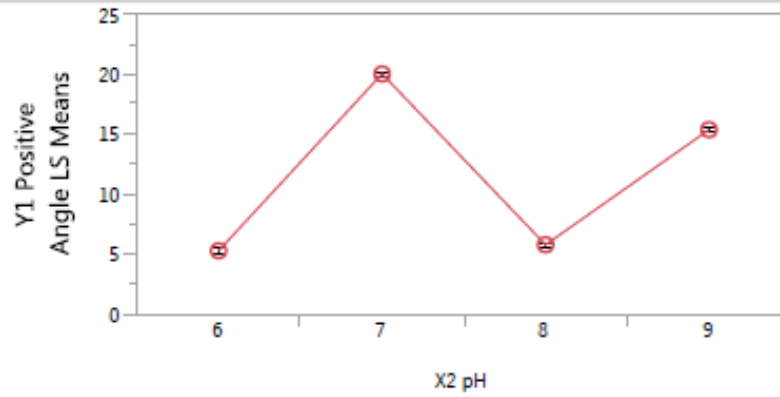
**Least Squares Means Table**

Level	Least Sq Mean	Std Error	Mean
6	5.267480	0.04382825	6.3882
7	19.995683	0.04548272	19.9957
8	5.769142	0.04382825	5.9196
9	15.357987	0.04548272	15.3580

**Response Y1 Positive Angle**

**X2 pH**

**LS Means Plot**



**LSMeans Differences Tukey HSD**

$\alpha = 0.050$   $Q = 6.92823$

		LSMean[j]			
Mean[i]-Mean[j]		6	7	8	9
Std Err Dif					
Lower CL Dif					
Upper CL Dif					
6		0	-14.728	-0.5017	-10.091
		0	0.06316	0.06198	0.06316
		0	-15.166	-0.9311	-10.528
		0	-14.291	-0.0722	-9.6529
7		14.7282	0	14.2265	4.6377
		0.06316	0	0.06316	0.06432
		14.2906	0	13.7889	4.19206
		15.1658	0	14.6642	5.08334
8		0.50166	-14.227	0	-9.5888
		0.06198	0.06316	0	0.06316
		0.07223	-14.664	0	-10.026
		0.93109	-13.789	0	-9.1512
9		10.0905	-4.6377	9.58885	0
		0.06316	0.06432	0.06316	0
		9.6529	-5.0833	9.15124	0
		10.5281	-4.1921	10.0265	0

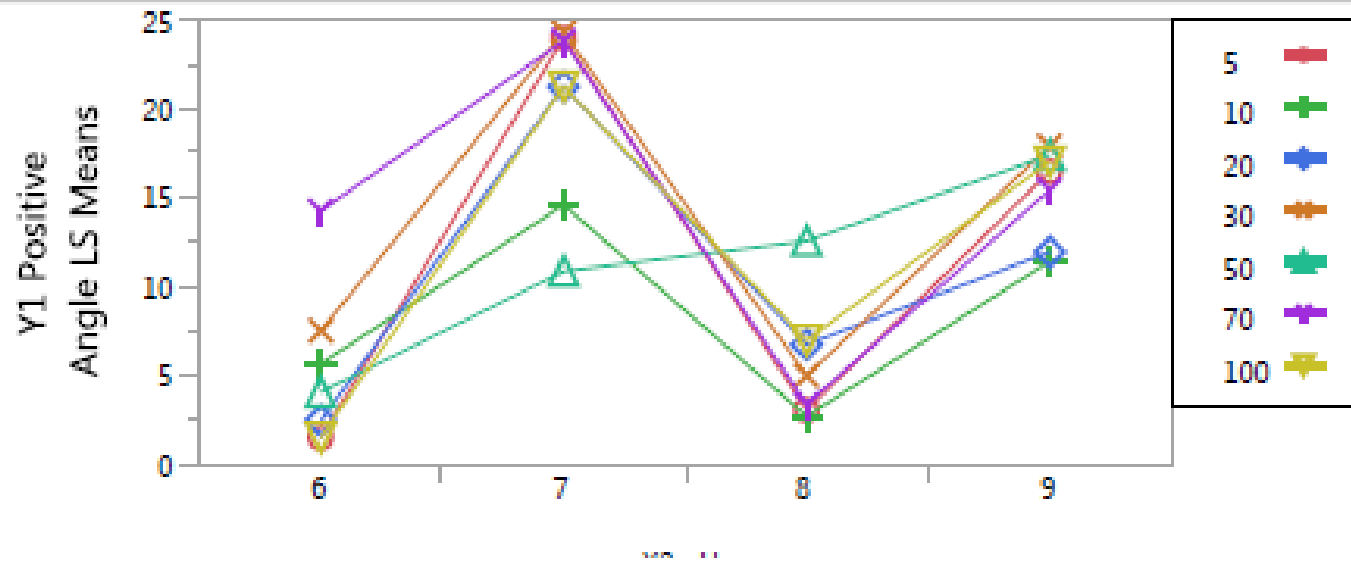
Level		Least Sq Mean
7	A	19.995683
9	B	15.357987
8	C	5.769142
6	D	5.267480

Levels not connected by same letter are significantly different.

Response Y1 Positive Angle

X1 Duty Cycle\*X2 pH

LS Means Plot



## Negative Ionization CCA Tukey Analysis

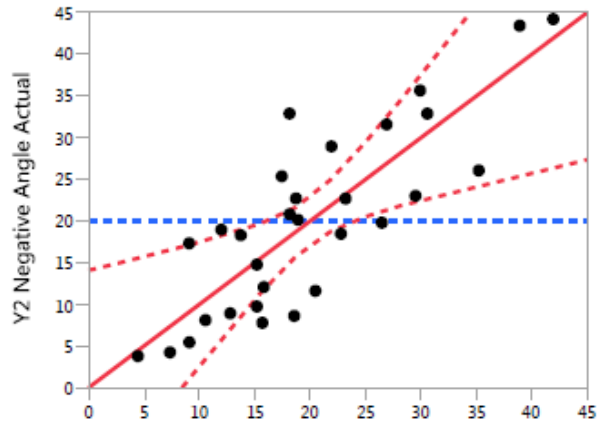
### Response Y2 Negative Angle

#### Whole Model

#### Effect Summary

Source	LogWorth	PValue
X1 Duty Cycle	2.980	0.00105
X2 pH	1.368	0.04282

#### Actual by Predicted Plot



Y2 Negative Angle Predicted P=0.0013 RSq=0.69 RMSE=7.391

#### Summary of Fit

RSquare	0.692715
RSquare Adj	0.554436
Root Mean Square Error	7.391025
Mean of Response	19.92667
Observations (or Sum Wgts)	30

#### Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	9	2462.9304	273.659	5.0096
Error	20	1092.5449	54.627	Prob > F
C. Total	29	3555.4754		0.0013*

#### Lack Of Fit

Source	DF	Sum of Squares	Mean Square	F Ratio
Lack Of Fit	18	1007.2348	55.9575	1.3119
Pure Error	2	85.3102	42.6551	Prob > F
Total Error	20	1092.5449		0.5189
			Max RSq	0.9760

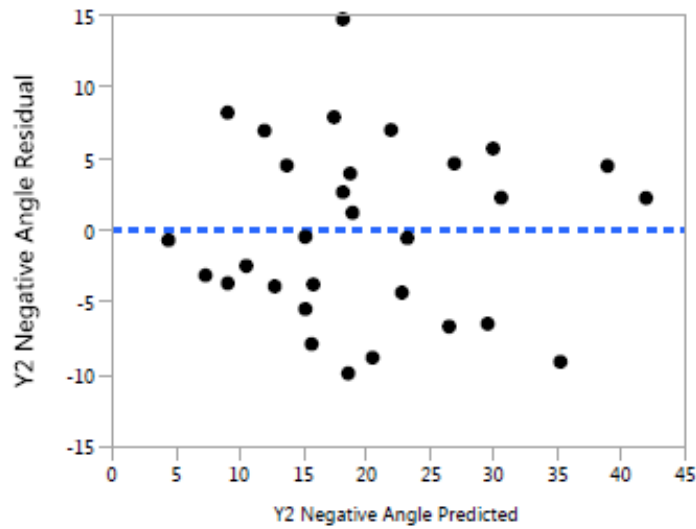
#### Effect Tests

Source	Nparm	DF	Sum of Squares	F Ratio	Prob > F
X1 Duty Cycle	6	6	1956.9228	5.9705	0.0010*
X2 pH	3	3	535.0193	3.2647	0.0428*

Response Y2 Negative Angle

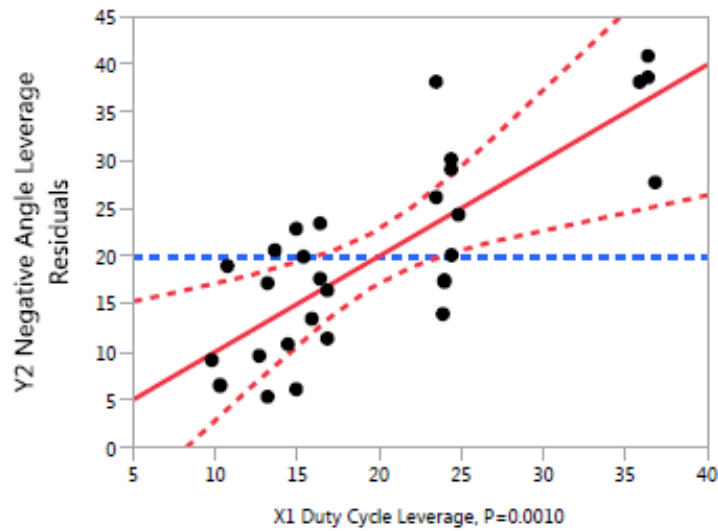
Whole Model

Residual by Predicted Plot



X1 Duty Cycle

Leverage Plot



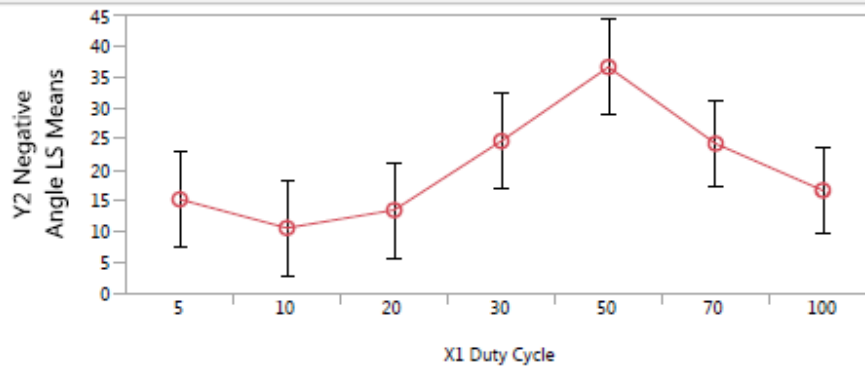
Least Squares Means Table

Level	Least Sq Mean	Std Error	Mean
5	15.163268	3.6955124	15.1633
10	10.516505	3.6955124	10.5165
20	13.412174	3.6955124	13.4122
30	24.612403	3.6955124	24.6124
50	36.615082	3.6955124	36.6151
70	24.193921	3.3375650	22.9779
100	16.615959	3.3375650	16.3266

Response Y2 Negative Angle

X1 Duty Cycle

LS Means Plot



LSMeans Differences Tukey HSD

$\alpha = 0.050$   $Q = 3.26677$

		LSMean[j]						
Mean[i]-Mean[j]		5	10	20	30	50	70	100
Std Err Dif								
Lower CL Dif								
Upper CL Dif								
LSMean[i]	5	0	4.64676	1.75109	-9.4491	-21.452	-9.0307	-1.4527
		0	5.22624	5.22624	5.22624	5.22624	4.97957	4.97957
		0	-12.426	-15.322	-26.522	-38.525	-25.298	-17.72
		0	21.7197	18.824	7.6238	-4.3789	7.23647	14.8144
	10	-4.6468	0	-2.8957	-14.096	-26.099	-13.677	-6.0995
		5.22624	0	5.22624	5.22624	5.22624	4.97957	4.97957
		-21.72	0	-19.969	-31.169	-43.172	-29.945	-22.367
	12.4262	0	14.1773	2.97704	-9.0256	2.5897	10.1677	
	20	-1.7511	2.89567	0	-11.2	-23.203	-10.782	-3.2038
	5.22624	5.22624	0	5.22624	5.22624	4.97957	4.97957	
	-18.824	-14.177	0	-28.273	-40.276	-27.049	-19.471	
	15.3218	19.9686	0	5.8727	-6.13	5.48537	13.0633	
	30	9.44914	14.0959	11.2002	0	-12.003	0.41848	7.99644
	5.22624	5.22624	5.22624	0	5.22624	4.97957	4.97957	
	-7.6238	-2.977	-5.8727	0	-29.076	-15.849	-8.2707	
	26.5221	31.1688	28.2732	0	5.07026	16.6856	24.2636	
	50	21.4518	26.0986	23.2029	12.0027	0	12.4212	19.9991
	5.22624	5.22624	5.22624	5.22624	0	4.97957	4.97957	
	4.37888	9.02564	6.12997	-5.0703	0	-3.846	3.732	
	38.5247	43.1715	40.2758	29.0756	0	28.6883	36.2662	
	70	9.03065	13.6774	10.7817	-0.4185	-12.421	0	7.57796
	4.97957	4.97957	4.97957	4.97957	4.97957	0	4.73404	
	-7.2365	-2.5897	-5.4854	-16.686	-28.688	0	-7.8871	
	25.2978	29.9445	27.0489	15.8486	3.84596	0	23.043	
	100	1.45269	6.09945	3.20378	-7.9964	-19.999	-7.578	0
	4.97957	4.97957	4.97957	4.97957	4.97957	4.73404	0	
	-14.814	-10.168	-13.063	-24.264	-36.266	-23.043	0	
	17.7198	22.3666	19.4709	8.27067	-3.732	7.88707	0	

**Response Y2 Negative Angle**

**X1 Duty Cycle**

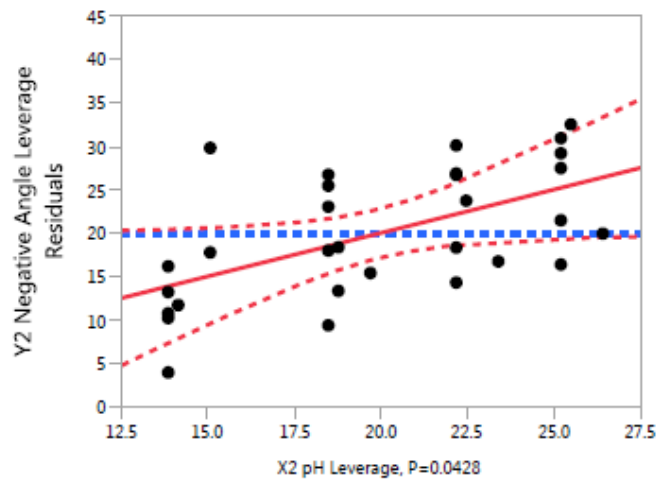
**LSMeans Differences Tukey HSD**

Level		Least Sq Mean
50	A	36.615082
30	A B	24.612403
70	A B	24.193921
100	B	16.615959
5	B	15.163268
20	B	13.412174
10	B	10.516505

Levels not connected by same letter are significantly different.

**X2 pH**

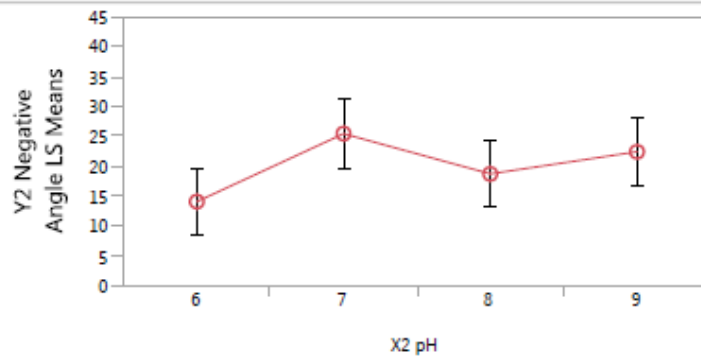
**Leverage Plot**



**Least Squares Means Table**

Level	Least Sq Mean	Std Error	Mean
6	14.081327	2.6423211	14.5854
7	25.437919	2.7935448	25.4379
8	18.714292	2.6423211	18.2711
9	22.411783	2.7935448	22.4118

**LS Means Plot**



**LSMeans Differences Tukey HSD**

$\alpha = 0.050$   $Q = 2.79894$

**Response Y2 Negative Angle**

**X2 pH**

**LSMeans Differences Tukey HSD**

		LSMean[j]			
Mean[i]-Mean[j]		6	7	8	9
Std Err Dif					
Lower CL Dif					
Upper CL Dif					
LSMean[i]	6	0	-11.357	-4.633	-8.3305
		0	3.84522	3.74259	3.84522
		0	-22.119	-15.108	-19.093
		0	-0.5941	5.84231	2.43209
	7	11.3566	0	6.72363	3.02614
		3.84522	0	3.84522	3.95067
		0.59405	0	-4.0389	-8.0315
		22.1191	0	17.4862	14.0838
	8	4.63296	-6.7236	0	-3.6975
		3.74259	3.84522	0	3.84522
		-5.8423	-17.486	0	-14.46
		15.1082	4.03891	0	7.06505
9	8.33046	-3.0261	3.69749	0	
	3.84522	3.95067	3.84522	0	
	-2.4321	-14.084	-7.0651	0	
	19.093	8.03154	14.46	0	

Level		Least Sq Mean
7	A	25.437919
9	A B	22.411783
8	A B	18.714292
6	B	14.081327

Levels not connected by same letter are significantly different.



## Appendix N: Positive Ionization Chromatographic Contrast Angle Regression Report

Upholds SW, DW, BP

Y1: Positive Angle

X1: DV pH6

X2: DV pH7

X3: DV pH8

X4: DV DC 70

X5: DV DC 70\*DV pH6

R Squared: .8000

R Squared, Adj: .7584

	percent	degrees		
Max Error	150.50%	9.07°	between 0 and 9 degrees	4.533645
Mean Error	38.30%	2.51°	Error: ±4.53°	
Median Error	17.50%	2.18°		

stdev    2.02 degrees

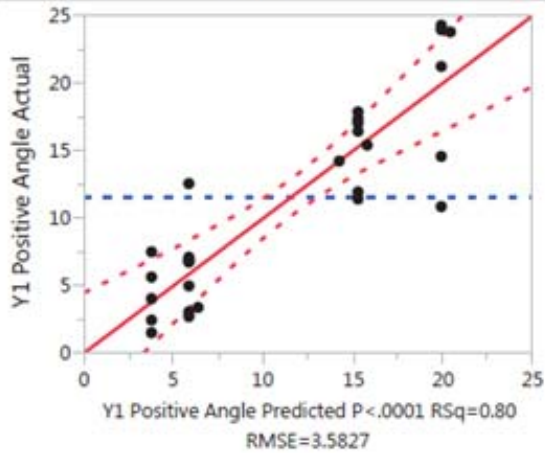
All VIF Scores below 2.0

Durbin Watson assumption of Independence upheld

**Response Y1 Positive Angle**

**Whole Model**

**Actual by Predicted Plot**



**Summary of Fit**

RSquare	0.800021
RSquare Adj	0.758359
Root Mean Square Error	3.582654
Mean of Response	11.53126
Observations (or Sum Wgts)	30

**Analysis of Variance**

Source	DF	Sum of Squares	Mean Square	F Ratio	Prob > F
Model	5	1232.3621	246.472	19.2025	
Error	24	308.0498	12.835		
C. Total	29	1540.4119			<.0001*

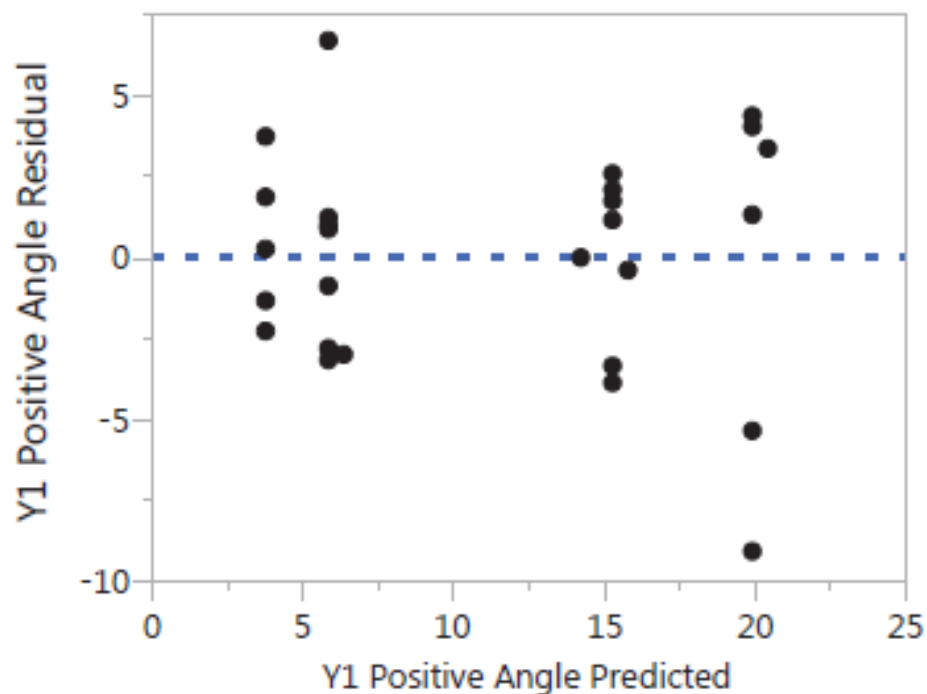
**Parameter Estimates**

Term	Estimate	Std Error	t Ratio	Prob >  t	Std Beta	VIF
Intercept	14.84291	1.377876	10.77	<.0001*	0	.
Dmy Var: pH6	-9.853601	1.870906	-5.27	<.0001*	-0.6081	1.5998735
Dmy Var: pH8	-9.429323	1.854626	-5.08	<.0001*	-0.58191	1.5721511
Dmy Var: DC 70	3.1633158	1.809509	1.75	0.0932	0.16452	1.0629204
Dmy Var: pH7	4.637696	1.915009	2.42	0.0234*	0.273739	1.5333333
(Dmy Var: DC 70 - 0.16667) * (Dmy Var: pH6 - 0.26667)	9.9500619	3.676148	2.71	0.0123*	0.254454	1.0606726

## Response Y1 Positive Angle

### Whole Model

### Residual by Predicted Plot

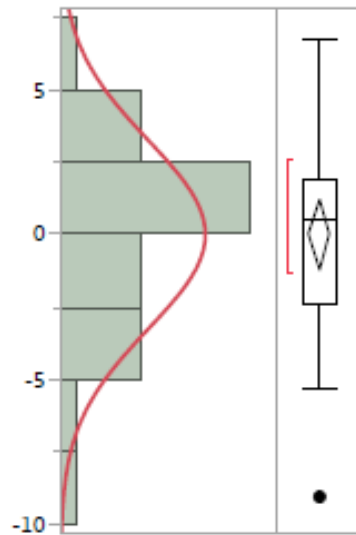


### Durbin-Watson

Durbin-Watson	Number of Obs.	AutoCorrelation	Prob < DW
2.7606244	30	-0.3936	0.9580

## Distributions

### Residual Y1 Positive Angle



Normal(4.1e-16,3.2592)

#### Quantiles

100.0%	maximum	6.70177
99.5%		6.70177
97.5%		6.70177
90.0%		4.00946
75.0%	quartile	1.92247
50.0%	median	0.57431
25.0%	quartile	-2.3999
10.0%		-3.8145
2.5%		-9.0673
0.5%		-9.0673
0.0%	minimum	-9.0673

#### Summary Statistics

Mean	4.145e-16
Std Dev	3.2592033
Std Err Mean	0.5950464
Upper 95% Mean	1.2170065
Lower 95% Mean	-1.217007
N	30

#### Fitted Normal

##### Parameter Estimates

Type	Parameter	Estimate	Lower 95%	Upper 95%
Location	$\mu$	4.145e-16	-1.217007	1.2170065
Dispersion	$\sigma$	3.2592033	2.5956521	4.3813965

-2log(Likelihood) = 155.02527928085

#### Goodness-of-Fit Test

Shapiro-Wilk W Test

## Distributions

### Residual Y1 Positive Angle

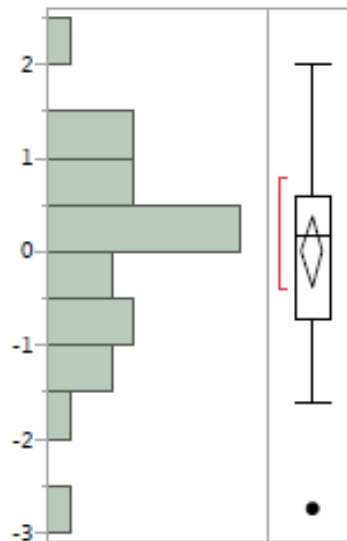
#### Fitted Normal

#### Goodness-of-Fit Test

W	Prob<W
0.973861	0.6492

Note: Ho = The data is from the Normal distribution. Small p-values reject Ho.

### Studentized Resid Y1 Positive Angle



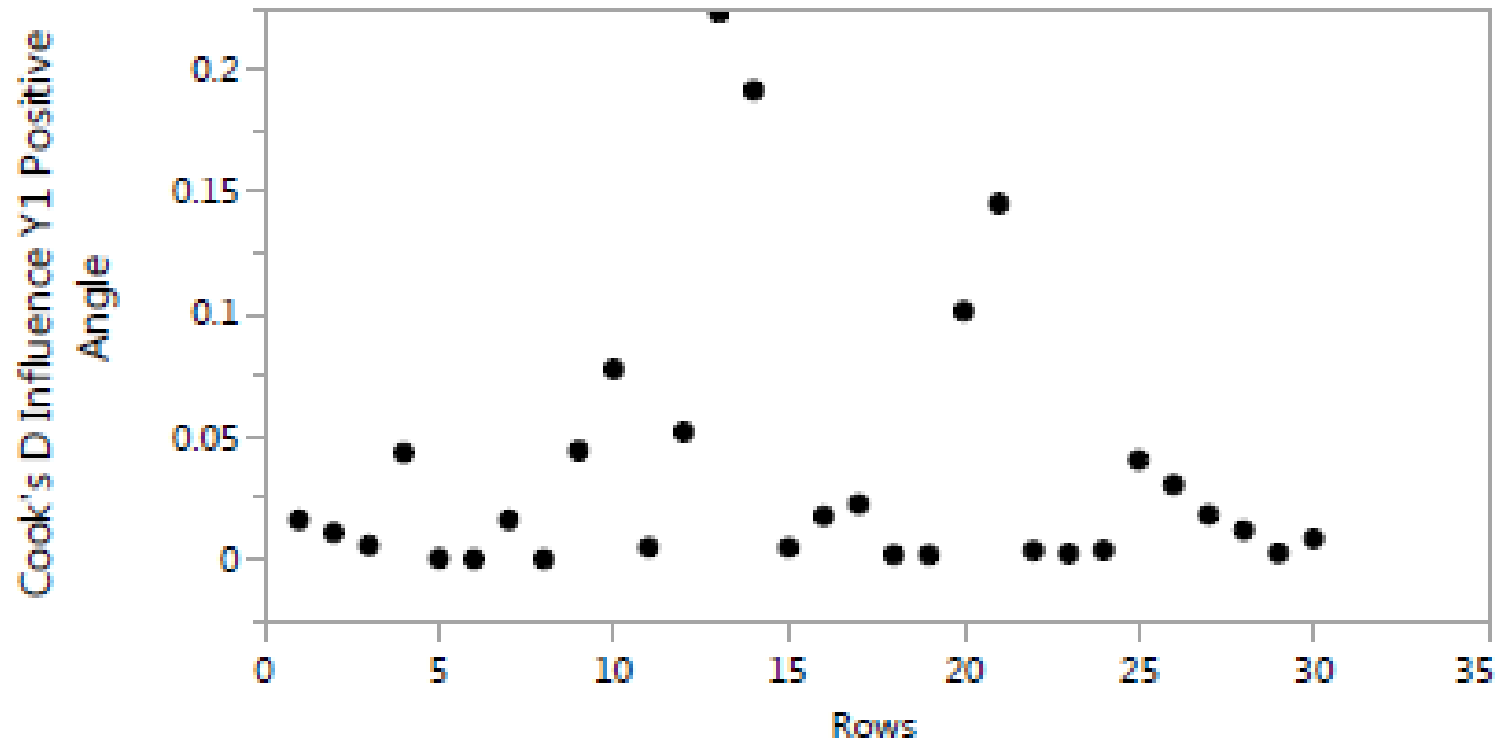
#### Quantiles

100.0%	maximum	2.00671
99.5%		2.00671
97.5%		2.00671
90.0%		1.24028
75.0%	quartile	0.58631
50.0%	median	0.1728
25.0%	quartile	-0.7294
10.0%		-1.1636
2.5%		-2.7463
0.5%		-2.7463
0.0%	minimum	-2.7463

#### Summary Statistics

Mean	-0.000156
Std Dev	1.0010628
Std Err Mean	0.1827682
Upper 95% Mean	0.3736469
Lower 95% Mean	-0.373959
N	30

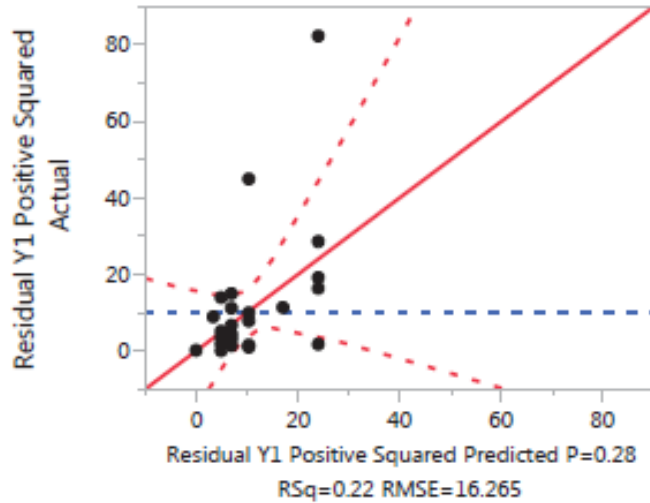
## Overlay Plot



## Response Residual Y1 Positive Squared

### Whole Model

#### Actual by Predicted Plot



#### Summary of Fit

RSquare	0.218743
RSquare Adj	0.055981
Root Mean Square Error	16.26544
Mean of Response	10.26833
Observations (or Sum Wgts)	30

#### Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	5	1777.7962	355.559	1.3439
Error	24	6349.5470	264.564	Prob > F
C. Total	29	8127.3432		0.2800

#### Parameter Estimates

Term	Estimate	Std Error	t Ratio	Prob> t
Intercept	6.8698404	6.25563	1.10	0.2830
Dmy Var: pH6	-1.696065	8.494012	-0.20	0.8434
Dmy Var: pH8	3.3715243	8.420099	0.40	0.6924
Dmy Var: DC 70	-6.415011	8.215268	-0.78	0.4425
Dmy Var: pH7	17.038839	8.694242	1.96	0.0617
(Dmy Var: DC 70-0.16667)*(Dmy Var: pH6-0.26667)	2.0311116	16.6899	0.12	0.9042

Breusch Pagan Test

Interact Two file in L Drive

N (sample size)  
dof (explained)  
Sum Sqrs Error (SSE)  
Sum Sqrs Regression (SSR)

User Defined
30
5
3.08E+02
1.78E+03

Test Statistic  
P-Value

Computer Calculates
8.443666723
0.133420116

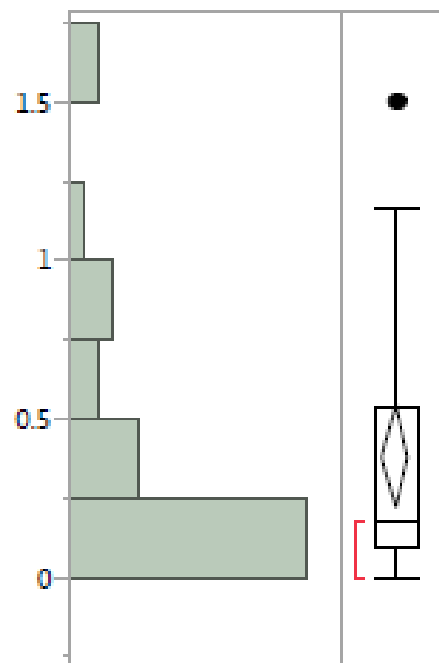
assumption constant variance  
compare w/alpha =0.05  
fail to reject upholds assumption of constant variance

Result - Computer Calculated
GOOD - Constant Variance



## Distributions

### APE Score Y1 (2)

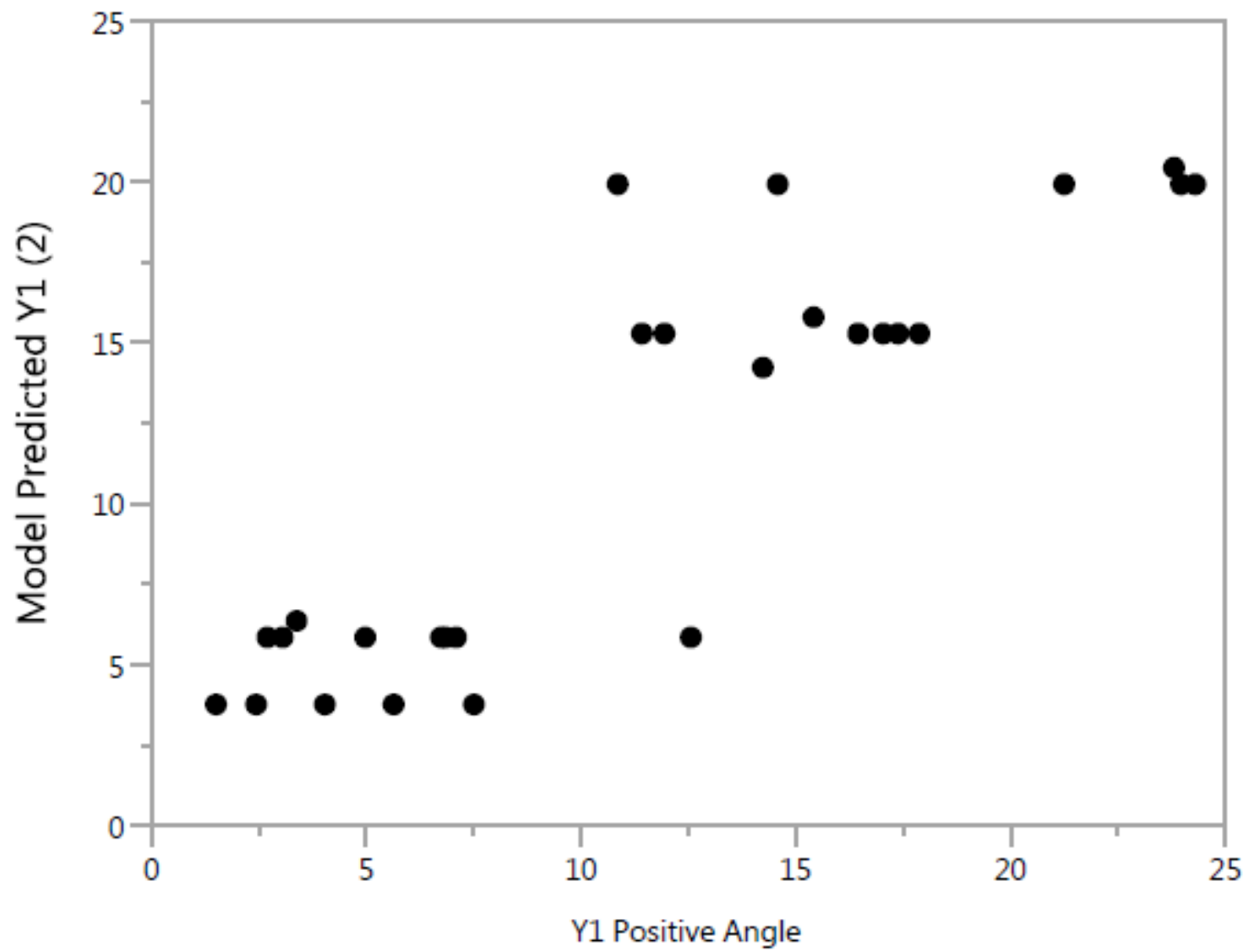


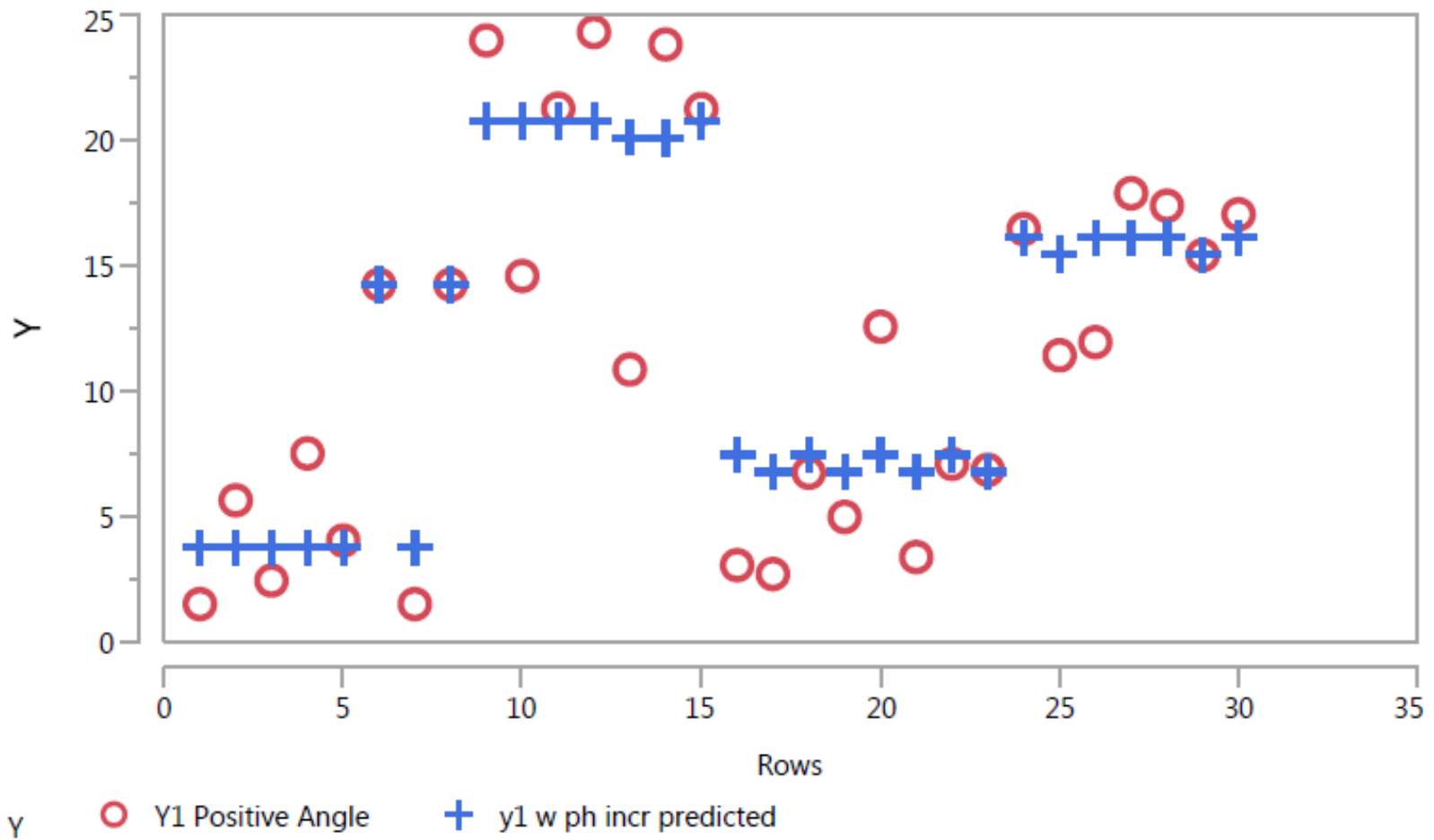
### Quantiles

100.0%	maximum	1.50459
99.5%		1.50459
97.5%		1.50459
90.0%		1.14275
75.0%	quartile	0.53675
50.0%	median	0.1754
25.0%	quartile	0.09472
10.0%		0.02855
2.5%		3.64e-6
0.5%		3.64e-6
0.0%	minimum	3.64e-6

### Summary Statistics

Mean	0.3825219
Std Dev	0.4287614
Std Err Mean	0.0782808
Upper 95% Mean	0.542624
Lower 95% Mean	0.2224197
N	30





## Appendix O: Negative Ionization Chromatographic Contrast Angle Regression Report

Upholds SW, DW, BP

Y1: Negative Angle

X1: DV pH6

X2: DV pH8

X3: DV DC 30

X4: DV DC 70

X5: DV DC 50

X6: DV DV70\*pH6

R Squared: .7500

R Squared, Adj: .6848

	Y2	APE	Degrees
Mean	19.9267	0.30664	6.110323
Median	19.3649	0.19593	3.794165

Mean Error ±6.11°

Median Error ±3.79°

	percent	degrees		
Max Error	140.30%	10.9°	between 0 and 10 degrees	5.4595
Mean Error	30.66%	4.50°	Error: ±5.46°	
Median Error	19.59%	3.97°		

stdev error 3.11 degrees

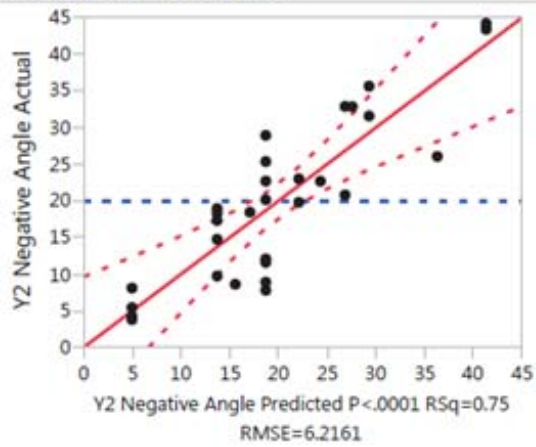
All VIF Scores below 2.0

Durbin Watson assumption of Independence upheld

## Response Y2 Negative Angle

### Whole Model

#### Actual by Predicted Plot



#### Summary of Fit

RSquare	0.750042
RSquare Adj	0.684835
Root Mean Square Error	6.216108
Mean of Response	19.92667
Observations (or Sum Wgts)	30

#### Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	6	2666.7555	444.459	11.5026
Error	23	888.7199	38.640	<b>Prob &gt; F</b>
C. Total	29	3555.4754		<b>&lt;.0001*</b>

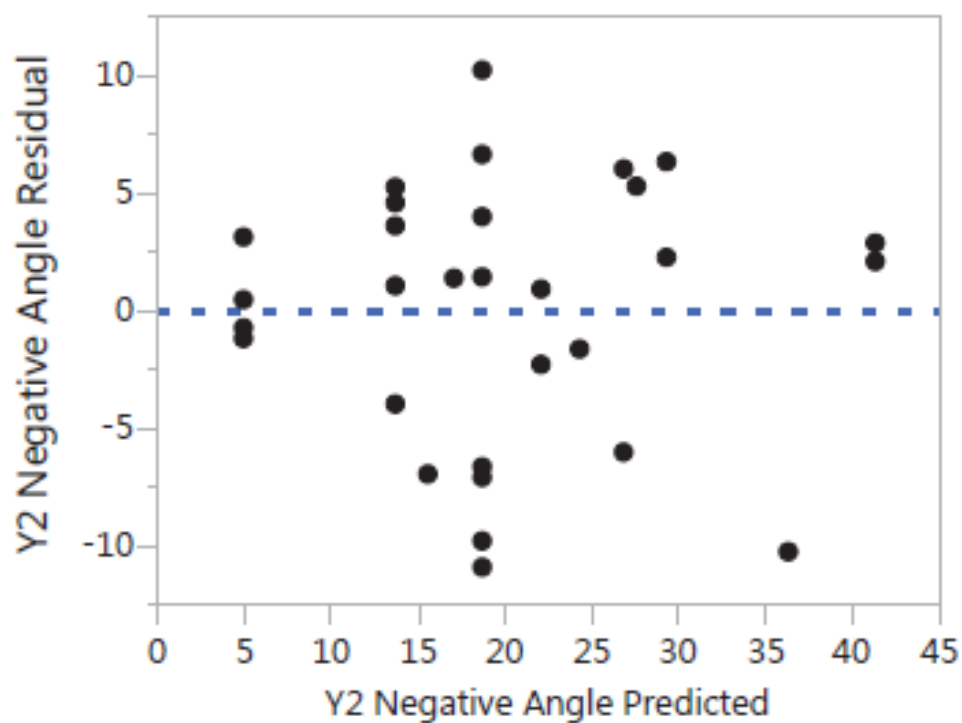
#### Parameter Estimates

Term	Estimate	Std Error	t Ratio	Prob> t	Std Beta	VIF
Intercept	17.87982	1.933547	9.25	<b>&lt;.0001*</b>	0	.
Dmy Var: pH6	-10.64895	2.78879	-3.82	<b>0.0009*</b>	-0.43257	1.180826
Dmy Var: pH8	-5.000822	2.758069	-1.81	0.0829	-0.20314	1.1549534
Dmy Var: DC 30	10.593667	3.456323	3.07	<b>0.0055*</b>	0.330791	1.0717753
Dmy Var: DC 50	22.596346	3.456323	6.54	<b>&lt;.0001*</b>	0.705579	1.0717753
Dmy Var: DC 70	8.3034399	3.254657	2.55	<b>0.0178*</b>	0.284252	1.1422523
(Dmy Var: DC 70-0.16667)*(Dmy Var: pH6-0.26667)	18.489657	6.378469	2.90	<b>0.0081*</b>	0.311231	1.0607207

## Response Y2 Negative Angle

### Whole Model

#### Residual by Predicted Plot

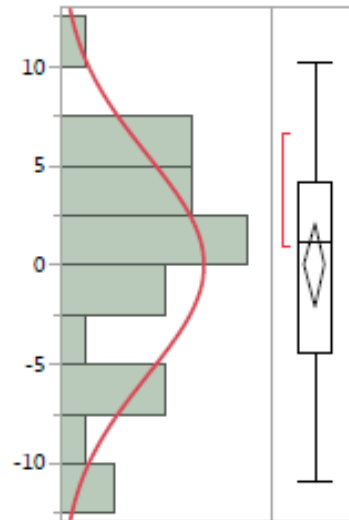


#### Durbin-Watson

Durbin-Watson	Number of Obs.	AutoCorrelation
1.8674995	30	0.0650

## Distributions

### Residual Y2 Negative Angle



Normal(3.8e-15,5.53584)

#### Quantiles

100.0%	maximum	10.2208
99.5%		10.2208
97.5%		10.2208
90.0%		6.29727
75.0%	quartile	4.12884
50.0%	median	1.214
25.0%	quartile	-4.487
10.0%		-9.5246
2.5%		-10.919
0.5%		-10.919
0.0%	minimum	-10.919

#### Summary Statistics

Mean	3.849e-15
Std Dev	5.535839
Std Err Mean	1.0107013
Upper 95% Mean	2.0671163
Lower 95% Mean	-2.067116
N	30

#### Fitted Normal

##### Parameter Estimates

Type	Parameter	Estimate	Lower 95%	Upper 95%
Location	$\mu$	3.849e-15	-2.067116	2.0671163
Dispersion	$\sigma$	5.535839	4.4087806	7.4419124

-2log(Likelihood) = 186.810900147079

#### Goodness-of-Fit Test

Shapiro-Wilk W Test

**Distributions**

**Residual Y2 Negative Angle**

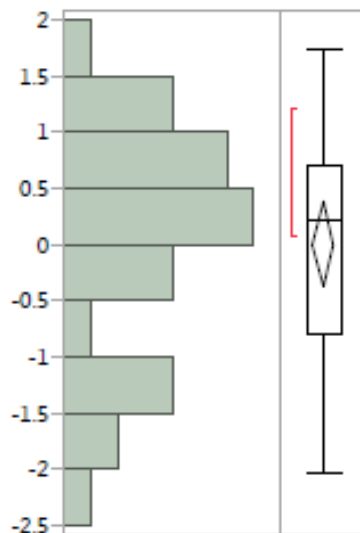
**Fitted Normal**

**Goodness-of-Fit Test**

W	Prob<W
0.950808	0.1777

Note: Ho = The data is from the Normal distribution. Small p-values reject Ho.

**Studentized Resid Y2 Negative Angle**



**Quantiles**

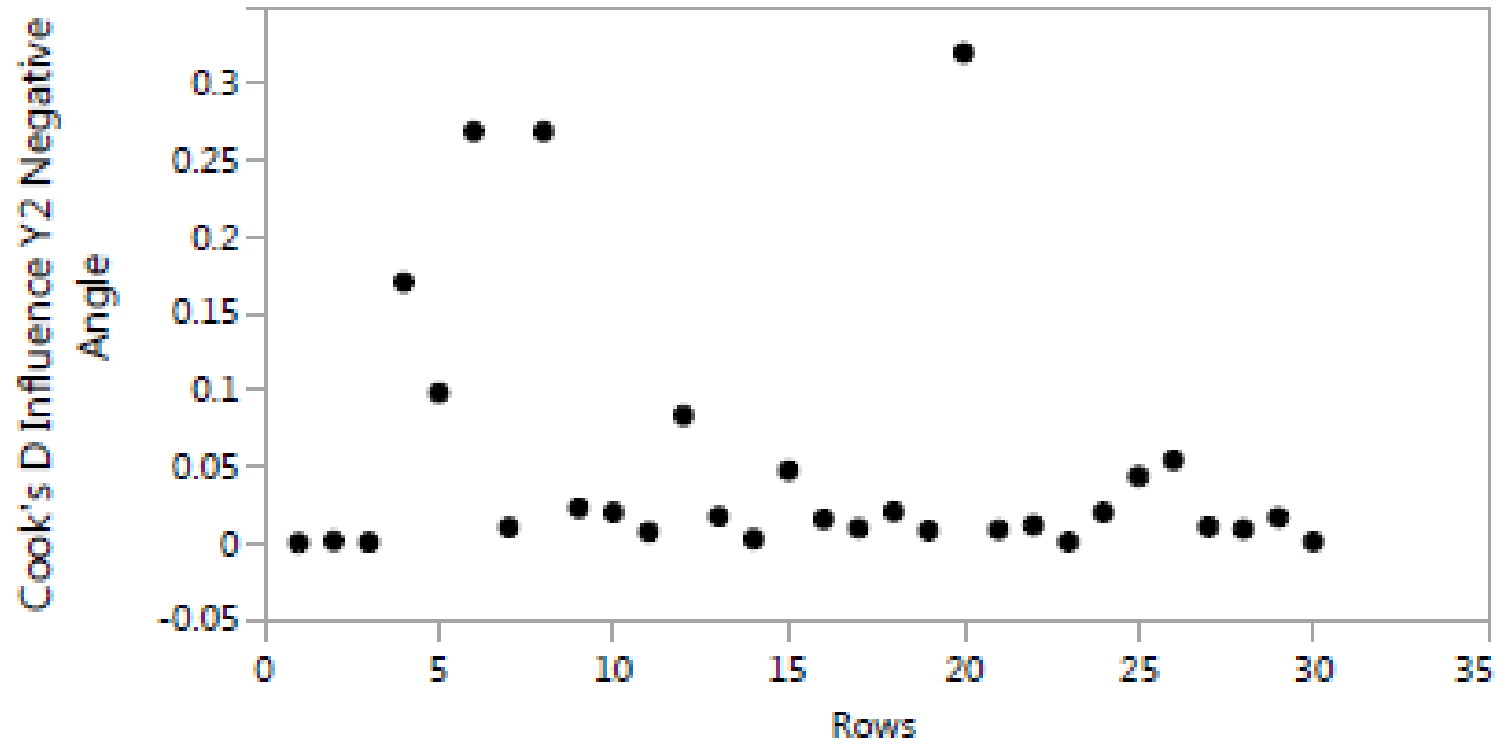
100.0%	maximum	1.7327
99.5%		1.7327
97.5%		1.7327
90.0%		1.1972
75.0%	quartile	0.70521
50.0%	median	0.21297
25.0%	quartile	-0.8004
10.0%		-1.6358
2.5%		-2.0437
0.5%		-2.0437
0.0%	minimum	-2.0437

**Summary Statistics**

Mean	-0.001621
Std Dev	1.0180402
Std Err Mean	0.1858679
Upper 95% Mean	0.3785214
Lower 95% Mean	-0.381764
N	30



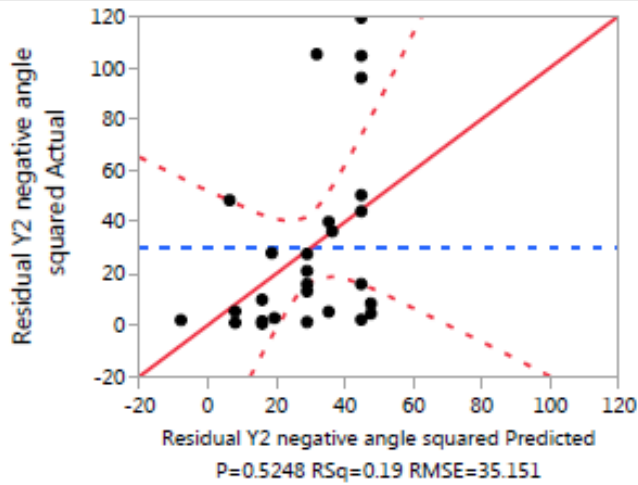
## Overlay Plot



## Response Residual Y2 negative angle squared

### Whole Model

#### Actual by Predicted Plot



#### Summary of Fit

RSquare	0.186727
RSquare Adj	-0.02543
Root Mean Square Error	35.15131
Mean of Response	29.624
Observations (or Sum Wgts)	30

#### Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	6	6525.019	1087.50	0.8801
Error	23	28419.129	1235.61	Prob > F
C. Total	29	34944.148		0.5248

#### Lack Of Fit

Source	DF	Sum of Squares	Mean Square	F Ratio
Lack Of Fit	5	14658.208	2931.64	3.8347
Pure Error	18	13760.921	764.50	Prob > F
Total Error	23	28419.129		0.0153*

Max RSq

0.6062

#### Parameter Estimates

Term	Estimate	Std Error	t Ratio	Prob> t
Intercept	42.234469	10.93397	3.86	0.0008*
Dmy Var: pH6	-19.40153	15.77026	-1.23	0.2310
Dmy Var: pH8	-15.84506	15.59653	-1.02	0.3202
Dmy Var: DC 30	-9.528971	19.54507	-0.49	0.6305
Dmy Var: DC 50	2.8217465	19.54507	0.14	0.8865
Dmy Var: DC 70	-21.5492	18.40467	-1.17	0.2536

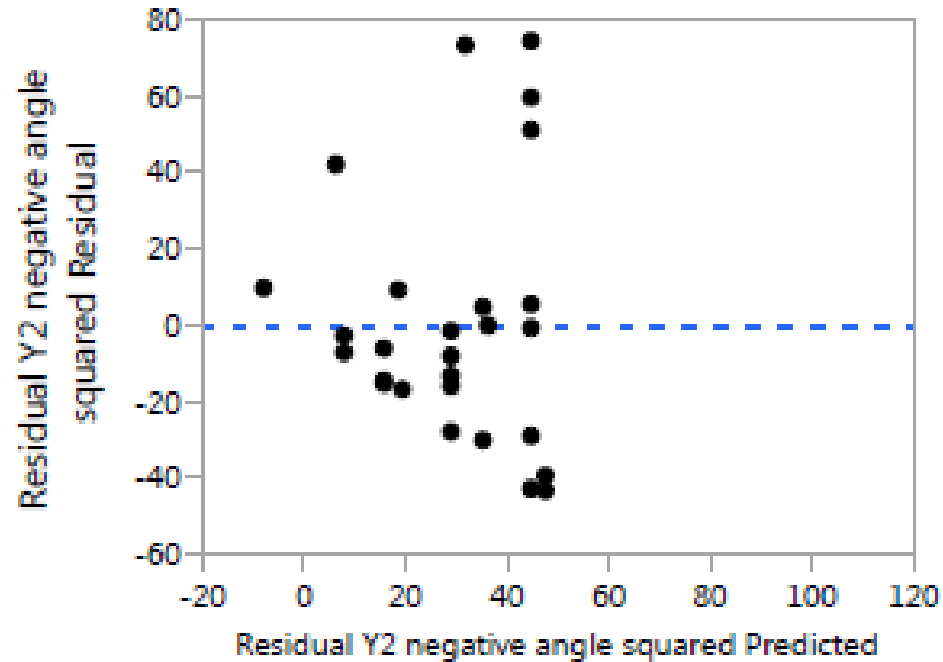
## Response Residual Y2 negative angle squared

### Whole Model

#### Parameter Estimates

Term	Estimate	Std Error	t Ratio	Prob> t
(Dmy Var: DC 70-0.16667)*(Dmy Var: pH6-0.26667)	57.35007	36.06944	1.59	0.1255

#### Residual by Predicted Plot



Breusch Pagan Test

Interact Two file in L Drive

N (sample size)  
dof (explained)  
Sum Sqrs Error (SSE)  
Sum Sqrs Regression (SSR)

User Defined
30
6
8.89E+02
6.53E+03

Test Statistic  
P-Value

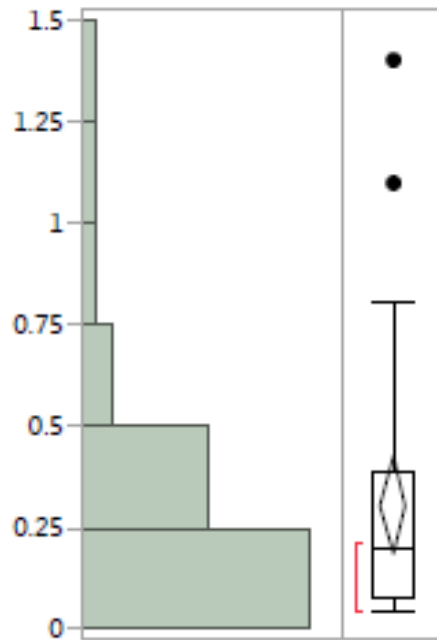
Computer Calculates
3.718109477
0.714760772

assumption constant variance  
compare w/alpha =0.05  
fail to reject upholds assumption of constant variance

Result - Computer Calculated
GOOD - Constant Variance

## Distributions

### APE Score Y2

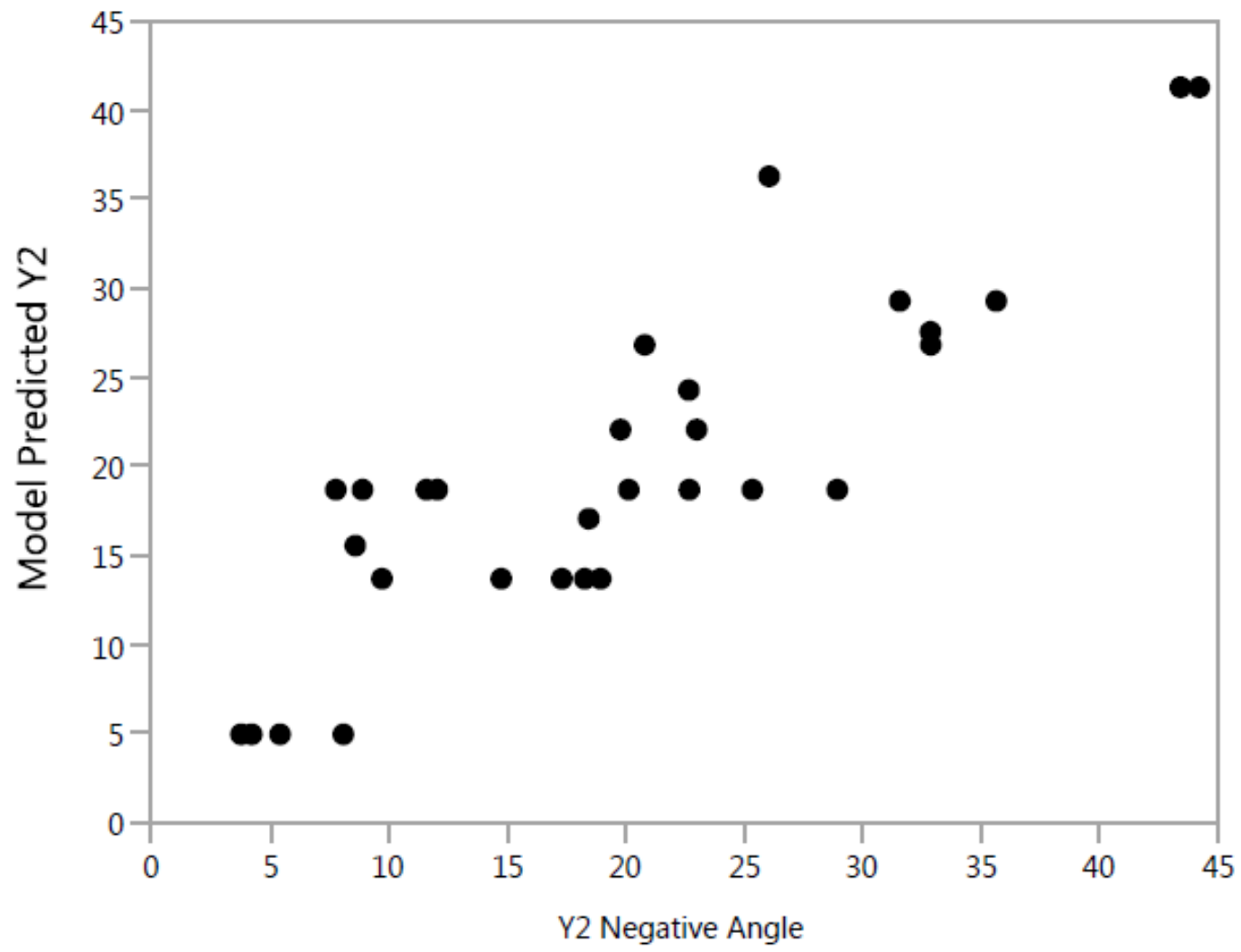


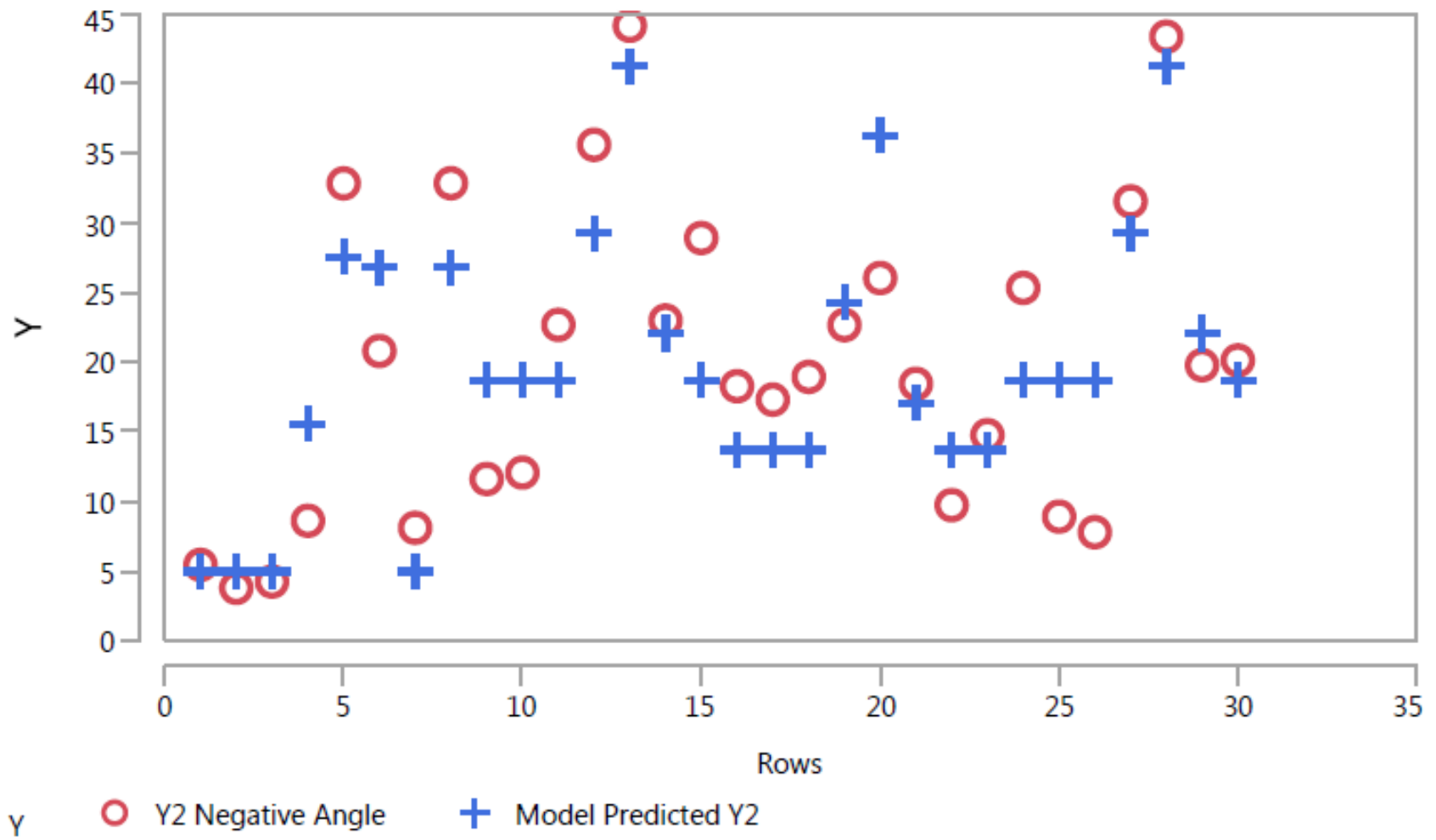
### Quantiles

100.0%	maximum	1.403
99.5%		1.403
97.5%		1.403
90.0%		0.78866
75.0%	quartile	0.38803
50.0%	median	0.19593
25.0%	quartile	0.07377
10.0%		0.06573
2.5%		0.03998
0.5%		0.03998
0.0%	minimum	0.03998

### Summary Statistics

Mean	0.3066352
Std Dev	0.3174315
Std Err Mean	0.0579548
Upper 95% Mean	0.4251661
Lower 95% Mean	0.1881044
N	30





### Appendix P: Byproduct Mass Calculations

	Atomic Weight	Sulfonic Acid Group	Sulfonic Acid Group'	Tar - Sulf	A (Tar)	A' (Tar - Na)	A'' (Tar - 2Na)	A''' (Tar - 3Na)
<b>C</b>	12.01	6	6	10	16	16	16	16
<b>H</b>	1.008	4	4	5	9	9	9	9
<b>N</b>	14.01	0	0	4	4	4	4	4
<b>Na</b>	22.99	1	0	2	3	2	1	0
<b>O</b>	16	3	3	6	9	9	9	9
<b>S</b>	32.06	1	1	1	2	2	2	2
	<b>Mass</b>	<b>179.142</b>	<b>156.152</b>	<b>355.22</b>	<b>534.362</b>	<b>511.372</b>	<b>488.382</b>	<b>465.392</b>

Mass	A	B	C	D	E	F
- 0Na (Product)	534.362	551.37	474.352	536.378	328.218	371.22
- 1Na (Product')	511.372	528.38	451.362	513.388	305.228	348.23
- 2Na (Product'')	488.382	505.39	428.372	490.398	282.238	325.24
- 3Na (Product''')	465.392	482.4	405.382	467.408	-	-



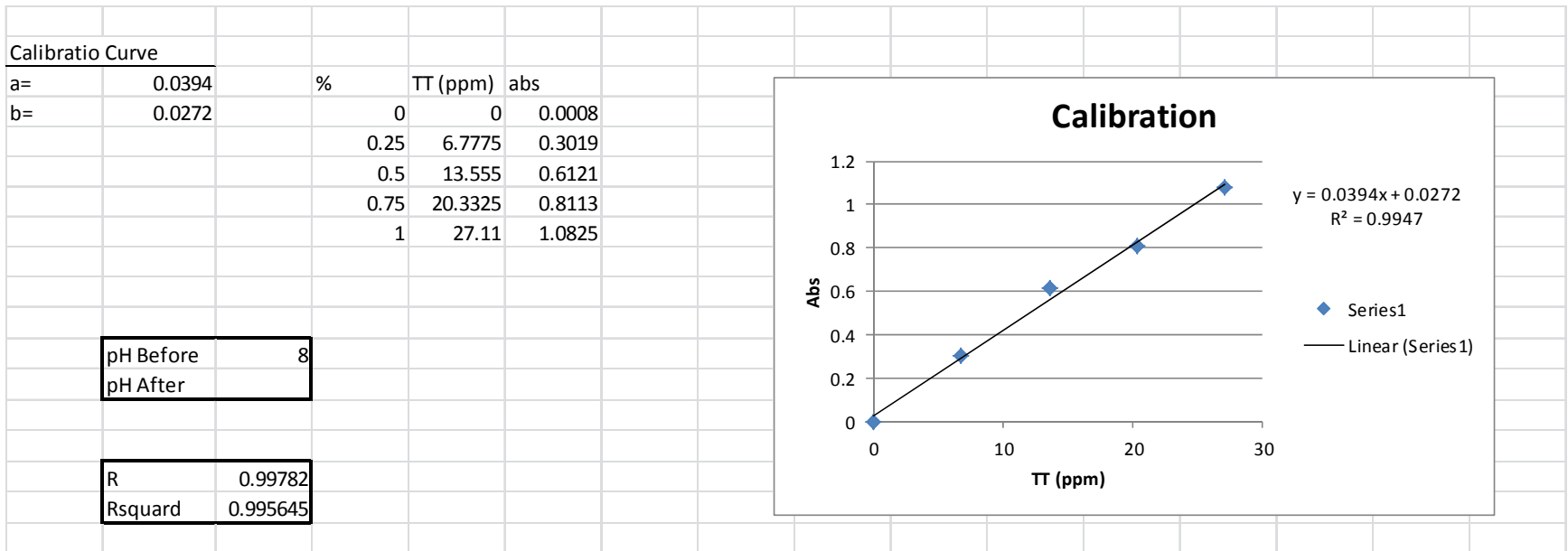
<b>B (Tar + OH)</b>	<b>B' (Tar + OH)</b>	<b>B'' (Tar + OH)</b>	<b>B''' (Tar + OH)</b>	<b>C (Tar - O - CO2)</b>	<b>C' (Tar - O - CO2)</b>	<b>C'' (Tar - O - CO2)</b>	<b>C''' (Tar - O - CO2)</b>
16	16	16	16	15	15	15	15
10	10	10	10	9	9	9	9
4	4	4	4	4	4	4	4
3	2	1	0	3	2	1	0
10	10	10	10	6	6	6	6
2	2	2	2	2	2	2	2
<b>551.37</b>	<b>528.38</b>	<b>505.39</b>	<b>482.4</b>	<b>474.352</b>	<b>451.362</b>	<b>428.372</b>	<b>405.382</b>

<b>D (Tar + 2H)</b>	<b>D' (Tar + 2H)</b>	<b>D'' (Tar + 2H)</b>	<b>D''' (Tar + 2H)</b>	<b>E (Tar - Sulf - CO2 + OH)</b>	<b>E' (Tar - Sulf - CO2 + OH)</b>	<b>E'' (Tar - Sulf - CO2 + OH)</b>
16	16	16	16	9	9	9
11	11	11	11	6	6	6
4	4	4	4	4	4	4
3	2	1	0	2	1	0
9	9	9	9	5	5	5
2	2	2	2	1	1	1
<b>536.378</b>	<b>513.388</b>	<b>490.398</b>	<b>467.408</b>	<b>328.218</b>	<b>305.228</b>	<b>282.238</b>

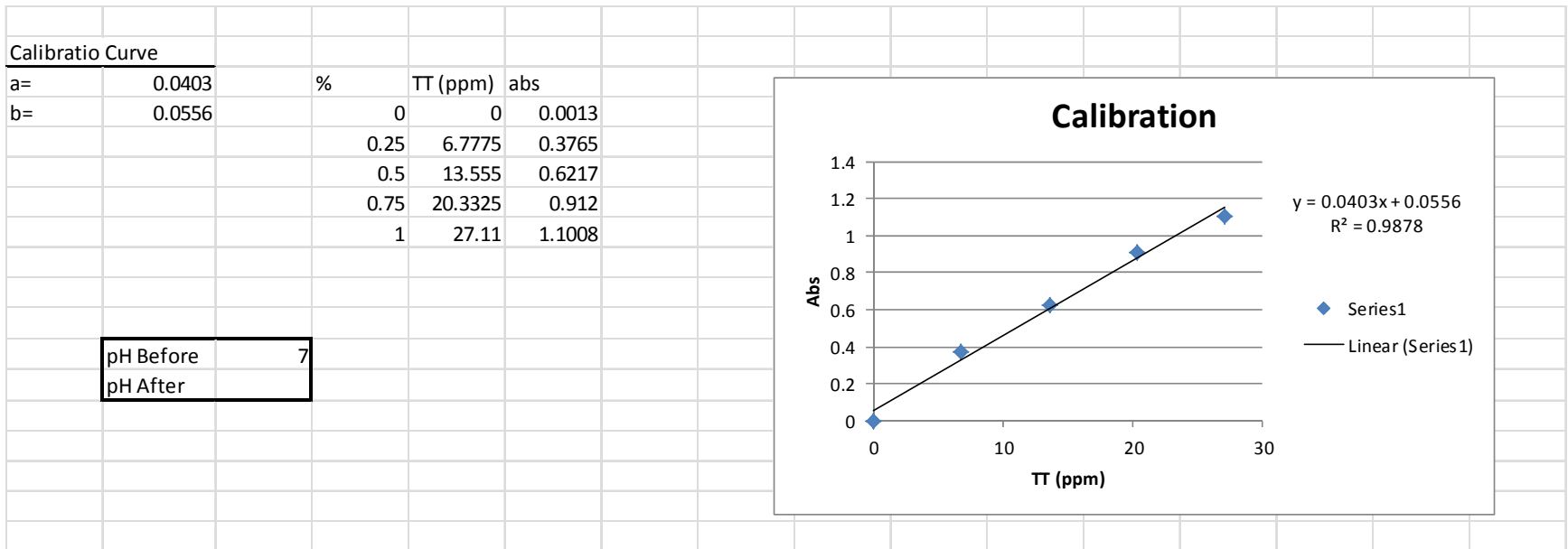
<b>F (Tar - Sulf + O)</b>	<b>F' (Tar - Sulf + O)</b>	<b>F'' (Tar - Sulf + O)</b>
10	10	10
5	5	5
4	4	4
2	1	0
7	7	7
1	1	1
<b>371.22</b>	<b>348.23</b>	<b>325.24</b>

## Appendix Q: AOP Original Data and Calibration Curves

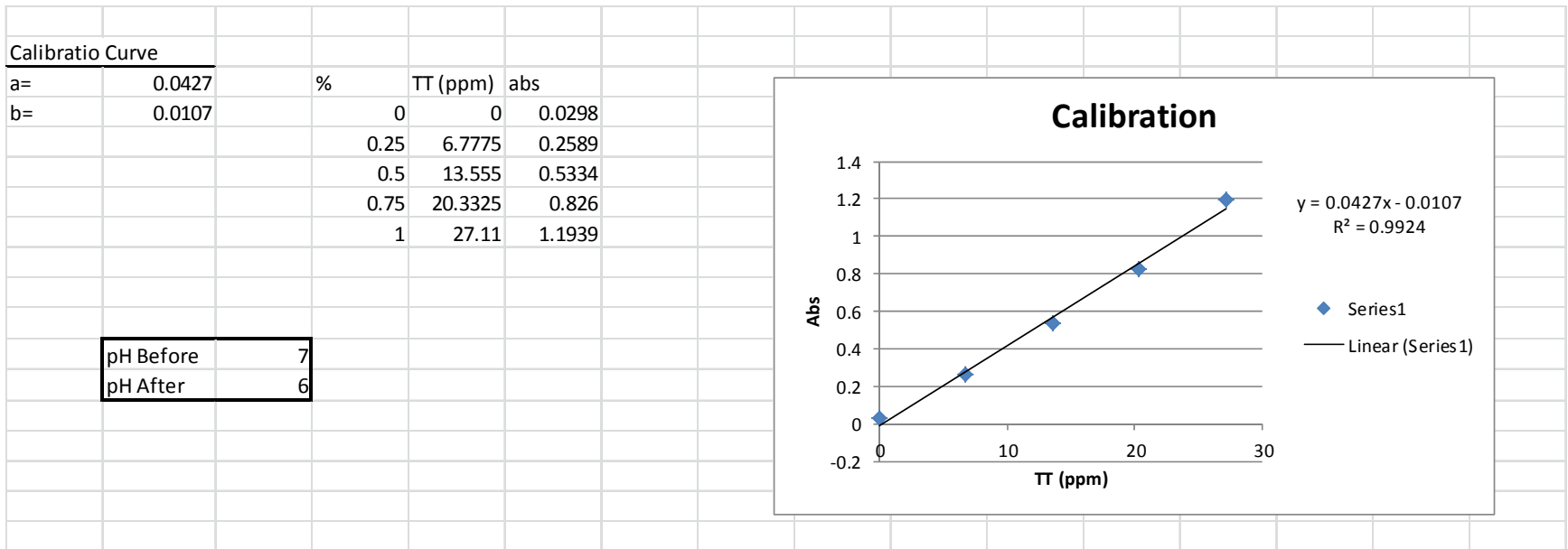
13Feb15_0.7@70%pH8					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.000623	
wavelength=	430				
time (min)	abs	C/Co	model	sum squares	
0	1.204469	42.83343	1	1	0
5	1.198508	42.61427	0.994884	0.996906	4.09E-06
10	1.201941	42.7405	0.99783	0.993854	1.58E-05
15	1.196972	42.5578	0.993565	0.990842	7.42E-06
20	1.194022	42.44934	0.991033	0.987871	1E-05
25	1.183733	42.07107	0.982202	0.984939	7.49E-06
30	1.185681	42.14269	0.983874	0.982047	3.34E-06
35	1.182127	42.01202	0.980823	0.979194	2.66E-06
40	1.171934	41.63727	0.972074	0.976378	1.85E-05
45	1.17808	41.86323	0.97735	0.973601	1.41E-05
50	1.17129	41.61359	0.971521	0.970861	4.37E-07
55	1.17153	41.62241	0.971727	0.968157	1.27E-05
60	1.165654	41.4064	0.966684	0.96549	1.43E-06
65	1.161083	41.23836	0.962761	0.962858	9.38E-09
70	1.156513	41.07033	0.958838	0.960262	2.03E-06
75	1.154611	41.00042	0.957206	0.9577	2.44E-07
80	1.160016	41.19913	0.961845	0.955173	4.45E-05
85	1.147367	40.73409	0.950988	0.952679	2.86E-06
90	1.146755	40.7116	0.950463	0.950219	5.94E-08
95	1.145745	40.67446	0.949596	0.947792	3.25E-06
100	1.142844	40.56781	0.947106	0.945398	2.92E-06
105	1.142975	40.57261	0.947218	0.943035	1.75E-05
110	1.138333	40.40196	0.943234	0.940705	6.4E-06
115	1.131792	40.16149	0.93762	0.938405	6.16E-07
120	1.134203	40.2501	0.939689	0.936136	1.26E-05
125	1.126926	39.98257	0.933443	0.933898	2.07E-07
130	1.123743	39.86555	0.930711	0.93169	9.58E-07
135	1.118662	39.67875	0.92635	0.929511	9.99E-06
140	1.122325	39.81341	0.929494	0.927361	4.55E-06
145	1.120632	39.75118	0.928041	0.925241	7.84E-06
150	1.12055	39.74815	0.92797	0.923148	2.33E-05
155	1.114975	39.54319	0.923185	0.921084	4.42E-06
160	1.111238	39.40579	0.919978	0.919047	8.66E-07
165	1.108001	39.28681	0.9172	0.917038	2.62E-08
170	1.104703	39.16556	0.914369	0.915055	4.71E-07
175	1.106082	39.21626	0.915553	0.913099	6.02E-06
180	1.102983	39.10233	0.912893	0.91117	2.97E-06
185	1.099889	38.98857	0.910237	0.909266	9.43E-07
190	1.094475	38.78952	0.90559	0.907388	3.23E-06
195	1.094014	38.77256	0.905194	0.905534	1.16E-07
200	1.100478	39.01021	0.910742	0.903706	4.95E-05
205	1.088652	38.57545	0.900592	0.901902	1.72E-06
210	1.08795	38.54961	0.899989	0.900123	1.78E-08
215	1.084575	38.42556	0.897093	0.898367	1.62E-06
220	1.089263	38.59791	0.901117	0.896634	2.01E-05
225	1.083812	38.3975	0.896438	0.894925	2.29E-06
230	1.0773	38.15809	0.890848	0.893239	5.72E-06
235	1.076219	38.11833	0.88992	0.891575	2.74E-06
240	1.07321	38.00773	0.887338	0.889934	6.74E-06
245	1.075173	38.07989	0.889023	0.888315	5.01E-07
250	1.0694	37.86764	0.884068	0.886717	7.02E-06
255	1.072208	37.9709	0.886478	0.885141	1.79E-06
260	1.066542	37.76259	0.881615	0.883586	3.88E-06
265	1.063778	37.66096	0.879242	0.882052	7.89E-06
270	1.068219	37.82422	0.883054	0.880538	6.33E-06
275	1.0619	37.59191	0.87763	0.879044	2E-06
280	1.056298	37.38595	0.872822	0.877571	2.26E-05
285	1.057561	37.43239	0.873906	0.876117	4.89E-06
290	1.052794	37.25713	0.869814	0.874683	2.37E-05
295	1.053016	37.26531	0.870005	0.873268	1.06E-05
300	1.054428	37.31722	0.871217	0.871872	4.29E-07
			sum=	0.000439	



7Mar15_0.7@0%pH7					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	1.97E-05	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.347136	23.50424	1	1	0
5	1.350849	23.57102	1.002841	0.999902	8.64E-06
10	1.348934	23.53658	1.001376	0.999805	2.47E-06
15	1.348248	23.52424	1.000851	0.999708	1.3E-06
20	1.3499	23.55396	1.002115	0.999613	6.26E-06
25	1.342373	23.41857	0.996355	0.999519	1E-05
30	1.340749	23.38938	0.995113	0.999426	1.86E-05
35	1.344021	23.44821	0.997616	0.999334	2.95E-06
40	1.349348	23.54403	1.001693	0.999243	6E-06
45	1.343877	23.44564	0.997507	0.999152	2.71E-06
50	1.350504	23.56482	1.002578	0.999063	1.24E-05
55	1.351606	23.58465	1.003421	0.998974	1.98E-05
60	1.342429	23.41959	0.996398	0.998887	6.19E-06
65	1.336644	23.31554	0.991972	0.9988	4.66E-05
70	1.348672	23.53188	1.001176	0.998715	6.06E-06
75	1.350174	23.55889	1.002325	0.99863	1.37E-05
80	1.344847	23.46307	0.998248	0.998546	8.85E-08
85	1.350204	23.55943	1.002348	0.998463	1.51E-05
90	1.347413	23.50923	1.000212	0.998381	3.35E-06
95	1.343704	23.44252	0.997374	0.998299	8.56E-07
100	1.343469	23.43829	0.997194	0.998219	1.05E-06
105	1.348678	23.53199	1.001181	0.998139	9.25E-06
110	1.349594	23.54844	1.001881	0.99806	1.46E-05
115	1.351111	23.57574	1.003042	0.997982	2.56E-05
120	1.335763	23.2997	0.991298	0.997905	4.37E-05
125	1.343258	23.4345	0.997033	0.997829	6.33E-07
130	1.339791	23.37214	0.99438	0.997753	1.14E-05
135	1.340201	23.37951	0.994694	0.997679	8.91E-06
140	1.343414	23.4373	0.997152	0.997605	2.05E-07
145	1.341348	23.40015	0.995571	0.997531	3.84E-06
150	1.351436	23.58159	1.003291	0.997459	3.4E-05
155	1.34084	23.39101	0.995183	0.997387	4.86E-06
160	1.340608	23.38683	0.995005	0.997316	5.34E-06
165	1.349836	23.55281	1.002066	0.997246	2.32E-05
170	1.337726	23.335	0.9928	0.997176	1.92E-05
175	1.336776	23.31792	0.992073	0.997108	2.53E-05
180	1.340186	23.37924	0.994682	0.99704	5.56E-06
185	1.341591	23.40452	0.995758	0.996972	1.48E-06
190	1.339185	23.36125	0.993916	0.996906	8.93E-06
195	1.34869	23.5322	1.00119	0.99684	1.89E-05
200	1.341588	23.40447	0.995755	0.996774	1.04E-06
205	1.346927	23.50049	0.99984	0.99671	9.8E-06
210	1.349863	23.55329	1.002087	0.996646	2.96E-05
215	1.342975	23.4294	0.996816	0.996583	5.44E-08
220	1.337947	23.33897	0.992969	0.99652	1.26E-05
225	1.348032	23.52036	1.000686	0.996458	1.79E-05
230	1.344025	23.4483	0.99762	0.996397	1.5E-06
235	1.3375	23.33093	0.992627	0.996336	1.38E-05
240	1.348585	23.53031	1.001109	0.996276	2.34E-05
245	1.339528	23.36741	0.994179	0.996217	4.15E-06
250	1.343466	23.43823	0.997192	0.996158	1.07E-06
255	1.343612	23.44087	0.997304	0.9961	1.45E-06
260	1.337768	23.33575	0.992832	0.996042	1.03E-05
265	1.344269	23.45268	0.997807	0.995985	3.32E-06
270	1.347889	23.51779	1.000577	0.995929	2.16E-05
275	1.341426	23.40154	0.995631	0.995873	5.88E-08
280	1.350573	23.56606	1.00263	0.995818	4.64E-05
285	1.337829	23.33684	0.992878	0.995763	8.32E-06
290	1.33766	23.33382	0.992749	0.995709	8.76E-06
295	1.335	23.28597	0.990714	0.995656	2.44E-05
300	1.338162	23.34285	0.993134	0.995603	6.1E-06
			sum=		0.000695

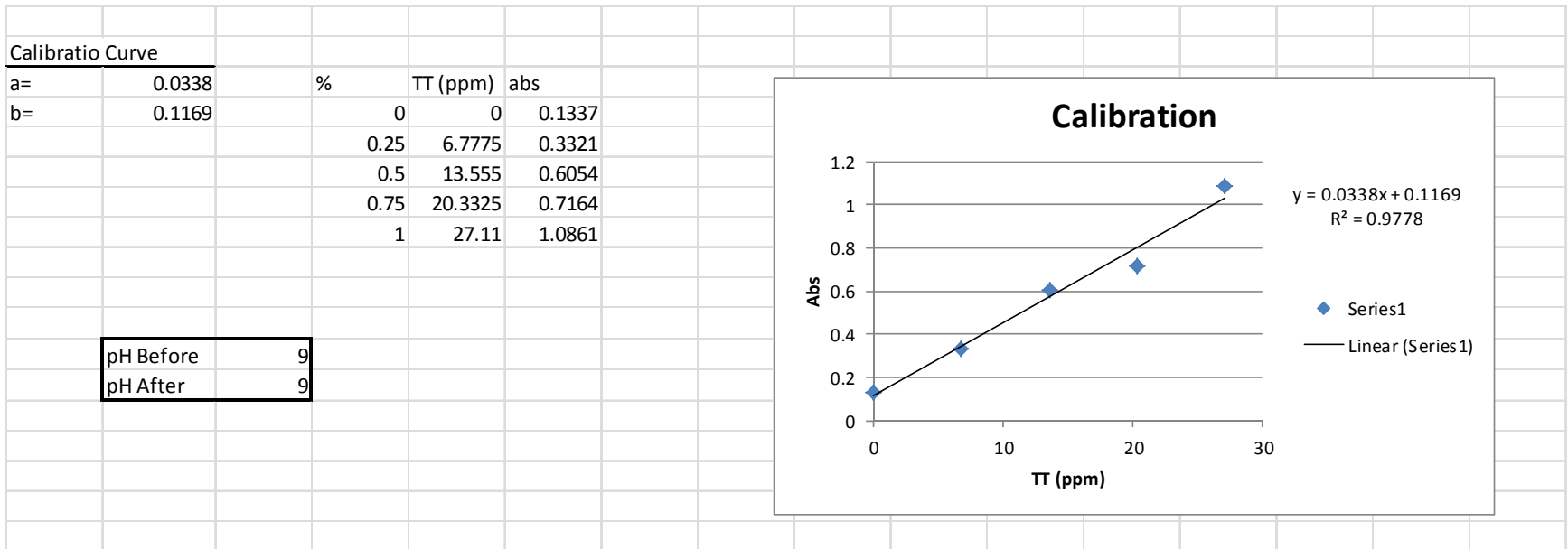


13Mar15_0.7@5%pH7					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	9.07E-05	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.23038	110.9981	1	1	0
5	1.222567	110.268	0.993422	0.999549	3.75E-05
10	1.234194	111.3546	1.003211	0.999103	1.69E-05
15	1.226878	110.6709	0.997052	0.998661	2.59E-06
20	1.225585	110.55	0.995963	0.998225	5.12E-06
25	1.232246	111.1725	1.001571	0.997793	1.43E-05
30	1.227749	110.7522	0.997785	0.997366	1.76E-07
35	1.226388	110.625	0.996639	0.996943	9.26E-08
40	1.223906	110.3931	0.99455	0.996525	3.9E-06
45	1.230713	111.0293	1.000281	0.996111	1.74E-05
50	1.226309	110.6176	0.996572	0.995702	7.57E-07
55	1.227442	110.7235	0.997526	0.995298	4.97E-06
60	1.222023	110.2171	0.992964	0.994897	3.74E-06
65	1.224014	110.4031	0.99464	0.994501	1.92E-08
70	1.220963	110.118	0.992071	0.994109	4.15E-06
75	1.218882	109.9235	0.990319	0.993722	1.16E-05
80	1.219184	109.9518	0.990573	0.993338	7.65E-06
85	1.226177	110.6053	0.996461	0.992959	1.23E-05
90	1.222691	110.2796	0.993526	0.992584	8.88E-07
95	1.214266	109.4921	0.986432	0.992213	3.34E-05
100	1.21531	109.5897	0.987312	0.991846	2.06E-05
105	1.213807	109.4492	0.986046	0.991482	2.96E-05
110	1.213169	109.3896	0.985509	0.991123	3.15E-05
115	1.213494	109.42	0.985783	0.990768	2.49E-05
120	1.221479	110.1663	0.992506	0.990416	4.37E-06
125	1.215341	109.5926	0.987337	0.990068	7.46E-06
130	1.219137	109.9474	0.990534	0.989724	6.55E-07
135	1.211527	109.2362	0.984126	0.989384	2.76E-05
140	1.218657	109.9025	0.99013	0.989047	1.17E-06
145	1.21438	109.5028	0.986529	0.988714	4.78E-06
150	1.216062	109.66	0.987945	0.988385	1.94E-07
155	1.210601	109.1497	0.983347	0.988059	2.22E-05
160	1.213534	109.4237	0.985816	0.987736	3.69E-06
165	1.221324	110.1518	0.992375	0.987417	2.46E-05
170	1.214742	109.5366	0.986833	0.987102	7.22E-08
175	1.21019	109.1112	0.983001	0.98679	1.44E-05
180	1.214652	109.5282	0.986757	0.986481	7.64E-08
185	1.213058	109.3792	0.985415	0.986176	5.78E-07
190	1.211967	109.2772	0.984496	0.985873	1.9E-06
195	1.214663	109.5293	0.986767	0.985575	1.42E-06
200	1.21959	109.9897	0.990915	0.985279	3.18E-05
205	1.211616	109.2445	0.984201	0.984986	6.17E-07
210	1.220786	110.1015	0.991922	0.984697	5.22E-05
215	1.211623	109.2452	0.984208	0.984411	4.14E-08
220	1.205627	108.6848	0.979159	0.984128	2.47E-05
225	1.218551	109.8926	0.990041	0.983848	3.84E-05
230	1.206918	108.8055	0.980246	0.983571	1.11E-05
235	1.216765	109.7257	0.988537	0.983297	2.75E-05
240	1.213016	109.3753	0.98538	0.983025	5.54E-06
245	1.213948	109.4624	0.986165	0.982757	1.16E-05
250	1.218909	109.9261	0.990342	0.982492	6.16E-05
255	1.206083	108.7274	0.979543	0.982229	7.22E-06
260	1.214847	109.5464	0.986921	0.98197	2.45E-05
265	1.206509	108.7672	0.979902	0.981713	3.28E-06
270	1.213019	109.3756	0.985382	0.981459	1.54E-05
275	1.213614	109.4312	0.985883	0.981207	2.19E-05
280	1.206276	108.7455	0.979705	0.980959	1.57E-06
285	1.205132	108.6385	0.978742	0.980713	3.88E-06
290	1.203713	108.5059	0.977547	0.98047	8.54E-06
295	1.200695	108.2238	0.975006	0.980229	2.73E-05
300	1.20452	108.5814	0.978227	0.979991	3.11E-06
			sum=		0.000781



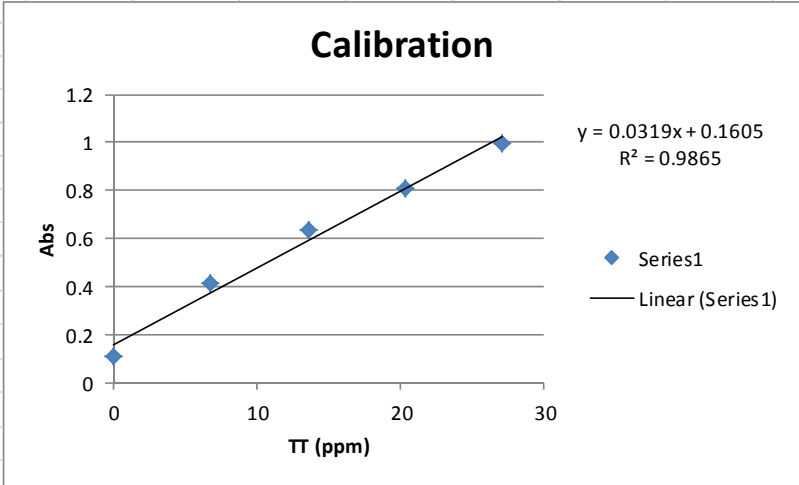
16Mar15_0.7@0%pH9					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	-1.6E-05	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.089044	9.026898	1	1	0
5	1.097648	9.100496	1.008153	1.000077	6.52E-05
10	1.094525	9.073781	1.005194	1.000154	2.54E-05
15	1.092652	9.057755	1.003418	1.000229	1.02E-05
20	1.091003	9.043651	1.001856	1.000304	2.41E-06
25	1.096163	9.087791	1.006746	1.000378	4.05E-05
30	1.093745	9.067112	1.004455	1.000452	1.6E-05
35	1.094047	9.06969	1.00474	1.000524	1.78E-05
40	1.100506	9.124945	1.010862	1.000596	0.000105
45	1.099427	9.115712	1.009839	1.000667	8.41E-05
50	1.093896	9.068397	1.004597	1.000738	1.49E-05
55	1.102695	9.143674	1.012936	1.000807	0.000147
60	1.097598	9.100072	1.008106	1.000876	5.23E-05
65	1.097597	9.100064	1.008105	1.000945	5.13E-05
70	1.094955	9.077459	1.005601	1.001012	2.11E-05
75	1.09943	9.115742	1.009842	1.001079	7.68E-05
80	1.092563	9.057	1.003335	1.001145	4.79E-06
85	1.090992	9.043558	1.001846	1.001211	4.03E-07
90	1.099896	9.119723	1.010283	1.001276	8.11E-05
95	1.094018	9.069441	1.004713	1.00134	1.14E-05
100	1.092546	9.056852	1.003318	1.001403	3.67E-06
105	1.09182	9.050645	1.002631	1.001466	1.36E-06
110	1.092992	9.060668	1.003741	1.001528	4.9E-06
115	1.092684	9.058035	1.003449	1.00159	3.46E-06
120	1.091814	9.050589	1.002624	1.001651	9.48E-07
125	1.091535	9.048204	1.00236	1.001711	4.22E-07
130	1.095445	9.081654	1.006066	1.001771	1.84E-05
135	1.092384	9.055468	1.003165	1.00183	1.78E-06
140	1.090872	9.042529	1.001732	1.001888	2.46E-08
145	1.092664	9.057857	1.00343	1.001946	2.2E-06
150	1.092723	9.05837	1.003487	1.002004	2.2E-06
155	1.089581	9.031486	1.000508	1.00206	2.41E-06
160	1.093762	9.067256	1.004471	1.002116	5.54E-06
165	1.089883	9.034076	1.000795	1.002172	1.9E-06
170	1.092827	9.059256	1.003585	1.002227	1.84E-06
175	1.086721	9.007025	0.997798	1.002281	2.01E-05
180	1.091185	9.045208	1.002028	1.002335	9.41E-08
185	1.093033	9.061019	1.00378	1.002389	1.94E-06
190	1.088751	9.024387	0.999722	1.002441	7.4E-06
195	1.089519	9.030961	1.00045	1.002494	4.18E-06
200	1.089049	9.026937	1.000004	1.002545	6.46E-06
205	1.088885	9.025533	0.999849	1.002596	7.55E-06
210	1.092084	9.052902	1.002881	1.002647	5.46E-08
215	1.098274	9.105855	1.008747	1.002697	3.66E-05
220	1.09094	9.043111	1.001796	1.002747	9.04E-07
225	1.089637	9.031969	1.000562	1.002796	4.99E-06
230	1.095751	9.084266	1.006355	1.002844	1.23E-05
235	1.08757	9.014283	0.998603	1.002893	1.84E-05
240	1.085639	8.997767	0.996773	1.00294	3.8E-05
245	1.089055	9.026987	1.00001	1.002987	8.86E-06
250	1.087058	9.009905	0.998118	1.003034	2.42E-05
255	1.088977	9.026326	0.999937	1.00308	9.88E-06
260	1.092321	9.054924	1.003105	1.003126	4.44E-10
265	1.090817	9.042059	1.00168	1.003171	2.22E-06
270	1.088707	9.024013	0.99968	1.003216	1.25E-05
275	1.090337	9.037959	1.001225	1.00326	4.14E-06
280	1.090565	9.039905	1.001441	1.003304	3.47E-06
285	1.091601	9.048764	1.002422	1.003347	8.55E-07
290	1.091923	9.051523	1.002728	1.00339	4.39E-07
295	1.090315	9.037766	1.001204	1.003433	4.97E-06
300	1.095662	9.083506	1.006271	1.003475	7.82E-06
			sum=		0.001118



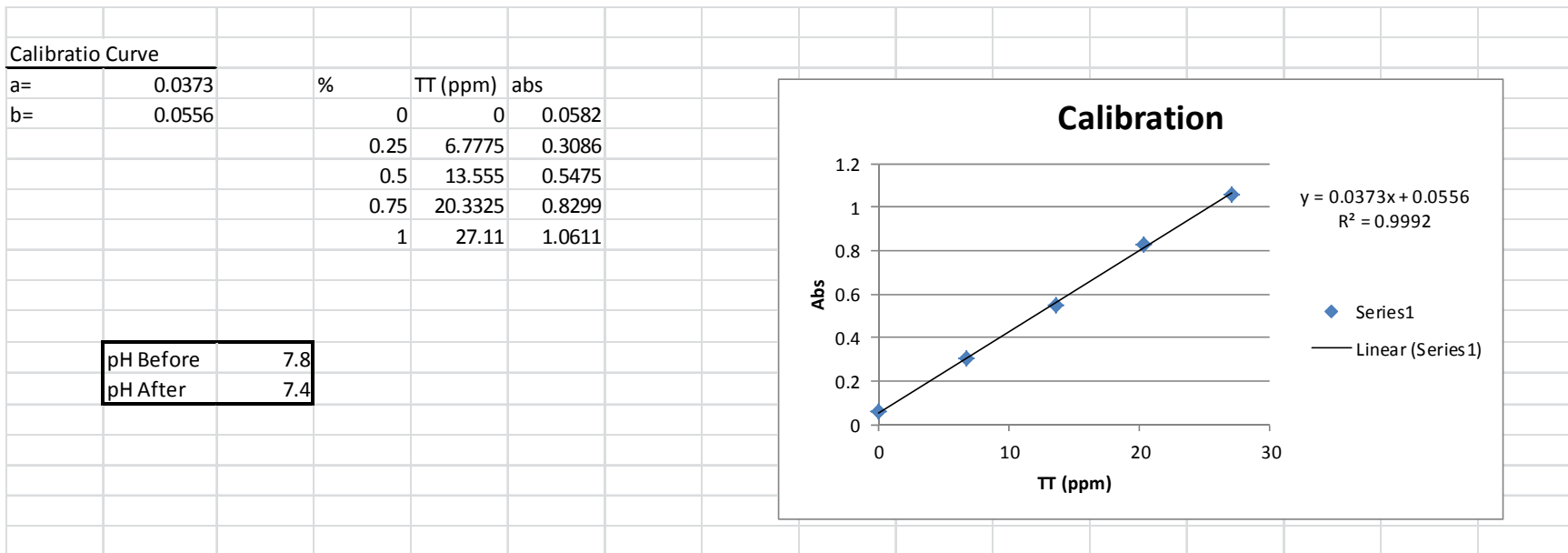


8Apr15_0.7@100%pH9H2O2Ctrl					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	4.34E-05	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	0.932205	5.609379	1	1	0
5	0.942214	5.67174	1.011117	0.999784	0.000128
10	0.934182	5.621696	1.002196	0.999571	6.89E-06
15	0.935651	5.63085	1.003828	0.999359	2E-05
20	0.936384	5.635414	1.004641	0.99915	3.02E-05
25	0.930519	5.59887	0.998127	0.998944	6.67E-07
30	0.933189	5.615508	1.001093	0.998739	5.54E-06
35	0.941072	5.664621	1.009848	0.998536	0.000128
40	0.927239	5.578434	0.994483	0.998336	1.48E-05
45	0.932213	5.609429	1.000009	0.998138	3.5E-06
50	0.930038	5.595873	0.997592	0.997942	1.22E-07
55	0.929404	5.591924	0.996888	0.997747	7.38E-07
60	0.931739	5.606473	0.999482	0.997555	3.71E-06
65	0.930879	5.601114	0.998527	0.997365	1.35E-06
70	0.93959	5.655386	1.008202	0.997177	0.000122
75	0.928589	5.58685	0.995984	0.996991	1.01E-06
80	0.933122	5.615092	1.001019	0.996807	1.77E-05
85	0.929218	5.590769	0.996682	0.996625	3.31E-09
90	0.932583	5.611732	1.000419	0.996445	1.58E-05
95	0.925239	5.565977	0.992263	0.996266	1.6E-05
100	0.927472	5.579886	0.994742	0.99609	1.82E-06
105	0.925332	5.566553	0.992365	0.995915	1.26E-05
110	0.92742	5.579561	0.994684	0.995743	1.12E-06
115	0.933001	5.614335	1.000884	0.995572	2.82E-05
120	0.92743	5.579629	0.994696	0.995402	4.98E-07
125	0.925467	5.567395	0.992515	0.995235	7.4E-06
130	0.923117	5.552755	0.989906	0.995069	2.67E-05
135	0.924275	5.559971	0.991192	0.994906	1.38E-05
140	0.925489	5.56753	0.99254	0.994743	4.86E-06
145	0.929579	5.593016	0.997083	0.994583	6.25E-06
150	0.929729	5.593952	0.99725	0.994424	7.98E-06
155	0.922473	5.548744	0.989191	0.994267	2.58E-05
160	0.928174	5.584264	0.995523	0.994112	1.99E-06
165	0.923094	5.552612	0.98988	0.993958	1.66E-05
170	0.928122	5.583939	0.995465	0.993806	2.75E-06
175	0.927673	5.581139	0.994966	0.993655	1.72E-06
180	0.926343	5.572854	0.993489	0.993506	3.18E-10
185	0.927574	5.58052	0.994855	0.993359	2.24E-06
190	0.921681	5.54381	0.988311	0.993213	2.4E-05
195	0.921884	5.545071	0.988536	0.993069	2.06E-05
200	0.917002	5.514651	0.983113	0.992926	9.63E-05
205	0.919723	5.531608	0.986136	0.992785	4.42E-05
210	0.921918	5.545282	0.988573	0.992645	1.66E-05
215	0.922173	5.546869	0.988856	0.992507	1.33E-05
220	0.919115	5.527822	0.985461	0.99237	4.77E-05
225	0.923572	5.555589	0.990411	0.992234	3.33E-06
230	0.920168	5.534383	0.98663	0.992101	2.99E-05
235	0.930028	5.595811	0.997581	0.991968	3.15E-05
240	0.918019	5.520991	0.984243	0.991837	5.77E-05
245	0.920589	5.537001	0.987097	0.991707	2.13E-05
250	0.924369	5.560554	0.991296	0.991579	7.99E-08
255	0.92658	5.574328	0.993751	0.991451	5.29E-06
260	0.930785	5.600532	0.998423	0.991326	5.04E-05
265	0.924951	5.56418	0.991942	0.991201	5.49E-07
270	0.926369	5.573013	0.993517	0.991078	5.95E-06
275	0.927791	5.581876	0.995097	0.990956	1.71E-05
280	0.936193	5.634222	1.004429	0.990836	0.000185
285	0.923098	5.552638	0.989885	0.990717	6.92E-07
290	0.927071	5.577388	0.994297	0.990599	1.37E-05
295	0.92644	5.573457	0.993596	0.990482	9.7E-06
300	0.929785	5.594299	0.997312	0.990366	4.82E-05
			sum=		0.001421

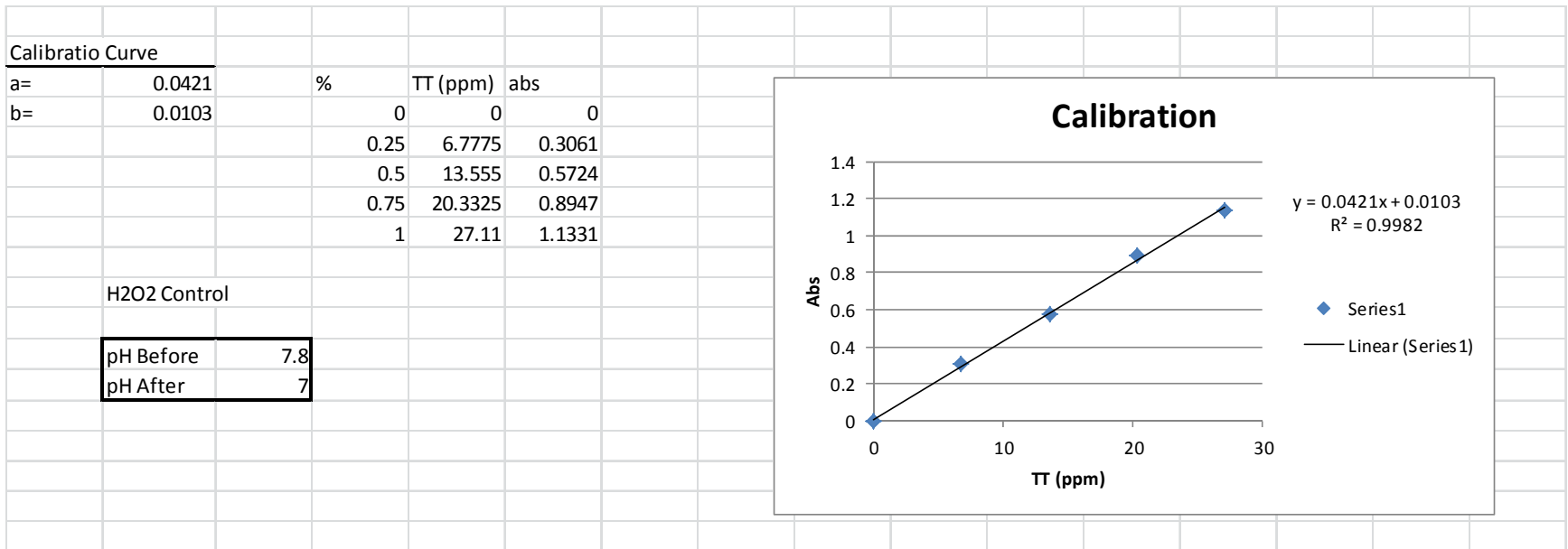
Calibratio Curve			
a=	0.0319	%	TT (ppm)
b=	0.1605		abs
		0	0 0.1116
		0.25	6.7775 0.4145
		0.5	13.555 0.6338
		0.75	20.3325 0.8081
		1	27.11 0.9953
H2O2 Control			
pH Before	9		
pH After	8.5		
R	0.608253		
Rsquard	0.369972		



9Apr15 0.7@10%pH7					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.00016	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.16541	20.28974	1	1	0
5	1.167143	20.32092	1.001537	0.999206	5.43E-06
10	1.165206	20.28608	0.99982	0.998421	1.96E-06
15	1.16667	20.31241	1.001117	0.997645	1.21E-05
20	1.162	20.22842	0.996978	0.996877	1E-08
25	1.165599	20.29314	1.000167	0.996118	1.64E-05
30	1.169795	20.36862	1.003887	0.995368	7.26E-05
35	1.160384	20.19935	0.995545	0.994625	8.46E-07
40	1.168191	20.33976	1.002465	0.993891	7.35E-05
45	1.155349	20.1088	0.991082	0.993165	4.34E-06
50	1.161528	20.21993	0.996559	0.992448	1.69E-05
55	1.155834	20.11751	0.991511	0.991738	5.12E-08
60	1.155432	20.11028	0.991155	0.991036	1.42E-08
65	1.153369	20.07318	0.989327	0.990342	1.03E-06
70	1.155217	20.10642	0.990965	0.989655	1.72E-06
75	1.155183	20.10581	0.990935	0.988976	3.84E-06
80	1.152546	20.05839	0.988598	0.988305	8.57E-08
85	1.155679	20.11473	0.991374	0.987641	1.39E-05
90	1.153079	20.06797	0.98907	0.986985	4.35E-06
95	1.147578	19.96904	0.984194	0.986335	4.59E-06
100	1.151601	20.04139	0.98776	0.985693	4.27E-06
105	1.147191	19.96207	0.983851	0.985059	1.46E-06
110	1.147445	19.96663	0.984075	0.984431	1.26E-07
115	1.146816	19.95532	0.983518	0.98381	8.54E-08
120	1.153031	20.0671	0.989027	0.983196	3.4E-05
125	1.140669	19.84477	0.978069	0.982589	2.04E-05
130	1.138873	19.81246	0.976477	0.981989	3.04E-05
135	1.150136	20.01504	0.986461	0.981395	2.57E-05
140	1.141989	19.86851	0.979239	0.980808	2.46E-06
145	1.151769	20.04441	0.987909	0.980227	5.9E-05
150	1.140806	19.84723	0.97819	0.979653	2.14E-06
155	1.146226	19.94471	0.982995	0.979086	1.53E-05
160	1.13883	19.81169	0.976439	0.978524	4.35E-06
165	1.141436	19.85856	0.978749	0.977969	6.08E-07
170	1.137207	19.7825	0.975	0.97742	5.85E-06
175	1.14017	19.83579	0.977627	0.976877	5.62E-07
180	1.137428	19.78647	0.975196	0.97634	1.31E-06
185	1.139001	19.81476	0.97659	0.975809	6.1E-07
190	1.139704	19.82741	0.977214	0.975284	3.72E-06
195	1.135321	19.74859	0.973329	0.974765	2.06E-06
200	1.13453	19.73436	0.972627	0.974252	2.64E-06
205	1.137133	19.78118	0.974935	0.973744	1.42E-06
210	1.133244	19.71123	0.971487	0.973242	3.08E-06
215	1.133356	19.71325	0.971587	0.972745	1.34E-06
220	1.130719	19.66581	0.969249	0.972254	9.03E-06
225	1.141598	19.86147	0.978892	0.971769	5.07E-05
230	1.128199	19.62048	0.967015	0.971289	1.83E-05
235	1.14049	19.84154	0.97791	0.970814	5.04E-05
240	1.126791	19.59517	0.965767	0.970344	2.09E-05
245	1.130763	19.6666	0.969288	0.96988	3.51E-07
250	1.136717	19.77369	0.974566	0.969421	2.65E-05
255	1.128552	19.62683	0.967328	0.968967	2.69E-06
260	1.127759	19.61257	0.966625	0.968518	3.58E-06
265	1.12366	19.53885	0.962992	0.968074	2.58E-05
270	1.127643	19.61049	0.966522	0.967635	1.24E-06
275	1.125492	19.5718	0.964615	0.9672	6.68E-06
280	1.128413	19.62434	0.967205	0.966771	1.89E-07
285	1.122943	19.52595	0.962356	0.966346	1.59E-05
290	1.122578	19.51939	0.962032	0.965926	1.52E-05
295	1.133249	19.71131	0.971491	0.965511	3.58E-05
300	1.125296	19.56827	0.964442	0.965101	4.34E-07
			sum=		0.00074

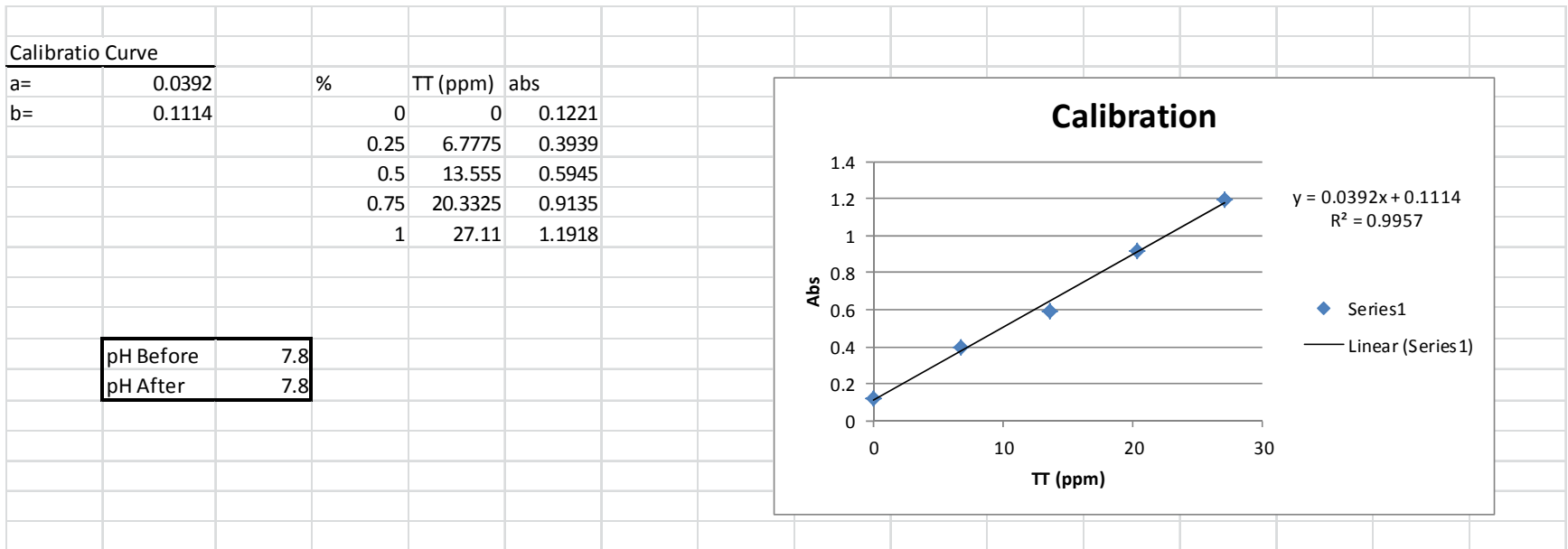


16Apr15 0.7@100%pH8H2O2Ctrl					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	9.41E-07	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.181593	110.6304	1	1	0
5	1.180632	110.5371	0.999157	0.999995	7.03E-07
10	1.181702	110.641	1.000096	0.999991	1.11E-08
15	1.183201	110.7865	1.001412	0.999986	2.03E-06
20	1.176988	110.1833	0.995959	0.999982	1.62E-05
25	1.188059	111.2581	1.005674	0.999977	3.25E-05
30	1.175248	110.0144	0.994432	0.999973	3.07E-05
35	1.177969	110.2786	0.99682	0.999968	9.91E-06
40	1.178779	110.3572	0.997531	0.999964	5.92E-06
45	1.175979	110.0854	0.995074	0.99996	2.39E-05
50	1.175632	110.0516	0.994769	0.999955	2.69E-05
55	1.178662	110.3459	0.997428	0.999951	6.36E-06
60	1.171872	109.6866	0.991469	0.999947	7.19E-05
65	1.174713	109.9625	0.993963	0.999943	3.58E-05
70	1.176388	110.1251	0.995433	0.999939	2.03E-05
75	1.175156	110.0055	0.994351	0.999935	3.12E-05
80	1.175789	110.0669	0.994907	0.999931	2.52E-05
85	1.180648	110.5387	0.999171	0.999927	5.71E-07
90	1.174901	109.9807	0.994128	0.999923	3.36E-05
95	1.174226	109.9152	0.993535	0.999919	4.08E-05
100	1.174946	109.985	0.994167	0.999915	3.3E-05
105	1.179317	110.4095	0.998003	0.999911	3.64E-06
110	1.178542	110.3342	0.997323	0.999907	6.68E-06
115	1.18413	110.8767	1.002227	0.999904	5.4E-06
120	1.176342	110.1206	0.995392	0.9999	2.03E-05
125	1.178303	110.311	0.997113	0.999896	7.75E-06
130	1.177618	110.2445	0.996512	0.999893	1.14E-05
135	1.184078	110.8717	1.002181	0.999889	5.25E-06
140	1.173139	109.8096	0.992581	0.999886	5.34E-05
145	1.17789	110.2708	0.99675	0.999882	9.81E-06
150	1.177909	110.2727	0.996767	0.999879	9.68E-06
155	1.176552	110.141	0.995576	0.999875	1.85E-05
160	1.186253	111.0828	1.00409	0.999872	1.78E-05
165	1.176188	110.1056	0.995257	0.999868	2.13E-05
170	1.180074	110.483	0.998668	0.999865	1.43E-06
175	1.182863	110.7537	1.001115	0.999862	1.57E-06
180	1.178446	110.3249	0.997239	0.999859	6.86E-06
185	1.175982	110.0857	0.995076	0.999855	2.28E-05
190	1.178735	110.353	0.997493	0.999852	5.57E-06
195	1.179872	110.4633	0.99849	0.999849	1.85E-06
200	1.182931	110.7603	1.001174	0.999846	1.76E-06
205	1.185531	111.0128	1.003457	0.999843	1.31E-05
210	1.182026	110.6724	1.00038	0.99984	2.92E-07
215	1.183977	110.8619	1.002093	0.999837	5.09E-06
220	1.182024	110.6722	1.000378	0.999834	2.96E-07
225	1.17636	110.1224	0.995408	0.999831	1.96E-05
230	1.177909	110.2727	0.996767	0.999828	9.37E-06
235	1.182387	110.7075	1.000697	0.999825	7.61E-07
240	1.179727	110.4492	0.998362	0.999822	2.13E-06
245	1.183571	110.8225	1.001736	0.999819	3.68E-06
250	1.183943	110.8585	1.002062	0.999816	5.04E-06
255	1.19078	111.5223	1.008063	0.999814	6.8E-05
260	1.192421	111.6816	1.009502	0.999811	9.39E-05
265	1.180769	110.5504	0.999277	0.999808	2.82E-07
270	1.183078	110.7746	1.001304	0.999805	2.24E-06
275	1.183793	110.844	1.001931	0.999803	4.53E-06
280	1.184114	110.8752	1.002213	0.9998	5.82E-06
285	1.182479	110.7164	1.000778	0.999798	9.61E-07
290	1.1899	111.4369	1.007291	0.999795	5.62E-05
295	1.183729	110.8378	1.001875	0.999792	4.34E-06
300	1.190069	111.4533	1.007439	0.99979	5.85E-05
			sum=	0.001034	

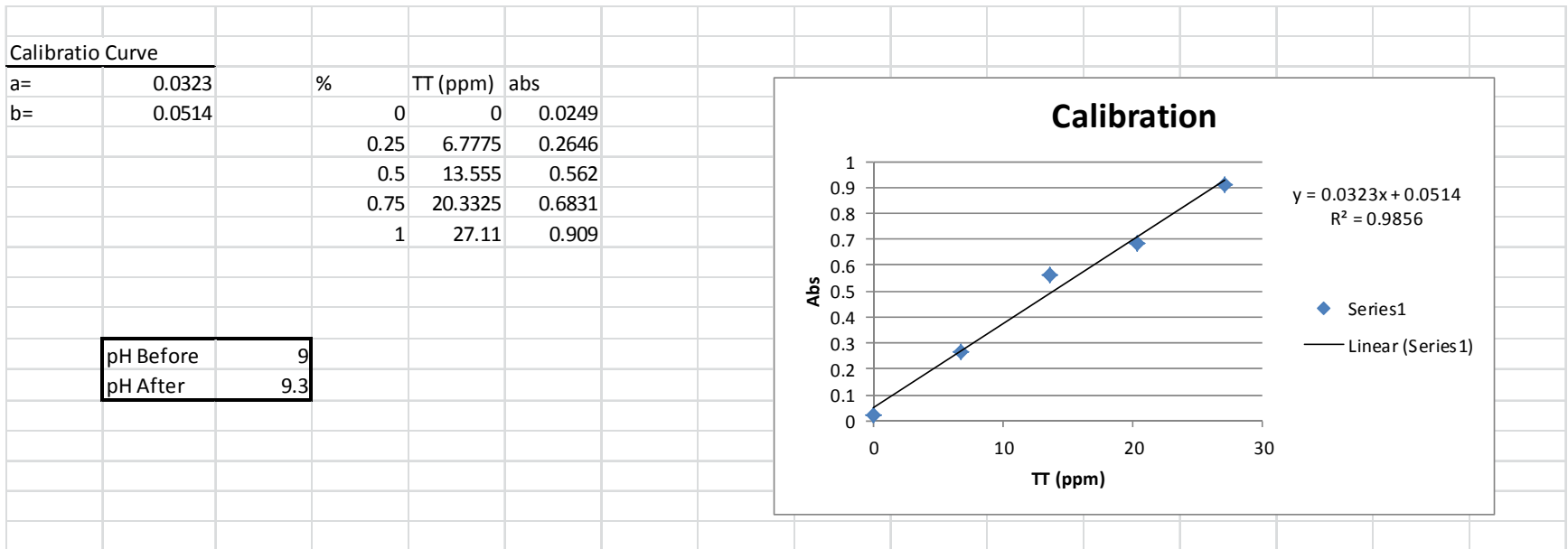


23Apr15_0.7@50%pH8					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.000749	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.163441	10.09193	1	1	0
5	1.157367	10.0374	0.994597	0.996282	2.84E-06
10	1.15644	10.02909	0.993773	0.992616	1.34E-06
15	1.152344	9.992314	0.990129	0.989002	1.27E-06
20	1.148051	9.953775	0.986311	0.985439	7.6E-07
25	1.145089	9.927192	0.983676	0.981925	3.07E-06
30	1.142747	9.906164	0.981593	0.97846	9.81E-06
35	1.139098	9.873414	0.978348	0.975045	1.09E-05
40	1.134523	9.832343	0.974278	0.971677	6.77E-06
45	1.129933	9.791144	0.970196	0.968356	3.38E-06
50	1.128852	9.78144	0.969234	0.965082	1.72E-05
55	1.124342	9.740953	0.965222	0.961853	1.13E-05
60	1.121271	9.713382	0.96249	0.95867	1.46E-05
65	1.117776	9.682013	0.959382	0.955532	1.48E-05
70	1.11552	9.661764	0.957375	0.952437	2.44E-05
75	1.111232	9.62327	0.953561	0.949386	1.74E-05
80	1.106211	9.578196	0.949095	0.946378	7.38E-06
85	1.103579	9.55457	0.946754	0.943412	1.12E-05
90	1.100689	9.528626	0.944183	0.940487	1.37E-05
95	1.098174	9.50605	0.941946	0.937604	1.89E-05
100	1.095854	9.485224	0.939882	0.934761	2.62E-05
105	1.091	9.441656	0.935565	0.931957	1.3E-05
110	1.086711	9.403147	0.931749	0.929193	6.53E-06
115	1.08444	9.382762	0.929729	0.926468	1.06E-05
120	1.081766	9.358759	0.927351	0.923781	1.27E-05
125	1.080595	9.348246	0.926309	0.921132	2.68E-05
130	1.074224	9.291056	0.920642	0.91852	4.51E-06
135	1.07242	9.274862	0.919038	0.915944	9.57E-06
140	1.069026	9.2444	0.916019	0.913405	6.84E-06
145	1.067921	9.234483	0.915037	0.910901	1.71E-05
150	1.062841	9.188875	0.910517	0.908432	4.35E-06
155	1.058944	9.153899	0.907052	0.905998	1.11E-06
160	1.059781	9.161412	0.907796	0.903598	1.76E-05
165	1.053022	9.100738	0.901784	0.901231	3.05E-07
170	1.05118	9.084197	0.900145	0.898898	1.55E-06
175	1.048702	9.061959	0.897941	0.896597	1.81E-06
180	1.045862	9.036466	0.895415	0.894329	1.18E-06
185	1.041926	9.001131	0.891914	0.892093	3.2E-08
190	1.039385	8.978321	0.889654	0.889888	5.47E-08
195	1.036104	8.948871	0.886735	0.887713	9.56E-07
200	1.03468	8.936087	0.885469	0.88557	1.02E-08
205	1.032759	8.918843	0.88376	0.883456	9.24E-08
210	1.030625	8.899687	0.881862	0.881372	2.4E-07
215	1.028037	8.876452	0.87956	0.879317	5.88E-08
220	1.023058	8.831761	0.875131	0.877291	4.67E-06
225	1.021992	8.82219	0.874183	0.875293	1.23E-06
230	1.019747	8.802035	0.872186	0.873324	1.3E-06
235	1.017038	8.777721	0.869776	0.871382	2.58E-06
240	1.013902	8.749565	0.866986	0.869467	6.15E-06
245	1.012704	8.738811	0.865921	0.867579	2.75E-06
250	1.008778	8.70357	0.862429	0.865718	1.08E-05
255	1.007712	8.694004	0.861481	0.863882	5.77E-06
260	1.006333	8.681626	0.860254	0.862072	3.31E-06
265	1.002012	8.642839	0.856411	0.860288	1.5E-05
270	1.001165	8.635236	0.855658	0.858529	8.24E-06
275	0.998898	8.61488	0.853641	0.856794	9.95E-06
280	0.996724	8.595372	0.851708	0.855084	1.14E-05
285	0.996181	8.59049	0.851224	0.853398	4.73E-06
290	0.993748	8.568655	0.84906	0.851735	7.15E-06
295	0.989932	8.534402	0.845666	0.850096	1.96E-05
300	0.987548	8.513001	0.843546	0.848479	2.43E-05
			sum=		0.000493

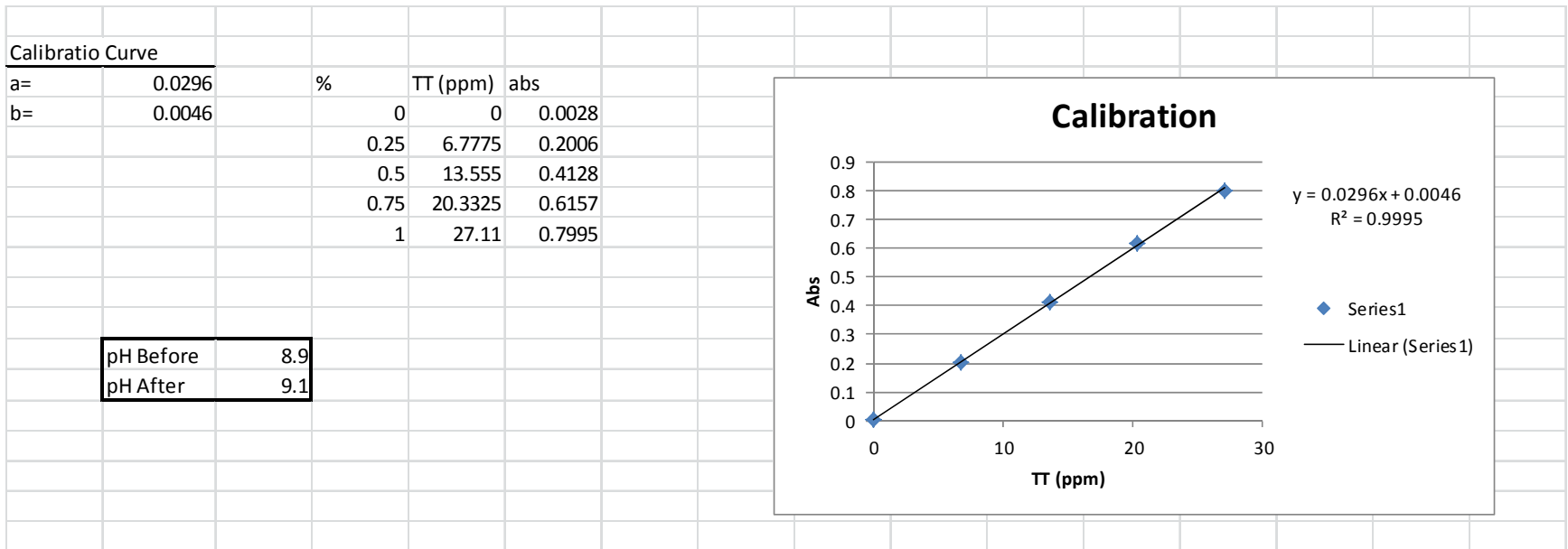




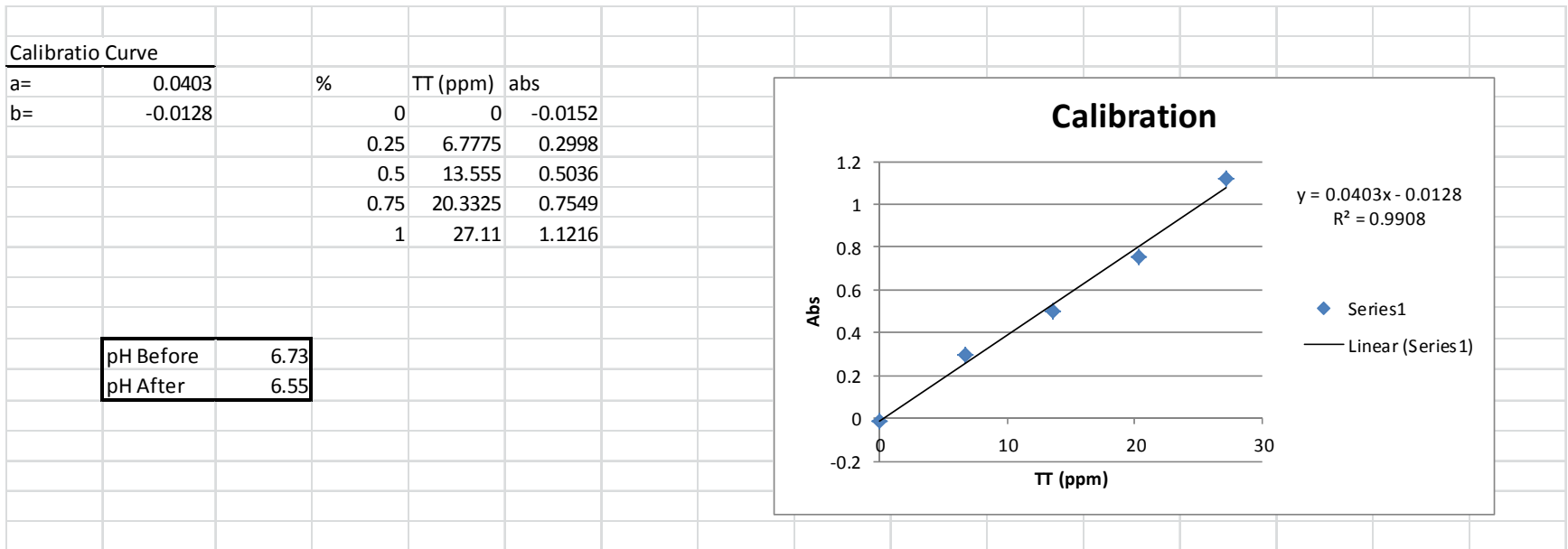
30Apr15 0.7@10%pH9					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.000102	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	0.917999	17.2315	1	1	0
5	0.91093	17.09397	0.992019	0.999494	5.59E-05
10	0.915517	17.18321	0.997198	0.998993	3.22E-06
15	0.917883	17.22925	0.999869	0.998497	1.88E-06
20	0.914883	17.17087	0.996481	0.998007	2.33E-06
25	0.911525	17.10555	0.992691	0.997523	2.33E-05
30	0.912456	17.12366	0.993741	0.997043	1.09E-05
35	0.91135	17.10215	0.992493	0.996569	1.66E-05
40	0.912496	17.12444	0.993786	0.9961	5.35E-06
45	0.912323	17.12108	0.993592	0.995636	4.18E-06
50	0.919087	17.25267	1.001228	0.995176	3.66E-05
55	0.912346	17.12152	0.993617	0.994722	1.22E-06
60	0.911024	17.09579	0.992124	0.994273	4.62E-06
65	0.909952	17.07495	0.990915	0.993829	8.49E-06
70	0.91444	17.16227	0.995982	0.993389	6.72E-06
75	0.916056	17.1937	0.997806	0.992955	2.35E-05
80	0.913786	17.14954	0.995243	0.992525	7.39E-06
85	0.908811	17.05275	0.989626	0.992099	6.11E-06
90	0.919094	17.2528	1.001236	0.991678	9.13E-05
95	0.911878	17.11241	0.993088	0.991262	3.34E-06
100	0.914829	17.16982	0.99642	0.99085	3.1E-05
105	0.916524	17.2028	0.998334	0.990443	6.23E-05
110	0.907497	17.02718	0.988142	0.99004	3.6E-06
115	0.914149	17.1566	0.995653	0.989642	3.61E-05
120	0.902724	16.93432	0.982753	0.989247	4.22E-05
125	0.907532	17.02785	0.988181	0.988858	4.57E-07
130	0.89766	16.83579	0.977036	0.988472	0.000131
135	0.906788	17.01338	0.987341	0.98809	5.61E-07
140	0.90436	16.96615	0.984601	0.987713	9.69E-06
145	0.901439	16.90932	0.981303	0.98734	3.64E-05
150	0.903564	16.95066	0.983702	0.98697	1.07E-05
155	0.903146	16.94252	0.983229	0.986605	1.14E-05
160	0.903619	16.95173	0.983764	0.986244	6.15E-06
165	0.903204	16.94365	0.983295	0.985886	6.71E-06
170	0.910728	17.09003	0.99179	0.985533	3.92E-05
175	0.91021	17.07995	0.991205	0.985183	3.63E-05
180	0.900486	16.89077	0.980226	0.984837	2.13E-05
185	0.903788	16.95502	0.983955	0.984495	2.92E-07
190	0.902815	16.93609	0.982856	0.984156	1.69E-06
195	0.902958	16.93888	0.983018	0.983821	6.46E-07
200	0.902247	16.92504	0.982215	0.98349	1.63E-06
205	0.909699	17.07002	0.990629	0.983163	5.57E-05
210	0.910978	17.09491	0.992073	0.982839	8.53E-05
215	0.90113	16.90331	0.980954	0.982518	2.45E-06
220	0.909079	17.05796	0.989928	0.982201	5.97E-05
225	0.90572	16.9926	0.986136	0.981887	1.8E-05
230	0.905792	16.994	0.986217	0.981577	2.15E-05
235	0.89817	16.84572	0.977612	0.98127	1.34E-05
240	0.898757	16.85714	0.978275	0.980966	7.25E-06
245	0.903272	16.94498	0.983372	0.980666	7.32E-06
250	0.89654	16.814	0.975771	0.980369	2.11E-05
255	0.897415	16.83103	0.976759	0.980075	1.1E-05
260	0.899652	16.87455	0.979285	0.979785	2.5E-07
265	0.904291	16.9648	0.984522	0.979497	2.53E-05
270	0.897824	16.83899	0.977221	0.979213	3.97E-06
275	0.899576	16.87307	0.979199	0.978931	7.15E-08
280	0.897826	16.83902	0.977223	0.978653	2.05E-06
285	0.897286	16.82852	0.976614	0.978378	3.11E-06
290	0.895888	16.80131	0.975035	0.978106	9.43E-06
295	0.897405	16.83083	0.976748	0.977836	1.19E-06
300	0.896698	16.81708	0.97595	0.97757	2.62E-06
				sum=	0.001153



7May15_0.7@50%pH9					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.000338	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	0.831617	174.3514	1	1	0
5	0.84202	176.613	1.012971	0.99832	0.000215
10	0.842645	176.7488	1.01375	0.99666	0.000292
15	0.832887	174.6276	1.001584	0.99502	4.31E-05
20	0.832964	174.6443	1.001679	0.9934	6.85E-05
25	0.838111	175.7632	1.008097	0.9918	0.000266
30	0.829065	173.7967	0.996818	0.990218	4.36E-05
35	0.828973	173.7768	0.996704	0.988655	6.48E-05
40	0.83472	175.0261	1.00387	0.987111	0.000281
45	0.826132	173.1591	0.993161	0.985586	5.74E-05
50	0.826396	173.2164	0.99349	0.984079	8.86E-05
55	0.820385	171.9098	0.985996	0.98259	1.16E-05
60	0.815865	170.9272	0.98036	0.981119	5.76E-07
65	0.813493	170.4116	0.977403	0.979665	5.12E-06
70	0.808753	169.381	0.971492	0.978229	4.54E-05
75	0.80711	169.0239	0.969443	0.976811	5.43E-05
80	0.806122	168.8091	0.968211	0.975409	5.18E-05
85	0.805845	168.749	0.967867	0.974024	3.79E-05
90	0.801495	167.8033	0.962443	0.972655	0.000104
95	0.802055	167.9251	0.963141	0.971303	6.66E-05
100	0.80406	168.3608	0.96564	0.969967	1.87E-05
105	0.796428	166.7018	0.956125	0.968648	0.000157
110	0.798641	167.1828	0.958884	0.967344	7.16E-05
115	0.789287	165.1493	0.94722	0.966055	0.000355
120	0.789447	165.1841	0.947421	0.964782	0.000301
125	0.79586	166.5783	0.955417	0.963525	6.57E-05
130	0.789275	165.1467	0.947206	0.962282	0.000227
135	0.78418	164.0392	0.940854	0.961055	0.000408
140	0.778392	162.7809	0.933637	0.959842	0.000687
145	0.778819	162.8737	0.934169	0.958643	0.000599
150	0.780135	163.1597	0.935809	0.957459	0.000469
155	0.780351	163.2068	0.93608	0.95629	0.000408
160	0.786902	164.6308	0.944247	0.955134	0.000119
165	0.789195	165.1294	0.947107	0.953992	4.74E-05
170	0.786163	164.4703	0.943326	0.952864	9.1E-05
175	0.792375	165.8206	0.951071	0.951749	4.6E-07
180	0.787412	164.7418	0.944883	0.950648	3.32E-05
185	0.790023	165.3094	0.948139	0.94956	2.02E-06
190	0.789488	165.1932	0.947472	0.948485	1.02E-06
195	0.78637	164.5152	0.943584	0.947422	1.47E-05
200	0.782832	163.7462	0.939173	0.946373	5.18E-05
205	0.785397	164.3037	0.942371	0.945336	8.79E-06
210	0.777221	162.5264	0.932177	0.944312	0.000147
215	0.781429	163.4412	0.937424	0.9433	3.45E-05
220	0.782526	163.6796	0.938791	0.942299	1.23E-05
225	0.776754	162.4247	0.931594	0.941311	9.44E-05
230	0.787476	164.7556	0.944962	0.940335	2.14E-05
235	0.781087	163.3666	0.936996	0.939371	5.64E-06
240	0.781366	163.4273	0.937344	0.938418	1.15E-06
245	0.778688	162.8452	0.934006	0.937476	1.2E-05
250	0.786374	164.5161	0.943589	0.936546	4.96E-05
255	0.789409	165.1759	0.947373	0.935627	0.000138
260	0.78613	164.4631	0.943285	0.934719	7.34E-05
265	0.784553	164.1203	0.941319	0.933822	5.62E-05
270	0.780011	163.1329	0.935655	0.932936	7.4E-06
275	0.784596	164.1296	0.941372	0.93206	8.67E-05
280	0.777181	162.5177	0.932127	0.931195	8.69E-07
285	0.77647	162.363	0.93124	0.93034	8.09E-07
290	0.811274	169.9292	0.974636	0.929495	0.002038
295	0.807501	169.109	0.969931	0.928661	0.001703
300	0.807986	169.2143	0.970536	0.927836	0.001823
			sum=		0.012239

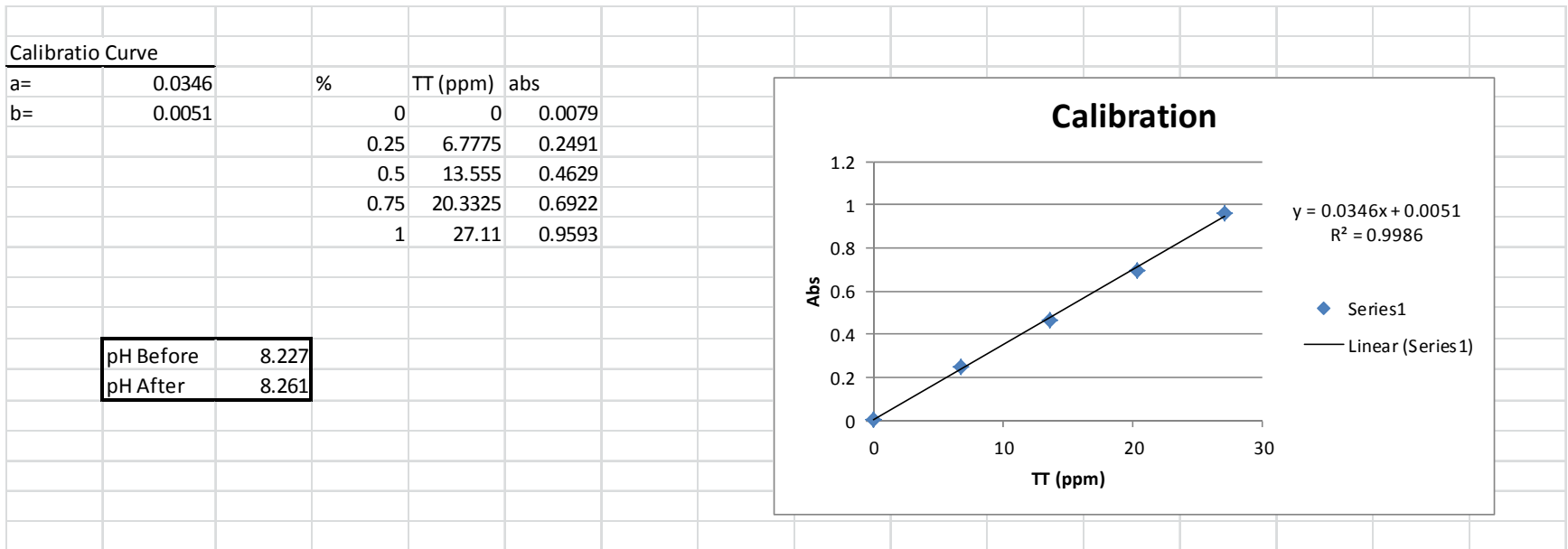


14May15 0.7@0%pH6					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	-3.5E-05	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.067307	-80.2349	1	1	0
5	1.075663	-80.8877	1.008136	1.000175	6.34E-05
10	1.06854	-80.3313	1.001201	1.000348	7.28E-07
15	1.071965	-80.5988	1.004536	1.000519	1.61E-05
20	1.070237	-80.4639	1.002854	1.000689	4.69E-06
25	1.069017	-80.3685	1.001666	1.000857	6.55E-07
30	1.068715	-80.3449	1.001371	1.001023	1.22E-07
35	1.067133	-80.2213	0.999831	1.001187	1.84E-06
40	1.069244	-80.3862	1.001886	1.00135	2.88E-07
45	1.063183	-79.9128	0.995985	1.001511	3.05E-05
50	1.068229	-80.307	1.000898	1.00167	5.96E-07
55	1.06805	-80.293	1.000724	1.001828	1.22E-06
60	1.066193	-80.1479	0.998915	1.001985	9.42E-06
65	1.070647	-80.4958	1.003252	1.002139	1.24E-06
70	1.068957	-80.3639	1.001608	1.002292	4.69E-07
75	1.071978	-80.5998	1.004548	1.002444	4.43E-06
80	1.0742	-80.7734	1.006712	1.002594	1.7E-05
85	1.076112	-80.9228	1.008574	1.002742	3.4E-05
90	1.068495	-80.3277	1.001157	1.002889	3E-06
95	1.068788	-80.3506	1.001442	1.003035	2.54E-06
100	1.06985	-80.4336	1.002476	1.003179	4.94E-07
105	1.068962	-80.3642	1.001612	1.003321	2.92E-06
110	1.068697	-80.3435	1.001354	1.003463	4.45E-06
115	1.070105	-80.4535	1.002725	1.003602	7.7E-07
120	1.068427	-80.3224	1.001091	1.003741	7.02E-06
125	1.075668	-80.8881	1.008141	1.003877	1.82E-05
130	1.070995	-80.523	1.003591	1.004013	1.78E-07
135	1.06969	-80.4211	1.002321	1.004147	3.33E-06
140	1.072817	-80.6654	1.005366	1.00428	1.18E-06
145	1.078577	-81.1154	1.010974	1.004411	4.31E-05
150	1.07001	-80.4461	1.002633	1.004541	3.64E-06
155	1.072011	-80.6024	1.004581	1.00467	7.96E-09
160	1.067944	-80.2847	1.000621	1.004797	1.74E-05
165	1.072309	-80.6257	1.004871	1.004923	2.72E-09
170	1.06957	-80.4117	1.002204	1.005048	8.09E-06
175	1.068949	-80.3632	1.001599	1.005172	1.28E-05
180	1.074089	-80.7648	1.006604	1.005294	1.72E-06
185	1.074581	-80.8032	1.007084	1.005415	2.78E-06
190	1.072225	-80.6191	1.004789	1.005535	5.57E-07
195	1.072863	-80.669	1.00541	1.005654	5.92E-08
200	1.079654	-81.1995	1.012023	1.005771	3.91E-05
205	1.070155	-80.4574	1.002773	1.005888	9.7E-06
210	1.073519	-80.7202	1.006049	1.006003	2.14E-09
215	1.073367	-80.7084	1.005902	1.006117	4.62E-08
220	1.073239	-80.6984	1.005777	1.006229	2.05E-07
225	1.07298	-80.6781	1.005524	1.006341	6.67E-07
230	1.078627	-81.1193	1.011022	1.006451	2.09E-05
235	1.072991	-80.679	1.005535	1.006561	1.05E-06
240	1.076036	-80.9169	1.0085	1.006669	3.35E-06
245	1.073729	-80.7367	1.006254	1.006776	2.73E-07
250	1.075669	-80.8882	1.008143	1.006882	1.59E-06
255	1.075588	-80.8818	1.008063	1.006987	1.16E-06
260	1.076295	-80.9371	1.008752	1.007091	2.76E-06
265	1.073183	-80.694	1.005722	1.007194	2.17E-06
270	1.075346	-80.8629	1.007828	1.007296	2.83E-07
275	1.075895	-80.9058	1.008362	1.007397	9.32E-07
280	1.073749	-80.7382	1.006273	1.007496	1.5E-06
285	1.073213	-80.6963	1.005751	1.007595	3.4E-06
290	1.074675	-80.8106	1.007175	1.007693	2.68E-07
295	1.074801	-80.8204	1.007298	1.00779	2.42E-07
300	1.074252	-80.7775	1.006763	1.007885	1.26E-06
			sum=	0.000412	

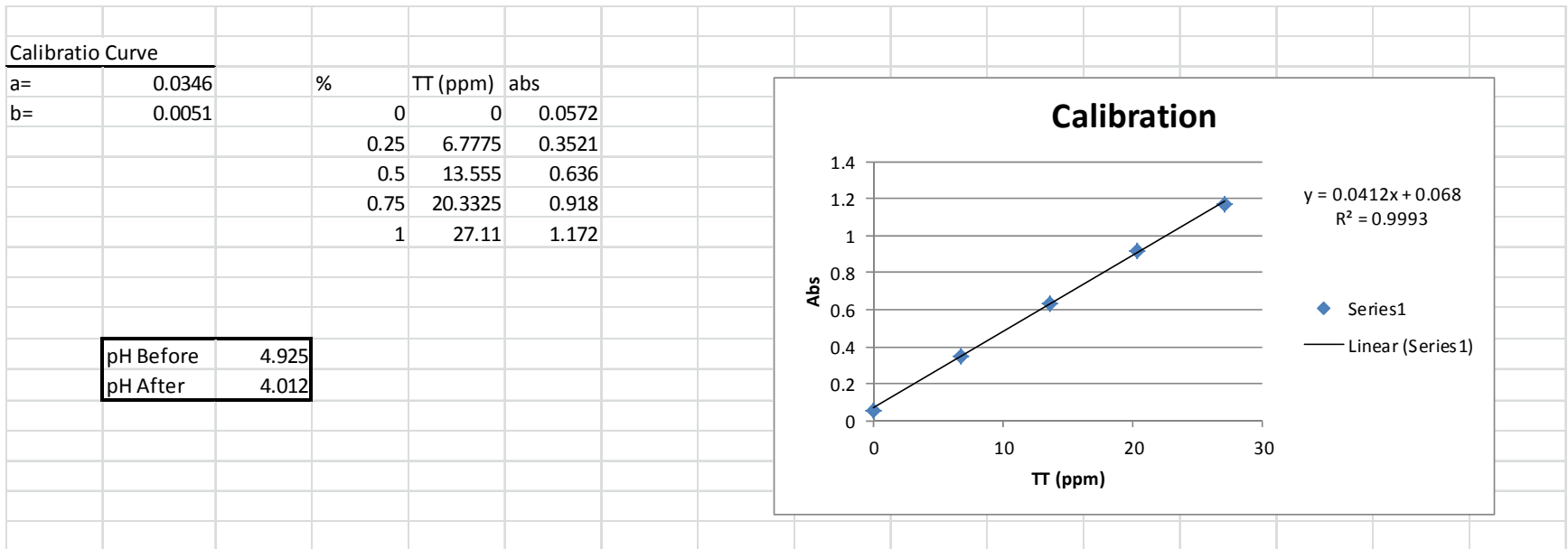


27May15_0.7@10%pH8					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	8.85E-05	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	0.954391	180.3512	1	1	0
5	0.960247	181.4995	1.006367	0.99956	4.63E-05
10	0.951523	179.7889	0.996882	0.999125	5.03E-06
15	0.951064	179.6988	0.996383	0.998694	5.34E-06
20	0.956796	180.8227	1.002614	0.998268	1.89E-05
25	0.947339	178.9684	0.992333	0.997847	3.04E-05
30	0.95117	179.7195	0.996498	0.99743	8.69E-07
35	0.948684	179.2321	0.993795	0.997018	1.04E-05
40	0.949842	179.4592	0.995054	0.99661	2.42E-06
45	0.955585	180.5853	1.001298	0.996206	2.59E-05
50	0.955684	180.6047	1.001406	0.995807	3.13E-05
55	0.948242	179.1455	0.993315	0.995412	4.4E-06
60	0.945163	178.5417	0.989967	0.995022	2.55E-05
65	0.945949	178.696	0.990822	0.994635	1.45E-05
70	0.946747	178.8523	0.991689	0.994253	6.57E-06
75	0.951341	179.7532	0.996684	0.993875	7.89E-06
80	0.948099	179.1174	0.993159	0.993501	1.17E-07
85	0.948485	179.1932	0.993579	0.993131	2.01E-07
90	0.946424	178.7891	0.991339	0.992765	2.03E-06
95	0.950032	179.4964	0.995261	0.992403	8.17E-06
100	0.946313	178.7672	0.991217	0.992044	6.84E-07
105	0.949449	179.3823	0.994628	0.99169	8.63E-06
110	0.943716	178.2579	0.988394	0.991339	8.68E-06
115	0.945153	178.5399	0.989957	0.990993	1.07E-06
120	0.94555	178.6176	0.990388	0.990649	6.85E-08
125	0.946674	178.838	0.99161	0.99031	1.69E-06
130	0.946914	178.885	0.991871	0.989974	3.6E-06
135	0.948797	179.2543	0.993918	0.989642	1.83E-05
140	0.941533	177.83	0.986021	0.989314	1.08E-05
145	0.942777	178.0738	0.987373	0.988989	2.61E-06
150	0.941898	177.9016	0.986418	0.988667	5.06E-06
155	0.940724	177.6713	0.985141	0.988349	1.03E-05
160	0.948396	179.1758	0.993483	0.988034	2.97E-05
165	0.94922	179.3372	0.994378	0.987723	4.43E-05
170	0.940928	177.7114	0.985363	0.987415	4.21E-06
175	0.948106	179.1188	0.993167	0.987111	3.67E-05
180	0.944371	178.3864	0.989106	0.986809	5.27E-06
185	0.940503	177.628	0.984901	0.986511	2.59E-06
190	0.947555	179.0107	0.992567	0.986216	4.03E-05
195	0.948292	179.1553	0.993369	0.985925	5.54E-05
200	0.938785	177.2912	0.983033	0.985636	6.77E-06
205	0.93964	177.4588	0.983963	0.985351	1.93E-06
210	0.936241	176.7924	0.980268	0.985068	2.3E-05
215	0.936272	176.7984	0.980301	0.984789	2.01E-05
220	0.93988	177.5059	0.984224	0.984513	8.35E-08
225	0.936241	176.7923	0.980267	0.984239	1.58E-05
230	0.936244	176.7929	0.98027	0.983969	1.37E-05
235	0.936132	176.771	0.980149	0.983701	1.26E-05
240	0.937732	177.0847	0.981888	0.983437	2.4E-06
245	0.935742	176.6945	0.979725	0.983175	1.19E-05
250	0.935584	176.6635	0.979553	0.982916	1.13E-05
255	0.939603	177.4516	0.983923	0.98266	1.6E-06
260	0.941106	177.7463	0.985557	0.982406	9.93E-06
265	0.941196	177.7639	0.985654	0.982156	1.22E-05
270	0.938645	177.2637	0.982881	0.981908	9.48E-07
275	0.938668	177.2682	0.982906	0.981662	1.55E-06
280	0.935474	176.6419	0.979433	0.98142	3.95E-06
285	0.939529	177.4371	0.983842	0.981179	7.09E-06
290	0.936802	176.9024	0.980878	0.980942	4.12E-09
295	0.930882	175.7416	0.974441	0.980707	3.93E-05
300	0.942672	178.0533	0.987259	0.980475	4.6E-05
				sum=	0.000779

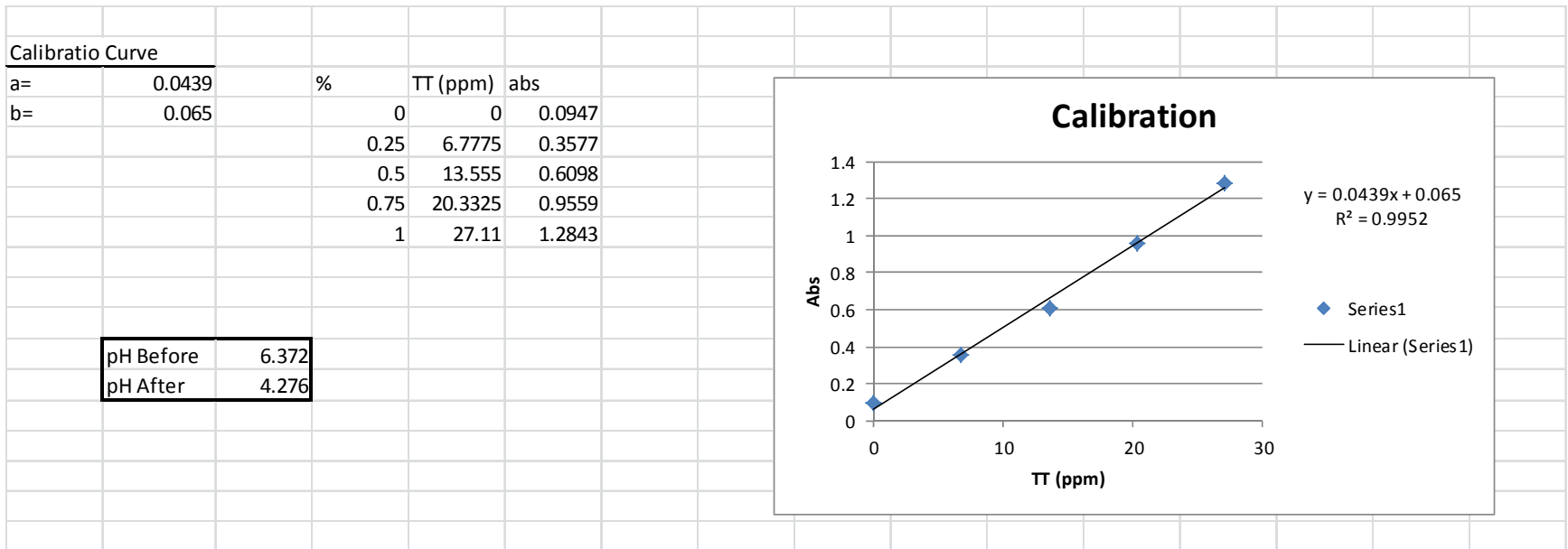




29May15_0.7@70%pH5					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.001262	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.160983	220.8594	1	1	0
5	1.154205	219.5305	0.993983	0.99374	5.88E-08
10	1.145808	217.8838	0.986527	0.987585	1.12E-06
15	1.140991	216.9395	0.982251	0.98153	5.2E-07
20	1.131695	215.1167	0.973998	0.975577	2.49E-06
25	1.128502	214.4906	0.971164	0.969721	2.08E-06
30	1.120145	212.852	0.963745	0.963963	4.76E-08
35	1.114923	211.828	0.959108	0.958299	6.53E-07
40	1.111939	211.2429	0.956459	0.95273	1.39E-05
45	1.102673	209.4261	0.948233	0.947253	9.6E-07
50	1.098922	208.6905	0.944902	0.941866	9.22E-06
55	1.098939	208.694	0.944918	0.936568	6.97E-05
60	1.09135	207.2058	0.93818	0.931358	4.65E-05
65	1.083879	205.741	0.931548	0.926235	2.82E-05
70	1.076443	204.2829	0.924946	0.921196	1.41E-05
75	1.072543	203.5183	0.921483	0.91624	2.75E-05
80	1.07262	203.5334	0.921552	0.911367	0.000104
85	1.061137	201.2818	0.911357	0.906574	2.29E-05
90	1.060725	201.2011	0.910992	0.90186	8.34E-05
95	1.053288	199.7427	0.904388	0.897225	5.13E-05
100	1.04365	197.8529	0.895832	0.892666	1E-05
105	1.044113	197.9438	0.896243	0.888182	6.5E-05
110	1.034765	196.1107	0.887944	0.883773	1.74E-05
115	1.032909	195.7469	0.886297	0.879437	4.71E-05
120	1.028372	194.8572	0.882268	0.875172	5.04E-05
125	1.024557	194.1091	0.878881	0.870978	6.25E-05
130	1.020765	193.3657	0.875515	0.866853	7.5E-05
135	1.014196	192.0776	0.869683	0.862797	4.74E-05
140	1.007951	190.853	0.864138	0.858808	2.84E-05
145	1.000481	189.3884	0.857507	0.854885	6.88E-06
150	0.998651	189.0296	0.855882	0.851026	2.36E-05
155	0.994341	188.1845	0.852056	0.847232	2.33E-05
160	0.990566	187.4443	0.848704	0.8435	2.71E-05
165	0.984463	186.2476	0.843286	0.83983	1.19E-05
170	0.979942	185.3611	0.839272	0.836221	9.31E-06
175	0.976622	184.7102	0.836325	0.832672	1.33E-05
180	0.972282	183.8591	0.832471	0.829181	1.08E-05
185	0.971034	183.6145	0.831364	0.825748	3.15E-05
190	0.961597	181.7641	0.822985	0.822372	3.77E-07
195	0.960708	181.5897	0.822196	0.819051	9.89E-06
200	0.954243	180.3221	0.816456	0.815786	4.5E-07
205	0.956462	180.7573	0.818427	0.812575	3.43E-05
210	0.94575	178.6568	0.808916	0.809416	2.5E-07
215	0.940967	177.7189	0.80467	0.80631	2.69E-06
220	0.93884	177.302	0.802782	0.803256	2.24E-07
225	0.933369	176.2293	0.797925	0.800252	5.41E-06
230	0.930589	175.6841	0.795457	0.797298	3.39E-06
235	0.930522	175.6711	0.795398	0.794392	1.01E-06
240	0.922535	174.1049	0.788307	0.791535	1.04E-05
245	0.917738	173.1643	0.784048	0.788725	2.19E-05
250	0.913876	172.4071	0.780619	0.785961	2.85E-05
255	0.910071	171.6611	0.777241	0.783243	3.6E-05
260	0.909049	171.4606	0.776334	0.78057	1.79E-05
265	0.900861	169.855	0.769064	0.777942	7.88E-05
270	0.898508	169.3937	0.766975	0.775357	7.02E-05
275	0.89489	168.6843	0.763763	0.772814	8.19E-05
280	0.894082	168.5259	0.763046	0.770314	5.28E-05
285	0.888591	167.4493	0.758172	0.767855	9.38E-05
290	0.886469	167.0332	0.756287	0.765437	8.37E-05
295	0.884531	166.6532	0.754567	0.763059	7.21E-05
300	0.881258	166.0113	0.751661	0.76072	8.21E-05
			sum=		0.001828



1Jun15_0.7@70%pH6					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.001235	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.266443	18.80835	1	1	0
5	1.259549	18.7023	0.994361	0.993878	2.34E-07
10	1.254731	18.62817	0.99042	0.987856	6.57E-06
15	1.239044	18.38683	0.977589	0.981933	1.89E-05
20	1.228587	18.22595	0.969035	0.976107	5E-05
25	1.219862	18.09172	0.961899	0.970377	7.19E-05
30	1.225991	18.18602	0.966912	0.964741	4.71E-06
35	1.21754	18.05599	0.959999	0.959197	6.42E-07
40	1.207736	17.90517	0.95198	0.953745	3.12E-06
45	1.202866	17.83025	0.947996	0.948382	1.49E-07
50	1.19635	17.73	0.942667	0.943107	1.94E-07
55	1.189701	17.62771	0.937228	0.937918	4.76E-07
60	1.183463	17.53173	0.932125	0.932815	4.76E-07
65	1.183312	17.52941	0.932002	0.927795	1.77E-05
70	1.174539	17.39445	0.924826	0.922858	3.87E-06
75	1.172568	17.36412	0.923213	0.918001	2.72E-05
80	1.16328	17.22122	0.915616	0.913225	5.72E-06
85	1.155836	17.10671	0.909528	0.908526	1E-06
90	1.156321	17.11416	0.909924	0.903905	3.62E-05
95	1.154088	17.07982	0.908098	0.89936	7.63E-05
100	1.149046	17.00224	0.903973	0.894889	8.25E-05
105	1.135931	16.80047	0.893245	0.890492	7.58E-06
110	1.130963	16.72405	0.889182	0.886167	9.09E-06
115	1.128831	16.69125	0.887438	0.881913	3.05E-05
120	1.122548	16.59458	0.882298	0.877728	2.09E-05
125	1.123443	16.60836	0.883031	0.873613	8.87E-05
130	1.114004	16.46315	0.87531	0.869564	3.3E-05
135	1.107829	16.36814	0.870259	0.865583	2.19E-05
140	1.110062	16.40249	0.872085	0.861666	0.000109
145	1.098321	16.22186	0.862482	0.857814	2.18E-05
150	1.096442	16.19295	0.860945	0.854025	4.79E-05
155	1.089032	16.07896	0.854884	0.850299	2.1E-05
160	1.089471	16.0857	0.855243	0.846633	7.41E-05
165	1.081205	15.95855	0.848482	0.843028	2.98E-05
170	1.077924	15.90807	0.845798	0.839481	3.99E-05
175	1.070823	15.79881	0.839989	0.835993	1.6E-05
180	1.064751	15.7054	0.835023	0.832562	6.05E-06
185	1.067039	15.74061	0.836895	0.829188	5.94E-05
190	1.057501	15.59386	0.829092	0.825869	1.04E-05
195	1.051362	15.49941	0.824071	0.822604	2.15E-06
200	1.04591	15.41553	0.819611	0.819393	4.76E-08
205	1.048769	15.45953	0.82195	0.816235	3.27E-05
210	1.036677	15.27349	0.812059	0.813128	1.14E-06
215	1.040371	15.33032	0.81508	0.810072	2.51E-05
220	1.034436	15.23902	0.810226	0.807067	9.98E-06
225	1.025826	15.10655	0.803183	0.804111	8.61E-07
230	1.019902	15.01541	0.798338	0.801203	8.21E-06
235	1.022951	15.06233	0.800832	0.798343	6.19E-06
240	1.018177	14.98887	0.796926	0.79553	1.95E-06
245	1.006435	14.80823	0.787322	0.792764	2.96E-05
250	1.008077	14.83349	0.788665	0.790042	1.9E-06
255	1.003735	14.76669	0.785114	0.787365	5.07E-06
260	0.998358	14.68396	0.780715	0.784733	1.61E-05
265	0.988277	14.52887	0.772469	0.782143	9.36E-05
270	0.987639	14.51907	0.771948	0.779596	5.85E-05
275	0.980316	14.4064	0.765958	0.777091	0.000124
280	0.982002	14.43233	0.767336	0.774626	5.31E-05
285	0.971037	14.26364	0.758368	0.772203	0.000191
290	0.971818	14.27567	0.759007	0.769819	0.000117
295	0.968982	14.23202	0.756686	0.767474	0.000116
300	0.965056	14.17163	0.753476	0.765167	0.000137
			sum=		0.002086



3Jun15 0.7@30%pH7					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.000423	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.261515	15.2963	1	1	0
5	1.268404	15.38274	1.005651	0.9979	6.01E-05
10	1.260961	15.28935	0.999546	0.995827	1.38E-05
15	1.259369	15.26937	0.998239	0.993779	1.99E-05
20	1.253829	15.19986	0.993695	0.991756	3.76E-06
25	1.260094	15.27847	0.998834	0.989759	8.24E-05
30	1.249113	15.14069	0.989827	0.987786	4.16E-06
35	1.247889	15.12533	0.988823	0.985838	8.91E-06
40	1.24284	15.06198	0.984681	0.983914	5.88E-07
45	1.240308	15.03021	0.982604	0.982014	3.48E-07
50	1.238479	15.00726	0.981104	0.980137	9.34E-07
55	1.237374	14.9934	0.980197	0.978284	3.66E-06
60	1.232355	14.93043	0.976081	0.976454	1.39E-07
65	1.234287	14.95466	0.977665	0.974646	9.11E-06
70	1.227262	14.86652	0.971903	0.972861	9.18E-07
75	1.227919	14.87477	0.972442	0.971098	1.81E-06
80	1.225893	14.84935	0.97078	0.969357	2.03E-06
85	1.229008	14.88844	0.973336	0.967638	3.25E-05
90	1.222734	14.80971	0.968189	0.96594	5.06E-06
95	1.221057	14.78867	0.966813	0.964263	6.51E-06
100	1.220366	14.78	0.966247	0.962606	1.33E-05
105	1.215819	14.72295	0.962517	0.960971	2.39E-06
110	1.208148	14.6267	0.956224	0.959355	9.8E-06
115	1.214183	14.70243	0.961175	0.95776	1.17E-05
120	1.214224	14.70294	0.961209	0.956184	2.52E-05
125	1.20431	14.57854	0.953076	0.954628	2.41E-06
130	1.202985	14.56192	0.951989	0.953092	1.21E-06
135	1.201988	14.54941	0.951171	0.951574	1.62E-07
140	1.198615	14.50708	0.948405	0.950075	2.79E-06
145	1.205065	14.58801	0.953695	0.948595	2.6E-05
150	1.19796	14.49887	0.947867	0.947133	5.39E-07
155	1.193979	14.44892	0.944602	0.945689	1.18E-06
160	1.200062	14.52525	0.949592	0.944264	2.84E-05
165	1.190423	14.40431	0.941685	0.942855	1.37E-06
170	1.193357	14.44112	0.944092	0.941465	6.9E-06
175	1.187998	14.37387	0.939696	0.940091	1.57E-07
180	1.182836	14.30911	0.935462	0.938735	1.07E-05
185	1.191449	14.41718	0.942527	0.937396	2.63E-05
190	1.182214	14.3013	0.934952	0.936073	1.26E-06
195	1.178614	14.25613	0.931998	0.934766	7.66E-06
200	1.17855	14.25534	0.931947	0.933476	2.34E-06
205	1.182685	14.30721	0.935338	0.932202	9.83E-06
210	1.175522	14.21734	0.929463	0.930943	2.19E-06
215	1.175078	14.21177	0.929098	0.929701	3.63E-07
220	1.172473	14.17908	0.926961	0.928473	2.29E-06
225	1.169183	14.1378	0.924262	0.927261	8.99E-06
230	1.171029	14.16096	0.925777	0.926064	8.25E-08
235	1.173138	14.18743	0.927507	0.924882	6.89E-06
240	1.17416	14.20026	0.928346	0.923714	2.15E-05
245	1.172227	14.17599	0.92676	0.922561	1.76E-05
250	1.165011	14.08546	0.920841	0.921422	3.38E-07
255	1.165853	14.09603	0.921532	0.920297	1.52E-06
260	1.157064	13.98575	0.914322	0.919187	2.37E-05
265	1.154284	13.95086	0.912041	0.91809	3.66E-05
270	1.156654	13.9806	0.913986	0.917007	9.12E-06
275	1.152421	13.92749	0.910513	0.915937	2.94E-05
280	1.15929	14.01368	0.916148	0.91488	1.61E-06
285	1.150468	13.90299	0.908912	0.913837	2.43E-05
290	1.158249	14.00061	0.915294	0.912806	6.19E-06
295	1.147096	13.86068	0.906146	0.911788	3.18E-05
300	1.154363	13.95186	0.912107	0.910783	1.75E-06
			sum=		0.000674

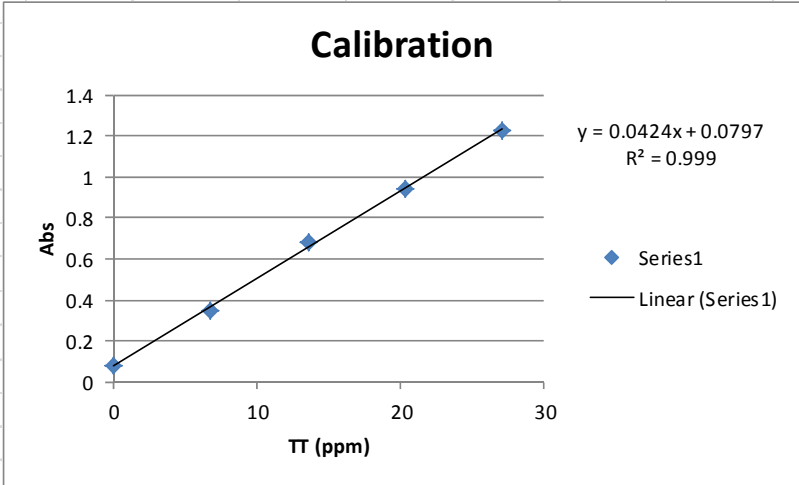
Calibratio Curve				
a=	0.0424	%	TT (ppm)	abs
b=	0.0797	0	0	0.0803
		0.25	6.7775	0.3513
		0.5	13.555	0.6779
		0.75	20.3325	0.9423
		1	27.11	1.223

pH Before	7.144
pH After	7.017

Notes: Took averages b/c better R<sup>2</sup>, pH aren't exact, rough estimate because I can't remember the exact numbers right now.



9Jun15_0.7@20%pH6					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.000356	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.177414	18.97682	1	1	0
5	1.175257	18.94075	0.998099	0.998228	1.67E-08
10	1.17346	18.9107	0.996516	0.996478	1.42E-09
15	1.173255	18.90728	0.996336	0.994749	2.52E-06
20	1.168647	18.83022	0.992275	0.993041	5.87E-07
25	1.169631	18.84667	0.993142	0.991353	3.2E-06
30	1.168131	18.82158	0.99182	0.989686	4.55E-06
35	1.169237	18.84008	0.992795	0.988039	2.26E-05
40	1.16988	18.85084	0.993361	0.986412	4.83E-05
45	1.160781	18.69868	0.985343	0.984804	2.91E-07
50	1.160818	18.6993	0.985376	0.983216	4.66E-06
55	1.158585	18.66195	0.983408	0.981647	3.1E-06
60	1.155749	18.61453	0.980909	0.980097	6.58E-07
65	1.162072	18.72027	0.986481	0.978566	6.26E-05
70	1.154804	18.59873	0.980076	0.977054	9.14E-06
75	1.152028	18.55231	0.97763	0.975559	4.29E-06
80	1.150214	18.52198	0.976032	0.974083	3.8E-06
85	1.147971	18.48447	0.974055	0.972624	2.05E-06
90	1.144944	18.43385	0.971388	0.971183	4.18E-08
95	1.142822	18.39837	0.969518	0.96976	5.85E-08
100	1.141644	18.37866	0.96848	0.968354	1.59E-08
105	1.14277	18.3975	0.969472	0.966964	6.29E-06
110	1.138524	18.32649	0.96573	0.965592	1.92E-08
115	1.138337	18.32336	0.965565	0.964236	1.77E-06
120	1.136058	18.28524	0.963557	0.962896	4.36E-07
125	1.133991	18.25069	0.961736	0.961573	2.65E-08
130	1.132048	18.21819	0.960024	0.960266	5.86E-08
135	1.13169	18.21221	0.959708	0.958974	5.39E-07
140	1.130828	18.19779	0.958948	0.957698	1.56E-06
145	1.129858	18.18158	0.958094	0.956437	2.74E-06
150	1.126851	18.13129	0.955444	0.955192	6.33E-08
155	1.12735	18.13963	0.955884	0.953962	3.69E-06
160	1.12455	18.09281	0.953417	0.952746	4.49E-07
165	1.122416	18.05712	0.951536	0.951546	9.92E-11
170	1.122586	18.05996	0.951685	0.950359	1.76E-06
175	1.121398	18.04011	0.950639	0.949188	2.11E-06
180	1.119646	18.01081	0.949095	0.94803	1.13E-06
185	1.117607	17.97671	0.947299	0.946886	1.7E-07
190	1.115129	17.93527	0.945115	0.945756	4.11E-07
195	1.117739	17.97891	0.947415	0.94464	7.7E-06
200	1.114904	17.93151	0.944916	0.943537	1.9E-06
205	1.118797	17.99661	0.948347	0.942448	3.48E-05
210	1.111693	17.87782	0.942087	0.941371	5.12E-07
215	1.108884	17.83083	0.939611	0.940308	4.86E-07
220	1.107949	17.81521	0.938788	0.939258	2.21E-07
225	1.1048	17.76254	0.936013	0.93822	4.87E-06
230	1.105686	17.77736	0.936793	0.937195	1.61E-07
235	1.103771	17.74533	0.935106	0.936182	1.16E-06
240	1.103526	17.74124	0.93489	0.935181	8.47E-08
245	1.099412	17.67244	0.931265	0.934193	8.57E-06
250	1.101416	17.70596	0.933031	0.933216	3.44E-08
255	1.097542	17.64117	0.929617	0.932251	6.94E-06
260	1.098345	17.6546	0.930324	0.931298	9.49E-07
265	1.095728	17.61084	0.928019	0.930357	5.47E-06
270	1.092557	17.5578	0.925224	0.929427	1.77E-05
275	1.100282	17.68699	0.932031	0.928508	1.24E-05
280	1.089122	17.50037	0.922197	0.9276	2.92E-05
285	1.089899	17.51336	0.922882	0.926703	1.46E-05
290	1.094135	17.5842	0.926614	0.925817	6.36E-07
295	1.09164	17.54247	0.924416	0.924941	2.77E-07
300	1.086544	17.45725	0.919925	0.924077	1.72E-05
			sum=	0.000362	



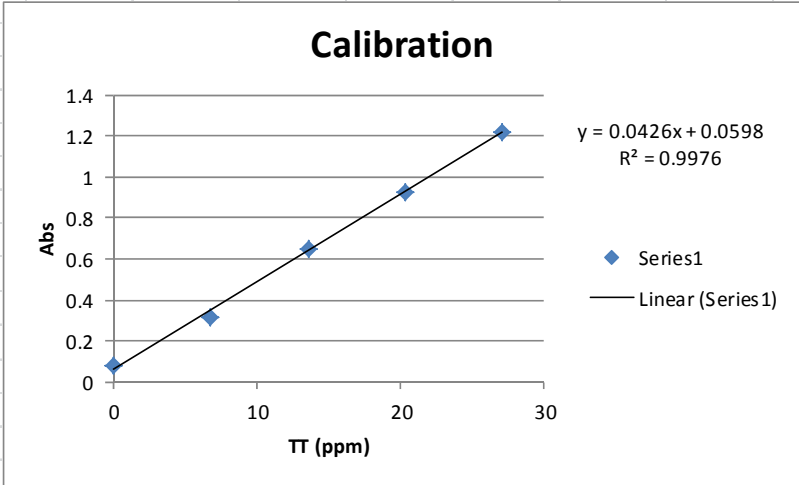
Calibratio Curve			
a=	0.0426	%	TT (ppm)
b=	0.0598		abs
		0	0 0.0834
		0.25	6.7775 0.3122
		0.5	13.555 0.6457
		0.75	20.3325 0.9269
		1	27.11 1.2213

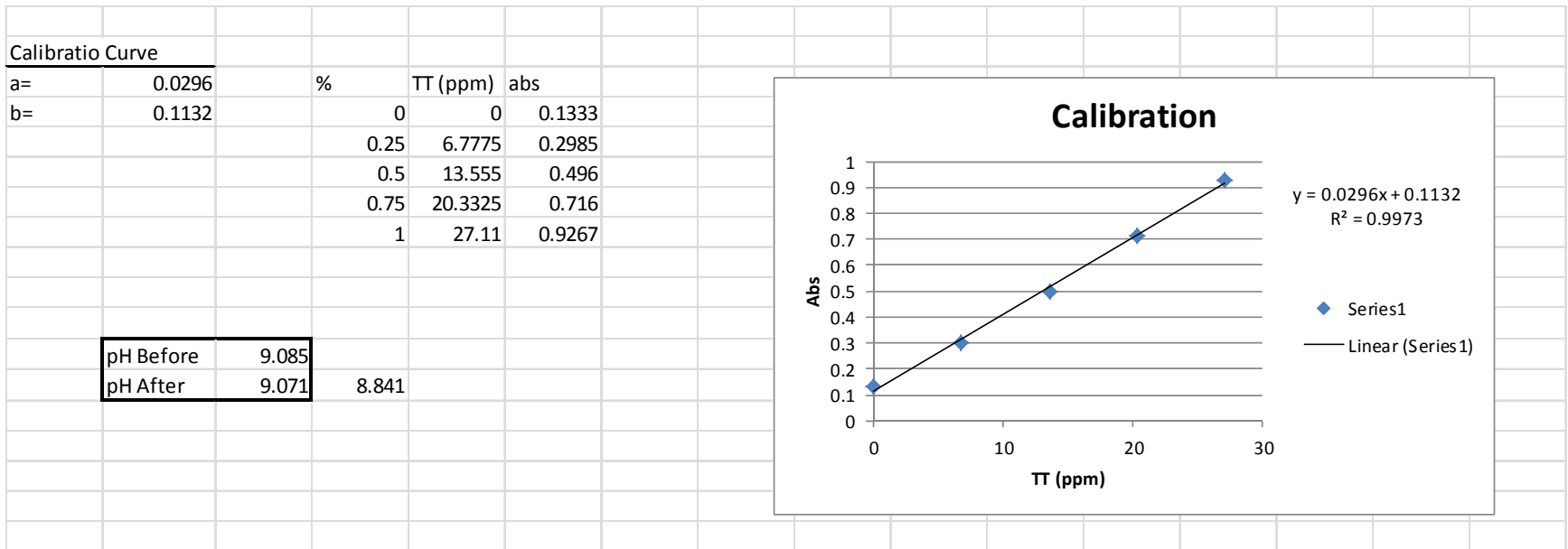
pH Before	6.433
pH After	5.55

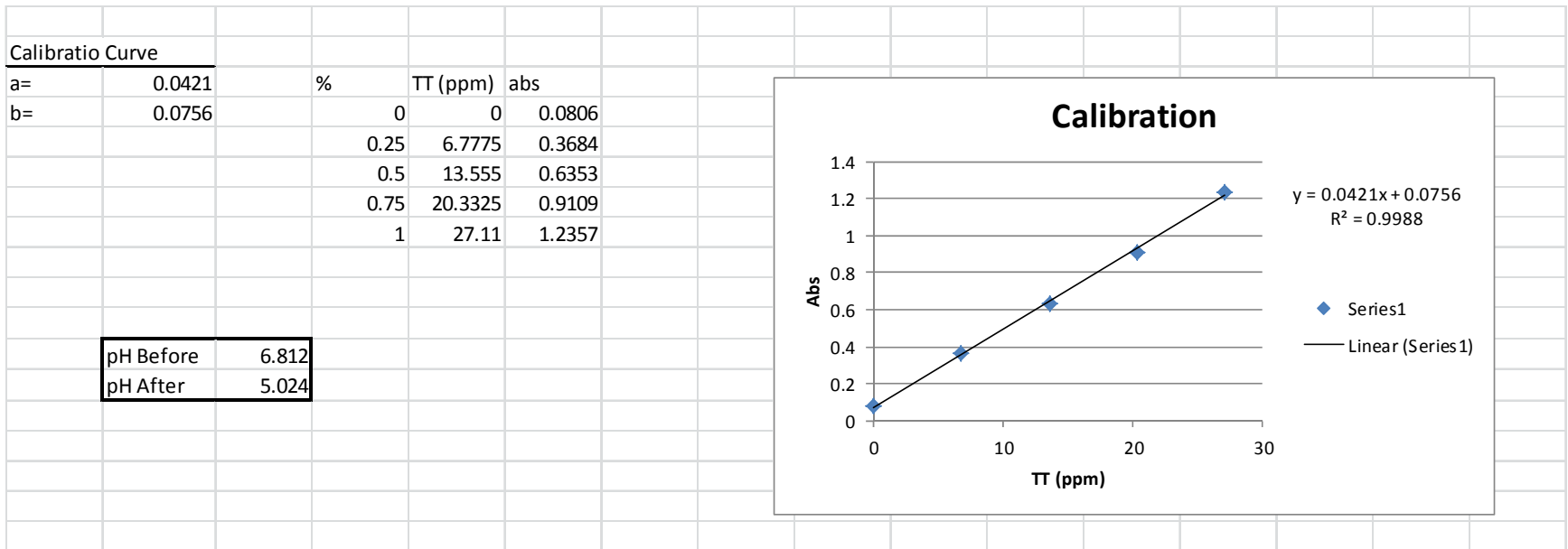
Note: Both Avg and 1st abs values gave same R^2 value



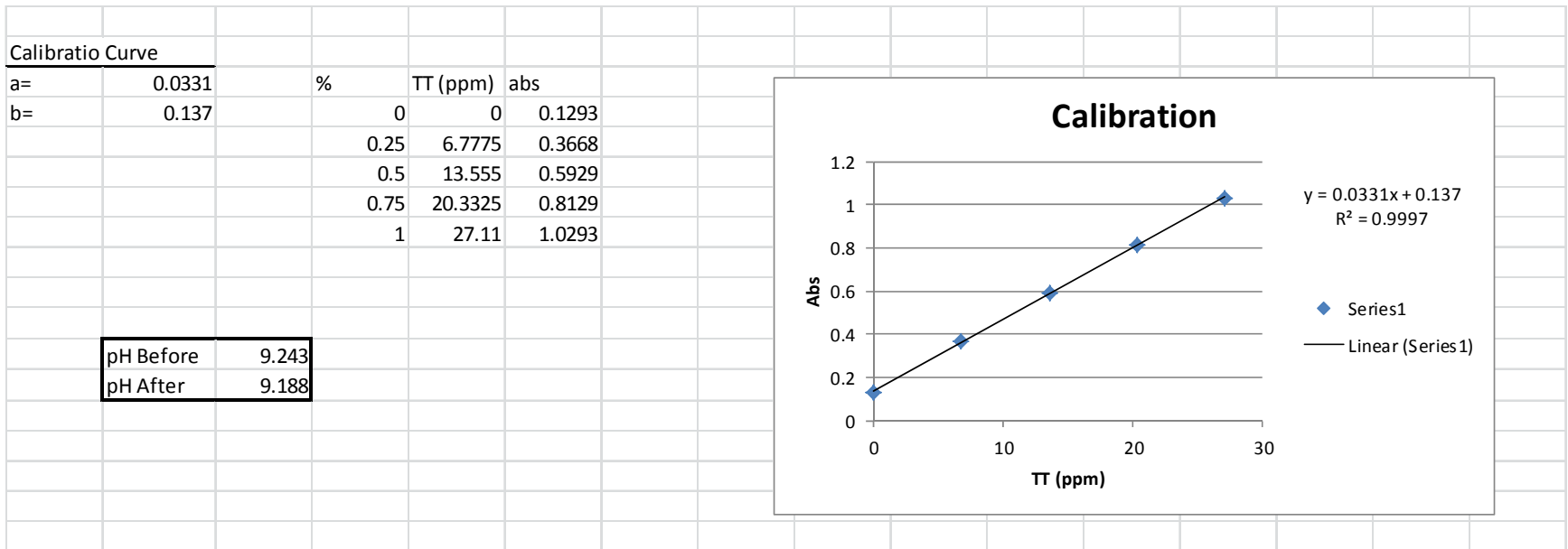
15Jun15_0.7@50%pH9					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.000283	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	0.859851	7.334377	1	1	0
5	0.855267	7.293875	0.994478	0.998593	1.69E-05
10	0.857092	7.310002	0.996677	0.997203	2.77E-07
15	0.855225	7.293506	0.994428	0.995829	1.96E-06
20	0.856037	7.300683	0.995406	0.994471	8.74E-07
25	0.853232	7.275904	0.992028	0.993129	1.21E-06
30	0.849618	7.243972	0.987674	0.991803	1.71E-05
35	0.848448	7.233637	0.986265	0.990493	1.79E-05
40	0.847485	7.225137	0.985106	0.989197	1.67E-05
45	0.851972	7.264769	0.990509	0.987917	6.72E-06
50	0.846437	7.215874	0.983843	0.986652	7.89E-06
55	0.848282	7.232174	0.986065	0.985402	4.4E-07
60	0.846378	7.215354	0.983772	0.984166	1.56E-07
65	0.846509	7.216506	0.983929	0.982945	9.68E-07
70	0.842216	7.178582	0.978758	0.981738	8.88E-06
75	0.842216	7.178584	0.978759	0.980546	3.19E-06
80	0.843433	7.18934	0.980225	0.979367	7.36E-07
85	0.840137	7.160218	0.976255	0.978202	3.79E-06
90	0.840649	7.164748	0.976872	0.977051	3.2E-08
95	0.838149	7.142661	0.973861	0.975913	4.21E-06
100	0.83988	7.157949	0.975945	0.974789	1.34E-06
105	0.836907	7.13169	0.972365	0.973677	1.72E-06
110	0.836429	7.127467	0.971789	0.972579	6.24E-07
115	0.834809	7.113157	0.969838	0.971494	2.74E-06
120	0.832747	7.09494	0.967354	0.970421	9.41E-06
125	0.833953	7.105588	0.968806	0.969361	3.08E-07
130	0.833057	7.097677	0.967727	0.968314	3.44E-07
135	0.831084	7.080247	0.965351	0.967278	3.71E-06
140	0.831846	7.086977	0.966268	0.966255	1.8E-10
145	0.828683	7.059039	0.962459	0.965244	7.75E-06
150	0.829133	7.063012	0.963001	0.964244	1.55E-06
155	0.830323	7.073527	0.964435	0.963257	1.39E-06
160	0.825872	7.034204	0.959073	0.962281	1.03E-05
165	0.830267	7.073026	0.964366	0.961316	9.3E-06
170	0.825149	7.027815	0.958202	0.960363	4.67E-06
175	0.826283	7.037837	0.959568	0.959421	2.19E-08
180	0.824388	7.021095	0.957286	0.958489	1.45E-06
185	0.825625	7.032027	0.958776	0.957569	1.46E-06
190	0.824904	7.025657	0.957908	0.95666	1.56E-06
195	0.826297	7.037961	0.959585	0.955761	1.46E-05
200	0.823198	7.010587	0.955853	0.954873	9.61E-07
205	0.823239	7.010942	0.955902	0.953995	3.64E-06
210	0.819759	6.980202	0.95171	0.953127	2.01E-06
215	0.819757	6.980181	0.951708	0.95227	3.16E-07
220	0.820974	6.990937	0.953174	0.951423	3.07E-06
225	0.820432	6.986147	0.952521	0.950585	3.75E-06
230	0.817326	6.958708	0.94878	0.949758	9.56E-07
235	0.818974	6.973264	0.950764	0.94894	3.33E-06
240	0.818159	6.96607	0.949784	0.948131	2.73E-06
245	0.816822	6.954258	0.948173	0.947333	7.06E-07
250	0.816029	6.947256	0.947218	0.946543	4.56E-07
255	0.816356	6.950138	0.947611	0.945763	3.42E-06
260	0.816669	6.952903	0.947988	0.944992	8.98E-06
265	0.8124	6.915193	0.942847	0.94423	1.91E-06
270	0.814029	6.929585	0.944809	0.943477	1.77E-06
275	0.811539	6.907586	0.94181	0.942732	8.52E-07
280	0.811109	6.903789	0.941292	0.941997	4.97E-07
285	0.810371	6.897267	0.940403	0.94127	7.52E-07
290	0.810306	6.896699	0.940325	0.940551	5.12E-08
295	0.809964	6.893678	0.939913	0.939841	5.16E-09
300	0.80902	6.885333	0.938775	0.93914	1.33E-07
			sum=		0.000225



17Jun15 0.7@30%pH6					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.000458	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.165817	14.86398	1	1	0
5	1.170727	14.92892	1.004369	0.997724	4.42E-05
10	1.164987	14.853	0.999261	0.995477	1.43E-05
15	1.158279	14.76427	0.993292	0.993258	1.12E-09
20	1.160089	14.78822	0.994903	0.991067	1.47E-05
25	1.155557	14.72826	0.990869	0.988904	3.86E-06
30	1.151658	14.67669	0.987399	0.986768	3.99E-07
35	1.150276	14.65841	0.98617	0.984658	2.28E-06
40	1.14844	14.63413	0.984536	0.982575	3.84E-06
45	1.144869	14.58689	0.981358	0.980519	7.05E-07
50	1.143944	14.57465	0.980535	0.978488	4.19E-06
55	1.13987	14.52077	0.97691	0.976483	1.82E-07
60	1.139212	14.51207	0.976324	0.974503	3.32E-06
65	1.134824	14.45402	0.972419	0.972548	1.68E-08
70	1.133254	14.43326	0.971022	0.970618	1.64E-07
75	1.132266	14.42019	0.970143	0.968712	2.05E-06
80	1.127833	14.36155	0.966198	0.96683	3.99E-07
85	1.127928	14.36281	0.966283	0.964971	1.72E-06
90	1.130731	14.39988	0.968777	0.963136	3.18E-05
95	1.121513	14.27795	0.960574	0.961324	5.63E-07
100	1.124387	14.31596	0.963131	0.959535	1.29E-05
105	1.120132	14.25969	0.959345	0.957769	2.48E-06
110	1.115178	14.19415	0.954936	0.956024	1.18E-06
115	1.120301	14.26192	0.959495	0.954302	2.7E-05
120	1.112203	14.15481	0.952289	0.952601	9.75E-08
125	1.117983	14.23125	0.957432	0.950922	4.24E-05
130	1.111615	14.14702	0.951765	0.949264	6.26E-06
135	1.106639	14.08121	0.947337	0.947626	8.34E-08
140	1.105383	14.06459	0.946219	0.946009	4.4E-08
145	1.10563	14.06786	0.946439	0.944413	4.11E-06
150	1.102756	14.02984	0.943882	0.942837	1.09E-06
155	1.098779	13.97723	0.940342	0.94128	8.8E-07
160	1.099489	13.98663	0.940975	0.939743	1.52E-06
165	1.097015	13.9539	0.938773	0.938226	2.99E-07
170	1.099873	13.9917	0.941316	0.936727	2.11E-05
175	1.09626	13.94392	0.938101	0.935248	8.14E-06
180	1.09693	13.95277	0.938697	0.933787	2.41E-05
185	1.09047	13.86732	0.932948	0.932344	3.65E-07
190	1.090749	13.87102	0.933197	0.93092	5.19E-06
195	1.093419	13.90633	0.935572	0.929513	3.67E-05
200	1.086762	13.81828	0.929648	0.928124	2.32E-06
205	1.082092	13.75651	0.925493	0.926753	1.59E-06
210	1.084137	13.78356	0.927312	0.925399	3.66E-06
215	1.081786	13.75246	0.925221	0.924062	1.34E-06
220	1.081377	13.74705	0.924857	0.922742	4.47E-06
225	1.077765	13.69927	0.921642	0.921438	4.17E-08
230	1.076004	13.67598	0.920075	0.920151	5.79E-09
235	1.072248	13.6263	0.916733	0.91888	4.61E-06
240	1.076615	13.68407	0.920619	0.917625	8.97E-06
245	1.074134	13.65124	0.91841	0.916386	4.1E-06
250	1.067405	13.56224	0.912423	0.915162	7.5E-06
255	1.067438	13.56267	0.912452	0.913954	2.26E-06
260	1.062486	13.49716	0.908045	0.912761	2.22E-05
265	1.061839	13.48861	0.907469	0.911583	1.69E-05
270	1.062082	13.49183	0.907686	0.91042	7.47E-06
275	1.060832	13.47529	0.906573	0.909271	7.28E-06
280	1.05631	13.41548	0.902549	0.908137	3.12E-05
285	1.055687	13.40724	0.901995	0.907017	2.52E-05
290	1.059826	13.46198	0.905678	0.905911	5.45E-08
295	1.053313	13.37583	0.899882	0.90482	2.44E-05
300	1.049913	13.33086	0.896856	0.903741	4.74E-05
			sum=	0.000548	

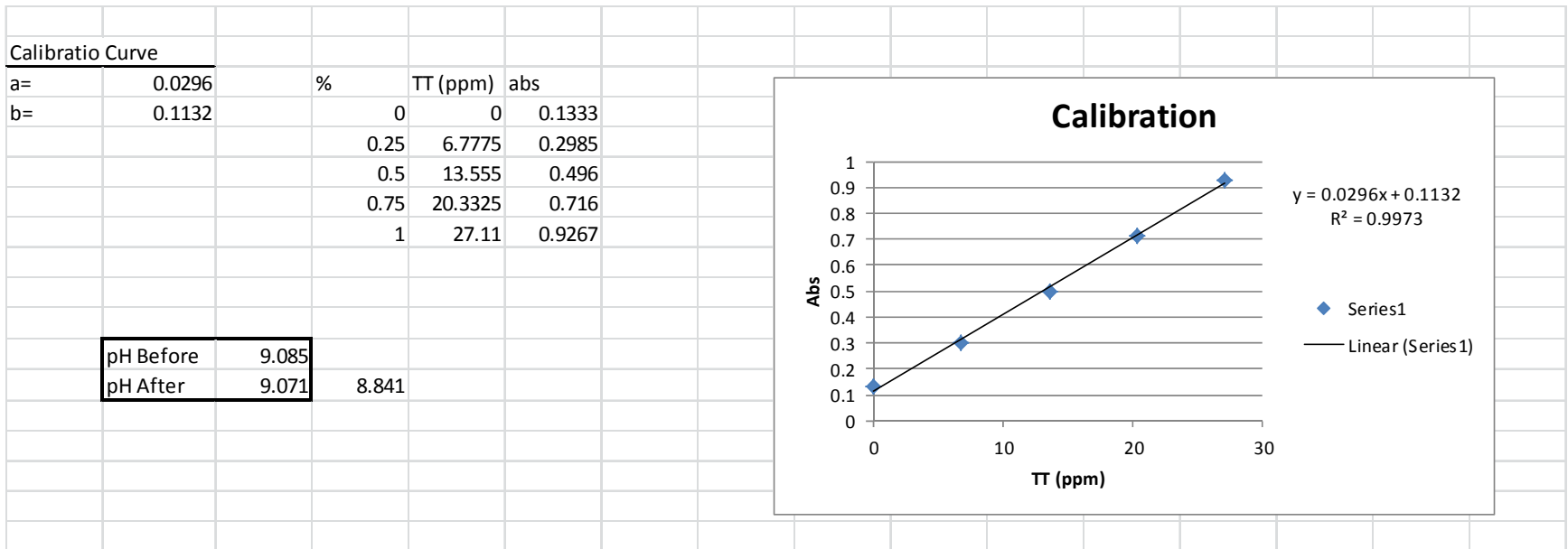


22Jun15 0.7@20%pH9					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	5.96E-05	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	0.93345	6.571896	1	1	0
5	0.94425	6.650732	1.011996	0.999703	0.000151
10	0.935591	6.587529	1.002379	0.99941	8.81E-06
15	0.936495	6.594122	1.003382	0.99912	1.82E-05
20	0.935765	6.588795	1.002571	0.998833	1.4E-05
25	0.936381	6.593294	1.003256	0.998548	2.22E-05
30	0.937102	6.598558	1.004057	0.998267	3.35E-05
35	0.931894	6.560538	0.998272	0.997989	7.98E-08
40	0.943152	6.642717	1.010776	0.997714	0.000171
45	0.935137	6.584212	1.001874	0.997442	1.96E-05
50	0.935403	6.586152	1.002169	0.997172	2.5E-05
55	0.9372	6.599269	1.004165	0.996906	5.27E-05
60	0.932829	6.567368	0.999311	0.996642	7.12E-06
65	0.931023	6.554184	0.997305	0.996381	8.53E-07
70	0.932822	6.567313	0.999303	0.996123	1.01E-05
75	0.933937	6.575454	1.000541	0.995868	2.18E-05
80	0.934861	6.582197	1.001567	0.995615	3.54E-05
85	0.931265	6.555951	0.997574	0.995365	4.88E-06
90	0.928376	6.534859	0.994364	0.995117	5.67E-07
95	0.92935	6.541969	0.995446	0.994873	3.29E-07
100	0.929217	6.540998	0.995298	0.994631	4.46E-07
105	0.931195	6.555436	0.997495	0.994391	9.64E-06
110	0.928509	6.535829	0.994512	0.994154	1.28E-07
115	0.928915	6.538799	0.994964	0.99392	1.09E-06
120	0.93069	6.551752	0.996935	0.993688	1.05E-05
125	0.928058	6.532539	0.994011	0.993458	3.06E-07
130	0.928674	6.537039	0.994696	0.993231	2.15E-06
135	0.934819	6.581887	1.00152	0.993006	7.25E-05
140	0.927916	6.531507	0.993854	0.992784	1.15E-06
145	0.931165	6.555218	0.997462	0.992564	2.4E-05
150	0.926259	6.519406	0.992013	0.992346	1.11E-07
155	0.933452	6.571914	1.000003	0.992131	6.2E-05
160	0.928166	6.53333	0.994132	0.991918	4.9E-06
165	0.925356	6.512816	0.99101	0.991707	4.86E-07
170	0.928139	6.533132	0.994101	0.991499	6.77E-06
175	0.93007	6.547229	0.996247	0.991292	2.45E-05
180	0.925813	6.51615	0.991518	0.991088	1.84E-07
185	0.924327	6.505307	0.989868	0.990886	1.04E-06
190	0.924228	6.504583	0.989757	0.990687	8.63E-07
195	0.920645	6.478433	0.985778	0.990489	2.22E-05
200	0.919201	6.467894	0.984175	0.990293	3.74E-05
205	0.924819	6.508898	0.990414	0.9901	9.87E-08
210	0.921127	6.481946	0.986313	0.989908	1.29E-05
215	0.921819	6.486998	0.987082	0.989719	6.95E-06
220	0.921435	6.484194	0.986655	0.989531	8.27E-06
225	0.921708	6.486189	0.986959	0.989346	5.7E-06
230	0.926016	6.517638	0.991744	0.989163	6.66E-06
235	0.925673	6.51513	0.991362	0.988981	5.67E-06
240	0.921096	6.481722	0.986279	0.988801	6.36E-06
245	0.919832	6.472496	0.984875	0.988624	1.41E-05
250	0.921281	6.483076	0.986485	0.988448	3.85E-06
255	0.919354	6.469004	0.984344	0.988274	1.54E-05
260	0.928222	6.533739	0.994194	0.988102	3.71E-05
265	0.917578	6.456046	0.982372	0.987932	3.09E-05
270	0.918887	6.465601	0.983826	0.987763	1.55E-05
275	0.92288	6.494747	0.988261	0.987597	4.41E-07
280	0.921591	6.485335	0.986829	0.987432	3.64E-07
285	0.923842	6.501767	0.989329	0.987269	4.24E-06
290	0.914252	6.431766	0.978677	0.987107	7.11E-05
295	0.921107	6.481803	0.986291	0.986947	4.31E-07
300	0.918746	6.464571	0.983669	0.986789	9.74E-06
				sum=	0.001135

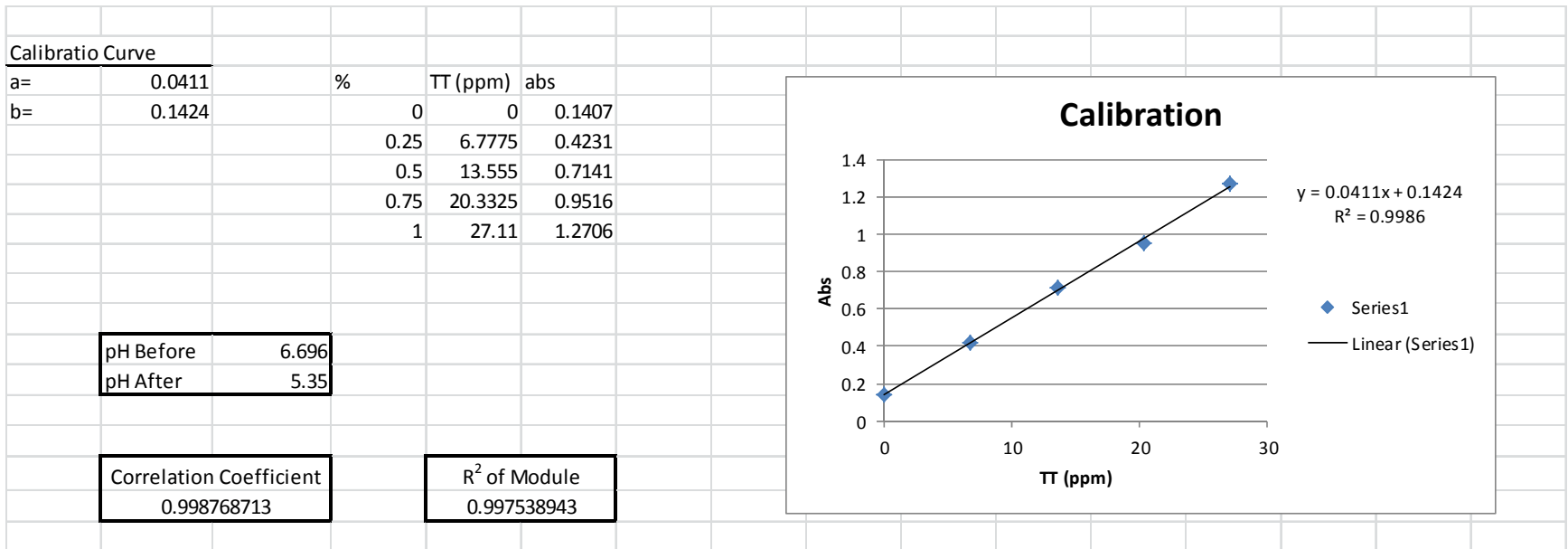


24Jun15 0.7@100%pH6 Throwout					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.001199	
wavelength=	430				
time (min)	abs	C/Co	model	sum squares	
0	1.237493	10.67043	1	1	0
5	1.229578	10.60051	0.993447	0.994052	3.66E-07
10	1.226262	10.57122	0.990702	0.988201	6.26E-06
15	1.216127	10.48169	0.982311	0.982444	1.78E-08
20	1.21564	10.47739	0.981908	0.976782	2.63E-05
25	1.206952	10.40064	0.974716	0.971211	1.23E-05
30	1.197791	10.31971	0.967131	0.96573	1.96E-06
35	1.19698	10.31254	0.96646	0.960339	3.75E-05
40	1.186696	10.22169	0.957945	0.955035	8.47E-06
45	1.178789	10.15185	0.9514	0.949817	2.5E-06
50	1.172988	10.1006	0.946597	0.944684	3.66E-06
55	1.171241	10.08517	0.945151	0.939634	3.04E-05
60	1.169725	10.07177	0.943895	0.934666	8.52E-05
65	1.162458	10.00758	0.937879	0.929779	6.56E-05
70	1.152499	9.9196	0.929634	0.924971	2.17E-05
75	1.147615	9.876455	0.925591	0.920242	2.86E-05
80	1.14359	9.8409	0.922259	0.915589	4.45E-05
85	1.137164	9.784133	0.916939	0.911012	3.51E-05
90	1.137999	9.79151	0.91763	0.906509	0.000124
95	1.129887	9.719848	0.910914	0.902079	7.81E-05
100	1.123968	9.66756	0.906014	0.897721	6.88E-05
105	1.116936	9.605446	0.900193	0.893433	4.57E-05
110	1.112112	9.562825	0.896198	0.889216	4.88E-05
115	1.104816	9.498374	0.890158	0.885067	2.59E-05
120	1.100966	9.46436	0.886971	0.880985	3.58E-05
125	1.093409	9.397602	0.880714	0.876969	1.4E-05
130	1.089509	9.363156	0.877486	0.873019	2E-05
135	1.086225	9.334141	0.874767	0.869133	3.17E-05
140	1.080285	9.281671	0.86985	0.86531	2.06E-05
145	1.078293	9.264076	0.868201	0.861549	4.42E-05
150	1.070276	9.193247	0.861563	0.857849	1.38E-05
155	1.066459	9.159534	0.858403	0.854209	1.76E-05
160	1.0623	9.122788	0.854959	0.850629	1.88E-05
165	1.056654	9.072915	0.850286	0.847106	1.01E-05
170	1.056486	9.071428	0.850146	0.843641	4.23E-05
175	1.046213	8.980682	0.841642	0.840232	1.99E-06
180	1.044108	8.962081	0.839899	0.836878	9.13E-06
185	1.03925	8.919172	0.835877	0.833578	5.28E-06
190	1.039777	8.923828	0.836314	0.830333	3.58E-05
195	1.028854	8.827336	0.827271	0.82714	1.72E-08
200	1.025082	8.794013	0.824148	0.823998	2.23E-08
205	1.019959	8.748754	0.819906	0.820908	1E-06
210	1.016042	8.714151	0.816663	0.817868	1.45E-06
215	1.01181	8.676763	0.813159	0.814878	2.95E-06
220	1.006184	8.627068	0.808502	0.811935	1.18E-05
225	1.004644	8.613466	0.807227	0.809041	3.29E-06
230	0.999937	8.571885	0.803331	0.806194	8.2E-06
235	0.994537	8.524179	0.79886	0.803393	2.05E-05
240	0.991102	8.493831	0.796016	0.800637	2.14E-05
245	0.987617	8.463044	0.79313	0.797926	2.3E-05
250	0.985851	8.447446	0.791669	0.795259	1.29E-05
255	0.977787	8.376215	0.784993	0.792636	5.84E-05
260	0.977226	8.37125	0.784528	0.790055	3.05E-05
265	0.974406	8.346345	0.782194	0.787516	2.83E-05
270	0.967829	8.288239	0.776748	0.785018	6.84E-05
275	0.97097	8.315991	0.779349	0.782561	1.03E-05
280	0.961828	8.235229	0.77178	0.780143	6.99E-05
285	0.963588	8.250774	0.773237	0.777765	2.05E-05
290	0.958313	8.204174	0.76887	0.775426	4.3E-05
295	0.957546	8.197406	0.768236	0.773124	2.39E-05
300	0.947788	8.111201	0.760157	0.77086	0.000115
			sum=	0.001697	

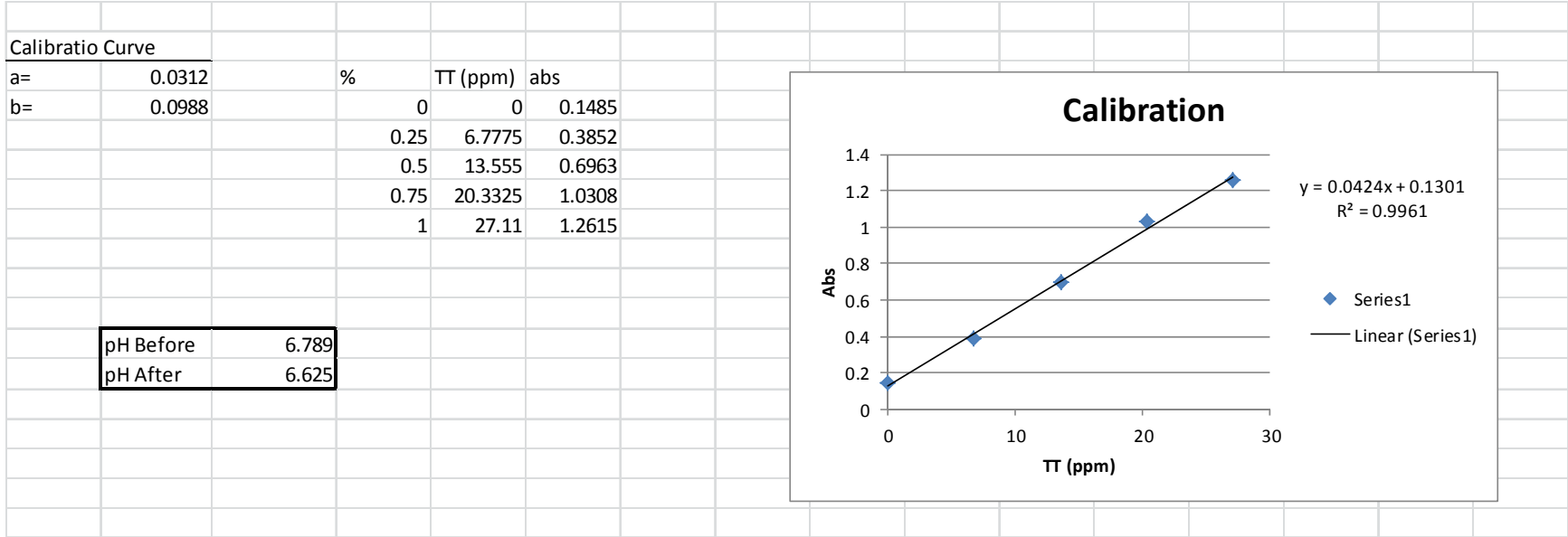




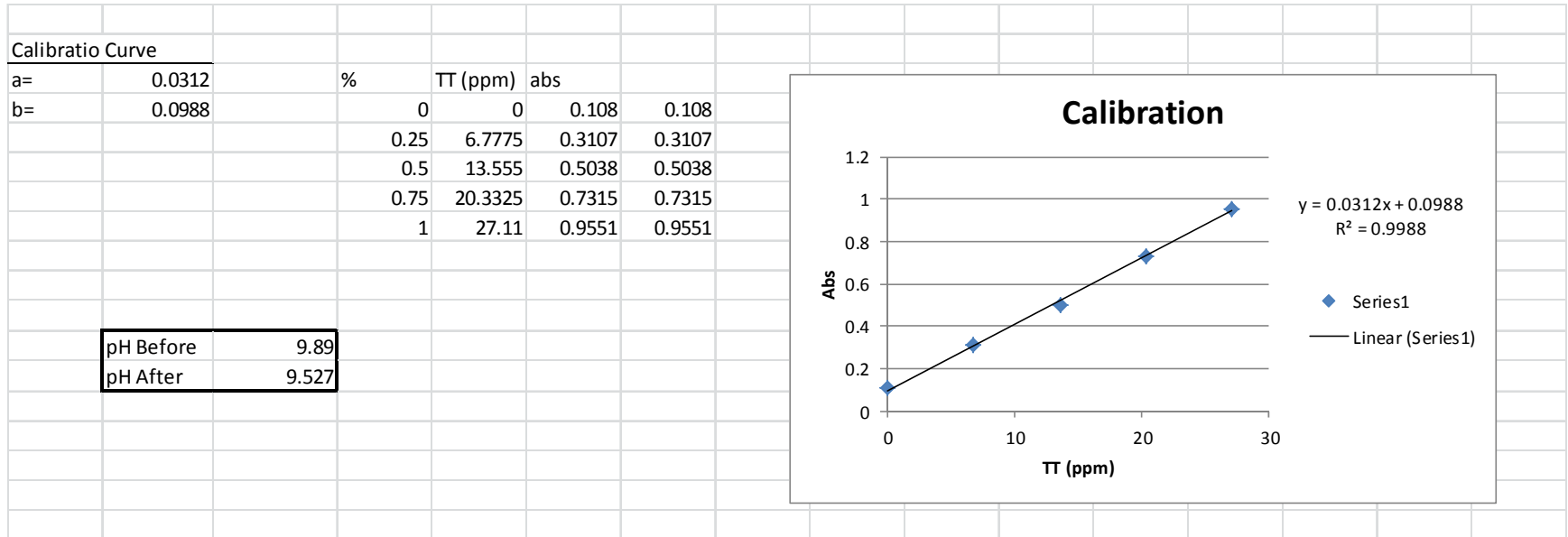
26Jun15 0.7@100%pHG					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.001224	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.236743	8.396371	1	1	0
5	1.227521	8.33161	0.992287	0.993933	2.71E-06
10	1.223997	8.306859	0.989339	0.987964	1.89E-06
15	1.215212	8.245167	0.981992	0.982094	1.04E-08
20	1.208181	8.19579	0.976111	0.976319	4.33E-08
25	1.200593	8.142504	0.969765	0.970639	7.64E-07
30	1.199269	8.133209	0.968658	0.965052	1.3E-05
35	1.187557	8.050959	0.958862	0.959556	4.82E-07
40	1.18941	8.063975	0.960412	0.95415	3.92E-05
45	1.181836	8.010783	0.954077	0.948832	2.75E-05
50	1.169094	7.921308	0.943421	0.943602	3.29E-08
55	1.167182	7.907882	0.941821	0.938457	1.13E-05
60	1.155692	7.827192	0.932211	0.933396	1.4E-06
65	1.155273	7.824246	0.93186	0.928418	1.19E-05
70	1.146178	7.76038	0.924254	0.923521	5.37E-07
75	1.140834	7.722851	0.919784	0.918705	1.17E-06
80	1.134842	7.680772	0.914773	0.913967	6.5E-07
85	1.134603	7.679091	0.914573	0.909306	2.77E-05
90	1.124961	7.611384	0.906509	0.904722	3.19E-06
95	1.120932	7.583093	0.903139	0.900213	8.56E-06
100	1.11216	7.521489	0.895802	0.895778	6.01E-10
105	1.107879	7.491428	0.892222	0.891415	6.51E-07
110	1.095025	7.40116	0.881471	0.887124	3.19E-05
115	1.103301	7.459277	0.888393	0.882902	3.01E-05
120	1.089516	7.362469	0.876863	0.87875	3.56E-06
125	1.087412	7.3477	0.875104	0.874666	1.92E-07
130	1.08594	7.337363	0.873873	0.870648	1.04E-05
135	1.083695	7.321593	0.871995	0.866696	2.81E-05
140	1.081671	7.307384	0.870303	0.862809	5.62E-05
145	1.071827	7.238254	0.862069	0.858986	9.51E-06
150	1.069559	7.222322	0.860172	0.855225	2.45E-05
155	1.058546	7.144985	0.850961	0.851525	3.18E-07
160	1.054079	7.113615	0.847225	0.847886	4.37E-07
165	1.057174	7.135353	0.849814	0.844307	3.03E-05
170	1.051629	7.096414	0.845176	0.840786	1.93E-05
175	1.042933	7.035347	0.837903	0.837322	3.38E-07
180	1.047667	7.068591	0.841863	0.833916	6.32E-05
185	1.036657	6.991272	0.832654	0.830565	4.37E-06
190	1.033443	6.968703	0.829966	0.827268	7.28E-06
195	1.032678	6.963327	0.829326	0.824026	2.81E-05
200	1.027649	6.928014	0.82512	0.820837	1.83E-05
205	1.018309	6.862426	0.817309	0.8177	1.53E-07
210	1.018005	6.860291	0.817054	0.814614	5.96E-06
215	1.010478	6.807431	0.810759	0.811579	6.72E-07
220	1.008011	6.790102	0.808695	0.808593	1.04E-08
225	1.009963	6.803813	0.810328	0.805656	2.18E-05
230	0.999766	6.732206	0.801799	0.802767	9.37E-07
235	0.995897	6.705036	0.798564	0.799926	1.86E-06
240	0.995564	6.702699	0.798285	0.797131	1.33E-06
245	0.988937	6.656156	0.792742	0.794381	2.69E-06
250	0.983293	6.616525	0.788022	0.791677	1.34E-05
255	0.979177	6.587619	0.784579	0.789017	1.97E-05
260	0.975001	6.558294	0.781087	0.7864	2.82E-05
265	0.972813	6.542929	0.779257	0.783826	2.09E-05
270	0.970348	6.525615	0.777195	0.781294	1.68E-05
275	0.967067	6.502581	0.774451	0.778804	1.89E-05
280	0.962899	6.473309	0.770965	0.776355	2.9E-05
285	0.960206	6.454393	0.768712	0.773945	2.74E-05
290	0.954588	6.414945	0.764014	0.771575	5.72E-05
295	0.958274	6.440832	0.767097	0.769243	4.61E-06
300	0.949053	6.376076	0.759385	0.76695	5.72E-05
				sum=	0.000848



29Jun15 0.7@5%pH6					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	9.69E-05	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.210083	11.93201	1	1	0
5	1.207514	11.90601	0.997821	0.999518	2.88E-06
10	1.203953	11.86997	0.994801	0.999041	1.8E-05
15	1.205359	11.8842	0.995993	0.99857	6.64E-06
20	1.203867	11.8691	0.994728	0.998103	1.14E-05
25	1.203846	11.86889	0.99471	0.997642	8.6E-06
30	1.205705	11.88771	0.996287	0.997186	8.08E-07
35	1.203731	11.86773	0.994612	0.996734	4.5E-06
40	1.203103	11.86137	0.994079	0.996287	4.88E-06
45	1.204514	11.87564	0.995276	0.995846	3.24E-07
50	1.201609	11.84624	0.992812	0.995409	6.74E-06
55	1.201632	11.84648	0.992832	0.994976	4.6E-06
60	1.198273	11.81248	0.989983	0.994549	2.08E-05
65	1.199479	11.82469	0.991005	0.994126	9.74E-06
70	1.202693	11.85721	0.993731	0.993707	5.8E-10
75	1.199519	11.82509	0.991039	0.993293	5.08E-06
80	1.196347	11.79298	0.988348	0.992884	2.06E-05
85	1.200211	11.83209	0.991626	0.992479	7.27E-07
90	1.2039	11.86943	0.994755	0.992078	7.17E-06
95	1.198488	11.81465	0.990165	0.991682	2.3E-06
100	1.199037	11.82022	0.990631	0.99129	4.34E-07
105	1.197168	11.80129	0.989045	0.990902	3.45E-06
110	1.201932	11.84952	0.993086	0.990518	6.6E-06
115	1.197947	11.80918	0.989706	0.990139	1.87E-07
120	1.202286	11.8531	0.993386	0.989763	1.31E-05
125	1.194916	11.7785	0.987135	0.989392	5.09E-06
130	1.195022	11.77957	0.987225	0.989025	3.24E-06
135	1.195559	11.78501	0.98768	0.988661	9.62E-07
140	1.198287	11.81262	0.989994	0.988302	2.86E-06
145	1.195995	11.78943	0.98805	0.987946	1.08E-08
150	1.193137	11.7605	0.985626	0.987595	3.88E-06
155	1.192179	11.7508	0.984813	0.987247	5.92E-06
160	1.191782	11.74678	0.984476	0.986903	5.89E-06
165	1.191055	11.73942	0.98386	0.986562	7.3E-06
170	1.189499	11.72368	0.98254	0.986225	1.36E-05
175	1.198409	11.81385	0.990097	0.985892	1.77E-05
180	1.189457	11.72325	0.982504	0.985563	9.35E-06
185	1.190276	11.73154	0.983199	0.985237	4.15E-06
190	1.192251	11.75152	0.984874	0.984914	1.63E-09
195	1.191204	11.74093	0.983986	0.984595	3.71E-07
200	1.18841	11.71265	0.981616	0.98428	7.1E-06
205	1.194491	11.7742	0.986774	0.983968	7.88E-06
210	1.191036	11.73923	0.983843	0.983659	3.41E-08
215	1.192284	11.75187	0.984902	0.983353	2.4E-06
220	1.189992	11.72866	0.982958	0.983051	8.71E-09
225	1.191913	11.7481	0.984587	0.982752	3.37E-06
230	1.192839	11.75748	0.985373	0.982457	8.5E-06
235	1.188999	11.71861	0.982116	0.982164	2.38E-09
240	1.190983	11.73869	0.983799	0.981875	3.7E-06
245	1.186759	11.69594	0.980215	0.981589	1.89E-06
250	1.184216	11.6702	0.978058	0.981306	1.05E-05
255	1.185755	11.68578	0.979364	0.981026	2.76E-06
260	1.1862	11.69028	0.979741	0.980749	1.02E-06
265	1.186179	11.69007	0.979723	0.980475	5.65E-07
270	1.191548	11.74441	0.984278	0.980204	1.66E-05
275	1.187257	11.70098	0.980638	0.979936	4.93E-07
280	1.187351	11.70194	0.980718	0.979671	1.1E-06
285	1.192489	11.75393	0.985076	0.979408	3.21E-05
290	1.187218	11.70059	0.980605	0.979149	2.12E-06
295	1.187313	11.70155	0.980686	0.978892	3.22E-06
300	1.188058	11.70909	0.981318	0.978638	7.18E-06
			sum=		0.000352

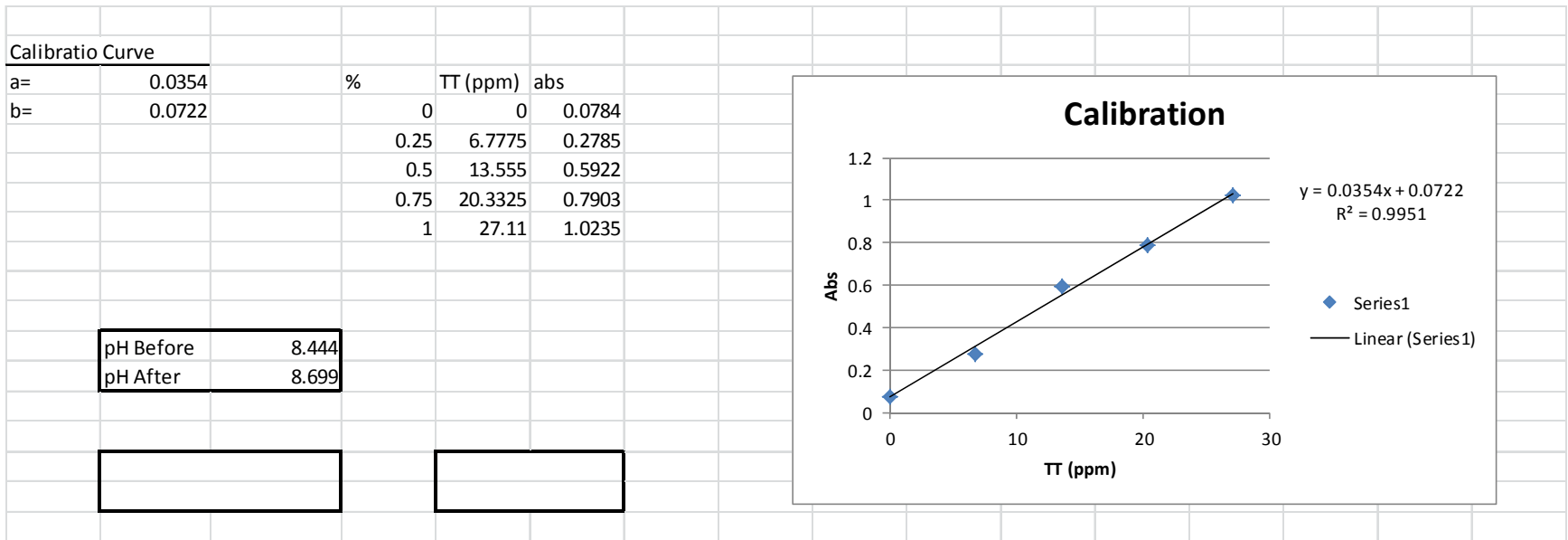


1jul15 0.7@100%pH9					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.000242	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	0.901425	8.807942	1	1	0
5	0.900986	8.8035	0.999496	0.998796	4.9E-07
10	0.908873	8.88333	1.008559	0.997606	0.00012
15	0.908235	8.876872	1.007826	0.996429	0.00013
20	0.907171	8.866108	1.006604	0.995266	0.000129
25	0.903385	8.827782	1.002253	0.994116	6.62E-05
30	0.901005	8.803697	0.999518	0.99298	4.27E-05
35	0.900706	8.800664	0.999174	0.991857	5.35E-05
40	0.901136	8.805021	0.999668	0.990746	7.96E-05
45	0.897292	8.76611	0.995251	0.989649	3.14E-05
50	0.894711	8.739985	0.992285	0.988564	1.38E-05
55	0.899757	8.791067	0.998084	0.987492	0.000112
60	0.895738	8.750386	0.993465	0.986432	4.95E-05
65	0.894342	8.736255	0.991861	0.985384	4.2E-05
70	0.891649	8.709	0.988767	0.984348	1.95E-05
75	0.89825	8.775807	0.996352	0.983324	0.00017
80	0.895874	8.751763	0.993622	0.982312	0.000128
85	0.890439	8.696751	0.987376	0.981312	3.68E-05
90	0.887278	8.66476	0.983744	0.980323	1.17E-05
95	0.884914	8.64083	0.981027	0.979345	2.83E-06
100	0.884503	8.636665	0.980554	0.978379	4.73E-06
105	0.884317	8.634786	0.980341	0.977424	8.51E-06
110	0.881993	8.611268	0.977671	0.97648	1.42E-06
115	0.884845	8.640131	0.980948	0.975546	2.92E-05
120	0.879261	8.583618	0.974532	0.974624	8.54E-09
125	0.880336	8.594493	0.975766	0.973712	4.22E-06
130	0.877738	8.568198	0.972781	0.972811	8.88E-10
135	0.878762	8.578564	0.973958	0.97192	4.15E-06
140	0.879805	8.589119	0.975156	0.971039	1.7E-05
145	0.878122	8.572085	0.973222	0.970169	9.33E-06
150	0.873984	8.530199	0.968467	0.969308	7.08E-07
155	0.882223	8.613594	0.977935	0.968457	8.98E-05
160	0.873079	8.521038	0.967427	0.967617	3.61E-08
165	0.871736	8.50745	0.965884	0.966785	8.13E-07
170	0.872509	8.515274	0.966772	0.965964	6.54E-07
175	0.878254	8.573426	0.973374	0.965152	6.76E-05
180	0.872496	8.515144	0.966758	0.964349	5.8E-06
185	0.868964	8.479396	0.962699	0.963555	7.34E-07
190	0.868911	8.478856	0.962638	0.962771	1.78E-08
195	0.874875	8.539221	0.969491	0.961996	5.62E-05
200	0.866475	8.454195	0.959838	0.961229	1.94E-06
205	0.866543	8.45489	0.959917	0.960472	3.08E-07
210	0.869059	8.480357	0.962808	0.959723	9.52E-06
215	0.86267	8.415686	0.955466	0.958983	1.24E-05
220	0.863839	8.427521	0.956809	0.958251	2.08E-06
225	0.868353	8.473212	0.961997	0.957528	2E-05
230	0.863772	8.426844	0.956732	0.956813	6.44E-09
235	0.857593	8.364306	0.949632	0.956106	4.19E-05
240	0.861403	8.402862	0.95401	0.955407	1.95E-06
245	0.859964	8.388302	0.952357	0.954717	5.57E-06
250	0.855614	8.344271	0.947358	0.954034	4.46E-05
255	0.856734	8.355606	0.948645	0.95336	2.22E-05
260	0.859743	8.386058	0.952102	0.952693	3.49E-07
265	0.854748	8.335501	0.946362	0.952033	3.22E-05
270	0.857415	8.362499	0.949427	0.951382	3.82E-06
275	0.853336	8.321211	0.94474	0.950738	3.6E-05
280	0.851216	8.299758	0.942304	0.950101	6.08E-05
285	0.859198	8.380549	0.951476	0.949471	4.02E-06
290	0.850508	8.29259	0.94149	0.948849	5.42E-05
295	0.85208	8.308505	0.943297	0.948234	2.44E-05
300	0.848349	8.270737	0.939009	0.947626	7.43E-05
			sum=		0.001992

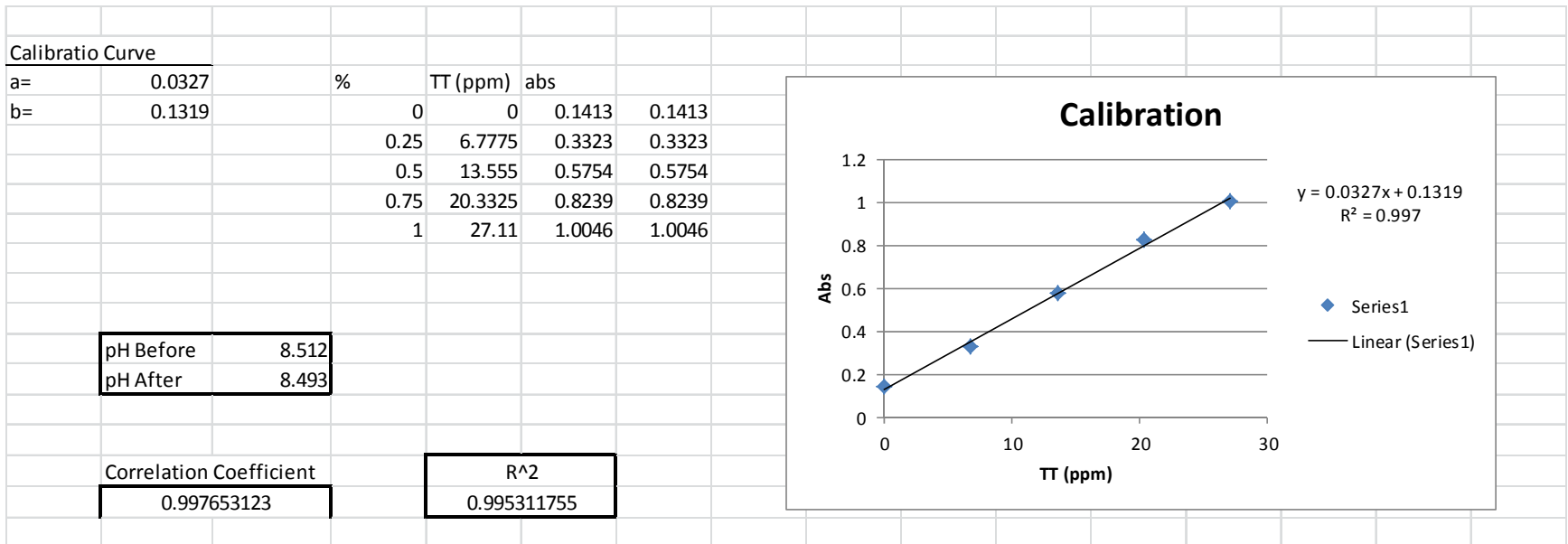


<a href="#">2Jul15_0.7@30%pH8</a>					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.000184	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	0.964623	12.87012	1	1	0
5	0.958008	12.77851	0.992882	0.999087	3.85E-05
10	0.962411	12.83949	0.99762	0.998183	3.18E-07
15	0.961793	12.83093	0.996955	0.997291	1.13E-07
20	0.963399	12.85317	0.998683	0.996408	5.18E-06
25	0.958179	12.78088	0.993066	0.995534	6.09E-06
30	0.962604	12.84216	0.997828	0.994671	9.96E-06
35	0.957762	12.7751	0.992617	0.993818	1.44E-06
40	0.960506	12.8131	0.995569	0.992974	6.74E-06
45	0.955501	12.74378	0.990183	0.992139	3.82E-06
50	0.95366	12.71829	0.988203	0.991314	9.68E-06
55	0.954978	12.73654	0.989621	0.990498	7.7E-07
60	0.957829	12.77603	0.992689	0.989692	8.99E-06
65	0.956815	12.76198	0.991598	0.988894	7.31E-06
70	0.951458	12.68778	0.985832	0.988105	5.17E-06
75	0.95115	12.68351	0.985501	0.987325	3.33E-06
80	0.951836	12.69302	0.98624	0.986554	9.9E-08
85	0.948637	12.64872	0.982797	0.985792	8.97E-06
90	0.949825	12.66516	0.984075	0.985038	9.28E-07
95	0.947888	12.63833	0.98199	0.984293	5.3E-06
100	0.94874	12.65015	0.982908	0.983556	4.19E-07
105	0.947672	12.63534	0.981758	0.982827	1.14E-06
110	0.945591	12.60652	0.979519	0.982106	6.7E-06
115	0.94539	12.60374	0.979302	0.981394	4.38E-06
120	0.944683	12.59395	0.978542	0.980689	4.61E-06
125	0.945991	12.61207	0.979949	0.979993	1.89E-09
130	0.949064	12.65463	0.983257	0.979304	1.56E-05
135	0.942704	12.56654	0.976412	0.978623	4.89E-06
140	0.949036	12.65423	0.983226	0.97795	2.78E-05
145	0.945737	12.60855	0.979676	0.977284	5.72E-06
150	0.946864	12.62415	0.980888	0.976626	1.82E-05
155	0.946933	12.62511	0.980963	0.975975	2.49E-05
160	0.943201	12.57343	0.976947	0.975331	2.61E-06
165	0.945544	12.60587	0.979468	0.974695	2.28E-05
170	0.944979	12.59804	0.97886	0.974066	2.3E-05
175	0.941854	12.55477	0.975498	0.973443	4.22E-06
180	0.938791	12.51235	0.972201	0.972828	3.93E-07
185	0.938602	12.50973	0.971998	0.97222	4.93E-08
190	0.935392	12.46527	0.968543	0.971618	9.46E-06
195	0.935435	12.46585	0.968589	0.971024	5.93E-06
200	0.941252	12.54643	0.974849	0.970436	1.95E-05
205	0.936946	12.48679	0.970215	0.969854	1.3E-07
210	0.933011	12.43228	0.96598	0.969279	1.09E-05
215	0.932804	12.42942	0.965758	0.968711	8.72E-06
220	0.932876	12.43041	0.965835	0.968149	5.35E-06
225	0.933721	12.44212	0.966744	0.967593	7.2E-07
230	0.930844	12.40227	0.963649	0.967044	1.15E-05
235	0.932258	12.42186	0.965171	0.9665	1.77E-06
240	0.933271	12.43588	0.96626	0.965963	8.81E-08
245	0.930553	12.39824	0.963335	0.965432	4.4E-06
250	0.933707	12.44193	0.96673	0.964907	3.32E-06
255	0.934052	12.4467	0.9671	0.964387	7.36E-06
260	0.928939	12.37589	0.961598	0.963874	5.18E-06
265	0.929708	12.38653	0.962426	0.963366	8.84E-07
270	0.930041	12.39115	0.962784	0.962864	6.38E-09
275	0.927041	12.34959	0.959556	0.962368	7.91E-06
280	0.928864	12.37485	0.961518	0.961877	1.29E-07
285	0.928815	12.37417	0.961465	0.961391	5.38E-09
290	0.927786	12.35992	0.960358	0.960912	3.07E-07
295	0.930702	12.40031	0.963496	0.960437	9.36E-06
300	0.928385	12.36822	0.961002	0.959968	1.07E-06
			sum=	0.000404	

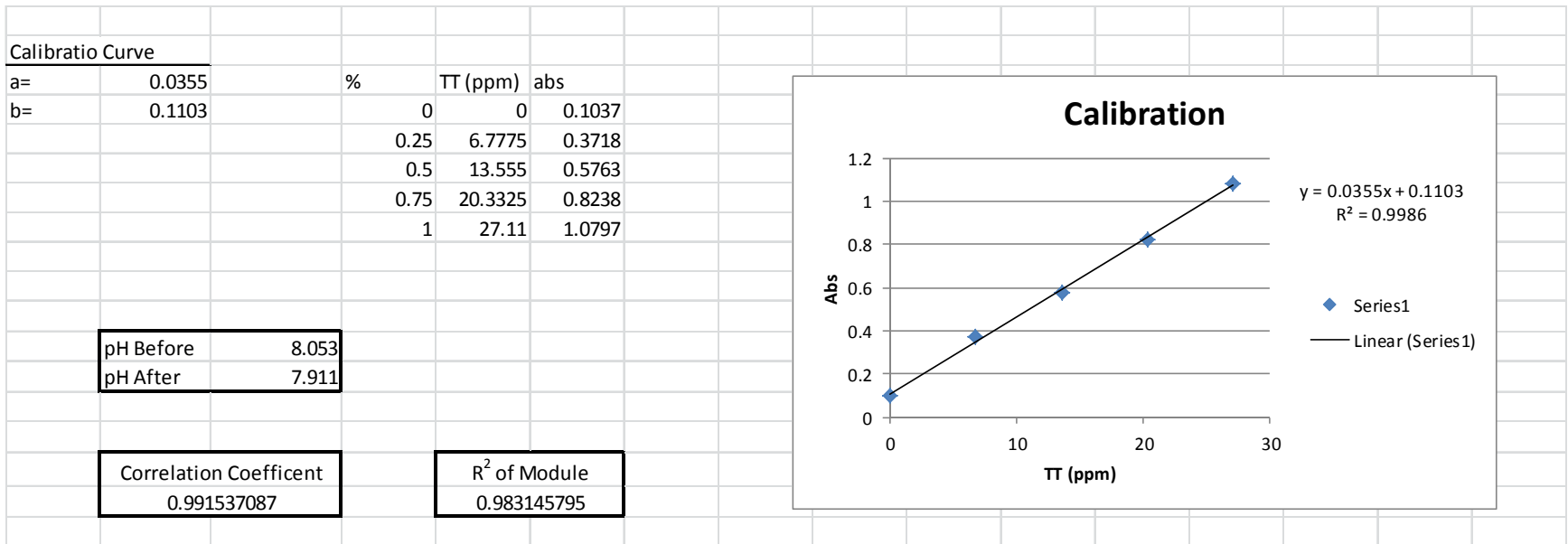




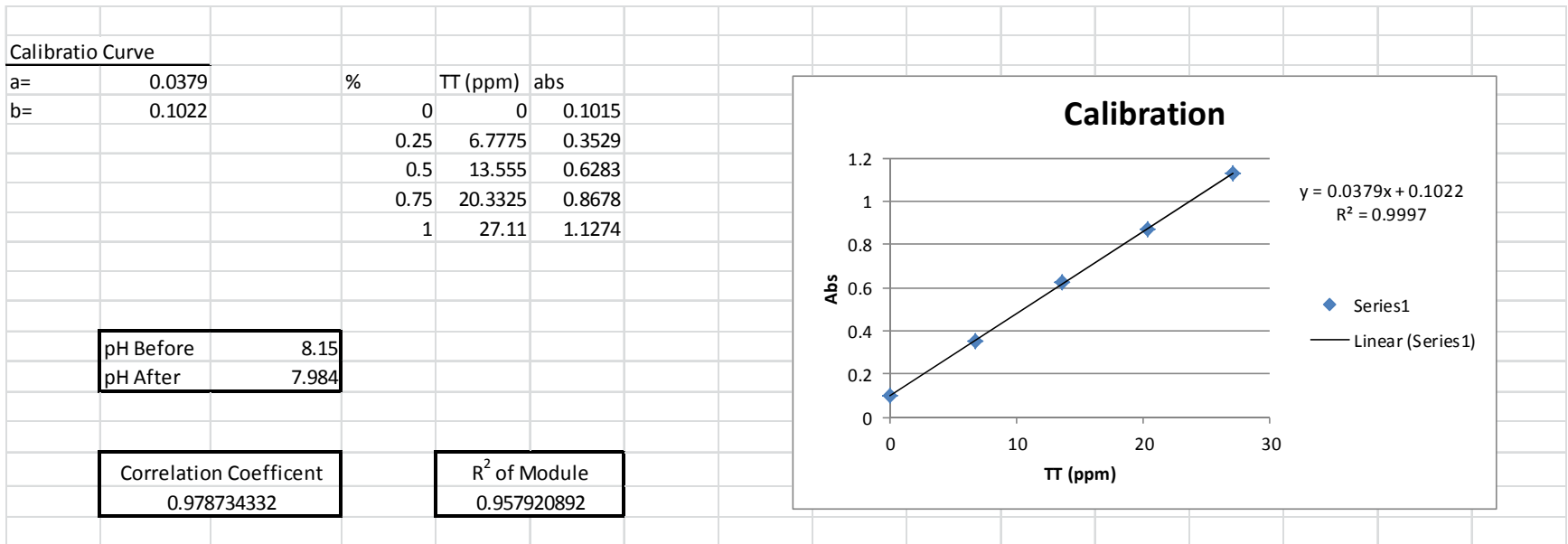
6Jul15_0.7@100%pH8					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.000472	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	0.926073	6.77311	1	1	1.23E-32
5	0.923546	6.753946	0.997171	0.997653	2.33E-07
10	0.923245	6.751671	0.996835	0.995337	2.24E-06
15	0.919688	6.724697	0.992852	0.993049	3.87E-08
20	0.917768	6.710141	0.990703	0.99079	7.62E-09
25	0.917023	6.704497	0.98987	0.98856	1.71E-06
30	0.915572	6.693493	0.988245	0.986359	3.56E-06
35	0.915245	6.691015	0.987879	0.984185	1.37E-05
40	0.91051	6.655121	0.98258	0.982038	2.93E-07
45	0.910952	6.658467	0.983074	0.979919	9.95E-06
50	0.910098	6.651994	0.982118	0.977827	1.84E-05
55	0.908409	6.639187	0.980227	0.975761	2E-05
60	0.906301	6.623206	0.977868	0.973721	1.72E-05
65	0.906002	6.620938	0.977533	0.971707	3.39E-05
70	0.900989	6.582937	0.971922	0.969718	4.86E-06
75	0.898614	6.564927	0.969263	0.967755	2.28E-06
80	0.898954	6.567508	0.969644	0.965816	1.47E-05
85	0.89735	6.555344	0.967848	0.963902	1.56E-05
90	0.893342	6.52496	0.963362	0.962013	1.82E-06
95	0.894073	6.530497	0.96418	0.960147	1.63E-05
100	0.893484	6.526031	0.963521	0.958305	2.72E-05
105	0.888544	6.48858	0.957991	0.956486	2.27E-06
110	0.888985	6.491926	0.958485	0.95469	1.44E-05
115	0.887667	6.48193	0.957009	0.952917	1.68E-05
120	0.886524	6.473271	0.955731	0.951166	2.08E-05
125	0.88421	6.455721	0.95314	0.949437	1.37E-05
130	0.881677	6.436523	0.950305	0.947731	6.63E-06
135	0.879099	6.416977	0.94742	0.946045	1.89E-06
140	0.876026	6.393676	0.943979	0.944382	1.62E-07
145	0.8767	6.398786	0.944734	0.942739	3.98E-06
150	0.876949	6.400675	0.945013	0.941117	1.52E-05
155	0.875605	6.390482	0.943508	0.939515	1.59E-05
160	0.872623	6.367875	0.94017	0.937934	5E-06
165	0.871917	6.362528	0.939381	0.936373	9.05E-06
170	0.867673	6.330347	0.934629	0.934832	4.1E-08
175	0.869165	6.341658	0.936299	0.93331	8.94E-06
180	0.867022	6.325413	0.933901	0.931807	4.38E-06
185	0.863003	6.294941	0.929402	0.930324	8.5E-07
190	0.862477	6.290953	0.928813	0.928859	2.09E-09
195	0.860064	6.272658	0.926112	0.927412	1.69E-06
200	0.859326	6.267068	0.925287	0.925984	4.87E-07
205	0.857527	6.253426	0.923272	0.924574	1.7E-06
210	0.856671	6.246935	0.922314	0.923182	7.54E-07
215	0.853033	6.219352	0.918242	0.921808	1.27E-05
220	0.855027	6.234477	0.920475	0.920451	5.75E-10
225	0.851664	6.208976	0.91671	0.919111	5.77E-06
230	0.85106	6.204397	0.916034	0.917788	3.08E-06
235	0.849822	6.195011	0.914648	0.916482	3.36E-06
240	0.848141	6.18227	0.912767	0.915192	5.88E-06
245	0.846559	6.170271	0.910995	0.913919	8.55E-06
250	0.847323	6.176068	0.911851	0.912661	6.57E-07
255	0.845445	6.161825	0.909748	0.91142	2.79E-06
260	0.845169	6.159736	0.90944	0.910194	5.69E-07
265	0.842026	6.135905	0.905921	0.908984	9.38E-06
270	0.840774	6.126413	0.90452	0.907789	1.07E-05
275	0.839904	6.119815	0.903546	0.90661	9.39E-06
280	0.838825	6.11164	0.902339	0.905445	9.65E-06
285	0.842222	6.137395	0.906141	0.904295	3.41E-06
290	0.836544	6.094341	0.899785	0.903159	1.14E-05
295	0.836388	6.093159	0.89961	0.902038	5.9E-06
300	0.833828	6.073749	0.896745	0.900931	1.75E-05
			sum=	0.000469	



9jul15_0.7@70%pH8 Accidental Redo					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.00045	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.071357	9.391269	1	1	1.23E-32
5	1.076478	9.437699	1.004944	0.997764	5.16E-05
10	1.064583	9.329852	0.99346	0.995556	4.39E-06
15	1.07242	9.400907	1.001026	0.993376	5.85E-05
20	1.061813	9.304744	0.990787	0.991223	1.91E-07
25	1.061378	9.300795	0.990366	0.989097	1.61E-06
30	1.058328	9.273148	0.987422	0.986998	1.8E-07
35	1.064293	9.327229	0.993181	0.984925	6.82E-05
40	1.059219	9.281227	0.988283	0.982878	2.92E-05
45	1.052529	9.220572	0.981824	0.980857	9.34E-07
50	1.046733	9.168025	0.976229	0.978862	6.93E-06
55	1.057988	9.270064	0.987094	0.976891	0.000104
60	1.048942	9.188052	0.978361	0.974945	1.17E-05
65	1.048937	9.188004	0.978356	0.973023	2.84E-05
70	1.040807	9.114294	0.970507	0.971126	3.82E-07
75	1.039713	9.104382	0.969452	0.969252	4E-08
80	1.043311	9.137003	0.972925	0.967402	3.05E-05
85	1.039915	9.106212	0.969647	0.965575	1.66E-05
90	1.037692	9.086055	0.9675	0.96377	1.39E-05
95	1.036777	9.077758	0.966617	0.961989	2.14E-05
100	1.029341	9.010345	0.959439	0.96023	6.26E-07
105	1.039207	9.099789	0.968963	0.958493	0.00011
110	1.02561	8.976519	0.955837	0.956778	8.85E-07
115	1.026331	8.983055	0.956533	0.955084	2.1E-06
120	1.027637	8.994891	0.957793	0.953411	1.92E-05
125	1.024548	8.966894	0.954812	0.95176	9.31E-06
130	1.02902	9.007431	0.959128	0.950129	8.1E-05
135	1.01916	8.918038	0.949609	0.948519	1.19E-06
140	1.028044	8.998581	0.958186	0.946929	0.000127
145	1.016024	8.889611	0.946582	0.945358	1.5E-06
150	1.009117	8.826992	0.939915	0.943808	1.52E-05
155	1.010642	8.840814	0.941387	0.942277	7.93E-07
160	1.010131	8.836187	0.940894	0.940765	1.66E-08
165	1.012159	8.854565	0.942851	0.939272	1.28E-05
170	1.01251	8.857754	0.94319	0.937798	2.91E-05
175	1.009678	8.832081	0.940457	0.936342	1.69E-05
180	1.001556	8.758442	0.932615	0.934905	5.24E-06
185	1.004215	8.782548	0.935182	0.933486	2.88E-06
190	0.997117	8.718192	0.928329	0.932084	1.41E-05
195	0.997403	8.720793	0.928606	0.9307	4.38E-06
200	0.996447	8.71212	0.927683	0.929333	2.72E-06
205	0.998368	8.729541	0.929538	0.927984	2.41E-06
210	0.990993	8.662676	0.922418	0.926651	1.79E-05
215	0.990423	8.657506	0.921867	0.925335	1.2E-05
220	0.989602	8.650062	0.921075	0.924036	8.77E-06
225	0.99115	8.664097	0.922569	0.922753	3.38E-08
230	0.985561	8.61343	0.917174	0.921486	1.86E-05
235	0.994439	8.69392	0.925745	0.920235	3.04E-05
240	0.988147	8.636868	0.91967	0.919	4.49E-07
245	0.986135	8.618632	0.917728	0.91778	2.69E-09
250	0.990653	8.659595	0.92209	0.916575	3.04E-05
255	0.975881	8.525668	0.907829	0.915386	5.71E-05
260	0.977707	8.542223	0.909592	0.914211	2.13E-05
265	0.972777	8.497529	0.904833	0.913052	6.75E-05
270	0.97915	8.555303	0.910985	0.911906	8.5E-07
275	0.975167	8.519196	0.90714	0.910776	1.32E-05
280	0.978898	8.553015	0.910741	0.909659	1.17E-06
285	0.97162	8.487035	0.903715	0.908556	2.34E-05
290	0.970248	8.474594	0.902391	0.907467	2.58E-05
295	0.970296	8.475032	0.902437	0.906392	1.56E-05
300	0.973651	8.505446	0.905676	0.90533	1.19E-07
			sum=		0.001252

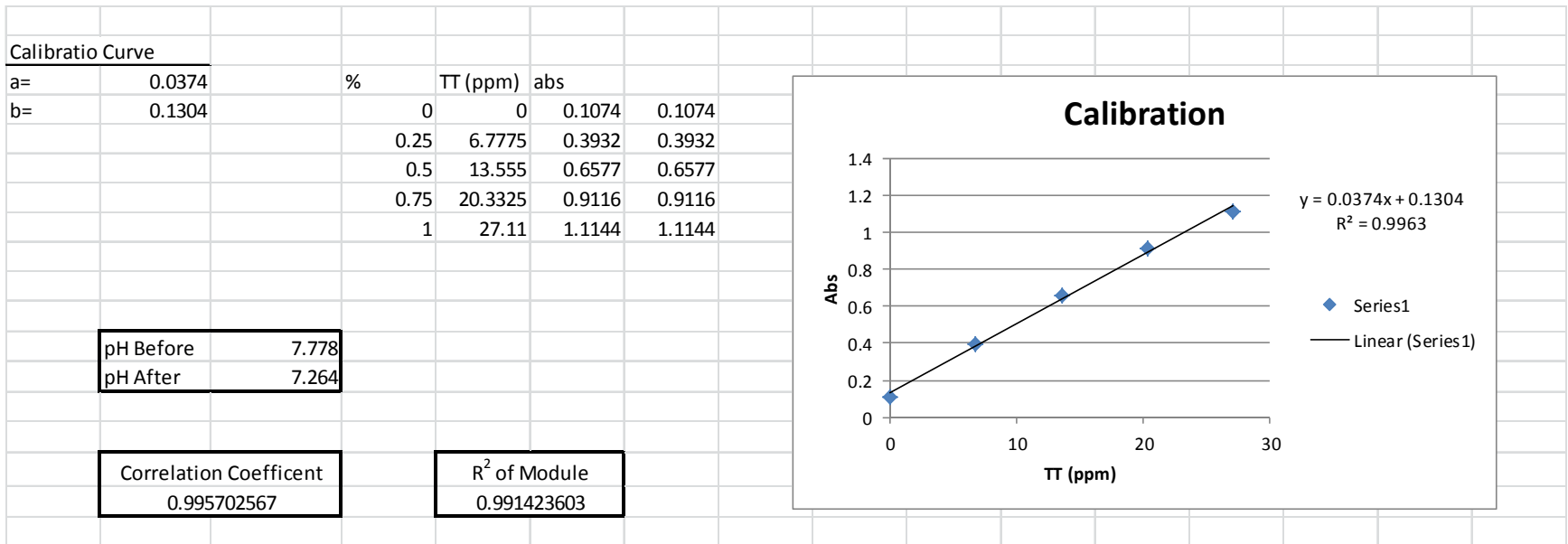


10Jul15 0.7@20%pH8					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.000141	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.066882	10.06832	1	1	0
5	1.06745	10.07388	1.000552	0.999301	1.57E-06
10	1.068568	10.08482	1.001639	0.998609	9.18E-06
15	1.065758	10.05732	0.998908	0.997926	9.64E-07
20	1.063806	10.03822	0.997011	0.997249	5.7E-08
25	1.067263	10.07204	1.00037	0.996581	1.44E-05
30	1.066126	10.06092	0.999265	0.995919	1.12E-05
35	1.063746	10.03763	0.996952	0.995265	2.85E-06
40	1.060081	10.00177	0.99339	0.994618	1.51E-06
45	1.058192	9.983288	0.991555	0.993978	5.87E-06
50	1.061567	10.01631	0.994835	0.993346	2.22E-06
55	1.054999	9.952043	0.988451	0.99272	1.82E-05
60	1.058162	9.982996	0.991526	0.992101	3.31E-07
65	1.062397	10.02444	0.995642	0.991489	1.72E-05
70	1.057306	9.974615	0.990693	0.990883	3.61E-08
75	1.056249	9.964275	0.989666	0.990285	3.82E-07
80	1.054746	9.949573	0.988206	0.989693	2.21E-06
85	1.057308	9.974636	0.990695	0.989107	2.52E-06
90	1.056111	9.962923	0.989532	0.988528	1.01E-06
95	1.053642	9.938763	0.987132	0.987955	6.77E-07
100	1.055239	9.954393	0.988685	0.987389	1.68E-06
105	1.054242	9.944633	0.987715	0.986829	7.87E-07
110	1.053548	9.937846	0.987041	0.986275	5.88E-07
115	1.053658	9.93892	0.987148	0.985727	2.02E-06
120	1.049527	9.898499	0.983133	0.985185	4.21E-06
125	1.049985	9.902983	0.983579	0.984649	1.15E-06
130	1.050172	9.90481	0.98376	0.984119	1.29E-07
135	1.047819	9.881791	0.981474	0.983595	4.5E-06
140	1.046309	9.867018	0.980007	0.983076	9.42E-06
145	1.046329	9.867207	0.980025	0.982564	6.44E-06
150	1.04582	9.862233	0.979531	0.982057	6.38E-06
155	1.048581	9.889242	0.982214	0.981555	4.34E-07
160	1.047534	9.878997	0.981196	0.981059	1.88E-08
165	1.045772	9.86176	0.979484	0.980569	1.18E-06
170	1.045481	9.85891	0.979201	0.980084	7.79E-07
175	1.044647	9.850758	0.978392	0.979604	1.47E-06
180	1.048079	9.884338	0.981727	0.979129	6.75E-06
185	1.045959	9.863592	0.979666	0.97866	1.01E-06
190	1.048072	9.884268	0.98172	0.978196	1.24E-05
195	1.042875	9.833415	0.976669	0.977737	1.14E-06
200	1.047896	9.882541	0.981548	0.977283	1.82E-05
205	1.040434	9.809526	0.974296	0.976835	6.44E-06
210	1.040753	9.812656	0.974607	0.976391	3.18E-06
215	1.042036	9.825207	0.975854	0.975952	9.55E-09
220	1.040158	9.806831	0.974029	0.975517	2.22E-06
225	1.041812	9.82301	0.975636	0.975088	3E-07
230	1.041647	9.821401	0.975476	0.974663	6.6E-07
235	1.038681	9.79238	0.972593	0.974243	2.72E-06
240	1.037735	9.783124	0.971674	0.973828	4.64E-06
245	1.04106	9.81566	0.974906	0.973417	2.22E-06
250	1.039045	9.795938	0.972947	0.973011	4.09E-09
255	1.040993	9.814996	0.97484	0.972609	4.98E-06
260	1.037223	9.778107	0.971176	0.972212	1.07E-06
265	1.038103	9.786721	0.972031	0.971819	4.53E-08
270	1.038829	9.793827	0.972737	0.97143	1.71E-06
275	1.035323	9.759516	0.969329	0.971045	2.95E-06
280	1.036628	9.772286	0.970598	0.970665	4.58E-09
285	1.03469	9.753332	0.968715	0.970289	2.48E-06
290	1.039991	9.805199	0.973867	0.969918	1.56E-05
295	1.034408	9.750567	0.968441	0.96955	1.23E-06
300	1.037601	9.781805	0.971543	0.969186	5.56E-06
			sum=		0.000231

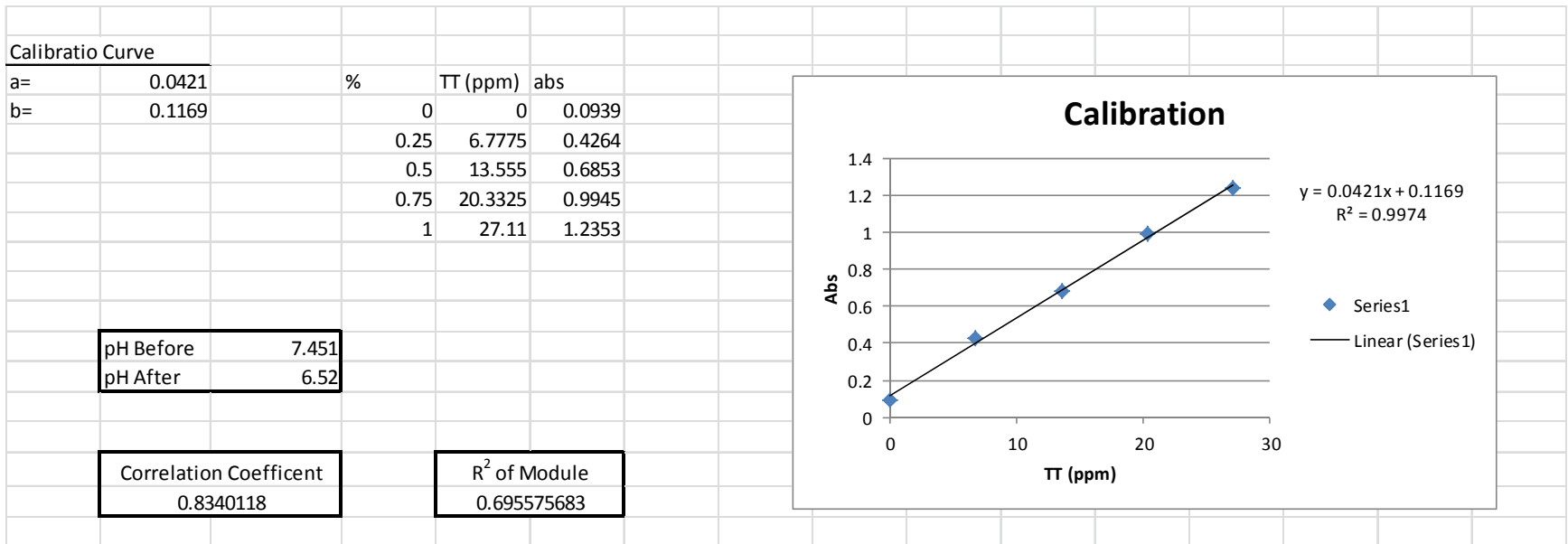


13Jul15 0.7@70%pH7					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.000511	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.127297	8.358103	1	1	0
5	1.1266	8.352762	0.999361	0.997462	3.6E-06
10	1.123517	8.32912	0.996532	0.994958	2.48E-06
15	1.123365	8.327953	0.996393	0.992485	1.53E-05
20	1.120969	8.30958	0.994195	0.990044	1.72E-05
25	1.116045	8.271814	0.989676	0.987634	4.17E-06
30	1.118339	8.289413	0.991782	0.985256	4.26E-05
35	1.115987	8.271371	0.989623	0.982907	4.51E-05
40	1.105952	8.194419	0.980416	0.980589	3E-08
45	1.107973	8.209915	0.98227	0.978301	1.58E-05
50	1.097724	8.131319	0.972867	0.976042	1.01E-05
55	1.098435	8.13677	0.973519	0.973813	8.63E-08
60	1.09797	8.133203	0.973092	0.971611	2.19E-06
65	1.091843	8.086222	0.967471	0.969439	3.87E-06
70	1.091707	8.08518	0.967346	0.967294	2.78E-09
75	1.087633	8.053932	0.963608	0.965176	2.46E-06
80	1.091654	8.084768	0.967297	0.963086	1.77E-05
85	1.083282	8.020566	0.959616	0.961023	1.98E-06
90	1.079975	7.995204	0.956581	0.958986	5.78E-06
95	1.079214	7.989368	0.955883	0.956975	1.19E-06
100	1.076547	7.968917	0.953436	0.95499	2.41E-06
105	1.081324	8.005555	0.95782	0.953031	2.29E-05
110	1.07645	7.968174	0.953347	0.951097	5.07E-06
115	1.067415	7.898891	0.945058	0.949187	1.71E-05
120	1.072539	7.938183	0.949759	0.947302	6.04E-06
125	1.065826	7.886702	0.9436	0.945442	3.39E-06
130	1.062752	7.863126	0.940779	0.943605	7.99E-06
135	1.064926	7.879803	0.942774	0.941792	9.65E-07
140	1.056231	7.81312	0.934796	0.940002	2.71E-05
145	1.064671	7.877848	0.94254	0.938235	1.85E-05
150	1.056672	7.816507	0.935201	0.936491	1.66E-06
155	1.054234	7.797803	0.932963	0.934769	3.26E-06
160	1.053548	7.79255	0.932335	0.933069	5.4E-07
165	1.061103	7.850483	0.939266	0.931391	6.2E-05
170	1.051631	7.777847	0.930576	0.929735	7.06E-07
175	1.047657	7.74737	0.926929	0.9281	1.37E-06
180	1.046672	7.73982	0.926026	0.926486	2.12E-07
185	1.044408	7.722456	0.923948	0.924893	8.92E-07
190	1.039998	7.688634	0.919902	0.92332	1.17E-05
195	1.041833	7.70271	0.921586	0.921767	3.29E-08
200	1.03743	7.668938	0.917545	0.920235	7.23E-06
205	1.042751	7.709744	0.922428	0.918722	1.37E-05
210	1.037382	7.66857	0.917501	0.917228	7.46E-08
215	1.032413	7.630464	0.912942	0.915754	7.91E-06
220	1.031074	7.620202	0.911714	0.914298	6.68E-06
225	1.033664	7.640065	0.914091	0.912862	1.51E-06
230	1.026413	7.584455	0.907437	0.911443	1.6E-05
235	1.03648	7.661659	0.916674	0.910043	4.4E-05
240	1.025751	7.57938	0.90683	0.908661	3.35E-06
245	1.024019	7.566093	0.905241	0.907297	4.23E-06
250	1.024329	7.568471	0.905525	0.90595	1.81E-07
255	1.019777	7.533565	0.901349	0.904621	1.07E-05
260	1.021593	7.547493	0.903015	0.903308	8.58E-08
265	1.024349	7.568628	0.905544	0.902013	1.25E-05
270	1.018423	7.523183	0.900107	0.900734	3.93E-07
275	1.023699	7.563644	0.904947	0.899471	3E-05
280	1.014235	7.491069	0.896264	0.898225	3.84E-06
285	1.019441	7.530993	0.901041	0.896994	1.64E-05
290	1.013931	7.488738	0.895985	0.89578	4.22E-08
295	1.010089	7.459269	0.89246	0.894581	4.5E-06
300	1.009663	7.456001	0.892069	0.893398	1.77E-06
			sum=	0.000571	





14Jul15 0.7@100%pH7H2O2Ctrl					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	-4.8E-05	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.122369	9.240966	1	1	0
5	1.124769	9.2615	1.002222	1.000238	3.94E-06
10	1.124286	9.257364	1.001774	1.000473	1.69E-06
15	1.122663	9.243482	1.000272	1.000706	1.88E-07
20	1.122574	9.242719	1.00019	1.000937	5.59E-07
25	1.122326	9.240597	0.99996	1.001166	1.45E-06
30	1.128052	9.289578	1.00526	1.001392	1.5E-05
35	1.120137	9.221872	0.997934	1.001615	1.36E-05
40	1.127716	9.286707	1.00495	1.001837	9.69E-06
45	1.122494	9.242039	1.000116	1.002056	3.76E-06
50	1.126376	9.275242	1.003709	1.002273	2.06E-06
55	1.123865	9.253765	1.001385	1.002488	1.22E-06
60	1.124652	9.260499	1.002114	1.002701	3.45E-07
65	1.125034	9.263761	1.002467	1.002912	1.98E-07
70	1.126515	9.276431	1.003838	1.00312	5.15E-07
75	1.125133	9.264612	1.002559	1.003327	5.9E-07
80	1.125053	9.263925	1.002484	1.003531	1.1E-06
85	1.122693	9.243738	1.0003	1.003733	1.18E-05
90	1.126802	9.278885	1.004103	1.003933	2.89E-08
95	1.131019	9.314962	1.008007	1.004132	1.5E-05
100	1.124052	9.255362	1.001558	1.004328	7.67E-06
105	1.124213	9.256738	1.001707	1.004522	7.93E-06
110	1.125966	9.271736	1.00333	1.004714	1.92E-06
115	1.126138	9.273209	1.003489	1.004905	2E-06
120	1.125806	9.270367	1.003182	1.005093	3.65E-06
125	1.129217	9.299543	1.006339	1.005279	1.12E-06
130	1.124727	9.261142	1.002183	1.005464	1.08E-05
135	1.131463	9.31876	1.008418	1.005647	7.68E-06
140	1.1273	9.283151	1.004565	1.005828	1.59E-06
145	1.12937	9.300852	1.006481	1.006007	2.24E-07
150	1.129982	9.306091	1.007047	1.006184	7.45E-07
155	1.128404	9.292594	1.005587	1.00636	5.97E-07
160	1.134	9.340466	1.010767	1.006533	1.79E-05
165	1.124939	9.262949	1.002379	1.006705	1.87E-05
170	1.125991	9.271953	1.003353	1.006876	1.24E-05
175	1.127111	9.281532	1.00439	1.007044	7.05E-06
180	1.128644	9.294644	1.005809	1.007211	1.97E-06
185	1.12807	9.289734	1.005277	1.007376	4.4E-06
190	1.130624	9.311586	1.007642	1.00754	1.05E-08
195	1.13548	9.353125	1.012137	1.007701	1.97E-05
200	1.13126	9.317024	1.008231	1.007862	1.36E-07
205	1.12994	9.305729	1.007008	1.00802	1.02E-06
210	1.137203	9.367864	1.013732	1.008177	3.09E-05
215	1.134822	9.347493	1.011528	1.008333	1.02E-05
220	1.128847	9.296382	1.005997	1.008486	6.2E-06
225	1.131729	9.321039	1.008665	1.008639	6.95E-10
230	1.131298	9.317347	1.008265	1.008789	2.75E-07
235	1.131314	9.317488	1.008281	1.008939	4.33E-07
240	1.127706	9.286617	1.00494	1.009086	1.72E-05
245	1.133226	9.333844	1.010051	1.009233	6.69E-07
250	1.134227	9.342401	1.010977	1.009377	2.56E-06
255	1.134057	9.340948	1.010819	1.009521	1.69E-06
260	1.133604	9.337077	1.010401	1.009662	5.45E-07
265	1.133405	9.335374	1.010216	1.009803	1.71E-07
270	1.134779	9.34713	1.011488	1.009942	2.39E-06
275	1.132816	9.330337	1.009671	1.01008	1.67E-07
280	1.133189	9.333527	1.010016	1.010216	3.97E-08
285	1.136019	9.357731	1.012636	1.010351	5.22E-06
290	1.133089	9.33267	1.009924	1.010484	3.14E-07
295	1.135788	9.355758	1.012422	1.010616	3.26E-06
300	1.133579	9.336861	1.010377	1.010747	1.37E-07
			sum=	0.000294	



15Jul15 0.7@0%pH8					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	9.88E-06	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.032964	6.584469	1	1	0
5	1.027988	6.551666	0.995018	0.999951	2.43E-05
10	1.027815	6.550527	0.994845	0.999902	2.56E-05
15	1.029322	6.560464	0.996354	0.999854	1.22E-05
20	1.029073	6.558818	0.996104	0.999806	1.37E-05
25	1.030498	6.568213	0.997531	0.999759	4.96E-06
30	1.030018	6.565047	0.99705	0.999713	7.09E-06
35	1.030133	6.565807	0.997166	0.999666	6.25E-06
40	1.031441	6.574428	0.998475	0.999621	1.31E-06
45	1.030505	6.568259	0.997538	0.999576	4.15E-06
50	1.028054	6.5521	0.995084	0.999531	1.98E-05
55	1.034395	6.5939	1.001432	0.999487	3.79E-06
60	1.035699	6.602495	1.002738	0.999443	1.09E-05
65	1.031571	6.575289	0.998606	0.999399	6.3E-07
70	1.030799	6.570198	0.997833	0.999356	2.32E-06
75	1.030987	6.571434	0.99802	0.999314	1.67E-06
80	1.032289	6.580018	0.999324	0.999272	2.71E-09
85	1.028216	6.553174	0.995247	0.99923	1.59E-05
90	1.028435	6.554614	0.995466	0.999189	1.39E-05
95	1.027328	6.547319	0.994358	0.999148	2.29E-05
100	1.029095	6.558962	0.996126	0.999108	8.89E-06
105	1.031768	6.576584	0.998802	0.999068	7.06E-08
110	1.030516	6.568332	0.997549	0.999029	2.19E-06
115	1.028942	6.557955	0.995973	0.99899	9.1E-06
120	1.030314	6.567001	0.997347	0.998951	2.57E-06
125	1.03199	6.578049	0.999025	0.998913	1.26E-08
130	1.030079	6.565448	0.997111	0.998875	3.11E-06
135	1.031352	6.573842	0.998386	0.998837	2.04E-07
140	1.030528	6.568409	0.997561	0.9988	1.54E-06
145	1.035907	6.60387	1.002947	0.998763	1.75E-05
150	1.030297	6.566889	0.99733	0.998727	1.95E-06
155	1.028803	6.557041	0.995834	0.998691	8.16E-06
160	1.02956	6.562028	0.996592	0.998656	4.26E-06
165	1.031895	6.577421	0.99893	0.99862	9.56E-08
170	1.032304	6.580117	0.999339	0.998586	5.68E-07
175	1.034119	6.592082	1.001156	0.998551	6.79E-06
180	1.028755	6.556727	0.995787	0.998517	7.45E-06
185	1.030184	6.566145	0.997217	0.998483	1.6E-06
190	1.028857	6.557393	0.995888	0.99845	6.56E-06
195	1.032383	6.580642	0.999419	0.998417	1E-06
200	1.029263	6.560073	0.996295	0.998384	4.36E-06
205	1.033191	6.585965	1.000227	0.998351	3.52E-06
210	1.02989	6.564206	0.996923	0.998319	1.95E-06
215	1.029156	6.559365	0.996187	0.998288	4.41E-06
220	1.03164	6.575741	0.998674	0.998256	1.75E-07
225	1.03172	6.576267	0.998754	0.998225	2.8E-07
230	1.030824	6.570361	0.997857	0.998194	1.14E-07
235	1.030044	6.565218	0.997076	0.998164	1.18E-06
240	1.032248	6.579747	0.999283	0.998134	1.32E-06
245	1.031637	6.57572	0.998671	0.998104	3.22E-07
250	1.030129	6.565778	0.997161	0.998075	8.34E-07
255	1.031917	6.577567	0.998952	0.998045	8.21E-07
260	1.032271	6.579899	0.999306	0.998017	1.66E-06
265	1.032304	6.580117	0.999339	0.997988	1.83E-06
270	1.034697	6.595895	1.001735	0.99796	1.43E-05
275	1.034623	6.595405	1.001661	0.997932	1.39E-05
280	1.032794	6.583349	0.99983	0.997904	3.71E-06
285	1.033015	6.584806	1.000051	0.997877	4.73E-06
290	1.032575	6.581903	0.99961	0.997849	3.1E-06
295	1.034345	6.593573	1.001383	0.997823	1.27E-05
300	1.03047	6.568031	0.997503	0.997796	8.56E-08
			sum=		0.00035

Calibratio Curve					
a=	0.0341	%	TT (ppm)	abs	
b=	0.1517	0	0	0.1285	0.1285
		0.25	6.7775	0.3935	0.3935
		0.5	13.555	0.6383	0.6383
		0.75	20.3325	0.8542	0.8542
		1	27.11	1.0522	1.0522

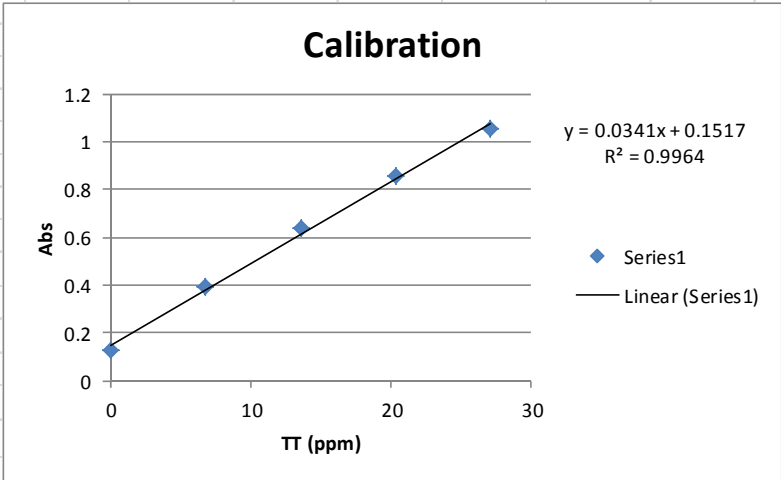
  

pH Before	8.164
pH After	8.059

Correlation Coefficient	-0.342715353
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R <sup>2</sup> of Module	0.117453813
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16Jul15 0.7@100%pH7					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	9.88E-06	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.148655	36.44917	1	1	0
5	1.147227	36.40219	0.998711	0.999951	1.54E-06
10	1.147631	36.4155	0.999076	0.999902	6.82E-07
15	1.152025	36.56004	1.003042	0.999854	1.02E-05
20	1.152366	36.57126	1.00335	0.999806	1.26E-05
25	1.153865	36.62055	1.004702	0.999759	2.44E-05
30	1.151102	36.52966	1.002208	0.999713	6.23E-06
35	1.149988	36.49304	1.001204	0.999666	2.36E-06
40	1.150893	36.5228	1.00202	0.999621	5.76E-06
45	1.142974	36.2623	0.994873	0.999576	2.21E-05
50	1.144872	36.32474	0.996586	0.999531	8.67E-06
55	1.145516	36.34591	0.997167	0.999487	5.38E-06
60	1.15245	36.574	1.003425	0.999443	1.59E-05
65	1.145917	36.3591	0.997529	0.999399	3.5E-06
70	1.148742	36.45203	1.000079	0.999356	5.22E-07
75	1.14745	36.40954	0.998913	0.999314	1.61E-07
80	1.147005	36.39489	0.998511	0.999272	5.79E-07
85	1.145357	36.3407	0.997024	0.99923	4.87E-06
90	1.152532	36.57671	1.003499	0.999189	1.86E-05
95	1.150652	36.51486	1.001802	0.999148	7.04E-06
100	1.154567	36.64366	1.005336	0.999108	3.88E-05
105	1.147133	36.39913	0.998627	0.999068	1.94E-07
110	1.14633	36.3727	0.997902	0.999029	1.27E-06
115	1.150652	36.51487	1.001802	0.99899	7.91E-06
120	1.144896	36.32554	0.996608	0.998951	5.49E-06
125	1.147619	36.41509	0.999065	0.998913	2.33E-08
130	1.149819	36.48748	1.001051	0.998875	4.74E-06
135	1.14695	36.39308	0.998461	0.998837	1.41E-07
140	1.14482	36.32303	0.996539	0.9988	5.11E-06
145	1.147915	36.42482	0.999332	0.998763	3.23E-07
150	1.146639	36.38285	0.998181	0.998727	2.99E-07
155	1.151927	36.55682	1.002954	0.998691	1.82E-05
160	1.151135	36.53074	1.002238	0.998656	1.28E-05
165	1.149057	36.46241	1.000363	0.99862	3.04E-06
170	1.150913	36.52345	1.002038	0.998586	1.19E-05
175	1.146207	36.36864	0.997791	0.998551	5.78E-07
180	1.157181	36.72962	1.007694	0.998517	8.42E-05
185	1.149079	36.46312	1.000383	0.998483	3.61E-06
190	1.151374	36.53863	1.002454	0.99845	1.6E-05
195	1.146112	36.36554	0.997706	0.998417	5.05E-07
200	1.144924	36.32646	0.996633	0.998384	3.06E-06
205	1.149696	36.48343	1.00094	0.998351	6.7E-06
210	1.149293	36.47017	1.000576	0.998319	5.09E-06
215	1.150159	36.49865	1.001358	0.998288	9.42E-06
220	1.150695	36.51627	1.001841	0.998256	1.29E-05
225	1.148021	36.42833	0.999428	0.998225	1.45E-06
230	1.150843	36.52116	1.001975	0.998194	1.43E-05
235	1.147017	36.3953	0.998522	0.998164	1.28E-07
240	1.151239	36.53418	1.002332	0.998134	1.76E-05
245	1.15491	36.65493	1.005645	0.998104	5.69E-05
250	1.153899	36.62166	1.004733	0.998075	4.43E-05
255	1.146356	36.37356	0.997926	0.998045	1.44E-08
260	1.145887	36.35814	0.997503	0.998017	2.64E-07
265	1.154231	36.63259	1.005032	0.997988	4.96E-05
270	1.15017	36.49902	1.001368	0.99796	1.16E-05
275	1.149101	36.46385	1.000403	0.997932	6.11E-06
280	1.150671	36.51551	1.00182	0.997904	1.53E-05
285	1.153143	36.5968	1.00405	0.997877	3.81E-05
290	1.149215	36.46758	1.000505	0.997849	7.05E-06
295	1.150167	36.49893	1.001365	0.997823	1.25E-05
300	1.150449	36.50818	1.001619	0.997796	1.46E-05
			sum=		0.000693

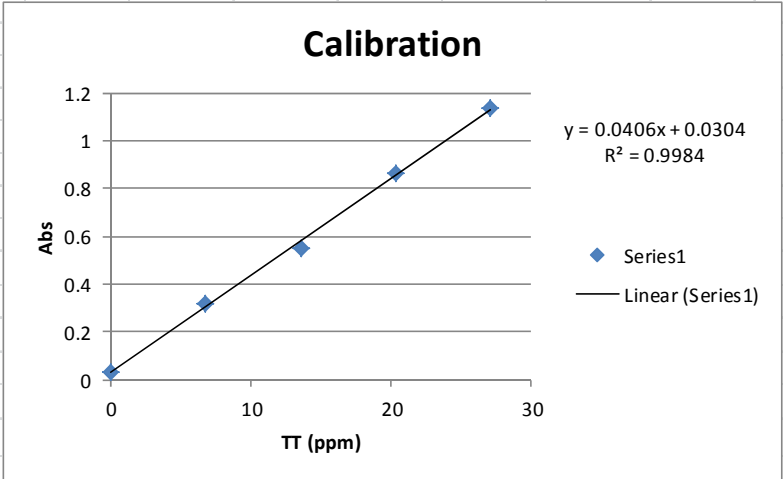
Calibratio Curve					
a=	0.0406	%	TT (ppm)	abs	
b=	0.0304	0	0	0.0329	0.0329
		0.25	6.7775	0.3192	0.3192
		0.5	13.555	0.5505	0.5505
		0.75	20.3325	0.8662	0.8662
		1	27.11	1.1354	1.1354

pH Before	7.896
pH After	7.684

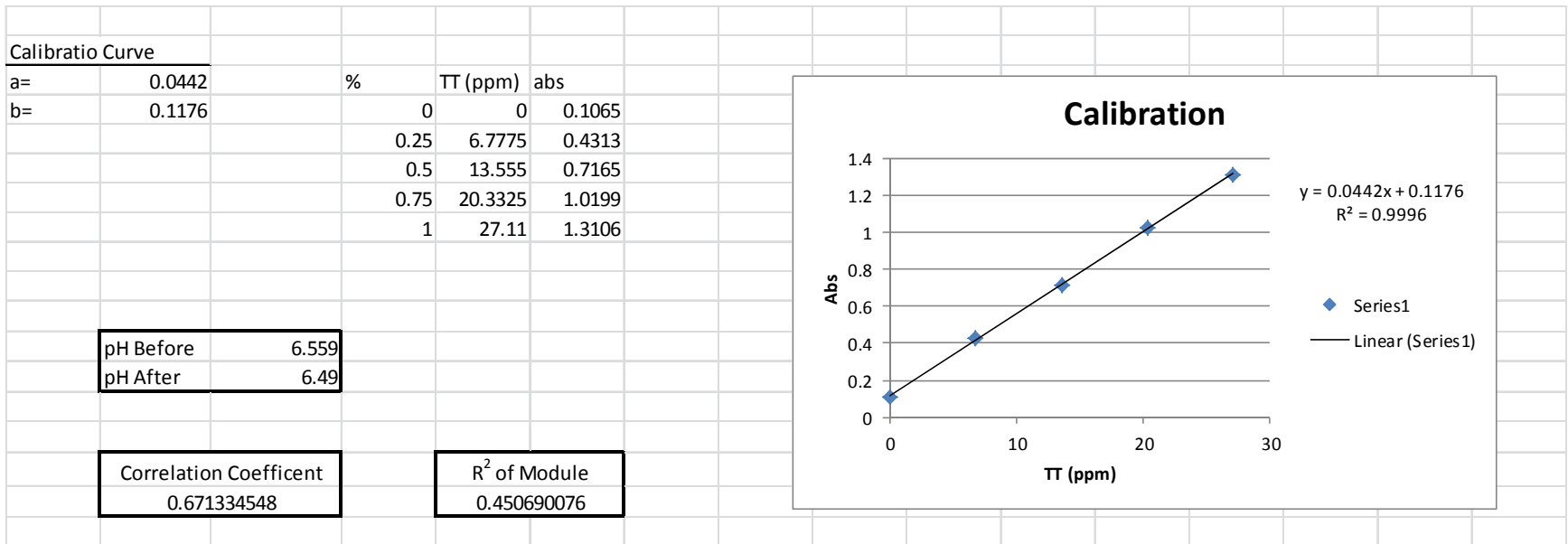
  

Correlation Coefficient	$R^2$ of Module
-0.164422772	0.027034848

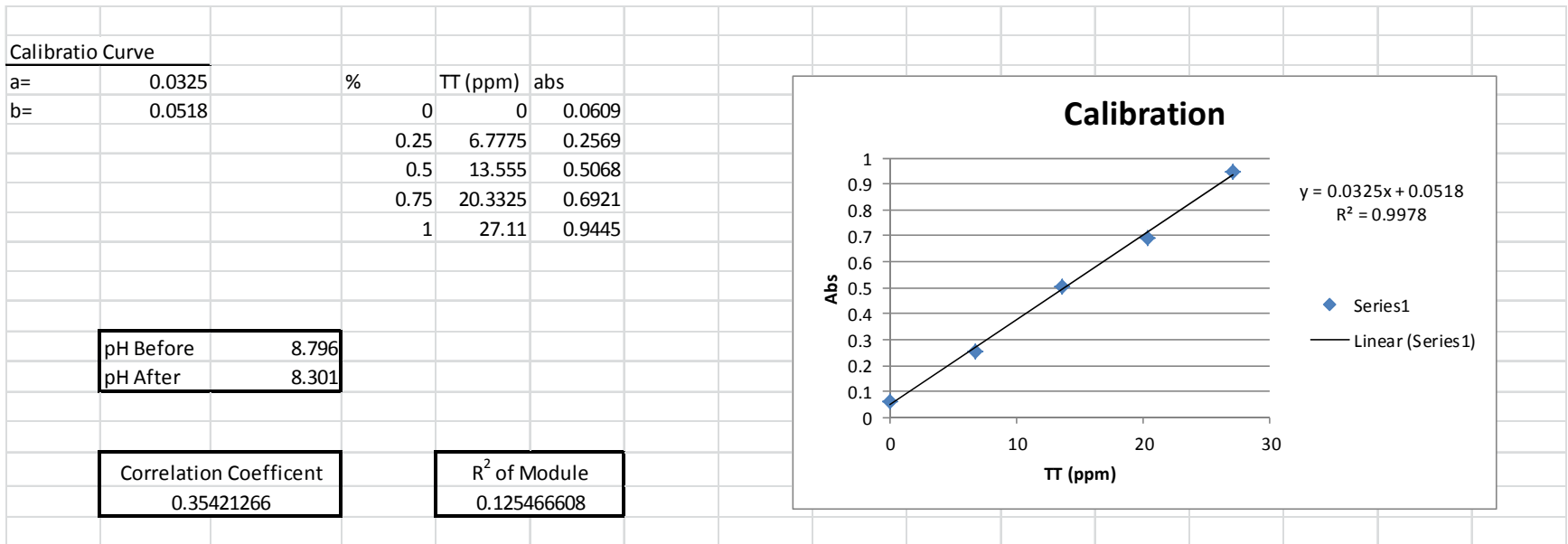


17Jul15 0.7@100%pH6H2O2Ctrl					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	-2.4E-05	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.219664	9.99544	1	1	0
5	1.220991	10.00672	1.001129	1.00012	1.02E-06
10	1.216736	9.970548	0.99751	1.000238	7.44E-06
15	1.22108	10.00749	1.001205	1.000355	7.23E-07
20	1.222512	10.01966	1.002423	1.000471	3.81E-06
25	1.224149	10.03358	1.003816	1.000586	1.04E-05
30	1.218693	9.987181	0.999174	1.000699	2.33E-06
35	1.224369	10.03545	1.004003	1.000812	1.02E-05
40	1.222574	10.02018	1.002475	1.000923	2.41E-06
45	1.223897	10.03144	1.003601	1.001033	6.6E-06
50	1.219209	9.991574	0.999613	1.001142	2.34E-06
55	1.221074	10.00744	1.0012	1.00125	2.48E-09
60	1.221347	10.00975	1.001432	1.001357	5.67E-09
65	1.220108	9.999218	1.000378	1.001462	1.18E-06
70	1.218392	9.984628	0.998918	1.001567	7.02E-06
75	1.220226	10.00022	1.000478	1.001671	1.42E-06
80	1.219218	9.991646	0.99962	1.001773	4.63E-06
85	1.222747	10.02166	1.002623	1.001875	5.6E-07
90	1.223442	10.02756	1.003214	1.001975	1.53E-06
95	1.220313	10.00096	1.000553	1.002074	2.32E-06
100	1.219841	9.996943	1.00015	1.002173	4.09E-06
105	1.219205	9.991539	0.99961	1.00227	7.08E-06
110	1.225183	10.04237	1.004695	1.002367	5.42E-06
115	1.217303	9.975369	0.997992	1.002462	2E-05
120	1.220792	10.00503	1.00096	1.002556	2.55E-06
125	1.223385	10.02708	1.003165	1.00265	2.66E-07
130	1.221247	10.0089	1.001347	1.002742	1.95E-06
135	1.219708	9.995817	1.000038	1.002834	7.82E-06
140	1.219231	9.991764	0.999632	1.002925	1.08E-05
145	1.221147	10.00805	1.001262	1.003014	3.07E-06
150	1.220875	10.00574	1.001031	1.003103	4.3E-06
155	1.226355	10.05234	1.005693	1.003191	6.26E-06
160	1.22249	10.01947	1.002405	1.003278	7.63E-07
165	1.221625	10.01212	1.001668	1.003364	2.88E-06
170	1.222907	10.02302	1.002759	1.003449	4.76E-07
175	1.220419	10.00186	1.000642	1.003534	8.36E-06
180	1.223402	10.02723	1.00318	1.003617	1.91E-07
185	1.222823	10.02231	1.002688	1.0037	1.02E-06
190	1.222456	10.01919	1.002376	1.003782	1.98E-06
195	1.22335	10.02679	1.003136	1.003863	5.28E-07
200	1.224047	10.03271	1.003729	1.003943	4.57E-08
205	1.227199	10.05952	1.006411	1.004022	5.71E-06
210	1.224787	10.039	1.004358	1.004101	6.63E-08
215	1.221443	10.01057	1.001514	1.004178	7.1E-06
220	1.223971	10.03207	1.003665	1.004255	3.49E-07
225	1.227032	10.0581	1.006269	1.004331	3.75E-06
230	1.226483	10.05343	1.005802	1.004407	1.95E-06
235	1.227157	10.05916	1.006375	1.004481	3.59E-06
240	1.230831	10.0904	1.009501	1.004555	2.45E-05
245	1.228028	10.06657	1.007116	1.004628	6.19E-06
250	1.225157	10.04215	1.004673	1.004701	7.57E-10
255	1.225779	10.04744	1.005202	1.004772	1.85E-07
260	1.228406	10.06978	1.007437	1.004843	6.73E-06
265	1.227172	10.05929	1.006388	1.004913	2.17E-06
270	1.222178	10.01682	1.002139	1.004983	8.09E-06
275	1.225338	10.04369	1.004827	1.005051	5.04E-08
280	1.225498	10.04505	1.004964	1.005119	2.43E-08
285	1.22537	10.04396	1.004854	1.005187	1.1E-07
290	1.229901	10.08249	1.008709	1.005253	1.19E-05
295	1.225596	10.04588	1.005047	1.005319	7.43E-08
300	1.227913	10.06559	1.007018	1.005385	2.67E-06
			sum=		0.000241

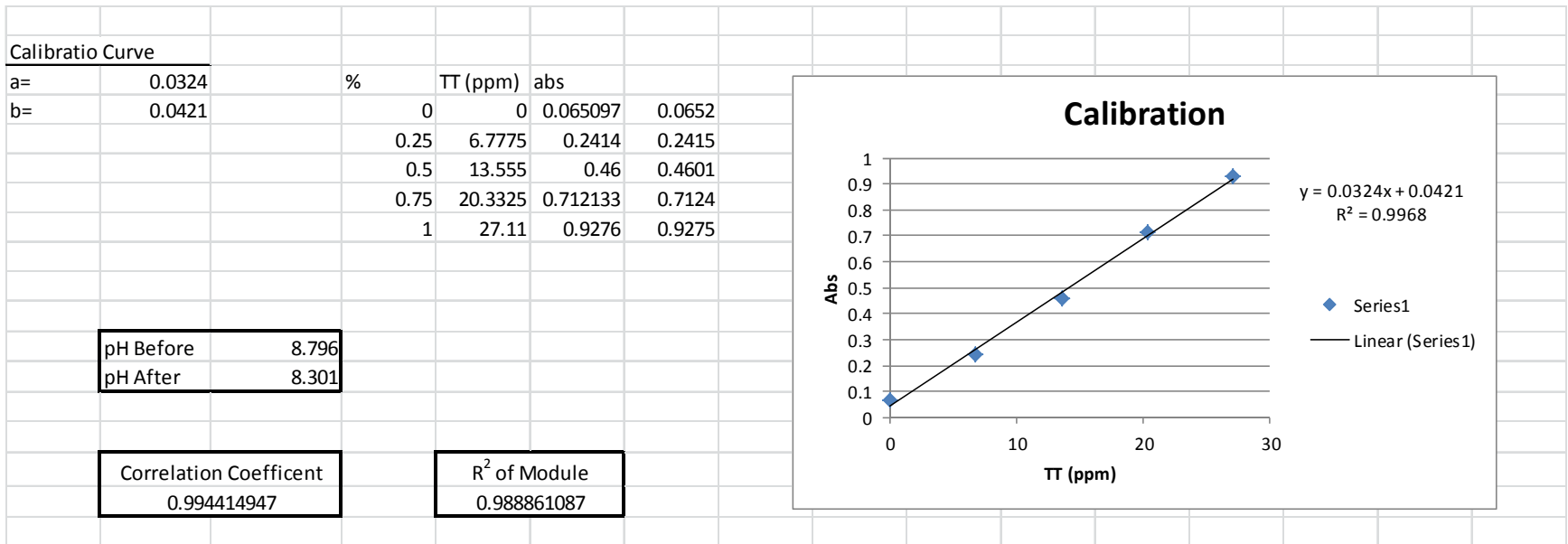




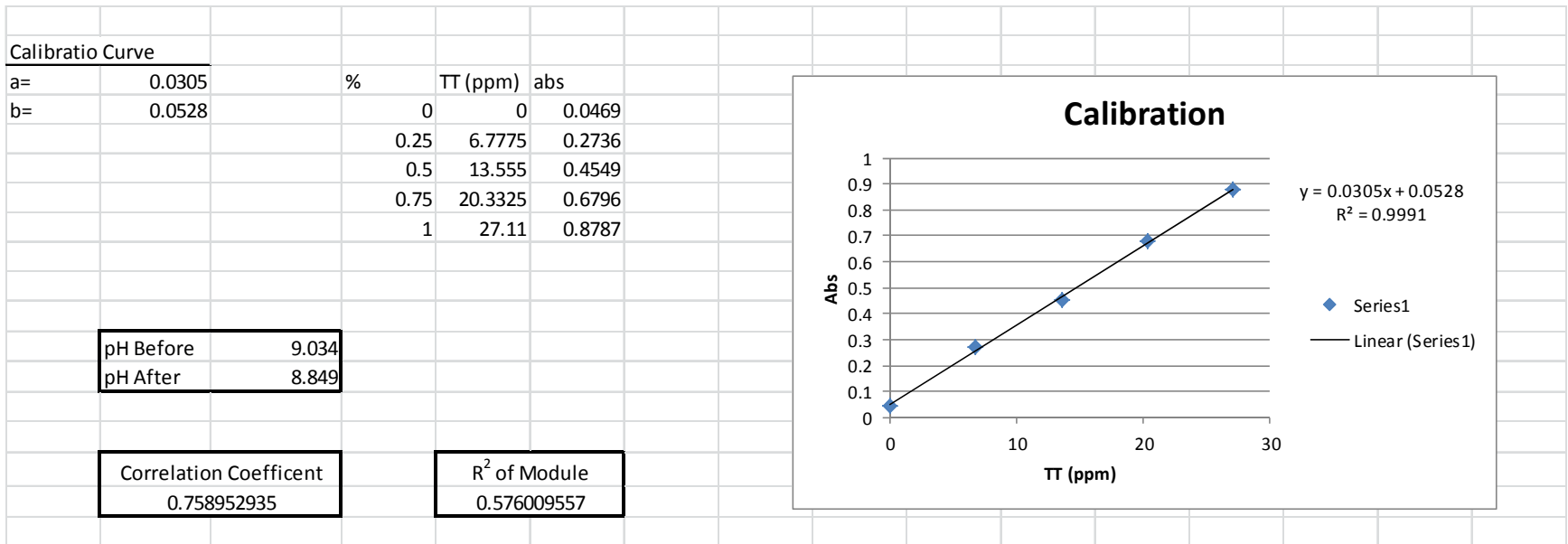
21Jul15 0.7@5%pH8					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	-3.8E-06	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	0.919907	17.13141	1	1	0
5	0.919112	17.11607	0.999105	1.000019	8.36E-07
10	0.919111	17.11605	0.999103	1.000038	8.73E-07
15	0.918874	17.11147	0.998836	1.000056	1.49E-06
20	0.919696	17.12733	0.999762	1.000074	9.76E-08
25	0.919887	17.13102	0.999977	1.000093	1.33E-08
30	0.916442	17.06452	0.996095	1.000111	1.61E-05
35	0.919867	17.13064	0.999955	1.000128	2.99E-08
40	0.9191	17.11584	0.999091	1.000146	1.11E-06
45	0.919644	17.12633	0.999704	1.000163	2.11E-07
50	0.92049	17.14267	1.000657	1.00018	2.27E-07
55	0.918074	17.09602	0.997934	1.000198	5.12E-06
60	0.920312	17.13922	1.000456	1.000214	5.84E-08
65	0.919912	17.1315	1.000005	1.000231	5.1E-08
70	0.920966	17.15185	1.001193	1.000248	8.95E-07
75	0.918707	17.10825	0.998648	1.000264	2.61E-06
80	0.921348	17.15923	1.001624	1.00028	1.81E-06
85	0.91785	17.0917	0.997682	1.000296	6.83E-06
90	0.919277	17.11925	0.99929	1.000312	1.04E-06
95	0.917546	17.08583	0.997339	1.000328	8.93E-06
100	0.919092	17.11568	0.999082	1.000343	1.59E-06
105	0.923484	17.20047	1.004031	1.000359	1.35E-05
110	0.9219	17.16988	1.002246	1.000374	3.51E-06
115	0.921099	17.15443	1.001344	1.000389	9.12E-07
120	0.92163	17.16467	1.001942	1.000404	2.37E-06
125	0.920499	17.14284	1.000667	1.000418	6.19E-08
130	0.918659	17.10731	0.998594	1.000433	3.38E-06
135	0.919477	17.1231	0.999515	1.000447	8.69E-07
140	0.918395	17.10222	0.998296	1.000462	4.69E-06
145	0.918912	17.1122	0.998879	1.000476	2.55E-06
150	0.919503	17.12362	0.999545	1.00049	8.93E-07
155	0.919258	17.11889	0.999269	1.000504	1.52E-06
160	0.919876	17.1308	0.999965	1.000517	3.06E-07
165	0.91886	17.11119	0.99882	1.000531	2.93E-06
170	0.91968	17.12702	0.999744	1.000544	6.4E-07
175	0.918688	17.10787	0.998626	1.000558	3.73E-06
180	0.916786	17.07116	0.996483	1.000571	1.67E-05
185	0.923407	17.19899	1.003945	1.000584	1.13E-05
190	0.918687	17.10787	0.998626	1.000597	3.88E-06
195	0.923699	17.20461	1.004273	1.00061	1.34E-05
200	0.922243	17.17651	1.002633	1.000622	4.04E-06
205	0.918553	17.10528	0.998475	1.000635	4.67E-06
210	0.919148	17.11676	0.999145	1.000647	2.26E-06
215	0.920675	17.14624	1.000866	1.000659	4.26E-08
220	0.919341	17.12048	0.999362	1.000671	1.71E-06
225	0.920077	17.13469	1.000191	1.000683	2.42E-07
230	0.917944	17.09352	0.997788	1.000695	8.45E-06
235	0.920228	17.1376	1.000361	1.000707	1.19E-07
240	0.921788	17.16771	1.002119	1.000719	1.96E-06
245	0.924806	17.22599	1.005521	1.00073	2.3E-05
250	0.918449	17.10327	0.998357	1.000741	5.68E-06
255	0.917183	17.07883	0.996931	1.000753	1.46E-05
260	0.920958	17.1517	1.001185	1.000764	1.77E-07
265	0.920651	17.14577	1.000839	1.000775	4.07E-09
270	0.921141	17.15523	1.00139	1.000786	3.66E-07
275	0.922384	17.17923	1.002792	1.000797	3.98E-06
280	0.923795	17.20647	1.004382	1.000807	1.28E-05
285	0.921688	17.16579	1.002007	1.000818	1.41E-06
290	0.924598	17.22197	1.005286	1.000828	1.99E-05
295	0.920918	17.15093	1.00114	1.000839	9.06E-08
300	0.921532	17.16278	1.001831	1.000849	9.65E-07
			sum=		0.000243



21Jul15 0.7@70%pH9					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.000263	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	0.908631	20.81308	1	1	0
5	0.909805	20.84097	1.00134	0.998694	7E-06
10	0.906645	20.76592	0.997734	0.997403	1.1E-07
15	0.908959	20.82087	1.000374	0.996128	1.8E-05
20	0.906432	20.76086	0.997491	0.994867	6.89E-06
25	0.906279	20.75723	0.997317	0.993621	1.37E-05
30	0.903117	20.68212	0.993708	0.992389	1.74E-06
35	0.900532	20.6207	0.990757	0.991171	1.72E-07
40	0.905263	20.73308	0.996156	0.989968	3.83E-05
45	0.900422	20.61809	0.990632	0.988779	3.43E-06
50	0.898675	20.57659	0.988638	0.987603	1.07E-06
55	0.897854	20.55709	0.987701	0.986441	1.59E-06
60	0.898898	20.58191	0.988893	0.985293	1.3E-05
65	0.897537	20.54957	0.987339	0.984158	1.01E-05
70	0.893284	20.44855	0.982486	0.983036	3.03E-07
75	0.895073	20.49105	0.984528	0.981927	6.76E-06
80	0.896427	20.5232	0.986072	0.980831	2.75E-05
85	0.893811	20.46107	0.983087	0.979748	1.11E-05
90	0.893771	20.46012	0.983042	0.978678	1.9E-05
95	0.890278	20.37716	0.979056	0.977619	2.06E-06
100	0.888563	20.33641	0.977098	0.976574	2.75E-07
105	0.887028	20.29994	0.975346	0.97554	3.77E-08
110	0.890295	20.37756	0.979075	0.974518	2.08E-05
115	0.885664	20.26756	0.97379	0.973508	7.92E-08
120	0.887024	20.29985	0.975341	0.97251	8.01E-06
125	0.884284	20.23478	0.972215	0.971524	4.77E-07
130	0.886953	20.29818	0.975261	0.970549	2.22E-05
135	0.882287	20.18734	0.969935	0.969585	1.23E-07
140	0.883399	20.21375	0.971205	0.968633	6.62E-06
145	0.878521	20.09788	0.965637	0.967691	4.22E-06
150	0.879859	20.12966	0.967164	0.966761	1.63E-07
155	0.880304	20.14024	0.967672	0.965841	3.35E-06
160	0.878055	20.08682	0.965106	0.964932	3.03E-08
165	0.878038	20.08641	0.965086	0.964033	1.11E-06
170	0.875997	20.03794	0.962757	0.963145	1.51E-07
175	0.874457	20.00135	0.960999	0.962268	1.61E-06
180	0.874876	20.01131	0.961478	0.9614	5.97E-09
185	0.877131	20.06487	0.964051	0.960543	1.23E-05
190	0.872262	19.94921	0.958494	0.959695	1.44E-06
195	0.872968	19.96599	0.9593	0.958858	1.96E-07
200	0.870661	19.91118	0.956667	0.95803	1.86E-06
205	0.87056	19.90878	0.956552	0.957212	4.36E-07
210	0.872261	19.94918	0.958493	0.956403	4.37E-06
215	0.868608	19.86242	0.954324	0.955604	1.64E-06
220	0.86851	19.8601	0.954213	0.954814	3.61E-07
225	0.869756	19.88968	0.955634	0.954033	2.56E-06
230	0.864986	19.77639	0.95019	0.953261	9.43E-06
235	0.866487	19.81204	0.951903	0.952498	3.54E-07
240	0.865188	19.7812	0.950422	0.951744	1.75E-06
245	0.864756	19.77093	0.949928	0.950999	1.15E-06
250	0.862065	19.707	0.946856	0.950262	1.16E-05
255	0.859516	19.64647	0.943948	0.949534	3.12E-05
260	0.86223	19.71093	0.947045	0.948815	3.13E-06
265	0.864209	19.75794	0.949304	0.948104	1.44E-06
270	0.863376	19.73814	0.948353	0.947401	9.07E-07
275	0.860978	19.68119	0.945617	0.946706	1.19E-06
280	0.857567	19.60016	0.941723	0.946019	1.85E-05
285	0.859707	19.651	0.944166	0.945341	1.38E-06
290	0.861253	19.68772	0.94593	0.94467	1.59E-06
295	0.857208	19.59165	0.941314	0.944007	7.25E-06
300	0.85842	19.62043	0.942697	0.943351	4.28E-07
			sum=	0.000368	

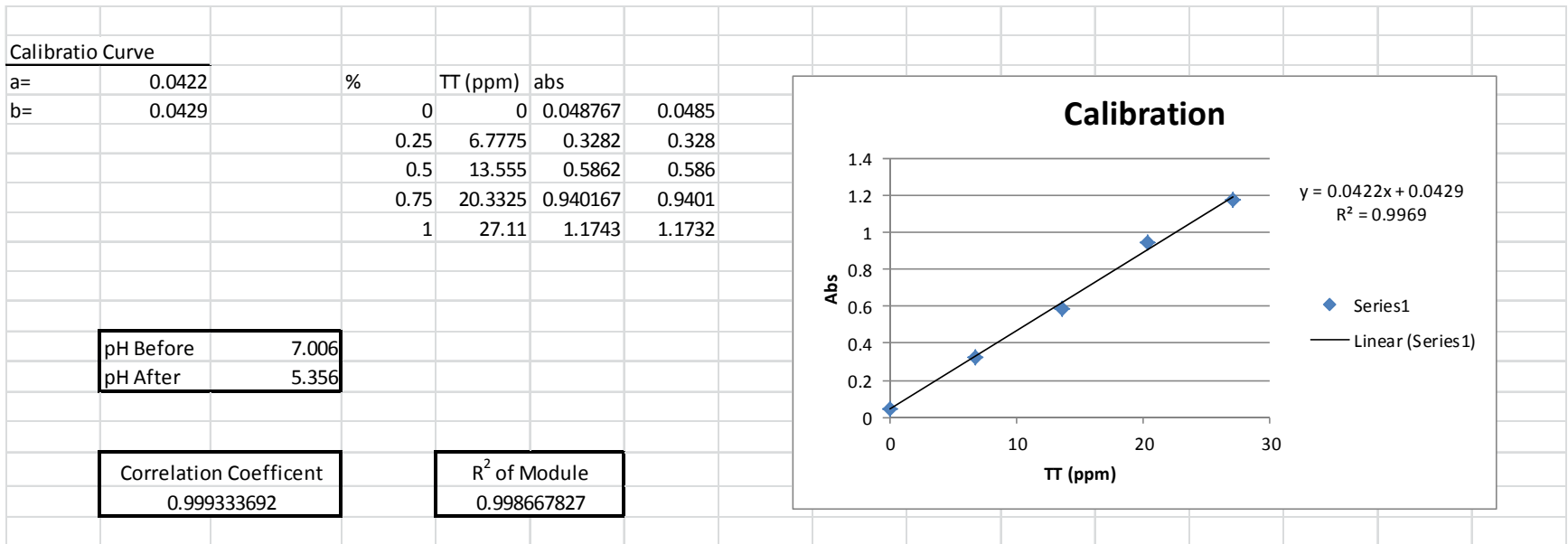


28Jul15 0.7@5%pH9					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	3.38E-05	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	0.894853	16.37033	1	1	0
5	0.893373	16.34229	0.998287	0.999832	2.38E-06
10	0.893825	16.35086	0.998811	0.999665	7.3E-07
15	0.892617	16.32798	0.997413	0.9995	4.36E-06
20	0.895918	16.39048	1.001231	0.999337	3.59E-06
25	0.89309	16.33694	0.99796	0.999176	1.48E-06
30	0.892219	16.32044	0.996953	0.999016	4.26E-06
35	0.891657	16.30978	0.996302	0.998858	6.54E-06
40	0.891846	16.31338	0.996521	0.998702	4.75E-06
45	0.891732	16.31121	0.996389	0.998547	4.66E-06
50	0.892946	16.33421	0.997794	0.998394	3.6E-07
55	0.895404	16.38076	1.000637	0.998243	5.73E-06
60	0.893377	16.34237	0.998292	0.998093	3.98E-08
65	0.893002	16.33527	0.997859	0.997945	7.38E-09
70	0.891549	16.30775	0.996178	0.997798	2.63E-06
75	0.891789	16.31229	0.996455	0.997653	1.43E-06
80	0.894578	16.36511	0.999681	0.997509	4.72E-06
85	0.891897	16.31434	0.99658	0.997367	6.2E-07
90	0.893233	16.33963	0.998125	0.997226	8.08E-07
95	0.891884	16.31408	0.996564	0.997087	2.73E-07
100	0.890363	16.28529	0.994806	0.996949	4.6E-06
105	0.89156	16.30795	0.99619	0.996813	3.89E-07
110	0.892712	16.32978	0.997523	0.996678	7.14E-07
115	0.891078	16.29882	0.995632	0.996545	8.33E-07
120	0.890886	16.29518	0.99541	0.996413	1.01E-06
125	0.889482	16.26859	0.993785	0.996282	6.23E-06
130	0.893055	16.33627	0.99792	0.996153	3.12E-06
135	0.891348	16.30394	0.995945	0.996025	6.34E-09
140	0.8919	16.31439	0.996583	0.995898	4.7E-07
145	0.889215	16.26355	0.993478	0.995773	5.27E-06
150	0.890512	16.2881	0.994977	0.995649	4.51E-07
155	0.891149	16.30017	0.995714	0.995526	3.54E-08
160	0.888227	16.24484	0.992334	0.995405	9.43E-06
165	0.891276	16.30258	0.995862	0.995285	3.33E-07
170	0.891513	16.30706	0.996135	0.995166	9.4E-07
175	0.895829	16.38881	1.001129	0.995048	3.7E-05
180	0.889517	16.26926	0.993826	0.994932	1.22E-06
185	0.891204	16.30122	0.995779	0.994817	9.25E-07
190	0.890926	16.29594	0.995456	0.994703	5.67E-07
195	0.890976	16.2969	0.995514	0.99459	8.55E-07
200	0.889738	16.27344	0.994082	0.994478	1.57E-07
205	0.890611	16.28998	0.995092	0.994368	5.24E-07
210	0.89097	16.29677	0.995507	0.994259	1.56E-06
215	0.890626	16.29026	0.995109	0.994151	9.19E-07
220	0.887776	16.23628	0.991812	0.994044	4.98E-06
225	0.889583	16.27051	0.993903	0.993938	1.24E-09
230	0.888578	16.25148	0.99274	0.993833	1.19E-06
235	0.88848	16.24961	0.992626	0.99373	1.22E-06
240	0.889887	16.27628	0.994255	0.993627	3.94E-07
245	0.8916	16.30872	0.996237	0.993526	7.35E-06
250	0.889584	16.27053	0.993904	0.993425	2.29E-07
255	0.889355	16.2662	0.993639	0.993326	9.81E-08
260	0.888481	16.24963	0.992627	0.993228	3.6E-07
265	0.887954	16.23966	0.992018	0.99313	1.24E-06
270	0.890225	16.28266	0.994645	0.993034	2.6E-06
275	0.886746	16.21678	0.99062	0.992939	5.37E-06
280	0.890508	16.28804	0.994973	0.992845	4.53E-06
285	0.888988	16.25924	0.993214	0.992751	2.14E-07
290	0.889292	16.265	0.993566	0.992659	8.22E-07
295	0.886796	16.21772	0.990678	0.992568	3.57E-06
300	0.887748	16.23576	0.99178	0.992477	4.87E-07
			sum=		0.000162



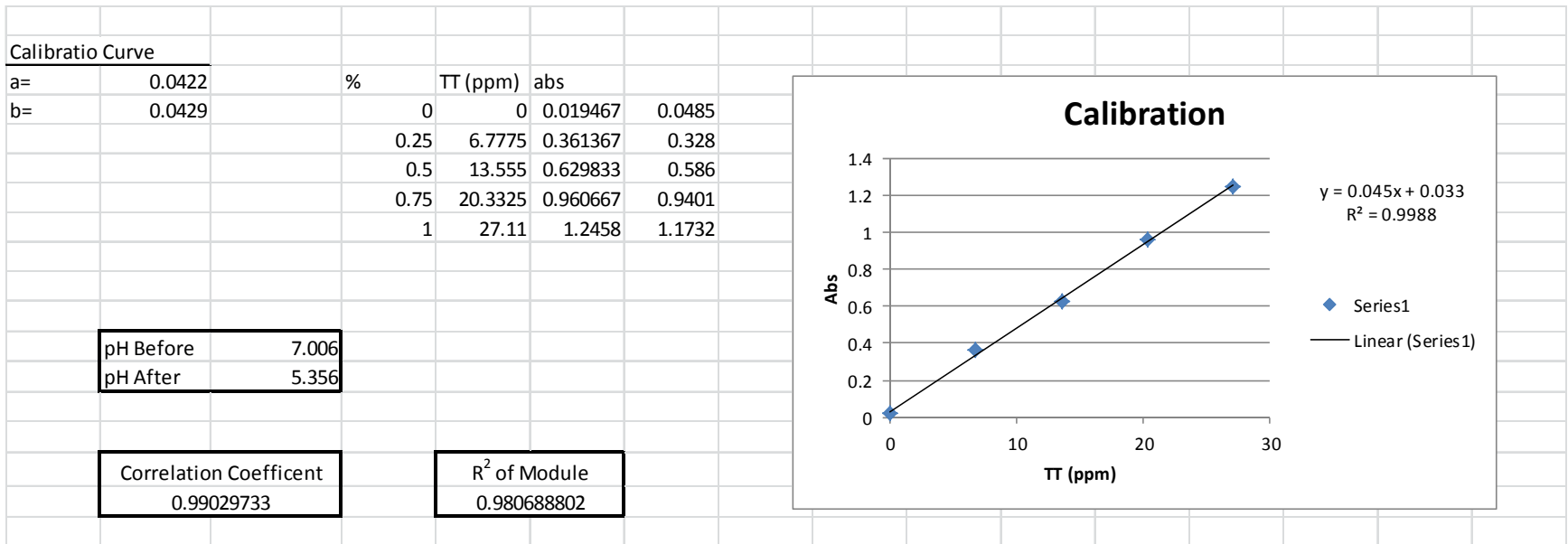
30Jul15 0.7@100%pH7					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.001025	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.149172	25.80354	1	1	0
5	1.143827	25.67895	0.995172	0.994916	6.52E-08
10	1.137243	25.52548	0.989224	0.989911	4.72E-07
15	1.131358	25.3883	0.983908	0.984982	1.15E-06
20	1.127556	25.29966	0.980472	0.980129	1.18E-07
25	1.121391	25.15597	0.974903	0.975351	2E-07
30	1.117589	25.06733	0.971469	0.970646	6.76E-07
35	1.109286	24.87381	0.963969	0.966014	4.18E-06
40	1.104321	24.75807	0.959483	0.961453	3.88E-06
45	1.101104	24.68307	0.956577	0.956962	1.48E-07
50	1.094831	24.53686	0.95091	0.95254	2.66E-06
55	1.090868	24.44447	0.94733	0.948186	7.33E-07
60	1.085204	24.31246	0.942214	0.943899	2.84E-06
65	1.080839	24.21069	0.93827	0.939678	1.98E-06
70	1.075463	24.08539	0.933414	0.935522	4.44E-06
75	1.06967	23.95034	0.92818	0.93143	1.06E-05
80	1.065019	23.84193	0.923979	0.9274	1.17E-05
85	1.061897	23.76916	0.921159	0.923433	5.17E-06
90	1.056443	23.64203	0.916232	0.919527	1.09E-05
95	1.051872	23.53547	0.912102	0.91568	1.28E-05
100	1.049933	23.49028	0.910351	0.911893	2.38E-06
105	1.043071	23.33032	0.904152	0.908164	1.61E-05
110	1.03904	23.23636	0.90051	0.904493	1.59E-05
115	1.035725	23.15909	0.897516	0.900878	1.13E-05
120	1.030211	23.03055	0.892534	0.897318	2.29E-05
125	1.026953	22.95461	0.889591	0.893814	1.78E-05
130	1.023207	22.8673	0.886208	0.890363	1.73E-05
135	1.019881	22.78976	0.883203	0.886965	1.42E-05
140	1.015515	22.688	0.879259	0.883619	1.9E-05
145	1.013225	22.63461	0.87719	0.880325	9.83E-06
150	1.01057	22.57273	0.874792	0.877082	5.24E-06
155	1.005995	22.46608	0.870659	0.873888	1.04E-05
160	1.002619	22.38738	0.867609	0.870744	9.83E-06
165	1.001338	22.35752	0.866452	0.867648	1.43E-06
170	0.997909	22.27761	0.863355	0.864599	1.55E-06
175	0.9949	22.20745	0.860636	0.861597	9.25E-07
180	0.990963	22.11568	0.857079	0.858642	2.44E-06
185	0.987957	22.04563	0.854364	0.855732	1.87E-06
190	0.984567	21.96659	0.851301	0.852867	2.45E-06
195	0.984042	21.95435	0.850827	0.850045	6.11E-07
200	0.979925	21.85839	0.847108	0.847268	2.54E-08
205	0.977954	21.81245	0.845328	0.844532	6.32E-07
210	0.973655	21.71224	0.841444	0.841839	1.56E-07
215	0.973458	21.70766	0.841266	0.839188	4.32E-06
220	0.96996	21.62611	0.838106	0.836577	2.34E-06
225	0.966974	21.5565	0.835408	0.834006	1.97E-06
230	0.964266	21.49338	0.832962	0.831475	2.21E-06
235	0.960611	21.40817	0.82966	0.828983	4.59E-07
240	0.960589	21.40766	0.82964	0.826529	9.68E-06
245	0.957655	21.33928	0.82699	0.824112	8.28E-06
250	0.955311	21.28465	0.824873	0.821733	9.86E-06
255	0.951846	21.20386	0.821742	0.819391	5.53E-06
260	0.950457	21.17148	0.820487	0.817084	1.16E-05
265	0.946606	21.08173	0.817009	0.814813	4.82E-06
270	0.945558	21.05731	0.816063	0.812577	1.21E-05
275	0.944271	21.02731	0.8149	0.810376	2.05E-05
280	0.939947	20.92651	0.810994	0.808208	7.76E-06
285	0.93703	20.8585	0.808358	0.806073	5.22E-06
290	0.937187	20.86216	0.8085	0.803972	2.05E-05
295	0.931171	20.72195	0.803066	0.801902	1.35E-06
300	0.930054	20.6959	0.802056	0.799865	4.8E-06
			sum=		0.000392





31Jul15 0.7@10%pH6 removal increases throwout

			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	-0.0003	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.245828	28.05659	1	1	1.23E-32
5	1.247947	28.10599	1.001761	1.001513	6.17E-08
10	1.247502	28.09562	1.001391	1.003012	2.63E-06
15	1.246327	28.06823	1.000415	1.004498	1.67E-05
20	1.248333	28.11498	1.002081	1.005971	1.51E-05
25	1.246422	28.07044	1.000494	1.007431	4.81E-05
30	1.251022	28.17767	1.004316	1.008878	2.08E-05
35	1.251163	28.18095	1.004433	1.010312	3.46E-05
40	1.253246	28.22952	1.006164	1.011734	3.1E-05
45	1.255379	28.27922	1.007935	1.013143	2.71E-05
50	1.257795	28.33554	1.009943	1.01454	2.11E-05
55	1.255595	28.28427	1.008115	1.015925	6.1E-05
60	1.260154	28.39054	1.011903	1.017297	2.91E-05
65	1.258026	28.34092	1.010134	1.018657	7.26E-05
70	1.259218	28.36872	1.011125	1.020005	7.89E-05
75	1.266387	28.53582	1.017081	1.021341	1.82E-05
80	1.260949	28.40906	1.012563	1.022666	0.000102
85	1.266868	28.54705	1.017481	1.023979	4.22E-05
90	1.265781	28.5217	1.016578	1.02528	7.57E-05
95	1.271334	28.65115	1.021191	1.02657	2.89E-05
100	1.270806	28.63883	1.020752	1.027848	5.04E-05
105	1.273727	28.70692	1.023179	1.029115	3.52E-05
110	1.272436	28.67682	1.022107	1.030371	6.83E-05
115	1.277927	28.80483	1.026669	1.031616	2.45E-05
120	1.279031	28.83056	1.027586	1.03285	2.77E-05
125	1.279032	28.83057	1.027587	1.034073	4.21E-05
130	1.283125	28.926	1.030988	1.035286	1.85E-05
135	1.287362	29.02475	1.034507	1.036487	3.92E-06
140	1.287537	29.02883	1.034653	1.037678	9.15E-06
145	1.287105	29.01876	1.034294	1.038859	2.08E-05
150	1.299139	29.29928	1.044292	1.040029	1.82E-05
155	1.288864	29.05976	1.035755	1.041189	2.95E-05
160	1.29286	29.15291	1.039075	1.042338	1.06E-05
165	1.299845	29.31574	1.044879	1.043477	1.96E-06
170	1.304202	29.4173	1.048499	1.044607	1.51E-05
175	1.305089	29.43798	1.049236	1.045726	1.23E-05
180	1.300929	29.341	1.045779	1.046836	1.12E-06
185	1.303498	29.40089	1.047914	1.047936	4.63E-10
190	1.313288	29.6291	1.056048	1.049026	4.93E-05
195	1.305132	29.43896	1.049271	1.050106	6.97E-07
200	1.307536	29.49501	1.051269	1.051177	8.42E-09
205	1.3117	29.59207	1.054728	1.052239	6.2E-06
210	1.313217	29.62743	1.055988	1.053291	7.28E-06
215	1.314878	29.66616	1.057369	1.054334	9.21E-06
220	1.3128	29.61772	1.055642	1.055367	7.56E-08
225	1.318178	29.74309	1.060111	1.056392	1.38E-05
230	1.318038	29.73982	1.059994	1.057407	6.69E-06
235	1.324108	29.88131	1.065037	1.058414	4.39E-05
240	1.323262	29.86158	1.064334	1.059412	2.42E-05
245	1.323209	29.86035	1.06429	1.060401	1.51E-05
250	1.319734	29.77934	1.061403	1.061381	4.79E-10
255	1.324654	29.89404	1.065491	1.062352	9.85E-06
260	1.319022	29.76276	1.060812	1.063315	6.27E-06
265	1.326054	29.92667	1.066654	1.06427	5.68E-06
270	1.325879	29.9226	1.066509	1.065216	1.67E-06
275	1.332235	30.07075	1.071789	1.066154	3.18E-05
280	1.32455	29.89162	1.065405	1.067083	2.82E-06
285	1.331146	30.04535	1.070884	1.068004	8.29E-06
290	1.32619	29.92983	1.066767	1.068918	4.63E-06
295	1.336945	30.18054	1.075703	1.069823	3.46E-05
300	1.334853	30.13177	1.073964	1.07072	1.05E-05
			sum=		0.001408

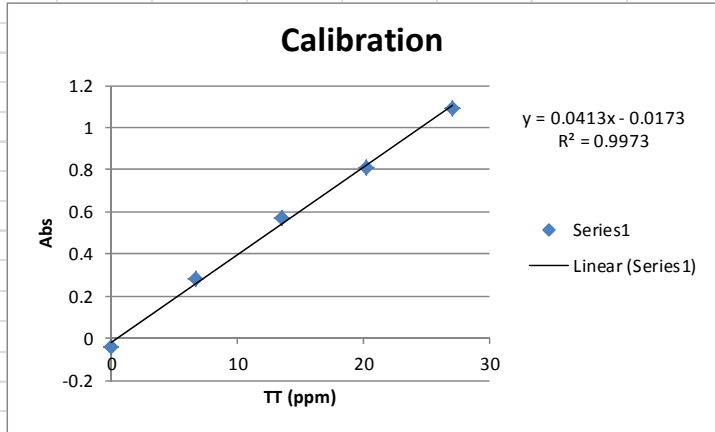


4Aug15 0.7@50%pH6					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.000641	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.099795	7.786094	1	1	1.23E-32
5	1.095667	7.755966	0.996131	0.996818	4.72E-07
10	1.093898	7.743053	0.994472	0.993679	6.29E-07
15	1.090264	7.716529	0.991065	0.990582	2.34E-07
20	1.087877	7.6991	0.988827	0.987527	1.69E-06
25	1.082084	7.656817	0.983396	0.984513	1.25E-06
30	1.080311	7.643878	0.981735	0.98154	3.79E-08
35	1.07819	7.628391	0.979746	0.978607	1.3E-06
40	1.072035	7.583469	0.973976	0.975713	3.02E-06
45	1.073144	7.591559	0.975015	0.972859	4.65E-06
50	1.068037	7.554285	0.970228	0.970043	3.43E-08
55	1.063766	7.523113	0.966224	0.967265	1.08E-06
60	1.060382	7.498412	0.963052	0.964524	2.17E-06
65	1.056723	7.471702	0.959621	0.96182	4.84E-06
70	1.05321	7.446055	0.956327	0.959153	7.98E-06
75	1.052098	7.437943	0.955286	0.956522	1.53E-06
80	1.047845	7.406894	0.951298	0.953926	6.91E-06
85	1.045092	7.386802	0.948717	0.951365	7.01E-06
90	1.045832	7.392206	0.949411	0.948839	3.27E-07
95	1.042096	7.364935	0.945909	0.946347	1.92E-07
100	1.038032	7.335268	0.942099	0.943889	3.2E-06
105	1.037477	7.331221	0.941579	0.941463	1.34E-08
110	1.033578	7.302757	0.937923	0.939071	1.32E-06
115	1.032161	7.292418	0.936595	0.93671	1.32E-08
120	1.026889	7.253932	0.931652	0.934382	7.45E-06
125	1.026496	7.251067	0.931284	0.932084	6.4E-07
130	1.025924	7.246892	0.930748	0.929818	8.65E-07
135	1.020337	7.206108	0.92551	0.927583	4.3E-06
140	1.019834	7.202441	0.925039	0.925377	1.14E-07
145	1.017562	7.185852	0.922908	0.923201	8.58E-08
150	1.013886	7.159025	0.919463	0.921055	2.53E-06
155	1.01317	7.153797	0.918791	0.918938	2.13E-08
160	1.01049	7.134235	0.916279	0.916849	3.24E-07
165	1.010395	7.133538	0.91619	0.914788	1.96E-06
170	1.006296	7.103619	0.912347	0.912755	1.67E-07
175	1.003437	7.082753	0.909667	0.910749	1.17E-06
180	1.000739	7.063061	0.907138	0.908771	2.67E-06
185	0.998802	7.048921	0.905322	0.906819	2.24E-06
190	0.996331	7.030884	0.903005	0.904894	3.57E-06
195	0.997191	7.037158	0.903811	0.902994	6.67E-07
200	0.993554	7.010613	0.900402	0.90112	5.16E-07
205	0.993152	7.00768	0.900025	0.899272	5.68E-07
210	0.989787	6.983118	0.896871	0.897448	3.33E-07
215	0.98841	6.973067	0.89558	0.895649	4.8E-09
220	0.987998	6.970055	0.895193	0.893874	1.74E-06
225	0.984573	6.945055	0.891982	0.892123	1.99E-08
230	0.98534	6.950658	0.892702	0.890396	5.32E-06
235	0.981085	6.919597	0.888712	0.888692	4.14E-10
240	0.980103	6.912427	0.887791	0.887011	6.09E-07
245	0.978944	6.903973	0.886706	0.885352	1.83E-06
250	0.97574	6.880584	0.883702	0.883717	2.22E-10
255	0.975224	6.876818	0.883218	0.882103	1.24E-06
260	0.97374	6.865982	0.881826	0.88051	1.73E-06
265	0.972471	6.856719	0.880637	0.87894	2.88E-06
270	0.969605	6.835806	0.877951	0.87739	3.14E-07
275	0.971403	6.848926	0.879636	0.875862	1.42E-05
280	0.967181	6.818112	0.875678	0.874354	1.75E-06
285	0.963882	6.79403	0.872585	0.872866	7.88E-08
290	0.963531	6.791469	0.872256	0.871398	7.36E-07
295	0.961524	6.776817	0.870374	0.869951	1.8E-07
300	0.958136	6.752088	0.867198	0.868522	1.75E-06
			sum=		0.000115

Calibratio Curve							
a=	0.0331	%	TT (ppm)	abs	2	3	1
b=	0.137	0	0	-0.0429	-0.0429	-0.0429	-0.0429
		0.25	6.7775	0.2795	0.2791	0.279	0.2804
		0.5	13.555	0.574	0.5739	0.5746	0.5735
		0.75	20.3325	0.813167	0.8308	0.8046	0.8041
		1	27.11	1.091	1.0887	1.0893	1.095
							0.997

pH Before	6.742
pH After	5.509

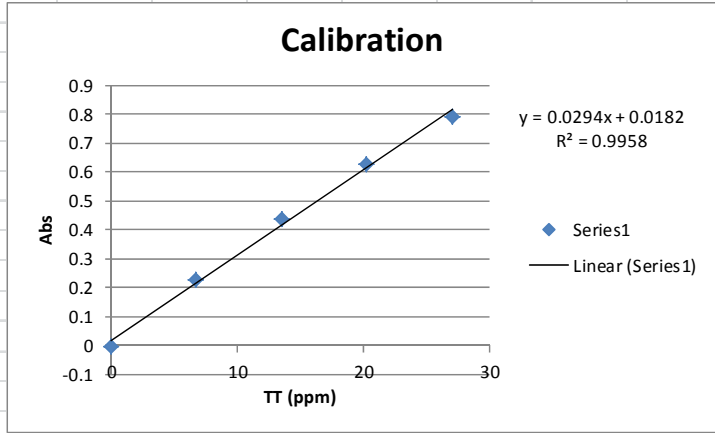


5Aug15 0.7@30%pH9					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	7.4676E-05	
wavelength=	430				
time (min)	abs	C/Co	model	sum squares	
0	0.84115	44.60165	1	1	0
5	0.844218	44.77022	1.00378	0.999628619	1.72E-05
10	0.842179	44.65821	1.001268	0.999261208	4.03E-06
15	0.8417	44.63185	1.000677	0.998897725	3.17E-06
20	0.841584	44.62549	1.000534	0.998538127	3.99E-06
25	0.84005	44.54119	0.998644	0.998182373	2.14E-07
30	0.838787	44.47179	0.997088	0.997830421	5.51E-07
35	0.83789	44.42253	0.995984	0.997482232	2.24E-06
40	0.83754	44.4033	0.995553	0.997137764	2.51E-06
45	0.838417	44.45147	0.996633	0.996796979	2.7E-08
50	0.837853	44.42049	0.995938	0.996459836	2.72E-07
55	0.838834	44.47438	0.997146	0.996126297	1.04E-06
60	0.836597	44.35147	0.994391	0.995796324	1.98E-06
65	0.837618	44.40758	0.995649	0.995469877	3.2E-08
70	0.836134	44.32607	0.993821	0.99514692	1.76E-06
75	0.838091	44.43356	0.996231	0.994827416	1.97E-06
80	0.836478	44.34494	0.994244	0.994511326	7.13E-08
85	0.837826	44.419	0.995905	0.994198616	2.91E-06
90	0.836529	44.34775	0.994307	0.993889248	1.75E-07
95	0.836039	44.32085	0.993704	0.993583186	1.47E-08
100	0.837972	44.42703	0.996085	0.993280397	7.86E-06
105	0.834401	44.23084	0.991686	0.992980844	1.68E-06
110	0.838194	44.43922	0.996358	0.992684493	1.35E-05
115	0.832397	44.12074	0.989218	0.99239131	1.01E-05
120	0.832583	44.13094	0.989446	0.992101261	7.05E-06
125	0.835586	44.29596	0.993146	0.991814312	1.77E-06
130	0.833799	44.19773	0.990944	0.99153043	3.44E-07
135	0.834447	44.23336	0.991743	0.991249583	2.43E-07
140	0.835441	44.28799	0.992968	0.990971738	3.98E-06
145	0.833264	44.16834	0.990285	0.990696863	1.7E-07
150	0.836302	44.33529	0.994028	0.990424927	1.3E-05
155	0.83389	44.20276	0.991057	0.990155897	8.11E-07
160	0.832316	44.11625	0.989117	0.989889742	5.97E-07
165	0.834666	44.24538	0.992012	0.989626433	5.69E-06
170	0.831427	44.06743	0.988022	0.989365938	1.81E-06
175	0.834021	44.20995	0.991218	0.989108228	4.45E-06
180	0.835262	44.27813	0.992746	0.988853273	1.52E-05
185	0.833914	44.20404	0.991085	0.988601043	6.17E-06
190	0.831121	44.05061	0.987645	0.988351509	4.99E-07
195	0.833133	44.16118	0.990124	0.988104642	4.08E-06
200	0.831508	44.07189	0.988122	0.987860414	6.86E-08
205	0.831994	44.09857	0.988721	0.987618797	1.21E-06
210	0.829884	43.98263	0.986121	0.987379763	1.58E-06
215	0.833004	44.15408	0.989965	0.987143283	7.96E-06
220	0.827967	43.87733	0.98376	0.986909332	9.92E-06
225	0.828405	43.90139	0.9843	0.986677881	5.66E-06
230	0.830151	43.99734	0.986451	0.986448904	3.67E-12
235	0.829737	43.97456	0.98594	0.986222375	7.97E-08
240	0.829579	43.96587	0.985745	0.985998267	6.4E-08
245	0.831949	44.09611	0.988665	0.985776555	8.34E-06
250	0.828375	43.89975	0.984263	0.985557213	1.68E-06
255	0.827999	43.87909	0.9838	0.985340215	2.37E-06
260	0.829174	43.94362	0.985246	0.985125537	1.46E-08
265	0.826822	43.81441	0.982349	0.984913154	6.57E-06
270	0.828503	43.90675	0.98442	0.984703041	8.02E-08
275	0.825774	43.75683	0.981058	0.984495174	1.18E-05
280	0.827117	43.8306	0.982712	0.984289528	2.49E-06
285	0.828802	43.92321	0.984789	0.984086081	4.94E-07
290	0.828454	43.90408	0.98436	0.983884809	2.26E-07
295	0.828637	43.91411	0.984585	0.983685688	8.08E-07
300	0.825195	43.72501	0.980345	0.983488696	9.88E-06
			sum=		0.000214

Calibratio Curve			
a=	0.0294	%	TT (ppm)
b=	0.0182		abs
		0	0 -0.0036
		0.25	6.7775 0.229
		0.5	13.555 0.4351
		0.75	20.3325 0.6281
		1	27.11 0.7915

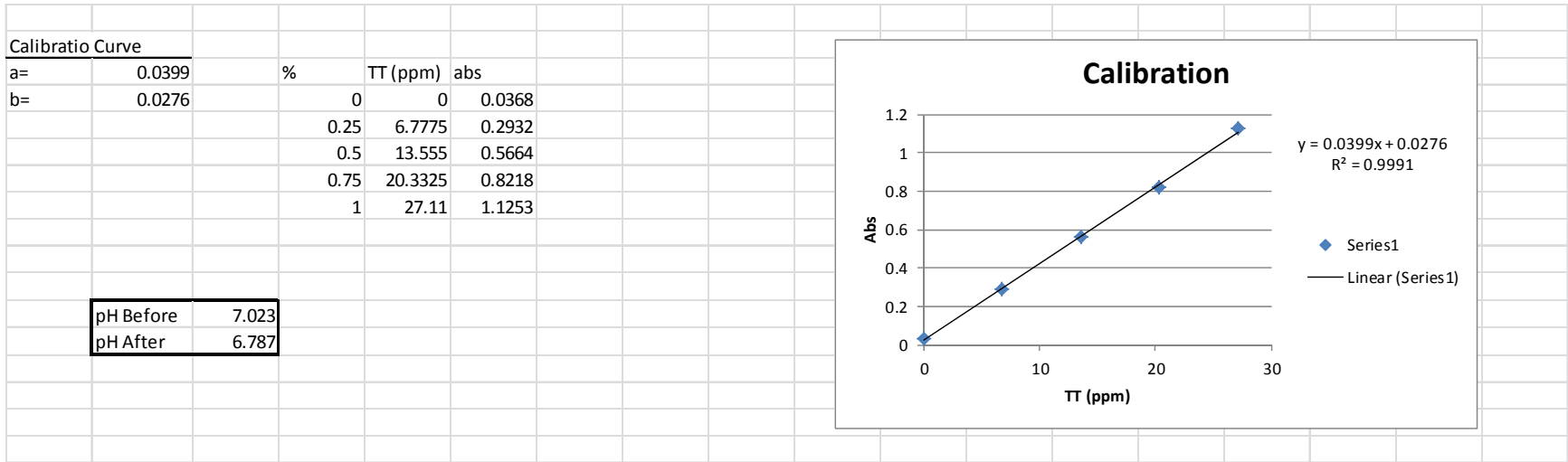
  

pH Before	9.003
pH After	8.937

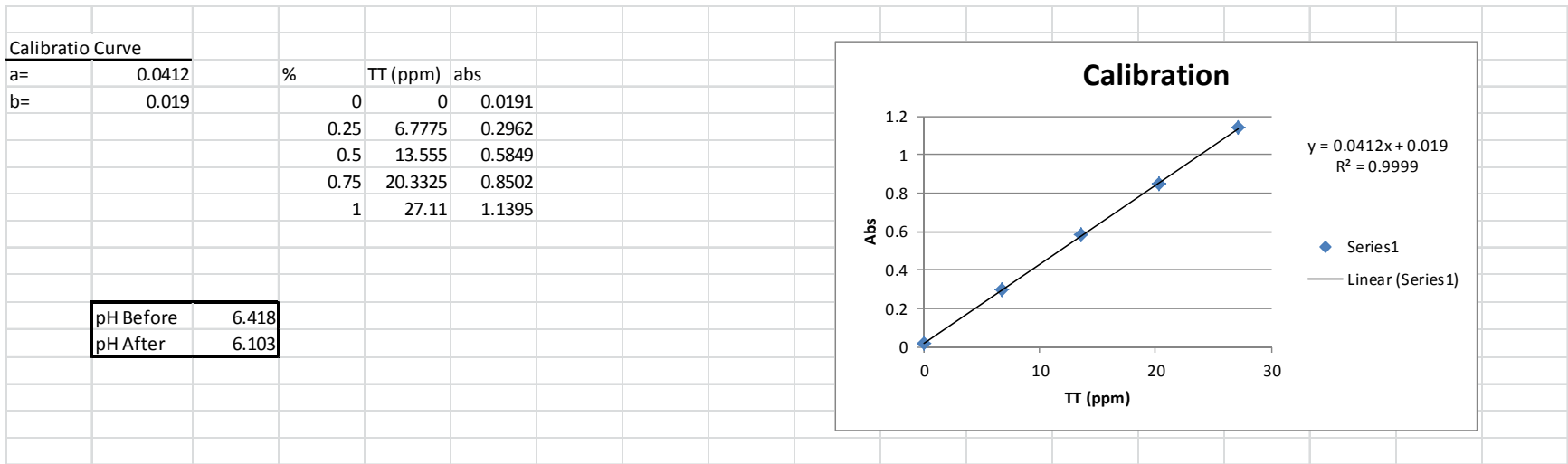


6Aug15 0.7@20%pH7					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.00022352	
wavelength=	430				
time (min)	abs	C/Co	model	sum squares	
0	1.102808	38.51116	1	1	0
5	1.10477	38.58226	1.001846	0.998888795	8.75E-06
10	1.101777	38.47381	0.99903	0.997790287	1.54E-06
15	1.099396	38.38753	0.99679	0.996704329	7.29E-09
20	1.097544	38.32044	0.995048	0.995630778	3.4E-07
25	1.097384	38.31462	0.994897	0.994569493	1.07E-07
30	1.095621	38.25076	0.993238	0.993520333	7.95E-08
35	1.096327	38.27635	0.993903	0.992483161	2.02E-06
40	1.098011	38.33737	0.995487	0.991457838	1.62E-05
45	1.093195	38.16285	0.990956	0.99044423	2.61E-07
50	1.093173	38.16206	0.990935	0.989442202	2.23E-06
55	1.089864	38.04218	0.987822	0.988451624	3.96E-07
60	1.090741	38.07396	0.988648	0.987472362	1.38E-06
65	1.089353	38.02365	0.987341	0.986504289	7E-07
70	1.090674	38.07152	0.988584	0.985547277	9.22E-06
75	1.084924	37.86318	0.983174	0.984601199	2.04E-06
80	1.087068	37.94086	0.985191	0.98366593	2.33E-06
85	1.086145	37.90742	0.984323	0.982741346	2.5E-06
90	1.083868	37.82492	0.982181	0.981827327	1.25E-07
95	1.083027	37.79446	0.98139	0.98092375	2.17E-07
100	1.083019	37.79415	0.981382	0.980030496	1.83E-06
105	1.080959	37.71951	0.979444	0.979147449	8.78E-08
110	1.080215	37.69258	0.978744	0.97827449	2.21E-07
115	1.078404	37.62696	0.977041	0.977411506	1.38E-07
120	1.078599	37.63401	0.977223	0.976558381	4.42E-07
125	1.077904	37.60884	0.97657	0.975715003	7.31E-07
130	1.076482	37.55731	0.975232	0.974881261	1.23E-07
135	1.073513	37.44976	0.972439	0.974057045	2.62E-06
140	1.075512	37.52216	0.974319	0.973242246	1.16E-06
145	1.074311	37.47865	0.973189	0.972436756	5.66E-07
150	1.072029	37.39599	0.971043	0.971640469	3.57E-07
155	1.069417	37.30134	0.968585	0.97085328	5.14E-06
160	1.070954	37.35702	0.970031	0.970075085	1.93E-09
165	1.070525	37.34149	0.969628	0.96930578	1.04E-07
170	1.067369	37.22715	0.966659	0.968545266	3.56E-06
175	1.068736	37.27666	0.967944	0.96779344	2.28E-08
180	1.066163	37.18344	0.965524	0.967050204	2.33E-06
185	1.067062	37.21602	0.96637	0.96631546	2.96E-09
190	1.065182	37.14789	0.964601	0.965589111	9.77E-07
195	1.066268	37.18724	0.965622	0.96487106	5.65E-07
200	1.063927	37.10242	0.96342	0.964161213	5.5E-07
205	1.066074	37.18022	0.96544	0.963459476	3.92E-06
210	1.061557	37.01656	0.96119	0.962765757	2.48E-06
215	1.063061	37.07106	0.962606	0.962079964	2.76E-07
220	1.061937	37.03033	0.961548	0.961402006	2.14E-08
225	1.059763	36.95154	0.959502	0.960731795	1.51E-06
230	1.059663	36.94792	0.959408	0.96006924	4.37E-07
235	1.059779	36.95212	0.959517	0.959414255	1.06E-08
240	1.057437	36.8673	0.957315	0.958766754	2.11E-06
245	1.058681	36.91234	0.958484	0.958126651	1.28E-07
250	1.056533	36.83452	0.956464	0.95749386	1.06E-06
255	1.057446	36.86762	0.957323	0.9568683	2.07E-07
260	1.055735	36.80562	0.955713	0.956249887	2.88E-07
265	1.056613	36.83744	0.956539	0.95563854	8.12E-07
270	1.055643	36.80227	0.955626	0.955034177	3.5E-07
275	1.054335	36.7549	0.954396	0.954436719	1.66E-09
280	1.053887	36.73867	0.953975	0.953846088	1.65E-08
285	1.053348	36.71912	0.953467	0.953262204	4.19E-08
290	1.050883	36.62981	0.951148	0.952684992	2.36E-06
295	1.053858	36.7376	0.953947	0.952114374	3.36E-06
300	1.050697	36.62307	0.950973	0.951550276	3.33E-07
			sum=		9.17E-05

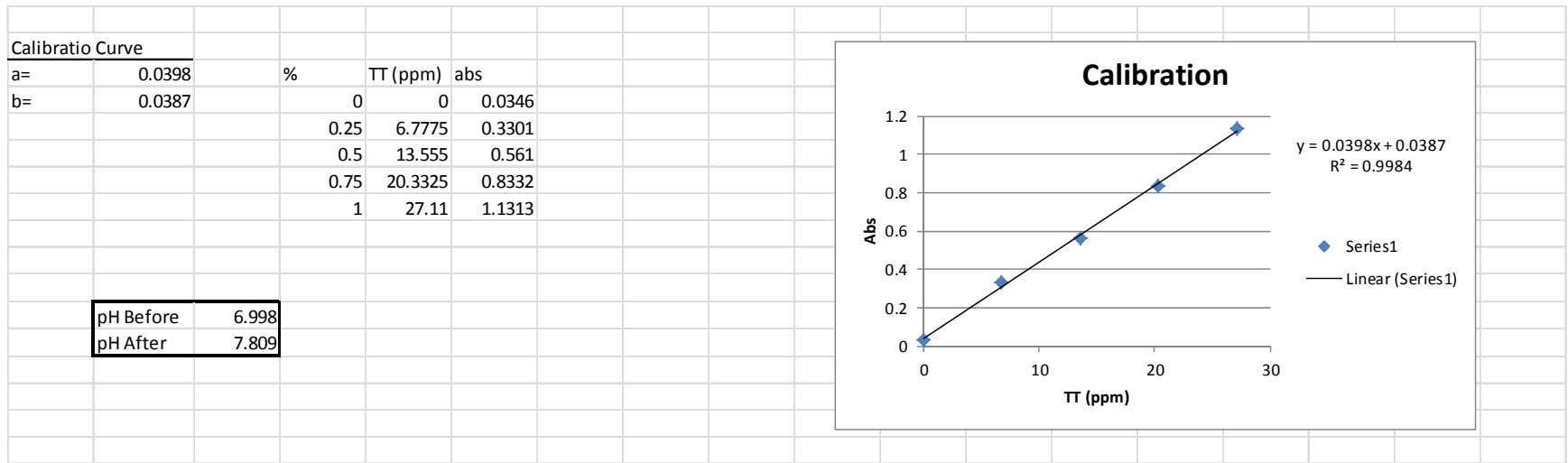




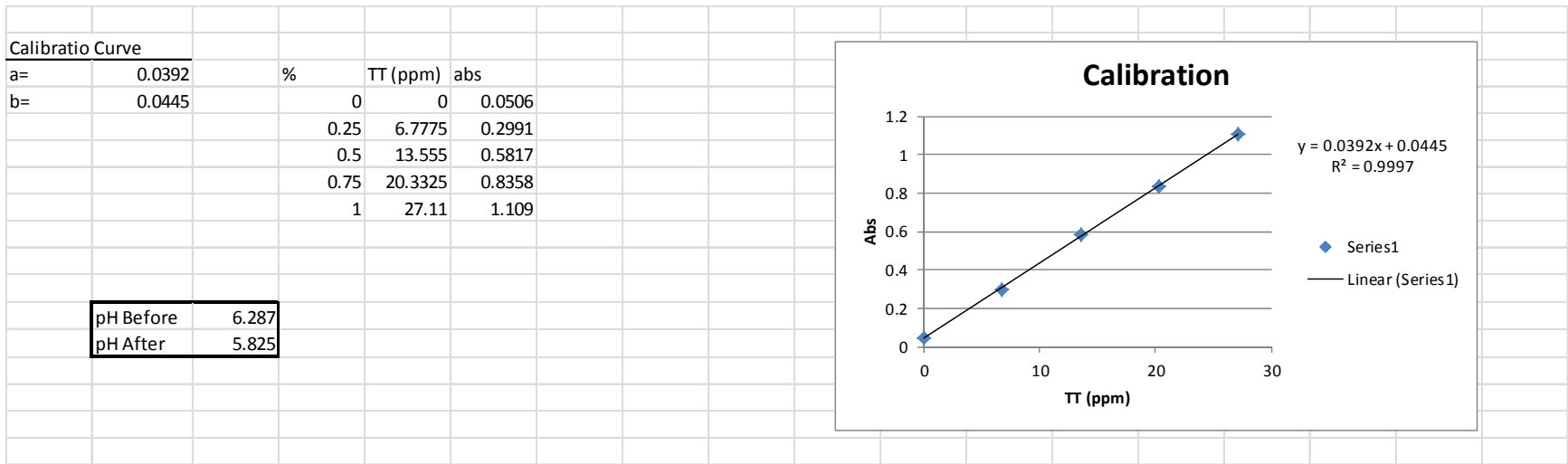
7Aug15_0.710%pH6					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.000139229	
wavelength=	430				
time (min)	abs	C/Co	model	sum squares	
0	1.135949	57.61835	1	1	0
5	1.136509	57.64783	1.000512	0.999307695	1.45E-06
10	1.136356	57.63977	1.000372	0.998623011	3.06E-06
15	1.133659	57.49787	0.997909	0.997945864	1.36E-09
20	1.135735	57.6071	0.999805	0.997276172	6.39E-06
25	1.132789	57.45207	0.997114	0.996613852	2.5E-07
30	1.131438	57.38095	0.99588	0.995958824	6.25E-09
35	1.130947	57.35512	0.995432	0.995311006	1.45E-08
40	1.12988	57.29894	0.994457	0.99467032	4.57E-08
45	1.130819	57.34839	0.995315	0.994036686	1.63E-06
50	1.127042	57.14959	0.991864	0.993410029	2.39E-06
55	1.12904	57.25472	0.993689	0.992790269	8.08E-07
60	1.128965	57.2508	0.993621	0.992177333	2.08E-06
65	1.126539	57.12312	0.991405	0.991571144	2.76E-08
70	1.125101	57.0474	0.990091	0.990971628	7.76E-07
75	1.124281	57.00426	0.989342	0.990378712	1.07E-06
80	1.127293	57.16278	0.992093	0.989792323	5.29E-06
85	1.124302	57.00538	0.989362	0.98921239	2.23E-08
90	1.125315	57.05871	0.990287	0.98863884	2.72E-06
95	1.121895	56.87869	0.987163	0.988071605	8.26E-07
100	1.124196	56.99979	0.989264	0.987510614	3.08E-06
105	1.122017	56.88512	0.987274	0.986955799	1.01E-07
110	1.122243	56.897	0.987481	0.986407091	1.15E-06
115	1.120697	56.81563	0.986068	0.985864424	4.15E-08
120	1.119913	56.77435	0.985352	0.985327731	5.87E-10
125	1.118212	56.68482	0.983798	0.984796946	9.98E-07
130	1.118621	56.70635	0.984172	0.984272005	1.01E-08
135	1.12048	56.80421	0.98587	0.983752842	4.48E-06
140	1.117733	56.65965	0.983361	0.983239394	1.48E-08
145	1.116923	56.617	0.982621	0.982731599	1.22E-08
150	1.11489	56.50997	0.980763	0.982229394	2.15E-06
155	1.115063	56.51909	0.980922	0.981732717	6.58E-07
160	1.113545	56.43923	0.979536	0.981241508	2.91E-06
165	1.116035	56.57025	0.98181	0.980755706	1.11E-06
170	1.114957	56.51355	0.980826	0.980275253	3.03E-07
175	1.114368	56.48255	0.980288	0.979800088	2.38E-07
180	1.116046	56.57085	0.98182	0.979330155	6.2E-06
185	1.11055	56.2816	0.9768	0.978865395	4.27E-06
190	1.11261	56.39002	0.978682	0.978405751	7.61E-08
195	1.113291	56.42585	0.979303	0.977951167	1.83E-06
200	1.111294	56.32073	0.977479	0.977501587	5.07E-10
205	1.111622	56.33799	0.977779	0.977056957	5.21E-07
210	1.109736	56.23875	0.976056	0.976617221	3.15E-07
215	1.109013	56.20066	0.975395	0.976182326	6.2E-07
220	1.109881	56.24635	0.976188	0.975752219	1.9E-07
225	1.108029	56.14892	0.974497	0.975326846	6.88E-07
230	1.106954	56.09233	0.973515	0.974906157	1.94E-06
235	1.106275	56.0566	0.972895	0.974490098	2.54E-06
240	1.107944	56.14444	0.974419	0.97407862	1.16E-07
245	1.109468	56.22461	0.975811	0.973671671	4.58E-06
250	1.106345	56.06025	0.972958	0.973269203	9.67E-08
255	1.105801	56.03163	0.972462	0.972871165	1.68E-07
260	1.104737	55.97565	0.97149	0.972477509	9.75E-07
265	1.105033	55.99123	0.97176	0.972088186	1.07E-07
270	1.106849	56.0868	0.973419	0.971703149	2.94E-06
275	1.105606	56.02135	0.972283	0.971322351	9.23E-07
280	1.102301	55.84745	0.969265	0.970945745	2.83E-06
285	1.103265	55.89817	0.970145	0.970573285	1.83E-07
290	1.104669	55.97205	0.971427	0.970204925	1.49E-06
295	1.101388	55.79934	0.96843	0.96984062	1.99E-06
300	1.101436	55.80188	0.968474	0.969480326	1.01E-06
			sum=		8.27E-05



11Aug15_0.7@50%pH7					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.000589571	
wavelength=	430				
time (min)	abs		C/Co	model	sum squares
0	1.085213	27.01325	1	1	0
5	1.082503	26.94323	0.997408	0.997071692	1.13E-07
10	1.078604	26.84247	0.993678	0.994182134	2.54E-07
15	1.076399	26.78551	0.991569	0.991330814	5.68E-08
20	1.073431	26.70882	0.98873	0.988517225	4.54E-08
25	1.071326	26.65442	0.986716	0.985740868	9.52E-07
30	1.067713	26.56105	0.98326	0.983001251	6.7E-08
35	1.065177	26.49553	0.980835	0.980297886	2.88E-07
40	1.061877	26.41025	0.977677	0.977630296	2.22E-09
45	1.058661	26.32717	0.974602	0.974998005	1.57E-07
50	1.054651	26.22354	0.970766	0.972400548	2.67E-06
55	1.05318	26.18554	0.969359	0.969837462	2.29E-07
60	1.051256	26.13582	0.967518	0.967308294	4.42E-08
65	1.047453	26.03754	0.96388	0.964812594	8.69E-07
70	1.046785	26.02029	0.963242	0.96234992	7.95E-07
75	1.042467	25.90871	0.959111	0.959919834	6.54E-07
80	1.039421	25.83001	0.956198	0.957521905	1.75E-06
85	1.038562	25.8078	0.955376	0.955155709	4.84E-08
90	1.035735	25.73475	0.952671	0.952820823	2.24E-08
95	1.033502	25.67707	0.950536	0.950516836	3.65E-10
100	1.030085	25.58877	0.947267	0.948243337	9.53E-07
105	1.027503	25.52203	0.944797	0.945999923	1.45E-06
110	1.027251	25.51552	0.944556	0.943786196	5.92E-07
115	1.023493	25.41843	0.940961	0.941601763	4.1E-07
120	1.02168	25.37158	0.939227	0.939446237	4.8E-08
125	1.018552	25.29074	0.936235	0.937319235	1.18E-06
130	1.01756	25.26512	0.935286	0.935220379	4.34E-09
135	1.01487	25.1956	0.932712	0.933149297	1.91E-07
140	1.013318	25.1555	0.931228	0.931105622	1.5E-08
145	1.012193	25.12644	0.930152	0.929088991	1.13E-06
150	1.009536	25.05778	0.92761	0.927099046	2.62E-07
155	1.008079	25.02012	0.926217	0.925135434	1.17E-06
160	1.004908	24.93818	0.923183	0.923197806	2.12E-10
165	1.004433	24.92592	0.922729	0.921285818	2.08E-06
170	1.00059	24.82663	0.919054	0.919399132	1.19E-07
175	0.999627	24.80172	0.918132	0.917537413	3.53E-07
180	0.996477	24.72034	0.915119	0.915700329	3.38E-07
185	0.99549	24.69483	0.914175	0.913887556	8.24E-08
190	0.993267	24.63738	0.912048	0.912098771	2.57E-09
195	0.991893	24.60188	0.910734	0.910333656	1.6E-07
200	0.990628	24.56921	0.909524	0.9085919	8.69E-07
205	0.988232	24.50728	0.907232	0.906873192	1.29E-07
210	0.986259	24.4563	0.905344	0.905177228	2.8E-08
215	0.983828	24.39348	0.903019	0.903503706	2.35E-07
220	0.982707	24.36451	0.901947	0.90185233	8.91E-09
225	0.981167	24.32473	0.900474	0.900222806	6.31E-08
230	0.978725	24.26162	0.898138	0.898614846	2.28E-07
235	0.976968	24.21622	0.896457	0.897028165	3.26E-07
240	0.976627	24.20741	0.896131	0.895462479	4.47E-07
245	0.974318	24.14775	0.893923	0.893917512	2.53E-11
250	0.972218	24.09349	0.891914	0.89239299	2.3E-07
255	0.970516	24.04951	0.890286	0.890888642	3.64E-07
260	0.969312	24.01839	0.889134	0.8894042	7.32E-08
265	0.967896	23.98182	0.88778	0.887939403	2.55E-08
270	0.967058	23.96015	0.886978	0.886493989	2.34E-07
275	0.965288	23.91442	0.885285	0.885067701	4.71E-08
280	0.963418	23.86609	0.883496	0.883660288	2.71E-08
285	0.96187	23.82609	0.882015	0.8822715	6.59E-08
290	0.961069	23.8054	0.881249	0.880901089	1.21E-07
295	0.959384	23.76187	0.879637	0.879548812	7.85E-09
300	0.957799	23.7209	0.878121	0.87821443	8.73E-09
				sum=	2.31E-05



12Aug15 0.7@70%pH6Redo					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.000827011	
wavelength=	430				
time (min)	abs	C/Co	model	sum squares	
0	1.102453	23.89334	1	1	0
5	1.100628	23.85231	0.998283	0.995894796	5.7E-06
10	1.095645	23.74033	0.993596	0.991848723	3.05E-06
15	1.090592	23.62678	0.988844	0.987860928	9.66E-07
20	1.08634	23.53125	0.984846	0.983930573	8.37E-07
25	1.083332	23.46364	0.982016	0.980056829	3.84E-06
30	1.079538	23.37838	0.978448	0.976238882	4.88E-06
35	1.074848	23.27298	0.974036	0.972475928	2.44E-06
40	1.070246	23.16957	0.969708	0.968767174	8.86E-07
45	1.066439	23.08403	0.966128	0.965111841	1.03E-06
50	1.064003	23.02929	0.963837	0.961509158	5.42E-06
55	1.058832	22.91307	0.958973	0.957958367	1.03E-06
60	1.054184	22.80863	0.954602	0.954458721	2.06E-08
65	1.051183	22.74119	0.951779	0.951009483	5.93E-07
70	1.047515	22.65876	0.94833	0.947609927	5.18E-07
75	1.044743	22.59646	0.945722	0.944259337	2.14E-06
80	1.041429	22.52201	0.942606	0.940957008	2.72E-06
85	1.03848	22.45573	0.939832	0.937702246	4.54E-06
90	1.036399	22.40896	0.937875	0.934494364	1.14E-05
95	1.031456	22.29789	0.933226	0.931332687	3.59E-06
100	1.029141	22.24586	0.931049	0.928216551	8.02E-06
105	1.025234	22.15807	0.927375	0.925145299	4.97E-06
110	1.022443	22.09536	0.92475	0.922118284	6.92E-06
115	1.018155	21.99898	0.920716	0.91913487	2.5E-06
120	1.01675	21.96742	0.919395	0.916194428	1.02E-05
125	1.012429	21.87032	0.915331	0.91329634	4.14E-06
130	1.010344	21.82346	0.91337	0.910439995	8.59E-06
135	1.007299	21.75504	0.910506	0.907624792	8.3E-06
140	1.004207	21.68556	0.907598	0.904850138	7.55E-06
145	1.000716	21.6071	0.904315	0.90211545	4.84E-06
150	0.998714	21.56212	0.902432	0.899420152	9.07E-06
155	0.995652	21.49331	0.899553	0.896763676	7.78E-06
160	0.992335	21.41876	0.896432	0.894145464	5.23E-06
165	0.9885	21.33258	0.892826	0.891564963	1.59E-06
170	0.984617	21.24532	0.889173	0.889021632	2.3E-08
175	0.982647	21.20107	0.887321	0.886514934	6.5E-07
180	0.981081	21.16587	0.885848	0.884044341	3.25E-06
185	0.978202	21.10117	0.88314	0.881609335	2.34E-06
190	0.974944	21.02795	0.880076	0.879209402	7.51E-07
195	0.971807	20.95746	0.877126	0.876844037	7.93E-08
200	0.970357	20.92489	0.875762	0.874512742	1.56E-06
205	0.966934	20.84796	0.872543	0.872215026	1.08E-07
210	0.964964	20.80369	0.87069	0.869950407	5.47E-07
215	0.963171	20.7634	0.869004	0.867718406	1.65E-06
220	0.958723	20.66344	0.86482	0.865518554	4.88E-07
225	0.957354	20.63269	0.863533	0.863350389	3.34E-08
230	0.955742	20.59646	0.862017	0.861213453	6.45E-07
235	0.951058	20.49119	0.857611	0.859107298	2.24E-06
240	0.949965	20.46663	0.856583	0.857031478	2.01E-07
245	0.947483	20.41085	0.854248	0.854985559	5.43E-07
250	0.944219	20.33751	0.851179	0.852969108	3.2E-06
255	0.941684	20.28054	0.848795	0.850981702	4.78E-06
260	0.939484	20.23111	0.846726	0.849022922	5.28E-06
265	0.936888	20.17275	0.844284	0.847092356	7.89E-06
270	0.93481	20.12606	0.842329	0.845189597	8.18E-06
275	0.933935	20.10641	0.841507	0.843314245	3.27E-06
280	0.930198	20.02243	0.837992	0.841465905	1.21E-05
285	0.927795	19.96843	0.835732	0.839644188	1.53E-05
290	0.925263	19.91154	0.833351	0.837848711	2.02E-05
295	0.923193	19.86501	0.831404	0.836079095	2.19E-05
300	0.922865	19.85764	0.831095	0.834334969	1.05E-05
			sum=	0.000273	

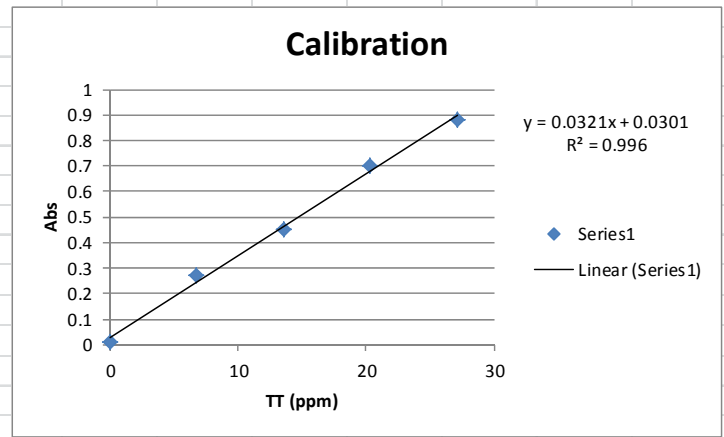


13Aug15 0.7@100%pH8					
			flow rate=	0.7	
			volume=	350	
			resid time	482	
			rate const	0.000481987	
wavelength=	430				
time (min)	abs	C/Co	model	sum squares	
0	0.886178	28.37468	1	1	0
5	0.884311	28.31265	0.997814	0.997605403	4.35E-08
10	0.882251	28.24421	0.995402	0.995241222	2.59E-08
15	0.880215	28.17659	0.993019	0.992907072	1.25E-08
20	0.87921	28.1432	0.991842	0.990602569	1.54E-06
25	0.875454	28.01842	0.987444	0.988327339	7.8E-07
30	0.874237	27.97797	0.986019	0.986081008	3.84E-09
35	0.873425	27.95099	0.985068	0.983863211	1.45E-06
40	0.871652	27.89209	0.982992	0.981673584	1.74E-06
45	0.868176	27.77661	0.978923	0.979511769	3.47E-07
50	0.867583	27.75692	0.978228	0.977377414	7.24E-07
55	0.865969	27.70327	0.976338	0.97527017	1.14E-06
60	0.864342	27.64925	0.974434	0.973189692	1.55E-06
65	0.863009	27.60495	0.972873	0.97113564	3.02E-06
70	0.861036	27.53941	0.970563	0.969107679	2.12E-06
75	0.859778	27.49762	0.96909	0.967105477	3.94E-06
80	0.85854	27.45646	0.96764	0.965128707	6.31E-06
85	0.857226	27.41283	0.966102	0.963177046	8.55E-06
90	0.855329	27.3498	0.963881	0.961250175	6.92E-06
95	0.853385	27.28521	0.961604	0.959347779	5.09E-06
100	0.850805	27.19951	0.958584	0.957469547	1.24E-06
105	0.849569	27.15845	0.957137	0.955615173	2.32E-06
110	0.846902	27.06982	0.954013	0.953784353	5.24E-08
115	0.846894	27.06958	0.954005	0.951976788	4.11E-06
120	0.845816	27.03376	0.952742	0.950192183	6.5E-06
125	0.843396	26.95334	0.949908	0.948430246	2.18E-06
130	0.843031	26.94124	0.949482	0.946690689	7.79E-06
135	0.840505	26.85732	0.946524	0.944973228	2.41E-06
140	0.839405	26.82076	0.945236	0.943277582	3.83E-06
145	0.838957	26.80589	0.944712	0.941603474	9.66E-06
150	0.836054	26.70945	0.941313	0.939950631	1.86E-06
155	0.833192	26.61434	0.937961	0.938318783	1.28E-07
160	0.834859	26.66974	0.939914	0.936707662	1.03E-05
165	0.832813	26.60176	0.937518	0.935117005	5.76E-06
170	0.829926	26.50584	0.934137	0.933546553	3.49E-07
175	0.828333	26.45293	0.932272	0.93199605	7.64E-08
180	0.828459	26.4571	0.932419	0.93046524	3.82E-06
185	0.82706	26.41063	0.930782	0.928953875	3.34E-06
190	0.825253	26.3506	0.928666	0.927461707	1.45E-06
195	0.823357	26.28761	0.926446	0.925988493	2.1E-07
200	0.822253	26.25094	0.925154	0.924533992	3.84E-07
205	0.821189	26.21557	0.923907	0.923097966	6.55E-07
210	0.820607	26.19623	0.923226	0.92168018	2.39E-06
215	0.818388	26.12253	0.920628	0.920280403	1.21E-07
220	0.816922	26.07383	0.918912	0.918898406	1.81E-10
225	0.814557	25.99524	0.916142	0.917533963	1.94E-06
230	0.81367	25.96579	0.915104	0.916186851	1.17E-06
235	0.813168	25.94909	0.914516	0.91485685	1.16E-07
240	0.811962	25.90903	0.913104	0.913543743	1.93E-07
245	0.809648	25.83215	0.910395	0.912247316	3.43E-06
250	0.807932	25.77514	0.908385	0.910967355	6.67E-06
255	0.808161	25.78275	0.908654	0.909703652	1.1E-06
260	0.80775	25.7691	0.908172	0.908456001	8.05E-08
265	0.804625	25.66529	0.904514	0.907224198	7.35E-06
270	0.80379	25.63753	0.903536	0.906008041	6.11E-06
275	0.802029	25.57903	0.901474	0.904807332	1.11E-05
280	0.802023	25.57885	0.901467	0.903621874	4.64E-06
285	0.801314	25.5553	0.900637	0.902451474	3.29E-06
290	0.79999	25.51128	0.899086	0.90129594	4.88E-06
295	0.798743	25.46988	0.897627	0.900155084	6.39E-06
300	0.796776	25.4045	0.895323	0.899028719	1.37E-05
			sum=		0.000188



Calibratio Curve				
a=	0.0321	%	TT (ppm)	abs
b=	0.0301	0	0	0.0122
		0.25	6.7775	0.2738
		0.5	13.555	0.4505
		0.75	20.3325	0.7028
		1	27.11	0.8842

pH Before	8.229
pH After	8.712



**Appendix R: LED Degradation over Time of Use**

Bulb No.	Time (Hrs)	Output	Slope
1	0	3.89E-04	-8.82E-07
1	102	2.99E-04	
2	0	4.05E-04	-2.94E-06
2	102	1.05E-04	
3	0	na	--
3	110.75	3.32E-04	
4	0	4.17E-04	-2.65E-07
4	111	3.88E-04	
5	0	na	--
5	110.75	4.71E-05	
6	0	4.55E-04	-1.12E-06
6	111	3.31E-04	
7	0	na	--
7	110.75	3.47E-04	
Average	0	4.16E-04	-1.43E-06
Average	106.5	2.64E-04	

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[VBAAAQBAJ&oi=fnd&pg=PP1&dq=water+chemistry+mark+benjamin&ots=09P](https://books.google.com/books?hl=en&lr=&id=dr-VBAAAQBAJ&oi=fnd&pg=PP1&dq=water+chemistry+mark+benjamin&ots=09P3HyZ_Ow&sig=F-EI40ndY1dJ1uY8XIOBUnkYzfA)

[3HyZ\\_Ow&sig=F-EI40ndY1dJ1uY8XIOBUnkYzfA](https://books.google.com/books?hl=en&lr=&id=dr-VBAAAQBAJ&oi=fnd&pg=PP1&dq=water+chemistry+mark+benjamin&ots=09P3HyZ_Ow&sig=F-EI40ndY1dJ1uY8XIOBUnkYzfA)

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[0&dq=water+quality+engineering+benjamin&ots=lCvKJn5jMx&sig=o4KCo00oX](https://books.google.com/books?hl=en&lr=&id=vRovU0TD8s0C&oi=fnd&pg=PT10&dq=water+quality+engineering+benjamin&ots=lCvKJn5jMx&sig=o4KCo00oXER-D8NOuBxUyVsQFYA)

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14. ABSTRACT Water treatment capability is required for military operations, production of drinking water, and industrial wastewater treatment. The Advanced Oxidation Process (AOP) is one of many viable steps for treating water; however, it is important to understand the byproducts of the treatment process to avoid creating other constituents more severe than the first. Tartrazine (TAR) was oxidized with pulsed Ultra-Violet (UV) Light Emitting Diodes (LEDs) in combination with hydrogen peroxide (H2O2) in an AOP at the laboratory scale. The relative concentration of TAR was reduced from 1 to between 1 - 0.75 over pH values between 6 and 9, and at Duty Cycles (DCs) ranging from 0% to 100%. The first order rate constant for TAR removal was statistically and positively correlated with DC, was statistically and negatively correlated with pH, and was typically greatest at pH6. DC and pH were variables in a regression model of the first order rate constant with adjusted R2 of 0.85. Chromatographic contrast angle determinations revealed that the byproduct profile was most significantly influenced by pH 7 under both positive and negative ionization, by the 70% DC for the positive ionization, and 50% DC for the negative ionization. DC and pH were variables in regression models...					
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