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Assessing the Reliability of the B-1B Lancer Using Survival Analysis

Francisco J. Rodriguez

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**ASSESSING THE RELIABILITY OF THE B-1B LANCER
USING SURVIVAL ANALYSIS**

THESIS

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AFIT-ENS-MS-18-M-156

**DEPARTMENT OF THE AIR FORCE
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ANALYSIS

THESIS

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In Partial Fulfillment of the Requirements for the
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Francisco J. Rodriguez, BS

Captain, USAF

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Abstract

During the 2017 posture statement to the US Senate Armed Services Committee, the Secretary of the Air Force and Chief of Staff of the Air Force stated the Air Force suffers from shrinking aircraft inventory, aging aircraft fleets, and flying beyond the expected service life. These trends are not an the exception to the B-1B Lancer, which has been in service since 1986. Recently, the B-1B Lancer has maintained the lowest mission capable (MC) rates of 47.7 percent. The purpose of this research is to explore the failure rates of the B-1B Lancer using survival analysis that investigates the failure behavior of the B-1B Lancer. A Cox proportional hazards regression model with frailty confirms the existence of unobserved heterogeneity or frailty in our analysis. When the frailty is controlled, combat missions increase in failure rates. Other variables, mainly flight hour or sortie duration related variables, are inconclusive and require further analysis. This study proposes insights based on findings and suggests future research directions.

Table of Contents

Abstract.....	iv
Table of Contents.....	v
I. Introduction.....	1
II. Literature Review.....	5
III. Methodology.....	8
IV. Data and Variables.....	10
V. Results and Discussion.....	13
VI. Conclusion.....	23
Bibliography.....	25
Appendix A: Excel Data File.....	27
Appendix B: R Commands and Results.....	83

List of Figures

Figure 1: Kaplan-Meier Survival Functions.....	16
Figure 2: Kaplan-Meier Hazards Functions.....	17

List of Tables

Table 1: Descriptive Statistics for Categorical Variables.....	10
Table 2: Descriptive Statistics for Continuous Variables.....	11
Table 3: Descriptive Statistics per Aircraft.....	13
Table 4: Kaplan-Meier Estimators for Survival Time.....	15
Table 5: Cox Proportional-Hazard Regression Results.....	18
Table 6: Cox PH Regression Results with Shared Frailty.....	20
Table 7: Cox PH Regression Results with Shared Frailty for Similar Aircraft.....	21

ASSESSING THE RELIABILITY OF THE B-1B LANCER USING SURVIVAL ANALYSIS

I. Introduction

In June 2017 the Secretary of the Air Force, Heather A. Wilson, and the Chief of Staff of the Air Force, General David L. Goldfein, presented to the United States Senate Armed Services Committee a candid state of affairs for the United States Air Force (DAF, 2017). These leaders stated that over the last quarter century, the number of aircraft in the Air Force inventory has been reduced from 8,600 aircraft to 5,500, while the operational demands for flying have increased. The Air Force of today averages procurement of 96 new aircraft per year compared to 510 aircraft prior to Operation Desert Storm in 1991. This reduction of aircraft procurement has resulted in the average age of the aircraft fleet to be more than 27 years old (DAF, 2017), with six different aircraft types over 50 years old (Everstine, 2014).

The United States Air Force has been flying combat missions without pause since 1991, with the latest missions supporting Operation Inherent Resolve to combat the Islamic State (ISIS), where 70 percent of the total coalition airstrikes having been conducted by the aircraft from the Air Force (DAF, 2017). These missions result in a very high accumulation of flying hours, requiring extensive and increased aircraft maintenance to support the high operations tempo. Currently, only 50 percent of the flying squadrons in the USAF are capable of executing all of their assigned missions (DAF, 2017). In 2014, the average mission capable rate for the Air Force fleet was 75

percent, with the lowest rate belonging to the B-1B Lancer at 47.7 percent (Everstine, 2014).

Manpower challenges are also a significant concern for senior USAF leaders. Recognizing that manpower levels were at dangerously low levels, the Fiscal Year 2018 (FY18) budget request allowed an increase in the total force (Active Duty, Air National Guard, Air Force Reserve, and civilians) from 660,707 to 669,611 personnel (DAF, 2017). Much of this increase in personnel is driven by a need for more maintenance personnel to support the aging fleet, and to support new aircraft entering the Air Force fleet. The FY18 budget request includes 11.9 billion dollars specifically for weapons systems sustainment, such as aircraft part and maintenance operations (DAF, 2017). The increased age of aircraft and higher usage leads to an increased cost of maintenance sustainment (Versprille, 2016).

As a consequence of the ever-aging USAF aircraft fleet, the supply of aircraft parts is becoming less dependable as companies that supplied parts for older aircraft have gone out of business (Versprille, 2016). Although an authorized method, cannibalization of parts from decommissioned aircraft at the 309th Aerospace Maintenance and Regeneration Group has become a routine operation for some aircraft types (Griffin and Tomlinson, 2016). Keeping legacy aircraft in the Air Force inventory longer than intentionally designed results in a negative feedback loop as illustrated by General Herbert Carlisle during his speech at the Air Force Association conference in February 2016, “If we keep the older weapons systems, we’re keeping the maintainers, we’re keeping the operations and maintenance costs... We’re doing all that for the aging fleet and that money can’t be put into new weapons systems.” (Versprille, 2016). An

infamous television segment by *Fox News* on the state of flying operations in the U.S. Air Force showed an aircraft maintenance technician with a landing gear component he had removed from a decommissioned B1-B Lancer static display aircraft to install in an operational B-1B due to parts scarcity (Griffin, 2016).

The B-1B Lancer has served in the United States Air Force since 1986, where it was originally designed as a supersonic long-range nuclear strike bomber to replace the B-52 Stratofortress (B-1B fact sheet, 2015). However, with the ending of the Cold War, the mission of the B-1B changed to that of a conventional bomber, a mission it was not originally designed to perform (B-1B fact sheet, 2015). A total of 100 aircraft were delivered to the Air Force between 1986 and 1988, but today only 64 aircraft are still active (B-1B fact sheet, 2015). The B-1B has been flying combat missions continuously since its first combat mission in 1998, averaging 23,000 flight hours annually over the last ten years (Everstine, 2014).

The B-1B Lancer having such a significant combat role in flying operations over the last decade while suffering from some of the most challenging maintenance issues in the Air Force is a cause for concern. While known to be highly unreliable for availability and having high failure rates, there is no study on this which employs survival analysis that could help better understand the failure behavior of the B-1B.

By using survival analysis, this thesis will answer the following question: *What is the B-1B's survival function concerning failures and what flying variables are related to its survival function to better predict its reliability?*

The purpose of this research is to explore the failure rates of the B-1B Lancer by using survival analysis utilizing flight hours, mission types, and a number of sorties as

variables to analyze the reliability of the B-1B. This research also will compare and contrast its finding with an existing study of B-1B failure rates conducted in 2017, and it will utilize the same baseline data but under a different methodology of analysis. This research also seeks to propose a desirable framework for reliability analysis for various other aircraft and identify future research directions for other weapon systems and weapon system components.

The scope of this research is an exploratory study with a limited sample of sortie information from 17 B-1B's flying from October 2013 to November 2016. The flight and maintenance data used as the basis for this research is assumed to be accurate, and that the sample used is unbiased and representative of the entire B-1B fleet.

II. Literature Review

The search for related studies utilizing survival analysis for aircraft or weapon systems did not result in any findings. However, studies were found where survival analysis was applied to complex equipment type items and traffic safety analysis.

A 2017 study on the failure rates of various electrical machines used in the diamond mining industry was used to better identify when different machines were likely to fail, but also which subcomponents would fail as well (Shevchuk, 2017). This study utilized the Kaplan-Meier estimator in the analysis which was able to overcome the challenges of processing incomplete data from maintenance records while still ensuring accuracy with the results given (Shevchuk, 2017).

Survival analysis was also used to investigate vehicle accidents at traffic intersections in Melbourne, Australia (Bagloee and Asadi, 2016). This study used survival analysis modeling of nine years of vehicle accident data to discover effective methods for reducing vehicle accidents and increasing pedestrian safety (Bagloee and Asadi, 2016).

While not specifically using survival analysis, a study conducted in 1977 on the F-4 Phantom by Tactical Air Command sought to determine what variables, such as accumulated flying hours, number of sorties flown, and mission types were driving increased maintenance requirements and failure rates (Hunsaker et al. 1977). This study found that the length of a sortie had minimal effect on failure rates. However, the type of missions flown did have a significant impact. The number of missions flown also drove

increased maintenance requirements when compared to other aircraft which accumulated the same total hours but in a fewer total number of sorties (Hunsaker et al. 1977).

The most significant study regarding the reliability of the B1-B Lancer was a 2017 analysis that used logistic regression and the systems reliability theory to predict B-1B failure rates based on different mission types and sortie duration (Williams, 2017). This study was motivated by the researcher's own maintenance experience with the B-1B in both stateside and deployed locations where he noticed that B-1B's conducting combat missions in a deployed location had higher mission capable rates than B-1B back at home station in the United States. The author sought to determine if the longer sorties inherent with combat missions had an impact on the failure rates of the B-1B and what the relationship, if any, there was between failure rates and mission types and sortie durations (Williams, 2017).

This research analyzed B-1B operations and maintenance data for 33 B-1B aircraft from October 2013 to November 2016. The data included sortie duration length, date of the mission, the mission types flown, the aircraft break codes, and the air aborts were sorted into a master data file consisting of a total of 5,067 sorties. This master data file was then used to conduct various logistic regression analysis tests on different mission types, combat, training, and combat and training missions combined (Williams, 2017).

The findings of this study concluded that sortie duration does have an impact on failure rates. The odds of a failure occurring from a sortie decrease by 3.8 percent for every additional hour flown in that sortie. This percentage was for all mission types combined. More specifically, for all training missions, the odds of failure occurring from

a sortie decreased by 7.8 percent for each additional hour flown in that sortie. However, some training mission types had no relationship between sortie length and sortie failure probability. Combat sorties had the greatest relationship between sortie failure rates and sortie duration, with an odds of sortie failure decreasing by 12.2 percent for every additional flight hour flown per sortie (Williams, 2017).

These findings led the researcher to propose that an additional flight hour for each training sortie could save the Air Force approximately \$12M per year in maintenance costs for the B-1B (Williams, 2017). The researcher did note that this would also increase fuel costs due to fuel consumption, and it would increase the rate at which aircraft would accumulate flight hours, therefore increasing the age of the airframe and accelerating timelines for flight hours driven maintenance (Williams, 2017).

The master data file used in the Williams study serves as the baseline of data for the survival analysis conducted in this thesis.

III. Methodology

There are three major approaches to survival analysis such as non-parametric, semi-parametric, and fully parametric models. This study employs non-parametric and semi-parametric models, that is, the Kaplan-Meier survival function and Cox proportional hazards regression along with descriptive statistics to perform the survival analysis on predicting B-1B failure rates. The KM survival function is defined as the product of all fractions that estimate the conditional probabilities for failure times $t_{(j-1)}$ and earlier. The Cox proportional hazard model, with fixed time covariates in scalar form, is also used where the baseline hazard function that is the function of a subject whose covariates all have the value of zero. In addition, because the function is arbitrary, there is no constant term in the model.

Cox and Oaks (1984:49) expresses the KM survival function as:

$$\widehat{\mathcal{S}}(t) = \prod^t \left(1 - \frac{d_j}{r_j} \right) \quad (1)$$

where

$\widehat{\mathcal{S}}(t)$ = estimator of the survival function

t = survival time

j = a time unit

d = failures

r = trials

Mills (2011:87) describes the Cox proportional hazard model with fixed-time covariates as:

$$h_i(t) = h_0(t) \{ \exp(\beta_1 x_{i1} + \dots + \beta_k x_{ik}) \}, \quad (2)$$

where

$h_i(t)$ = survival function

$h_0(t)$ = baseline function whose parameters are all zeros

β = regression coefficient

x = covariate

where $h_0(t)$ is the unspecified baseline hazard function. For the Cox proportional hazards model for frailty, Mills (2011:168) states the hazard rate for the j th individual in the i th subgroup as follows:

$$h(t_{ij}) = h_0(t) \{ \exp(\beta' \mathbf{x}_{ij} + \Psi' w_j) \}, \quad (3)$$

where

$h(t_{ij})$ = survival function

$h_0(t)$ = baseline function whose parameters are all zeros

β = regression coefficient

x = covariate

$\Psi' w_j$ = subgroup frailty

The subgroup frailty, w_j , is distributed with the mean 0 and variance 1. These models are solved using R version 3.3.2 (2016) with the survival package. The R commands and results are available in Appendix B.

IV. Data and Variables

The dataset for this study, which is retrieved from Williams (2017), includes 1,953 observations for 17 B-1B aircraft. This data is available in Appendix A. Failure events in the data set are recorded in days for 38 months from October 2013 to November 2016. Since the time unit is a day, the use of continuous time survival models is appropriate (Yamaguchi, 1991:16).

There are categorical and continuous variables as presented in Table 1 and Table 2. The categorical variables are Combat Mission (1 for combat missions and 0 for non-combat missions) and Failure (1 for failures).

Table 1: Descriptive Statistics for Categorical Variables

	Total Cases	Frequency	Percent
Combat Mission	1,953	901	46.1
Failure	1,953	682	34.9

Combat Mission is a dummy variable and indicates a number of sorties flown for combat orders. A total of 901 combat sorties are recorded during the observation period. Regarding the number of failures, 17 aircraft experienced 682 failure events during the period. On average, this is 40.12 failures per aircraft during the 38 months. The descriptive statistics for continuous variables are shown in Table 2.

Table 2: Descriptive Statistics for Continuous Variables

	Total Cases	Minimum	Maximum	Mean	Standard Deviation
Flight Hours per Sortie	1,953	0.5	24.1	8.232	4.189
Flight Hours (Lagged)	1,953	0.5	24.1	8.231	4.186
Flight Hours between Failures	682	0.5	340.4	23.244	34.585
Cumulative Sorties*	17	5.0	283.0	146.590	67.440

*: Total number during the observation period.

The mean for flight hours per sortie is 8.23 hours. In addition to flight hours per sortie, flight hours (lagged), which are lagged for one period, will be included in survival analysis. Flight hours between failures are included to measure the cumulative effect of flight hours on the failure of an airplane. Flight hours between failures show the highest variability among the continuous variables as its standard deviation to the mean indicates. Cumulative sorties represent the number of sorties flown per aircraft during the observation period. Instead of calendar days, cumulative sorties will be used for modeling time in survival analysis. By using cumulative sorties, the aircraft on the ground for maintenance and/or awaiting spare parts will not be counted as available or not failed. When comparing the mean for flight hours per sortie with flight hours between failures, an aircraft suffers a failure almost every three sorties. The values used to calculate the average number of sorties between failures does not factor in maintenance issues detected on the ground between sorties.

There are various factors that affect the reliability of aircraft. Mission type for military aircraft is one of these factors. Sherbrooke (1997) found that mission type was significant for predicting aircraft spares demand. Williams (2017) also identified that mission type was significant when he grouped missions into combat and training categories. Therefore:

H1: Combat missions will increase failure rates.

Pohl (1991) used flight hours in the simulation study for assessing the reliability of fighter jets. Sherbrooke found that sortie duration or flight hours per sorties affected to aircraft spares demand that was related to the failure of aircraft. Williams (2017) concluded that sortie duration was positively related to the survival function of aircraft. Therefore:

H2: Longer flight hours per sortie will increase failure rate.

Similarly, Sherbrooke (1997) argued that previous sorties were correlated with failures at the time the failures were found. Therefore:

H3: Previous flight hours (lagged flight hours) will affect failure rates.

Additionally, we assume that cumulative flight hours between failures are related to the survival of aircraft. Therefore:

H4: Flight hours between failures will increase failure rates.

These hypotheses are tested using non-parametric and parametric survival analyses.

V. Results and Discussion

Simple summary statistics of the variables per aircraft during the observation period are presented in Table 3. Instead of the tail numbers of the 17 aircraft, numbers one (1) through 17 are assigned to them. These identification numbers (ID) are also necessary for modeling frailty in survival analysis for recurrent events such as number of failures in this study.

Table 3: Descriptive Statistics per Aircraft

ID	Failures	Total Flight Hours	Flight Hours/Failure	Combat Missions	Total Sorties
1	76	2,152.70	28.3	157	255
2	43	986.90	23.0	47	183
3	52	1,455.90	28.0	110	176
4	53	938.20	17.7	45	168
5	61	1,252.90	20.5	73	185
6	43	873.20	20.3	44	143
7	66	2,102.20	31.9	136	283
8	53	912.20	17.2	52	137
9	22	277.80	12.6	0	74
10	6	65.00	10.8	0	20
11	36	1,103.10	30.6	61	173
12	49	1,833.00	37.4	124	231
13	27	375.70	13.9	1	109
14	2	15.70	7.9	0	5
15	29	388.90	13.4	0	135
16	27	935.20	34.6	51	126
17	37	407.90	11.0	0	135
Min	2	15.70	7.9	0	5
Max	76	2,152.70	37.4	157	283
Mean	40	945.68	21.1	53	149
SD	20	660.50	9.2	52	73

As Table 3 reveals, some aircraft such as ID numbers 1, 3, 7, and 12, have flown more than others. In addition, they have carried out more combat missions or sorties. Because the B-1B Lancer has been operated in the Air Force since 1986, the aircraft with fewer flight hours, for example, ID numbers 9, 10, and 14, may be under maintenance or simply not utilized much during the 38-month period. Based on this assumption, we can conclude that some aircraft are either more or less reliable than others.

When the ratios between combat missions or sorties and total sorties during the period are compared, the reliable aircraft have flown for greater flight hours than the less reliable aircraft. For example, the reliability for aircraft 1 was 61.57 percent while the reliability for aircraft 2 was 25.57 percent. The fourth column in Table 3, mean flight hours per failure, supports this finding. This finding will therefore be used in interpreting the results of the survival analysis. This issue is related to the assumption of homogeneity of the subjects. Therefore, we will not discuss the results of hypothesis testing until we address the violation of the homogeneity assumption.

Non-parametric survival analyses, Kaplan-Meier (KM) estimators, have been applied to the data set before trying semi-parametric survival models. The mean and median along with 95 percent confidence intervals by the KM analysis are exhibited in Table 4.

Table 4: Kaplan-Meier Estimators for Survival Time

Combat Mission (1=yes)	Mean				Median			
	Estimate	Standard Error	95% Confidence Interval		Estimate	Standard Error	95% Confidence Interval	
			Lower Bound	Upper Bound			Lower Bound	Upper Bound
0	153.75	3.63	146.63	160.87	162.00	4.38	153.42	170.58
1	168.09	3.73	160.79	175.40	161.00	8.78	143.80	178.21
Overall	163.14	2.78	157.69	168.59	164.00	3.73	156.70	171.30

The 95 percent confidence intervals for combat and non-combat missions or sorties around the arithmetic mean values are slightly overlapping. The same intervals around the median values are also significantly overlapping. Therefore, it is shown that the survival functions of the aircraft are not different between combat and non-combat missions in this data set. This finding is supported by the survival functions depicted in Figure 1.

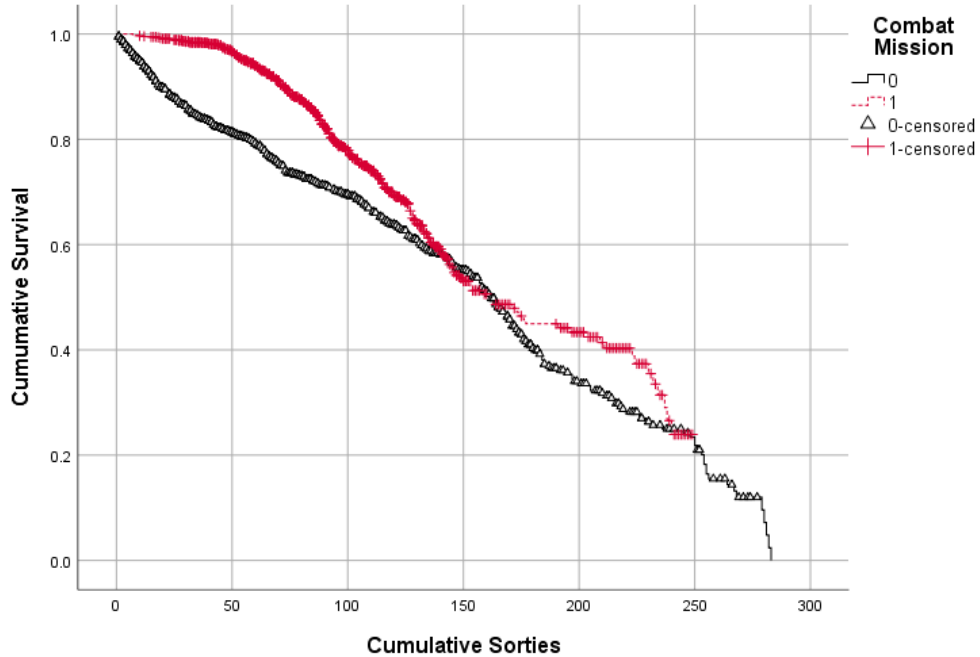


Figure 1: Kaplan-Meier Survival Functions for Combat and Non-Combat Missions

In Figure 1, two functions are overlapping around 150 and 250 sorties. As the 95 percent confidence intervals are not independent in Table 4, Figure 1 confirms that two types of missions yield overlapping survival functions when the observations for 17 aircraft are pooled for analysis.

The KM hazards functions (see Figure 2) follow similar patterns found in Figure 1. Overall, non-parametric models or KM estimators fail to discern the survival hazards functions by mission types.

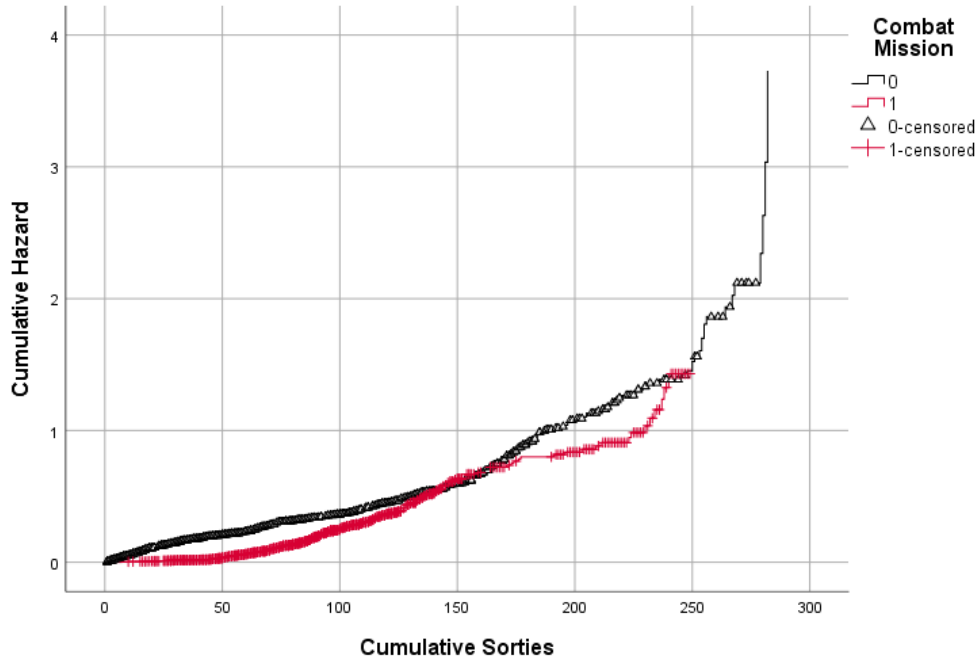


Figure 2: Kaplan-Meier Hazards Functions for Combat and Non-Combat Missions

A Cox proportional hazards model, a semi-parametric approach, is employed to confirm the factors that affect the survival of the aircraft. The results of the model are presented in Table 5. The dependent variable of this model is the number of failure events. Time is measured using the cumulative number of sorties during the observation period. R with the survival package is used for estimating the Cox proportional hazards function.

Table 5: Cox Proportional-Hazard Regression Results

	Coef	Exp (Coef)	SE (Coef)	z	Pr(> z)	Lower (95%)	Upper (95%)
Combat Mission	0.0792	1.0824	0.1199	0.661	0.5089	0.8558	1.3690
Flight Hours between Failures	-0.0041	0.9959	0.0015	-2.736	0.0062***	0.9930	0.9988
Flight Hours	-0.0670	0.9352	0.0132	-5.063	0.0000***	0.9113	0.9598
Flight Hours (Lagged)	0.0067	1.0068	0.01241	0.542	0.5876	0.9826	1.0315

Significance: *** = significant at 0.01

The change in the log-likelihood values from -4,468.748 to -4,436.381 is statistically significant at $\alpha = 0.01$, proving the validity of this model. Two variables such as combat mission and flight hours (lagged) are not significant in the model. The remaining two variables, flight hours between failures and flight hours (per sortie) are statistically significant at $\alpha = 0.01$. Before interpreting these significant variables, it must be ensured that failure events in the model are recurrent and need to be treated accordingly.

The next model, a Cox proportional hazard regression with shared frailty is used. The exponentiated regression coefficient for flight hours between failures is less than one, which implies that this variable moves the opposite direction to that of the failure rate. The magnitude of the variable is $[(0.9959 - 1) \times 100\% = 0.41\%]$ or 0.41 percent when other variables are held. That is, one hour increase in flight hours between failures will decrease failure hazards by 0.41 percent. Holding other variables constant, one hour

increase in flight hours per sortie will reduce the failure hazards by 6.48 percent.

Therefore, it can be concluded that increased flight hours can reduce failure rates as Williams (2017) claimed. However, as shown in Table 3, the more reliable aircraft flew longer hours than the less reliable aircraft. In addition, when a malfunction on an aircraft is found during the flight, the airplane aborts a mission and returns to base, therefore having fewer flight hours. Accordingly, these results show mathematical relationships, not causal relationships. Therefore, based on these findings, recommending longer flight hours to decrease the hazards rate is questionable. The appropriate interpretation is that reliable aircraft fly longer hours than unreliable aircraft as confirmed in Table 3.

Table 3 shows that some aircraft have more flight hours and combat sorties than other aircraft during the observation period. It indicates that the aircraft that are frail to failures have fewer flight hours than the aircraft that are not. To examine the frailty of subjects on the model and handle recurrent events or failures, a Cox proportional hazards (PH) model with shared frailty is conducted, which is a random effect model. The same dependent and independent variables along with the same time measure are included in this model. Table 6 exhibits results of the model.

Table 6: Cox PH Regression Results with Shared Frailty

	Coef	Exp (Coef)	SE (Coef)	χ^2	<i>p</i>	Lower (95%)	Upper (95%)
Combat Mission	0.6163	1.8520	0.1329	21.49	0.0000***	1.4272	2.4032
Flight Hours between Failures	-0.0021	0.9979	0.0015	2.04	0.1500	0.9950	1.0008
Flight Hours	-0.0683	0.9339	0.0134	26.00	0.0000***	0.9097	0.9588
Flight Hours (Lagged)	0.0068	1.0068	0.0130	0.28	0.6000	0.9816	1.0327
Frailty (ID)				880.80	0.0000***		

Note: Variance of random effect = 0.9912***

Significance: *** = significant at 0.01

The change in the loglikelihood values from -4,468.748 to -4,261.436 is significant for the validity of the model. Frailty is measured by including identification numbers (ID). The same identification number is assigned for the failure events of a specific aircraft. The significance of frailty (ID) confirms the existence of frailty among the aircraft in the model. The indicator of frailty or the variance of random effect, which should be zero if no frailty presents, takes the value of 0.9923. When accounted for frailty, results are different from the model without it. Combat mission and flight hours per sortie are significant at $\alpha = 0.01$. Combat mission, a dummy variable, increase a failure rate by 85.2 percent for combat sorties compared to non-combat sorties. Again, caution must be used when interpreting combat mission. It is reasonable to conclude the most reliable aircraft are assigned for combat missions. Regression models can be used for confirming causal relationships but they are not sufficient to prove the causal relationships. Other measures such as theories, experiments, and temporal relationships

should be considered. Therefore, this study does not support the claim that B-1B's should fly longer sorties to reduce failure hazards.

To confirm the results in Table 6, two similar aircraft are selected: numbers 1 and 12, with 410 observations and 125 failures. The results of the Cox PH regression model are presented in Table 7.

Table 7: Cox PH Regression Results with Shared Frailty for Similar Aircraft

	Coef	Exp (Coef)	SE (Coef)	χ^2	<i>p</i>	Lower (95%)	Upper (95%)
Combat Mission	2.2086	9.1029	0.0322	46.86	0.0000***	4.8366	17.1323
Flight Hours between Failures	0.0018	1.0018	0.0025	0.50	0.4800	0.9969	1.0067
Flight Hours	-0.0758	0.9270	0.0272	7.78	0.0053***	0.8789	0.9777
Flight Hours (Lagged)	-0.0059	0.9941	0.0279	0.05	0.8300	0.9411	1.0500
Frailty (ID)				0.17	0.4200		

Note: Variance of random effect = 0.0013

Significance: *** = significant at 0.01

The results in Table 7 are similar to those in Table 6 except frailty is not significant, and the variance of random effect is close to zero (0.0013). Frailty is confirmed among the aircraft. In the future, when the reliability of aircraft are analyzed, it is necessary to group aircraft for frailty and develop models accordingly. If not, the estimated coefficients may be misleading.

Regarding the hypotheses, the results with frailty support “H1: Combat missions will increase failure rates.” The statistic for H2 is significant but its direction is reversed. In addition, because the reliable aircraft fly longer than the less reliable ones, further

study is needed on this issue. The statistics for H3 and H4 are insignificant and inconclusive at this time.

This study demonstrates the application of survival analysis to analyzing the reliability of the B-1B Lancer. Survival analysis is known to be superior to logistics regression for incorporating time and treating recurrent events. At the time of this study, there were no other studies with survival analysis on military aircraft. Therefore, the major contributions of this study are trifold: first, incorporating time and recurrent events using survival analysis, second, proposing a pertinent research framework for the survival analysis of military aircraft, and third, providing appropriate insights for predicting aircraft failures. This study can be extended to analyzing the reliability of various types of aircraft and weapon systems. In addition, the framework in this research can be applied to studies on testing and evaluating new products or systems that experience oscillating behaviors between two states such as working or not working. Finally, this study needs further efforts to improve due to some limitations.

This study is exploratory in nature, and additional studies that address the limitations and future directions are recommended, such as: including time-dependent variables such as the age of the aircraft, modeling different types of episodes, testing fully parametric survival models, applying survival analysis to major components or line replaceable units such as engines, navigation systems, etc., and trying survival analysis with different aircraft types such as cargo, tanker, and fighter aircraft.

VI. Conclusion

The Secretary of the United States Air Force and Chief of Staff of the Air Force expressed their concern on shrinking aircraft inventory, aging aircraft fleets, and flying beyond expected service life in the 2017 posture statement to the US Senate Armed Services Committee. In 2014, the average mission capable rate for the Air Force fleet was 75 percent, with the lowest rate belonging to the B-1B Lancer at 47.7 percent (Everstine, 2014).

This study examines the reliability of the B-1B Lancer using the sample dataset from 17 B-1B aircraft. Unlike the previous study (Williams, 2017), which uses logistics regression, this study applies survival analysis to the data set for identifying factors that affect the failures of the B-1B Lancer. The major advantages of survival analysis over logistics regression are incorporating time and handling recurrent events such as failures, in its model. When considering failures as recurrent events in a Cox partial hazards model with frailty, it is shown that some aircraft are frailer than others, and combat missions increase hazards. The other significant variable is flight hours, which has the exponentiated coefficient slightly smaller than one (1) in the model.

Because the Air Force puts longer flight hours and combat missions on more reliable aircraft than less reliable ones, the use of caution is required for the interpretation of this variable. The reliable airplanes fly longer hours as proven in Tables 3 and 6. It happens when unobserved heterogeneity exists in a model. Survival analysis assumes the homogeneity of subjects in an ordinary model.

Unobserved heterogeneity such as more reliable or less reliable airplanes in this study can hinder proper estimates of parameters in the model. Thus, this study proposes grouping aircraft by reliability categories or other criteria and investigating their reliability. This study can be extended to analyzing the reliability of various types of aircraft and weapon systems. The framework in this research can be also applied to studies on testing and evaluating new products or systems that experience oscillating behaviors between two states such as working or not working.

Major contributions of this study include proposing a research framework for the survival analysis of aircraft, modeling failures as recurrent events, and providing managerial insights. This study also comes with limitations that should be addressed in the future. They are including time-dependent variables, modeling various types of episodes, testing fully parametric survival models, conducting survival analysis at a major component level, and expanding the study to the variety of aircraft. Since this study is an initial attempt and exploratory for the Air Force, we expect additional studies in this area.

Bibliography

- Bagloee, Saeed Asadi., & Asadi, Mohsen. (2016). Crash analysis at intersections in the CBD: A survival analysis model. *Transportation Research Part A: Policy and Practice*.
- Cox, David Roxbee., & Oakes, D. (1984). *Analysis of Survival Data*. New York: Chapman and Hall.
- Department of the Air Force (2017, June 6). The Future of Air and Space Power: Air Force Posture Statement Fiscal Year 2018 President's Budget Request. *Presentation to the Committee on Armed Services, United States Senate*.
- Everstine, Brian. (2014, October 13). Race Against Time: More People Money Needed to Keep Aging Fleets Flying. *Air Force Times*. Retrieved January 20, 2018, from <https://www.airforcetimes.com/story/military/2014/10/13/race-against-time-more-people-money-needed-to-keep-aging-fleets-flying/17180797/>
- Griffin, Jennifer., & Tomlinson, Lucas. (2016, May 14). 'Wiped Out': Air Force losing pilots and planes to cuts, scrounging for spare parts. *Fox News*. Retrieved January 16, 2018, from <http://www.foxnews.com/politics/2016/05/14/wiped-out-air-force-losing-pilots-and-planes-to-cuts-scrounging-for-spare-parts.html?intcmp=hppop>
- Hunsaker, H. D., Conway, F., Jr., & Doherty, E. R. (1977, Apr). Logistics Impact of Sortie Oriented Air Crew Training. Retrieved January 08, 2018, from <http://oai.dtic.mil/oai/oai?verb=getRecord&metadataPrefix=html&identifier=ADA091628>
- Mills, Melinda. (2011). *Introducing Survival and Event History Analysis*. London: SAGE Publications Ltd.
- Pohl, Letitia M. (1991). Evaluation of F-15E availability during operational test. *1991 Winter Simulation Conference Proceedings., Simulation Conference* Retrieved February 18, 2018, from <http://dl.acm.org/citation.cfm?id=304238.304322>
- Sherbrooke, Craig C. (1997, Apr). Using Sorties vs. Flying Hours to Predict Aircraft Spares. Retrieved February 10, 2018, from <http://oai.dtic.mil/oai/oai?verb=getRecord&metadataPrefix=html&identifier=ADA331910>
- Shevchuk, Vladislav A., Muravlev, Oleg P., & Stolyarova, Olga O. (2017). Survival analysis of A.C. machines in the diamond industry using the Kaplan-Meier estimator. *MATEC Web of Conferences, Vol 141, P 01033 (2017)*, 01033.
- United States Air Force (2015, December). B-1B Lancer Fact Sheet. Retrieved January 12, 2018, www.af.mil/About-Us/Fact-Sheets/Display/Article/104500/b-1b-lancer/

Versprille, Allyson. (2016, April). Air Force Modernization at Risk as Maintenance Costs Continue to Climb. *National Defense Magazine*. Retrieved January 15, 2018, from <http://www.nationaldefensemagazine.org/articles/2016/4/1/2016april-air-force-modernization-at-risk-as-maintenance-costs-continue-to-climb>

Williams, Russell H. (2017, March). Predicting Failure Rates for the B-1B Bomber. MS thesis. AFIT/ENS/LSCM. Department of Logistics and Operational Sciences, Air Force Institute of Technology (AU), Wright-Patterson AFB, OH

Yamaguchi, Kazuo. (1991). *Event History Analysis*. Newbury Park, CA: SAGE Publications, Inc.

Appendix A: Excel Data File

EQPID	JULIAN DATE	Operating	Mission1 (1=Combat)	Mission2 (1=Depot)	HRS	Cumulative Flight Hours	Cumulative Sorties	ANY FAILURE
		Time in Days Since Last Failure						
A5060	13330	1	0	0	2.1	5.6	3	0
A5060	13339	9	0	0	10.9	16.5	4	1
A5060	13343	4	0	0	2.5	25.4	7	0
A5060	13345	6	0	0	1.9	27.3	8	1
A5060	13347	2	0	0	5	32.3	10	0
A5060	13351	6	0	0	3.6	33.9	11	1
A5060	13354	3	0	0	1.9	35.8	12	1
A5060	14003	14	0	0	2.2	38	13	0
A5060	14003	14	0	0	2	40	14	1
A5060	14031	28	0	0	2.1	42.1	15	1
A5060	14043	12	0	1	9.5	51.6	16	0
A5060	14044	13	0	1	7.9	59.5	17	0
A5060	14046	15	1	0	12.9	72.4	18	1
A5060	14048	2	1	0	12.3	84.7	19	1
A5060	14050	2	1	0	11.8	96.5	20	1
A5060	14051	1	1	0	12.3	108.8	21	0
A5060	14055	5	1	0	12.1	120.9	22	0
A5060	14056	6	1	0	12.3	133.2	23	0
A5060	14058	8	1	0	12.6	145.8	24	1
A5060	14060	2	1	0	12.7	158.8	25	1
A5060	14066	6	1	0	11.3	170.1	26	0
A5060	14067	7	1	0	12.5	182.6	27	0
A5060	14068	8	1	0	12.4	195	28	0
A5060	14069	9	1	0	12.4	207.4	29	1
A5060	14071	2	1	0	10.8	218.2	30	0
A5060	14072	3	1	0	12.6	230.8	31	0
A5060	14073	4	1	0	12.8	243.6	32	0
A5060	14075	6	1	0	11.8	255.4	33	0
A5060	14077	8	1	0	11.9	267.3	34	0
A5060	14078	9	1	0	14.1	281.4	35	0

A5060	14080	11	1	0	13.1	294.5	36	0
A5060	14081	12	1	0	12.2	306.7	37	1
A5060	14084	3	1	0	15.6	322.3	38	0
A5060	14085	4	1	0	12.1	334.4	39	0
A5060	14092	11	1	0	12.3	346.7	40	0
A5060	14094	13	1	0	12.3	359	41	0
A5060	14095	14	1	0	13.1	372.1	42	0
A5060	14096	15	1	0	12.6	384.7	43	0
A5060	14097	16	1	0	11.3	396	44	0
A5060	14098	17	1	0	12.7	408.7	45	0
A5060	14100	19	1	0	13.1	421.8	46	0
A5060	14104	23	1	0	11.6	433.4	47	0
A5060	14105	24	1	0	12.1	445.5	48	0
A5060	14106	25	1	0	11.9	457.4	49	0
A5060	14108	27	1	0	12.2	469.6	50	0
A5060	14110	29	1	0	14.2	483.8	51	1
A5060	14112	2	1	0	13.2	497	52	0
A5060	14113	3	1	0	12.7	509.7	53	0
A5060	14114	4	1	0	11	520.7	54	0
A5060	14116	5	1	0	12.2	532.9	55	1
A5060	14117	1	1	0	12	544.9	56	0
A5060	14118	2	1	0	12.2	557.1	57	1
A5060	14120	2	1	0	12.1	569.2	58	0
A5060	14121	3	1	0	12.2	581.4	59	0
A5060	14123	5	1	0	7.3	588.7	60	1
A5060	14125	2	1	0	21.4	610.1	62	0
A5060	14127	4	1	0	1.1	611.2	63	0
A5060	14129	6	1	0	12.5	623.7	64	0
A5060	14131	8	1	0	12.2	635.9	65	0
A5060	14132	9	1	0	13.5	649.4	66	0
A5060	14134	11	1	0	12.2	661.6	67	0
A5060	14136	13	1	0	12.6	674.2	68	0
A5060	14137	15	1	0	12.7	686.9	69	0
A5060	14139	17	1	0	10	696.9	70	0
A5060	14141	19	1	0	13.5	710.4	71	0
A5060	14142	20	1	0	10.6	721	72	0
A5060	14143	21	1	0	13	747.5	73	0

A5060	14144	22	1	0	13.5	761	74	0
A5060	14146	24	1	0	12.7	773.7	75	0
A5060	14147	25	1	0	12.3	786	76	0
A5060	14148	26	1	0	13.2	799.2	78	0
A5060	14149	27	1	0	12.3	811.5	79	0
A5060	14152	30	1	0	12.9	824.4	80	0
A5060	14154	32	1	0	12.1	836.5	81	0
A5060	14155	33	1	0	12.8	849.3	82	0
A5060	14157	35	1	0	10.6	859.9	83	0
A5060	14159	37	1	0	12.8	872.7	84	0
A5060	14160	38	1	0	13.1	885.8	85	0
A5060	14162	40	1	0	14.1	899.9	86	0
A5060	14164	42	1	0	10.4	910.3	87	1
A5060	14170	6	1	0	13.8	924.1	88	0
A5060	14172	8	1	0	12.9	937	89	0
A5060	14174	10	1	0	12	949	90	0
A5060	14175	11	1	0	12.5	961.5	91	0
A5060	14176	12	1	0	11	972.5	92	1
A5060	14177	1	1	0	12.7	985.2	93	0
A5060	14178	2	1	0	11.6	996.8	94	0
A5060	14179	3	1	0	11.5	1008.3	95	0
A5060	14180	4	1	0	11.8	1020.1	96	0
A5060	14181	5	1	0	11.8	1031.9	97	0
A5060	14183	6	1	0	11.8	1043.7	98	0
A5060	14184	7	1	0	12.2	1055.9	99	0
A5060	14185	8	1	0	11.9	1067.8	100	0
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A5060	14188	11	1	0	12.3	1092.4	102	0
A5060	14190	13	1	0	11.8	1104.2	103	1
A5060	14192	2	1	0	12.4	1116.6	104	0
A5060	14194	4	1	0	12.2	1128.8	105	1
A5060	14196	2	1	0	12.7	1141.5	106	1
A5060	14197	1	1	0	12.7	1154.2	107	0
A5060	14199	3	1	0	12.7	1166.9	108	0
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A5060	14201	5	1	0	11.3	1191.6	110	0
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A5060	14206	1	1	0	13.1	1225.7	113	1
A5060	14208	2	1	0	1	1226.7	114	1
A5060	14209	1	1	0	1	1227.7	115	1
A5060	14210	1	1	0	12.5	1240.2	116	0
A5060	14211	2	1	0	12.1	1252.3	117	0
A5060	14213	4	1	0	12.6	1264.9	118	0
A5060	14216	7	1	0	12.3	1277.2	119	0
A5060	14219	10	1	0	11.5	1288.7	120	0
A5060	14220	11	1	0	11.2	1299.9	121	0
A5060	14223	14	1	0	12.6	1312.5	122	0
A5060	14224	15	1	0	11.8	1324.3	123	1
A5060	14226	2	1	0	12.6	1336.9	124	0
A5060	14229	5	1	0	10.1	1347	125	0
A5060	14230	6	1	0	2	1349	126	1
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A5060	14235	3	1	0	12.9	1386.2	129	1
A5060	14239	4	1	0	12.8	1399	130	1
A5060	14243	4	1	0	12	1411	131	0
A5060	14244	5	1	0	10.6	1421.6	132	0
A5060	14246	7	1	0	12.3	1433.9	133	1
A5060	14247	1	1	0	12.5	1446.4	134	0
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A5060	14249	1	1	0	15.7	1472.4	136	1
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A5060	14255	6	1	0	12.5	1522.5	140	0
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A5060	14258	9	1	0	12.2	1547.8	142	0
A5060	14259	10	1	0	12	1559.8	143	0
A5060	14261	12	1	0	12	1571.8	144	1
A5060	14262	1	1	0	11.8	1583.6	145	0
A5060	14266	5	1	0	11.7	1595.3	146	1
A5060	14268	2	1	0	12.4	1607.7	147	1
A5060	14270	2	1	0	13.5	1621.2	148	0

A5060	14271	3	1	0	13.1	1634.3	149	1
A5060	14272	1	1	0	13.1	1647.4	150	0
A5060	14273	2	1	0	13	1660.4	151	0
A5060	14274	3	1	0	9.8	1670.2	152	1
A5060	14274	0	1	0	10.3	1680.5	153	1
A5060	14275	1	1	0	10.9	1691.4	154	0
A5060	14276	2	1	0	11	1702.4	155	0
A5060	14278	4	1	0	12.6	1715	156	0
A5060	14279	5	1	0	11.8	1726.8	157	0
A5060	14280	6	1	0	12.8	1739.6	158	1
A5060	14282	2	1	0	13	1752.6	159	0
A5060	14288	8	1	0	12.5	1765.1	160	0
A5060	14290	10	1	0	6.2	1771.3	161	1
A5060	14292	2	1	0	7.7	1779	162	1
A5060	14293	1	1	0	1.1	1780.1	163	1
A5060	14294	1	1	0	12.9	1793	164	0
A5060	14296	3	1	0	13.9	1806.9	165	0
A5060	14298	5	1	0	7.9	1814.8	166	0
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A5060	14346	2	1	0	1.1	1905.7	175	0
A5060	14348	4	1	0	3.9	1909.6	176	1
A5060	14364	16	1	0	1.2	1910.8	177	1
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A5060	15041	36	0	0	3.3	1935.7	179	0
A5060	15104	99	0	0	1.7	1937.4	180	1
A5060	15106	2	0	0	4	1941.4	182	0
A5060	15106	3	0	0	5	1946.4	183	1
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A5060	15162	28	0	0	3.2	1954.6	185	1
A5060	15166	4	0	0	1.7	1956.3	186	0

A5060	15166	4	0	0	1.7	1958	187	1
A5060	15188	22	0	0	8	1966	188	1
A5060	15231	43	0	0	6.4	1972.4	190	0
A5060	15233	45	0	0	2.2	1974.6	191	1
A5060	15237	4	0	0	5.6	1980.2	193	0
A5060	15239	6	0	0	3.1	1983.3	194	0
A5060	15239	6	0	0	3	1986.3	195	1
A5060	15302	63	0	0	3.8	1990.1	196	0
A5060	15302	63	0	0	4	1994.1	197	1
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A5060	16006	62	0	0	2.8	2014.6	204	1
A5060	16019	13	0	0	2.9	2017.5	205	1
A5060	16047	28	0	0	8.2	2025.7	208	0
A5060	16049	30	0	0	2.8	2028.5	209	0
A5060	16049	30	0	0	2.2	2030.7	210	1
A5060	16056	7	0	0	1.7	2032.4	211	1
A5060	16098	41	0	0	6.1	2038.5	212	0
A5060	16101	44	0	0	3.4	2041.9	213	0
A5060	16102	45	0	0	3.9	2045.8	214	1
A5060	16106	4	0	0	2.3	2048.1	215	1
A5060	16111	5	0	0	2.7	2050.8	216	0
A5060	16113	7	0	0	3.4	2054.2	217	0
A5060	16119	13	0	0	2	2056.2	218	0
A5060	16137	31	0	0	3.6	2059.8	219	1
A5060	16158	21	0	0	9.9	2069.7	222	0
A5060	16160	23	0	0	10.8	2080.5	225	0
A5060	16162	25	0	0	3.9	2084.4	226	1
A5060	16174	12	0	0	4	2088.4	227	0
A5060	16176	14	0	0	2.1	2090.5	228	1
A5060	16176	0	0	0	2.2	2092.7	229	1
A5060	16187	11	0	0	1.8	2094.5	230	0
A5060	16189	13	0	0	5.7	2100.2	232	0
A5060	16193	17	0	0	7.3	2107.5	235	0

A5060	16195	19	0	0	3.2	2110.7	236	1
A5060	16197	2	0	0	4.7	2115.4	238	0
A5060	16201	6	0	0	1.7	2117.1	239	0
A5060	16203	8	0	0	5.4	2122.5	241	0
A5060	16214	19	0	0	7.8	2130.3	244	0
A5060	16223	28	0	1	16.1	2146.4	245	1
A5060	16230	7	0	0	6.4	2152.8	247	0
A5060	16234	11	0	0	2.8	2155.6	248	1
A5060	16238	4	0	0	2.9	2158.5	249	0
A5060	16238	4	0	0	1.9	2160.4	250	1
A5060	16251	13	0	0	3.5	2163.9	251	0
A5060	16256	18	0	1	10.2	2174.1	252	0
A5060	16261	23	0	0	3.6	2177.7	253	1
A5060	16271	7	0	1	2.4	2180.1	254	1
A5060	16306	35	0	0	3.3	2183.4	255	1
A5066	13275	1	0	0	5.6	5.6	2	0
A5066	13277	3	0	0	5.1	10.7	4	0
A5066	13280	6	0	0	5.5	16.2	6	0
A5066	13281	7	0	0	2.8	19	7	0
A5066	13283	9	0	0	6.5	25.5	9	0
A5066	13289	15	0	0	3	28.5	10	1
A5066	13294	5	0	0	6.4	32.9	12	0
A5066	13296	7	0	0	5.4	38.3	14	0
A5066	13298	9	0	0	2.5	40.8	15	1
A5066	13304	6	0	0	6.5	47.3	17	0
A5066	13309	11	0	0	2.3	49.6	18	0
A5066	13311	13	0	0	2.6	52.2	19	0
A5066	13316	18	0	0	7.7	59.9	21	0
A5066	13318	20	0	0	8	67.9	23	0
A5066	13322	24	0	0	1.9	69.8	24	0
A5066	13322	24	0	0	2.1	71.9	25	1
A5066	13343	21	0	0	2.2	74.1	26	1
A5066	13345	2	0	0	8.6	82.7	29	0
A5066	13347	4	0	0	2.8	85.5	30	0
A5066	13354	11	0	0	1.8	87.3	31	0
A5066	13354	11	0	0	1.6	88.9	32	1
A5066	14021	32	0	0	4.2	93.1	33	0

A5066	14023	34	0	0	3.4	96.5	34	0
A5066	15006	382	0	1	1.6	98.1	35	0
A5066	15013	389	0	0	5.1	103.2	36	0
A5066	15013	389	0	0	2.5	105.7	37	1
A5066	15015	2	0	0	4.9	110.6	38	0
A5066	15021	8	0	0	3	113.6	39	1
A5066	15040	19	0	0	7.7	121.3	40	0
A5066	15042	21	0	0	7.3	128.6	41	0
A5066	15044	23	0	0	3.3	131.9	42	0
A5066	15044	23	0	0	2.4	134.3	43	1
A5066	15051	7	0	0	5.3	139.6	45	0
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A5066	15061	17	0	0	3.1	152.7	49	1
A5066	15063	2	0	0	6	158.7	51	0
A5066	15064	3	0	0	4.1	162.8	52	0
A5066	15065	4	0	0	6.2	169	54	0
A5066	15068	7	0	0	2.2	171.2	55	1
A5066	15070	2	0	0	3.2	174.4	56	0
A5066	15071	3	0	0	3.3	177.7	57	0
A5066	15072	4	0	0	4	181.7	58	1
A5066	15079	7	0	0	2.3	184	59	1
A5066	15082	3	0	0	10.3	194.3	62	0
A5066	15084	5	0	0	4.8	199.1	63	0
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A5066	15093	9	0	0	2.5	207	65	1
A5066	15113	21	0	0	3.7	210.7	66	1
A5066	15118	5	0	0	6.3	217	67	1
A5066	15119	1	0	0	6.1	223.1	68	0
A5066	15120	2	0	0	5.8	228.9	69	0
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A5066	15127	9	0	0	5.5	240.7	71	1
A5066	15183	55	0	0	1.3	242	72	0
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A5066	15243	60	0	0	7.1	251.3	75	0
A5066	15245	62	0	0	8.8	260.1	77	0
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A5066	15259	76	1	0	17.2	284.2	80	0
A5066	15261	78	1	0	12.5	296.7	81	0
A5066	15263	80	1	0	10.8	307.5	82	0
A5066	15264	81	1	0	10.8	318.3	83	0
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A5066	15267	1	1	0	8.4	339.4	85	0
A5066	15269	3	1	0	10.5	349.9	86	0
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A5066	15292	3	1	0	1.2	419.1	93	1
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A5066	15299	3	1	0	12.1	432.1	95	1
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A5066	15315	4	1	0	10.2	453.3	97	0
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A5066	15320	9	1	0	11.2	487.2	100	0
A5066	15322	11	1	0	13	500.2	101	0
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A5066	15332	21	1	0	12.1	561	106	0
A5066	15334	23	1	0	9.1	570.1	107	0
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A5066	15340	29	1	0	8.8	609.8	111	0
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A5066	16015	13	1	0	9.7	742.8	125	1
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A5066	16193	32	0	0	4.9	860	158	0
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A5066	16210	2	0	0	8.4	879.4	163	0
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A5066	16323	2	0	0	2.7	954.4	179	0
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A5066	16332	6	0	1	11.1	973.1	182	0
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A5069	14247	1	0	0	2.6	2.6	1	1
A5069	14253	7	0	0	2.5	5.1	2	1
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A5069	14255	3	0	0	8.2	19	4	0
A5069	14258	6	0	0	6	25	6	0
A5069	14259	7	0	0	5.3	30.3	7	0
A5069	14259	7	0	0	2.8	33.1	8	1
A5069	14260	1	0	0	3.1	36.2	9	1
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A5069	14279	19	0	0	7	61.2	16	0
A5069	14281	21	0	0	8.2	69.4	19	0
A5069	14287	27	0	0	9	78.4	21	0
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A5069	14301	41	0	0	1.9	88.6	24	0
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A5069	14322	1	0	0	2.9	121.8	32	0

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A5069	14329	8	0	0	3.6	131.4	35	0
A5069	14329	8	0	0	2.5	133.9	36	1
A5069	14337	8	0	0	8.2	142.1	39	0
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A5069	14351	22	0	0	3.6	149.1	41	0
A5069	14351	23	0	0	2.2	151.3	42	0
A5069	14353	25	0	0	4.5	155.8	43	0
A5069	14356	28	0	0	2.9	158.7	44	1
A5069	14364	8	1	0	17.4	176.1	45	1
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A5069	15004	2	1	0	13.1	198.5	47	1
A5069	15007	3	1	0	12.1	210.6	48	0
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A5069	15011	7	1	0	14.5	240.1	50	1
A5069	15014	3	1	0	12.1	252.2	51	1
A5069	15015	1	1	0	12.8	265	52	0
A5069	15017	3	1	0	13.4	278.4	53	1
A5069	15018	1	1	0	12.6	291	54	1
A5069	15024	6	1	0	12.7	303.7	55	0
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A5069	15029	11	1	0	12.2	332.4	57	0
A5069	15031	13	1	0	13.1	345.5	58	0
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A5069	15039	2	1	0	9.1	385.1	62	0
A5069	15062	25	1	0	12.4	397.5	63	1
A5069	15066	5	1	0	11.6	409.1	64	0
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A5069	15083	4	1	0	12.2	515.4	73	0
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A5069	15086	7	1	0	12.7	539.4	75	1
A5069	15087	1	1	0	6	545.4	76	0
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A5069	15091	5	1	0	13.5	584.2	79	0
A5069	15092	6	1	0	12.2	596.4	80	0
A5069	15094	8	1	0	12.4	608.8	81	0
A5069	15095	9	1	0	12.2	621	82	0
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A5069	15106	20	1	0	13.4	695	88	0
A5069	15107	21	1	0	12.2	707.2	89	0
A5069	15109	23	1	0	12.6	719.8	90	0
A5069	15110	24	1	0	12.5	732.3	91	0
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A5069	15167	1	1	0	1	1016.5	116	1
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A5069	15234	4	0	1	1	1317	145	1

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A5069	15250	16	1	0	7.8	1342.9	148	0
A5069	15251	17	1	0	4.6	1347.5	149	0
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A5069	16168	2	0	0	4	1411.8	160	1
A5069	16195	27	0	0	2.9	1414.7	161	0
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A5069	16197	2	0	0	2.8	1420.2	163	0
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A5069	16239	29	0	0	5	1435.6	169	0
A5069	16244	34	0	0	3.2	1438.8	170	1
A5069	16252	8	0	0	1.6	1440.4	171	1
A5069	16266	14	0	0	8.7	1449.1	174	0
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A5069	16306	54	0	0	1.6	1456	176	1
A5072	14106	1	0	0	4.2	4.2	1	1
A5072	14133	28	0	0	6	10.2	2	1
A5072	14148	15	0	0	8.3	18.5	4	0
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A5072	14154	6	0	1	15.6	36.1	6	0
A5072	14157	9	1	0	6.5	42.6	7	1
A5072	14159	2	1	0	10.5	53.1	8	1
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A5072	14166	2	1	0	12.2	101	12	0
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A5072	14183	6	0	0	7.7	126.6	15	0
A5072	14189	12	0	0	4	130.6	16	0
A5072	14189	12	0	0	1.7	132.3	17	1
A5072	14203	14	0	0	6.7	139	19	0
A5072	14204	15	0	0	1.3	140.3	20	0
A5072	14211	22	0	0	8	148.3	22	0
A5072	14211	22	0	0	2.2	150.5	23	1
A5072	14230	19	0	0	1.7	152.2	24	1
A5072	14232	2	0	0	1.4	153.6	25	1
A5072	14252	20	0	0	2.1	155.7	26	0
A5072	14252	20	0	0	3	158.7	27	1
A5072	14281	29	0	0	3	161.7	28	1
A5072	14283	2	0	0	2.1	163.8	29	0
A5072	14283	2	0	0	2.3	166.1	30	1
A5072	14307	1	0	0	4.4	170.5	31	1
A5072	14310	3	0	0	4.7	175.2	32	0
A5072	14317	10	0	0	1.6	176.8	33	1
A5072	14324	7	0	0	5.3	182.1	34	1
A5072	14338	14	0	0	3	185.1	36	0
A5072	14338	14	0	0	2.9	188	37	1
A5072	15005	32	0	0	3.4	191.4	39	0
A5072	15007	34	0	0	2.1	193.5	40	1
A5072	15014	7	0	0	4.7	198.2	41	1
A5072	15016	2	0	0	5.6	203.8	42	1
A5072	15029	13	0	0	3	206.8	43	0
A5072	15054	38	0	0	7.3	214.1	45	0
A5072	15054	38	0	0	1.9	216	46	1
A5072	15065	12	0	0	3.4	219.4	47	1
A5072	15068	3	0	0	3.1	222.5	48	0
A5072	15069	4	0	0	3.1	225.6	49	1
A5072	15072	3	0	0	3.8	229.4	50	0
A5072	15091	22	0	0	4.8	234.2	51	1
A5072	15093	2	0	0	1.6	235.8	52	0
A5072	15097	6	0	1	16.4	252.2	53	0

A5072	15101	10	1	0	12.3	264.5	54	0
A5072	15104	13	1	0	13.2	277.7	55	0
A5072	15107	16	1	0	11.8	289.5	56	0
A5072	15108	17	1	0	13.1	302.6	57	0
A5072	15110	19	1	0	14.1	316.7	58	0
A5072	15112	21	1	0	11.5	328.8	59	0
A5072	15114	23	1	0	11.8	340	60	0
A5072	15116	25	1	0	12.2	352.2	61	1
A5072	15118	2	1	0	12.2	364.4	62	0
A5072	15119	3	1	0	12.6	377	63	0
A5072	15120	4	1	0	12	389	64	0
A5072	15121	5	1	0	12.9	401.9	65	1
A5072	15132	11	1	0	11.9	413.8	66	0
A5072	15136	15	1	0	12.1	425.9	67	0
A5072	15138	17	1	0	10.5	436.4	68	0
A5072	15139	18	1	0	10.1	446.5	69	0
A5072	15141	20	1	0	12	458.5	70	0
A5072	15143	22	1	0	12.8	471.3	71	0
A5072	15144	23	1	0	11.3	482.6	72	1
A5072	15146	2	1	0	11.2	493.8	73	1
A5072	15147	1	1	0	10.7	504.5	74	1
A5072	15156	9	1	0	12.2	516.7	75	0
A5072	15158	11	1	0	12.3	529	76	1
A5072	15159	1	1	0	1	530	77	1
A5072	15161	2	1	0	10.5	540.5	78	0
A5072	15162	3	1	0	11.9	552.4	79	1
A5072	15164	2	1	0	11.3	563.7	80	0
A5072	15165	3	1	0	12.4	576.1	81	0
A5072	15167	5	1	0	13.8	589.9	82	0
A5072	15168	6	1	0	12	601.9	83	0
A5072	15169	7	1	0	11.1	613	84	0
A5072	15171	8	1	0	10.9	623.9	85	0
A5072	15175	12	1	0	11.1	635	86	0
A5072	15184	21	1	0	12.1	647.1	87	0
A5072	15186	23	1	0	11.5	658.6	88	1
A5072	15193	7	1	0	11.3	669.9	89	0
A5072	15195	9	1	0	13.3	683.2	90	1

A5072	15199	4	1	0	1.2	684.4	91	1
A5072	15209	10	0	1	18.7	703.1	92	1
A5072	15227	18	0	0	2.4	705.5	93	1
A5072	15279	52	0	0	4.2	709.7	95	0
A5072	15281	54	0	0	6.9	716.6	97	0
A5072	15281	54	0	0	2.2	718.8	98	1
A5072	15289	8	0	0	3.1	721.9	99	0
A5072	15293	12	0	0	5	726.9	100	0
A5072	15294	13	0	0	4.8	731.7	101	0
A5072	15296	15	0	0	3.5	735.2	102	0
A5072	15307	26	0	0	2.7	737.9	103	0
A5072	15307	26	0	0	2.3	740.2	104	1
A5072	15309	2	0	0	7.3	747.5	106	0
A5072	15335	38	0	0	3.4	750.9	107	1
A5072	16020	51	0	0	4.4	755.3	108	0
A5072	16020	51	0	0	3.6	758.9	109	1
A5072	16032	12	0	0	10.2	769.1	111	0
A5072	16034	14	0	0	3.5	772.6	112	1
A5072	16048	14	0	0	8.3	780.9	115	0
A5072	16050	16	0	0	4.3	785.2	117	0
A5072	16056	22	0	0	5.4	790.6	118	0
A5072	16060	26	0	0	5.7	796.3	120	0
A5072	16098	64	0	0	6.1	802.4	121	0
A5072	16101	67	0	0	3.1	805.5	122	1
A5072	16101	0	0	0	3.2	808.7	123	1
A5072	16102	1	0	0	6.2	814.9	125	0
A5072	16103	2	0	0	3.6	818.5	126	0
A5072	16104	3	0	0	5.5	824	128	0
A5072	16105	4	0	0	2.2	826.2	129	0
A5072	16106	5	0	0	2.8	829	130	0
A5072	16108	7	0	0	6.1	835.1	132	0
A5072	16109	8	0	0	3.3	838.4	133	1
A5072	16109	1	0	0	2.7	841.1	134	0
A5072	16110	2	0	0	5	846.1	136	0
A5072	16111	3	0	0	2.9	849	137	1
A5072	16112	1	0	0	6.5	855.5	139	0
A5072	16113	2	0	0	3.5	859	140	0

A5072	16153	42	0	0	8.9	867.9	143	0
A5072	16155	44	0	0	5.2	873.1	145	0
A5072	16159	48	0	0	4	877.1	146	0
A5072	16159	48	0	0	1.8	878.9	147	1
A5072	16161	2	0	0	4.1	883	148	0
A5072	16161	2	0	0	2.9	885.9	149	1
A5072	16165	4	0	0	1.8	887.7	150	0
A5072	16167	6	0	0	9.9	897.6	153	0
A5072	16169	8	0	0	4.6	902.2	155	0
A5072	16180	19	0	0	2.9	905.1	156	0
A5072	16180	19	0	0	2.2	907.3	157	1
A5072	16187	7	0	0	7.1	914.4	160	0
A5072	16189	9	0	0	3.7	918.1	162	0
A5072	16194	14	0	0	2	920.1	163	0
A5072	16196	16	0	0	5.2	925.3	165	0
A5072	16201	21	0	0	2.9	928.2	166	0
A5072	16201	22	0	0	2.7	930.9	167	1
A5072	16231	30	0	0	4.2	935.1	168	1
A5079	13276	1	0	0	3.1	3.1	1	1
A5079	13295	20	0	1	2.4	5.5	2	1
A5079	13305	10	0	0	3.8	9.3	4	0
A5079	13309	14	0	0	3.4	12.7	5	1
A5079	13311	2	0	0	2.6	15.3	6	0
A5079	13311	2	0	0	5.1	20.4	7	1
A5079	13340	29	0	0	2.8	23.2	8	1
A5079	13350	10	0	0	4.3	27.5	9	0
A5079	13352	12	0	0	1.9	29.4	10	1
A5079	14008	21	0	0	1.7	31.1	11	0
A5079	14013	26	0	0	6.3	37.4	13	0
A5079	14013	26	0	0	3.1	40.5	14	1
A5079	14050	37	0	0	7.2	47.7	15	0
A5079	14050	37	0	0	1.7	49.4	16	1
A5079	14052	2	0	0	2.2	51.6	17	1
A5079	14056	4	0	0	4	55.6	18	0
A5079	14056	4	0	0	3.6	59.2	19	1
A5079	14059	3	0	0	4.5	63.7	21	0
A5079	14076	20	0	0	2.6	66.3	22	0

A5079	14076	20	0	0	1.7	68	23	1
A5079	14078	2	0	0	5.7	73.7	25	0
A5079	14079	3	0	0	5.8	79.5	26	0
A5079	14079	3	0	0	2.7	82.2	27	1
A5079	14083	4	0	0	7	89.2	30	0
A5079	14085	6	0	0	3.9	93.1	31	1
A5079	14094	9	0	0	1.9	95	32	1
A5079	14099	6	0	0	3.5	98.5	33	1
A5079	14101	2	0	0	4.1	102.6	34	0
A5079	14104	5	0	0	7.7	110.3	36	0
A5079	14106	7	0	0	3.9	114.2	37	1
A5079	14106	0	0	0	2	116.2	38	1
A5079	14108	2	0	0	3.6	119.8	39	0
A5079	14112	6	0	0	8.3	128.1	41	0
A5079	14114	8	0	0	9.1	137.2	43	0
A5079	14118	12	0	0	4.1	141.3	44	0
A5079	14120	14	0	0	8.4	149.7	46	0
A5079	14170	64	0	0	11.1	160.8	48	0
A5079	14176	70	0	0	6.4	167.2	50	0
A5079	14178	72	0	0	3.6	170.8	52	0
A5079	14196	80	0	0	6	176.8	54	0
A5079	14197	81	0	0	7.3	184.1	56	0
A5079	14198	82	0	0	7.9	192	58	0
A5079	14251	145	0	0	1.7	193.7	59	1
A5079	14253	2	0	0	7.3	201	60	1
A5079	14266	13	0	0	3.8	204.8	61	1
A5079	14268	2	0	0	3.1	207.9	62	0
A5079	14275	9	0	0	9.8	217.7	64	0
A5079	14288	22	0	0	8.3	226	66	0
A5079	14290	24	0	0	5.4	231.4	67	0
A5079	14301	35	1	0	16.6	248	68	0
A5079	14303	37	1	0	12.8	260.8	69	1
A5079	14307	4	1	0	14.4	275.2	70	0
A5079	14308	5	1	0	11.2	286.4	71	1
A5079	14310	2	1	0	11.2	297.6	72	0
A5079	14312	4	1	0	12.6	310.2	73	0
A5079	14313	5	1	0	13.3	323.5	74	0

A5079	14314	6	1	0	11.6	335.1	75	1
A5079	14316	2	1	0	13.6	348.7	76	1
A5079	14320	4	1	0	11.8	360.5	77	0
A5079	14321	5	1	0	6.2	366.7	78	0
A5079	14323	7	1	0	12.3	379	79	0
A5079	14324	8	1	0	11.9	390.9	80	0
A5079	14326	10	1	0	9.8	400.7	81	0
A5079	14327	11	1	0	13.7	414.4	82	0
A5079	14328	12	1	0	13.5	427.9	83	1
A5079	14331	3	1	0	11.4	439.3	84	0
A5079	14332	4	1	0	11.7	451	85	0
A5079	14334	6	1	0	12.7	463.7	86	1
A5079	14335	1	1	0	11.4	475.1	87	1
A5079	14336	1	1	0	11.7	486.8	88	1
A5079	14338	2	1	0	12.4	499.2	89	1
A5079	14346	8	1	0	16.6	515.8	90	1
A5079	14348	2	1	0	13.1	528.9	91	0
A5079	14350	4	1	0	4.9	533.8	92	1
A5079	14352	2	1	0	1.8	535.6	93	1
A5079	14354	2	1	0	12.6	548.2	94	0
A5079	14355	3	1	0	13	561.2	95	0
A5079	14356	4	1	0	12.3	573.5	96	0
A5079	14357	5	1	0	12	585.5	97	0
A5079	14358	6	1	0	13.1	598.6	98	0
A5079	14360	8	1	0	11.7	610.3	99	1
A5079	14361	1	1	0	12.9	623.2	100	0
A5079	14363	3	1	0	8.8	632	101	1
A5079	15003	5	1	0	13.9	645.9	102	1
A5079	15004	1	1	0	11.3	657.2	103	0
A5079	15005	2	1	0	9.3	666.5	104	0
A5079	15008	5	1	0	12.3	678.8	105	1
A5079	15013	5	1	0	13	691.8	106	0
A5079	15014	6	1	0	12.4	704.2	107	1
A5079	15020	6	1	0	11.9	716.1	108	0
A5079	15021	7	1	0	12.2	728.3	109	0
A5079	15023	9	1	0	13	741.3	110	1
A5079	15025	2	1	0	11.3	752.6	111	1

A5079	15025	0	1	0	12.8	765.4	112	1
A5079	15029	4	1	0	12.8	778.2	113	0
A5079	15030	5	1	0	12.8	791	114	0
A5079	15031	6	1	0	11	802	115	0
A5079	15042	17	1	0	11.7	813.7	116	0
A5079	15044	19	1	0	11.6	825.3	117	0
A5079	15045	20	1	0	11.8	837.1	118	1
A5079	15048	3	1	0	12.8	849.9	119	0
A5079	15050	5	1	0	9.7	859.6	120	1
A5079	15051	1	1	0	1.5	861.1	121	1
A5079	15052	1	1	0	11.2	872.3	122	0
A5079	15053	2	1	0	10.8	883.1	123	1
A5079	15055	2	1	0	12.4	895.5	124	0
A5079	15060	7	1	0	13.9	909.4	125	0
A5079	15063	10	1	0	12.5	921.9	126	0
A5079	15065	12	1	0	11	932.9	127	1
A5079	15074	9	1	0	1.2	934.1	128	1
A5079	15075	1	1	0	12.3	946.4	129	0
A5079	15077	3	1	0	13.2	959.6	130	0
A5079	15078	4	1	0	14.3	973.9	131	0
A5079	15080	6	1	0	11.1	985	132	0
A5079	15082	8	1	0	12.9	997.9	133	1
A5079	15083	1	1	0	9	1006.9	134	0
A5079	15085	3	1	0	11.7	1018.6	135	0
A5079	15086	4	1	0	11.5	1030.1	136	0
A5079	15087	5	1	0	12.1	1042.2	137	0
A5079	15088	6	1	0	12.7	1054.9	138	1
A5079	15089	1	1	0	12.9	1067.8	139	0
A5079	15091	3	1	0	11.7	1079.5	140	1
A5079	15092	1	1	0	1.2	1080.7	141	1
A5079	15109	17	0	1	18.7	1099.4	142	1
A5079	15224	15	0	0	3.5	1102.9	144	0
A5079	15227	17	0	0	4	1106.9	145	1
A5079	15239	12	0	0	10.1	1117	147	0
A5079	15243	16	0	0	9.4	1126.4	149	0
A5079	15245	18	0	0	9.8	1136.2	151	0
A5079	15252	85	0	0	8.5	1144.7	153	0

A5079	15254	87	0	0	3.9	1148.6	154	1
A5079	15268	14	0	0	3.1	1151.7	155	1
A5079	15280	12	0	0	4.1	1155.8	156	0
A5079	15280	12	0	0	3.5	1159.3	157	1
A5079	15287	7	0	0	5.3	1164.6	158	1
A5079	15293	6	0	0	4.8	1169.4	159	0
A5079	15299	12	0	0	9.1	1178.5	161	0
A5079	15301	14	0	0	9.2	1187.7	163	0
A5079	15306	19	0	0	8.3	1196	166	0
A5079	15310	23	0	0	3.1	1199.1	167	0
A5079	15310	23	0	0	2.1	1201.2	168	1
A5079	15345	35	0	0	2.9	1204.1	169	0
A5079	15355	45	0	0	3.8	1207.9	170	0
A5079	15355	45	0	0	3.9	1211.8	171	1
A5079	16005	15	0	0	6.9	1218.7	173	0
A5079	16019	29	0	0	3.5	1222.2	174	1
A5079	16021	2	0	0	2.2	1224.4	175	0
A5079	16021	3	0	0	2.8	1227.2	176	1
A5079	16029	8	0	0	2.2	1229.4	177	1
A5079	16035	6	0	0	8.5	1237.9	179	0
A5079	16047	18	0	0	1.6	1239.5	180	0
A5079	16049	20	0	0	5.3	1244.8	182	0
A5079	16056	27	0	0	4	1248.8	183	0
A5079	16113	84	0	0	2.7	1251.5	184	1
A5079	16118	5	0	0	0.5	1252	185	1
A5081	13281	1	0	0	3.6	3.6	1	0
A5081	13283	3	0	0	2.8	6.4	2	0
A5081	13288	8	0	0	3.2	9.6	3	0
A5081	13290	10	0	0	3.1	12.7	4	0
A5081	13290	10	0	0	3.3	16	5	1
A5081	13317	27	0	0	3.8	19.8	6	0
A5081	13317	27	0	0	3.5	23.3	7	1
A5081	13322	5	0	0	3	26.3	8	0
A5081	13324	7	0	0	6.6	32.9	10	0
A5081	13326	9	0	0	4	36.9	12	0
A5081	13336	19	0	0	4.7	41.6	14	0
A5081	13350	33	0	0	7.9	49.5	17	0

A5081	13352	35	0	0	3.9	53.4	18	1
A5081	14009	22	0	0	2.3	55.7	19	1
A5081	14035	26	0	0	7.9	63.6	20	0
A5081	14042	33	0	0	6.1	69.7	21	0
A5081	14044	35	0	0	7.8	77.5	23	0
A5081	14049	40	0	0	8.7	86.2	24	1
A5081	14052	3	0	0	2.4	88.6	25	0
A5081	14055	6	0	0	3.9	92.5	26	1
A5081	14057	2	0	0	4	96.5	27	1
A5081	14071	14	0	0	9.7	106.2	29	0
A5081	14076	19	0	0	4.7	110.9	30	1
A5081	14078	2	0	0	9.8	120.7	32	0
A5081	14080	4	0	0	4.5	125.2	33	0
A5081	14084	8	0	0	10.8	136	36	0
A5081	14086	10	0	0	10	146	38	0
A5081	14091	15	0	0	3	149	39	0
A5081	14091	15	0	0	2.7	151.7	40	1
A5081	14104	3	0	0	4.2	155.9	41	1
A5081	14106	2	0	0	4.1	160	42	1
A5081	14189	83	0	0	9	169	44	0
A5081	14192	86	0	0	4.8	173.8	45	0
A5081	14196	90	0	0	2.7	176.5	46	1
A5081	14196	0	0	0	1.2	177.7	47	1
A5081	14205	9	0	0	4.9	182.6	49	0
A5081	14206	10	0	0	4.5	187.1	51	0
A5081	14217	21	0	0	8	195.1	53	0
A5081	14219	23	0	0	5.4	200.5	54	1
A5081	14226	7	0	0	6.4	206.9	56	0
A5081	14228	9	0	0	3.4	210.3	57	0
A5081	14231	12	0	0	4.9	215.2	59	0
A5081	14231	12	0	0	2.3	217.5	60	1
A5081	15065	200	0	0	0.5	218	61	1
A5081	15071	6	0	0	4	222	62	0
A5081	15089	24	0	0	4.3	226.3	63	0
A5081	15090	25	0	0	2.7	229	64	0
A5081	15092	27	0	0	5.1	234.1	65	1
A5081	15097	5	0	1	16.4	250.5	66	1

A5081	15101	4	1	0	1.4	251.9	67	1
A5081	15103	2	1	0	13	264.9	68	0
A5081	15105	4	1	0	12.7	277.6	69	1
A5081	15109	4	1	0	12.5	290.1	70	0
A5081	15113	8	1	0	12	302.1	71	0
A5081	15115	10	1	0	13.2	315.3	72	0
A5081	15117	12	1	0	12.1	327.4	73	1
A5081	15119	2	1	0	11.9	339.3	74	1
A5081	15121	2	1	0	11.6	350.9	75	0
A5081	15122	3	1	0	11.2	362.1	76	0
A5081	15124	5	1	0	12.5	374.6	77	0
A5081	15125	6	1	0	11.8	386.4	78	0
A5081	15126	7	1	0	11.2	397.6	79	0
A5081	15127	8	1	0	11.5	409.1	80	1
A5081	15129	2	1	0	1.1	410.2	81	1
A5081	15130	1	1	0	10.9	421.1	82	0
A5081	15131	2	1	0	13.1	434.2	83	0
A5081	15133	4	1	0	11.2	445.4	84	0
A5081	15134	5	1	0	12.5	457.9	85	0
A5081	15136	7	1	0	11.9	469.8	86	0
A5081	15137	8	1	0	12.1	481.9	87	1
A5081	15139	2	1	0	12.7	494.6	88	0
A5081	15140	3	1	0	3.4	498	89	1
A5081	15142	2	1	0	13.4	511.4	90	1
A5081	15143	1	1	0	13	524.4	91	0
A5081	15144	2	1	0	10.2	534.6	92	1
A5081	15146	2	1	0	6.7	541.3	93	1
A5081	15147	1	1	0	12.3	553.6	94	0
A5081	15149	3	1	0	11.2	564.8	95	0
A5081	15150	4	1	0	13.1	577.9	96	0
A5081	15151	5	1	0	12.3	590.2	97	0
A5081	15152	6	1	0	10.8	601	98	1
A5081	15161	9	1	0	11.6	612.6	99	0
A5081	15163	11	1	0	13	625.6	100	0
A5081	15165	13	1	0	9.2	634.8	101	1
A5081	15187	22	1	0	12	646.8	102	1
A5081	15190	3	1	0	11.9	658.7	103	1

A5081	15194	4	1	0	12.8	671.5	104	0
A5081	15196	6	1	0	11.1	682.6	105	0
A5081	15198	8	1	0	14.3	696.9	106	0
A5081	15201	11	1	0	11.8	708.7	107	0
A5081	15203	13	1	0	13.8	722.5	108	0
A5081	15204	14	1	0	13.1	735.6	109	1
A5081	15206	2	1	0	12.4	748	110	0
A5081	15209	5	0	1	18.7	766.7	111	1
A5081	15231	22	0	0	3	769.7	112	0
A5081	15244	35	0	0	1.9	771.6	113	1
A5081	15253	9	0	0	5.2	776.8	114	0
A5081	15253	9	0	0	5.1	781.9	115	1
A5081	15323	70	0	0	1.5	783.4	116	1
A5081	15327	4	0	0	3.7	787.1	117	1
A5081	15329	2	0	0	2.7	789.8	118	0
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A5081	15336	9	0	0	4	799.3	121	0
A5081	15341	14	0	0	4.3	803.6	122	1
A5081	15345	4	0	0	5.3	808.9	124	0
A5081	15351	10	0	0	3.2	812.1	125	1
A5081	15351	0	0	0	1	813.1	126	0
A5081	15355	4	0	0	3.6	816.7	127	0
A5081	15356	5	0	0	3.7	820.4	128	1
A5081	16019	28	0	0	3.6	824	129	0
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A5081	16026	35	0	0	6.5	833.6	131	1
A5081	16028	2	0	0	9	842.6	133	0
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A5081	16036	10	0	0	2.9	851.5	135	0
A5081	16040	14	0	0	8.3	859.8	137	0
A5081	16042	16	0	0	6.2	866	139	0
A5081	16047	21	0	0	6.2	872.2	141	0
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A5081	16049	23	0	0	3.1	878.4	143	1
A5083	13354	1	0	0	1.8	1.8	1	0
A5083	14016	28	0	0	4.6	6.4	3	0
A5083	14021	33	0	0	2.9	9.3	4	1

A5083	14023	2	0	0	4.2	13.5	5	1
A5083	14028	5	0	0	4.7	18.2	6	0
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A5083	14042	14	0	0	8.3	29.9	8	0
A5083	14044	16	0	0	3.2	33.1	9	1
A5083	14049	5	0	0	8.6	41.7	10	0
A5083	14051	7	0	0	8.2	49.9	11	1
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A5083	14055	4	0	0	2.7	54.6	13	1
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A5083	14063	6	0	0	1.7	62.7	16	1
A5083	14065	2	0	0	4	66.7	17	0
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A5083	14069	4	0	0	8.9	78.5	21	0
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A5083	14072	2	0	0	10.8	94.3	25	0
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A5083	14079	9	1	0	12.8	123.8	27	0
A5083	14080	10	1	0	12.6	136.4	28	0
A5083	14081	11	1	0	12.2	148.6	29	0
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A5083	14084	1	1	0	11.6	162.2	31	0
A5083	14086	3	1	0	12.8	175	32	1
A5083	14087	1	1	0	13.7	188.7	33	0
A5083	14090	4	1	0	12.9	201.6	34	0
A5083	14091	5	1	0	11.7	213.3	35	0
A5083	14092	6	1	0	12.2	225.5	36	0
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A5083	14101	15	1	0	11.8	293.9	42	0
A5083	14102	16	1	0	11.9	305.8	43	0
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A5083	14105	19	1	0	12.8	342.6	46	0
A5083	14106	20	1	0	12	354.6	47	0
A5083	14107	21	1	0	12.4	367	48	1
A5083	14109	2	1	0	12	379	49	0
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A5083	14111	4	1	0	12.2	403.9	51	0
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A5083	14115	2	1	0	12.5	429.4	53	1
A5083	14116	1	1	0	12.1	441.5	54	0
A5083	14118	3	1	0	11.8	453.3	55	0
A5083	14119	4	1	0	10.5	463.8	56	0
A5083	14120	5	1	0	12.4	476.2	57	1
A5083	14121	1	1	0	12.5	488.7	58	0
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A5083	14125	5	1	0	9.3	522.9	61	0
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A5083	14135	9	1	0	12.4	568.4	65	0
A5083	14136	10	1	0	13	581.4	66	0
A5083	14138	12	1	0	12.3	593.7	67	0
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A5083	14145	2	1	0	13.4	645.4	71	1
A5083	14146	1	1	0	12.2	657.6	72	0
A5083	14147	2	1	0	13.3	670.9	73	0
A5083	14149	4	1	0	12	682.9	74	0
A5083	14150	5	1	0	8.8	691.7	75	1
A5083	14152	2	1	0	11.6	703.3	76	0
A5083	14153	3	1	0	13.4	716.7	77	0
A5083	14155	5	1	0	12.1	728.8	78	0
A5083	14158	8	1	0	12.7	741.5	79	0
A5083	14162	13	1	0	12.3	753.8	80	0
A5083	14163	14	1	0	12.7	766.5	81	0
A5083	14165	16	1	0	12.7	779.2	82	0

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A5083	14167	18	1	0	12.3	803.6	84	0
A5083	14168	19	1	0	12.9	816.5	85	1
A5083	14169	1	1	0	14.1	830.6	86	0
A5083	14170	2	1	0	13.4	844	87	0
A5083	14171	3	1	0	12.7	856.7	88	1
A5083	14173	2	1	0	11.9	868.6	89	0
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A5083	14181	10	1	0	11.9	892.1	91	0
A5083	14182	11	1	0	15.1	907.2	92	0
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A5083	14191	5	1	0	11.8	941.4	95	0
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A5083	14198	12	1	0	12.3	1002.7	100	0
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A5083	14201	15	1	0	12	1026.3	102	0
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A5083	14302	22	0	0	9.5	1064.8	109	0
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A5083	14308	28	0	0	4.7	1073.6	112	0
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A5083	16098	79	0	0	2.1	2007.7	251	1
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A5083	16127	2	0	0	4.8	2026.6	258	0
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A5083	16145	4	0	0	5.8	2054.2	266	0
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A5083	16207	62	0	0	3.6	2060	268	1
A5083	16209	2	0	0	2.2	2062.2	269	0
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A5083	16239	2	0	0	2.5	2097.2	280	1
A5083	16244	5	0	0	2.1	2099.3	281	1
A5083	16258	14	0	0	2	2101.3	282	1
A5083	16270	12	0	0	3.3	2104.6	283	1
A5084	13282	1	0	0	1.6	1.6	1	0
A5084	13302	21	0	0	2	3.6	2	1
A5084	13304	2	0	0	4.5	8.1	3	0
A5084	13311	9	0	0	8.5	16.6	6	1
A5084	13317	6	0	0	4.3	20.9	7	1
A5084	13326	9	0	0	4	24.9	8	0
A5084	13352	36	0	0	7.2	32.1	10	0
A5084	14008	57	0	0	4	36.1	11	1
A5084	14045	37	0	0	5.9	42	12	0
A5084	14050	42	0	0	7.8	49.8	13	1
A5084	14052	2	0	0	1.2	51	14	1
A5084	14058	6	0	0	6.9	57.9	16	0
A5084	14062	10	0	0	6.7	64.6	18	1
A5084	14064	2	0	0	7	71.6	21	0
A5084	14066	4	0	0	1.5	73.1	22	1
A5084	14071	5	0	0	12.1	85.2	25	0
A5084	14072	6	0	0	11.9	97.1	28	1
A5084	14087	15	0	0	3.6	100.7	29	1

A5084	14091	4	0	0	3	103.7	30	0
A5084	14093	6	0	0	6	109.7	31	1
A5084	14097	4	0	0	7.6	117.3	33	1
A5084	14099	2	0	0	4.2	121.5	34	0
A5084	14101	4	0	0	3.6	125.1	35	1
A5084	14104	3	0	0	7.3	132.4	37	0
A5084	14134	33	0	0	7	139.4	39	0
A5084	14136	35	0	0	3.9	143.3	41	0
A5084	14167	66	0	0	9.7	153	44	1
A5084	14183	16	0	1	16.2	169.2	45	0
A5084	14187	20	1	0	11.6	180.8	46	1
A5084	14189	2	1	0	13.2	194	47	1
A5084	14191	2	1	0	11.9	205.9	48	0
A5084	14193	4	1	0	11.1	217	49	0
A5084	14194	5	1	0	11.6	228.6	50	1
A5084	14202	8	1	0	5.1	233.7	51	1
A5084	14203	1	1	0	12.9	246.6	52	0
A5084	14204	2	1	0	12	258.6	53	0
A5084	14206	4	1	0	10.8	269.4	54	0
A5084	14207	5	1	0	11.7	281.1	55	1
A5084	14208	1	1	0	9.7	290.8	56	1
A5084	14217	9	1	0	11.3	302.1	57	0
A5084	14218	10	1	0	5.2	307.3	58	1
A5084	14220	2	1	0	11.6	318.9	59	0
A5084	14221	3	1	0	13.1	332	60	0
A5084	14222	4	1	0	13	345	61	0
A5084	14225	7	1	0	11.9	356.9	62	1
A5084	14228	3	1	0	12.9	369.8	63	1
A5084	14229	1	1	0	12.6	382.4	64	1
A5084	14230	1	1	0	12.7	395.1	65	1
A5084	14231	1	1	0	12.8	407.9	66	0
A5084	14232	2	1	0	12.4	420.3	67	0
A5084	14233	3	1	0	12.1	432.4	68	0
A5084	14234	4	1	0	13	445.4	69	1
A5084	14245	11	1	0	11.8	457.2	70	1
A5084	14247	2	1	0	12.7	469.9	71	1
A5084	14248	1	1	0	12.3	482.2	72	0

A5084	14250	3	1	0	12.5	494.7	73	0
A5084	14251	4	1	0	12.7	507.4	74	1
A5084	14258	7	1	0	12.2	519.6	75	1
A5084	14260	2	1	0	12.5	532.1	76	1
A5084	14266	6	1	0	11.7	543.8	77	0
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A5084	14268	8	1	0	12.1	567.2	79	1
A5084	14269	1	1	0	12.5	579.7	80	0
A5084	14270	2	1	0	11.7	591.4	81	1
A5084	14271	1	1	0	13.6	605	82	1
A5084	14272	1	1	0	12.1	617.1	83	1
A5084	14274	2	1	0	1.2	618.3	84	1
A5084	14275	1	1	0	10	628.3	85	1
A5084	14276	1	1	0	12.2	640.5	86	1
A5084	14277	1	1	0	12.7	653.2	87	0
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A5084	14281	5	1	0	14	678.7	89	1
A5084	14282	1	1	0	13.3	692	90	0
A5084	14283	2	1	0	12.3	704.3	91	0
A5084	14285	4	1	0	12.8	717.1	92	0
A5084	14286	5	1	0	13.1	730.2	93	1
A5084	14289	3	1	0	13.5	743.7	94	0
A5084	14297	11	1	0	12.7	756.4	95	1
A5084	14302	5	1	0	13	769.4	96	1
A5084	14307	5	1	0	13.1	782.5	97	0
A5084	14310	8	0	1	17.6	800.1	98	1
A5084	15051	107	0	0	1.3	801.4	99	1
A5084	15140	89	0	0	3.5	804.9	100	0
A5084	15146	95	0	0	5.6	810.5	101	1
A5084	15160	14	0	0	9.6	820.1	104	0
A5084	15161	15	0	0	1.9	822	105	0
A5084	15162	16	0	0	4.3	826.3	106	0
A5084	15162	16	0	0	3.8	830.1	107	1
A5084	15169	6	0	0	6.3	836.4	109	0
A5084	16225	428	0	0	1.8	838.2	110	1
A5084	16232	7	0	0	4.5	842.7	112	0
A5084	16236	12	0	0	6.8	849.5	114	0

A5084	16243	19	0	0	7.1	856.6	116	0
A5084	16251	27	0	0	2.9	859.5	117	0
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A5084	16253	2	0	0	2.8	864.8	119	1
A5084	16263	10	0	0	6.1	870.9	122	0
A5084	16265	12	0	0	4.3	875.2	124	0
A5084	16267	14	0	0	1.9	877.1	125	0
A5084	16267	14	0	0	1.6	878.7	126	1
A5084	16312	45	0	0	10	888.7	129	0
A5084	16314	47	0	0	4.8	893.5	131	0
A5084	16322	55	0	0	2.4	895.9	132	1
A5084	16326	4	0	0	6.1	902	134	0
A5084	16326	4	0	0	2.2	904.2	135	1
A5084	16333	7	0	0	3	907.2	136	0
A5084	16335	9	0	0	5	912.2	137	1
A5085	14157	1	0	1	1.4	1.4	1	1
A5085	14168	12	0	0	6.3	7.7	3	0
A5085	14168	12	0	0	4.4	12.1	4	1
A5085	14183	15	0	0	2.4	14.5	5	0
A5085	14183	15	0	0	3.2	17.7	6	1
A5085	15132	215	0	0	7.1	24.8	8	0
A5085	15134	217	0	0	4.6	29.4	9	1
A5085	15138	4	0	0	3.1	32.5	10	0
A5085	15138	4	0	0	1.7	34.2	11	1
A5085	15148	10	0	0	2.2	36.4	12	1
A5085	15159	10	0	0	3.2	39.6	13	0
A5085	15159	10	0	0	2.6	42.2	14	1
A5085	15159	0	0	0	1.2	43.4	15	1
A5085	15161	2	0	0	2.3	45.7	16	0
A5085	15161	2	0	0	2.5	48.2	17	1
A5085	15168	7	0	0	2.8	51	18	1
A5085	15238	70	0	0	7.8	58.8	20	0
A5085	15240	72	0	0	2.7	61.5	21	0
A5085	15251	83	0	0	2.3	63.8	22	1
A5085	15267	16	0	0	1.6	65.4	23	0
A5085	16134	249	0	0	2	67.4	24	0
A5085	16179	281	0	0	10.1	77.5	27	0

A5085	16181	283	0	0	2.9	80.4	28	0
A5085	16187	289	0	0	5.5	85.9	30	0
A5085	16189	291	0	0	2.9	88.8	31	1
A5085	16193	4	0	0	1.6	90.4	32	0
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A5085	16195	2	0	0	4.3	97.5	35	0
A5085	16200	7	0	0	2.4	99.9	36	1
A5085	16202	2	0	0	4	103.9	38	0
A5085	16204	4	0	0	6.1	110	40	0
A5085	16207	7	0	0	2.9	112.9	41	0
A5085	16207	7	0	0	2.4	115.3	42	1
A5085	16218	11	0	0	15.8	131.1	43	0
A5085	16227	20	0	0	3.4	134.5	44	0
A5085	16229	22	0	0	4	138.5	45	0
A5085	16231	24	0	0	3	141.5	46	0
A5085	16235	28	0	0	3.5	145	47	0
A5085	16236	29	0	0	2.1	147.1	48	0
A5085	16237	30	0	0	6.9	154	50	0
A5085	16241	34	0	0	7.8	161.8	51	0
A5085	16242	35	0	0	6.6	168.4	53	0
A5085	16243	36	0	0	3.2	171.6	54	0
A5085	16244	37	0	0	3.5	175.1	55	0
A5085	16249	42	0	0	2.7	177.8	56	0
A5085	16252	45	0	0	3.5	181.3	57	1
A5085	16256	4	0	1	10.1	191.4	58	0
A5085	16257	5	0	0	3.6	195	59	0
A5085	16257	5	0	0	1.7	196.7	60	1
A5085	16258	1	0	0	7.8	204.5	62	0
A5085	16261	4	0	0	3.4	207.9	63	0
A5085	16261	4	0	0	3	210.9	64	1
A5085	16269	8	0	0	3.5	214.4	65	1
A5085	16271	2	0	1	8.9	223.3	66	0
A5085	16275	6	0	0	9.9	233.2	67	1
A5085	16314	39	0	1	7.5	233.2	67	0
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A5085	16322	2	0	0	6.9	258.6	71	0
A5085	16326	6	0	0	4.5	263.1	72	0

A5085	16326	6	0	0	3.6	266.7	73	1
A5085	16332	6	0	1	11.1	277.8	74	1
A5087	13289	1	0	1	2.9	2.9	1	0
A5087	13294	6	0	0	5.9	8.8	3	0
A5087	13298	10	0	0	1.8	10.6	4	1
A5087	13329	31	0	0	8.4	19	7	0
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A5087	13346	15	0	0	5.3	28.5	9	0
A5087	13350	19	0	0	6.7	35.2	11	0
A5087	13352	21	0	0	3.7	38.9	12	1
A5087	13354	2	0	0	1.9	40.8	13	0
A5087	14003	16	0	0	4	44.8	15	1
A5087	14080	77	0	0	4.4	49.2	16	0
A5087	14098	95	0	0	2.6	51.8	17	1
A5087	14100	2	0	0	7.2	59	19	0
A5087	14105	7	0	0	6	65	20	1
A6093	14164	1	0	0	1.3	1.3	1	1
A6093	14167	4	0	0	4.2	5.5	2	1
A6093	14169	2	0	0	3.5	9	3	0
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A6093	14175	6	0	0	7.7	20.6	6	0
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A6093	14181	12	0	0	1.4	25	8	0
A6093	14189	20	0	0	3.9	28.9	9	1
A6093	14192	3	0	0	4.4	33.3	10	0
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A6093	14202	13	0	0	3.2	46.4	15	0
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A6093	14204	2	0	0	1.4	50.9	17	1
A6093	14205	1	0	0	4.9	55.8	19	0
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A6093	14216	12	0	0	3.3	62.2	21	1
A6093	14218	2	0	0	13	75.2	23	0
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A6093	14220	4	0	0	4.2	81.6	26	0
A6093	14233	17	0	0	4.3	85.9	27	1

A6093	14238	5	0	0	6.1	92	28	1
A6093	14239	1	0	0	9.3	101.3	31	0
A6093	14246	8	0	0	2	103.3	32	0
A6093	14248	10	0	0	1.6	104.9	33	1
A6093	14248	0	0	0	5.2	110.1	35	0
A6093	14252	4	0	0	9.4	119.5	38	0
A6093	14254	6	0	0	9.3	128.8	41	0
A6093	14258	10	0	0	3.9	132.7	42	0
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A6093	14262	14	0	0	5.3	147.4	47	0
A6093	14265	17	0	0	7.5	154.9	50	0
A6093	14267	19	0	0	2.6	157.5	51	1
A6093	14282	15	0	0	4.4	161.9	52	1
A6093	14287	5	0	0	3.4	165.3	53	1
A6093	14301	14	0	1	7	172.3	54	0
A6093	14303	16	0	0	6.2	178.5	55	0
A6093	14307	20	0	0	4.3	182.8	56	1
A6093	14311	4	0	0	3.9	186.7	58	0
A6093	14316	9	0	0	7.4	194.1	60	0
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A6093	15007	65	0	0	3	224.1	70	1
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A6093	15041	19	1	0	13.3	313	86	0
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A6093	15049	27	1	0	11.7	362.8	90	0
A6093	15050	28	1	0	12.4	375.2	91	0
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A6093	15064	2	1	0	14.1	437.6	96	0
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A6093	15111	5	1	0	12.5	641.8	113	0
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A6093	15151	33	1	0	12.2	762.9	123	0
A6093	15152	34	1	0	11.2	774.1	124	0
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A6093	15155	37	1	0	11.2	796.7	126	0

A6093	15157	39	1	0	12.5	809.2	127	1
A6093	15159	2	1	0	9.7	818.9	128	1
A6093	15162	3	1	0	11	829.9	129	0
A6093	15163	4	1	0	11.7	841.6	130	0
A6093	15165	6	1	0	13.2	854.8	131	0
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A6093	15172	13	1	0	9.6	910	136	0
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A6093	15186	27	1	0	11.4	954.7	140	0
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A6093	15191	4	1	0	9.7	976	142	0
A6093	15193	6	1	0	12.9	988.9	143	0
A6093	15198	11	0	0	17.3	1006.2	144	1
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A6093	16026	50	0	0	6.4	1043.7	156	0
A6093	16026	50	0	0	5	1048.7	157	1
A6093	16028	2	0	0	3.1	1051.8	158	1
A6093	16098	70	0	0	3.5	1055.3	159	1
A6093	16103	5	0	0	3.3	1058.6	160	0
A6093	16103	5	0	0	3.7	1062.3	161	1
A6093	16104	1	0	0	6.2	1068.5	163	0
A6093	16105	2	0	0	2.9	1071.4	164	1
A6093	16113	8	0	0	2.2	1073.6	165	1
A6093	16158	45	0	0	3.8	1077.4	166	1
A6093	16160	2	0	0	6	1083.4	168	0
A6093	16160	2	0	0	3.9	1087.3	169	1

A6093	16179	19	0	0	4	1091.3	170	0
A6093	16181	21	0	0	8.3	1099.6	172	0
A6093	16201	41	0	0	3.5	1103.1	173	1
A6094	13280	1	0	0	5.3	5.3	2	0
A6094	13282	3	0	0	6.1	11.4	4	0
A6094	13283	4	0	0	3	14.4	5	0
A6094	13289	10	0	0	8	22.4	7	0
A6094	13294	15	0	0	6.1	28.5	9	0
A6094	13296	17	0	0	7.2	35.7	11	0
A6094	13298	19	0	0	2.7	38.4	12	1
A6094	13302	4	0	0	2.8	41.2	13	0
A6094	13304	6	0	0	2.4	43.6	14	0
A6094	13309	11	0	0	2.4	46	15	0
A6094	13311	13	0	0	3.4	49.4	16	0
A6094	13311	14	0	0	2.5	51.9	17	1
A6094	13340	29	0	0	2.1	54	18	1
A6094	13344	4	0	0	2.6	56.6	19	1
A6094	13346	2	0	0	5.6	62.2	21	0
A6094	13350	6	0	0	5.8	68	23	0
A6094	13352	8	0	0	3.5	71.5	24	1
A6094	13354	2	0	0	3.5	75	26	0
A6094	14007	20	1	0	16.4	91.4	27	1
A6094	14010	3	1	0	11.7	103.1	28	0
A6094	14012	5	1	0	12.8	115.9	29	0
A6094	14014	7	1	0	12	127.9	30	0
A6094	14016	9	1	0	11.8	139.7	31	0
A6094	14018	11	1	0	14.3	154	32	0
A6094	14020	13	1	0	11.9	165.9	33	0
A6094	14021	14	1	0	11.9	177.8	34	0
A6094	14022	15	1	0	12.7	190.5	35	0
A6094	14023	16	1	0	12.8	203.3	36	0
A6094	14025	18	1	0	12	215.3	37	0
A6094	14026	19	1	0	15.4	230.7	38	0
A6094	14027	20	1	0	0.5	231.2	39	0
A6094	14028	21	1	0	12.4	243.6	40	1
A6094	14029	1	1	0	12.6	256.2	41	0
A6094	14030	2	1	0	12.4	268.6	42	0

A6094	14031	3	1	0	13.2	281.8	43	0
A6094	14033	5	1	0	12.3	294.1	44	0
A6094	14034	6	1	0	11.4	305.5	45	0
A6094	14035	7	1	0	11.8	317.3	46	1
A6094	14036	1	1	0	12.5	329.8	47	0
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A6094	14039	4	1	0	12.5	354.5	49	1
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A6094	14056	7	1	0	12.9	468.4	58	0
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A6094	14059	10	1	0	12.6	493.7	60	1
A6094	14060	1	1	0	14.3	508	61	0
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A6094	14064	5	1	0	12.4	544.6	64	0
A6094	14065	6	1	0	12.3	556.9	65	0
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A6094	14067	1	1	0	1.1	571.1	67	1
A6094	14069	2	1	0	11.8	582.9	68	0
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A6094	14076	9	1	0	12.3	619.7	71	1
A6094	14077	1	1	0	12.7	632.4	72	0
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A6094	14091	1	1	0	13	761.4	82	1
A6094	14106	5	1	0	12.3	773.7	83	0
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A6094	14109	8	1	0	12.1	797.1	85	1
A6094	14110	1	1	0	9	806.1	86	1
A6094	14115	5	1	0	12.5	818.6	87	0
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A6094	14122	3	1	0	12	845	90	0
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A6094	14125	2	1	0	1.1	858.5	92	1
A6094	14126	1	1	0	12.3	870.8	93	0
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A6094	14128	3	1	0	12.5	894.8	95	0
A6094	14129	4	1	0	12.2	907	96	0
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A6094	14132	7	1	0	14.3	934.2	98	0
A6094	14134	9	1	0	13.7	947.9	99	0
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A6094	14137	12	1	0	12.7	973.3	101	0
A6094	14138	13	1	0	12.7	986	102	0
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A6094	14142	2	1	0	1.2	991.5	105	1
A6094	14153	11	1	0	13.5	1005	106	0
A6094	14155	13	1	0	14.2	1019.2	107	0
A6094	14156	14	1	0	12.8	1032	108	0
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A6094	14162	20	1	0	12.3	1069.6	111	0
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A6094	14178	6	1	0	11.7	1197.2	122	0
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A6094	14182	10	1	0	11.6	1231.9	125	0
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A6094	14188	3	1	0	12.4	1295.9	130	1
A6094	14189	1	1	0	0.9	1296.8	131	1
A6094	14193	4	1	0	11.8	1308.6	132	0
A6094	14195	6	1	0	12.1	1320.7	133	0
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A6094	14205	16	1	0	12.5	1407	140	0
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A6094	14211	3	1	0	11.9	1442.6	143	1
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A6094	14343	5	0	0	3.5	1620.3	171	1
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A6094	14352	6	0	1	3.8	1629.1	174	0
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A6094	15231	3	0	0	5.7	1638.2	177	0
A6094	15251	23	0	0	6.7	1644.9	179	0
A6094	15253	25	0	0	10.3	1655.2	181	0
A6094	15258	30	0	0	5.3	1660.5	182	0
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A6094	15266	38	0	0	9.6	1678	188	0
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A6094	15299	13	0	0	9	1725.9	201	0
A6094	15301	15	0	0	9.1	1735	203	0
A6094	15306	20	0	0	3.9	1738.9	204	0
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A6094	15308	2	0	0	8.4	1750.3	207	0
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A6094	15322	16	0	0	7.1	1765.5	212	0
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A6094	15328	22	0	0	4.4	1773.4	215	0
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A6094	16251	8	0	0	7.5	1801.7	223	0
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A6094	16309	2	0	0	5.4	1821.6	227	0
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A6095	14113	1	0	0	7.3	7.3	2	0
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A6095	14135	22	0	0	5.4	15.2	4	1
A6095	14142	7	0	0	3.9	19.1	5	0
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A6095	14155	7	0	0	3.4	29.7	9	0
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A6095	14184	9	0	0	5.6	52.3	15	1
A6095	14217	33	0	0	4.8	57.1	16	0
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A6095	15216	5	0	0	3.1	122.7	34	0
A6095	15232	21	0	0	6.4	129.1	36	0
A6095	15237	26	0	0	9.6	138.7	38	0
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A6095	15265	6	0	0	7.4	165.8	45	0
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A6095	15274	9	0	0	6.9	175.6	48	0
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A6095	16092	39	0	0	4.7	238.4	64	1
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A6095	16147	10	0	0	4.5	287.6	79	0
A6095	16154	17	0	0	7.5	295.1	81	0
A6095	16158	21	0	0	3.3	298.4	82	1
A6095	16201	43	0	0	1.4	299.8	83	0

A6095	16203	45	0	0	2.5	302.3	84	0
A6095	16203	45	0	0	2.7	305	85	1
A6095	16225	22	0	0	1.7	306.7	86	0
A6095	16229	26	0	0	9.5	316.2	89	0
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A6095	16258	55	0	0	3.5	346.4	101	0
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A6095	16313	5	0	0	4.2	368.7	107	0
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A6097	16253	1	0	0	0	0	1	0
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A6097	16319	1	0	0	1.8	5.8	2	1
A6097	16321	3	0	0	7.6	17.4	4	0
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A6099	14141	1	0	0	3.8	3.8	1	0
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A6099	14205	15	0	0	2.8	13.8	4	1
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A6099	14323	14	0	0	6.6	27.2	7	1
A6099	14342	19	0	0	2.5	29.7	8	1
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A6099	14351	5	0	0	5.7	42.8	11	0
A6099	14353	7	0	0	3.3	39.2	12	1
A6099	15005	17	0	0	1.7	40.9	14	0
A6099	15007	19	0	1	9	49.9	15	0
A6099	15009	21	0	0	3.3	53.2	17	0
A6099	15013	25	0	0	5.7	58.9	18	1
A6099	15013	1	0	0	1.8	60.7	19	0

A6099	15015	3	0	0	3.6	64.3	21	1
A6099	15021	6	0	0	9	73.3	23	1
A6099	15028	7	0	0	8	81.3	31	1
A6099	15037	9	0	0	3.9	85.2	41	0
A6099	15041	13	0	0	7.8	93	42	0
A6099	15042	14	0	0	6.3	99.3	43	0
A6099	15049	21	0	0	7.1	106.4	45	0
A6099	15061	33	0	0	3	109.4	46	0
A6099	15062	34	0	0	5.4	114.8	48	0
A6099	15064	36	0	0	3.3	118.1	49	0
A6099	15068	40	0	0	6.6	124.7	51	0
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A6099	15071	43	0	0	3.2	136	55	0
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A6099	15076	48	0	0	10	152.6	60	0
A6099	15090	62	0	0	5.6	158.2	61	0
A6099	15097	69	0	0	6.3	164.5	62	0
A6099	15099	71	0	0	5.1	169.6	63	1
A6099	15113	14	0	0	5	174.6	64	0
A6099	15117	18	0	0	4	178.6	65	0
A6099	15123	24	0	0	6.2	184.8	66	1
A6099	15266	143	0	0	4.4	189.2	68	1
A6099	15268	2	0	0	1	190.2	69	0
A6099	15271	5	0	0	5	195.2	71	0
A6099	15275	9	0	0	2.9	198.1	72	1
A6099	15279	13	0	0	3.6	201.7	73	1
A6099	15281	2	0	0	6.8	208.5	75	0
A6099	15294	15	0	0	4.8	213.3	76	0
A6099	15295	16	0	0	1.6	214.9	77	0
A6099	15314	35	0	0	7.3	222.2	79	0
A6099	15317	38	0	0	2.5	224.7	80	0
A6099	15320	41	0	0	7.8	232.5	82	0
A6099	15322	43	0	0	4.3	236.8	83	0
A6099	15324	45	0	0	3.1	239.9	85	0
A6099	15334	55	0	0	6.7	246.6	87	0

A6099	15336	57	0	0	4	250.6	89	0
A6099	15338	59	0	0	4.9	255.5	91	0
A6099	15348	69	0	0	4.2	259.7	92	0
A6099	15351	72	0	0	4.3	264	95	1
A6099	16015	29	0	0	1.8	265.8	96	1
A6099	16022	7	0	0	4.4	270.2	98	0
A6099	16026	11	0	0	4.3	274.5	100	0
A6099	16028	13	0	0	2.6	277.1	101	1
A6099	16032	4	0	0	6.5	283.6	102	0
A6099	16034	6	0	0	5.8	289.4	104	0
A6099	16036	8	0	0	4.9	294.3	106	0
A6099	16040	12	0	0	6.9	301.2	108	0
A6099	16042	14	0	0	6.3	307.5	110	1
A6099	16047	5	0	0	5.6	313.1	112	0
A6099	16049	7	0	0	6	319.1	114	0
A6099	16054	12	0	0	5.4	324.5	116	0
A6099	16056	14	0	0	2.3	326.8	117	0
A6099	16130	88	0	0	3.2	330	118	1
A6099	16132	3	0	0	9.4	339.4	121	1
A6099	16139	10	0	0	4.4	343.8	122	0
A6099	16141	12	0	0	3.5	347.3	124	0
A6099	16154	25	0	0	7.7	355	126	1
A6099	16173	19	0	0	8.6	363.6	129	0
A6099	16175	21	0	0	4.8	368.4	130	1
A6099	16186	11	0	0	3.3	371.7	131	1
A6099	16188	2	0	0	0.8	372.5	132	1
A6099	16190	2	0	0	2	374.5	133	1
A6099	16229	41	0	0	5.6	380.1	134	1
A6099	16235	6	0	0	1.9	382	135	1
A6102	13346	56	0	0	8	8	3	1
A6102	13352	6	0	0	5.5	13.5	5	0
A6102	14007	26	0	1	2.4	15.9	6	1
A6102	14013	6	0	0	6.7	22.6	8	0
A6102	14015	8	0	0	8.3	30.9	11	0
A6102	14017	10	0	0	5	35.9	13	1
A6102	14035	18	0	0	16.2	52.1	14	0
A6102	14037	20	1	0	12.7	64.8	15	0

A6102	14038	21	1	0	12.9	77.7	16	0
A6102	14039	22	1	0	9.6	87.3	17	0
A6102	14041	24	1	0	12.1	99.4	18	0
A6102	14043	26	1	0	12.4	111.8	19	0
A6102	14044	27	1	0	11.9	123.7	20	0
A6102	14046	29	1	0	12.6	136.3	21	0
A6102	14048	31	1	0	12.2	148.5	22	0
A6102	14050	33	0	0	16.4	164.9	24	0
A6102	14052	35	1	0	12.2	177.1	25	0
A6102	14053	36	1	0	10.4	187.5	26	0
A6102	14056	39	1	0	12.5	200	27	0
A6102	14058	41	1	0	12.8	212.8	28	0
A6102	14059	42	1	0	12.1	224.9	29	0
A6102	14061	44	1	0	13	237.9	30	0
A6102	14062	45	1	0	12.5	250.4	31	0
A6102	14063	46	1	0	12.6	263	32	0
A6102	14068	51	1	0	13.2	276.2	33	0
A6102	14069	52	1	0	12	288.2	34	0
A6102	14070	53	1	0	12.4	300.6	35	0
A6102	14071	54	1	0	12.2	312.8	36	0
A6102	14073	56	1	0	12.4	325.2	37	0
A6102	14075	58	1	0	13.5	338.7	38	0
A6102	14076	59	1	0	12.2	350.9	39	0
A6102	14079	62	1	0	12.7	363.6	40	0
A6102	14082	65	1	0	12.7	376.3	41	1
A6102	14083	1	1	0	11.7	388	42	0
A6102	14085	3	1	0	10.8	398.8	43	0
A6102	14086	4	1	0	12.3	411.1	44	1
A6102	14088	2	1	0	13	424.1	45	0
A6102	14089	3	1	0	12.2	436.3	46	0
A6102	14090	4	1	0	12.2	448.5	47	0
A6102	14094	8	1	0	13.7	462.2	48	0
A6102	14101	15	1	0	12.5	474.7	49	0
A6102	14103	17	1	0	13.4	488.1	50	0
A6102	14105	19	1	0	12.5	500.6	51	0
A6102	14108	22	1	0	12.4	513	52	1
A6102	14111	3	1	0	12.8	525.8	53	1

A6102	14127	16	1	0	10.3	536.1	54	0
A6102	14128	17	1	0	13.3	549.4	55	0
A6102	14140	29	1	0	10.6	560	56	0
A6102	14144	33	1	0	9.7	569.7	57	0
A6102	14154	43	1	0	13.3	583	58	1
A6102	14165	10	1	0	12.4	595.4	59	0
A6102	14169	14	1	0	12.6	608	60	0
A6102	14170	15	1	0	11	619	61	0
A6102	14173	18	1	0	12.5	631.5	62	1
A6102	14177	4	1	0	11.2	642.7	63	0
A6102	14179	6	1	0	12.2	654.9	64	0
A6102	14185	12	1	0	6.1	661	65	1
A6102	14186	13	1	0	7.8	668.8	66	0
A6102	14187	14	1	0	11.3	680.1	67	0
A6102	14189	15	0	1	18.1	698.2	68	1
A6102	14323	134	0	1	1.7	699.9	69	1
A6102	15028	70	0	0	5.2	705.1	70	1
A6102	15035	77	0	0	11.3	716.4	73	1
A6102	15042	7	0	0	6.8	723.2	74	0
A6102	15044	9	0	0	4.6	727.8	76	0
A6102	15055	20	0	0	4	731.8	77	1
A6102	15061	6	0	0	5.1	736.9	79	0
A6102	15063	8	0	0	5.8	742.7	81	1
A6102	15064	9	0	0	4.2	746.9	81	0
A6102	15065	10	0	0	2.9	749.8	81	0
A6102	15069	14	0	0	3.3	753.1	82	1
A6102	15071	2	0	0	3.2	756.3	83	0
A6102	15072	3	0	0	3.2	759.5	84	0
A6102	15072	4	0	0	1.6	761.1	85	0
A6102	15076	8	0	0	9.8	770.9	87	1
A6102	15090	14	0	0	5.3	776.2	88	0
A6102	15097	21	0	0	7.1	783.3	89	0
A6102	15099	23	0	0	6.6	789.9	90	0
A6102	15104	28	0	0	15.6	805.5	91	0
A6102	15106	30	0	0	9.2	814.7	94	0
A6102	15111	35	0	0	7.5	822.2	96	0
A6102	15117	41	0	0	5.5	827.7	97	0

A6102	15119	43	0	0	11.5	839.2	99	0
A6102	15121	45	0	0	6.1	845.3	100	0
A6102	15125	49	0	0	11.9	857.2	102	0
A6102	15127	51	0	0	10.5	867.7	104	0
A6102	15128	52	0	0	4.8	872.5	105	1
A6102	15131	55	0	0	4.7	877.2	106	0
A6102	15133	57	0	0	10.4	887.6	108	0
A6102	15135	59	0	0	4.5	892.1	109	1
A6102	15139	4	0	0	3.2	895.3	110	1
A6102	15146	11	0	0	2.4	897.7	112	0
A6102	15148	13	0	0	1.9	899.6	113	1
A6102	15161	13	0	0	4.1	903.7	114	1
A6102	15175	27	0	0	8.3	912	116	1
A6102	15209	34	0	0	6.1	918.1	118	0
A6102	15224	49	0	0	3.8	921.9	119	0
A6102	16236	61	0	0	4.9	926.8	121	0
A6102	16243	68	0	0	4.3	931.1	123	1
A6102	16265	90	0	0	1.6	932.7	124	1
A6102	16271	96	0	0	2.5	935.2	126	1
A6104	14119	12	0	0	8.1	8.1	2	1
A6104	14121	14	0	0	2.7	10.8	3	1
A6104	14125	18	0	0	7.7	18.5	5	0
A6104	14127	20	0	0	2	20.5	6	0
A6104	14128	21	0	0	9.3	29.8	8	1
A6104	14141	34	0	0	2.3	32.1	9	0
A6104	14147	40	0	0	7.6	39.7	11	1
A6104	14149	42	0	0	2.1	41.8	12	0
A6104	14153	46	0	0	2.4	44.2	13	0
A6104	14155	48	0	0	7.1	51.3	14	1
A6104	14157	2	0	0	6.2	57.5	15	1
A6104	14160	3	0	0	3.2	60.7	16	1
A6104	14162	2	0	0	4.6	65.3	17	1
A6104	14164	4	0	0	5.1	70.4	19	1
A6104	14177	17	0	0	7.7	78.1	21	1
A6104	14181	21	0	0	7.4	85.5	23	1
A6104	14183	23	0	0	1.4	86.9	24	1
A6104	15117	299	0	0	4.5	91.4	25	0

A6104	15131	313	0	0	9.5	100.9	27	0
A6104	15133	315	0	0	4.7	105.6	28	1
A6104	15139	6	0	0	4	109.6	29	0
A6104	15153	20	0	0	2.3	111.9	30	0
A6104	15154	21	0	0	3.8	115.7	31	0
A6104	15155	22	0	0	7.8	123.5	33	0
A6104	15156	23	0	0	5	128.5	35	0
A6104	15159	26	0	0	2.9	131.4	36	1
A6104	15163	4	0	0	1.5	132.9	37	0
A6104	15166	7	0	0	5.3	138.2	38	0
A6104	15182	23	0	0	9.5	147.7	40	0
A6104	15201	42	0	0	1.4	149.1	41	0
A6104	15237	78	0	0	4.4	153.5	43	1
A6104	15259	22	0	0	9.7	163.2	46	0
A6104	15261	24	0	0	5.4	168.6	48	0
A6104	15265	28	0	0	8.4	177	50	0
A6104	15267	30	0	0	10.6	187.6	53	1
A6104	15280	43	0	0	9.3	196.9	56	0
A6104	15281	44	0	0	7.2	204.1	58	0
A6104	15287	50	0	0	4.7	208.8	60	0
A6104	15292	55	0	0	7	215.8	62	1
A6104	15293	1	0	0	0.5	216.3	63	1
A6104	15296	3	0	0	4	220.3	64	0
A6104	15300	7	0	0	2.4	222.7	65	1
A6104	15302	2	0	0	4.4	227.1	67	0
A6104	15313	13	0	0	5.5	232.6	69	0
A6104	15316	16	0	0	6.5	239.1	71	1
A6104	15322	6	0	0	7.4	246.5	73	1
A6104	16008	51	0	0	4.2	250.7	75	0
A6104	16011	54	0	0	6.3	257	77	0
A6104	16013	56	0	0	7	264	79	0
A6104	16015	58	0	0	1.9	265.9	80	0
A6104	16025	68	0	0	3.6	269.5	81	0
A6104	16027	70	0	0	2.4	271.9	82	1
A6104	16055	98	0	0	6.1	278	84	0
A6104	16057	100	0	0	3.1	281.1	85	1
A6104	16102	45	0	0	4.7	285.8	86	1

A6104	16104	2	0	0	2.2	288	87	1
A6104	16106	2	0	0	3.1	291.1	88	1
A6104	16110	4	0	0	1.7	292.8	89	0
A6104	16112	6	0	0	6.7	299.5	91	1
A6104	16181	69	0	0	4.3	303.8	92	1
A6104	16193	81	0	0	3.6	307.4	94	1
A6104	16195	2	0	0	2.6	310	95	1
A6104	16221	28	0	0	16	326	69	0
A6104	16227	34	0	0	3.4	329.4	70	1
A6104	16229	36	0	0	9.4	338.8	71	0
A6104	16234	41	0	0	3.5	342.3	72	0
A6104	16235	42	0	0	3.2	345.5	73	1
A6104	16250	15	0	0	3.2	348.7	74	1
A6104	16258	8	0	0	7.4	356.1	76	0
A6104	16261	11	0	0	3	359.1	77	1
A6104	16265	4	0	1	9.6	368.7	78	0
A6104	16266	5	0	0	2.4	371.1	79	1
A6104	16269	8	0	0	3.5	374.6	80	1
A6104	16271	2	0	0	8.9	383.5	81	0
A6104	16311	42	0	0	4.9	388.4	83	0
A6104	16312	43	0	0	7.4	395.8	85	0
A6104	16313	44	0	0	4.2	400	86	0
A6104	16315	46	0	1	6	406	87	0
A6104	16318	49	0	0	1.9	407.9	88	1

Appendix B: R Commands and Results

```
> mydata <-
read.csv("C:/Users/.../Documents/Frailty/B1B_FHRS_Frailty_2.csv")
> attach(mydata)
> library(survival)
> Cox1<-coxph(Surv(C_Sorties, Failure ~ CombatM + FHRS_BF +
Flight_HRS + Lag1_FHRS, data = mydata)
> summary(Cox1)
```

Call:

```
coxph(formula = Surv(C_Sorties, Failure) ~ CombatM + FHRS_BF +
Flight_HRS + Lag1_FHRS, data = mydata)
```

n= 1953, number of events= 682

	coef	exp(coef)	se(coef)	z	Pr(> z)
CombatM	0.079166	1.082384	0.119857	0.661	0.50893
FHRS_BF	-0.004106	0.995902	0.001501	-2.736	0.00621 **
Flight_HRS	-0.066993	0.935201	0.013232	-5.063	4.13e-07 ***
Lag1_FHRS	0.006732	1.006755	0.012413	0.542	0.58756

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	exp(coef)	exp(-coef)	lower .95	upper .95
CombatM	1.0824	0.9239	0.8558	1.3690
FHRS_BF	0.9959	1.0041	0.9930	0.9988
Flight_HRS	0.9352	1.0693	0.9113	0.9598
Lag1_FHRS	1.0068	0.9933	0.9826	1.0315

Concordance= 0.627 (se = 0.013)

Rsquare= 0.033 (max possible= 0.99)

Likelihood ratio test= 64.74 on 4 df, p=2.925e-13

Wald test = 61.62 on 4 df, p=1.321e-12

Score (logrank) test = 62.52 on 4 df, p=8.555e-13

```
> Frailty1.Cox <- coxph(Surv(C_Sorties, Failure ~ CombatM +
FHRS_BF + Flight_HRS + Lag1_FHRS + frailty(ID), data=mydata)
> summary(Frailty1.Cox)
```

Call:

```
coxph(formula = Surv(C_Sorties, Failure) ~ CombatM + FHRS_BF +
Flight_HRS + Lag1_FHRS + frailty(ID), data = mydata)
```

n= 1953, number of events= 682

coef	se(coef)	se2	Chisq	DF	p
------	----------	-----	-------	----	---

CombatM	0.616284	0.132928	0.132621	21.49	1.00	3.5e-06
FHRS_BF	-0.002126	0.001489	0.001488	2.04	1.00	1.5e-01
Flight_HRS	-0.068339	0.013402	0.013399	26.00	1.00	3.4e-07
Lag1_FHRS	0.006806	0.012953	0.012950	0.28	1.00	6.0e-01
frailty(ID)				880.80	15.15	0.0e+00

	exp(coef)	exp(-coef)	lower .95	upper .95
CombatM	1.8520	0.5399	1.4272	2.4032
FHRS_BF	0.9979	1.0021	0.9950	1.0008
Flight_HRS	0.9339	1.0707	0.9097	0.9588
Lag1_FHRS	1.0068	0.9932	0.9816	1.0327

Iterations: 8 outer, 44 Newton-Raphson

Variance of random effect=0.991288 I-likelihood = -4300.9
 Degrees of freedom for terms= 1.0 1.0 1.0 1.0 15.2
 Concordance= 0.689 (se = 0.013)
 Likelihood ratio test= 414.6 on 19.15 df, p=0

> **Cox1\$loglik**

[1] -4468.748 -4436.381

> **Frailty1.Cox\$loglik**

[1] -4468.748 -4261.436

>

> **Frailty6.Cox<-coxph(Surv(C_Sorties, Failure ~ CombatM + FHRS_BF + Flight_HRS + Lag1_FHRS + frailty(ID), data=mydata)**

> **summary(Frailty6.Cox)**

Call:

coxph(formula = Surv(C_Sorties, Failure) ~ CombatM + FHRS_BF + Flight_HRS + Lag1_FHRS + frailty(ID), data = mydata)

n= 410, number of events= 125

	coef	se(coef)	se2	Chisq	DF	p
CombatM	2.208591	0.322646	0.322298	46.86	1.00	7.6e-12
FHRS_BF	0.001772	0.002499	0.002499	0.50	1.00	4.8e-01
Flight_HRS	-0.075812	0.027180	0.027174	7.78	1.00	5.3e-03
Lag1_FHRS	-0.005926	0.027930	0.027924	0.05	1.00	8.3e-01
frailty(ID)				0.17	0.06	4.2e-01

	exp(coef)	exp(-coef)	lower .95	upper .95
CombatM	9.1029	0.1099	4.8366	17.1323
FHRS_BF	1.0018	0.9982	0.9969	1.0067
Flight_HRS	0.9270	1.0788	0.8789	0.9777
Lag1_FHRS	0.9941	1.0059	0.9411	1.0500
gamma:1	0.9898	1.0103	0.9224	1.0621
gamma:12	1.0102	0.9899	0.9421	1.0832

Iterations: 5 outer, 15 Newton-Raphson
Variance of random effect=0.001321009 I-likelihood = -570.8
Degrees of freedom for terms= 1.0 1.0 1.0 1.0 0.1
Concordance= 0.604 (se = 0.032)
Likelihood ratio test= 56.7 on 4.06 df, p=1.559e-11

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14. ABSTRACT During the 2017 posture statement to the US Senate Armed Services Committee, the Secretary of the Air Force and Chief of Staff of the Air Force stated the Air Force suffers from shrinking aircraft inventory, aging aircraft fleets, and flying beyond expected service life. These trends are not exception to the B-1B Lancer, which has been in service since 1986. Recently, the B-1B Lancer has maintained the lowest mission capable (MC) rates, 47.7 percent. The purpose of this research is to explore the failure rates of the B-1B Lancer using survival analysis that could help better understand the failure behavior of the B-1B Lancer. A Cox proportional hazards regression model with frailty confirms the existence of unobserved heterogeneity or frailty in our analysis. When the frailty is controlled, combat missions increase failure rates. Other variables, mainly flight hour or sortie duration related variables, are inconclusive and require further analysis. This study proposes insights based on findings and suggests future research directions.					
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