

Modeling solar desalination with reverse osmosis (RO) powered by concentrating solar power (CSP) plan

Ahmed Remlaoui^{1,*}, Hammou Soumia², Bent Abdelkader Nafissa², Driss Nehari¹

¹ Smart Structure Laboratory, University Center of Ain-Témouchent, 46000 Ain-Témouchent, ALGERIA ² Department of Mechanical Engineering, University Center of Ain-Témouchent, 46000 Ain-Témouchent, ALGERIA

donremlaoui@gmail.com

Abstract – This article deals with the desalination of seawater and brackish water, which can deal with the problem of water scarcity that threatens certain countries in the world; it is now possible to meet the demand for drinking water. Currently, among the various desalination processes, the reverse osmosis technique is the most used. Electrical energy consumption is the most attractive factor in the cost of operating seawater by reverse osmosis in desalination plants. Desalination of water by solar energy can be considered as a very important drinking water alternative. For determining the electrical energy consumption of a single reverse osmosis module, we used the System Advisor Model (SAM) to determine the technical characteristics and costs of a parabolic cylindrical installation and Reverse Osmosis System Analysis (ROSA) to obtain the electrical power of a single reverse osmosis module. The electrical power of a single module is 4101 KW; this is consistent with the manufacturer's data that this power must be between 3900 kW and 4300 KW. Thus, the energy consumption of the system is 4.92 KWh/m3. Thermal power produced by the solar cylindroparabolic field during the month of May has the maximum that is 208MWth, and the minimum value during the month of April, which equals 6 MWth. Electrical power produced by the plant varied between 47MWe, and 23.8MWe. The maximum energy was generated during the month of July (1900 MWh) with the maximum energy stored (118 MWh).

Keywords: System Advisor Model (SAM), Reverse Osmosis System Analysis (ROSA), Rankine cycle, parabolic trough power.

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I. Introduction

The use of seawater desalination to provide fresh drinking water is a well-established and flourishing industry. The two main technologies used are thermal desalination and Reverse Osmosis (RO) membrane filtration. The desalination of brackish water or seawater by conventional treatment units requires a large electrical energy and / or heat. Among the processes, distillation and reverse osmosis are technologies whose performance has been proven to desalinate salt water [1]. Concentrating solar power (CSP) technology is considered as one of the alternative solutions of power generation from solar energy. In this technology, sunrays are focused onto a solar receiver with the help of mirrors. The energy captured by the receiver is converted to heat or electricity through a series of process [2]. Martin et al. used a mathematical programming technique to optimize the operation of a CSP plant employing regenerative Rankine cycle for a site in Spain. [3]. A simulation model for predicting the electrical output of a 50 MWe PTC power plant was developed by Garcia et

al. [4]. The model results were compared with the experimental data of a power plant operating in Spain.

During our modeling and simulation work, we used software, SAM [5] (System Advisor Model) for the energy study of a parabolic concentrator and ROSA [6] (Reverse Osmosis System Analysis) to obtain the electrical power of a single reverse osmosis module.

The objective of this work is the technical and economic study of a parabolic plant used to produce electricity consumed by a reverse osmosis module. The results obtained make it possible to highlight the effect of the electrical energy consumption on the cost of desalination by reverse osmosis.

II. Presentation of the solar desalination plant used

The heat generated by a CSP plant can be utilized to produce the required electric power needed to drive the

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RO pumps [7].It has been reported that CSP/RO coupling is more efficient and requires less energy than CSP/MED coupling [8]. Fig. 1 shows a schematic diagram of a CSP/RO coupling [9].

The parabolic-cylindrical mirror-type solar power plant consists of parallel rows of long, semi-cylindrical, north-south-oriented mirrors that circle around it to follow the sun's course. The sun's rays are concentrated on a longitudinal receiver tube arranged all along the installation. Inside this tube circulates a coolant that will be used to capture and transport heat; the fluid temperature can reach up to 400 $^{\circ}$ C. The coolant heat is transmitted to the water that vaporizes, the steam produced operates a turbine, and this turbine drives the

generator that produces electricity. This plant has a molten salt tank that can store heat for several hours, and thus produce electricity in the night.

The transfer fluid was chosen according to its physicochemical properties. In this study, Therminol VP-1 was used because of its thermal stability up to temperatures of 400°C. Therminol VP-1 is a hydrocarbon - based synthetic fluid consisting of a mixture of 75 % diphenyl oxide ($C_{12}H_{10}OH$) and 25% diphenyl ($C_{12}H_{10}$). On the other hand, since the molten salts based on sodium and potassium nitrates have a good exchange coefficient and a good thermal inertia, which allows them to store heat, they are used in the present study.

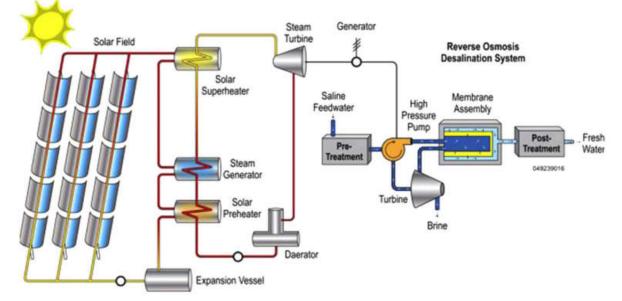


Figure 1. Schematic diagram of the Rankine cycle with solar field powering RO desalination system [8]

III. System simulation

III.1. Reverse osmosis (RO)

The approach used to obtain the electrical power required to run ten (10) reverse osmosis modules is done using the ROSA software.

The ROSA 9.1 software is the latest version, used in the analysis to determine membrane performance and energy requirements for desalination [6].

ROSA can be used to finalize and optimize the design of an installation, provide details for the selection of a feed pump and provide information for post-processing requirements [6].

The ROSA program has four input pages, a report page and a cost analysis page. The six tabs are:

- 1. Project Information.
- 2. Feed water data.

- 3.Scaling information.
- 4. System Configuration.
- 5. Report.
- 6. Cost analysis.
- Table 1 shows the main parameters of feed water Table 1. Supply water settings

Number of modules $= 10$			
Seawater salinity	36132 mg/l		
Temperature	18.8		
РН	8.5		

Figure 2 shows the configuration of the system, in the case of a single module or there are 246 pressure tubes, each tube equipped with 7 membranes (1722 membranes in total). The type of membrane is SW 30 HR-380. The permeate flow rate is 20,000 m³/d and the conversion rate is 47 %.

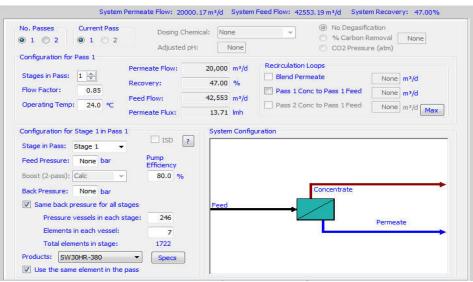


Figure 2. The configuration of the reverse osmosis system on ROSA

III.2. Rankine cycle with solar field

After having completed the first step concerning the reverse osmosis module and the definition of the power necessary to operate the reverse osmosis desalination unit, we will proceed to the next step, which concerns the dimensioning of the CSP plant in order to provide a power supply for the reverse osmosis unit. We used another technical-economic software to determine the technical characteristics and costs of the CSP system, as well as the performance analysis of the parabolic cylindrical CSP plant.

In this part, we will make a simulation of a CSP plant, whose heat transfer fluid is thermal oil (Therminol VP1), this plant is tested for the Ain Témouchent site, the nominal power of this plant is 40.7 MWe. The System Advisor Model (SAM) code was used to simulate the

annual behavior of the CSP plant at the time scale. SAM predicts the dynamic behavior of the parabolic trough.

The System Advisor Model (SAM) software is a software that performs cost and performance analysis of solar installations. This software was developed by the National Renewable Energy Laboratory (NREL), Sandia's national laboratories in partnership with the United States Department of Energy (DOE), and the Solar Energy Technology and Program (SETP). It has been designed to facilitate decision-making for those involved in the renewable energy industry [5].

The empirical model of a CSP modeling plant is identical to the physical model, only it uses a set of curve fitting equations derived from the regression analysis of the measured data from SEGS (Solar Energy Generating Systems) projects in the southwestern United States, is shown in Figure 3.

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Trough (empr), Commercial	NREL National Solar Radiation Da	stabase (NSRDB)					
ocation and Resource	Download the latest weather files to choose files to download for single			Download a typic	al-year (TMY) file for n	nost long-term ca	sh flow analyses, o
iolar Field							
Collectors (SCAs)	Download a TMY file for Americas SAM's CSP models use a different time convention for weather data		TMY or Single-year for Americas and Asia ata than the NREL NSRDB. See Help for details.			Map on NSRDB website	
Receivers (HCEs)	Solar Resource Library					Internationa	Data Sources
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Thermal Storage	Weather file C:\SAM\2017.9.5	\solar_resource\USA AZ Tucson	(TMY2).csv				
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Electricity Rates		1.0 Dec. 10 De	Average wir	nd speed	39 m/s		
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Incentives Electricity Rates Electric Load Simulate >	Diffuse horizontal -Files in Library Search for: Name	1.41 kWh/m²/day	Station ID	Latitude	Longitude		

Figure 3. The CSP plant in SAM program

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The parameters concentrating the different components
of the installation are:
  1-Solar Field
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- 2-Collectors (SCAs)
- 3-Receivers (HCEs)
- 4-Power Block
- 5-Thermal Storage

Results and discussion IV.

IV.1. Meteorological data

Figure 4a Shows the solar radiation, the most extreme estimations of solar radiation was 1000 W.m⁻². Figure 4.b shows the change in ambient temperature and Figure 4c shows the wind speed during the year for the selected site. Note that the maximum and minimum temperature recorded is equal to 37 ° C and 1 ° C respectively and we note that the maximum wind speed is 15 m/s.

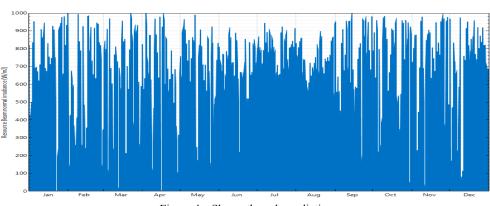


Figure 4a. Shows the solar radiation

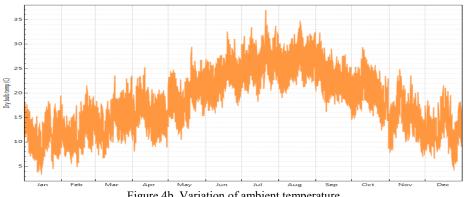
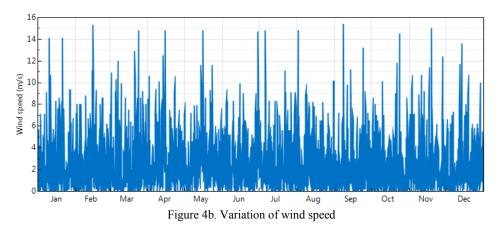


Figure 4b. Variation of ambient temperature



IV.3. System performance of CSP plan

IV.2. Reverse osmosis

After introducing, the previous data into the ROSA code. The simulation results shown in Table 2, we note that the electrical power of a single module is 4101 KW; this is consistent with the manufacturer's data that this power must be between 3900 kW and 4300 KW. Thus, the energy consumption of the system is 4.92 KWh/m3.

Table2: RO system details			
Parameter	Value		
Feed flow rate [m3/j]	42553.19		
pressure brine [bar]	66.61		
brine flow rate [m3/j]	22553.02		
pressure Permeate [bar]	65.20		
Permeate flow rate [m3/j]	20000.17		
salinity [mg/l]	277.51		
The power [kw]	4101.57		
Specific energy [kwh/m3]	4.92		

IV.3.1. Thermal power produced by the solar cylindro-parabolic field

Figure 5 shows the total heat output produced during the year. We note that the thermal power during the month of May has the maximum that is 208MWth, and the minimum value of the thermal power recorded during the month of April, which equals 6 MWth.

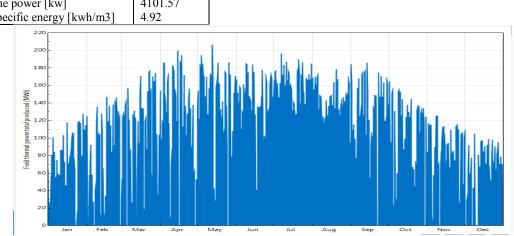


Figure 5. Total thermal power produced during the year (MWt)

IV.3.2. Electrical power produced by the plant

Figure 6 shows the hourly variation in the net power generated during the year. Note that the power is varied

between 47MWe, and 23.8MWe. It is observable that the power produced is proportional to the incident direct radiation on the solar reflectors.

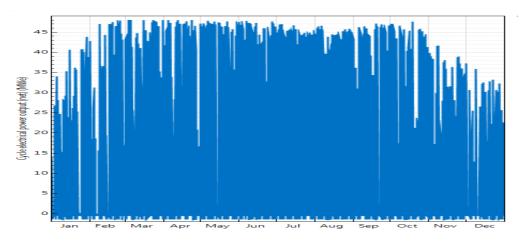


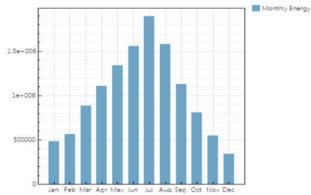
Figure 6. System power generated during the year (KWe)

IV.3.3. Power of CSP plant

As can be seen in the graphs above that: The maximum thermal power absorbed was estimated at 12 Mwt as well as the maximum electrical output power (net) was estimated at 4.5 Mwe, and the maximum electrical power of production (gross) was estimated at 4.8 Mwe and Incident of maximum thermal power on the ground was estimated at 30 Mwt .its maximum thermal loss of the reservoir was estimated at 0 Mwt and TES Maximum thermal energy in storage was estimated at 4 Mwt.

IV.3.4. Energy generated and thermal energy in storage

The energy generated by each month and the thermal energy for storage illustrated in Figure 7. It can be seen that the maximum energy was generated during the



month of July (1900 MWh) with the maximum energy stored (118 MWh).

IV.3.5. Field HTF temperature hot and cold header

The heat transfer fluid (HTF) flows from the cold reservoir to the hot reservoir, the minimum temperature of the cold header inlet has reached a value of 160 °C, and the maximum temperature obtained at the header outlet hot is 400 0C. The variation of the temperature of the hot and cold header input is shown in the Figure 8.

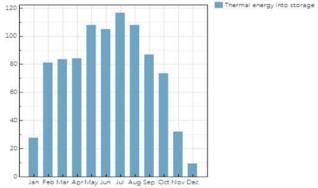


Figure 7. Monthly energy generated and thermal energy in storage (MWh)



Figure 8. Field HTF temperature hot and cold header

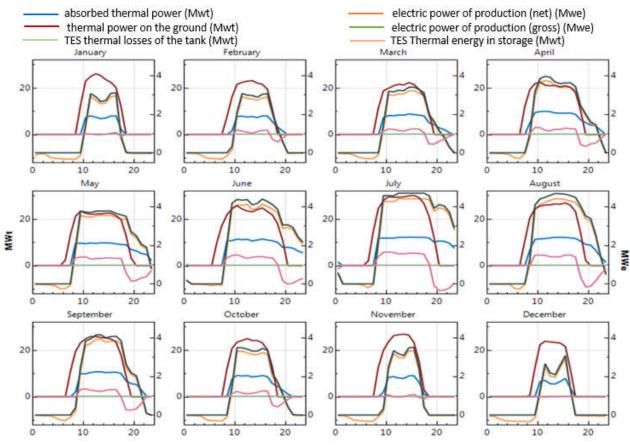


Figure 9. Absorbed thermal power (Mwt) and field power (Mwt), gross and net electric power (Mwe), TES thermal losses from the tank (Mwt) and in storage (Mwt)

IV.3.6. TES HTF, hot and cold tanks volume

For power generation after sunset, the HTF fluid should be stored in the storage tank for a storage capacity of 8:00 h. The total HTF maximum thermal energy storage (TES) is 1300 m^3 , the maximum hot tank HTF

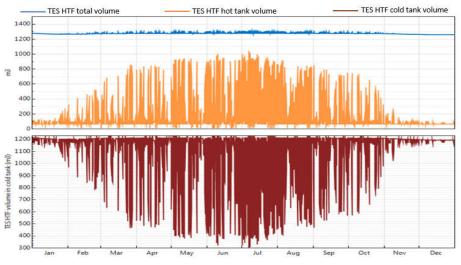


Figure 10. TES HTF total volume, hot and cold tanks volume

volume is 1000 m^3 and the maximum cold tank HTF volume is 1200 m^3 as shown in Figure 9 and Figure 10.

Table 3: Technical characteristics of CSP system

The simulation is carried out using the SAM software, the technical characteristics of the CSP system are shown in Table 3 and the system costs are shown in Table 4.

IV.4.	Technical c	characteristics	and system costs	
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	The variables	Values
Collector	Reflective Opening Area [m ²]	817.5
	Opening width, total structure [m]	5.75
	Length of collector assembly [m]	150
	Number of modules per assembly [-]	12
	Average length of the surface at the focal length [m]	2.11
	Distance between assemblies [m]	1
Receiver	Inside diameter of absorber tube [m]	0.076
	Outer diameter of absorber tube [m]	0.08
The solar	Line spacing [m]	15
field	Irradiation [W/m ²]	950
	Thermal field production [MW]	23.5613
	Solar Field Area (acres)	25
	Total Area (acres)	35

Tuble 1. CBT system costs.			
The costs	Values		
Site Improvements (\$)	981000		
Solar field (\$)	5 886 000		
HTF system (\$)	2354400		
Storage (\$)	6 125950		
Total direct cost (\$)	22 120782		
Total Indirect Cost (\$)	3 672293		
Total cost of installation (\$)	25 793022		
Total cost of the facility per capacity (\$ / kW)	6 833		

V. Conclusion

This article focuses on the techno-economic modeling of a cylindro-parabolic power plant to generate the electrical energy required for desalination by reverse osmosis. The results show that:

- The electrical power of a single module is 4101 KW; this is consistent with the manufacturer's data that this power must be between 3900 kW and 4300 KW. Thus, the energy consumption of the system is 4.92 KWh/m³.
- Thermal power produced by the solar cylindroparabolic field during the month of May has the maximum that is 208 MWth and the minimum value during the month of April, which equals 6 MWth.
- Electrical power produced by the plant varied between 47MWe, and 23.8MWe
- The maximum energy was generated during the month of July (1900 MWh) with the maximum energy stored (118 MWh).
- The minimum temperature of the cold header inlet has reached a value of 160 °C, and the maximum temperature obtained at the header outlet hot is 400 ⁰C.
- Total cost of the facility per capacity is 6.833 \$/kW

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