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National Uranium Resource Evaluation

AERIAL GAMMA RAY AND MAGNETIC SURVEY
MANITOWOC AND TRAVERSE CITY QUADRANGLES
WISCONSIN AND MICHIGAN

FINAL REPORT

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 **EG&G GEOMETRICS**
Sunnyvale, California 94086

July 1981

GEOLOGICAL SURVEY OF WYOMING



PREPARED FOR U.S. DEPARTMENT OF ENERGY

Grand Junction Office, Colorado

metadc1202326

This report is a result of work performed by EG&G geoMetrics through a Bendix Field Engineering Corporation Subcontract, as part of the National Uranium Resource Evaluation. NURE is a program of the U.S. Department of Energy's Grand Junction, Colorado, Office to acquire and compile geologic and other information with which to assess the magnitude and distribution of uranium resources and to determine areas favorable for the occurrence of uranium in the United States.

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Prepared by
EG&G geoMetrics
Sunnyvale, California

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Prepared for the U.S. Department of Energy
Grand Junction Office, Colorado
Under Contract No. DE-AC13-76GJ01664
and Bendix Field Engineering Corporation
Subcontract No. 80-479-L

ABSTRACT

The combined quadrangles of Manitowoc and Traverse City include an approximate land area of 8,800 square miles and an additional water surface area of 4,800 square miles in Michigan and Wisconsin. A thick sequence of Paleozoic sediments overlies the crystalline basement forming the northwestern quadrant of the Michigan Basin. The sediments thin toward the west to approximately 500 feet in Wisconsin. A pervasive layer of Wisconsinan Stage (Pleistocene) glacial drift and glacial lake sediments cover the entire land surface.

A search of available literature revealed no known uranium deposits.

A total of nine (9) uranium anomalies were detected and are discussed briefly in this report. Radiometric data appears to reflect differences in saturated versus unsaturated ground conditions rather than differences between map units. None of the anomalies were considered significant and all appear to be related to cultural features.

Magnetic data appears to be in general agreement with the structural interpretation of the area. Broad wavelength magnetic contours correspond to the deeply buried basement rocks in the east with increasing complexity in magnetic data occurring toward the west where basement rocks are closer to the surface.

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INTRODUCTION

General

The Manitowoc and Traverse City quadrangles include a land area of 8,800 square miles and an additional water surface area of 4,800 square miles. Both quadrangles encompass most of the northern part of the lower Michigan peninsula. In addition, the Manitowoc quadrangle contains a broad expanse of Lake Michigan and part of northeastern Wisconsin (see Figure 1).

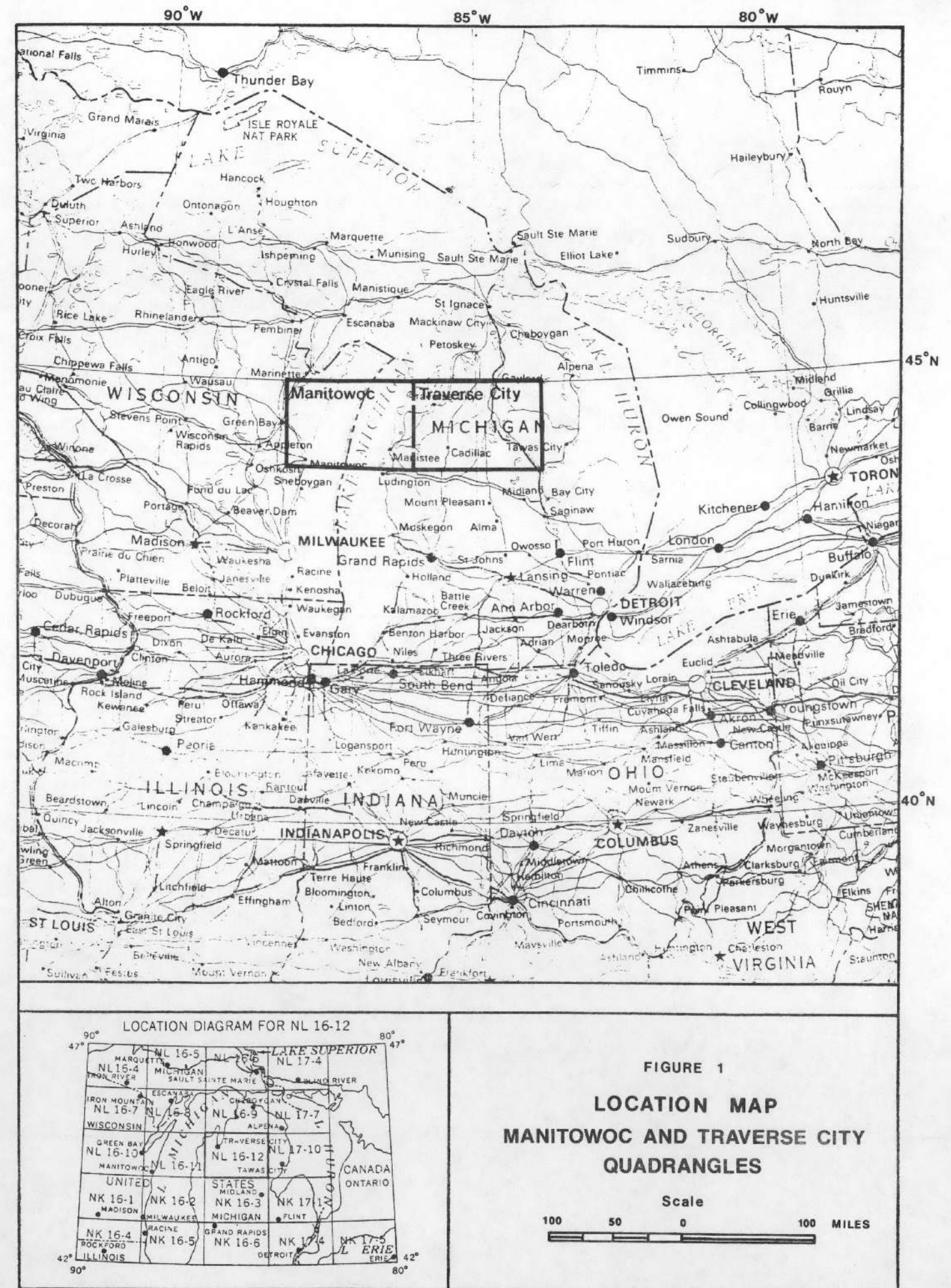
The geologic base maps used in this report were compiled at a scale of 1:250,000 by Amuedo and Ivey, Consulting Geologists (Traverse City, 1980) and Fremont Geologic Consultants (Manitowoc, 1980). Published sources of geologic data for the base maps include reports by the Michigan Geological Survey, Geological Society of America and U.S. Geological Survey dating from 1915 and later. Additional data was extracted from published and manuscript maps at scales of 1:220,000 and larger. Geologic unit descriptions in this report conform to those of the base map legends which are found in Appendix C. Supplementary geologic information came from Cohee and others (1962), Flint (1959, 1971) and Weller (1975). Cultural and physiographic information was taken from the 1:250,000 scale topographic quadrangles.

Radiometric and magnetic data for both Manitowoc and Traverse City quadrangles were acquired in May and June 1981 and processed in July of the same year. A detailed summary of data acquisition, processing, interpretation, and presentation methods can be found in Appendix A. A flight line summary report for the Manitowoc and Traverse City quadrangles is contained in Appendix B. It should be noted that although Appendices C, D, E, and H are presented as separate quadrangles, the interpretation report, statistics, data tapes and microfiche are processed and presented as one area.

Physiography

The Manitowoc and Traverse City quadrangles lie within a broad glaciated plain which is situated near the northern boundary of the Midwestern Physiographic Province. Landforms produced by the most recent stage of glaciation characterize the region and include such features as moraines, drumlins, glacial outwash valleys, and dissected landscape that resulted from erosion of glacial till. A deranged drainage pattern, typical of glaciated regions, is developed throughout the area within Michigan and to a lesser extent in Wisconsin. Here numerous glacially formed lakes are scattered among swampy lowlands and stream courses.

In both Michigan and Wisconsin marshlands occupy considerable area within low-lying outwash and moraine deposits. A regional topographic summit in Michigan produces a drainage system that radiates to the east, south, and west. The two principle rivers, the Manistee and AuSable Rivers, drain central Michigan in opposite directions, flowing into Lake Michigan and Lake Huron respectively. The smaller Muskegon River flows out of the region toward the south (see Figures 3a and 3b). In Wisconsin the course of present day streams reflects the influence of ancient glacially controlled drainage patterns.



Four streams cross the entire width of the Door Peninsula occupying channels that are larger than would otherwise be expected from such short courses. They empty toward the southeast into Lake Michigan. Green Bay separates the Door Peninsula from the mainland to the west.

The topography in both Michigan and Wisconsin displays some variability with areas of relatively flat surfaces included among areas where stream erosion has caused up to 300 feet of local relief. The lowest elevation is the mean level of Lake Michigan which is 580 feet. The highest point is 1,725 feet at the Cadillac Lookout tower 8 miles south-southeast of the town of Cadillac, Michigan. Total elevation difference over the entire region is 1,145 feet.

In Michigan, land application is primarily rural although numerous small population centers, a military reservation and oil and gas fields are present throughout the area. Wisconsin has a somewhat more developed primary and secondary road network and also contains the city of Green Bay (87,800 pop.). Railroads serve only the larger communities in both states.

GEOLOGY

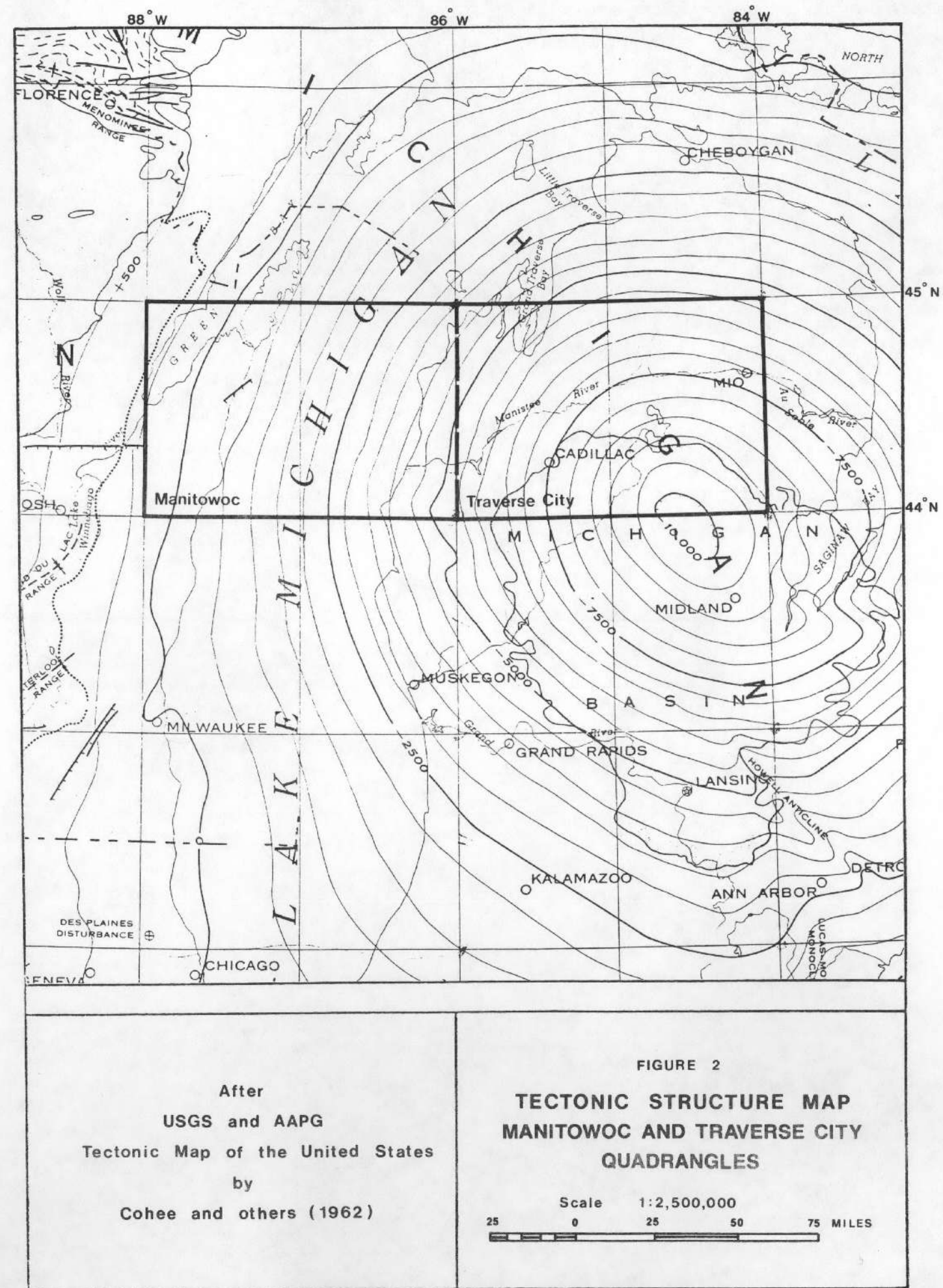
Structure

The basement rocks below the Manitowoc and Traverse City quadrangles are influenced by a regional downwarping called the Michigan Basin which contains more than 10,000 feet of Paleozoic sediments (see Figure 2). The quadrangles overlie the north and western sectors of the Michigan Basin where a total relief of 10,500 feet in the basement surface occurs between the east and west map boundaries. Sedimentary strata reach a maximum thickness of 11,000 feet below the southeast corner of the Traverse City quadrangle and thins to approximately 500 feet under Green Bay. The basement surface displays a constant dip eastward with no faults or folds, and no faults are indicated on the geologic base maps for these quadrangles.

Surface Geology

A mantle of Pleistocene sediments spreads across the entire land surface of the Manitowoc and Traverse City quadrangles. These deposits consist of a combination of glacial, periglacial, and post-glacial material. Bedrock units do not reach through this cover and therefore no exposures older than Pleistocene are shown on the base map.

A variety of glacial deposits from the Wisconsin Stage cover Michigan in a mosaic of outwash sediments, till plains, glacial ponded water deposits and lake plain sediments. Flat-lying outwash and spillway sediments occupy many of the modern valleys and lake basins. The direction of outwash flow at the time of deglaciation was toward the south and west, approximating today's drainage conditions. Outwash sediments account for 30 percent of all glacial material in Michigan. A number of major lateral moraines and prominent end moraines lie between the outwash deposits. The area occupied by all moraine deposits comprises 55 percent of all glacial material while glacial ponded water deposits and lake plains sediments constitute the remaining 15 percent.



Ground moraines typically form flat land surfaces that are often interrupted by hummocky topography produced by end moraines. Both ground and end moraines are composed of till which contains an unsorted, unstratified mixture of clay, silt, sand, and gravel. Outwash and lake sediments form nearly flat surfaces and contain stratified sediments including clay, silt, sand and gravel.

Uranium

According to available literature, there are no known Uranium deposits in the Manistowoc and Traverse City quadrangles (Butler and others, 1962, Schnabel, 1955).

INTERPRETATION OF GEOPHYSICAL DATA

Radiometric Data

A total of 9 groups of uranium (Bi214) samples meet the minimum statistical requirements set forth in the data interpretation section of Appendix A. These are displayed, along with all other anomalous samples and pertinent data, on Figures 3 and 3a. The anomalies are summarized in a table in Appendix G. The potassium, uranium, thorium, and ratio pseudo-contour maps, which reflect radiometric responses for each quadrangle, are found in Appendix H. Discussion of the abundances of potassium, uranium, and thorium are in terms of apparent equivalent percent and apparent equivalent ppm. These equivalent units are derived from scaling of counts per second by the sensitivities calculated for the detection system and as such cannot be taken as directly determined geochemical values.

Values for potassium, uranium, and thorium are low throughout the survey area, as are the respective values in survey areas to the north and south. The unusually low values are due, in part, to the excessive surface moisture represented by marshes and broad low valleys where saturation of the ground tends to suppress the emission of gamma rays into the atmosphere. Radiometric values are significantly lower in Michigan due to this phenomenon. Areas of higher standing ground are often responsible for a greater number of anomalous samples as illustrated by the drainage divide between the Manistee and Betsie Rivers in the west center of the Traverse City quadrangle (see Appendix H and the Uranium Anomaly Map, Figure 3a). The greater number of anomalous samples here are not restricted to any single map unit. In addition, these same units in lower lying areas contain no highly anomalous samples. The average value for uranium considering all map units throughout the area is .95 ppmeU. Potassium and thorium areawide average values are .81 percent and 2.01 ppmeTh respectively.

Statistical analysis shows map unit Qde (drumlins and eskers) has the highest mean value for the three sampled elements. Potassium has a mean value of 1.45 percent while uranium and thorium have mean values of 1.22 ppmeU and 3.71 ppmeTh respectively. This map unit occurs over a limited area in Wisconsin, and represents only a small number of data points however (see Appendix H).

Map unit Qwn (glacial water-laid moraine) has the second highest mean value for uranium, 1.19 ppmeU, although it too represents only a small proportion of the survey area in Michigan. The highest measured peak values for potassium and thorium are located over map unit O1 (glacial lake deposits). These are 2.36 percent potassium and 7.46 ppmeTh respectively. The map unit Qma (marsh deposits) in Wisconsin is responsible for the highest measured peak value for uranium of 2.72 ppmeU.

Most of the map units show either a slight bimodal tendency or a skewing toward higher values in all three radiometric elements (see Appendix F). The area west of Lake Michigan produces generally higher overall values and is partially responsible for this skewing. An additional reason for the skewing stems from the masking of anomalous samples due to the relative amount of moisture within a given map unit as mentioned above. This is especially true in Michigan.

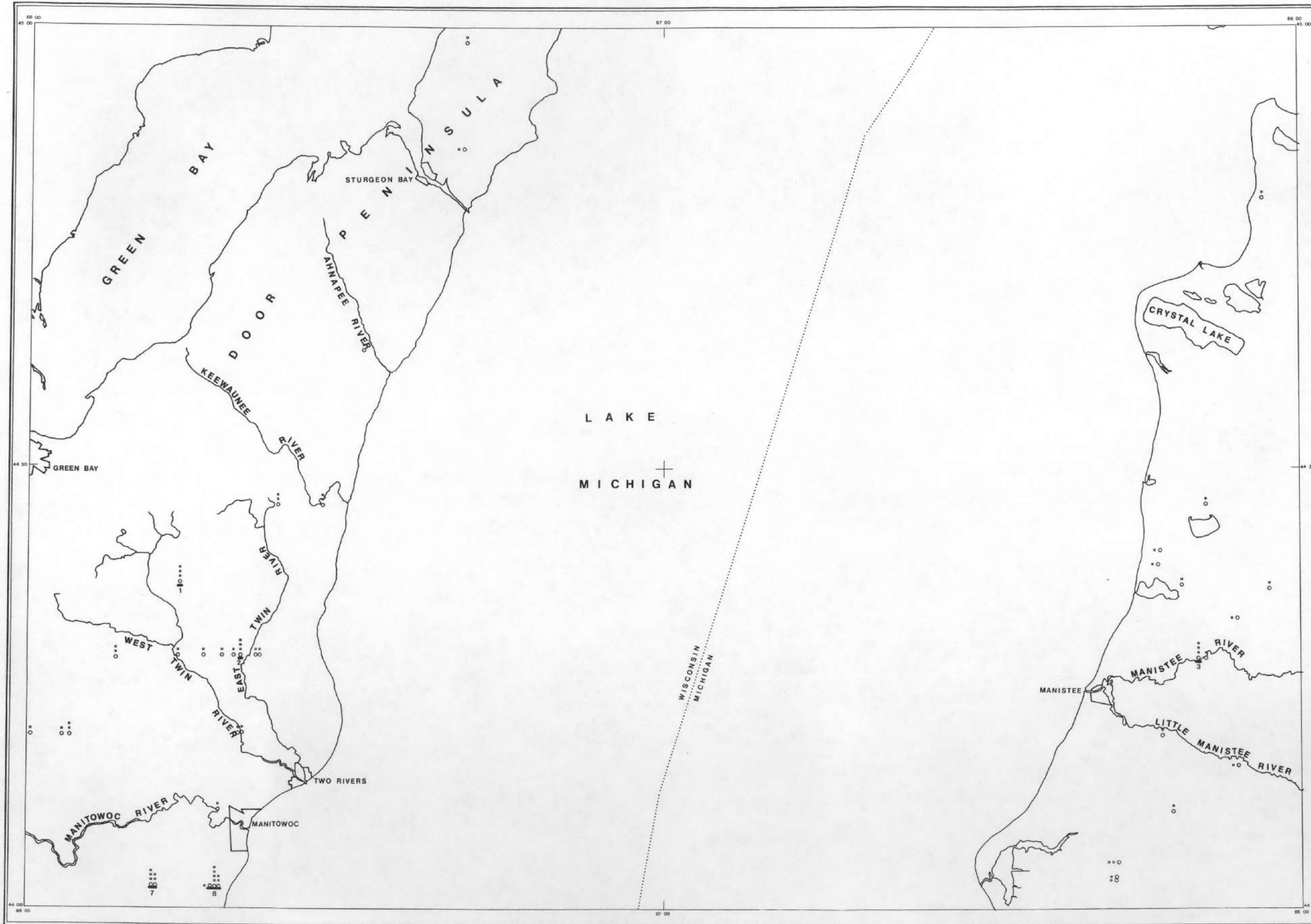
Of the nine uranium anomalies identified in the two quadrangles and appearing in Figures 3 and 3a, four occur over map unit QGM (glacial ground moraine). The anomalies follow no discernable trend and are widely scattered throughout the southern part of the area. Peak values for these anomalies range from 1.2 ppmeU to 2.4 ppmeU. Specific anomalies appear to result entirely from cultural influences (such as the effect of roads, railroads, pipelines, etc.) and locally unsaturated areas that tend to enhance uranium values.

Magnetic Data

The pseudo-contour map of the magnetic data appears in Appendix H.

The general aspect of the pseudo-contour map confirms the structural interpretation for the basement in this area. The relatively flat magnetic terrain reflects the great thickness of the sedimentary column in Michigan, where low residual magnetic values are broadly distributed and are only occasionally interrupted by smaller magnetic features. In Wisconsin where the basement is close to the surface, magnetic values are larger. A poorly defined east-west strike is evident in the pseudo-contours. The shorter wavelength magnetic features superimposed on the regional background may be due to structures within the magnetic basement or folds which bring basement rocks closer to the surface.

MANITOWOC



URANIUM ANOMALY/
INTERPRETATION MAP

MANITOWOC QUADRANGLE
U.S. DEPARTMENT OF ENERGY

APPROXIMATE SCALE 1:500,000

EXPLANATION

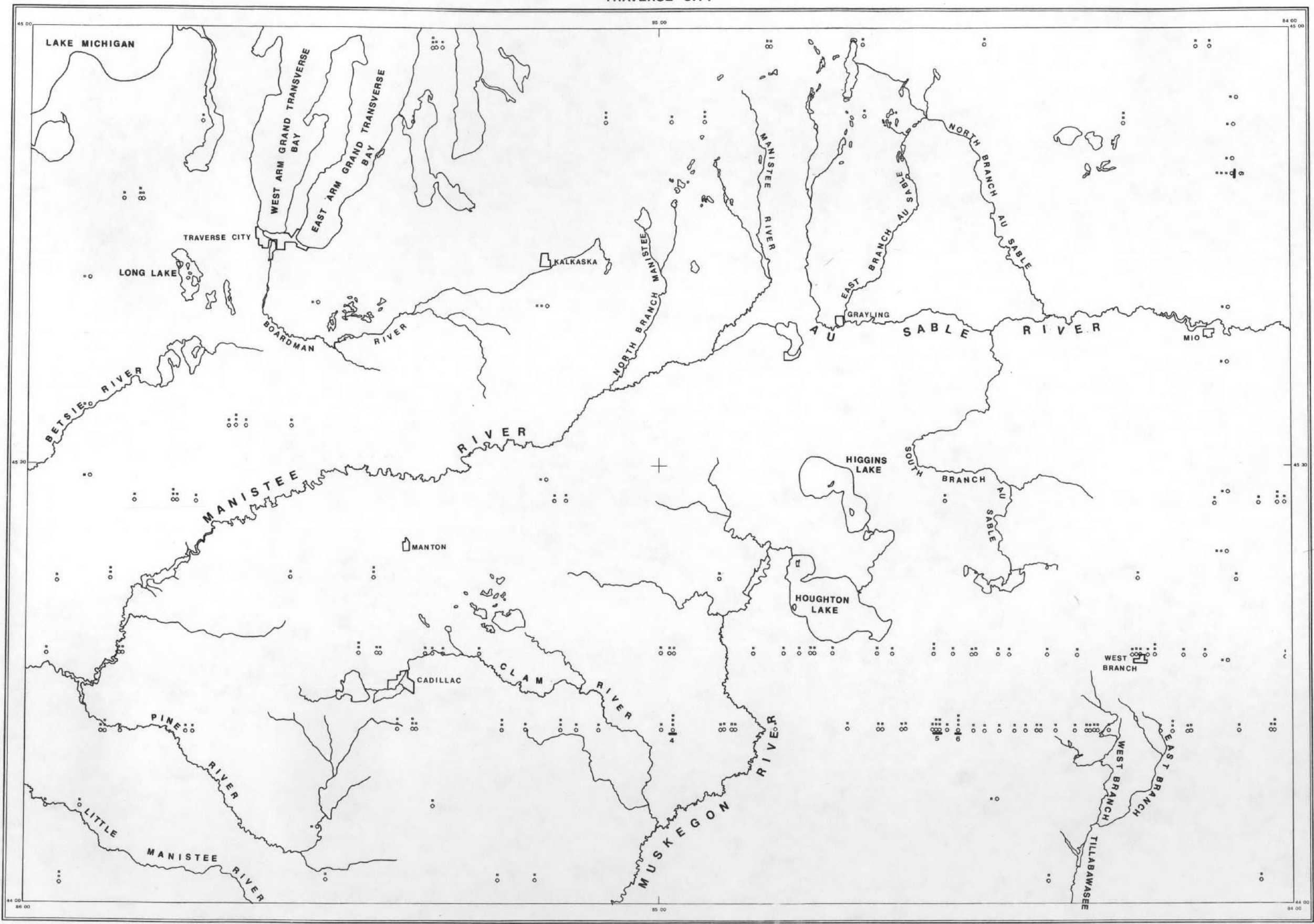
- - CITY OR TOWN
- - URANIUM SAMPLE MEETING FOLLOWING CRITERIA:
 - (1) $1.0 \leq U \leq \infty$
 - (2) $-1.0 \leq T \leq \infty$
 - (3) $1.0 \leq U/T \leq \infty$
- IN STANDARD DEVIATION UNITS.
EACH SQUARE REPRESENTS 1 STANDARD DEVIATION.
- - URANIUM ANOMALY:
A SINGLE SAMPLE OF 3 OR MORE STANDARD DEVIATIONS OR GROUP OF ADJOINING SAMPLES WHICH TOGETHER TOTAL 4 OR MORE STANDARD DEVIATIONS, $4.0 \leq \text{sum} \leq \infty$, WITH AT LEAST ONE SAMPLE OF 2 OR MORE STANDARD DEVIATIONS.

SURVEY AND
COMPILED BY:

EG&G GEOMETRICS

Figure 3 - Uranium Anomaly/Interpretation Map - Manitowoc Quadrangle

TRAVERSE CITY



URANIUM ANOMALY/
INTERPRETATION MAP

TRAVERSE CITY QUADRANGLE
U.S. DEPARTMENT OF ENERGY

APPROXIMATE SCALE 1:500,000

EXPLANATION

- - CITY OR TOWN
- - URANIUM SAMPLE MEETING FOLLOWING CRITERIA:
 - (1) $1.0 \leq U \leq \infty$
 - (2) $-1.0 \leq T \leq \infty$
 - (3) $1.0 \leq U/T \leq \infty$
- IN STANDARD DEVIATION UNITS. EACH SQUARE REPRESENTS 1 STANDARD DEVIATION.
- ◻ - URANIUM ANOMALY: A SINGLE SAMPLE OF 3 OR MORE STANDARD DEVIATIONS OR GROUP OF ADJOINING SAMPLES WHICH TOGETHER TOTAL 4 OR MORE STANDARD DEVIATIONS, $4.0 \leq \text{SUM} \leq \infty$, WITH AT LEAST ONE SAMPLE OF 2 OR MORE STANDARD DEVIATIONS.

SURVEY AND
COMPILED BY:
EG&G GEOMETRICS

Figure 3a - Uranium Anomaly/Interpretation Map - Traverse City Quadrangle

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**APPENDIX A - Data Acquisition, Processing, and
Interpretation Methods**

INTRODUCTION

General

Under the U.S. Department of Energy's (DoE), National Uranium Resource Evaluation (NURE) Program, geoMetrics, Inc., conducted a high sensitivity airborne radiometric and magnetic survey. The data collection and processing were conducted under requirements set forth in Bendix Field Engineering Corporation specification 1200-C, dated February, 1979. The objectives of the (DoE)/NURE program, of which this project is a small part, may be summarized as follows:

"To develop and compile geologic and other information with which to assess the magnitude and distribution of uranium resources and to determine areas favorable for the occurrence of uranium in the United States." (DoE)

As an integral part of the DoE/NURE Program, the National Airborne Radiometric Program is designed to provide cost effective, semiquantitative reconnaissance radio element distribution information to aid in the assessment of regional distribution of uraniferous materials within the United States.

All Airborne data collected by geoMetrics during the course of this project were done so utilizing a Beechcraft B65 Queen Air Airplane (U.S. Registry No. N9AG) and a Rockwell Aero Commander (Registry No. N1213B). Both aircraft used 3584 cubic inches of NaI crystal and a high sensitivity proton magnetometer (0.25 gamma).

Each report contains a detailed geologic summary, interpretation report, reduced scale copies of all maps and profiles, histograms, and statistical tables for each quadrangle contained within the project. In addition, each report contains an appendix detailing the survey description, specifications, data collection and processing methods, and interpretation methods.

All data processing, statistical analyses, and interpretation were performed at the geoMetrics computer facility, Sunnyvale, California. After processing, the corrected data were statistically evaluated to define those areas which were radiometrically anomalous relative to other areas within each computer map unit. Standard deviation maps and radiometric and magnetic profile data were first evaluated individually and then integrated into a final interpretation map for each NTMS quadrangle.

Corrected profiles of all radiometric variables (total count, potassium, uranium, thorium, uranium/thorium, uranium/potassium, and thorium

/potassium, ratios), magnetic data, radar altimeter data, barometric altimeter data, air temperature, and airborne bismuth contributions are presented as profiles in this report. Single record and averaged data are presented on microfiche in report. These data are given at 1.0 second sample intervals, corrected for Compton Scatter, referenced to 400 foot mean terrain clearance as Standard Temperature and Pressure and corrected for atmospheric bismuth. Digital magnetic tapes are available containing raw spectral data, single record data, magnetic data, and statistical analysis results.

OPERATIONS

PRODUCTION SUMMARY

The production summary presented below describes the general procedures involved in gathering data for the entire project. The detailed daily production summary in Appendix B describes a portion of the total project.

Prior to the start of the survey operations, the airplanes were calibrated at the DoE test pads and Dynamic Test Range (the Queen Air in April 1980, and the Aero Commander in October 1980). Requirements for system calibrations are listed in the 1250-A specifications from BFEC.

Throughout the course of the overall project, the average ground speed maintained by the Queen Air was 140 mph. The Aero Commander averaged 150 mph.

Nearly 100% of the data collected were within the specification limits of 200-700 feet. Several deviations over short distances were required to meet military regulations, FAA safety requirements, and to ensure that livestock were not endangered due to low flying aircraft. A sample altitude statistical distribution is shown in Figure I.

DATA COLLECTION PROCEDURES

Operating Parameters/Sampling Procedures

This survey was conducted using data collection parameters summarized below:

1. Data sampling was performed by a time-base system using 1.0 second sample intervals. All sensor data with analog output were digitally sampled at each scan based upon the clock timing rate of 1.0 seconds. The data so collected are the instantaneous values of the altimeter, temperature, pressure, and magnetometer parameters determined at the time of the data scan, but represent a count time of 1.0 seconds for the gamma ray spectrometer data.
2. The airplanes' objective ground speeds, mentioned previously, were not exceeded unless dictated by safety.
3. The airplane's downward looking crystal volume was 3,072 cubic inches providing an objective V/V (crystal volume in cubic inches divided by ground speed in miles per hour) of 22.0 at 140 m.p.h.
4. The upward looking crystal volume was 512 cubic inches.

NUMBER OF OCCURRENCES

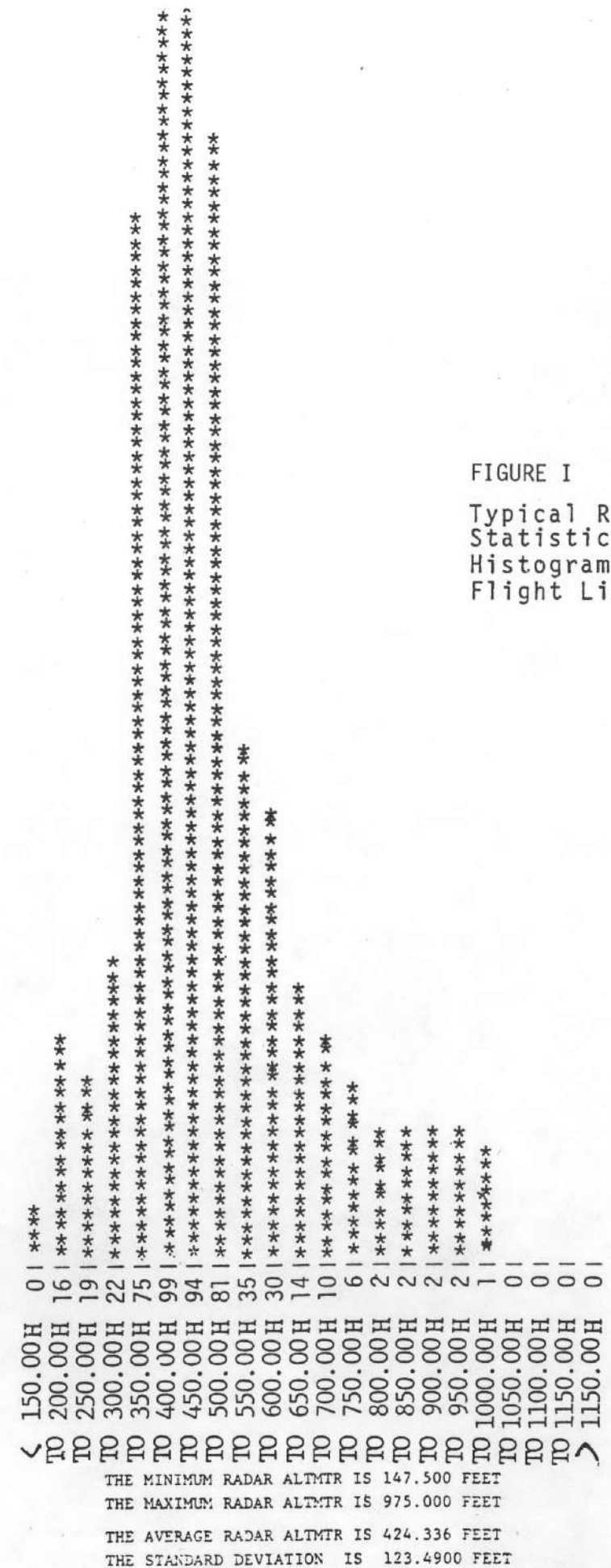


FIGURE I
Typical Radar Altimeter
Statistical Summary
Histogram for Single
Flight Line

Navigation/Flight Path Recovery

For all of the quadrangles, profiles were flown east-west at 6 mile (9.6 km) spacing. North-south tie lines were flown at 18 mile (28.8 km) spacing.

Navigation was accomplished using visual navigation techniques. Flight lines were drawn on 1:250,000 quadrangles and the pilot/navigator utilized these maps to provide visual navigation features.

Simultaneously, a 35 mm tracking camera was used to record actual flight position. This camera's fiducial numbering system was directly synchronized to the digital recording system such that a one-to-one correlation between position and data could be made. Upon completion of a data collection flight, the 35 mm film was processed and actual flight path positions located on the appropriate scale map sheets.

Infield System Calibration

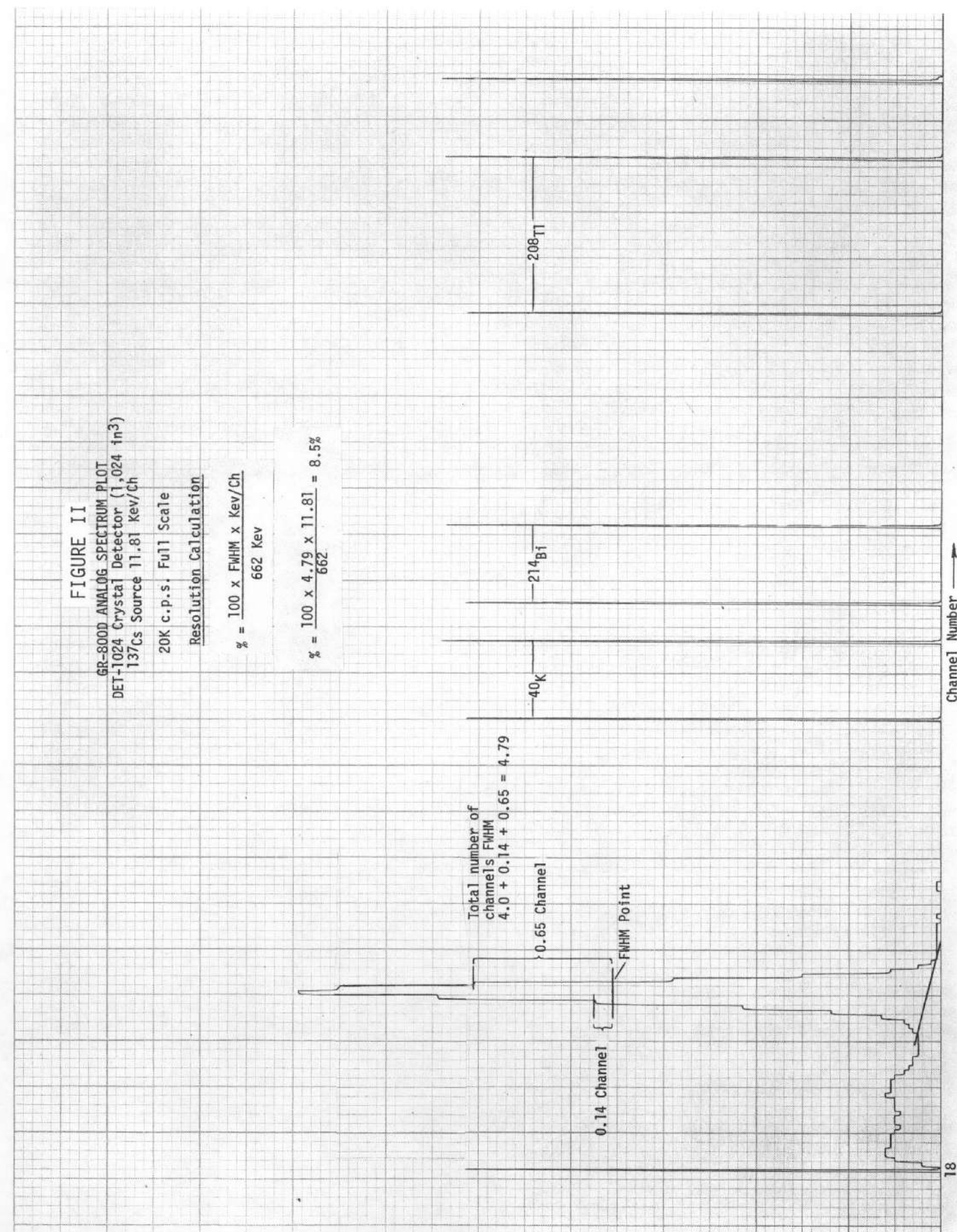
Due to the complex nature of both the system and the required data interpretation, much emphasis was placed on infield calibration of the data collection system. The objective of this calibration was to ensure continuous high quality of the data collected. The daily calibration procedures used are summarized below:

A. Pre Flight

1. Use cesium sources (same positioning on crystals every day), peak each Photomultiplier tube/crystal using the digital split-window detector of the GR-800. Then using thallium sources, repeat the tuning of the individual crystals.
2. Run full cesium spectrum on analog recorder for both down and up looking crystals. Calculate the cesium resolution (see sample in Figure II). Run spectrum out past the K40 peak on down crystals for evaluation of system tuning.
3. Finally run a full thorium analog spectrum of the down crystals and check for centering of K40 and Tl208 peaks in spectrum.
4. Repeat 1-3 until system is within contract specifications.

B. During Flight

1. Fly test line at survey altitude (400 ft), for approximately five miles, prior to production data collection (record both analog and digital).
2. Prior to production data collection, the above data are evaluated to ensure +20% limits on total count compared to average of all test flights from that base of operations.



DATA COLLECTION SYSTEM

AIRCRAFT

Two aircraft were used for this survey: (1) a Beechcraft Queen Air - Model 65 (U.S. Reg. No. N9AG), and (2) a Rockwell Aero Commander 680F (U.S. Reg. No. N1213B). Both these aircraft, being medium size with twin engines, possess overall performance and safety features which make them ideal for low level, fixed-wing airborne geophysical surveys in areas of up to moderately high topographic relief. They can carry adequate payloads at low constant airspeeds, while maintaining economy and a wide envelope of safety. Performance data for the two craft in their present survey configuration are given below.

	<u>QUEEN AIR</u>	<u>AERO COMMANDER</u>
Maximum Aircraft Gross Weight	7,700 lbs.	8,500 lbs.
Aircraft Empty (dry)	4,640 lbs.	5,200 lbs.
Max. useful load including fuel	3,060 lbs.	3,300 lbs.
Geophysical Package	1,110 lbs.	1,110 lbs.
Navigation Equipment	125 lbs.	125 lbs.
Fuel Tanks Full	1,380 lbs.	1,338 lbs.
Pilot & Electronics Operator	350 lbs.	350 lbs.
Total	2,965 lbs.	2,923 lbs.
Min. Control Speed at G.W. (IAS)	95 mph	NG
Safe Single Eng. Speed @ G.W. (IAS)	105 mph	NG
Rate of Climb 2 engines @ gross (FPM)	1,300	1,500
Rate of climb 1 engine @ gross (FPM)	210	250
Avgas consumption (ga/hr) at 75% power	36	38
Endurance (75% power)	6 hrs/6 mins.	5 hrs/30 mins.
Range (75% power - 45 min. reserve)	1,200 miles	1,100 miles
Cruise Configuration stalling speed at gross weight (IAS)		
0° bank	80 mph	80 mph
45° bank	95 mph	NG

3. During production data collection, monitor radon analog data for unusual increases. Visually correlate these with temperature and barometric pressure.
4. Upon completion of production data collection, re-fly test line at survey altitude (400 ft). Record both analog and digital.

C. Post Flight

1. Verify test line total count within 20% of average for all test lines at that base of operations.
2. Using cesium sources (same position as pre-flight), run full cesium spectrum for both down and up crystals (allow it to record through the K40 peak in the down crystals). Repeat the procedure using thallium sources and examine the T1208 window.
3. Calculate the resolution of down and up crystal pack.
4. Determine shift, if any, in T1208 peak position.

Field Digital Data Verification

At the completion of each flight, the raw digital data tapes were checked for data quality and completeness on geoMetrics' G-725. The G-725 system is a totally portable mini computer (and peripherals) consisting of; an Interdata 516, two 9 track tape drives, a CRT, a line printer, and two floppy discs. Any digital problems encountered were immediately evaluated by the electronics operator and data man, thus assuring optimum data quality. In addition, histogram information for each measured variable was generated. Thus a summary display of altitude, etc., is available for immediate evaluation.

Electronics

The major components of the airborne data collection system are summarized below (shown schematically in Figure III):

1. Gamma Ray Spectrometer, geoMetrics GR-800, utilizing a dual 256 channel capability to provide spectral data in the 0.4 to 3.0 MeV range for both the downward looking and the upward looking crystal packages and coverage in the 3.0 to 6.0 MeV range for cosmic background.
2. Crystal Detector, geoMetrics Model DET-3072/512R consisting of 3072 cubic inches in the downward looking configuration and 512 cubic inches appropriately shielded in an upward looking configuration.
3. A geoMetrics Digital Data Acquisition System, Model G-714 with "read-after-write" data verification, recording the following on magnetic tape:
 - a. 512 channels of gamma ray spectrometer data
 - b. Total magnetic intensity
 - c. Fiducial number from data system/camera
 - d. Manually inserted information, i.e. date, survey area, and flight line number
 - e. Altitude from radar altimeter and barometric altimeter (by analog-to-digital conversion)
 - f. Time in days, hours, minutes and seconds
 - g. Outside air temperature
4. Magnetometer, geoMetrics Airborne Model G-803, capable of 0.125 gamma sensitivity, but operated at 0.25 gamma sensitivity.
5. Radar Altimeter, Bonzer Model Mark 10 with recording output and display operating over an altitude range of 0 to 2,500 feet.
6. Rosemont Barometric Altimeter with recording output and display.
7. Recording Thermometer for monitoring outside air temperature.
8. Tracking Camera. Automax 35 mm framing camera with wide angle lens and 10 character fiducial/line number display to provide flight path recovery data.

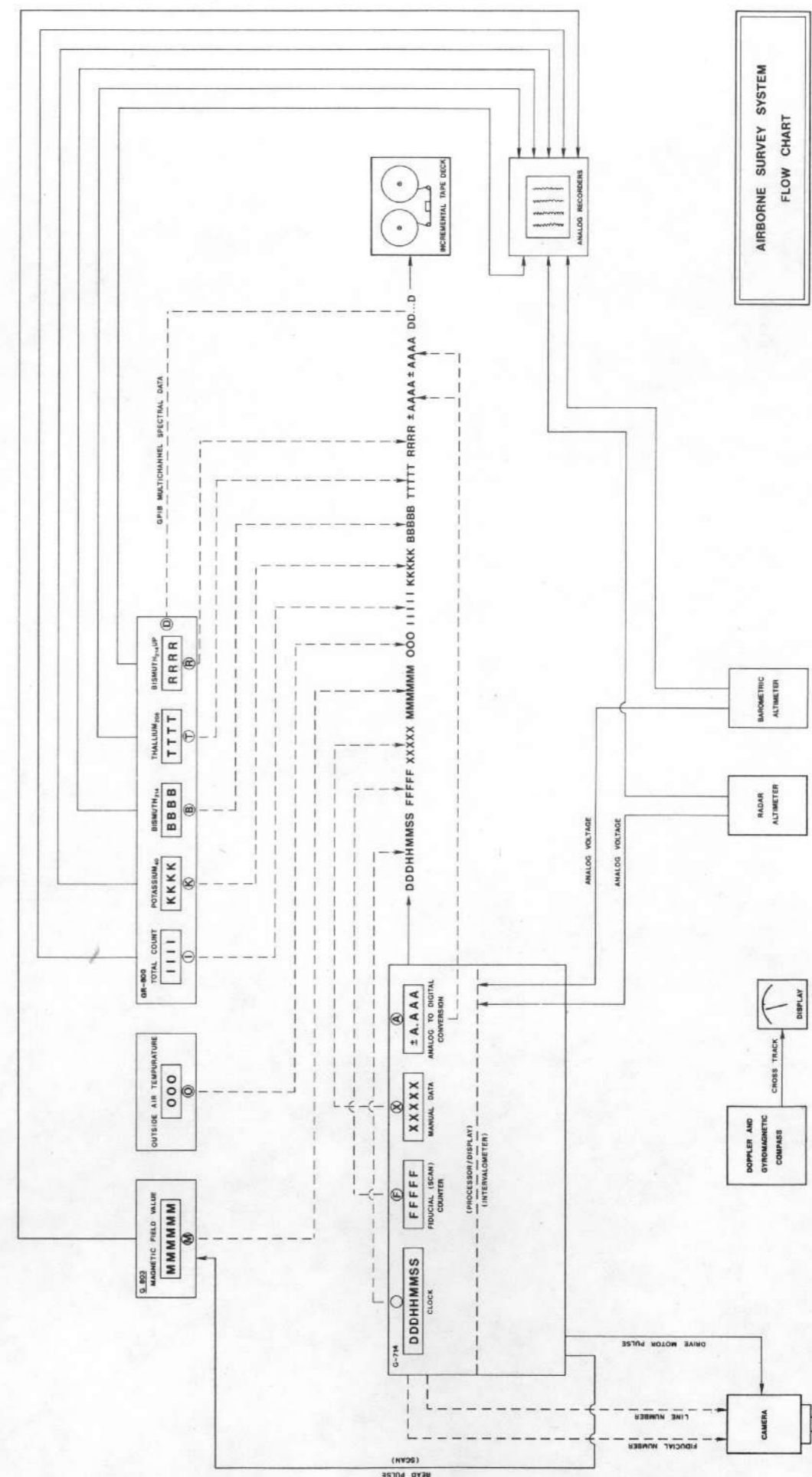


FIGURE III

SYSTEM CALIBRATION

9. Analog Recorder geoMetrics (MARS 6) to record the following data:
- Bi214 using a window about the 1.76 MeV peak from the downward looking system.
 - Bi air background from the upward looking system.
 - Magnetometer
 - Radar Altitude
 - Total count for downward looking system (0.4 to 3.0 MeV)
 - Barometric Altitude
 - Time markers
10. HP 7155 single channel analog recorder during pre and post flight calibrations, this recorder is used to plot a full analog spectra for both the down and up crystal systems via the GR-800. Thus, a hard copy record of the data used for resolution, drift, etc., checks are available at all times. This approach provides instant verification of system parameters (refer to Figure II).

AIRCRAFT AND COSMIC BACKGROUND

Full spectral data are collected at five (5) altitudes over water (14,000 feet, 12,000 feet; 10,000 feet; 8,000 feet and 6,000 feet) in an area where the existence of no airborne Bi214 can be assured (off shore over the Pacific Ocean). This results in separate spectra as shown schematically in Figure 10. We define $S(12,000)$ to be the spectra at 12,000 feet from 0.4 MeV to 3.0 MeV with $S(8,000)$ the same spectra at a lower altitude (8,000) and $C_i(h)$ the total count between 3.0 and 6.0 MeV at respective altitudes.¹ Since the aircraft background is constant, the difference between any two altitudes separated sufficiently - typically, 2,000 feet - yields the cosmic spectral curve shape as shown schematically in Figure VI. Thus

$$S(12,000) - S(8,000) = \Delta S$$

and

$$\sum C_{12}(h_i) - \sum C_8(h_i) = \Delta C$$

This cosmic spectral curve is scaled back to 12,000 feet as follows:

$$\frac{C_{12}(h_i)}{\Delta C} \times \Delta S = \Delta C(12,000) \text{ the Cosmic Spectrum (shape and magnitude at 12,000 feet)}$$

The aircraft background is derived as follows:

$$S(12,000) - C(12,000) = A/C \text{ Background}$$

Since data were collected at five altitudes, this procedure was repeated for each combination of altitudes and results averaged. Typical aircraft and cosmic spectra are shown in Figures V, AND VI respectively.

SYSTEM CONSTANTS

System constants were determined by occupation of the DoE Walker Field Test Pads. (See Ward, 1978, and Stromswold, 1978, for complete descriptions of the building and monitoring of the pads). The five test pads contained varying concentrations of K, U, and T as presented by BFEC:

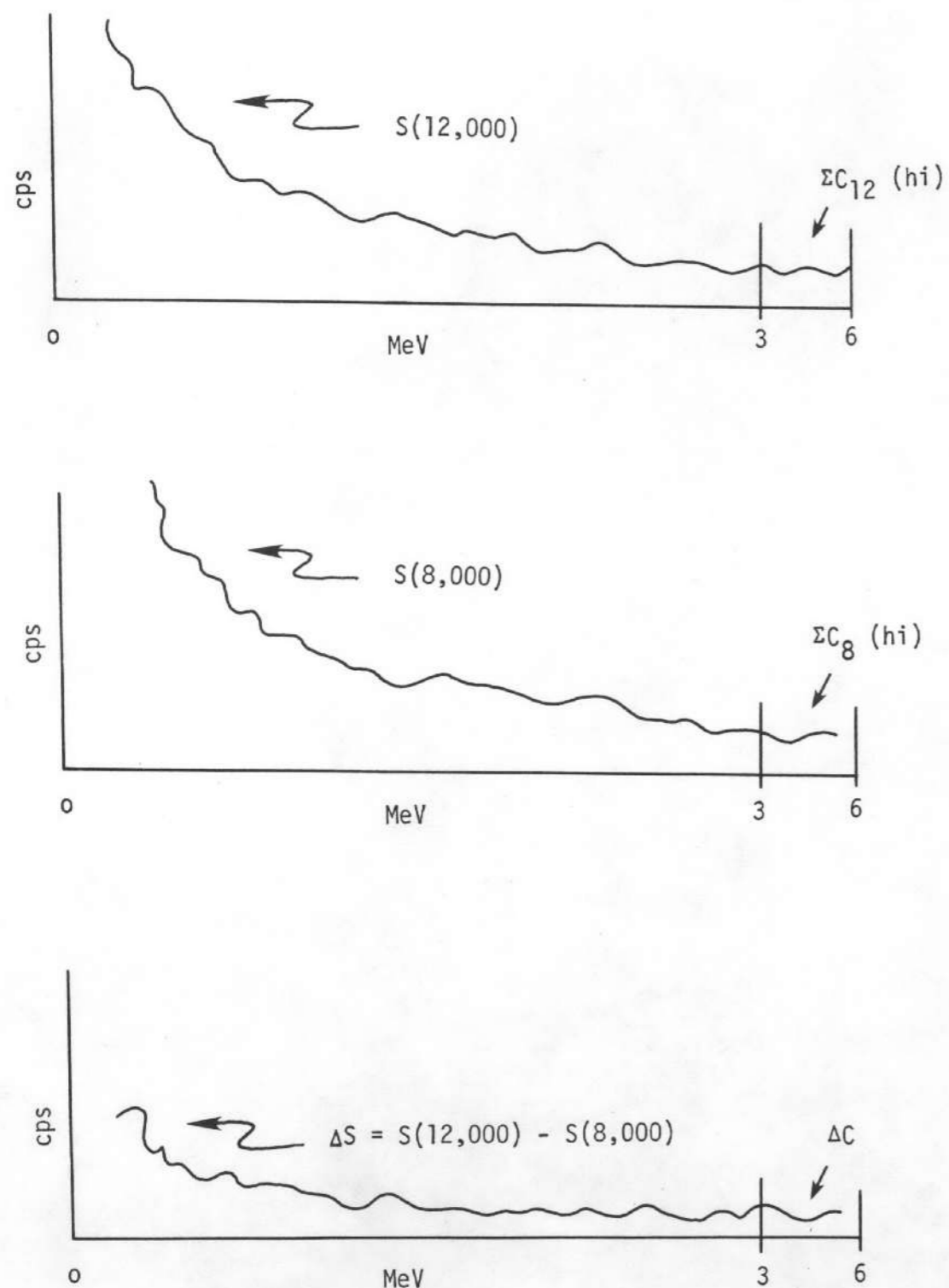


FIGURE IV - Multiple altitude spectra schematic

<u>PAD</u>	<u>K</u>	<u>U</u>	<u>I</u>
Matrix	1.45%	2.19 ppm	6.26 ppm
K	5.14%	5.09 ppm	8.48 ppm
U	2.03%	30.29 ppm	9.19 ppm
T	2.01%	5.14 ppm	45.33 ppm
Mixed	4.11%	20.39 ppm	17.52 ppm

Since the measurements were taken over a relatively short time period (a few hours), it was assumed that the matrix pad measurements contain not only the effects of the matrix pad itself, but also aircraft background (which is a constant), cosmic background (constant over the time period of interest), and all other local background (e.g. BiAir, etc.) effects. (The matrix pad is constructed with only the basic concrete mix without the additional elemental minerals). Thus, by subtracting the matrix pad count rates from the count rates in the four pads, we have eliminated aircraft and cosmic background and BiAir effects for the four pads. The pad concentrations are then modified in a similar fashion by the subtraction of the matrix pad concentrations. The differential concentrations in the pads are given in the table below.

<u>PAD</u>	<u>K</u>	<u>U</u>	<u>I</u>
K-Matrix	3.7%	2.9 ppm	2.2 ppm
U-Matrix	0.6%	28.5 ppm	2.9 ppm
T-Matrix	0.6%	3.0 ppm	39.0 ppm
Mixed-Matrix	2.7%	18.8 ppm	11.3 ppm

Considering the above, we can define a functional relationship between the differential concentrations and the residual count rates which will provide a method of determining the calibration constants for the spectrometer system. These calibration constants are the six (6) stripping coefficients which account for the interactions occurring between the elemental channels in the system (Compton scatter coefficients, etc.).

On the basis of an ideal situation, one would anticipate that some of these interactions should be negligible. This is not totally the case, since we are dealing with a system which has less than infinite resolving power (i.e. the energies are smeared to some extent).

DERIVED AIRCRAFT BACKGROUND SPECTRUM FROM PACIFIC OCEAN DATA

DOWNWARD-LOOKING CRYSTAL SPECTRUM FOR LINE AC BGD, DATED 072577

TC (0-6 MEV) 184.97 TC (0.4-3.0 MEV) 141.17 COSMIC (3-6 MEV) 0.00
 U (1.1E MEV) 9.91 K (1.4E MEV) 14.54 U (1.7E MEV) 4.36 T (2.6E MEV) 4.20

AIRCRAFT BACKGROUND
 ROTARY WING AIRCRAFT
 DOWNWARD LOOKING CRYSTAL
 2048 CUBIC INCHES
 DATE: 25 JULY 1977

CH 0 (0.000 MEV)	0.000 CPS I
CH 1 (0.012 MEV)	0.000 CPS I
CH 2 (0.024 MEV)	0.000 CPS I
CH 3 (0.036 MEV)	0.000 CPS I
CH 4 (0.047 MEV)	0.000 CPS I
CH 5 (0.059 MEV)	0.000 CPS I
CH 6 (0.071 MEV)	0.000 CPS I
CH 7 (0.083 MEV)	0.000 CPS I
CH 8 (0.095 MEV)	0.000 CPS I
CH 9 (0.107 MEV)	0.000 CPS I
CH 10 (0.118 MEV)	0.000 CPS I
CH 11 (0.130 MEV)	0.000 CPS I
CH 12 (0.142 MEV)	0.000 CPS I
CH 13 (0.154 MEV)	0.000 CPS I
CH 14 (0.165 MEV)	0.000 CPS I
CH 15 (0.177 MEV)	0.000 CPS I
CH 16 (0.189 MEV)	0.000 CPS I
CH 17 (0.201 MEV)	0.000 CPS I
CH 18 (0.213 MEV)	-0.000 CPS I
CH 19 (0.225 MEV)	-0.000 CPS I
CH 20 (0.236 MEV)	0.000 CPS I
CH 21 (0.248 MEV)	0.000 CPS I
CH 22 (0.260 MEV)	3.795 CPS I
CH 23 (0.272 MEV)	4.200 CPS I
CH 24 (0.284 MEV)	4.334 CPS I
CH 25 (0.295 MEV)	3.748 CPS I
CH 26 (0.307 MEV)	3.897 CPS I
CH 27 (0.319 MEV)	3.318 CPS I
CH 28 (0.331 MEV)	4.236 CPS I
CH 29 (0.343 MEV)	2.433 CPS I
CH 30 (0.355 MEV)	2.996 CPS I
CH 31 (0.366 MEV)	2.559 CPS I
CH 32 (0.378 MEV)	2.263 CPS I
CH 33 (0.390 MEV)	2.192 CPS I
CH 34 (0.402 MEV)	2.081 CPS I
CH 35 (0.414 MEV)	2.121 CPS I
CH 36 (0.426 MEV)	2.114 CPS I
CH 37 (0.437 MEV)	1.976 CPS I
CH 38 (0.449 MEV)	2.096 CPS I
CH 39 (0.461 MEV)	2.188 CPS I
CH 40 (0.473 MEV)	2.228 CPS I
CH 41 (0.485 MEV)	2.158 CPS I
CH 42 (0.496 MEV)	2.185 CPS I
CH 43 (0.508 MEV)	2.158 CPS I
CH 44 (0.520 MEV)	2.217 CPS I
CH 45 (0.532 MEV)	2.217 CPS I
CH 46 (0.544 MEV)	1.997 CPS I
CH 47 (0.556 MEV)	1.477 CPS I
CH 48 (0.567 MEV)	2.548 CPS I
CH 49 (0.579 MEV)	2.588 CPS I
CH 50 (0.591 MEV)	2.798 CPS I
CH 51 (0.603 MEV)	2.481 CPS I
CH 52 (0.615 MEV)	2.378 CPS I
CH 53 (0.626 MEV)	1.966 CPS I
CH 54 (0.638 MEV)	1.882 CPS I
CH 55 (0.650 MEV)	1.661 CPS I
CH 56 (0.662 MEV)	1.480 CPS I
CH 57 (0.674 MEV)	1.474 CPS I
CH 58 (0.686 MEV)	1.447 CPS I
CH 59 (0.697 MEV)	1.431 CPS I
CH 60 (0.709 MEV)	1.476 CPS I
CH 61 (0.721 MEV)	1.483 CPS I
CH 62 (0.733 MEV)	1.467 CPS I
CH 63 (0.745 MEV)	1.579 CPS I
CH 64 (0.756 MEV)	1.497 CPS I
CH 65 (0.768 MEV)	1.548 CPS I
CH 66 (0.780 MEV)	1.481 CPS I
CH 67 (0.792 MEV)	1.428 CPS I
CH 68 (0.804 MEV)	1.155 CPS I
CH 69 (0.816 MEV)	1.246 CPS I
CH 70 (0.827 MEV)	1.245 CPS I
CH 71 (0.839 MEV)	1.161 CPS I
CH 72 (0.851 MEV)	1.253 CPS I
CH 73 (0.863 MEV)	1.231 CPS I
CH 74 (0.875 MEV)	1.425 CPS I
CH 75 (0.887 MEV)	1.452 CPS I
CH 76 (0.899 MEV)	1.543 CPS I
CH 77 (0.910 MEV)	1.444 CPS I
CH 78 (0.922 MEV)	1.364 CPS I
CH 79 (0.934 MEV)	1.299 CPS I
CH 80 (0.946 MEV)	1.159 CPS I
CH 81 (0.957 MEV)	1.144 CPS I
CH 82 (0.969 MEV)	1.085 CPS I
CH 83 (0.981 MEV)	1.061 CPS I
CH 84 (0.993 MEV)	0.941 CPS I
CH 85 (1.005 MEV)	0.919 CPS I
CH 86 (1.017 MEV)	0.822 CPS I
CH 87 (1.028 MEV)	0.816 CPS I
CH 88 (1.040 MEV)	0.853 CPS I
CH 89 (1.052 MEV)	0.981 CPS I
CH 90 (1.064 MEV)	0.828 CPS I
CH 91 (1.076 MEV)	0.867 CPS I
CH 92 (1.087 MEV)	0.968 CPS I
CH 93 (1.099 MEV)	0.851 CPS I
CH 94 (1.111 MEV)	0.905 CPS I
CH 95 (1.123 MEV)	0.847 CPS I
CH 96 (1.135 MEV)	0.861 CPS I
CH 97 (1.147 MEV)	0.800 CPS I
CH 98 (1.158 MEV)	0.727 CPS I
CH 99 (1.170 MEV)	0.751 CPS I
CH 100 (1.182 MEV)	0.607 CPS I
CH 101 (1.194 MEV)	0.663 CPS I
CH 102 (1.206 MEV)	0.657 CPS I
CH 103 (1.217 MEV)	0.633 CPS I
CH 104 (1.229 MEV)	0.719 CPS I
CH 105 (1.241 MEV)	0.671 CPS I
CH 106 (1.253 MEV)	0.475 CPS I
CH 107 (1.265 MEV)	0.601 CPS I
CH 108 (1.277 MEV)	0.681 CPS I
CH 109 (1.289 MEV)	0.649 CPS I
CH 110 (1.300 MEV)	0.686 CPS I
CH 111 (1.312 MEV)	0.638 CPS I
CH 112 (1.324 MEV)	0.652 CPS I
CH 113 (1.336 MEV)	0.644 CPS I
CH 114 (1.347 MEV)	0.652 CPS I
CH 115 (1.359 MEV)	0.791 CPS I
CH 116 (1.371 MEV)	0.787 CPS I
CH 117 (1.383 MEV)	0.834 CPS I
CH 118 (1.395 MEV)	0.984 CPS I
CH 119 (1.407 MEV)	1.076 CPS I
CH 120 (1.418 MEV)	1.124 CPS I
CH 121 (1.430 MEV)	1.088 CPS I
CH 122 (1.442 MEV)	1.218 CPS I
CH 123 (1.454 MEV)	1.231 CPS I
CH 124 (1.466 MEV)	1.207 CPS I
CH 125 (1.477 MEV)	0.926 CPS I
CH 126 (1.489 MEV)	0.967 CPS I
CH 127 (1.501 MEV)	0.664 CPS I
CH 128 (1.513 MEV)	0.635 CPS I
CH 129 (1.525 MEV)	0.512 CPS I
CH 130 (1.537 MEV)	0.488 CPS I
CH 131 (1.548 MEV)	0.480 CPS I
CH 132 (1.560 MEV)	0.360 CPS I
CH 133 (1.572 MEV)	0.339 CPS I
CH 134 (1.584 MEV)	0.318 CPS I
CH 135 (1.596 MEV)	0.310 CPS I
CH 136 (1.608 MEV)	0.259 CPS I
CH 137 (1.619 MEV)	0.259 CPS I
CH 138 (1.631 MEV)	0.353 CPS I
CH 139 (1.643 MEV)	0.323 CPS I
CH 140 (1.655 MEV)	0.232 CPS I
CH 141 (1.667 MEV)	0.326 CPS I
CH 142 (1.678 MEV)	0.267 CPS I
CH 143 (1.690 MEV)	0.276 CPS I
CH 144 (1.702 MEV)	0.245 CPS I
CH 145 (1.714 MEV)	0.347 CPS I
CH 146 (1.726 MEV)	0.388 CPS I
CH 147 (1.738 MEV)	0.293 CPS I
CH 148 (1.749 MEV)	0.355 CPS I
CH 149 (1.761 MEV)	0.279 CPS I
CH 150 (1.773 MEV)	0.334 CPS I
CH 151 (1.785 MEV)	0.245 CPS I
CH 152 (1.797 MEV)	0.255 CPS I
CH 153 (1.808 MEV)	0.174 CPS I
CH 154 (1.820 MEV)	0.228 CPS I
CH 155 (1.832 MEV)	0.188 CPS I
CH 156 (1.844 MEV)	0.115 CPS I
CH 157 (1.856 MEV)	0.084 CPS I
CH 158 (1.868 MEV)	0.147 CPS I
CH 159 (1.879 MEV)	0.147 CPS I
CH 160 (1.891 MEV)	0.139 CPS I
CH 161 (1.903 MEV)	0.109 CPS I
CH 162 (1.915 MEV)	0.091 CPS I
CH 163 (1.927 MEV)	0.151 CPS I
CH 164 (1.938 MEV)	0.088 CPS I
CH 165 (1.950 MEV)	0.136 CPS I
CH 166 (1.962 MEV)	0.157 CPS I
CH 167 (1.974 MEV)	0.119 CPS I
CH 168 (1.986 MEV)	0.199 CPS I
CH 169 (1.998 MEV)	0.113 CPS I
CH 170 (2.009 MEV)	0.186 CPS I
CH 171 (2.021 MEV)	0.147 CPS I
CH 172 (2.033 MEV)	0.173 CPS I
CH 173 (2.045 MEV)	0.171 CPS I
CH 174 (2.057 MEV)	0.154 CPS I
CH 175 (2.069 MEV)	0.148 CPS I
CH 176 (2.080 MEV)	0.162 CPS I
CH 177 (2.092 MEV)	0.184 CPS I
CH 178 (2.104 MEV)	0.138 CPS I
CH 179 (2.116 MEV)	0.137 CPS I
CH 180 (2.128 MEV)	0.119 CPS I
CH 181 (2.139 MEV)	0.189 CPS I
CH 182 (2.151 MEV)	0.148 CPS I
CH 183 (2.163 MEV)	0.181 CPS I
CH 184 (2.175 MEV)	0.114 CPS I
CH 185 (2.187 MEV)	0.088 CPS I
CH 186 (2.199 MEV)	0.091 CPS I
CH 187 (2.210 MEV)	0.085 CPS I
CH 188 (2.222 MEV)	0.136 CPS I
CH 189 (2.234 MEV)	0.117 CPS I
CH 190 (2.246 MEV)	0.113 CPS I
CH 191 (2.258 MEV)	0.118 CPS I
CH 192 (2.270 MEV)	0.088 CPS I
CH 193 (2.281 MEV)	0.097 CPS I
CH 194 (2.293 MEV)	0.095 CPS I
CH 195 (2.305 MEV)	0.087 CPS I
CH 196 (2.317 MEV)	0.059 CPS I
CH 197 (2.329 MEV)	0.115 CPS I
CH 198 (2.340 MEV)	0.041 CPS I
CH 199 (2.352 MEV)	0.070 CPS I
CH 200 (2.364 MEV)	0.087 CPS I
CH 201 (2.376 MEV)	0.085 CPS I
CH 202 (2.388 MEV)	0.084 CPS I
CH 203 (2.399 MEV)	0.086 CPS I
CH 204 (2.411 MEV)	0.123 CPS I
CH 205 (2.423 MEV)	0.076 CPS I
CH 206 (2.435 MEV)	0.115 CPS I
CH 207 (2.447 MEV)	0.147 CPS I
CH 208 (2.459 MEV)	0.188 CPS I
CH 209 (2.471 MEV)	0.129 CPS I
CH 210 (2.482 MEV)	0.092 CPS I
CH 211 (2.494 MEV)	0.127 CPS I
CH 212 (2.506 MEV)	0.160 CPS I
CH 213 (2.518 MEV)	0.206 CPS I
CH 214 (2.530 MEV)	0.262 CPS I
CH 215 (2.542 MEV)	0.184 CPS I
CH 216 (2.553 MEV)	0.206 CPS I
CH 217 (2.565 MEV)	0.195 CPS I
CH 218 (2.577 MEV)	0.173 CPS I
CH 219 (2.589 MEV)	0.201 CPS I
CH 220 (2.601 MEV)	0.229 CPS I
CH 221 (2.612 MEV)	0.232 CPS I
CH 222 (2.624 MEV)	0.187 CPS I
CH 223 (2.636 MEV)	0.171 CPS I
CH 224 (2.648 MEV)	0.177 CPS I
CH 225 (2.660 MEV)	0.089 CPS I
CH 226 (2.672 MEV)	0.184 CPS I
CH 227 (2.683 MEV)	0.124 CPS I
CH 228 (2.695 MEV)	0.131 CPS I
CH 229 (2.707 MEV)	0.098 CPS I
CH 230 (2.719 MEV)	0.027 CPS I
CH 231 (2.730 MEV)	0.012 CPS I
CH 232 (2.742 MEV)	-0.026 CPS I
CH 233 (2.754 MEV)	-0.024 CPS I
CH 234 (2.766 MEV)	0.038 CPS I
CH 235 (2.778 MEV)	0.093 CPS I
CH 236 (2.790 MEV)	0.060 CPS I
CH 237 (2.801 MEV)	0.038 CPS I
CH 238 (2.813 MEV)	0.062 CPS I
CH 239 (2.825 MEV)	0.098 CPS I
CH 240 (2.837 MEV)	0.078 CPS I
CH 241 (2.849 MEV)	0.078 CPS I
CH 242 (2.860 MEV)	0.047 CPS I
CH 243 (2.872 MEV)	0.084 CPS I
CH 244 (2.884 MEV)	0.084 CPS I
CH 245 (2.896 MEV)	0.025 CPS I
CH 246 (2.908 MEV)	0.025 CPS I
CH 247 (2.920 MEV)	-0.015 CPS I
CH 248 (2.931 MEV)	0.037 CPS I
CH 249 (2.943 MEV)	-0.005 CPS I
CH 250 (2.955 MEV)	0.042 CPS I
CH 251 (2.967 MEV)	0.062 CPS I
CH 252 (2.979 MEV)	-0.018 CPS I
CH 253 (2.990 MEV)	0.031 CPS I
CH 254 (3.002 MEV)	-0.002 CPS I
CH 255 (3.014 MEV)	0.000 CPS I

FIGURE V

Thus, energy peaks within a spectrum of a given element are Gaussian shaped rather than pure line spectra. Additionally, we are dealing with finite spectral windows, multiple peaked spectra, and pulse pileup; all tend to couple each window's response to the other.

Keeping in mind that we are dealing with the count rates corresponding to the concentrations presented in the last table, we define the following:

- KC_i = uncorrected system count rate for the K channel
- UC_i = uncorrected system count rate for the U channel
- TC_i = uncorrected system count rate for the T channel
- K_i = the percent differential concentration of potassium
- U_i = ppm differential concentration of uranium
- T_i = ppm differential concentration of thorium

where "i" refers to the ith pad.

We also define the following:

- ζ_{kk} = sensitivity of KC_i to concentrations of K_i
- ζ_{ku} = sensitivity of KC_i to concentrations of U_i
- ζ_{kt} = sensitivity of KC_i to concentrations of T_i
- ζ_{uk} = sensitivity of UC_i to concentrations of K_i
- ζ_{uu} = sensitivity of UC_i to concentrations of U_i
- ζ_{ut} = sensitivity of UC_i to concentrations of T_i
- ζ_{tk} = sensitivity of TC_i to concentrations of K_i
- ζ_{tu} = sensitivity of TC_i to concentrations of U_i
- ζ_{tt} = sensitivity of TC_i to concentrations of T_i

Using the above definitions, we now construct the functional relationship by means of the following nine (9) equations in sets of three (3) per pad.

$$\begin{array}{l} \text{K pad} \\ \text{U pad} \\ \text{T pad} \end{array} \begin{array}{l} KC_k = \zeta_{kk}K + \zeta_{ku}U + \zeta_{kt}T \\ UC_k = \zeta_{uk}K + \zeta_{uu}U + \zeta_{ut}T \\ TC_k = \zeta_{tk}K + \zeta_{tu}U + \zeta_{tt}T \\ KC_u = \zeta_{kk}K + \zeta_{ku}U + \zeta_{kt}T \\ UC_u = \zeta_{uk}K + \zeta_{uu}U + \zeta_{ut}T \\ TC_u = \zeta_{tk}K + \zeta_{tu}U + \zeta_{tt}T \\ KC_t = \zeta_{kk}K + \zeta_{ku}U + \zeta_{kt}T \\ UC_t = \zeta_{uk}K + \zeta_{uu}U + \zeta_{ut}T \\ TC_t = \zeta_{tk}K + \zeta_{tu}U + \zeta_{tt}T \end{array}$$

Separating these equation into consistent groups, we get for the uncorrected count rates in the K channel

$$\begin{array}{l} \text{(K pad)} \\ \text{(U pad)} \\ \text{(T pad)} \end{array} \begin{array}{l} KC_k = \zeta_{kk}K_k + \zeta_{ku}U_k + \zeta_{kt}T_k \\ KC_u = \zeta_{kk}K_u + \zeta_{ku}U_u + \zeta_{kt}T_u \\ KC_t = \zeta_{kk}K_t + \zeta_{ku}U_t + \zeta_{kt}T_t \end{array}$$

The equations can be expressed in matrix notation

$$\begin{bmatrix} KC_k \\ KC_u \\ KC_t \end{bmatrix} = \begin{bmatrix} K_k & U_k & T_k \\ K_u & U_u & T_u \\ K_t & U_t & T_t \end{bmatrix} \cdot \begin{bmatrix} \zeta_{kk} \\ \zeta_{ku} \\ \zeta_{kt} \end{bmatrix}$$

Where the k, u and t subscripts represent the K, U and T pads.

In a similar manner we can write two other matrix equations for UC_i and TC_i respectively.

$$\begin{bmatrix} UC_k \\ UC_u \\ UC_t \end{bmatrix} = \begin{bmatrix} K_k & U_k & T_k \\ K_u & U_u & T_u \\ K_t & U_t & T_t \end{bmatrix} \cdot \begin{bmatrix} \zeta_{uk} \\ \zeta_{uu} \\ \zeta_{ut} \end{bmatrix}$$

$$\begin{bmatrix} TC_k \\ TC_u \\ TC_t \end{bmatrix} = \begin{bmatrix} K_k & U_k & T_k \\ K_u & U_u & T_u \\ K_t & U_t & T_t \end{bmatrix} \cdot \begin{bmatrix} \zeta_{tk} \\ \zeta_{tu} \\ \zeta_{tt} \end{bmatrix}$$

Collecting the above, these equations can be expressed in matrix form as

$$\begin{bmatrix} KC_k & UC_k & TC_k \\ KC_u & UC_u & TC_u \\ KC_t & UC_t & TC_t \end{bmatrix} = \begin{bmatrix} K_t & U_k & T_k \\ K_u & U_u & T_u \\ K_t & U_t & T_t \end{bmatrix} \cdot \begin{bmatrix} \zeta_{kk} & \zeta_{uk} & \zeta_{tk} \\ \zeta_{ku} & \zeta_{uu} & \zeta_{tu} \\ \zeta_{kt} & \zeta_{ut} & \zeta_{tt} \end{bmatrix}$$

or

$$\bar{A} = \bar{B} \cdot \bar{\zeta}$$

where \bar{A} is the residual count rate matrix, \bar{B} is the matrix of the known differential concentrations and $\bar{\zeta}$ the sensitivity matrix.

Rearranging the above equations we have

$$\bar{B} = \bar{A} \cdot \bar{\zeta}^{-1}$$

We now define

$$\bar{\zeta}^{-1} = \bar{\Delta}$$

Eliminating $\bar{\zeta}$, we get

$$\bar{B} = \bar{A} \cdot \bar{\Delta}$$

We can now solve for $\bar{\Delta}$ by matrix inversion.

Therefore, the differential concentrations in the mixed pad can be derived from the k,u,t pads to check the computed $\bar{\Delta}$.

$$\begin{bmatrix} K_m \\ U_m \\ T_m \end{bmatrix} = \begin{bmatrix} \Delta_{kk} & \Delta_{ku} & \Delta_{kt} \\ \Delta_{uk} & \Delta_{uu} & \Delta_{ut} \\ \Delta_{tk} & \Delta_{tu} & \Delta_{tt} \end{bmatrix} \cdot \begin{bmatrix} KC_m \\ UC_m \\ TC_m \end{bmatrix}$$

where the subscript m refers to the mixed pad. Expanding this in algebraic form we obtain the following set of equations:

$$K_m = \Delta_{kk}(KC_m + \frac{\Delta_{ku}UC_m}{\Delta_{kk}} + \frac{\Delta_{kt}TC_m}{\Delta_{kk}})$$

$$U_m = \Delta_{uu}(UC_m + \frac{\Delta_{ut}TC_m}{\Delta_{kk}} + \frac{\Delta_{uk}}{\Delta_{uu}} KC_m)$$

$$T_m = \Delta_{tt}(TC_m + \frac{\Delta_{tu}UC_m}{\Delta_{tt}} + \frac{\Delta_{tk}}{\Delta_{tt}} KC_m)$$

The terms in parentheses in the above 3 equations are the "corrected stripped count rates" for the system, and the stripping coefficients are as follows:

$$S_{ku} = \frac{\Delta_{ku}}{\Delta_{kk}} \quad (\text{effect of uranium on potassium})$$

$$S_{kt} = \frac{\Delta_{kt}}{\Delta_{kk}} \quad (\text{effect of thorium on potassium})$$

$$S_{ut} = \frac{\Delta_{ut}}{\Delta_{uu}} \quad (\text{effect of thorium on uranium})$$

$$S_{uk} = \frac{\Delta_{uk}}{\Delta_{uu}} \quad (\text{effect of potassium on uranium})$$

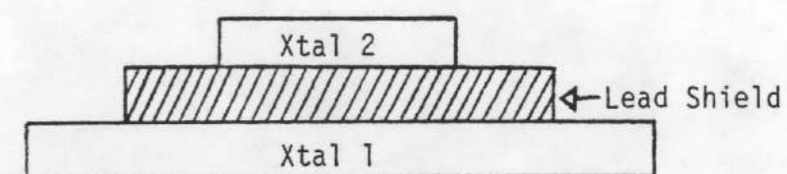
$$S_{tu} = \frac{\Delta_{tu}}{\Delta_{tt}} \quad (\text{effect of uranium on thorium})$$

$$S_{tk} = \frac{\Delta_{tk}}{\Delta_{tt}} \quad (\text{effect of potassium on thorium})$$

These stripping coefficients are defined in terms of S_{ij} in order to eliminate confusion with α , β , and γ , which are sometimes defined slightly differently.

ATMOSPHERIC RADON CORRECTION

Consider the crystal configuration shown below:



Let 1 and 2 designate the down and up crystal respectively. The down crystal sees radiation rates of I_1 composed of the air signal I_a and the ground signal I_g plus aircraft and cosmic background.

$$\text{Therefore } I_1 = I_g + I_a + A_1 + C_1$$

Similarly, the up crystal sees the air signal and ground signal (both somewhat attenuated) plus an aircraft and cosmic background.

$$\text{Therefore } I_2 = \ell I_g + m I_a + A_2 + C_2$$

Where m is the response to the air signal and ℓ is the % of the ground signal getting through to the up detector.

Using the test pad data, the factor ℓ can be determined. Consider the two previous equations. When we subtract the matrix pad data from the K, U, and T pad data, we have essentially set A_1 , A_2 , C_1 , and C_2 and I_a equal to zero.

$$\begin{aligned} \text{Therefore } I_1 &= I_g \\ I_2 &= \ell I_g \\ &= \left(\frac{I_2}{I_1} \right) \end{aligned}$$

Instead of using the count rates we can use the resultant sensitivities $1/\Delta_{uu}$ to determine ℓ for the elemental channel U.

$$= \frac{1/\Delta_{uu} \text{ (up)}}{1/\Delta_{uu} \text{ (down)}}$$

It should be noted that due to "shine around" (since the shielding is not an infinite plane, the upward looking crystal responds to the surrounding terrain) on the test pads, as altitude increases, should decrease, thus $\ell = f(h)$.

Only the factor m remains to be determined. This unfortunately cannot be determined from test pad data. It can however be determined by flying over water (e.g. use of the Lake Mead over-water data).

Consider the equations for I_1 and I_2 again

$$I_1 = I_g + I_a + A_1 + C_1$$

$$I_2 = \ell I_g + m I_a + A_2 + C_2$$

Over water $I_g = 0$

We have A_1 , A_2 , C_1 , and C_2 defined.

Removing the aircraft and cosmic background from the over water data and we are left with

$$I_1 = I_a$$

$$I_2 = m I_a$$

Since m is the shielding factor response to the air signal, we should have an air signal to "shield". Thus m is best determined if there is radon present.

Both up and down counting rates are corrected for aircraft and cosmic background and so we can solve the following two equations for I_a .

$$I_1 = I_g + I_a$$

$$I_2 = \ell I_g + m I_a$$

$$m I_a = I_2 - \ell I_g$$

$$\text{but } I_g = I_1 - I_a$$

$$\text{then } I_a (m - \ell) = I_2 - \ell I_1$$

$$\text{or } I_a = \frac{I_2 - \ell I_1}{m - \ell} = \text{Bi Air}$$

and I_a is then the Bi Air contribution from the surrounding air. This is then subtracted from the down looking U count resulting in corrected data.

DATA PROCESSING

DATA PREPARATION

The following sections summarize the techniques used for reduction and processing of the airborne data collected by geoMetrics.

Field Tape Verification and Edit

The field data tapes containing the airborne data are read on a computer to verify the recording and data quality. Data recovery is essentially 100% from the field tapes. During this phase, statistics are generated summarizing all the variables recorded for each flight line. Simultaneously, the spectral peaks are evaluated for shifts using a centroid calculation and the particular window's peak channel. The data are also checked for correct scan lengths and proper justification of data fields within each scan and live time calculations are made. During this process, the desired window data fields are extracted from each spectrum and rewritten as a reformatted copy tape. (Portions of this operation were performed in the field using the G-725 field computer system.)

The reformatted raw data for each flight line (with aborted or unnecessary flight line data edited out) are then checked for consistency, data spikes, gradients, etc. Every correction suggested by the computer is evaluated by the data processing personnel prior to implementation. Upon completion of the phase, the data on the output tape are "clean" and ready for subsequent correction of the radiometrics and tying of the magnetics.

Flight Line Location

A single frame 35 mm camera is used for obtaining position recovery information. The photo locations are spotted or transferred to a suitable base map and are digitized. The fiducial numbers of the spotted points along each line are entered during the digitizing process. A computer program is used to check the consistency of these data using calculated intersections from tie line to tie line and from traverse to traverse. This program allows easy detection of entry errors as well as potential flight path recovery errors.

A computer program then calculates the map location for each intersection and the beginning and end of each line based on the fiducial numbers and the control line/tie grid. A computer plot is made of these locations to check against the field plot and correct editing

information. These flight lines are then overlain on the geologic base map and each map unit is digitized such that each sample falls within a single unit. This resulting location information is then merged with the geophysical data using the fiducial numbers as common reference.

RADIOMETRIC DATA REDUCTION

Reduction of the raw window data was carried out utilizing system calibration constants as derived from high altitude over water flights, Lake Mead Dynamic Test Range, and the Walker Field Test Pads. The data reduction sequence used is summarized in Figure VII. Processing of the data was performed using the window energies given below:

Total count	-	0.4 to 3.0 MeV
K	-	1.37 to 1.57 MeV
U	-	1.66 to 1.87 MeV (downward looking system)
U _{up}	-	1.04 to 1.21 MeV and 1.65 to 2.42 MeV (upward looking system)
T	-	2.41 to 2.81 MeV
Cosmic	-	3 to 6 MeV (downward and upward looking system)

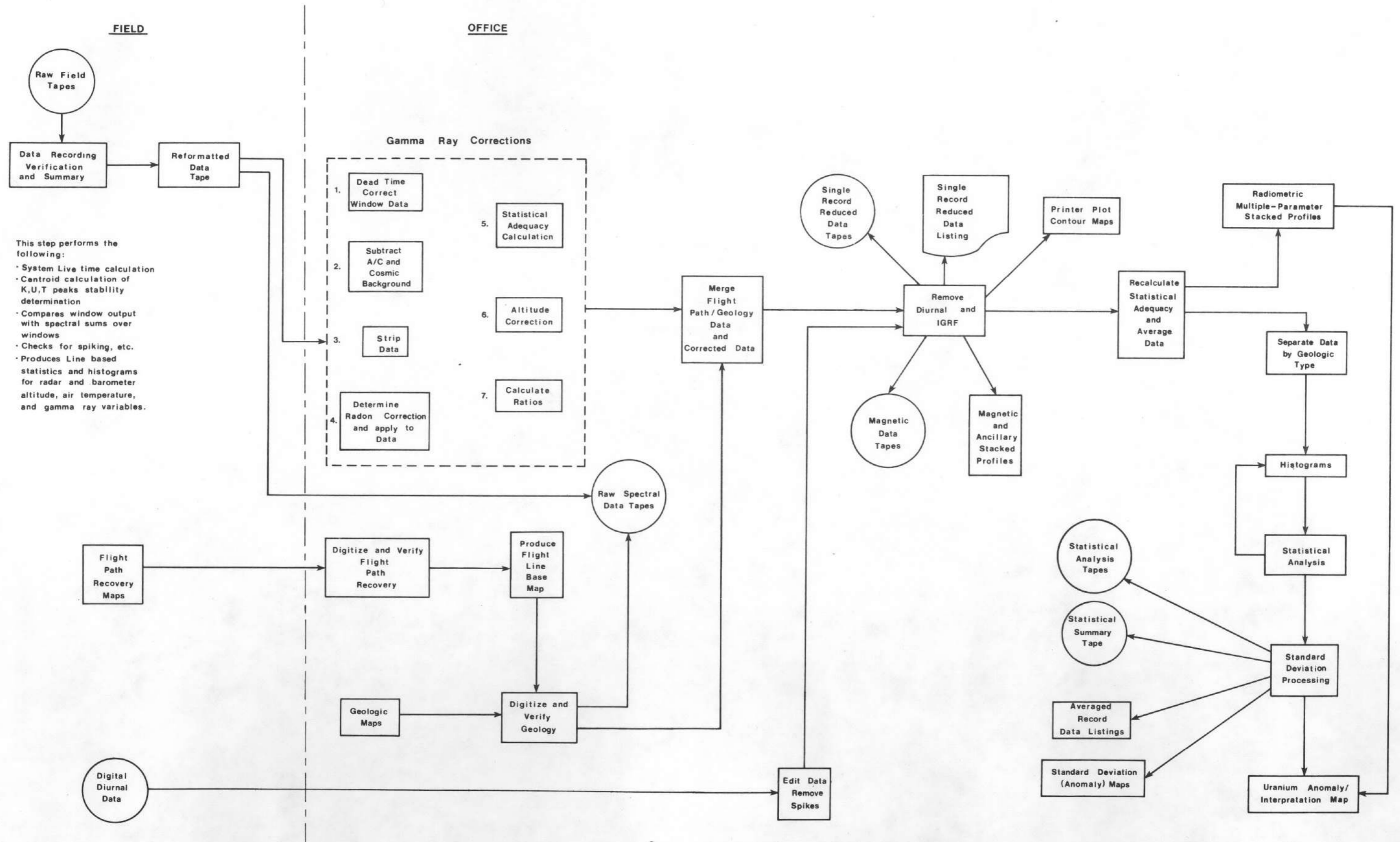
Aircraft and Cosmic background for the Queen Air/Aero Commander over these windows are as follows:

	<u>QUEEN AIR</u>		<u>AERO COMMANDER</u>	
	Aircraft	Cosmic*	Aircraft	Cosmic*
TC (cps)	152.04	2.3833	220.37	2.3915
K (cps)	16.06	0.1322	18.82	0.1334
U _{dn} (cps)	6.50	0.1098	10.85	0.1082
U _{up} (cps)	3.17	0.5540	5.35	0.5915
T (cps)	3.42	0.1503	4.35	0.1513

*Cosmic background values are in cps per 1.0 cps in the 3-6 MeV window.

DATA PROCESSING FLOW DIAGRAM

FIGURE VII



Compton corrections to the down data were made using the following constants:

S_{ij}	QUEEN AIR	AERO COMMANDER
S_{ku}	0.8437	0.8717
S_{kt}	0.1584	0.1408
S_{ut}	0.2703	0.2877
S_{uk}	0.0	0.0
S_{tu}	0.05614	0.09453
S_{tk}	0.0	0.0

The ij subscripts represent the influence of the j^{th} window on the i^{th} window.

All parameters except for S_{ut} are considered constants. S_{ut} was considered an altitude dependent parameter utilizing the following expression (after Grasty, 1975).

$$S_{ut} = S_{ut_0} + 0.0076h, \text{ where } h \text{ is the altitude in hundreds of feet.}$$

Altitude attenuation coefficients used are defined as follows:

ALTITUDE ATTENUATION COEFFICIENTS

	QUEEN AIR	AERO COMMANDER
TC (per foot)	0.002011	0.001688
K (per foot)	0.002740	0.002800
U (per foot)	0.002479	0.002536
T (per foot)	0.002048	0.002102

All radiometric data presented in the strip charts have been normalized to 400 feet mean terrain clearance at STP using the expression:

$$\exp - u_j \frac{273.15}{760} \times \frac{P}{T} (h - 400)$$

where h is the height in feet, u_j is the appropriate altitude attenuation coefficient, P is in mm of Hg, and T is in degrees Kelvin. In cases where the altitude exceeds 1,000 feet, the correction coefficients were limited to the 1,000 foot value.

Bi Air calculations are made using the following expressions:

$$U_{up} = (R_{us} + \frac{C'_{uk}}{C'_{uu}} R_{ks} + \frac{C'_{ut}}{C'_{uu}} R_{ts}) \ell$$

$$Bi_{Air} = \frac{\dots}{m - \ell}$$

Where U_{up} = count rate from upward detectors

ℓ = crystal coupling constant

m = crystal geometric factor

$C'_{uk}, C'_{ut}, C'_{uu}$ = stripping coefficients relating down data to up data

R_{us} = stripped uranium count rate - down system

R_{ks} = stripped potassium count rate - down system

R_{ts} = stripped thorium count rate - down system

The numerical values for the constants ℓ, m, C'_{uk} , and C'_{uu} are given below:

	QUEEN AIR	AERO COMMANDER
ℓ	0.1101	0.0890
m	0.596	0.445
C'_{uk}	0.00947	0.00964
C'_{uu}	0.07136	0.08562
C'_{ut}	0.04636	0.05644
$\mu\ell$	-0.000032	-0.00019
μm	-0.000192	-0.000112

μ_l & μ_m are altitude dependent as follows:

$$l = l - \mu_l \times h, \text{ where } h \text{ is in feet}$$

$$m = m - \mu_m \times h, \text{ where } h \text{ is in feet}$$

These Bi Air data are filtered and the filtered results are then removed on a point by point basis from the corrected uranium window data.

The window data are then evaluated for statistical adequacy prior to altitude correction to ensure they are significant within the context of the anticipated errors in count statistics.

Statistical Adequacy Test

The statistical adequacy test is made to determine whether the corrected data sample is sufficiently greater than the "noise" to represent the "signal" of interest.

We can define three separate criteria for detection thresholds (ref. Currie, Analytical Chemistry, Volume 40, No. 3, March 1968) of which only one is directly applicable to our case; this is the "critical level". This is the level at which the decision is made that a signal is "detected". We thus define this critical level as that level at which the data are statistically adequate.

Setting the actual levels in counts per second, "a priori" for each elemental window is difficult at best since the full effect of all parameters affecting the counts is not known to a sufficient degree of certainty. If the corrections to the data are a significant portion of the count rate, most of the error (exclusive of systematic errors due to electronics, etc.) in the corrected data can be ascribed to random errors within the applied corrections. The corrections are basically the results of counting radioactive decay products (gamma rays) and are therefore assumed to follow the classical Poisson distribution. The following assumptions concerning these corrections are:

1. In the best case, the error in each correction is additive.
2. The sum of these corrections also follows a Poisson distribution.
3. The uncertainty in the correction itself is equal to the square root of the correction applied.
4. This uncertainty is directly reflected in the corrected single record count rate.

With these assumptions in mind, the criterion for determining the statistical adequacy of a given data sample is defined as follows:

"If a corrected single record data sample exceeds 1.5 times the square root of the summed correction applied to that data sample, then that data sample is statistically adequate."

Since any calculation using statistically inadequate data (such as ratios) is also inadequate, the adequacy of each element of the single sample record data is tested prior to the calculation. This is done during the course of the processing by retaining all corrections applied to each data sample and determining its adequacy as explained above.

Not only are the results of this statistical adequacy test used to insure that calculated ratios will be meaningful but they are also utilized to determine the optimum interval over which the data should be averaged (e.g. 5 seconds or 7 seconds, etc.) to improve the overall data statistical adequacy. In the case of this project, the resulting averaging sample interval was 7 seconds.

Conversion to Equivalent ppm and Percent

At this point the data are single record corrected samples in units of counts per second. These data are then converted to equivalent ppm (parts per million) uranium, thorium and percent potassium. The conversion factors are the sensitivities derived from the Lake Mead Dynamic Test Range data at 400 feet mean terrain clearance.

<u>Radioelement</u>	<u>Equivalent Percent/ppm</u>	<u>Queen Air Counts/Second</u>	<u>Aero Commander Counts/Second</u>
K	1%K	91.5	96.3
U	1 ppmeU	10.4	9.2
T	1 ppmeT	6.4	6.7

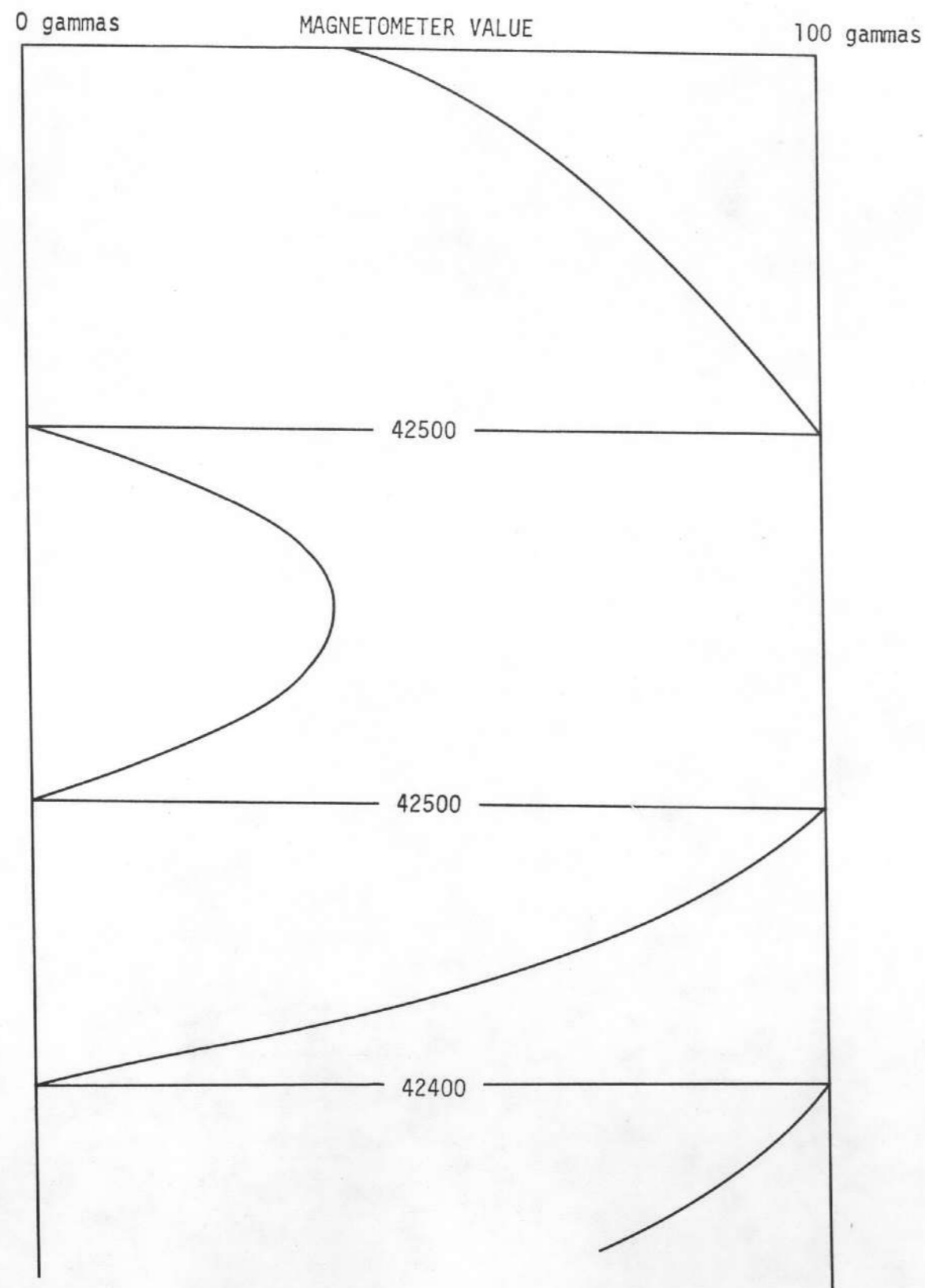


FIGURE VIII Plotter Step Value Labeling

FLIGHT PATH MAPS

For each of the NTMS quadrangle sheets covered by this survey, a flight path position map is available at a scale of 1:250,000. The actual flight path has been superimposed on the geologic quadrangle maps. Flight lines and tie lines are annotated along with fiducial numbers of located positions. Reduced scale (1:500,000) copies of these can be found in this report.

STANDARD DEVIATION MAPS

Gamma ray standard deviation maps have been prepared for each NTMS quadrangle included in this survey. The six maps generated represent the following parameters: percent potassium, equivalent ppm uranium, equivalent ppm thorium, and eU/eT, eU/%K and eT/%K ratios. The data contained in each map represent only those data which are considered statistically adequate. This automatically excludes all data collected over water or data which falls outside of altitude specifications (i.e. altitude greater than 700 and less than 200 feet). The symbolism of each of the six maps is identical. The center of each circle represents the central averaged sample since the data had been averaged over a 7 second interval. The small boxes adjacent to each of the circles represents one standard deviation from the mean for that specific data sample. In order to determine whether the data shown are represented by positive or negative standard deviations, consider each map with north pointing away from the viewer. For east/west lines (traverse lines) positive standard deviations lie above or to the north of the traverse line with negative standard deviation below or to the south. On the north/south lines (tie lines) positive standard deviations are to the left of the viewer (west) with negative standard deviations to the right (east).

These maps were generated at a scale of 1:250,000 for each NTMS sheet and in addition, are presented in each report at a reduced scale of approximately 1:500,000.

HISTOGRAMS

Computer generated histograms, showing the equivalent ppm and percent distributions for the three gamma ray emitters and their ratios measured and calculated as a function of computer map unit are presented in this report (See Figure IX). Information contained on these histograms includes the standard deviation as calculated about the arithmetic mean (or median), and the total number of samples from which the statistics were derived.

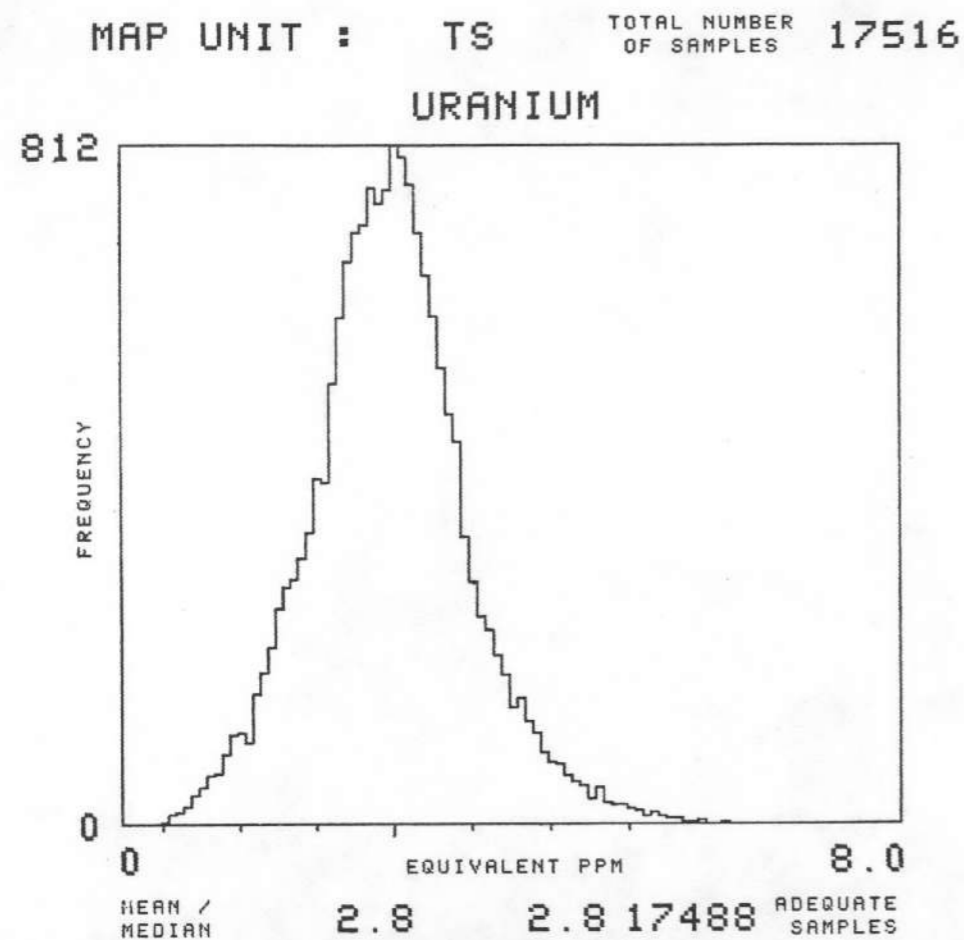


FIGURE IX Sample Computer Map Unit Histogram

DATA LISTINGS

Single record reduced and averaged record (statistical analysis) data listings have been prepared on microfiche. The microfiche are contained in each report. Each of the single record and averaged record data listings are presented for the data contained in a single quadrangle. The data contained in the single record data listings are summarized below:

1. Fiducial number
2. System/Quality (SAKUT) - The first digit identifies the system used to collect the sample. The remaining digits define the results of statistical adequacy testing for altitude, potassium, uranium, and thorium. A value of 0 indicated that the data are statistically adequate. A value of 1 indicates that the data are statistically inadequate. All data collected in excess of 700 feet and less than 200 feet are considered statistically inadequate.
3. Time - time presented in hours, minutes, and seconds
4. Altitude - altitude presented in feet above terrain
5. LAT/LONG - Latitude and Longitude presented in terms of decimal degrees
6. Magnetic field expressed in residual gammas
7. Geology - code representing geologic units
8. %K, eU, eT - percent potassium, equivalent ppm of uranium and thorium
9. eU/eTH, eU/%K, eTH/%K - calculated ratios of the three parameters
10. Total count - corrected total count data (0.4 to 3.0 MeV)
11. COS - downward looking cosmic count rate in the 3-6 MeV channel
12. Uair - atmospheric Bi-214 equivalent ppm
13. Temperature - outside air temperature in degrees centigrade
14. Press - barometric pressure in mm of mercury

The averaged record (statistical analysis) data listings are summarized below:

1. Fiducial number
2. System/Quality (SAKUT) - The first digit identifies the system used to collect the sample. The remaining digits define the results of statistical adequacy testing for altitude, potassium, uranium, and thorium. A value of 0 indicated that the data are statistically adequate. A value of 1 indicates that the data are statistically inadequate. All data collected in excess of 700 feet and less than 200 feet are considered statistically inadequate.
3. LAT/LONG - Latitude and longitude presented in terms of decimal degrees
4. Magnetic field expressed in residual gammas
5. Geology - code representing geologic formations
6. %K, eU, eT - percent potassium, equivalent ppm of uranium and thorium data and the number of (+) standard deviations from the mean
7. eU/eTh, eU/%K, eTh/%K - calculated ratios of the three parameters, and the number of (+) standard deviations from the mean
8. Total count - corrected total count data (0.4 to 3.0 MeV)
9. COS - downward looking cosmic count rate in the 3-6 MeV channel
10. Uair - atmospheric Bi-214 in equivalent ppm

DATA TAPES

Data tape files have been generated for each of the 1:250,000 NTMS quadrangle sheets. The tapes are IBM compatible and recorded on 9 track EBCDIC at 800 bpi. Five separate types of data tapes are presented: raw spectral data tapes, single record reduced data tapes, statistical analysis tapes, magnetic data tapes and a statistical analysis summary tape. Detailed descriptions of the data tape formats follow this discussion.

DATA INTERPRETATION METHODS

General

The stated objective of the NURE Program is the evaluation of the uranium potential of the United States. In support of this goal, high sensitivity airborne radiometric and magnetic surveys have been implemented to obtain reconnaissance information pertaining to regional distribution of uraniumiferous materials. Within this context, data interpretation has been oriented toward regional detection and description of anomalously high concentrations of uranium.

By far the most significant natural sources of gamma radiation in the geologic environment are the radioactive decay series of potassium 40 (K40), thorium 232 (Th232) and uranium 238 (U238) of which 0.7% is uranium 235. Potassium 40 is the largest contributor to natural radioactivity, accounting for nearly 98%, as it is the most abundant gamma ray emitter-.012% of all potassium in nature. (Refer to GSA Memoir 97 for abundances of uranium, thorium, and potassium).

Potassium 40 is directly identified by the airborne spectrometer from a single clear peak at 1.46 mev (million electron volts) in its gamma ray spectrum. However, thorium 232 and uranium 238 do not have any clear, distinct peaks at sufficiently high energies to allow direct detection from airborne systems. Instead, daughter products which do have distinct peaks are measured as representing the abundance of the parent element. For thorium 232, the daughter nuclide thallium 208 (Tl208) has a distinct peak at 2.62 mev while uranium 238 has a daughter, bismuth 214 (Bi214) possessing a clear peak at 1.76 mev (see Figure 7 for a composite decay series spectrum). Consequently the fundamental assumption implicit to airborne uranium and thorium measurements is that the measured daughter products are in radioactive equilibrium - the number of atoms of disintegrating daughter nuclides are equal to the number being formed (see Adams and Gasparini, 1970).

An airborne gamma ray measurement is the sum of photons counted during a specified time interval from a multitude of gamma ray sources which include the three geologic emitters that are being sought plus other interfering sources. These others include, but are not limited to higher energy cosmic rays, aircraft and instruments, contributions from overlapping decay series and airborne radon 222. (See Burson, 1974 and McSharry, 1973 for a more complete discussion of airborne radiometric measurements, and Radiometric Data Reduction in this volume for a complete description of data correction procedures).

When correlating ground data (geochemical, geological, etc.) with the corrected data derived from raw airborne measurements, the interpreter must remember what an individual airborne gamma ray sample physically measures. First, the terrestrial component of the gamma radiation measured by the airborne detector emanated primarily from the upper 18 inches of material on the earth's surface (Gregory and

Horwood, 1963). The airborne measurement cannot "see" any deeper into the underlying rock material and is essentially a measurement of the soil's or exposed (weathered) rock's radioactivity. Secondly, since each airborne sample is an accumulation of gamma rays measured on a moving platform over a fixed period of time, the individual sample represents a large areal extent of surficial material. For this survey, with specifications of 400 feet mean terrain clearance and an average ground speed of 140 miles per hour, a one second sample corresponds to an oval approximately 750 feet long by 600 feet wide (assuming an infinite, uniformly distributed source). Accordingly, averaged samples represent tremendous volumes of surficial materials.

Methodology

As described previously, the gamma ray data were located by computer map units, histograms were produced and statistical analyses performed. The basic unit for interpretation then is the averaged sample and its attendant deviations about a particular map unit's mean.

The uranium anomaly/interpretation map displays each individual averaged sample that meets the following criteria:

1. The averaged uranium sample must be greater than or equal to 1 standard deviation above its map unit mean.
2. The sample must have a U/T ratio greater than or equal to 1 standard deviation above its unit mean.
3. Each U/T ratio defined in (2) must have a corresponding thorium value lying at least greater than minus one (-1) standard deviation below the mean. If the thorium sample is less than one standard deviation below the mean, the U/T ratio is considered questionable.

All the possible anomalies displayed on the map are then examined for clusters, trends, and comparisons with all other available data.

Minimum requirements in the subsequent interpretation discussions of each quadrangle for anomalies listed in the uranium anomaly summary are defined as follows:

Two (2) consecutive averaged U samples lying two or more standard deviations above the mean or three (3) consecutive averaged U samples, two of which are one (1) or more standard deviations and the third of which is two (2) or more standard deviations above the mean.

Statistical anomalies which meet the above criteria can result from several factors or circumstances including: (1) true concentration of uraniferous minerals, (2) differential surface cover (soils and/or

vegetation) within a lithologic unit, (3) local weather conditions such as rain and snow, (4) extreme facies variation within a mapped unit, and (5) differential weathering of rocks within mapped units. Obviously an averaged sample which lies on the boundary between two map units is not truly reflecting either one, but is rather an average of both. Thus, for two markedly different units, such a sample would be anomalous relative to one of the units and not be a true indication of radioactive differences within the unit.

The percent potassium, equivalent ppm thorium and uranium, the three ratios and residual magnetic data were plotted as separate pseudo-contour maps and overlain on the geologic base map and standard deviation maps. Regional trends of each variable and average values could thus be easily and quickly determined and compared with the associated geological, magnetic, and statistical trends. Only the long wavelengths within each variable would show any line-to-line continuity on the pseudo-contour maps and thus, only regional trends will appear.

Each quadrangle's stacked profiles were also overlain on the corresponding geologic and standard deviation maps and anomaly map to further delineate trends and to allow a more detailed analysis of individual anomalies. Since the interpretation was concentrated on detection of anomalous uranium, subtle trends present in the potassium and thorium channels and ratios were only examined in a cursory manner. Even during such a brief examination of the profiles, it was evident that the spectrometer system was highly sensitive to changes in surface materials even in areas of low counting rates such as glacial drift. Thus radiometrics have a real potential for performing general surficial mapping "geochemical analysis" on a geologic unit (or soils) basis in addition to merely radioactive mineral "anomaly hunting".

TAPE FORMATS

SINGLE RECORD REDUCED DATA TAPE

REFERENCE: Paragraphs 4.7.6 and 6.1.6, BFEC 1200-C

The Single Record Tape is an unlabeled, nine track, 800 BPI, NRZI. All data are recorded as EBCDIC characters. Each tape contains but one file of format, header, data, and trailer records for no more than one quadrangle. The tape is divided into 6900-character blocks containing the following information.

Block 1 - Format Data

This block contains 6768 characters in 94 consecutive lines of 72 characters containing the following literal description.

02 0978 (DATA TAPE TYPE AND FORMAT SPECIFICATION DATE CODES)

SINGLE RECORD REDUCED DATA TAPE

FORMAT FOR TAPE IDENTIFICATION BLOCK (SECOND BLOCK)

<u>ITEM</u>	<u>FORMAT</u>	<u>DESCRIPTION</u>
1.	A40	QUADRANGLE NAME AS PROJECT IDENTIFICATION
2.	A20	NAME OF SUBCONTRACTOR
3.	I4	APPROXIMATE DATE OF SURVEY (MONTH, YEAR)
4.	I1	NUMBER OF AERIAL SYSTEMS USED TO COLLECT DATA FOR THIS QUADRANGLE
5.	I1	AERIAL SYSTEM IDENTIFICATION CODE FOR FIRST SYSTEM
6.	A20	AIRCRAFT IDENTIFICATION BY TYPE AND FAA NUMBER FOR FIRST SYSTEM
7.	F6.1	NOMINAL ALTITUDE SYSTEM SENSITIVITY RELATIVE TO TERRESTRIAL POTASSIUM (K-40) TO ONE DECIMAL PLACE IN CPS PER PERCENT K
8.	F6.1	NOMINAL ALTITUDE SYSTEM SENSITIVITY RELATIVE TO TERRESTRIAL URANIUM (BI-214) TO ONE DECIMAL PLACE IN CPS PER PPM EQUIVALENT U
9.	F6.1	NOMINAL ALTITUDE SYSTEM SENSITIVITY RELATIVE TO TERRESTRIAL THORIUM (TL-208) TO ONE DECIMAL PLACE IN CPS PER PPM EQUIVALENT TH

<u>ITEM</u>	<u>FORMAT</u>	<u>DESCRIPTION</u>
13	I3	NUMBER OF CHANNELS (0-3 MEV) IN 4PI SYSTEM FOR FIRST AERIAL SYSTEM
14	I3	NUMBER OF CHANNELS (0-3 MEV) IN 2PI SYSTEM FOR FIRST AERIAL SYSTEM
15-24	(SAME)	REPEAT OF ITEMS 5-14 FOR SECOND AERIAL SYSTEM
*	*	*
*	*	*
*	*	*
85-94	(SAME)	REPEAT OF ITEMS 5-14 FOR NINTH AERIAL SYSTEM
95	I3	NUMBER OF FLIGHT LINES ON THIS TAPE
96	I4	FIRST FLIGHT LINE NUMBER ON THIS TAPE
97	I6	FIRST RECORD NUMBER OF FIRST FLIGHT LINE
98	I3	JULIAN DATE (DAY OF YEAR) FIRST FLIGHT-LINE DATA WAS COLLECTED
99-101	I4,I6,I3	REPEAT OF ITEMS 96-98 FOR SECOND FLIGHT LINE ON THIS TAPE
*	*	*
*	*	*
*	*	*
390-392	I4,I6,I3	REPEAT OF ITEMS 96-98 FOR 99th FLIGHT LINE ON THIS TAPE

FORMAT FOR SINGLE RECORD REDUCED DATA RECORD (THIRD THRU LAST BLOCK)

<u>ITEM</u>	<u>FORMAT</u>	<u>DESCRIPTION</u>
1	I1	AERIAL SYSTEM IDENTIFICATION CODE
2	I4	FLIGHT LINE NUMBER
3	I6	RECORD IDENTIFICATION NUMBER
4	I6	GMT TIME OF DAY (HHMMSS)
5	F8.4	LATITUDE TO FOUR DECIMAL PLACES IN DEGREES
6	F8.4	LONGITUDE TO FOUR DECIMAL PLACES IN DEGREES
7	F6.1	TERRAIN CLEARANCE TO ONE DECIMAL PLACE IN METERS
8	F7.1	RESIDUAL (IGRF REMOVED) MAGNETIC FIELD INTENSITY TO ONE DECIMAL PLACE IN GAMMAS
9	A8	SURFACE GEOLOGIC MAP UNIT CODE
10	I4	QUALITY FLAG CODES
11	F6.1	APPARENT CONCENTRATION OF TERRESTRIAL POTASSIUM (K-40) TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
12	F4.1	UNCERTAINTY IN TERRESTRIAL POTASSIUM TO ONE DECIMAL PLACE IN PERCENT K
13	F6.1	APPARENT CONCENTRATION OF TERRESTRIAL URANIUM (BI-214) TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
14	F4.1	UNCERTAINTY IN TERRESTRIAL URANIUM TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
15	F6.1	APPARENT CONCENTRATION OF TERRESTRIAL THORIUM (TL-208) TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH
16	F4.1	UNCERTAINTY IN TERRESTRIAL THORIUM TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH

ITEM	FORMAT	DESCRIPTION
17	F6.1	URANIUM-TO-THORIUM RATIO TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PPM EQUIVALENT TH
18	F6.1	URANIUM-TO-POTASSIUM RATIO TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PERCENT K
19	F5.1	THORIUM-TO-POTASSIUM RATIO TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH PER PERCENT K
20	F8.1	GROSS GAMMA (0.4-3.0 MEV) COUNT RATE TO ONE DECIMAL PLACE IN COUNTS PER SECOND
21	F6.1	UNCERTAINTY IN GROSS GAMMA COUNT RATE TO ONE DECIMAL PLACE IN COUNTS PER SECOND
22	F5.1	ATMOSPHERIC BI-214 4PI CORRECTION TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
23	F4.1	UNCERTAINTY IN ATMOSPHERIC BI-214 4PI CORRECTION TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
24	F4.1	OUTSIDE AIR TEMPERATURE TO ONE DECIMAL PLACE IN DEGREES CELSIUS
25	F5.1	OUTSIDE AIR PRESSURE TO ONE DECIMAL PLACE IN MMHG

This description serves to identify the format of data on subsequent blocks on the tape. The remaining 132 characters on this block are blanks.

Block 2 - Single Record Reduced Identification Data

The second block contains the identifier information for the data contained in subsequent blocks. The identification information is written according to the format description in the first half of the first block. The remaining 4978 characters on this block are blanks.

Block 3 - Single Record Reduced Data

These blocks contain data written according to the format description in the second half of the first block. There will be 50 logical records per physical block. As of August 1979, the method for determining uncertainties specified in the data blocks remains undefined, and those values are filled with 9's under format control.

STATISTICAL ANALYSIS TAPE

REFERENCE: Paragraphs 4.7.7 and 6.1.6, BFEC 1200-C

The statistical analysis data tape is an unlabeled, nine track, 800 BPI, NRZI. All data is recorded as EBCDIC characters. The block length is 8000 characters long. Each tape contains one file of data for no more than one quadrangle.

Block 1 - Format Description Data

The first physical block on this tape contains a format description for data on subsequent blocks. The first 7560 characters on this block contains 105 lines of 72 characters exactly as written below:

03 0978 (DATA TAPE TYPE AND FORMAT SPECIFICATION DATE CODES)

STATISTICAL ANALYSIS DATA TAPE

FORMAT FOR TAPE IDENTIFICATION BLOCK (SECOND BLOCK)

ITEM	FORMAT	DESCRIPTION
1	A40	QUADRANGLE NAME AS PROJECT IDENTIFICATION
2	A20	NAME OF SUBCONTRACTOR
3	I4	APPROXIMATE DATE OF SURVEY (MONTH, YEAR)
4	I1	NUMBER OF AERIAL SYSTEMS USED TO COLLECT DATA FOR THIS QUADRANGLE
5	I1	AERIAL SYSTEM IDENTIFICATION CODE FOR FIRST SYSTEM
6	A20	AIRCRAFT IDENTIFICATION BY TYPE AND FAA NUMBER FOR FIRST SYSTEM
7	F6.1	NOMINAL ALTITUDE SYSTEM SENSITIVITY RELATIVE TO TERRESTRIAL POTASSIUM (K-40) TO ONE DECIMAL PLACE IN CPS PER PERCENT K
8	F6.1	NOMINAL ALTITUDE SYSTEM SENSITIVITY RELATIVE TO TERRESTRIAL URANIUM (BI-214) TO ONE DECIMAL PLACE IN CPS PER PPM EQUIVALENT U
9	F6.1	NOMINAL ALTITUDE SYSTEM SENSITIVITY RELATIVE TO TERRESTRIAL THORIUM (TL-208) TO ONE DECIMAL PLACE IN CPS PER PPM EQUIVALENT TH
10	I6	BLANK FIELD (99999)
11	F6.3	4PI-SYSTEM DATA COLLECTION INTERVAL TO THREE DECIMAL PLACES IN SECONDS FOR FIRST SYSTEM
12	F6.3	2PI-SYSTEM DATA COLLECTION INTERVAL TO THREE DECIMAL PLACES IN SECONDS FOR FIRST SYSTEM
13	I3	NUMBER OF CHANNELS (0-3 MEV) IN 4PI SYSTEM FOR FIRST AERIAL SYSTEM
14	I3	NUMBER OF CHANNELS (0-3 MEV) IN 2PI SYSTEM FOR FIRST AERIAL SYSTEM

ITEM	FORMAT	DESCRIPTION
15-24	(SAME)	REPEAT OF ITEMS 5-14 FOR SECOND AERIAL SYSTEM
*	*	*
*	*	*
*	*	*
85-94	(SAME)	REPEAT OF ITEMS 5-14 FOR NINTH AERIAL SYSTEM
95	I3	NUMBER OF FLIGHT LINES ON THIS TAPE
96	I4	FIRST FLIGHT LINE NUMBER ON THIS TAPE
97	I6	FIRST RECORD NUMBER OF FIRST FLIGHT LINE
98	I3	JULIAN DATE (DAY OF YEAR) FIRST FLIGHT-LINE DATA WAS COLLECTED
99-101	I4,I6,I3	REPEAT OF ITEMS 96-98 FOR SECOND FLIGHT LINE ON THIS TAPE
*	*	*
*	*	*
*	*	*
390-392	I4,I6,I3	REPEAT OF ITEMS 96-98 FOR 99th FLIGHT LINE ON THIS TAPE

FORMAT FOR STATISTICAL ANALYSIS DATA RECORD (THIRD THRU LAST BLOCK)

ITEM	FORMAT	DESCRIPTION
1	I1	AERIAL SYSTEM IDENTIFICATION CODE
2	I4	FLIGHT LINE NUMBER
3	I6	RECORD IDENTIFICATION NUMBER
4	I6	GMT TIME OF DAY (HHMMSS)
5	F8.4	LATITUDE TO FOUR DECIMAL PLACES IN DEGREES
6	F8.4	LONGITUDE TO FOUR DECIMAL PLACES IN DEGREES
7	F6.1	TERRAIN CLEARANCE TO ONE DECIMAL PLACE IN METERS
8	F7.1	RESIDUAL (IGRF Removed) MAGNETIC FIELD INTENSITY TO ONE DECIMAL PLACE IN GAMMAS
9	A8	SURFACE GEOLOGIC MAP UNIT CODE
10	I4	QUALITY FLAG CODES
11	F6.1	APPARENT CONCENTRATION OF TERRESTRIAL POTASSIUM (K-40) TO ONE DECIMAL PLACE IN PERCENT K
12	F4.1	UNCERTAINTY IN TERRESTRIAL POTASSIUM TO ONE DECIMAL PLACE IN PERCENT K
13	F5.1	POTASSIUM STANDARD DEVIATION FROM THE MEAN TO ONE DECIMAL PLACE AND ALGEBRAICALLY SIGNED
14	F6.1	AVERAGED CONCENTRATION OF TERRESTRIAL URANIUM (BI-214) TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
15	F4.1	UNCERTAINTY IN TERRESTRIAL URANIUM TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
16	F5.1	URANIUM STANDARD DEVIATION FROM THE MEAN TO ONE DECIMAL PLACE AND ALGEBRAICALLY SIGNED
17	F6.1	AVERAGED CONCENTRATION OF TERRESTRIAL THORIUM (TL-208) TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH
18	F4.1	UNCERTAINTY IN TERRESTRIAL THORIUM TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH
19	F5.1	THORIUM STANDARD DEVIATION FROM THE MEAN TO ONE DECIMAL PLACE AND ALGEBRIACALLY SIGNED.

ITEM	FORMAT	DESCRIPTION
20	F8.1	GROSS GAMMA (0.4-3.0 MEV) COUNT RATE TO ONE DECIMAL PLACE IN COUNTS PER SECOND
21	F6.1	UNCERTAINTY IN GROSS GAMMA COUNT RATE TO ONE DECIMAL PLACE IN COUNTS PER SECOND
22	F5.1	ATMOSPHERIC BI-214 4PI CORRECTION TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
23	F4.1	UNCERTAINTY IN ATMOSPHERIC BI-214 4PI CORRECTION TO ONE DEICMAL PLACE IN PPM EQUIVALENT U
24	F4.1	AVERAGED URANIUM-TO-THORIUM RATIO TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PPM EQUIVALENT TH
25	F5.1	URANIUM-TO-THORIUM RATIO STANDARD DEVIATION FROM THE MEAN TO ONE DECIMAL PLACE AND ALGEBRAICALLY SIGNED
26	F6.1	AVERAGED URANIUM-TO-POTASSIUM RATIO TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PERCENT K
27	F5.1	THORIUM-TO-POTASSIUM RATIO STANDARD DEVIATION FROM THE MEAN TO ONE DECIMAL PLACE AND ALGEBRAICALLY SIGNED
D8	F6.1	AVERAGED THORIUM-TO-POTASSIUM RATIO TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH PER PERCENT K
29	F5.1	THORIUM-TO-POTASSIUM RATIO STANDARD DEVIATION FROM THE MEAN TO ONE DECIMAL PLACE AND ALGEBRAICALLY SIGNED

The remaining 440 characters in this block are blanks.

Block 2 - Statistical Analysis Identification Data

The second block contains the identifier information for the data contained in subsequent blocks according to the format specification in the first part of Block 1. The final 6078 characters on this block are blanks.

Block 3 - Statistical Analysis Data

The third and subsequent blocks contain statistical analysis data in the format specified by the second part of the Block 1. Fifty logical records are allowed per block. The method for determining uncertainty values shown, as of August 1979, remains undefined. These values are filled with 9's under format control.

MAGNETIC DATA TAPE

REFERENCE: Paragraphs 4.7.8 and 6.1.6, BFEC 1200-C

The Magnetic Data Tape is an unlabeled, nine track, 800 BPI, NRZI. All data are recorded as EBCDIC characters. Each tape contains data for no more than one quadrangle and are divided into 8000-character blocks as described below.

Block 1 - Tape Format Description

The first block contains 3384 characters of format information in exactly the following format:

04 0978 (DATA TAPE TYPE AND FORMAT SPECIFICATION DATE CODES)

MAGNETIC DATA TAPE

FORMAT FOR TAPE IDENTIFICATION BLOCK (SECOND BLOCK)

ITEM	FORMAT	DESCRIPTION
1	A40	QUADRANGLE NAME AS PROJECT IDENTIFICATION
2	A20	NAME OF SUBCONTRACTOR
3	I4	APPROXIMATE DATE OF SURVEY (MONTH., YEAR)
4	I3	NUMBER OF FLIGHT LINES ON THIS TAPE
5	I4	FIRST FLIGHT LINE ON THIS TAPE
6	I6	FIRST RECORD NUMBER OF FIRST FLIGHT LINE
7	I3	JULIAN DATE (DAY OF YEAR) FIRST FLIGHT-LINE DATA WAS COLLECTED
8	F8.4	LATITUDE OF GROUND BASE STATION TO FOUR DECIMAL PLACES IN DEGREES FOR FIRST FLIGHT LINE
9	F8.4	LONGITUDE OF GROUND BASE STATION TO FOUR DECIMAL PLACES IN DEGREES FOR FIRST FLIGHT LINE
10-14	(SAME)	REPEAT OF ITEMS 5-9 FOR SECOND FLIGHT LINE ON THIS TAPE
*	*	*
*	*	*
*	*	*
495-499	(SAME)	REPEAT OF ITEMS 5-9 FOR 99th FLIGHT LINE ON THIS TAPE

FORMAT FOR MAGNETIC DATA RECORD (THIRD THRU LAST BLOCK)

ITEM	FORMAT	DESCRIPTION
1	I1	AERIAL SYSTEM IDENTIFICATION CODE
2	I4	FLIGHT LINE NUMBER
3	I6	RECORD IDENTIFICATION NUMBER
4	I6	GMT TIME OF DAY (HHMMSS)
5	F8.4	LATITUDE TO FOUR DECIMAL PLACES IN DEGREES

ITEM	FORMAT	DESCRIPTION
6	F8.4	LONGITUDE TO FOUR DECIMAL PLACES IN DEGREES
7	F6.1	TERRAIN CLEARANCE TO ONE DECIMAL PLACE IN METERS
8	F5.1	OUTSIDE AIR PRESSURE TO ONE DECIMAL PLACE IN MMHG
9	A8	SURFACE GEOLOGIC MAP UNIT CODE
10	F7.1	TOTAL MAGNETIC FIELD INTENSITY TO ONE DECIMAL PLACE IN GAMMAS
11	F7.1	RESIDUAL (IGRF REMOVED) MAGNETIC FIELD INTENSITY TO ONE DECIMAL PLACE IN GAMMAS
12	F7.1	DIURNAL MAGNETIC INTENSITY VARIATION TO ONE DECIMAL PLACE IN GAMMAS
13	F7.1	MAGNETIC DEPTH-TO-BASEMENT TO ONE DECIMAL PLACE IN METERS (IF REQUIRED)

The remaining 4616 characters in this block are blanks.

Block 2 - Magnetic Tape Identification Data

This block contains information about the data in subsequent blocks organized according to the format specification in the first half of Block 1.

Block 3 - Magnetic Data

This block and subsequent block contains magnetic data for the quadrangle organized according to the format specifications in the second half of Block 1. There will be 100 logical records per physical block.

STATISTIC ANALYSIS SUMMARY TAPE

REFERENCE: Paragraphs 4.7.9, BFEC 1200-C

The statistical analysis summary tape is an unlabeled, nine track, 800 BPI, NRZI. All data is recorded as EBCDIC characters. The block length is 700 characters long. Each tape contains one file of data for no more than one quadrangle.

Block 1 - Format Description Data

The first physical block on this tape contains a format description for data on subsequent blocks. The first 4320 characters on this block contains 60 lines of 72 characters exactly as written below:

05 0978 (DATA TAPE TYPE AND FORMAT SPECIFICATION DATE CODE)

STATISTICAL ANALYSIS SUMMARY TAPE (OR FILE)

FORMAT FOR TAPE IDENTIFICATION BLOCK (SECOND BLOCK)

ITEM	FORMAT	DESCRIPTION
1	A40	QUADRANGLE NAME AS PROJECT IDENTIFICATION
2	A20	NAME OF SUBCONTRACTOR
3	I4	APPROXIMATE DATE OF SURVEY (MONTH, YEAR)
4	I6	NUMBER OF GEOLOGIC MAP UNITS USED FOR THIS QUADRANGLE

FORMAT FOR STATISTICAL ANALYSIS SUMMARY DATA RECORD (THIRD THRU LAST BLOCK)

ITEM	FORMAT	DESCRIPTION
1	A8	SURFACE GEOLOGIC MAP UNIT IDENTIFYING CODE
2	I6	TOTAL RECORDS FOR GEOLOGIC MAP UNIT
3	I6	NUMBER OF POTASSIUM RECORDS COMPUTED FOR GEOLOGIC UNIT
4	F6.1	POTASSIUM CONCENTRATION MEAN TO ONE DECIMAL PLACE IN PERCENT K
5	F6.1	POTASSIUM CONCENTRATION STANDARD DEVIATION TO ONE DECIMAL PLACE IN PERCENT K
6	A3	POTASSIUM CONCENTRATION DISTRIBUTION CODE
7	I6	NUMBER OF URANIUM RECORDS COMPUTED FOR GEOLOGIC UNIT
8	F6.1	URANIUM CONCENTRATION MEAN TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
9	F6.1	URANIUM CONCENTRATION STANDARD DEVIATION TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
10	A3	URANIUM CONCENTRATION DISTRIBUTION CODE
11	I6	NUMBER OF THORIUM RECORDS COMPUTED FOR GEOLOGIC UNIT
12	F6.1	THORIUM CONCENTRATION MEAN TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH
13	F6.1	THORIUM CONCENTRATION STANDARD DEVIATION TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH
14	A3	THORIUM CONCENTRATION DISTRIBUTION CODE
15	I6	NUMBER OF URANIUM-TO-THORIUM RATIO RECORDS COMPUTED FOR GEOLOGIC UNIT

16	F6.1	URANIUM-TO-THORIUM RATIO MEAN TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PPM EQUIVALENT U PER PPM EQUIVALENT TH
17	F6.1	URANIUM-TO-THORIUM RATIO STANDARD DEVIATION TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PPM EQUIVALENT TH
18	A3	URANIUM-TO-THORIUM RATIO DISTRIBUTION CODE
19	I6	NUMBER OF URANIUM-TO-POTASSIUM RATIO RECORDS COMPUTED FOR GEOLOGIC UNIT
20	F6.1	URANIUM -TO-POTASSIUM RATIO MEAN TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PERCENT K
21	F6.1	URANIUM-TO-POTASSIUM RATIO STANDARD DEVIATION TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PERCENT K
22	A3	URANIUM-TO-POTASSIUM RATIO DISTRIBUTION CODE
23	I6	NUMBER OF THORIUM-TO-POTASSIUM RATIO RECORDS COMPUTED FOR GEOLOGIC UNIT
24	F6.1	THORIUM-TO-POTASSIUM RATIO MEAN TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH PER PERCENT K
25	F6.1	THORIUM-TO-POTASSIUM RATIO STANDARD DEVIATION TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH PER PERCENT K
26	A3	THORIUM-TO-POTASSIUM RATIO DISTRIBUTION CODE

The remaining 2680 characters on this block shall be blanks.

Block 2 - Statistical Analysis Identification Data

The second block contains the identifier information for the data contained in subsequent blocks according to the format specification in the first part of Block 1. The final 6930 characters on this block are blanks.

Block 3 - Statistical Analysis Summary Data

The third and subsequent blocks contain statistical analysis data in the format specified by the second part of the Block 1. Fifty logical records are allowed per block.

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- Burson, Z. G., 1974, Airborne Surveys of Terrestrial Gamma Radiation in Environmental Research; IEEE Trans. Nucl. Sci., NS-21, No. 1, p. 558-571.
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- Grasty, R. L., Uranium Measurement by Airborne Gamma-Ray Spectrometry; Geophysics, Vol. 40, No. 3, June 1975, p. 503-519.
- Gregory, A. F., and Horwood, J. L., 1963, A Spectrometric Study of the Attenuation in Air of Gamma Rays from Mineral Resources; U.S. Atomic Energy Commission Report CEX-60-3, Washington, D.C.
- McSharry, P. J. and Emerson, D. W., The Collection and Processing of Gamma Ray Spectrometer Data; 2nd International Conference on Geophysics of the Earth and Oceans, Sydney, Australia, January 1973.

APPENDIX B - Flight Summary

APPENDIX B
DAILY PRODUCTION SUMMARY
QUEEN AIR N9AG
MAY, JUNE, 1981

May	25-27	Base Mobilization
	28	337 line miles, Racine, Detroit, Grand Rapids
	29	Weather - nil production
	30	756 line miles, Milwaukee, Midland, Flint
	31	547 " " Racine, Grand Rapid, Detroit
June	1	791 " " Racine, Grand Rapids, Detroit
	2-3	Weather - nil production
	4	696 line miles, Racine, Grand Rapids, Detroit
	5	645 " " Milwaukee, Midland, Flint
	6	467 " " " " "
	7	471 " " Manitowoc, Racine, Milwaukee
	8	Weather - nil production
	9	417 line miles, Manitowoc, Milwaukee, Midland, Grand Rapids
	10	661 " " Flint, Milwaukee, Midland
	11	652 " " Flint, Milwaukee, midland
	12	751 " " Manitowoc, Racine, Traverse, Tawas City
	13-14	Weather - nil production
	15	766 line miles, Midland, Manitowoc, Traverse, Tawas City
	16	744.4 " " " " " " " "

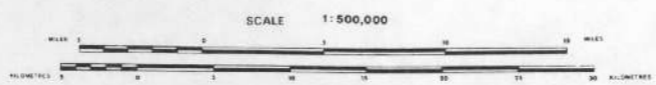
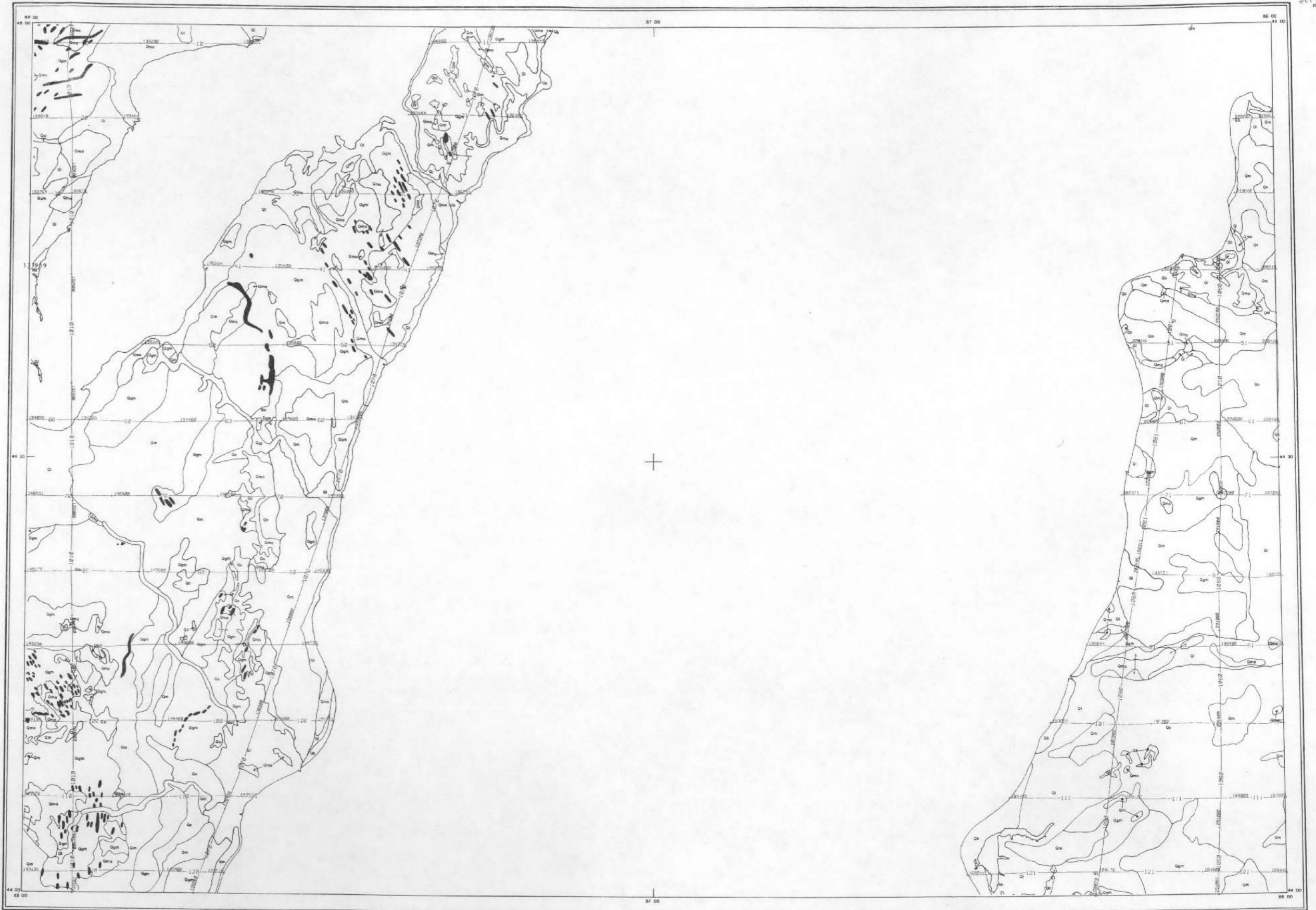
Total miles for the above periods = 8701.4 line miles

Total miles for the included quadrangles:

Racine	419.2
Grand Rapids	1,637.4
Detroit	833.7
Milwaukee	489.2
Midland	1,617.0
Flint	1,001.2
Manitowoc	628.5
Traverse City	1,588.6
Tawas City	486.6

APPENDIX C - Flight Path and Geologic Map

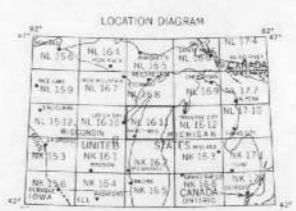
MANITOWOC



SCALE 1:500,000

FRANCHISE NUMBER 052-0
 LINE NUMBER

FLIGHT LINE SPACING 6.0 MILES
 FLIGHT ALTITUDE 400 FEET AMT
 FLOWN AND COMPILED 1980-1981



SURVEY AND
 COMPILED BY:
 EG&G GEOMETRIX

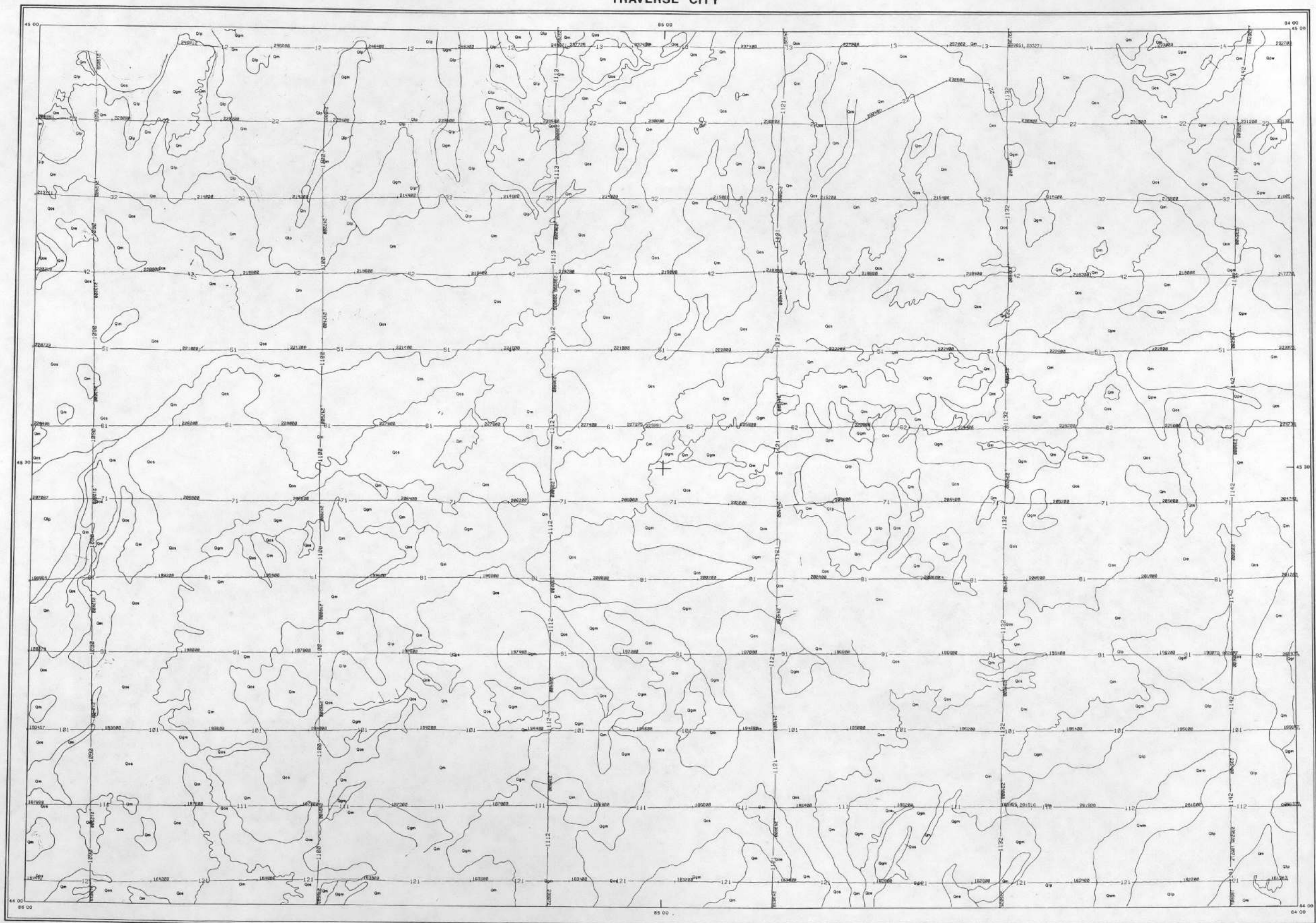
FLIGHT PATH RECOVERY

GREAT LAKES PROJECT

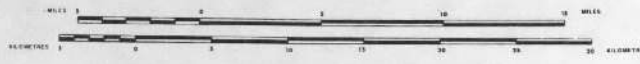
U. S. DEPARTMENT OF ENERGY

TRAVERSE CITY

fc2 mt

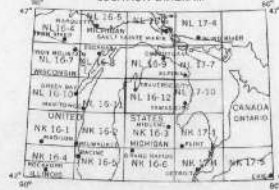


SCALE 1:500,000



FLIGHT LINE SPACING 6.0 MILES
 FLIGHT ALTITUDE 400 FEET AMT
 FLOWN AND COMPILED 1980-1981

LOCATION DIAGRAM




FLIGHT PATH RECOVERY

GREAT LAKES PROJECT

U.S. DEPARTMENT OF ENERGY

SURVEY AND
 COMPILED BY
EG&G GEOMETRICS

MANITOWOC QUADRANGLE
GEOLOGIC MAP EXPLANATION
(Martel Laboratories, 1981)

Cenozoic	Qal	Alluvium	Pleistocene & Holocene
	Qb	Beach deposits <i>Pleistocene & Recent beaches & dunes</i>	
	Qma	Marsh deposits <i>Muck, peat, & silt.</i>	
	Qm	Moraines <i>Unconsolidated, unsorted deposits. Includes lateral & end moraines.</i>	
	Qgm	Ground moraines <i>Till plains.</i>	
	Ql	Lake deposits <i>Near-shore sand & off-shore clay deposits. Locally includes alluvium.</i>	
	Qo	Outwash <i>Meltwater deposits. Includes glacial channel deposits &, locally, alluvium.</i>	
		Drumlins & eskers	

Quaternary

TRAVERSE CITY QUADRANGLE
 GEOLOGIC MAP EXPLANATION
 (Martel Laboratories, 1981)

CENOZOIC	Qm	PLEISTOCENE	QUATERNARY
	Glacial Moraine Glacial sediments and sediments related to glaciation, beds and lenses of till, gravel, sand, silt and clay with numerous boulders and cobbles.		
	Qgm		
	Glacial Ground Moraine Smooth-surfaced glacial till forming relatively flat land, except where it thinly caps broad, rolling hills near the glacial margin. Unsorted and unstratified mixture of clay, silt, sand, and coarser fragments laid down under an ice sheet during a stage of retreat.		
	Qwm		
	Glacial Water-Laid Moraine Near shore deposits of moderately well to poorly sorted sand, gravel and coarse cobbles laid down along the margins of major glacial lakes.		
	Qpw		
	Glacial Ponded Water Deposits Silt, sand, and clay, commonly laminated, deposited in isolated interglacial lakes.		
	Qlp		
	Glacial Lake Flains Lake bottom sediments of major glacial lakes, composed of silt and clay, commonly laminated, in places covered by marl and peat.		
	Qos		
	Glacial Outwash and Spillways Chiefly sand and gravel laid down by water issuing from glacial moraines. Forms gently undulating to nearly flat surfaces.		

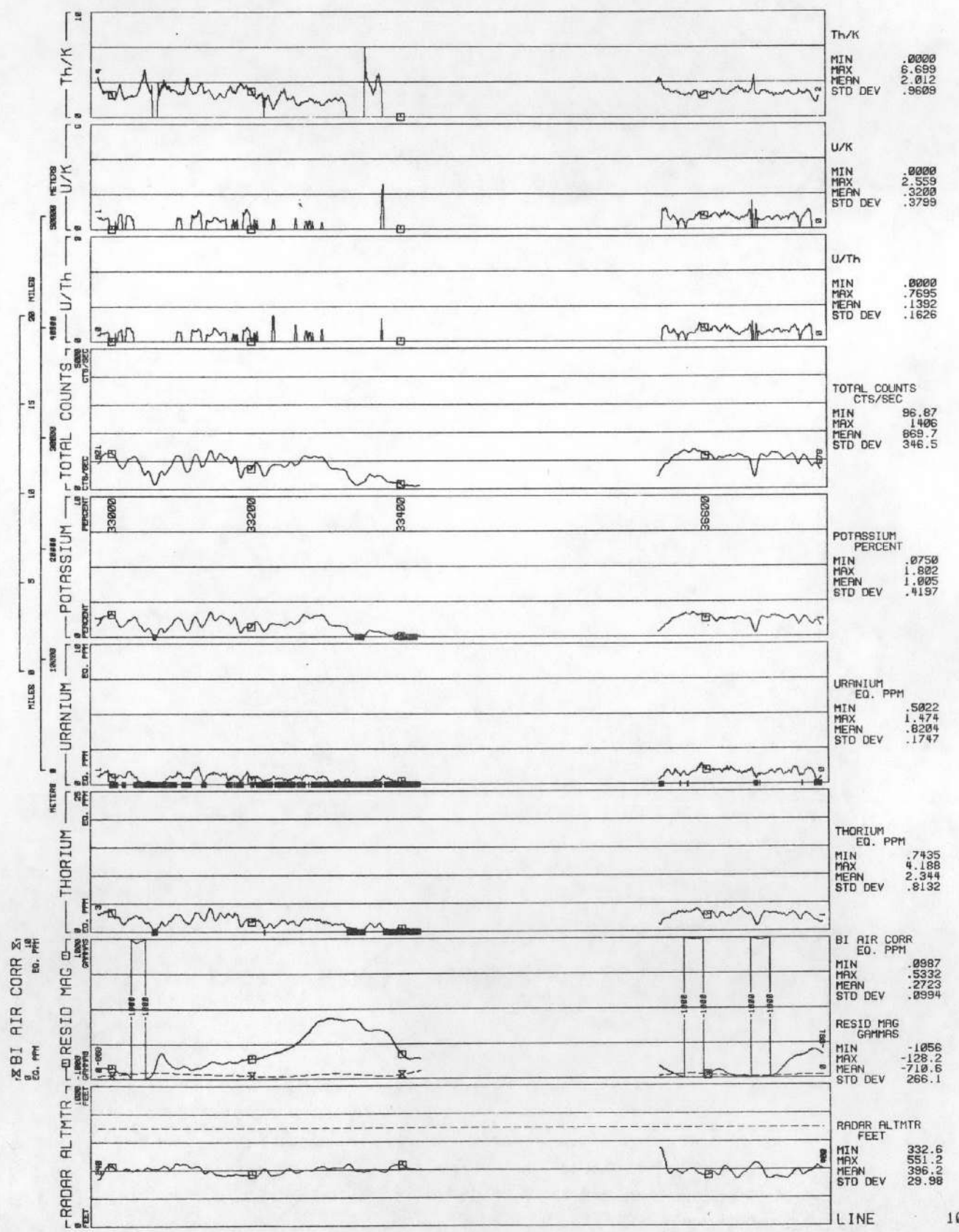
SYMBOLS



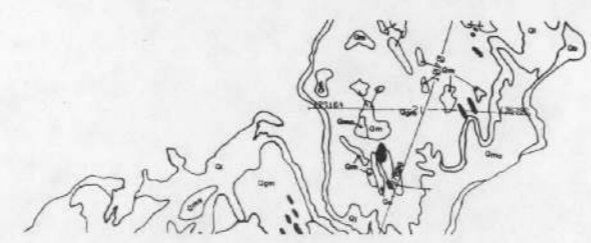
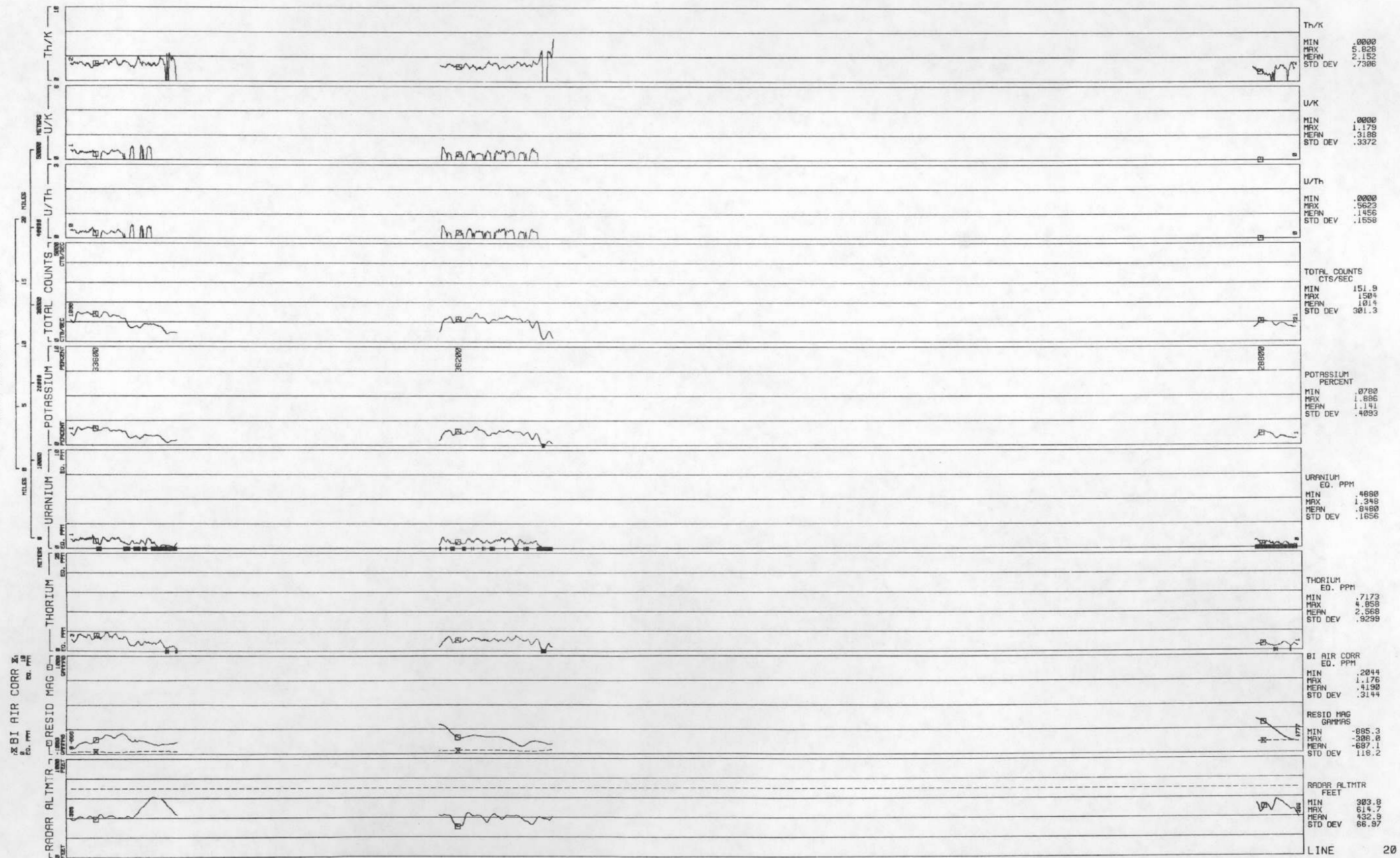
APPENDIX D - Profiles



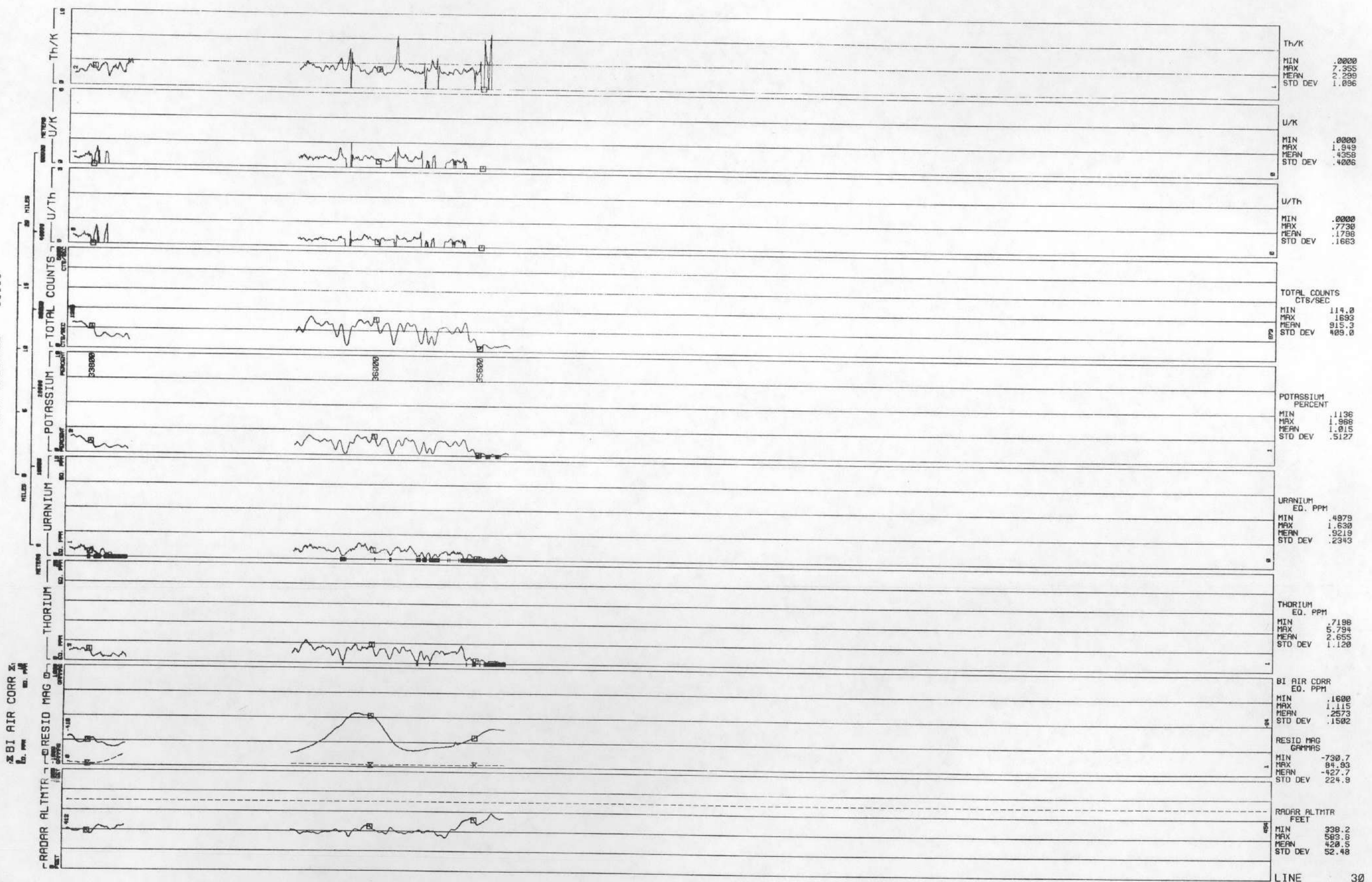
LINE 10
 MANITOWOC QUADRANGLE NTMS NL 16-11
 DATA ACQUIRED 81158

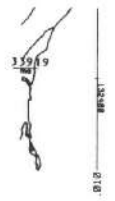


LINE 20
MANITOWOC QUADRANGLE NTMS NL 16-11
DATA ACQUIRED 81158

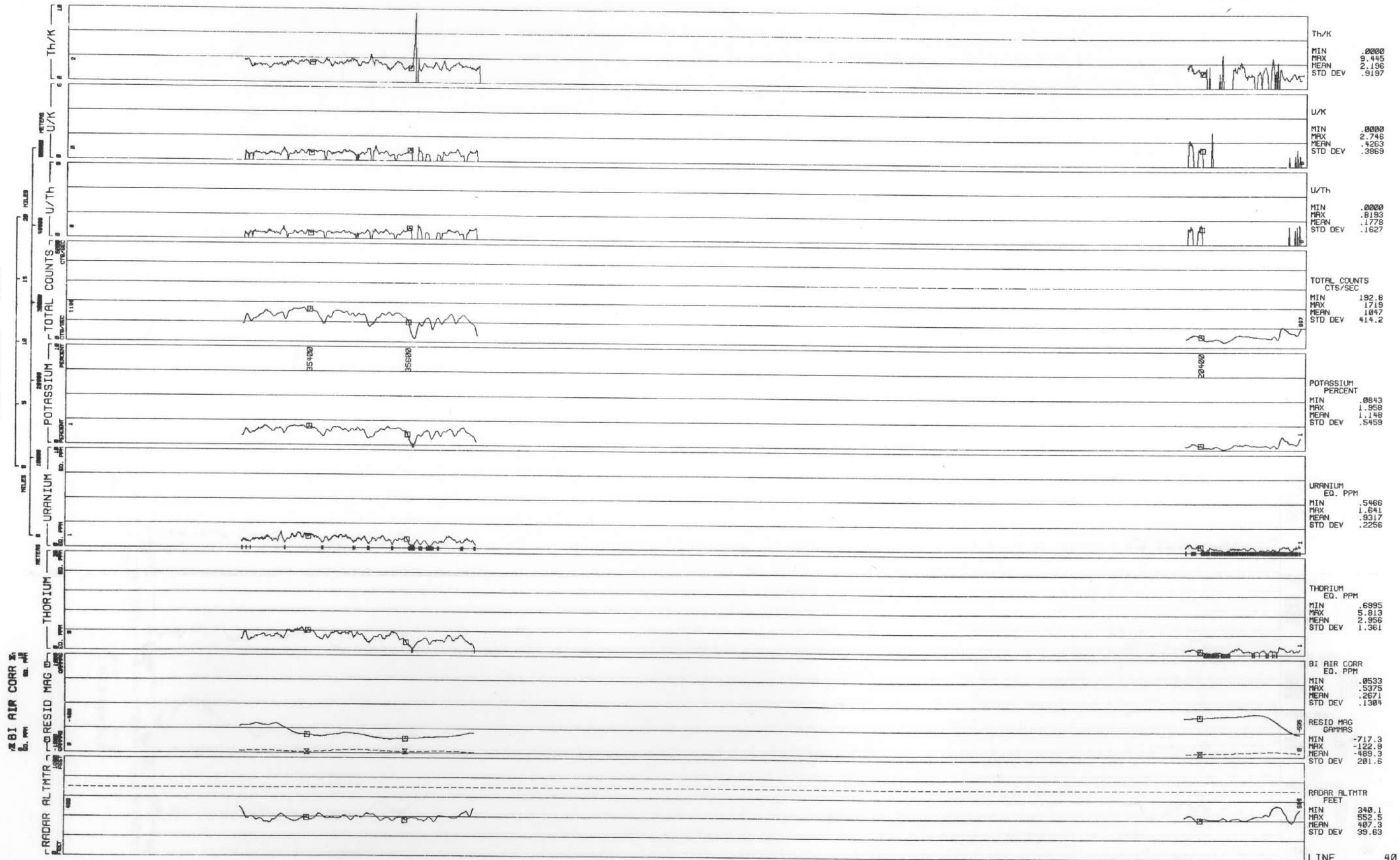


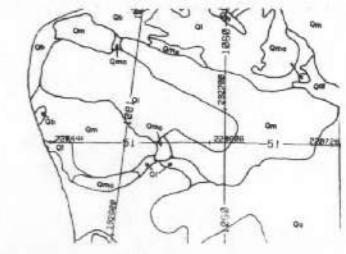
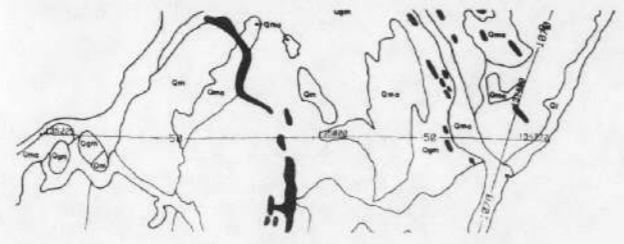
LINE 30
MANITOWOC QUADRANGLE NTMS NL 16-11
DATA ACQUIRED 81158



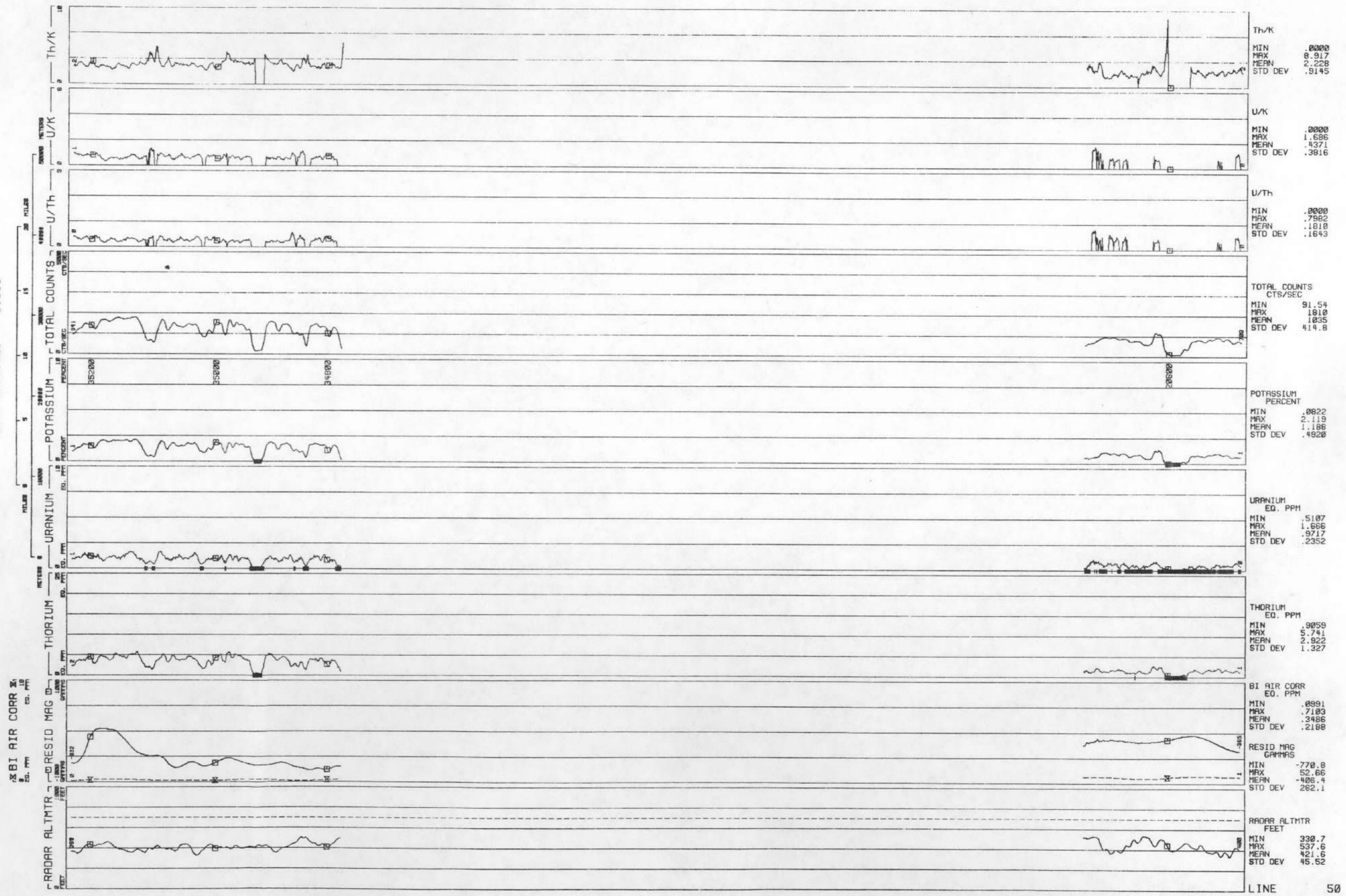


LINE 40
MANITOWOC QUADRANGLE NTMS NL 16-11
DATA ACQUIRED 01158



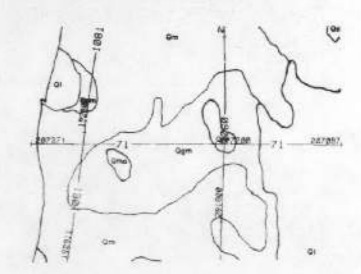
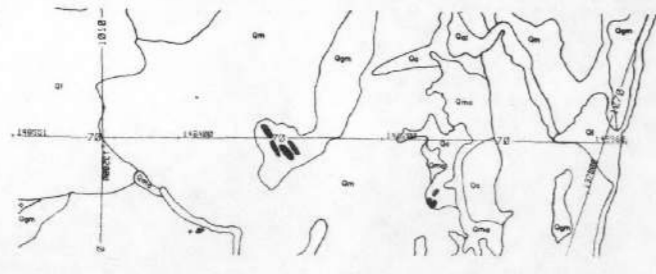


LINE 50
 MANITOWOC QUADRANGLE NTMS NL 16-11
 DATA ACQUIRED 81158

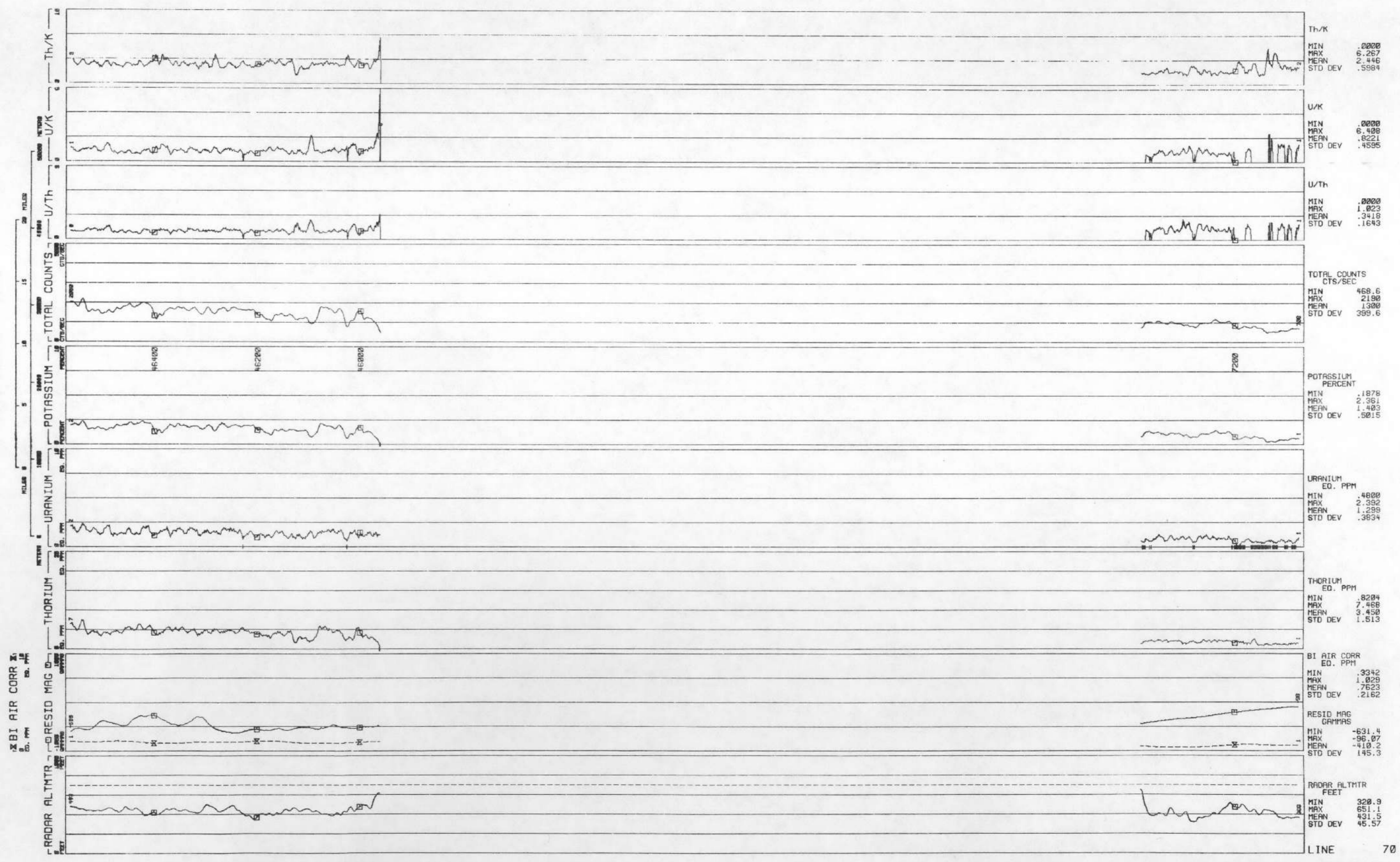


LINE 60
MANITOWOC QUADRANGLE NTMS NL 16-11
DATA ACQUIRED 81158



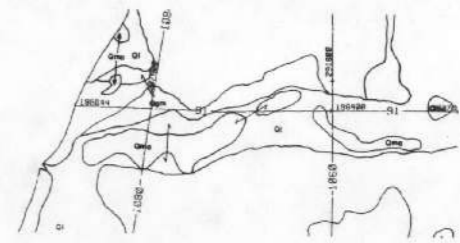
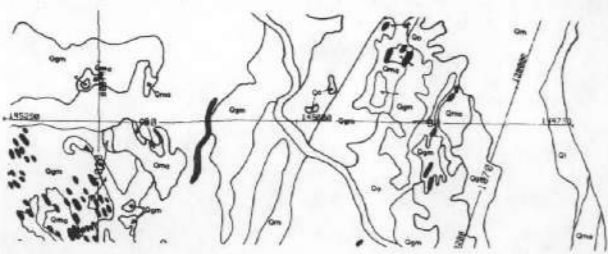


LINE 70
 MANITOWOC QUADRANGLE NTMS NL 16-11
 DATA ACQUIRED 811160

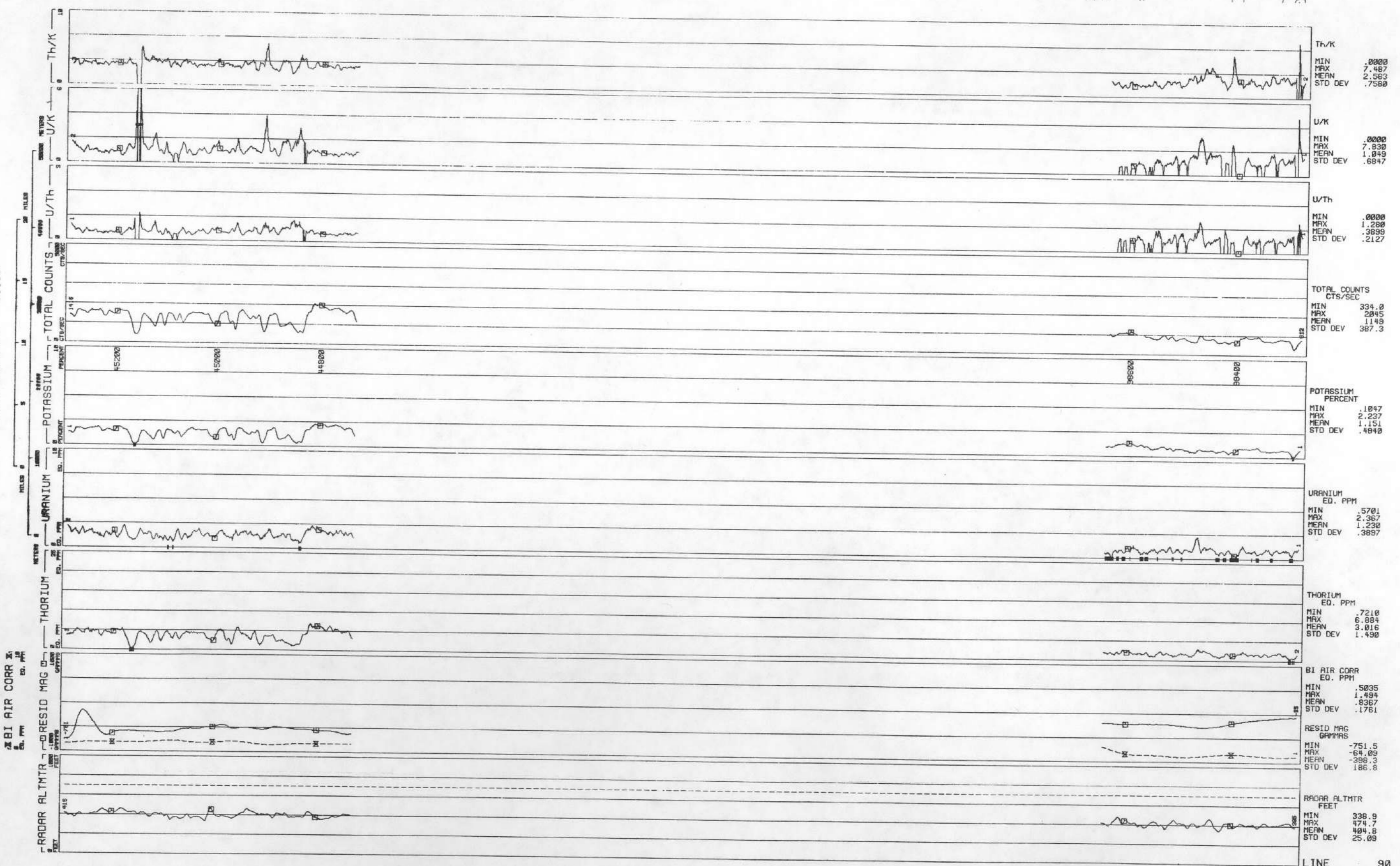


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DATA ACQUIRED 81160

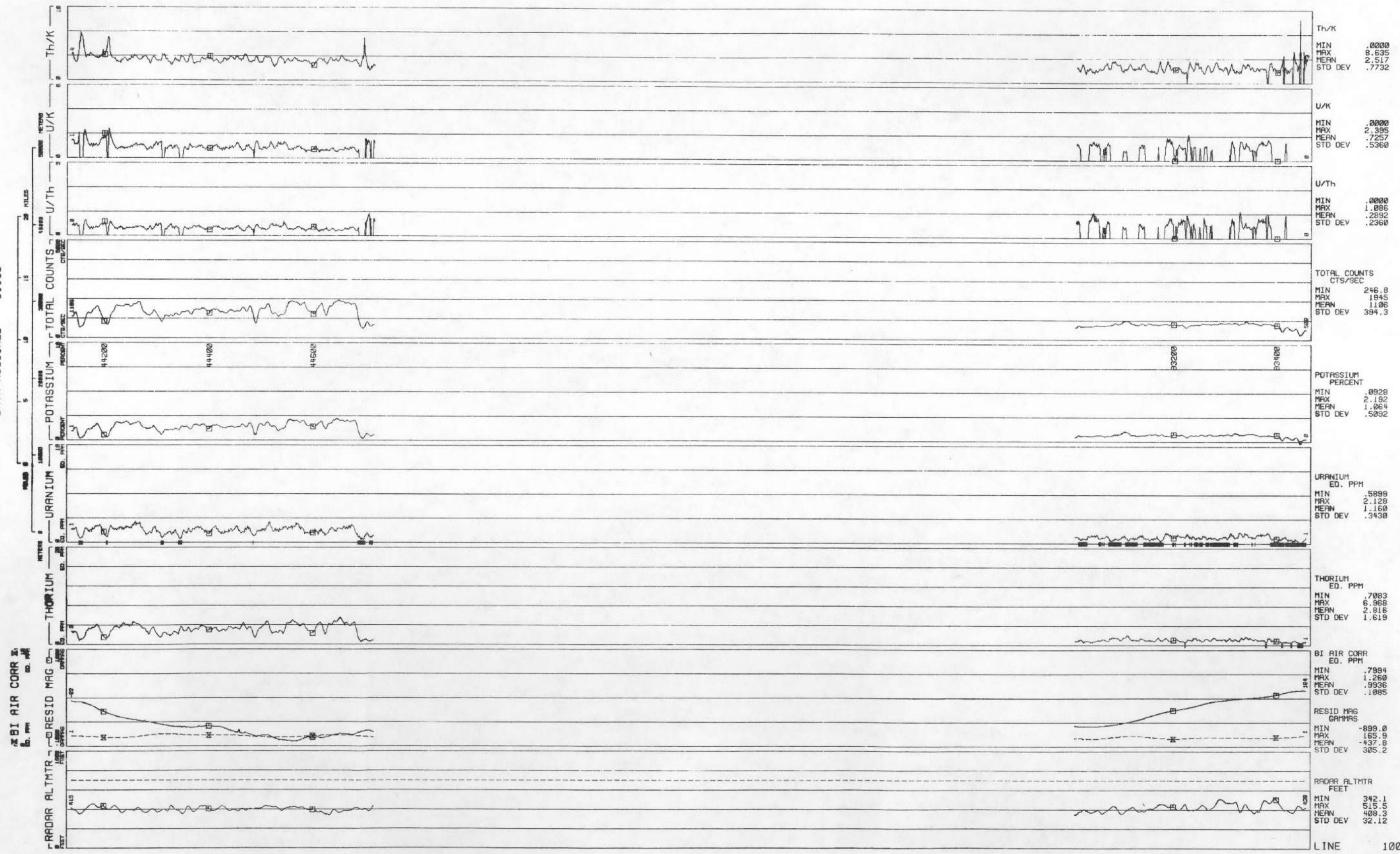


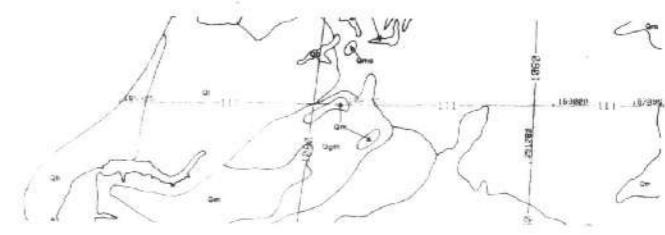
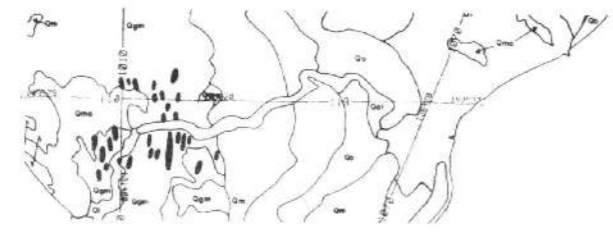


LINE 90
 MANITOWOC QUADRANGLE NTMS NL 16-11
 DATA ACQUIRED 81160

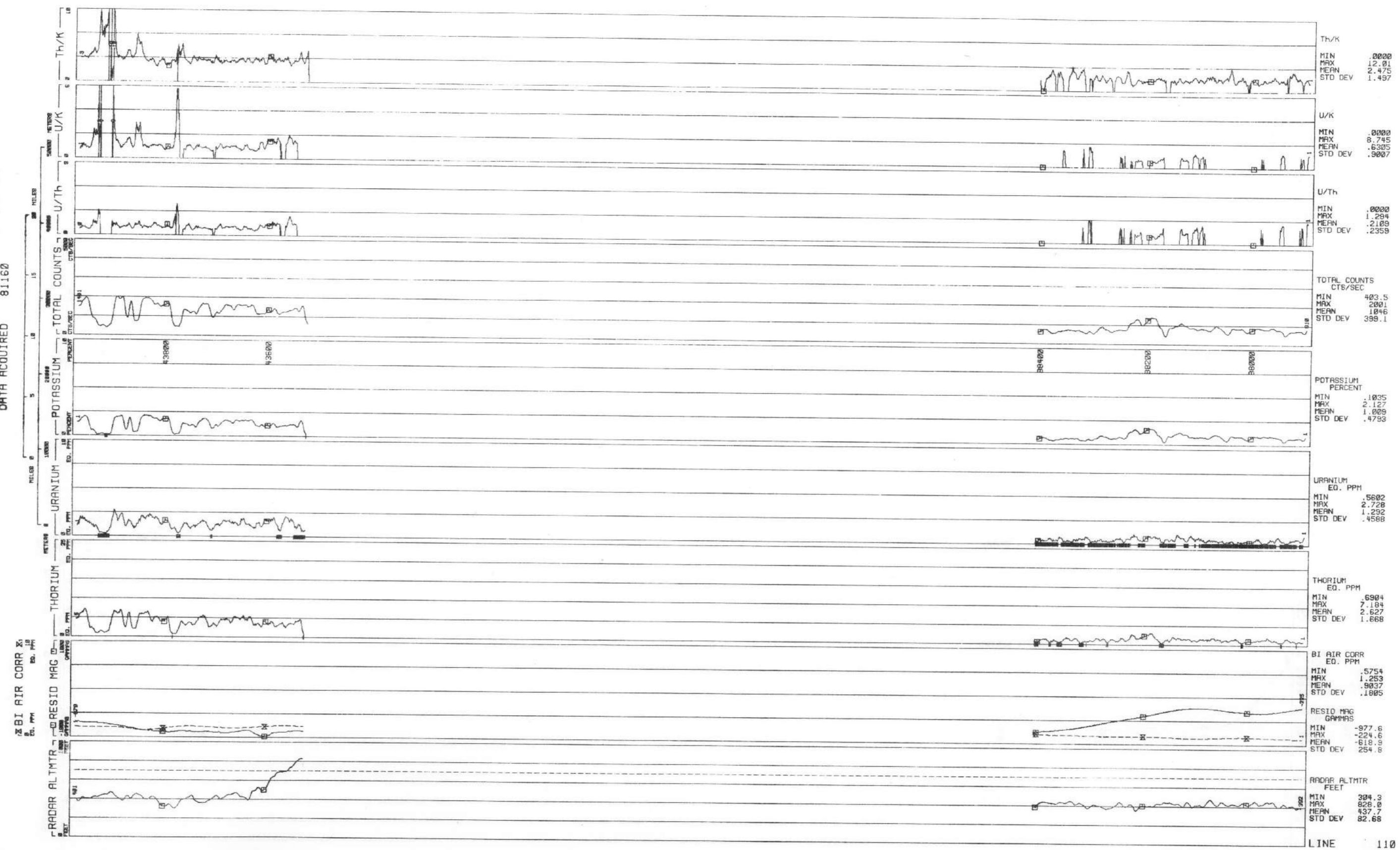


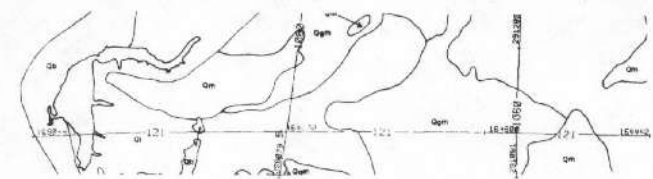
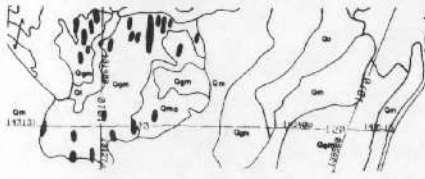
LINE 100
MANITOWOC QUADRANGLE NTMS NL 16-11
DATA ACQUIRED 81160



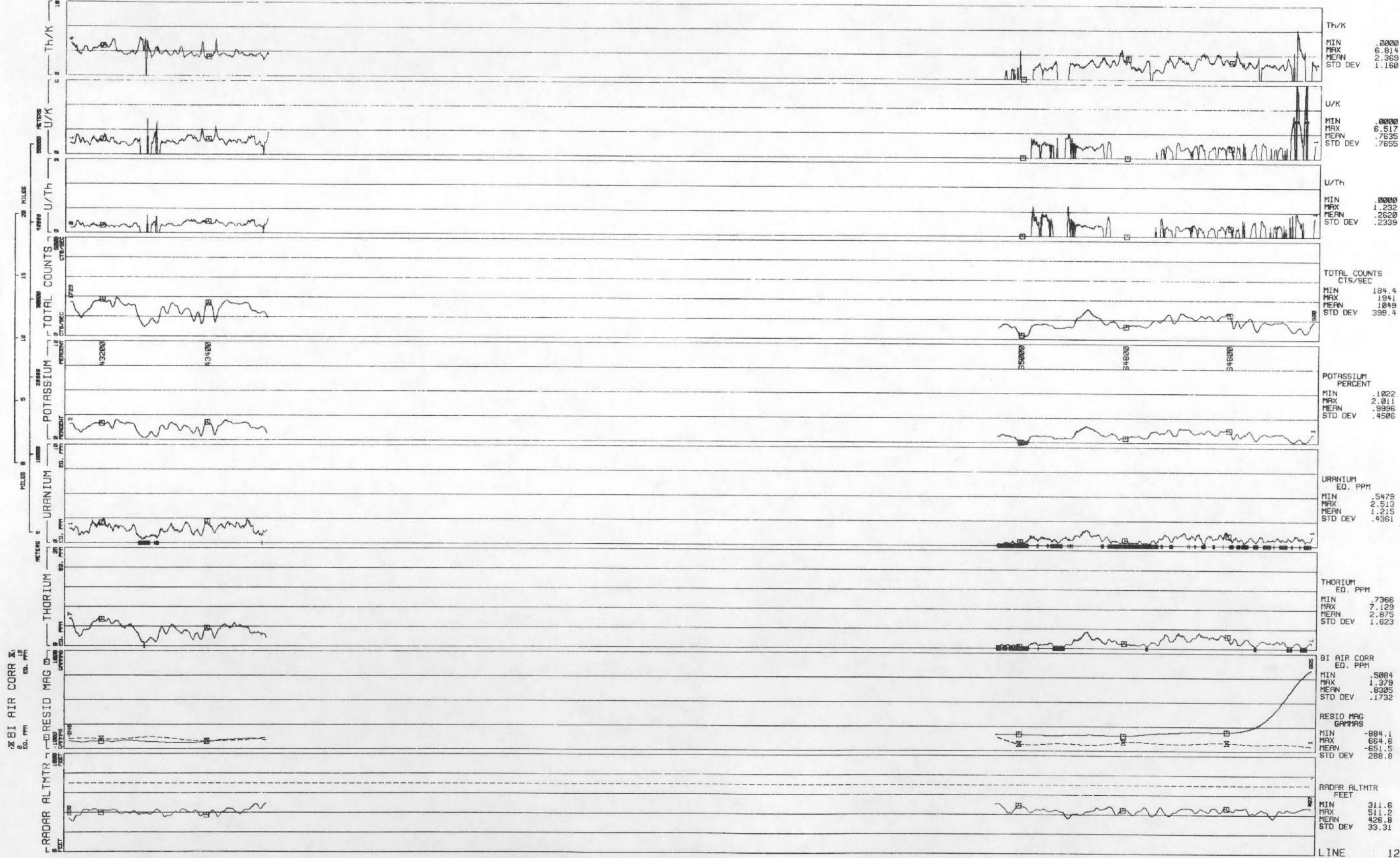


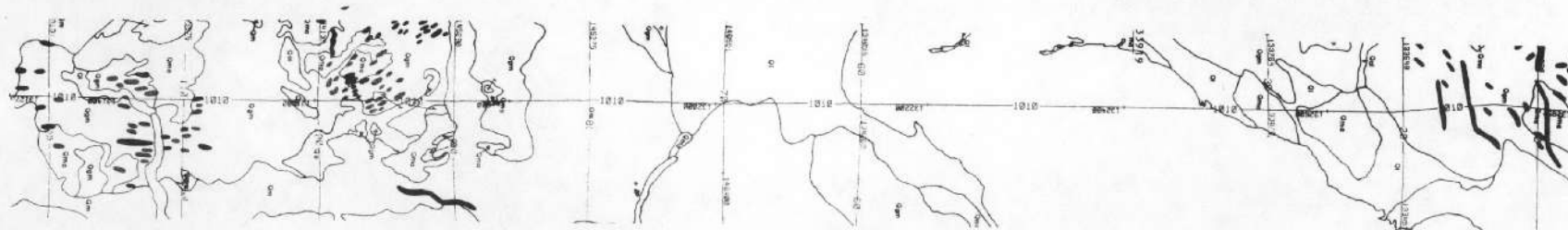
LINE 110
MANITOWOC QUADRANGLE NTMS NL 16-11
DATA ACQUIRED 81160



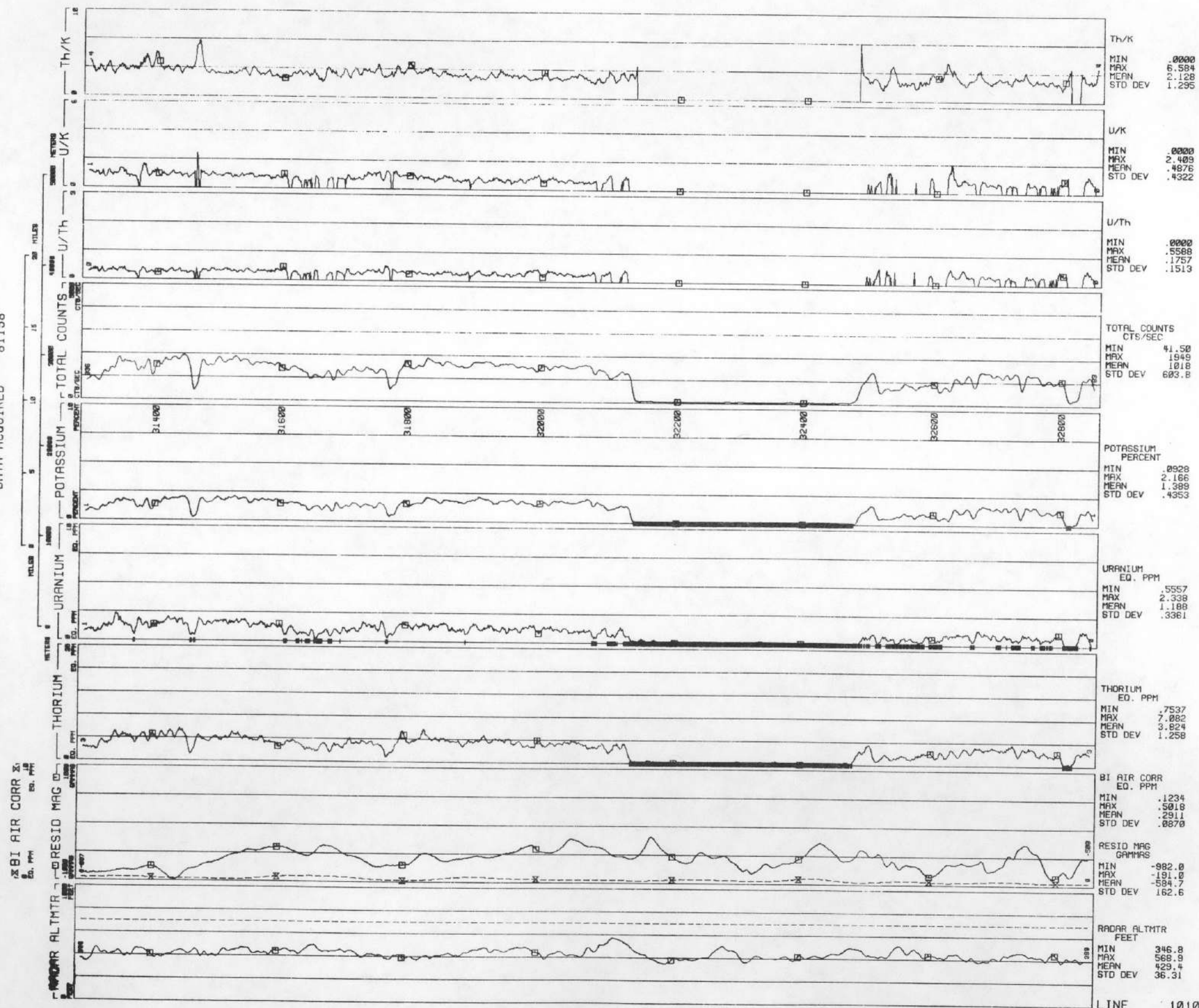


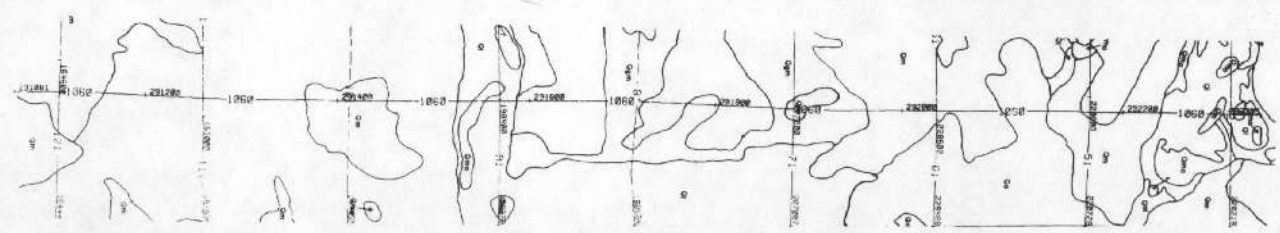
LINE 120
MANITOWOC QUADRANGLE NTMS NL 16-11
DATA ACQUIRED 81160



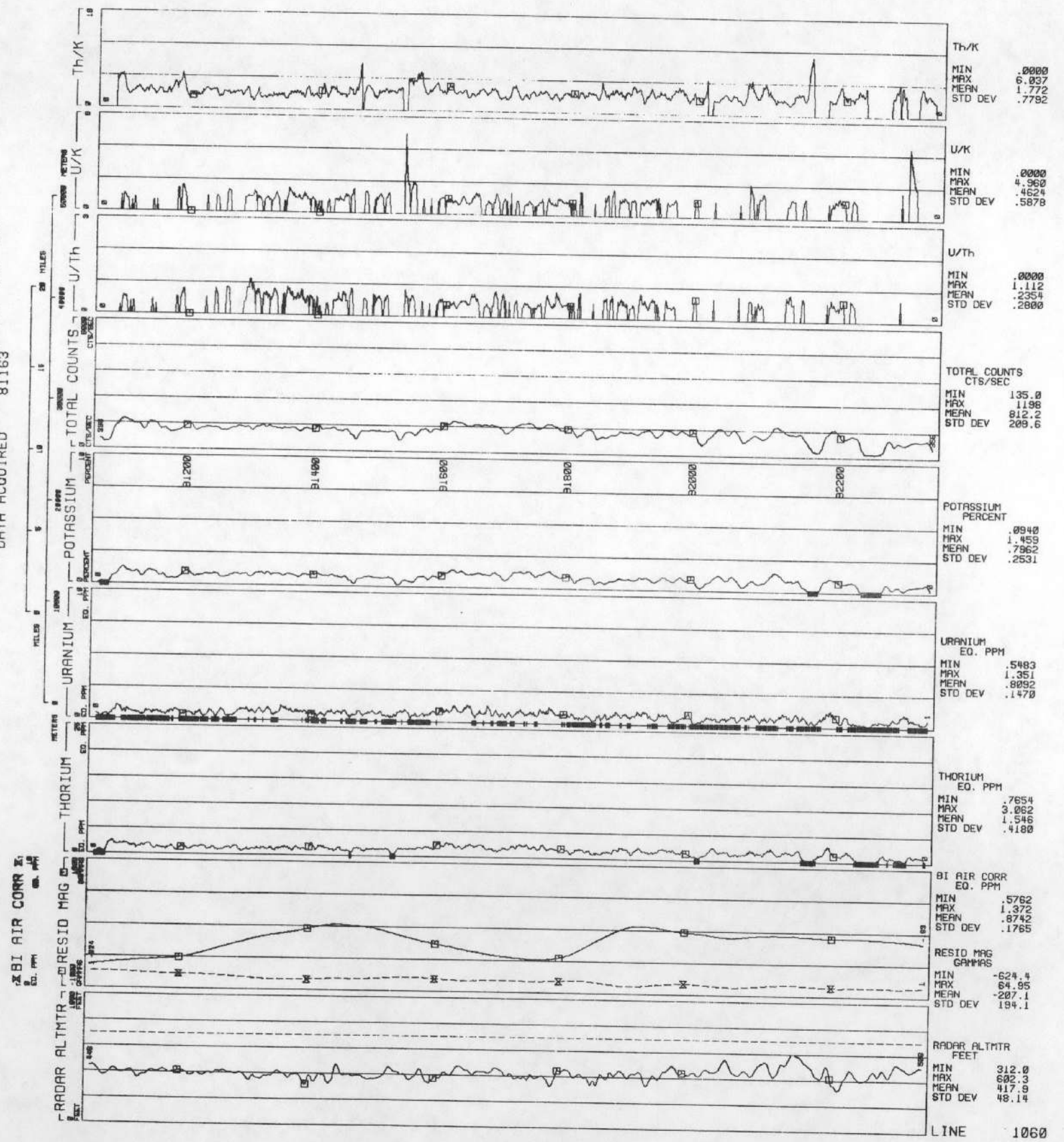


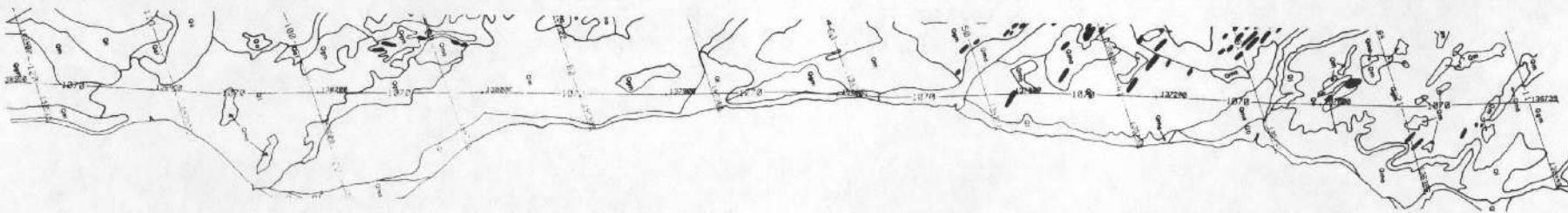
LINE 1010
 MANITOWOC QUADRANGLE NTMS NL 16-11
 DATA ACQUIRED 81158



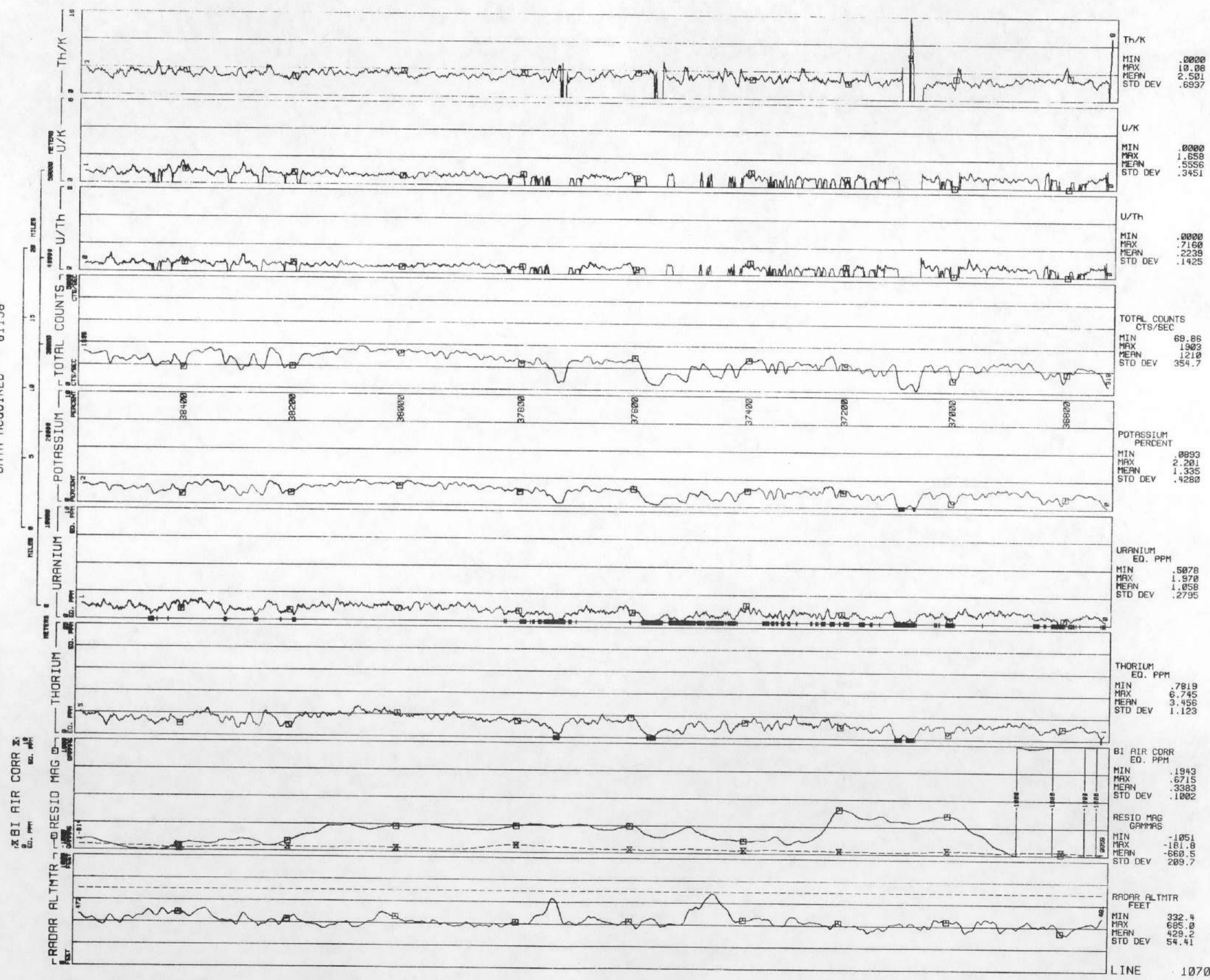


LINE 1060
 MANITOWOC QUADRANGLE NTMS NL 16-11
 DATA ACQUIRED 81163

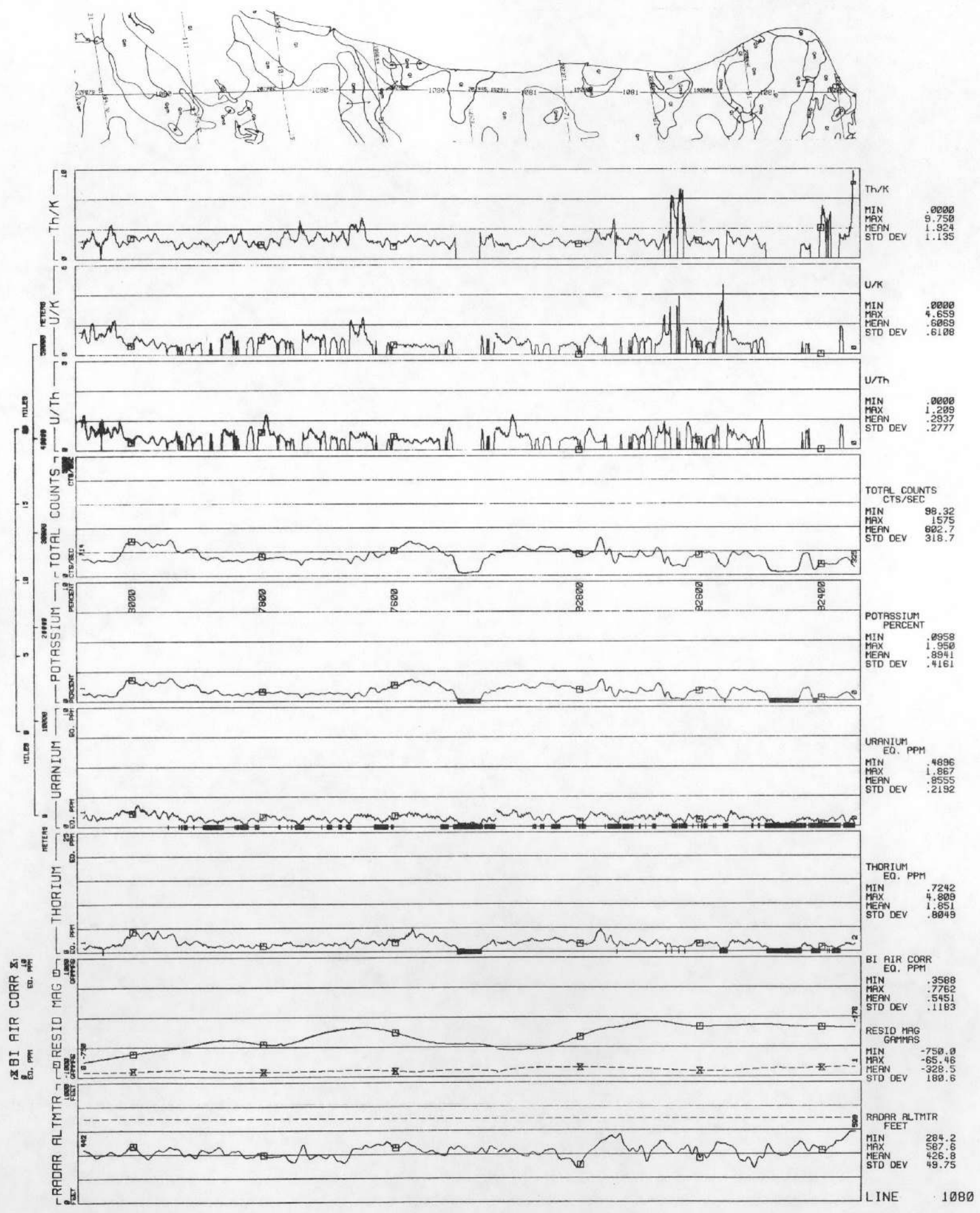


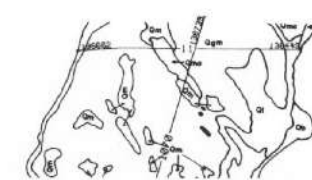
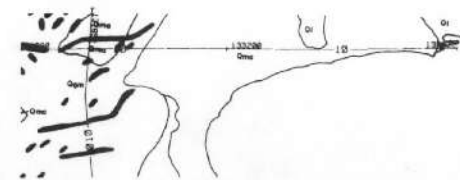


LINE 1070
 MANITOWOC QUADRANGLE NTMS NL 16-11
 DATA ACQUIRED 81158

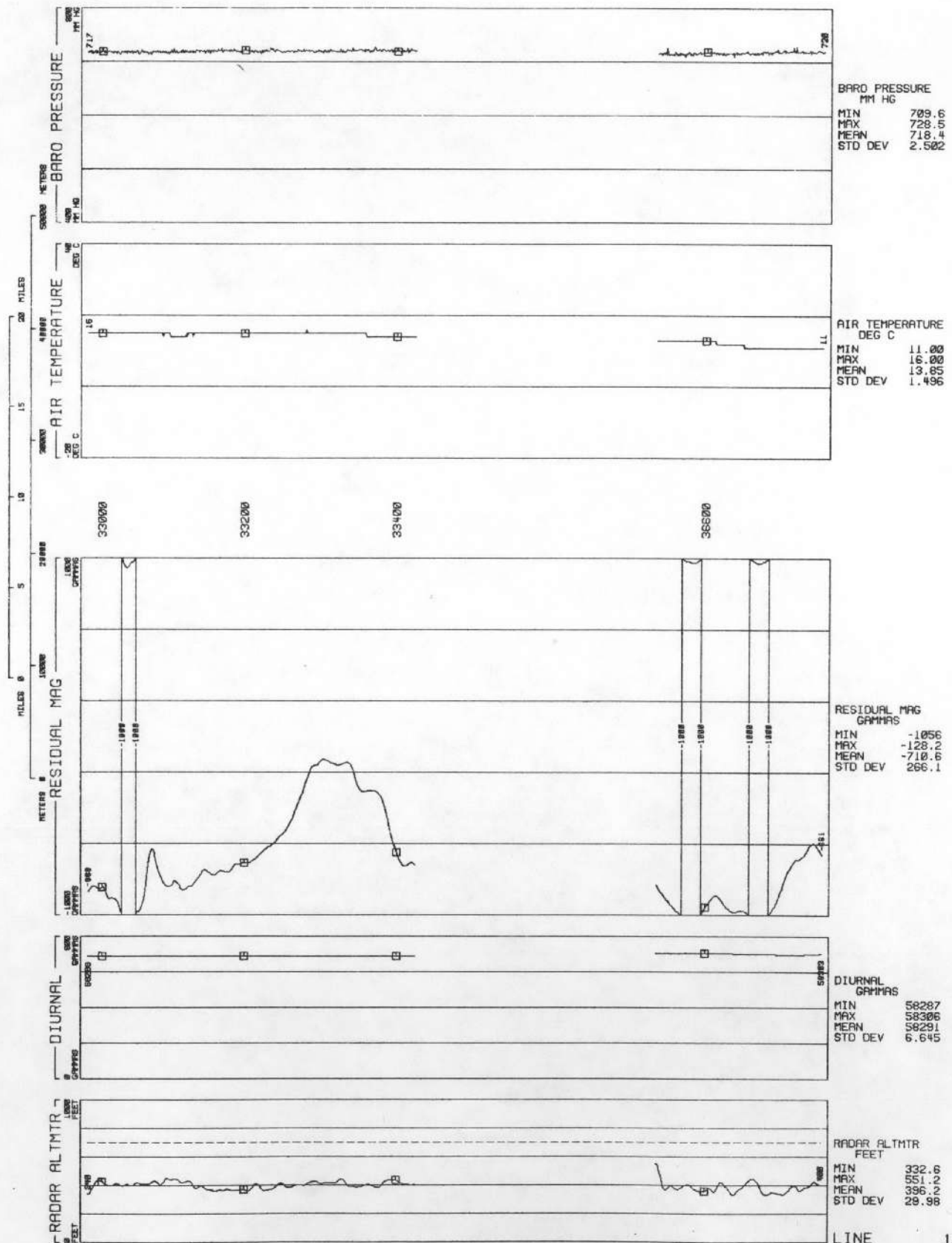


LINE 1080
MANITOWOC QUADRANGLE NTMS NL 16-11
DATA ACQUIRED 81163

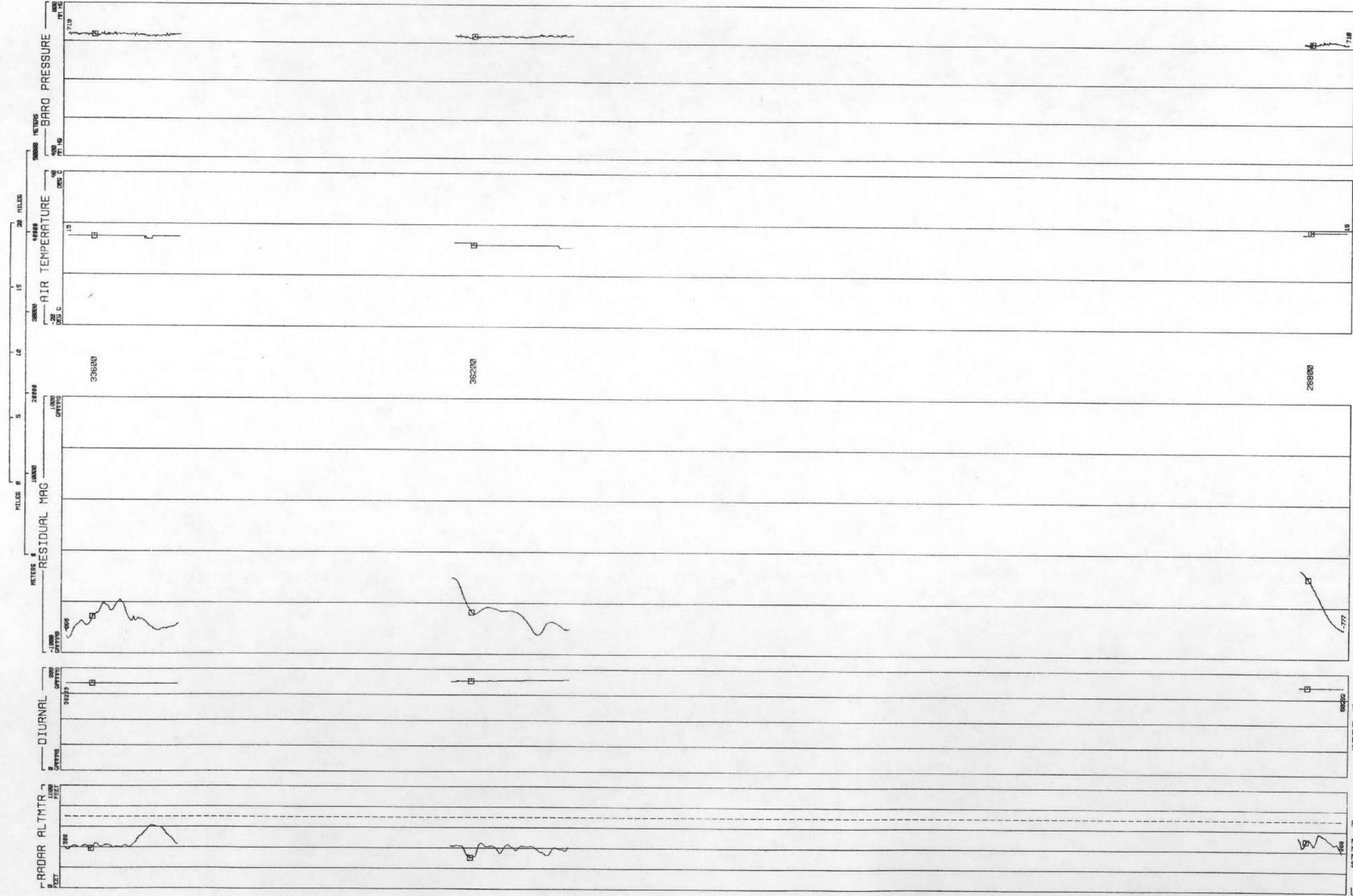
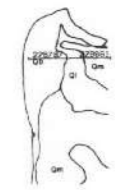
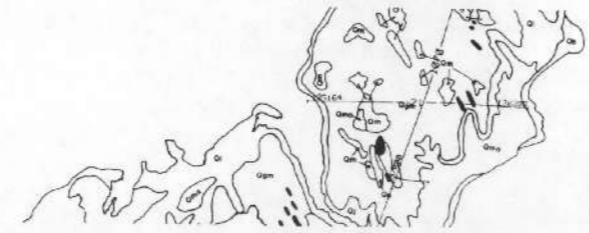
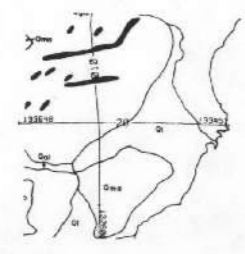




LINE 10
 MANITOWOC QUADRANGLE NTMS NL 16-11
 DATA ACQUIRED 81158



LINE 20
MANITOWOC QUADRANGLE NTMS NL 16-11
DATA ACQUIRED 81158



BARO PRESSURE
MM HG
MIN 706.4
MAX 726.8
MEAN 717.0
STD DEV 3.108

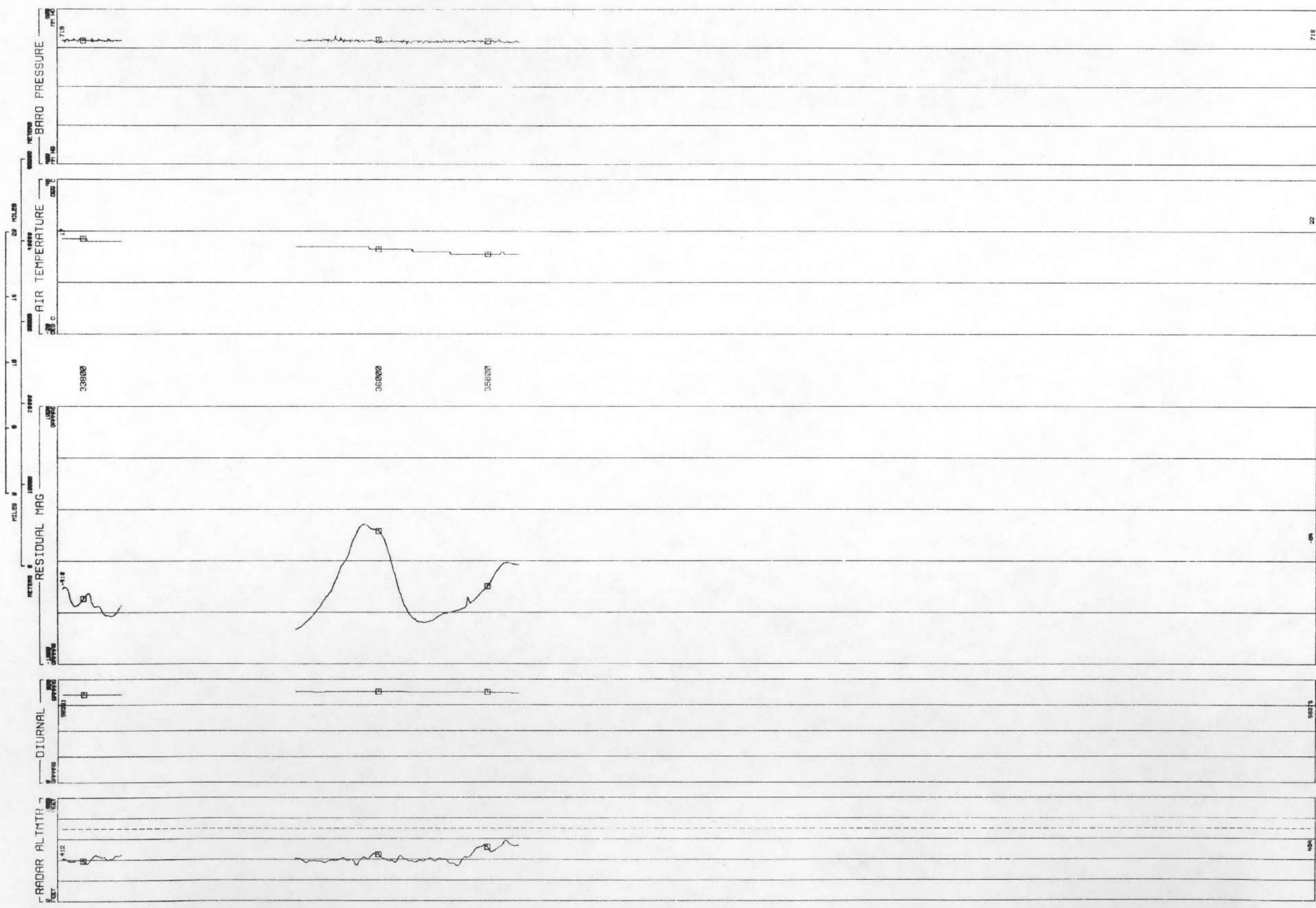
AIR TEMPERATURE
DEG C
MIN 11.00
MAX 19.00
MEAN 14.22
STD DEV 2.398

RESIDUAL MAG
GAMMAS
MIN -885.3
MAX -308.0
MEAN -687.1
STD DEV 118.2

DIURNAL
GAMMAS
MIN 58283
MAX 58318
MEAN 58297
STD DEV 13.64

RADAR ALTMTR
FEET
MIN 383.8
MAX 614.7
MEAN 432.9
STD DEV 66.97

LINE 30
MANITOWOC QUADRANGLE NTMS NL 16-11
DATA ACQUIRED 81158



BARO PRESSURE
MM HG
MIN 711.1
MAX 731.7
MEAN 718.0
STD DEV 2.207

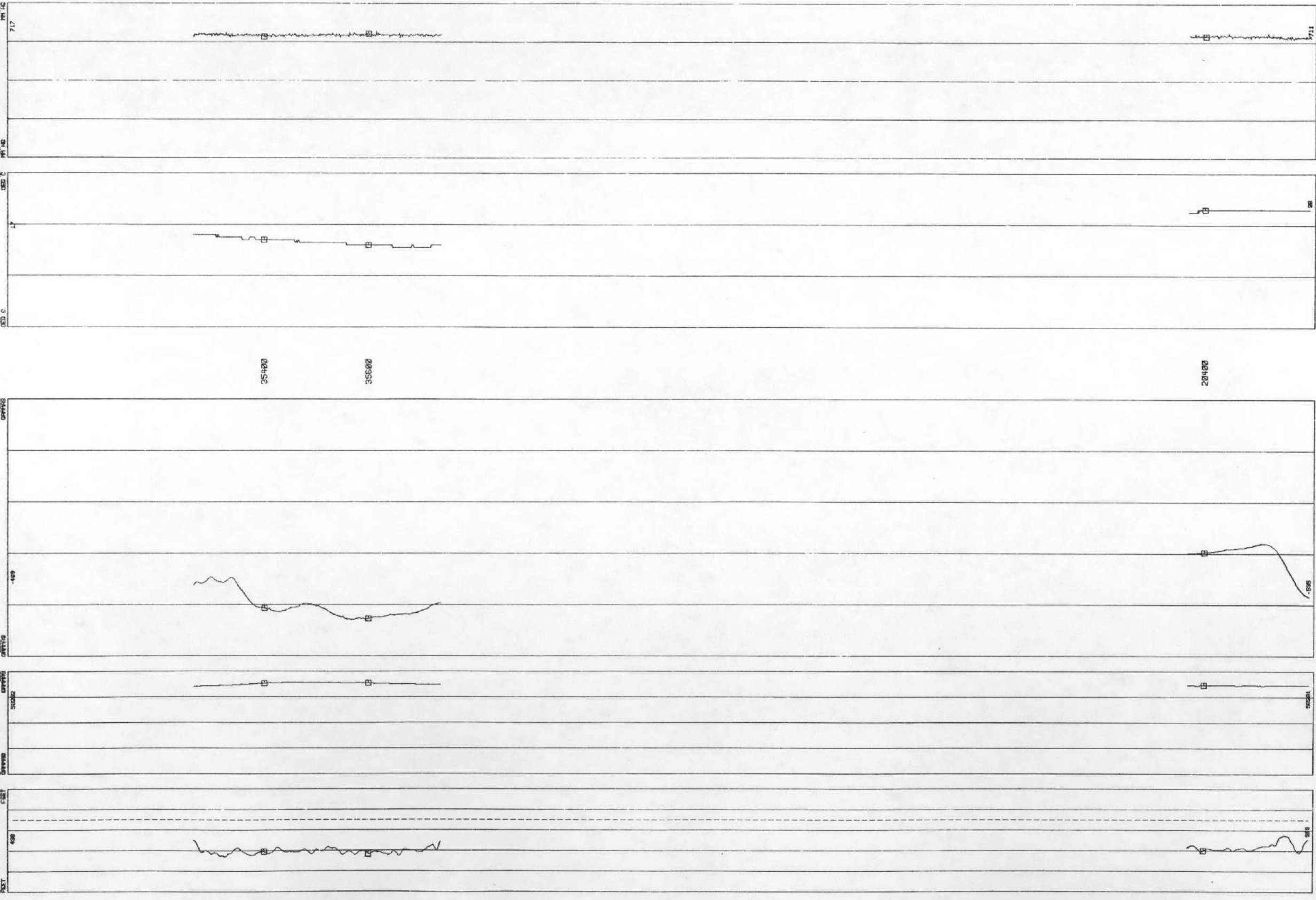
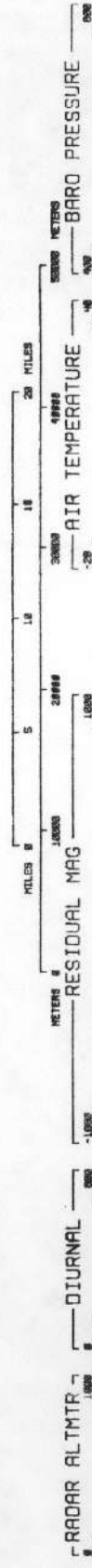
AIR TEMPERATURE
DEG C
MIN 11.00
MAX 22.00
MEAN 13.39
STD DEV 1.983

RESIDUAL MAG
GAMMAS
MIN -730.7
MAX 84.93
MEAN -427.7
STD DEV 224.9

DIURNAL
GAMMAS
MIN 58275
MAX 58304
MEAN 58296
STD DEV 8.777

RADAR ALTMTR
FEET
MIN 338.2
MAX 583.8
MEAN 420.5
STD DEV 52.48

LINE 40
MANITOWOC QUADRANGLE NTMS NL 16-11
DATA ACQUIRED 81158



BARO PRESSURE
MM HG

MIN	709.3
MAX	728.0
MEAN	716.9
STD DEV	2.378

AIR TEMPERATURE
DEG C

MIN	11.00
MAX	26.00
MEAN	17.14
STD DEV	5.992

RESIDUAL MAG
GPMAS

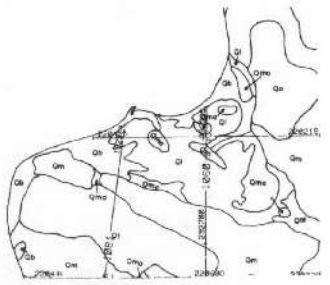
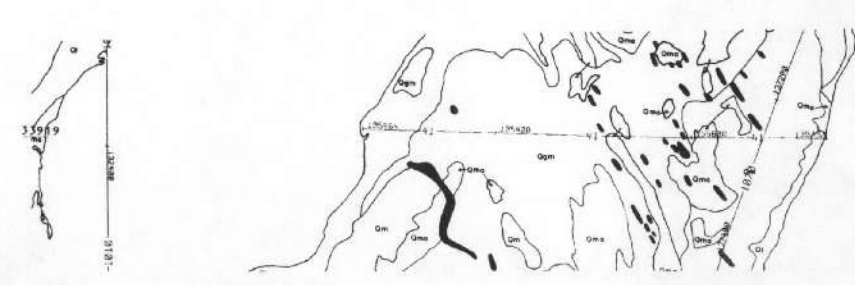
MIN	-717.3
MAX	-122.9
MEAN	-489.3
STD DEV	201.6

DIURNAL
GPMAS

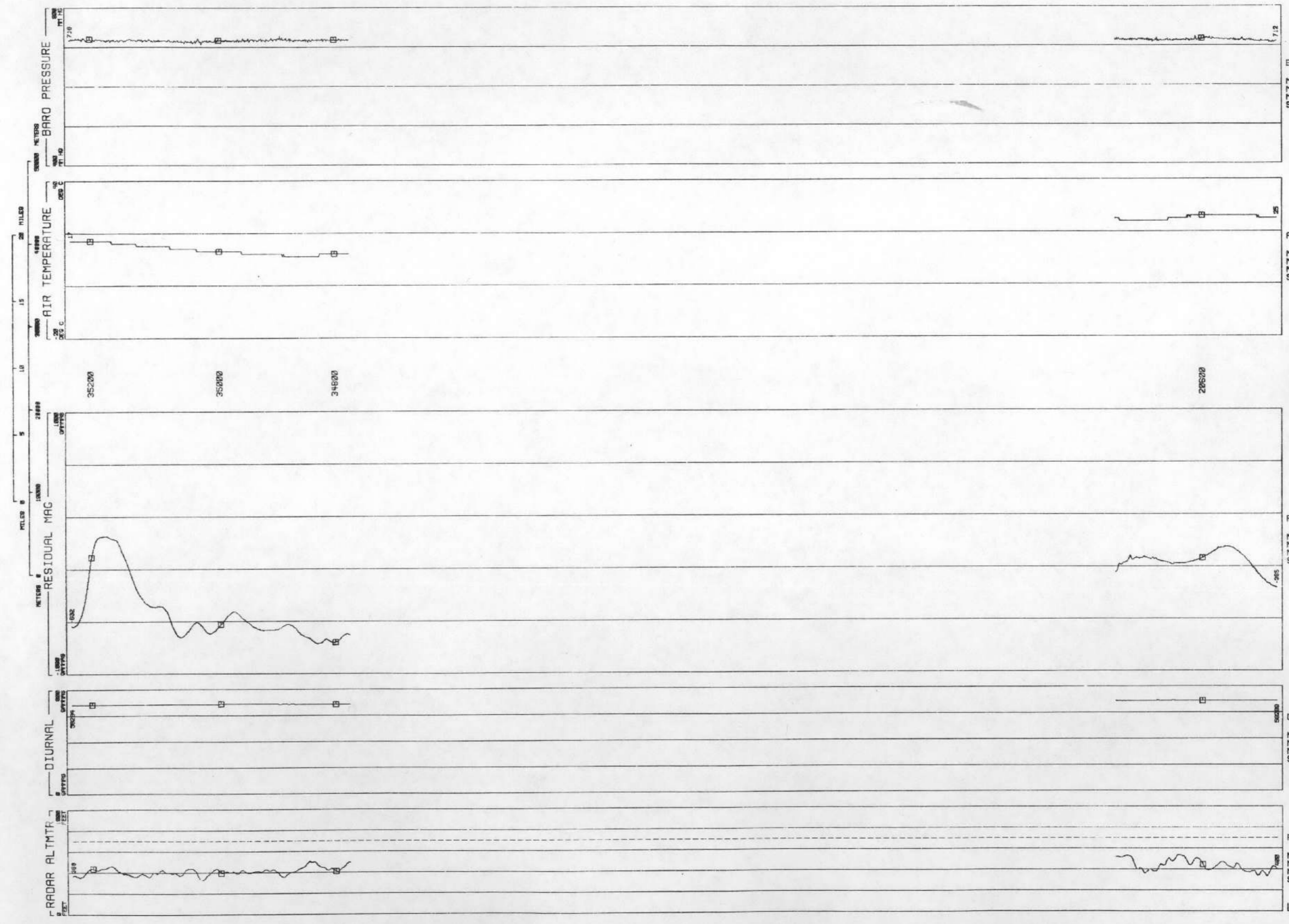
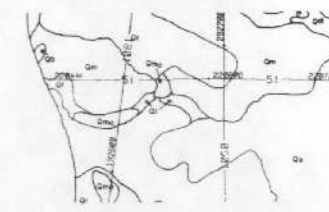
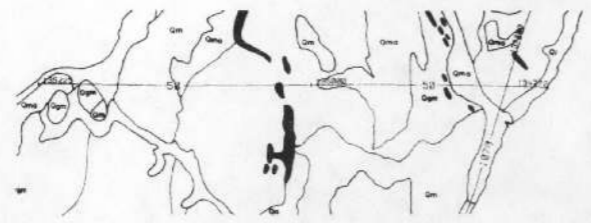
MIN	58281
MAX	58313
MEAN	58297
STD DEV	9.571

RADAR ALTMTR
FEET

MIN	340.1
MAX	552.5
MEAN	407.3
STD DEV	39.63



50
LINE
MANITOWOC QUADRANGLE NTMS NL 16-11
DATA ACQUIRED 81158



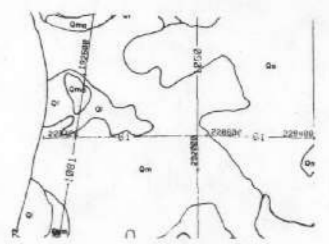
BARO PRESSURE
MM HG
MIN 706.6
MAX 728.5
MEAN 715.6
STD DEV 2.747

AIR TEMPERATURE
DEG C
MIN 11.00
MAX 26.00
MEAN 17.93
STD DEV 5.880

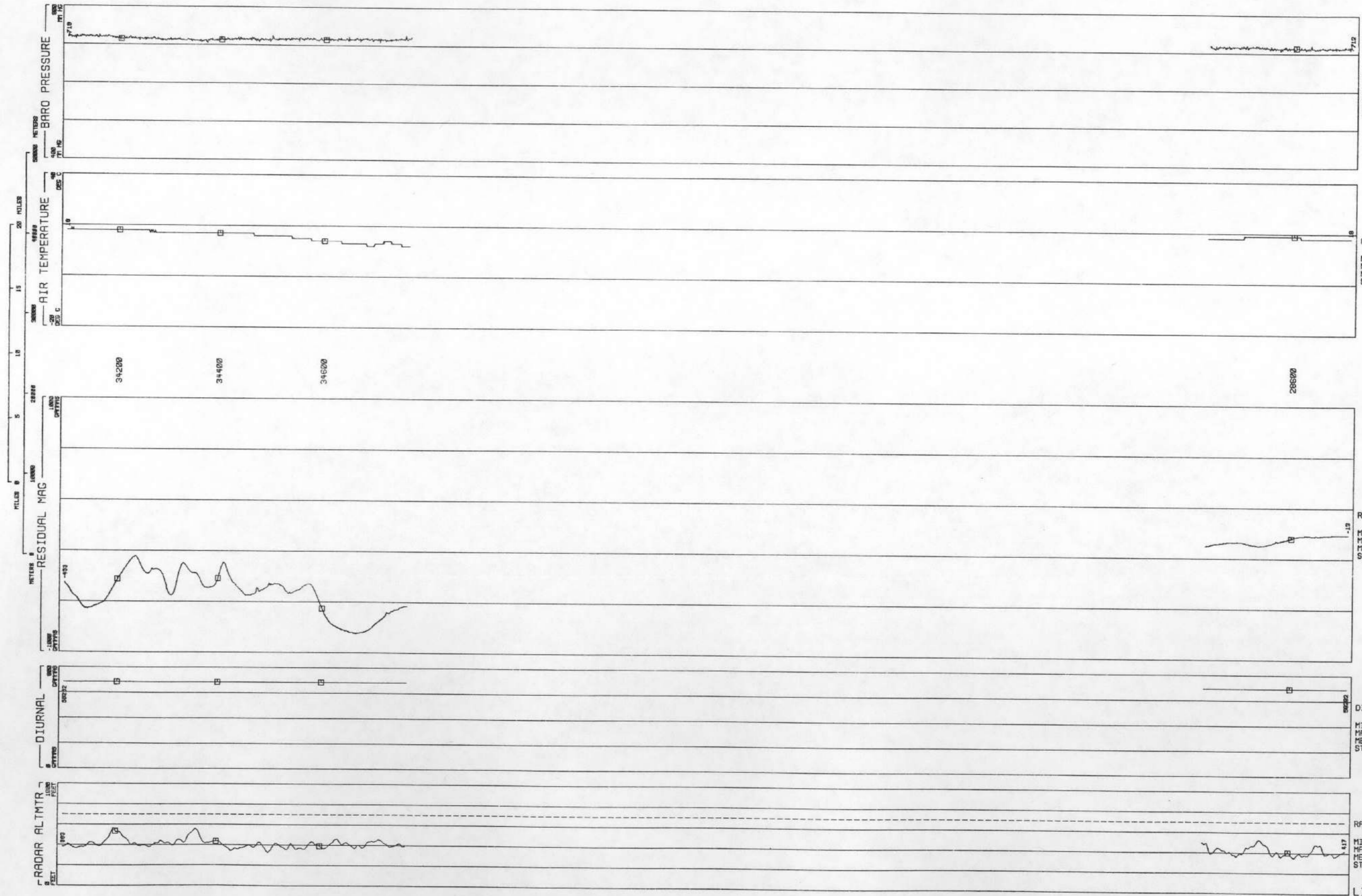
RESIDUAL MAG
GAMMAS
MIN -770.8
MAX 52.66
MEAN -486.4
STD DEV 262.1

DIURNAL
GAMMAS
MIN 58283
MAX 58290
MEAN 58285
STD DEV 2.864

RADAR ALTMTR
FEET
MIN 330.7
MAX 537.6
MEAN 421.6
STD DEV 45.52



LINE 60
 MANITOWOC QUADRANGLE NTMS NL 16-11
 DATA ACQUIRED 81158



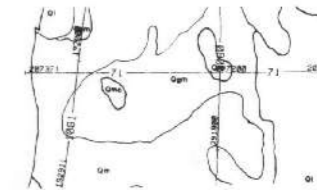
BARO PRESSURE
 MM HG
 MIN 705.3
 MAX 727.2
 MEAN 715.4
 STD DEV 2.894

AIR TEMPERATURE
 DEG C
 MIN 12.00
 MAX 16.00
 MEAN 16.70
 STD DEV 1.964

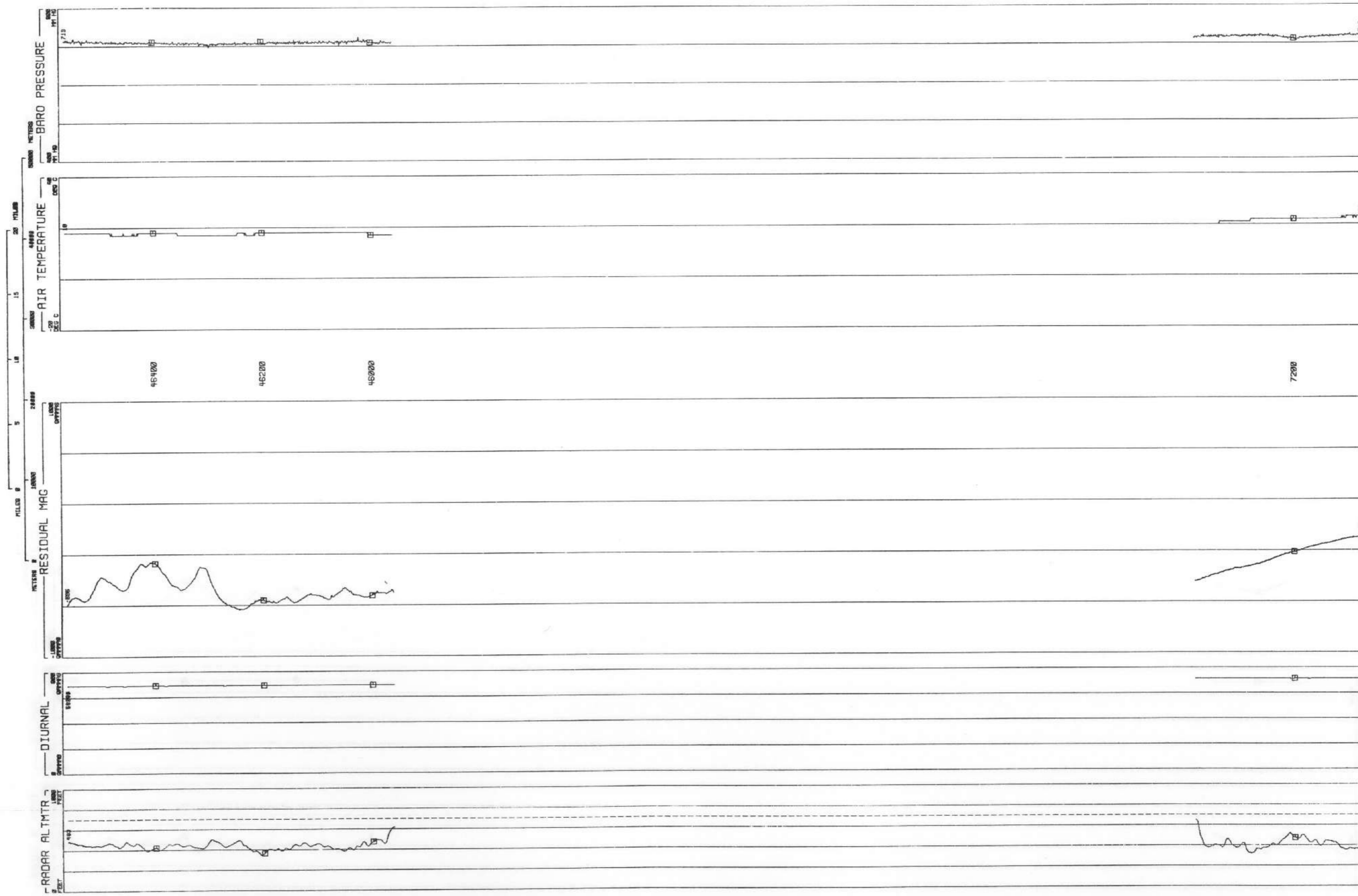
RESIDUAL MAG
 GAMMAS
 MIN -846.3
 MAX -10.98
 MEAN -391.2
 STD DEV 256.5

DIURNAL
 GAMMAS
 MIN 58282
 MAX 58293
 MEAN 58284
 STD DEV 4.357

RADAR ALTMTR
 FEET
 MIN 327.3
 MAX 555.1
 MEAN 413.8
 STD DEV 43.11



LINE 70
 MANITOWOC QUADRANGLE NTMS NL 16-11
 DATA ACQUIRED 81160



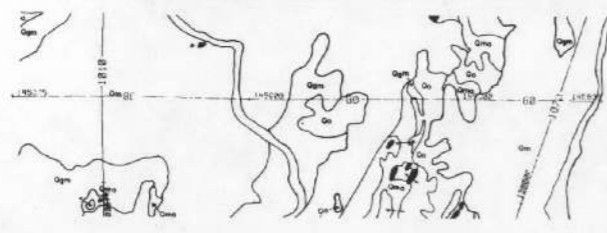
BARO PRESSURE
 MM HG
 MIN 698.0
 MAX 723.1
 MEAN 711.5
 STD DEV 4.491

AIR TEMPERATURE
 DEG C
 MIN 17.00
 MAX 23.00
 MEAN 18.92
 STD DEV 1.968

RESIDUAL MAG
 GAMMAS
 MIN -631.4
 MAX -36.07
 MEAN -410.2
 STD DEV 145.3

DIURNAL
 GAMMAS
 MIN 58289
 MAX 58313
 MEAN 58294
 STD DEV 9.929

RADAR ALTMTR
 FEET
 MIN 320.9
 MAX 651.1
 MEAN 431.5
 STD DEV 45.57



LINE 80
 MANITOWOC QUADRANGLE NTMS NL 16-11
 DATA ACQUIRED 81160



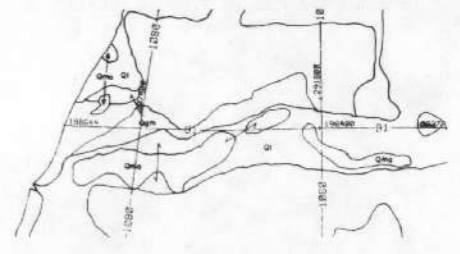
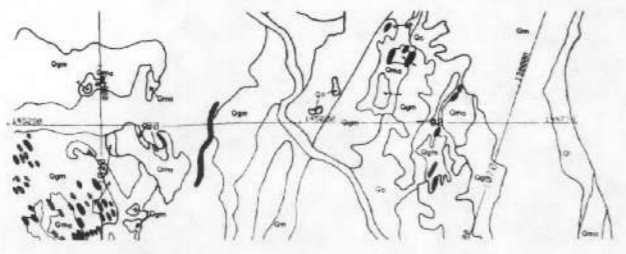
BARO PRESSURE
 MM HG
 MIN 701.9
 MAX 724.2
 MEAN 711.7
 STD DEV 5.067

AIR TEMPERATURE
 DEG C
 MIN 17.00
 MAX 22.00
 MEAN 18.39
 STD DEV 1.912

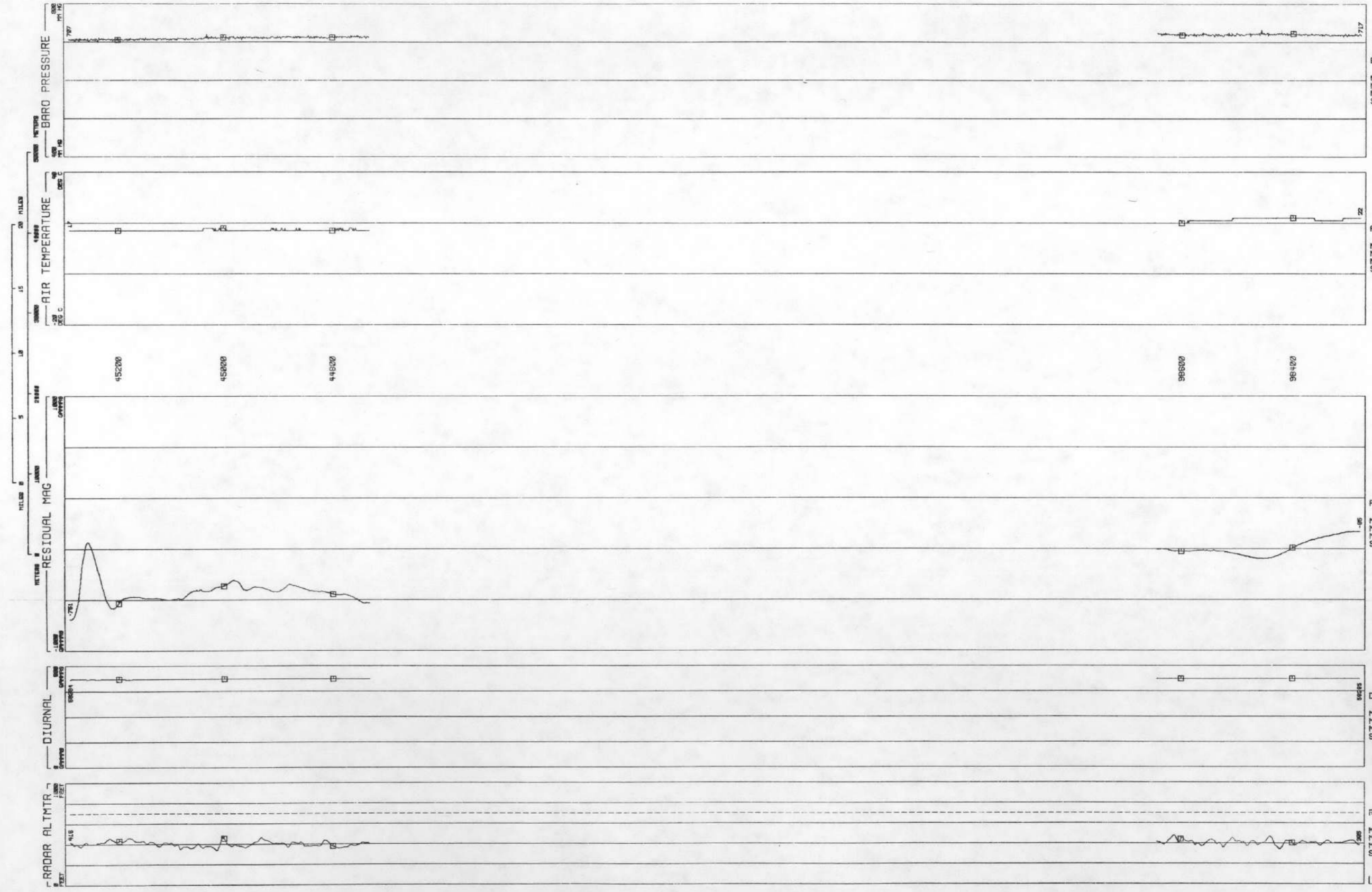
RESIDUAL MAG
 GRAMMAS
 MIN -644.4
 MAX -230.5
 MEAN -515.7
 STD DEV 98.57

DIURNAL
 GRAMMAS
 MIN 58291
 MAX 58297
 MEAN 58291
 STD DEV 3.286

RADAR ALTMTR
 FEET
 MIN 327.8
 MAX 529.8
 MEAN 411.5
 STD DEV 39.94



LINE 90
 MANITOWOC QUADRANGLE NTMS NL 16-11
 DATA ACQUIRED 81160



BARO PRESSURE
 MM HG
 MIN 698.8
 MAX 731.5
 MEAN 713.8
 STD DEV 5.866

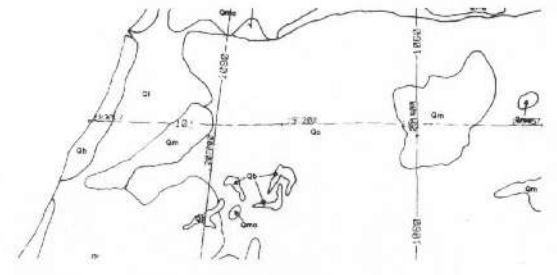
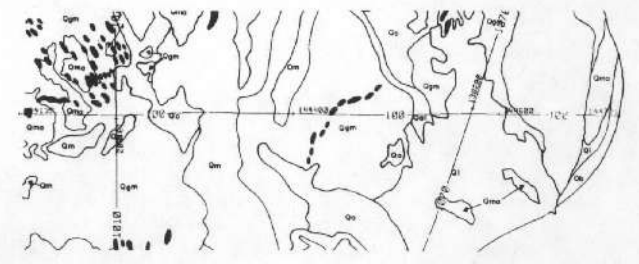
AIR TEMPERATURE
 DEG C
 MIN 17.00
 MAX 22.00
 MEAN 18.78
 STD DEV 2.134

RESIDUAL MAG
 GAMMAS
 MIN -751.5
 MAX -64.09
 MEAN -398.3
 STD DEV 186.8

DIURNAL
 GAMMAS
 MIN 58293
 MAX 58298
 MEAN 58292
 STD DEV 3.360

RADAR ALTMTR
 FEET
 MIN 338.9
 MAX 474.7
 MEAN 404.8
 STD DEV 25.09

LINE 100
MANITOWOC QUADRANGLE NTMS NL 16-11
DATA ACQUIRED 81160



BARO PRESSURE
MM HG
MIN 699.6
MAX 729.1
MEAN 714.5
STD DEV 5.243

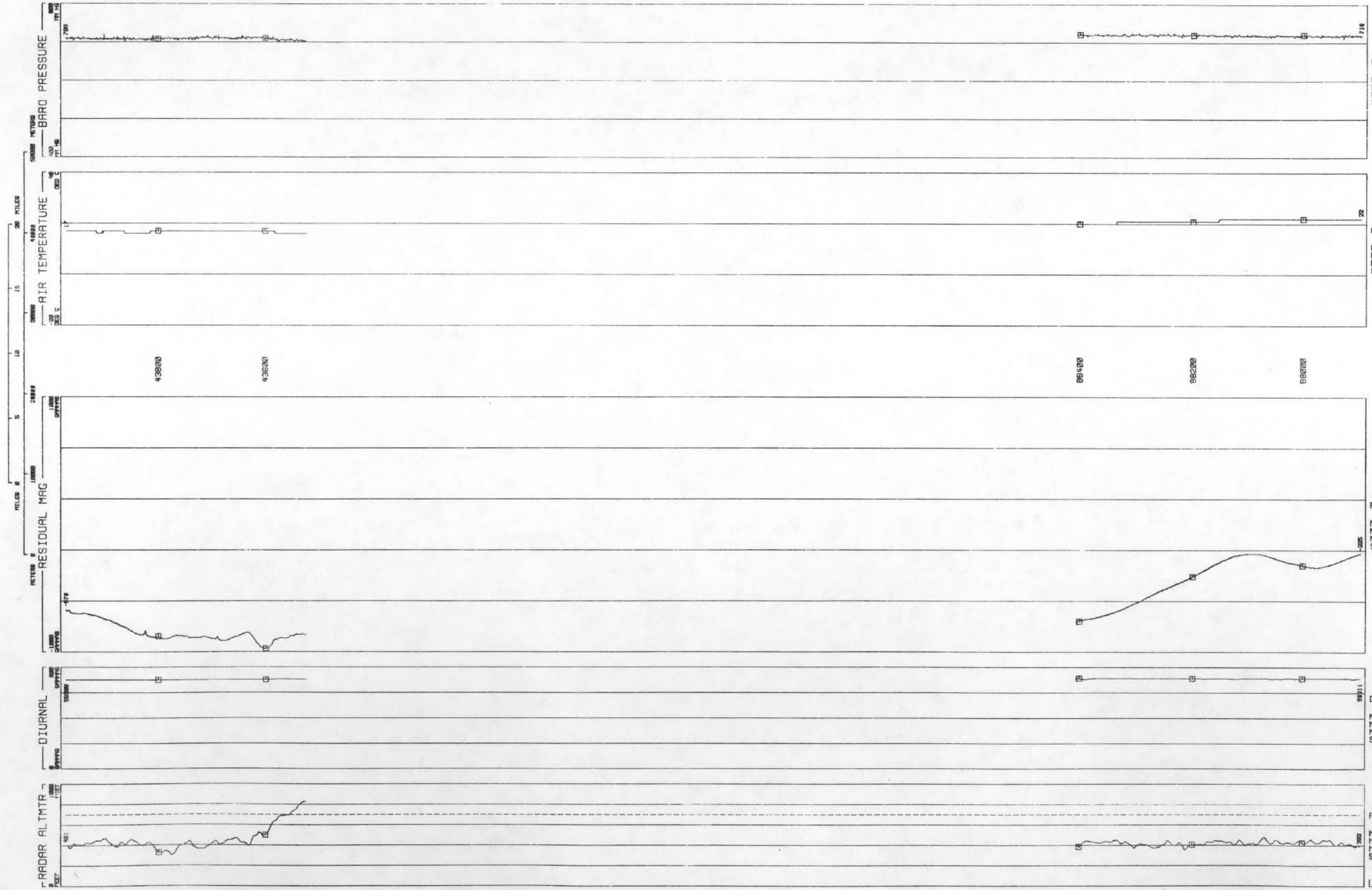
AIR TEMPERATURE
DEG C
MIN 16.00
MAX 21.00
MEAN 18.32
STD DEV 1.422

RESIDUAL MAG
GAMMAS
MIN -899.8
MAX 165.9
MEAN -437.8
STD DEV 305.2

DIURNAL
GAMMAS
MIN 58292
MAX 58300
MEAN 58293
STD DEV 4.292

RADAR ALTMTR
FEET
MIN 342.1
MAX 515.5
MEAN 400.3
STD DEV 32.12

LINE 110
MANITOWOC QUADRANGLE NTMS NL 16-11
DATA ACQUIRED 8.1160



BARO PRESSURE
MM HG
MIN 700.1
MAX 725.8
MEAN 714.4
STD DEV 5.896

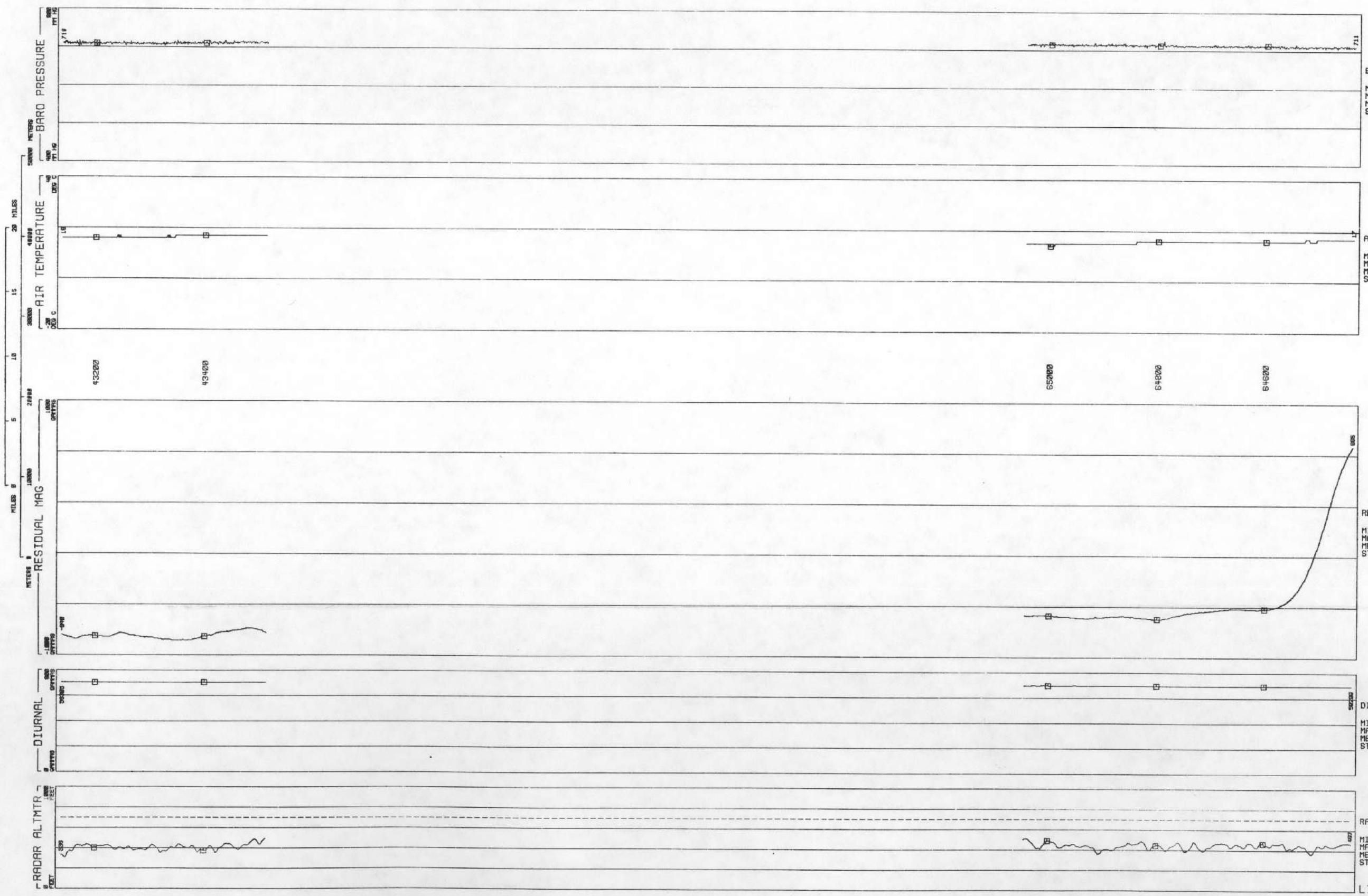
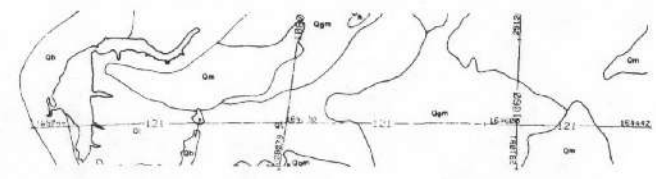
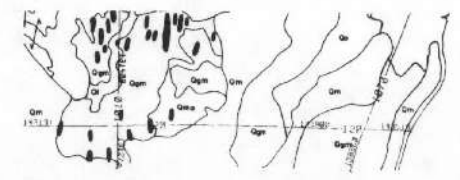
AIR TEMPERATURE
DEG C
MIN 16.00
MAX 22.00
MEAN 19.19
STD DEV 2.387

RESIDUAL MAG
GAMMAS
MIN -977.6
MAX -618.0
MEAN -618.0
STD DEV 254.8

DIURNAL
GAMMAS
MIN 58299
MAX 58311
MEAN 58303
STD DEV 5.825

RADAR ALTMTR
FEET
MIN 304.3
MAX 828.0
MEAN 437.7
STD DEV 82.68

LINE 120
MANITOWOC QUADRANGLE NTMS NL 16-11
DATA ACQUIRED 811160



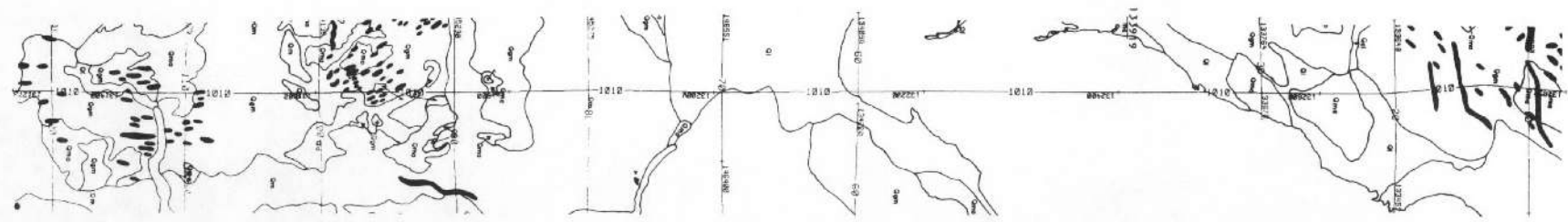
BARO PRESSURE
MM HG
MIN 701.7
MAX 724.2
MEAN 712.0
STD DEV 2.887

AIR TEMPERATURE
DEG C
MIN 14.00
MAX 17.00
MEAN 16.04
STD DEV .7828

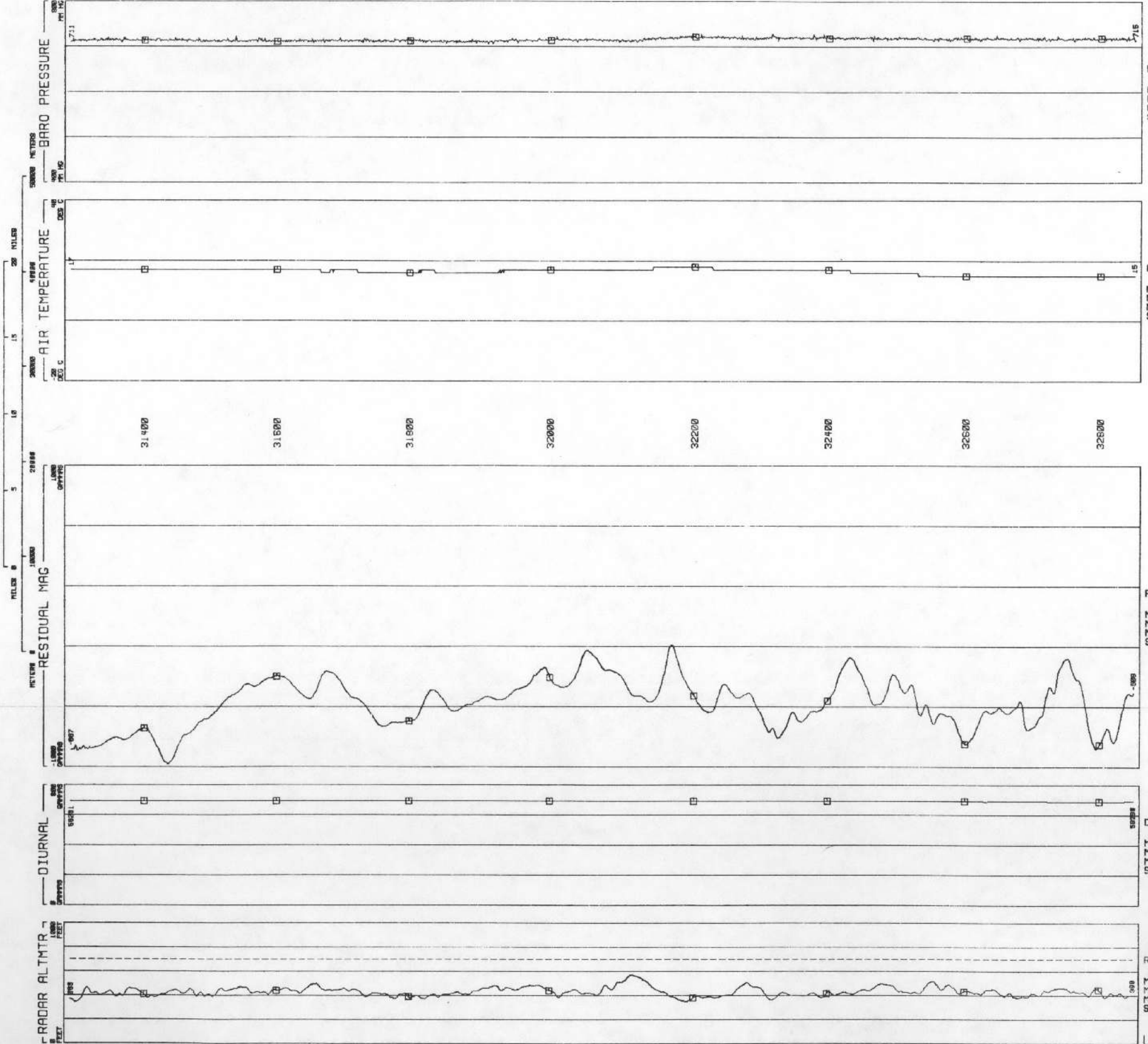
RESIDUAL MAG
GAMMAS
MIN 884.1
MAX 664.6
MEAN 651.5
STD DEV 288.8

DIURNAL
GAMMAS
MIN 58295
MAX 58305
MEAN 58299
STD DEV 3.692

RADAR ALTMTR
FEET
MIN 311.6
MAX 511.2
MEAN 426.8
STD DEV 33.31



LINE 1010
 MANITOWOC QUADRANGLE NTMS NL 16-11
 DATA ACQUIRED 81158



BARO PRESSURE
 MM HG
 MIN 705.1
 MAX 728.3
 MEAN 715.5
 STD DEV 3.684

AIR TEMPERATURE
 DEG C
 MIN 15.00
 MAX 18.00
 MEAN 16.46
 STD DEV .8756

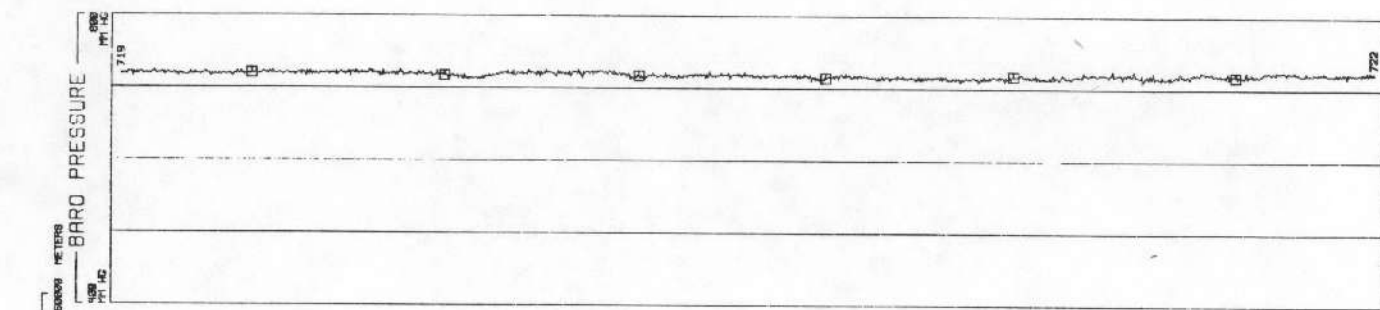
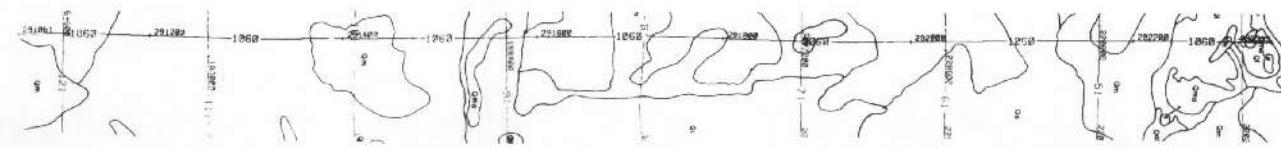
RESIDUAL MAG
 GAMMAS
 MIN -982.0
 MAX -191.0
 MEAN -584.7
 STD DEV 162.6

DIURNAL
 GAMMAS
 MIN 58289
 MAX 58293
 MEAN 58288
 STD DEV 2.969

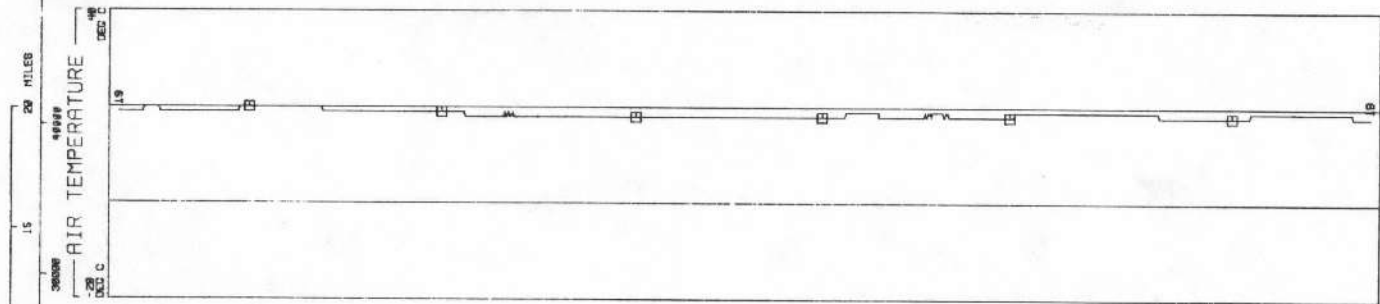
RADAR ALTMTR
 FEET
 MIN 346.8
 MAX 568.9
 MEAN 429.4
 STD DEV 36.31

LINE 1010

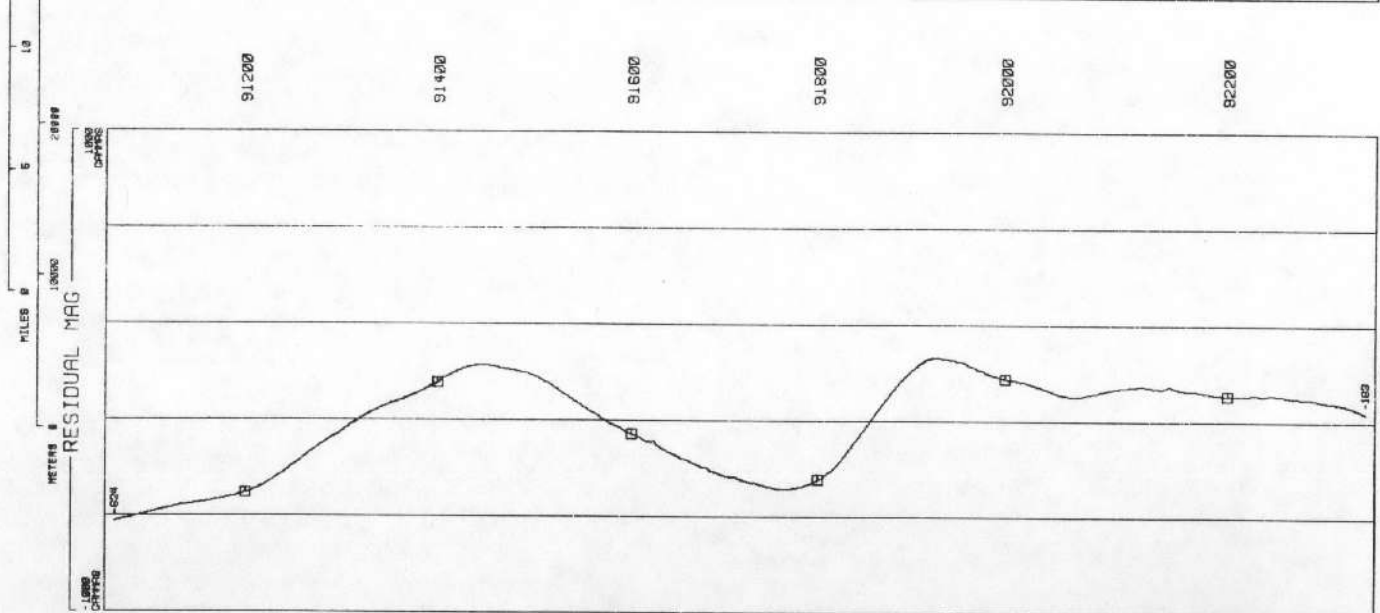
LINE 1060
MANITOWOC QUADRANGLE NTMS NL 16-11
DATA ACQUIRED 81163



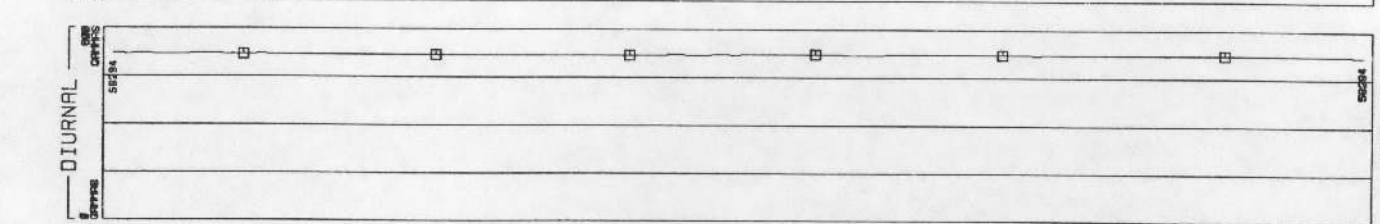
BARO PRESSURE
MM HG
MIN 709.3
MAX 725.6
MEAN 718.2
STD DEV 2.968



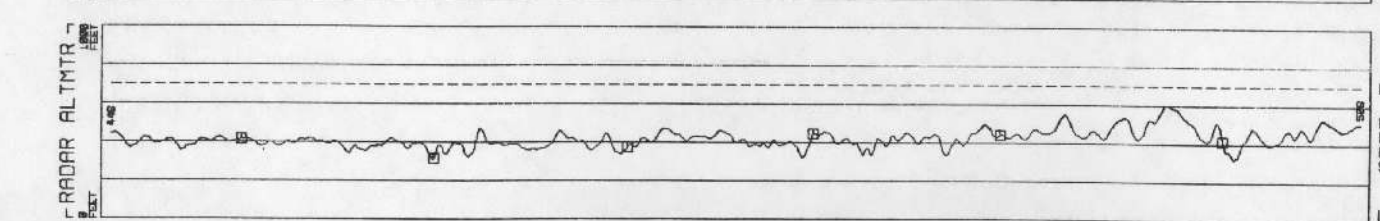
AIR TEMPERATURE
DEG C
MIN 18.00
MAX 20.00
MEAN 18.58
STD DEV .6173



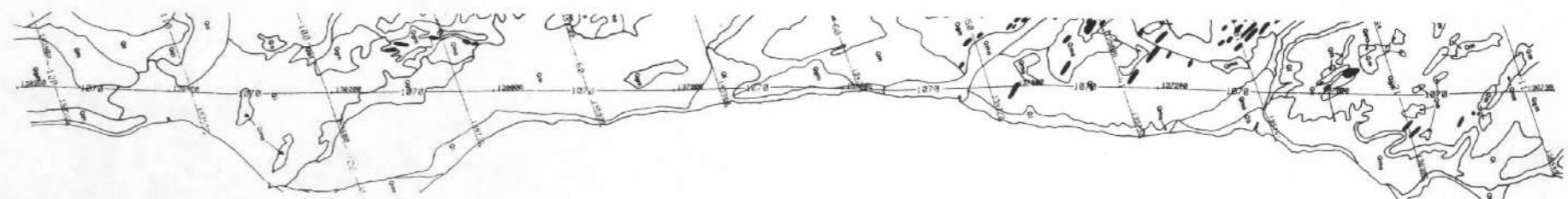
RESIDUAL MAG
GAMMAS
MIN -624.4
MAX 64.95
MEAN -207.1
STD DEV 184.1



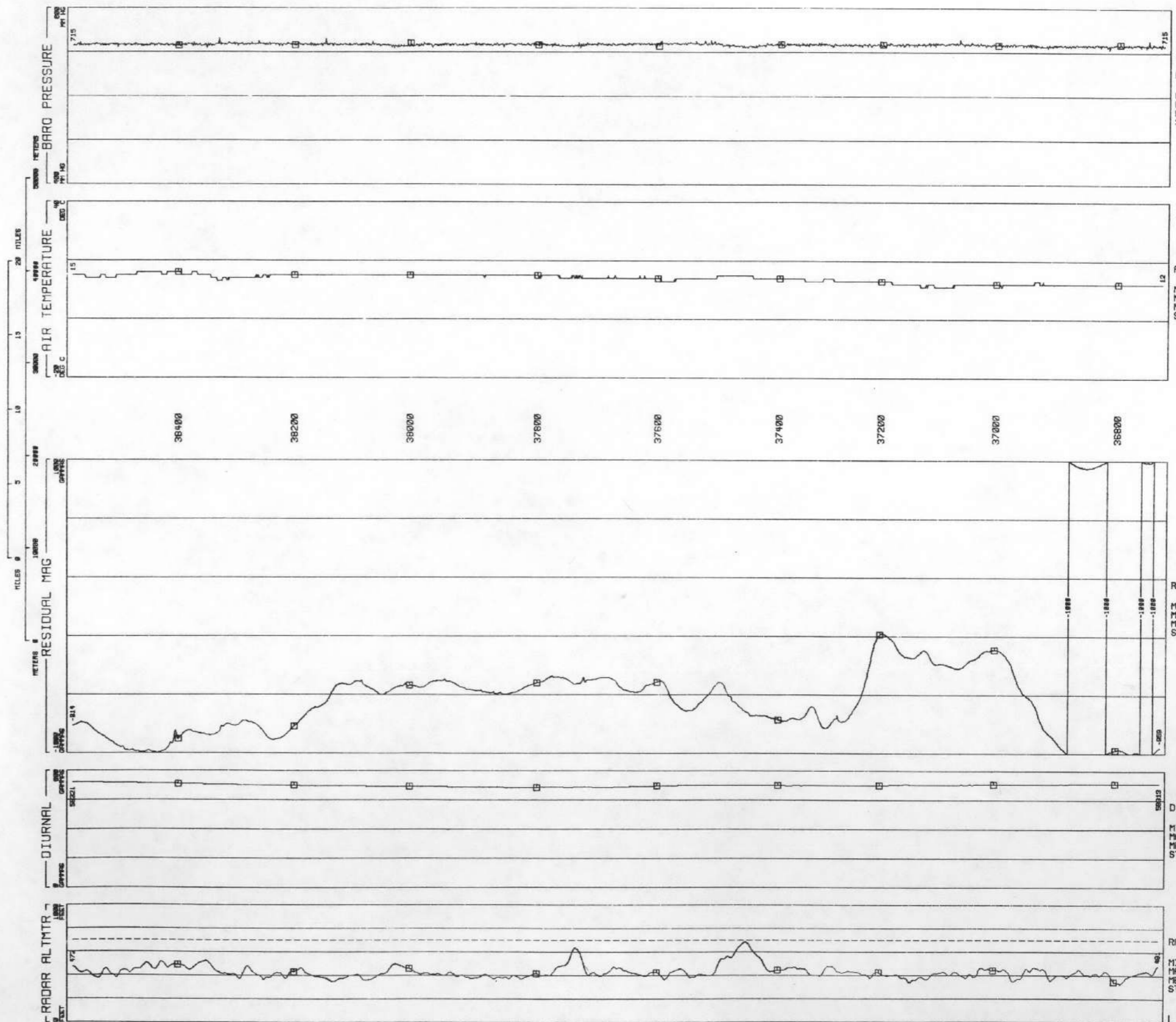
DIURNAL
GAMMAS
MIN 5829.2
MAX 5829.6
MEAN 5829.6
STD DEV 4.897



RADAR ALTMTR
FEET
MIN 312.0
MAX 602.3
MEAN 417.9
STD DEV 48.14



LINE 1070
 MANITOWOC QUADRANGLE NTMS NL 16-11
 DATA ACQUIRED 81158



BARO PRESSURE
 MM HG
 MIN 708.3
 MAX 731.0
 MEAN 716.7
 STD DEV 2.245

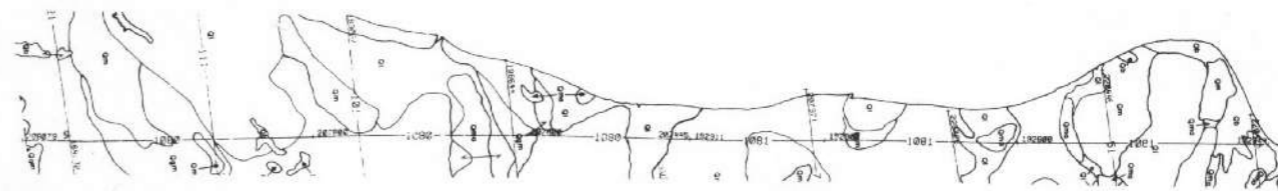
AIR TEMPERATURE
 DEG C
 MIN 11.00
 MAX 16.00
 MEAN 13.85
 STD DEV 1.297

RESIDUAL MAG
 GAMMAS
 MIN -1051
 MAX -181.8
 MEAN -660.5
 STD DEV 209.7

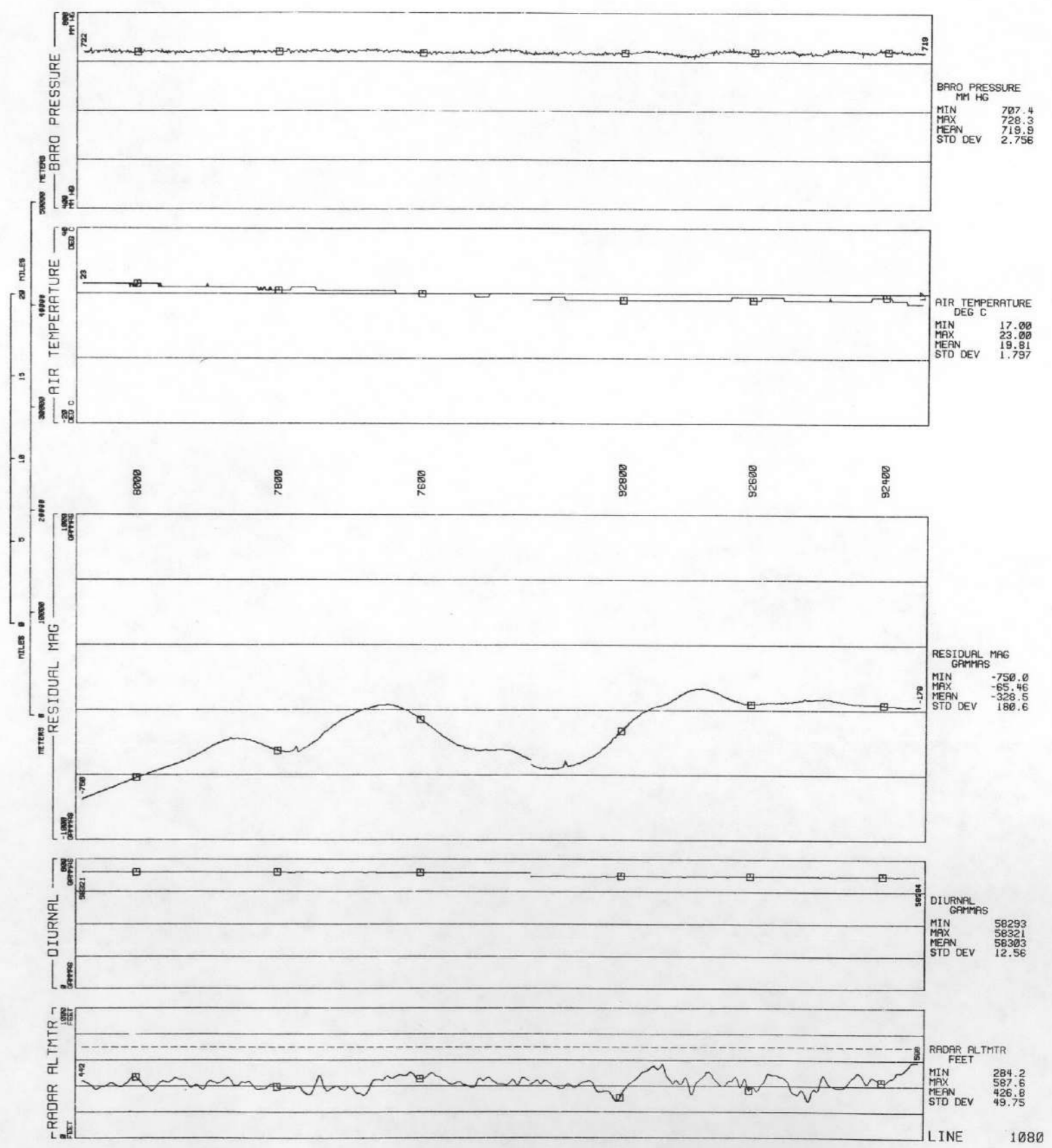
DIURNAL
 GAMMAS
 MIN 58284
 MAX 58321
 MEAN 58296
 STD DEV 18.04

RADAR ALTMTR
 FEET
 MIN 332.4
 MAX 685.0
 MEAN 429.2
 STD DEV 54.41

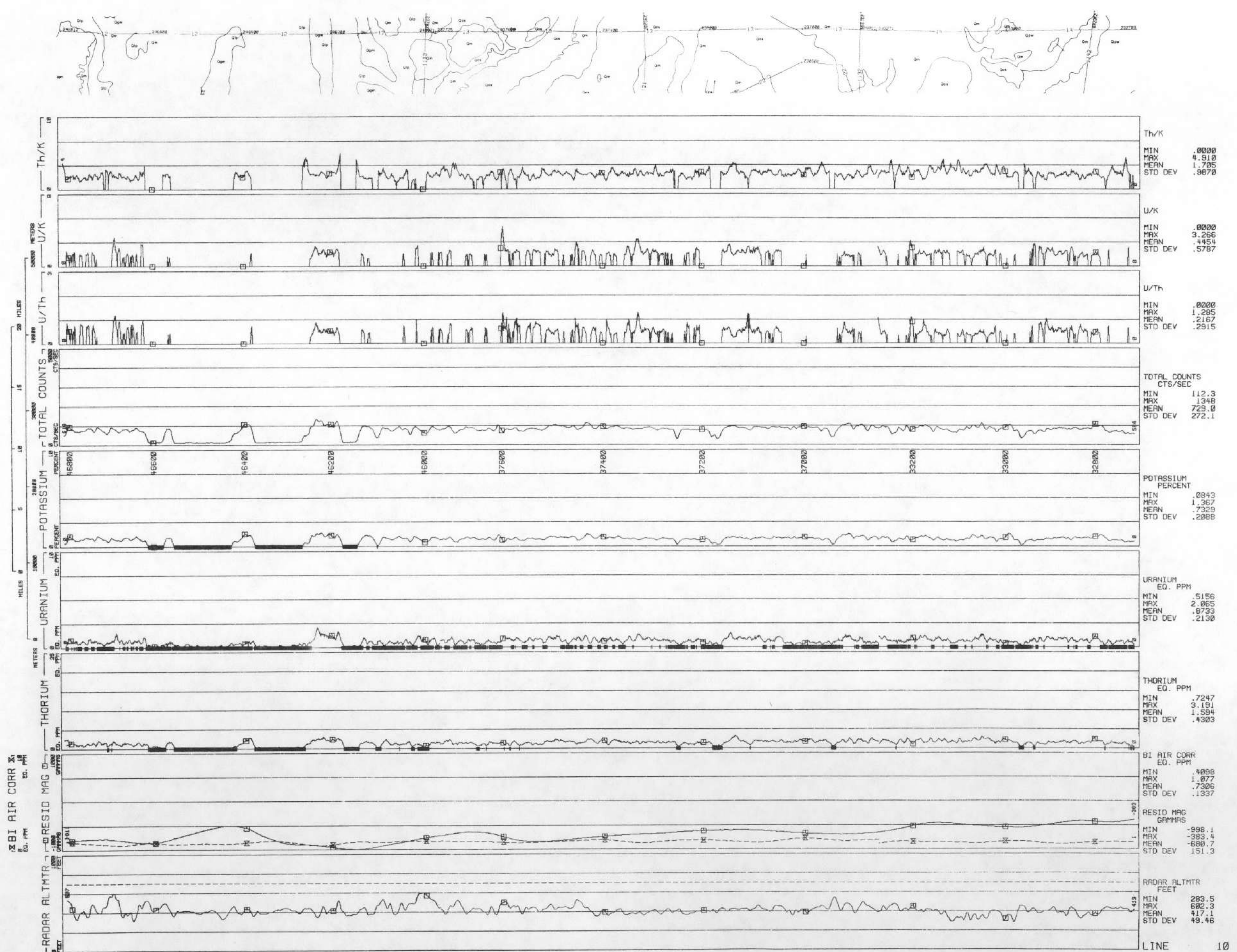
LINE 1070

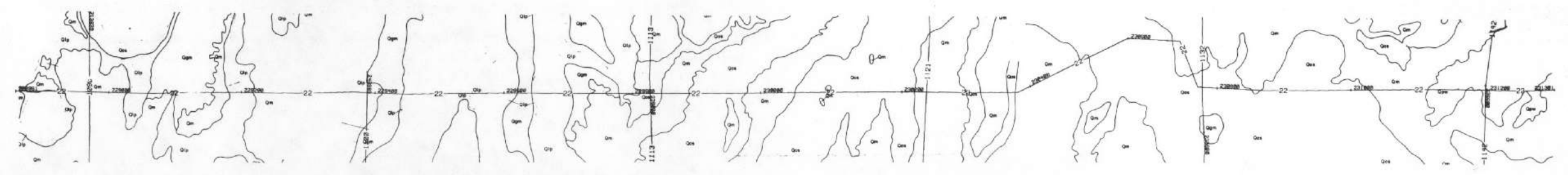


LINE 1080
 MANITOWOC QUADRANGLE NTMS NL 16-11
 DATA ACQUIRED 81163

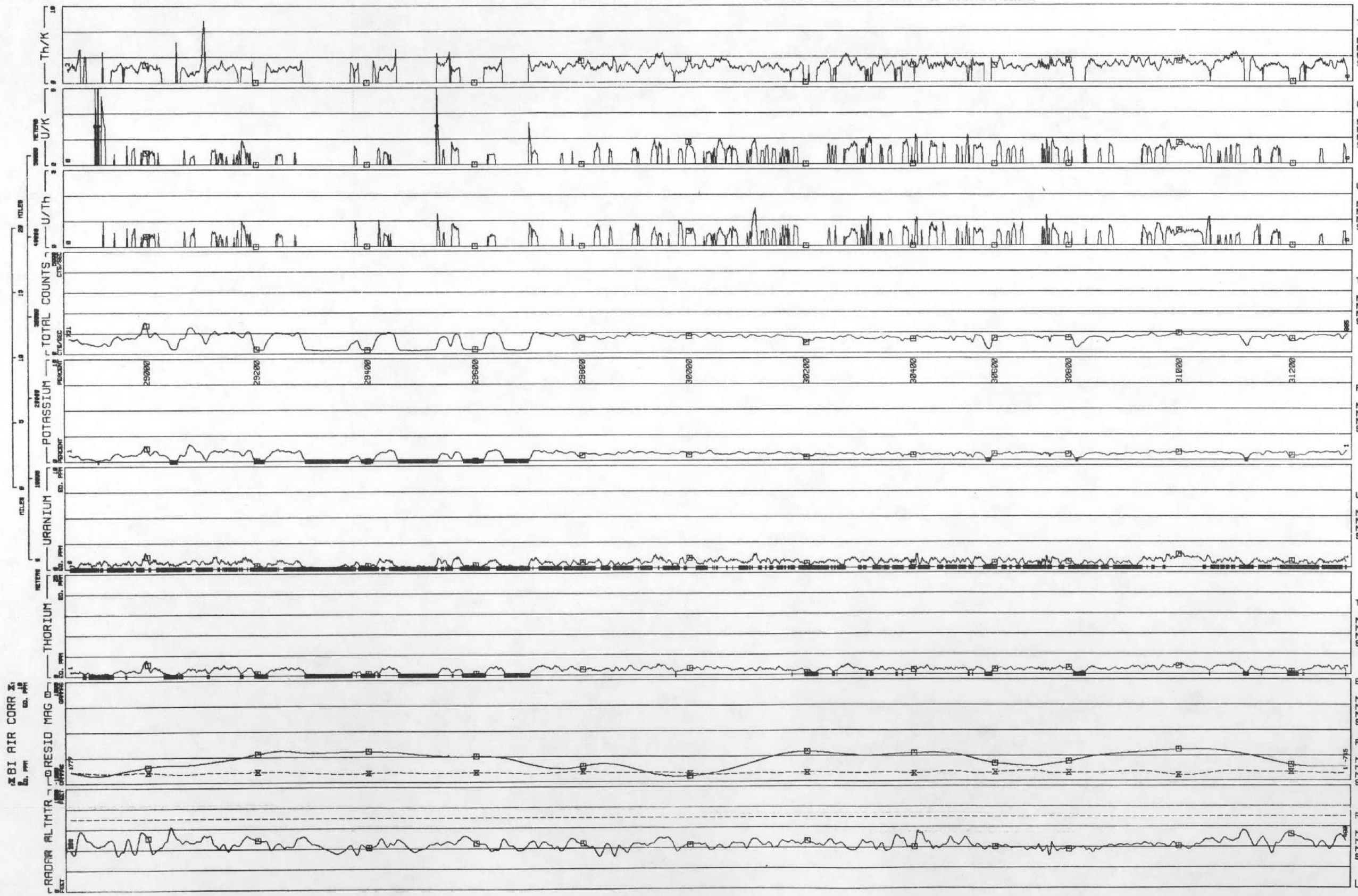


LINE 10
TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
DATA ACQUIRED 81158

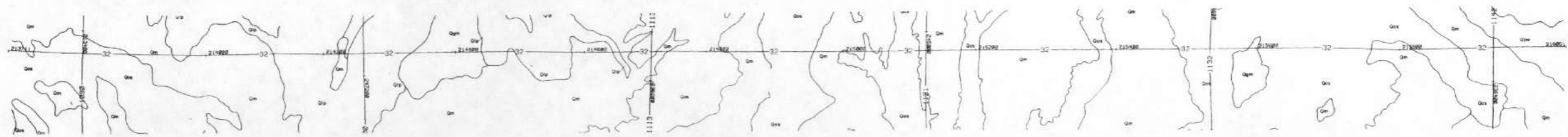




TRaverse CITY QUADRANGLE - NTMS NL 16-12
 DATA ACQUIRED 81158

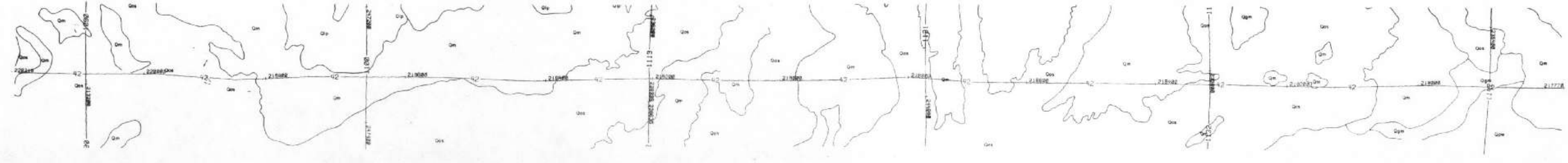


Th/K	MIN .0000
	MAX 8.025
	MEAN 1.724
	STD DEV 1.033
U/K	MIN .0000
	MAX 7.391
	MEAN .3810
	STD DEV .6733
U/Th	MIN .0000
	MAX 1.479
	MEAN .1644
	STD DEV .2786
TOTAL COUNTS CTS/SEC	MIN 147.1
	MAX 1528
	MEAN 704.2
	STD DEV 239.5
POTASSIUM PERCENT	MIN .0788
	MAX 1.676
	MEAN .6475
	STD DEV .2061
URANIUM EQ. PPM	MIN .5091
	MAX 1.574
	MEAN .8235
	STD DEV .1548
THORIUM EQ. PPM	MIN .6500
	MAX 3.858
	MEAN 1.462
	STD DEV .3921
BI AIR CORR EQ. PPM	MIN .5264
	MAX 1.138
	MEAN .8785
	STD DEV .1008
RESID MAG GAMMAS	MIN -901.5
	MAX -373.0
	MEAN -572.5
	STD DEV 143.4
RADAR ALTMTR FEET	MIN 328.1
	MAX 628.4
	MEAN 434.8
	STD DEV 46.89

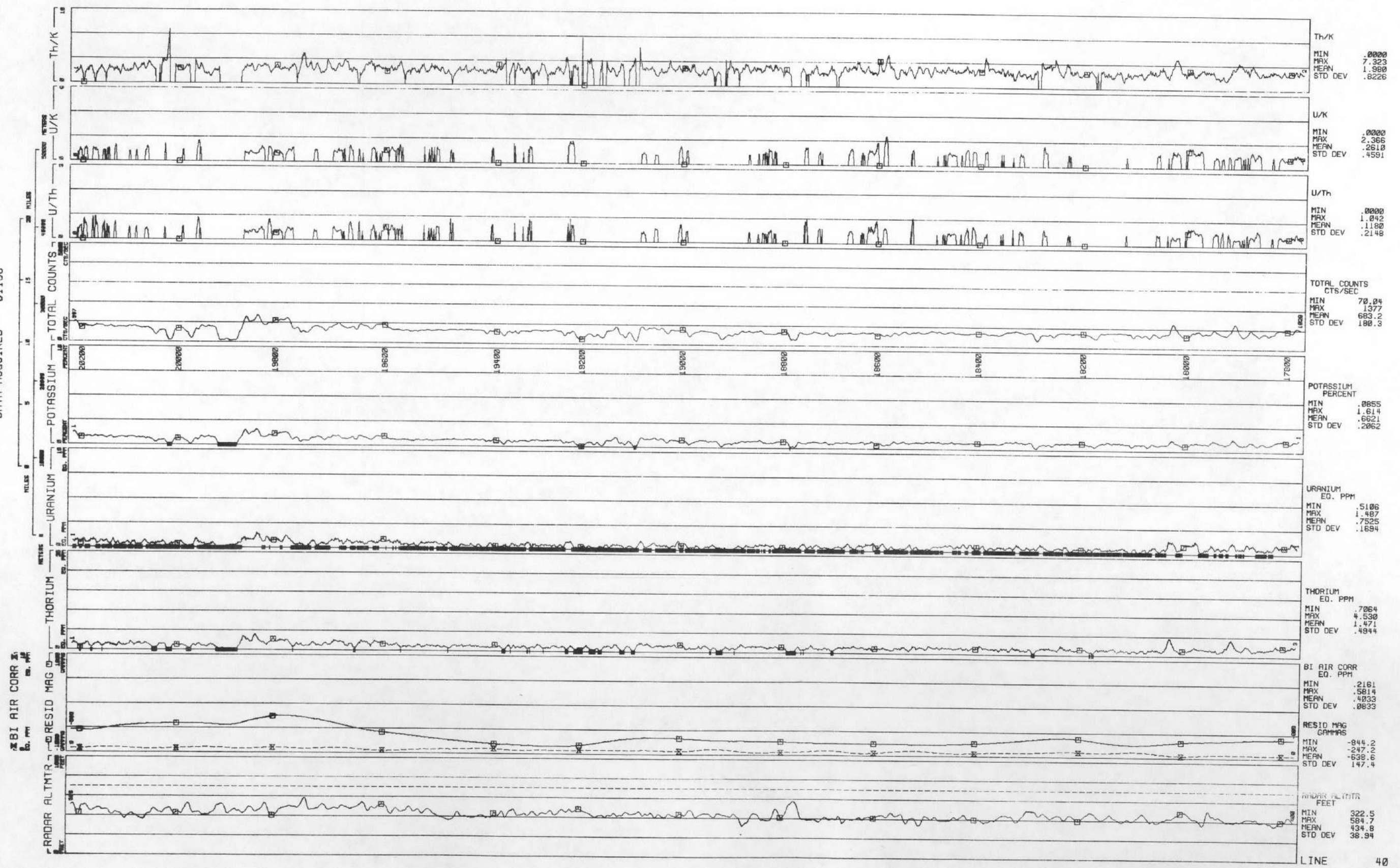


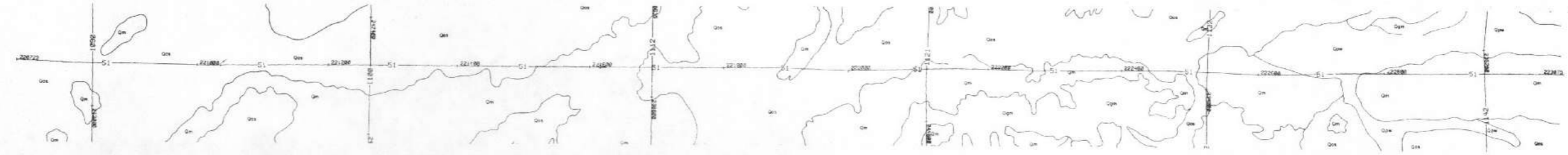
LINE 30
 TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
 DATA ACQUIRED 81158



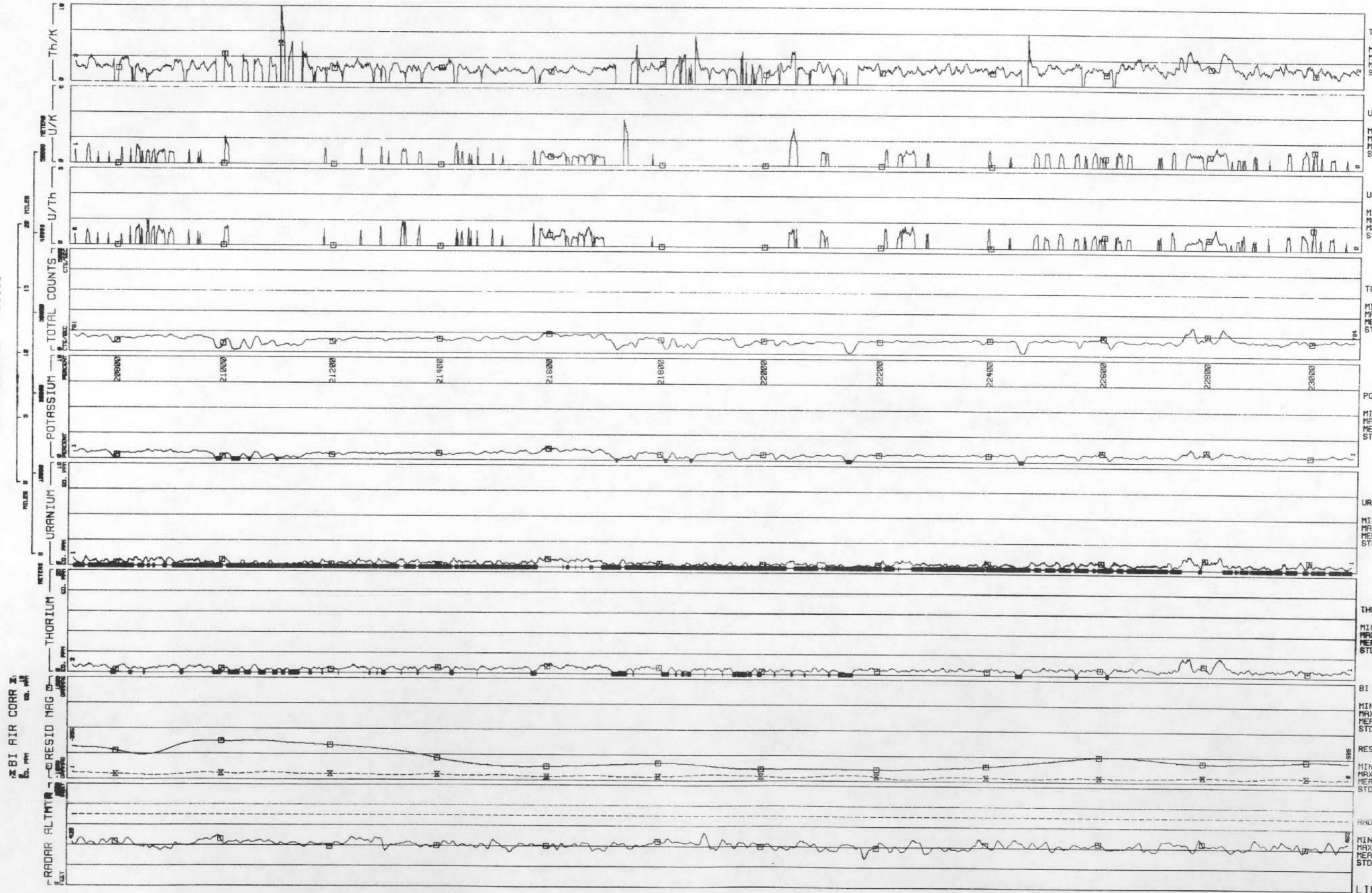


LINE 40
 TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
 DATA ACQUIRED 81158





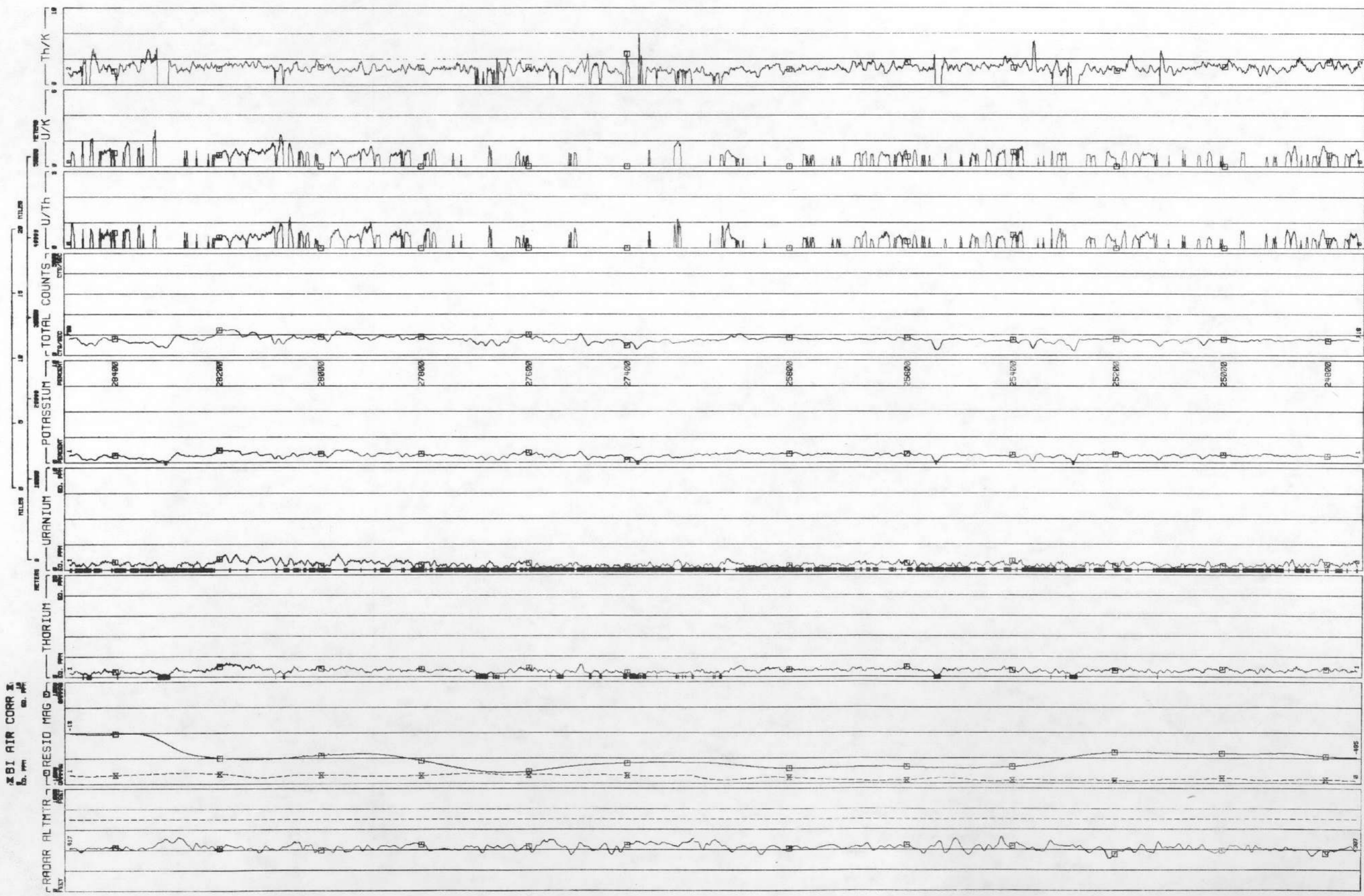
LINE 50
TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
DATA ACQUIRED 81158



Th/K	MIN .0000 MAX 10.33 MEAN 1.881 STD DEV .9845
U/K	MIN .0000 MAX 3.576 MEAN .2134 STD DEV .4467
U/Th	MIN .0000 MAX .9800 MEAN .0983 STD DEV .2075
TOTAL COUNTS CTS/SEC	MIN 70.76 MAX 1411 MEAN 654.8 STD DEV 169.9
POTASSIUM PERCENT	MIN .0777 MAX 1.336 MEAN .6209 STD DEV .1951
URANIUM EQ. PPM	MIN .5033 MAX 1.374 MEAN .6971 STD DEV .1494
THORIUM EQ. PPM	MIN .6776 MAX 4.628 MEAN 1.374 STD DEV .5044
BI AIR CORR EQ. PPM	MIN .1988 MAX .6800 MEAN .4562 STD DEV .0934
RESID MAG GAMMAS	MIN -769.4 MAX -228.6 MEAN -580.1 STD DEV 162.1
RADAR ALTIMETER FEET	MIN 288.6 MAX 528.6 MEAN 415.1 STD DEV 30.35



LINE 60
 TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
 DATA ACQUIRED 01158



Th/K
 MIN .0000
 MAX 6.579
 MEAN 2.850
 STD DEV .7588

U/K
 MIN .0000
 MAX 2.824
 MEAN .3503
 STD DEV .5246

U/Th
 MIN .0000
 MAX 1.227
 MEAN .1635
 STD DEV .2497

TOTAL COUNTS
 CTS/SEC
 MIN 217.2
 MAX 1254
 MEAN 760.0
 STD DEV 144.5

POTASSIUM
 PERCENT
 MIN .0031
 MAX 1.259
 MEAN .7019
 STD DEV .1096

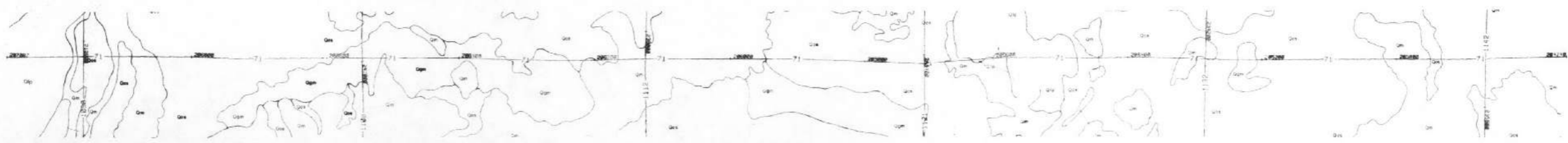
URANIUM
 ED. PPM
 MIN .4999
 MAX 1.551
 MEAN .7793
 STD DEV .1650

THORIUM
 ED. PPM
 MIN .7238
 MAX 3.349
 MEAN 1.552
 STD DEV .4431

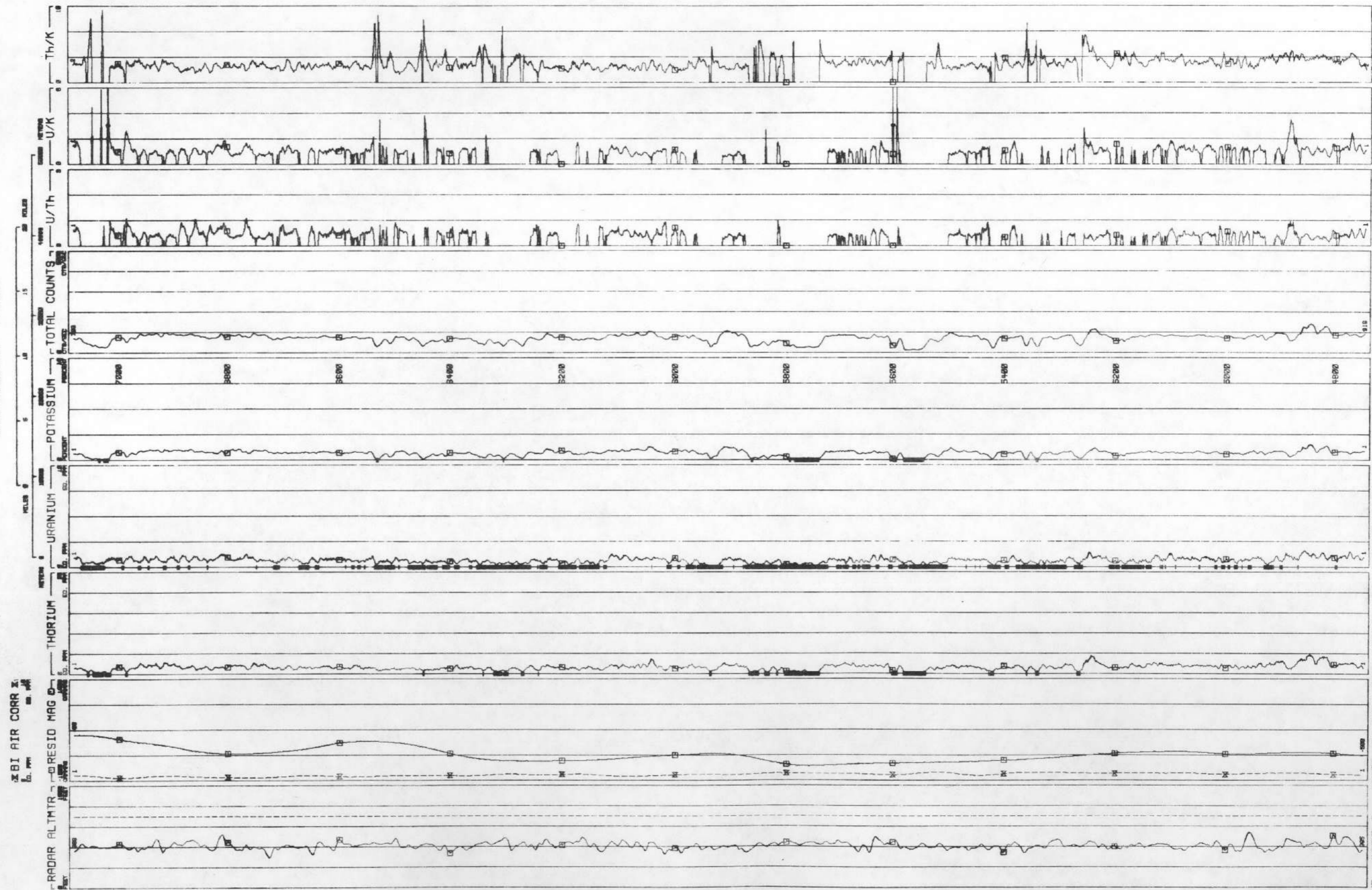
BI AIR CORR
 ED. PPM
 MIN 2052
 MAX 1.058
 MEAN .6085
 STD DEV .2584

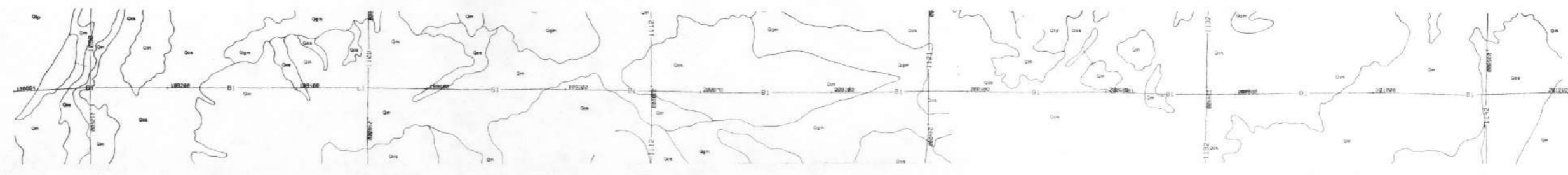
RESID MAG
 GAMMAS
 MIN -781.3
 MAX -5.477
 MEAN -518.9
 STD DEV 181.2

RADAR ALTMTR
 FEET
 MIN 313.8
 MAX 526.9
 MEAN 422.9
 STD DEV 31.40

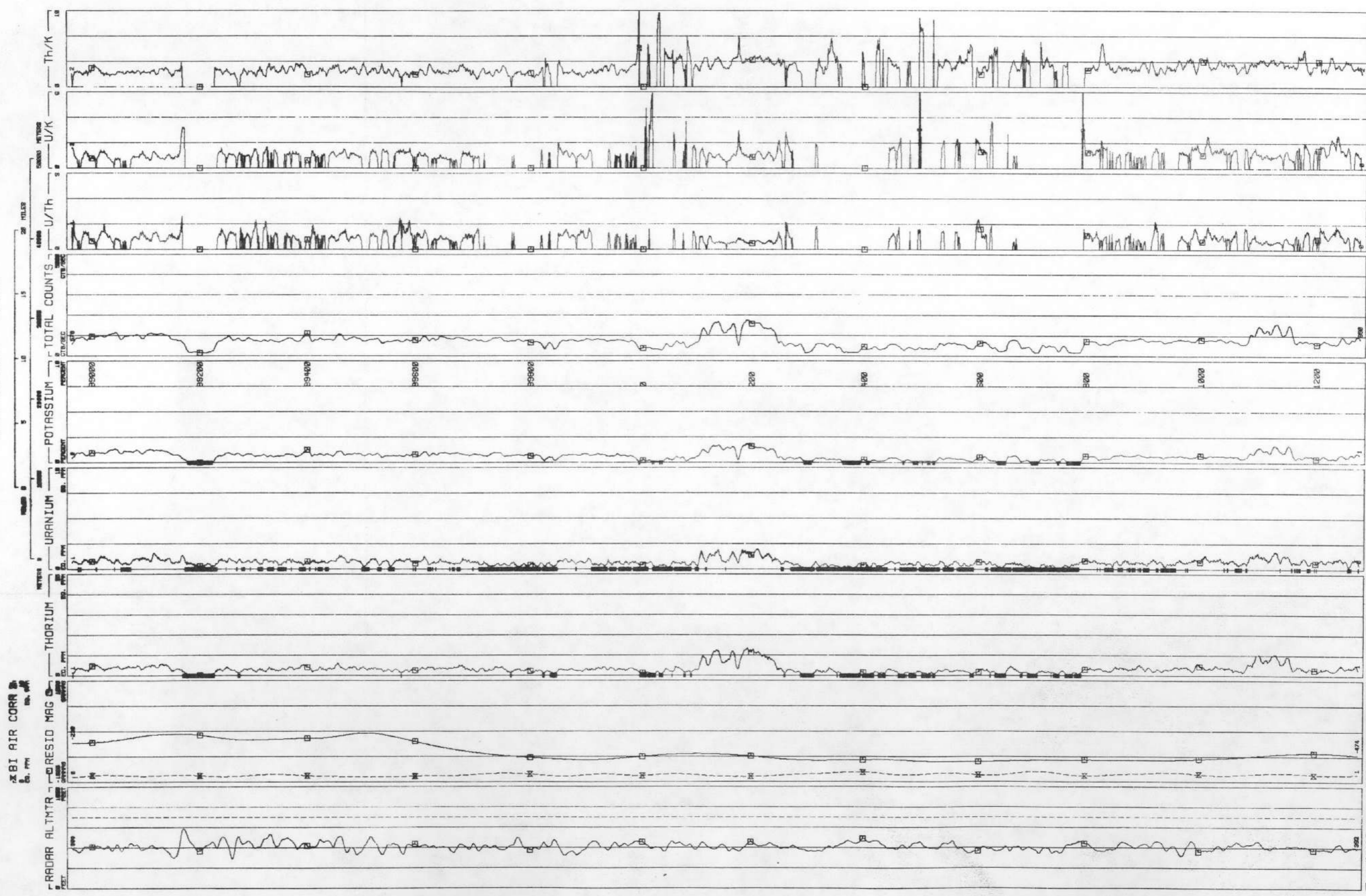


LINE 70
 TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
 DATA ACQUIRED 8.1.60

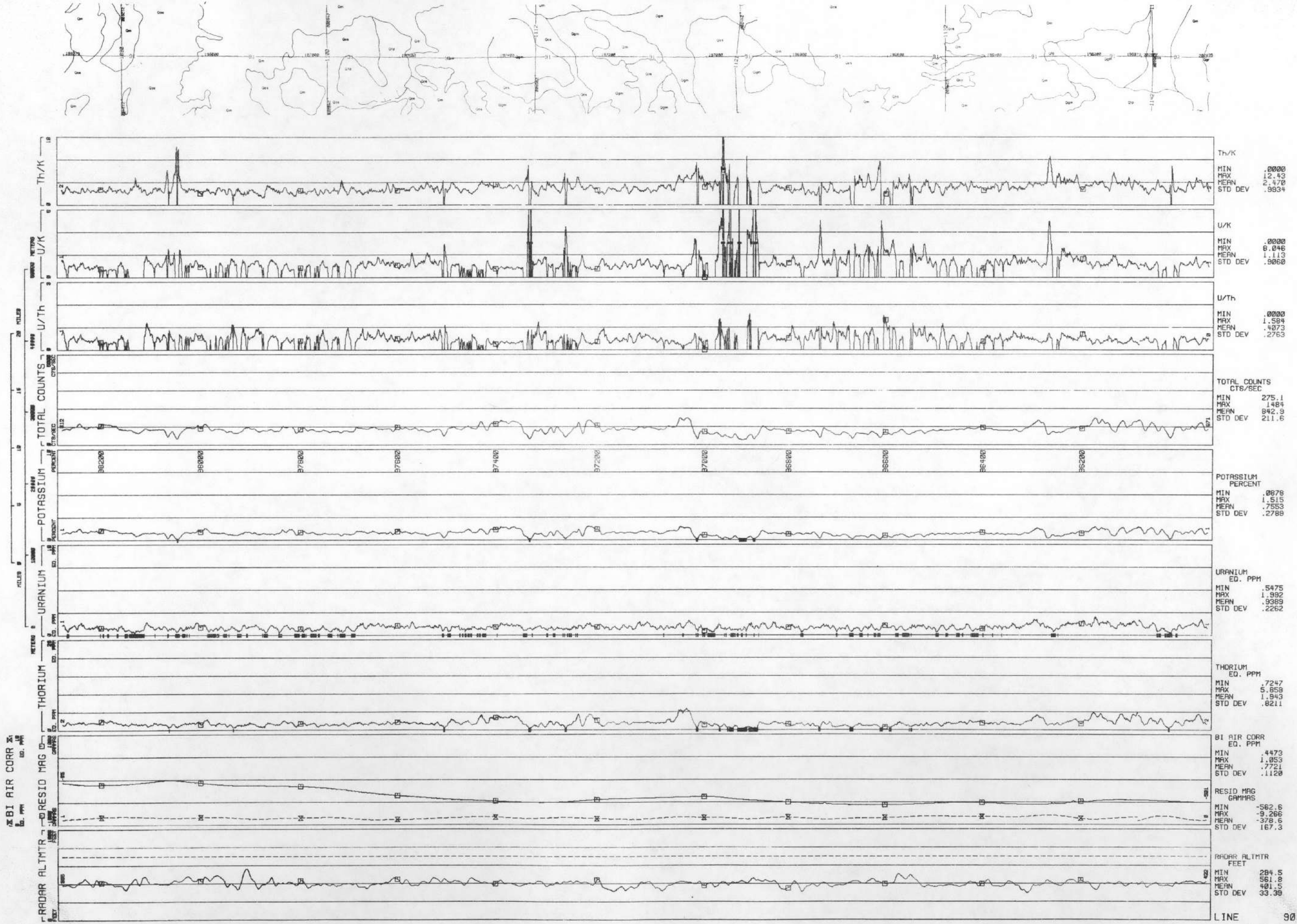


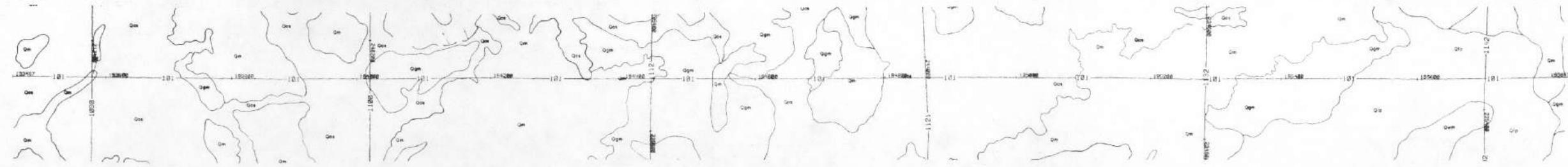


LINE 80
 TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
 DATA ACQUIRED 81160

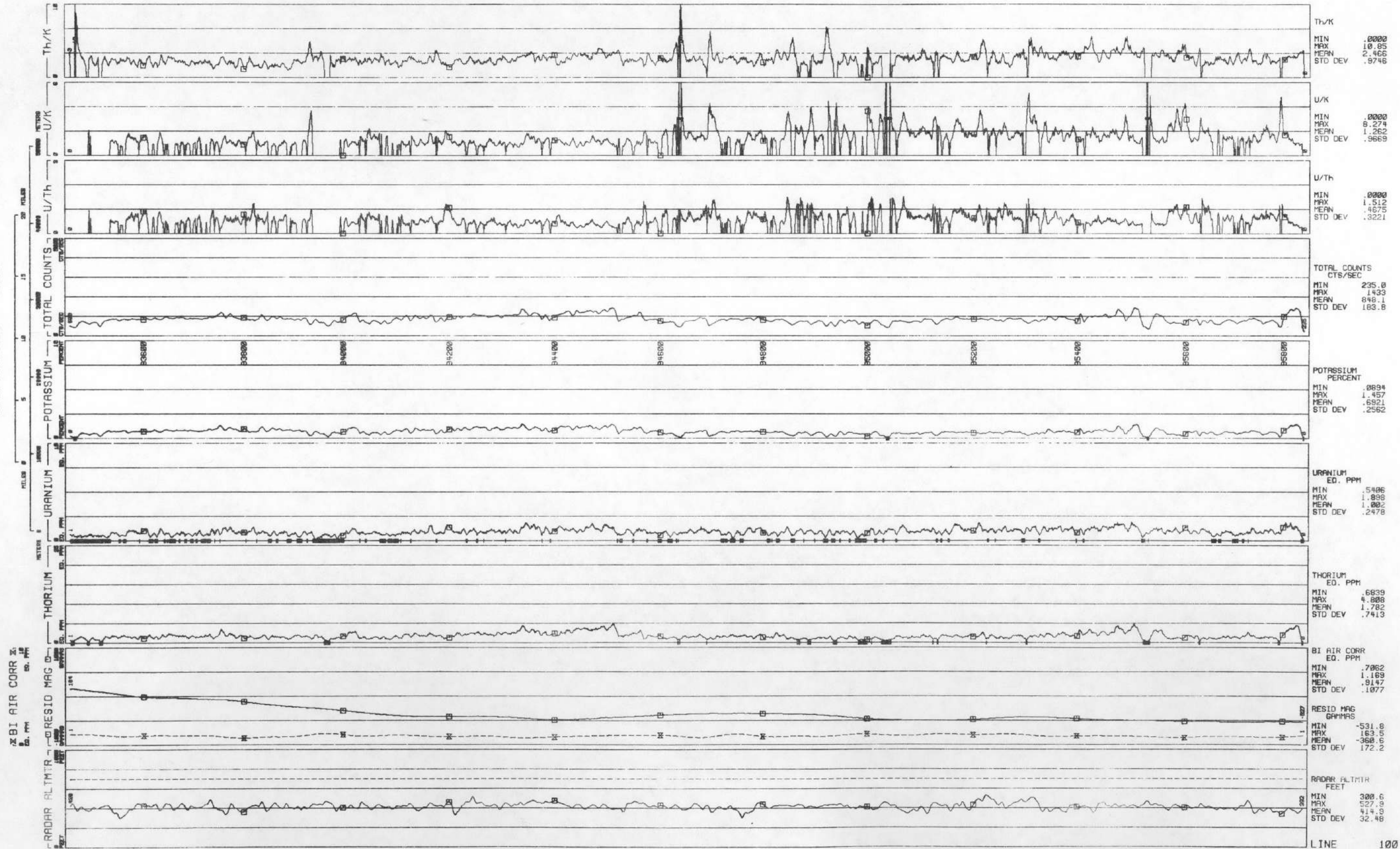


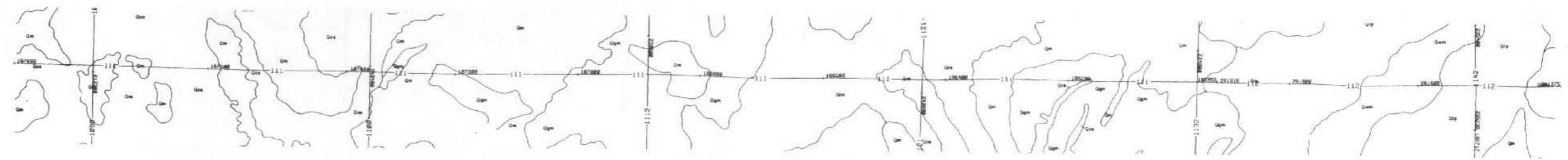
LINE 90
TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
DATA ACQUIRED 81160



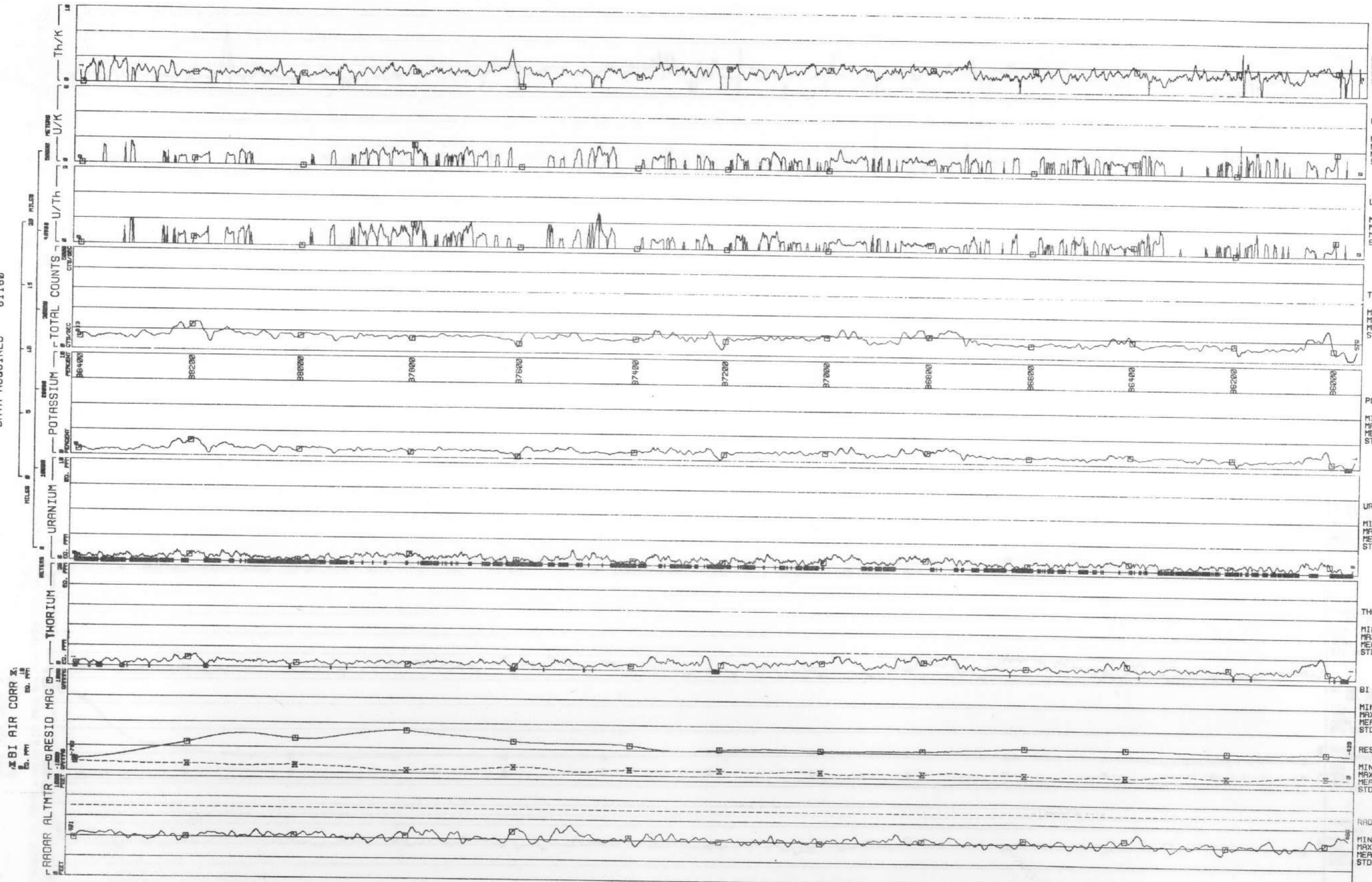


LINE 100
 TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
 DATA ACQUIRED 81160

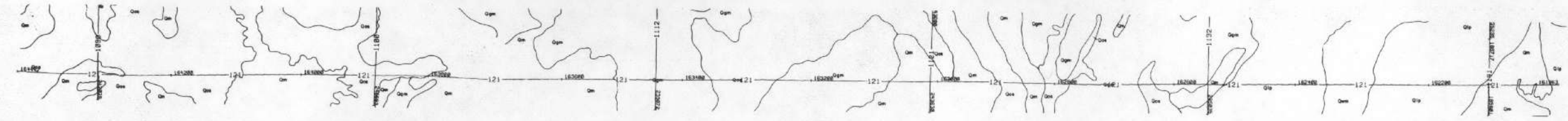




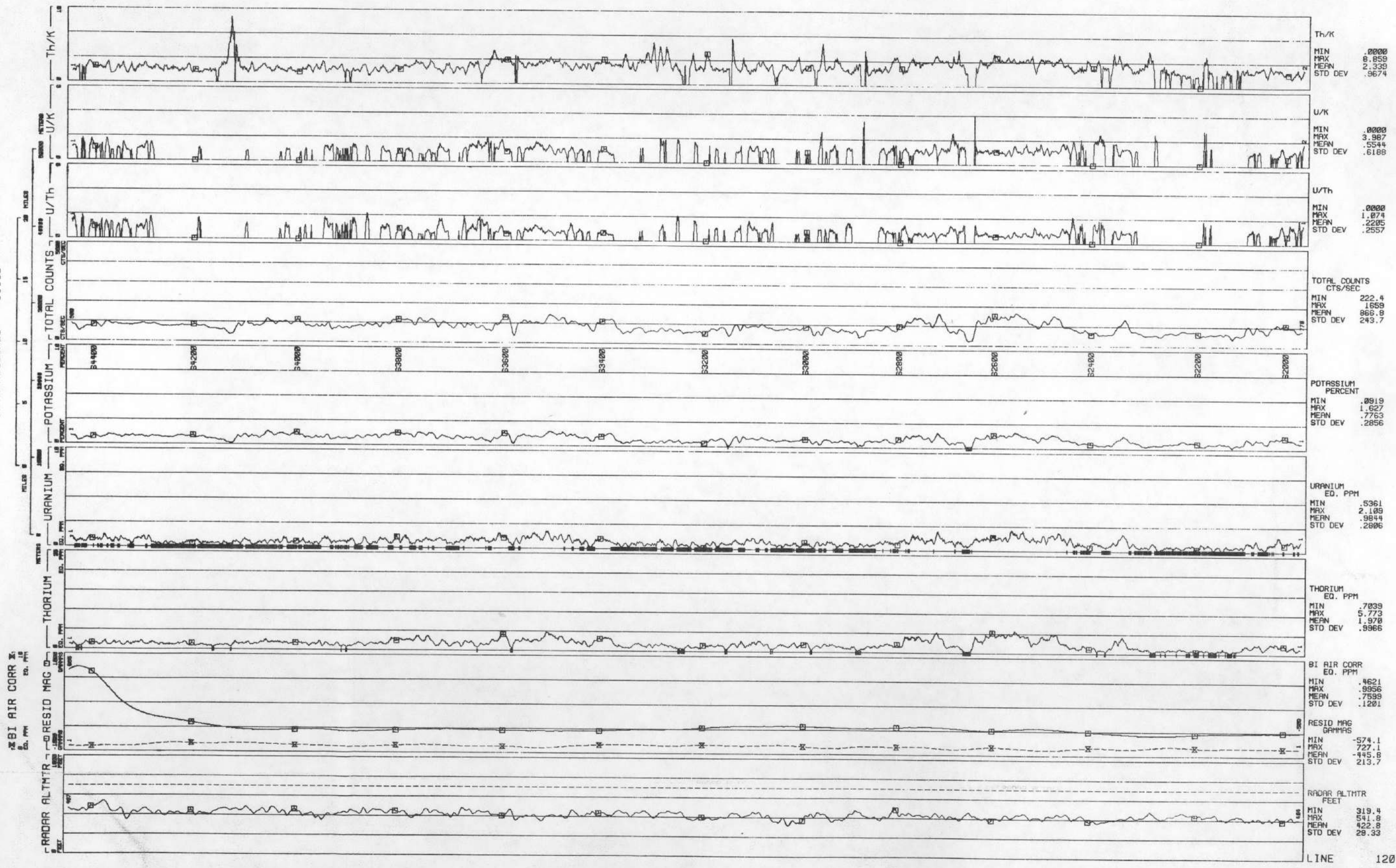
LINE 110
 TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
 DATA ACQUIRED 81160

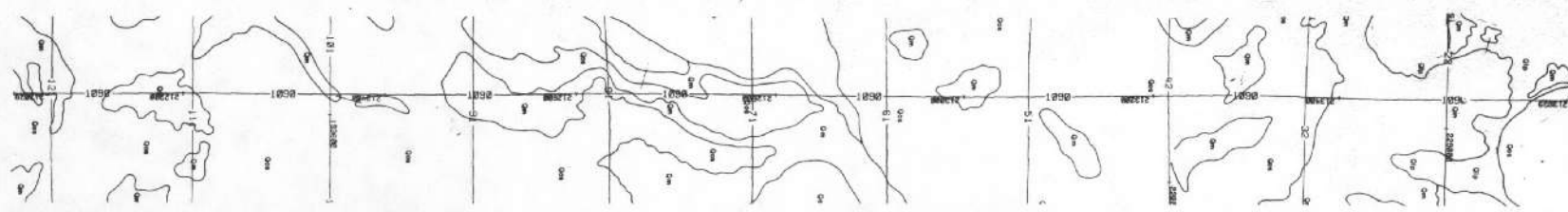


Th/K	MIN .0000
	MAX 5.562
	MEAN 2.151
	STD DEV .7560
U/K	MIN .0000
	MAX 2.448
	MEAN .4049
	STD DEV .5050
U/Th	MIN .0000
	MAX 1.425
	MEAN .1878
	STD DEV .2518
TOTAL COUNTS	MIN 123.5
CTS/SEC	MAX 1566
	MEAN 800.2
	STD DEV 193.8
POTASSIUM PERCENT	MIN .0855
	MAX 1.738
	MEAN .7812
	STD DEV .2494
URANIUM ED. PPM	MIN .4989
	MAX 1.427
	MEAN .7967
	STD DEV .1692
THORIUM ED. PPM	MIN .7101
	MAX 5.246
	MEAN 1.773
	STD DEV .7745
BI AIR CORR ED. PPM	MIN .2638
	MAX .8884
	MEAN .5289
	STD DEV .1556
RESID MAG GAMMAS	MIN -762.9
	MAX -141.4
	MEAN -397.3
	STD DEV 109.6
RADAR ALTHTR FEET	MIN 326.3
	MAX 541.6
	MEAN 418.6
	STD DEV 32.61

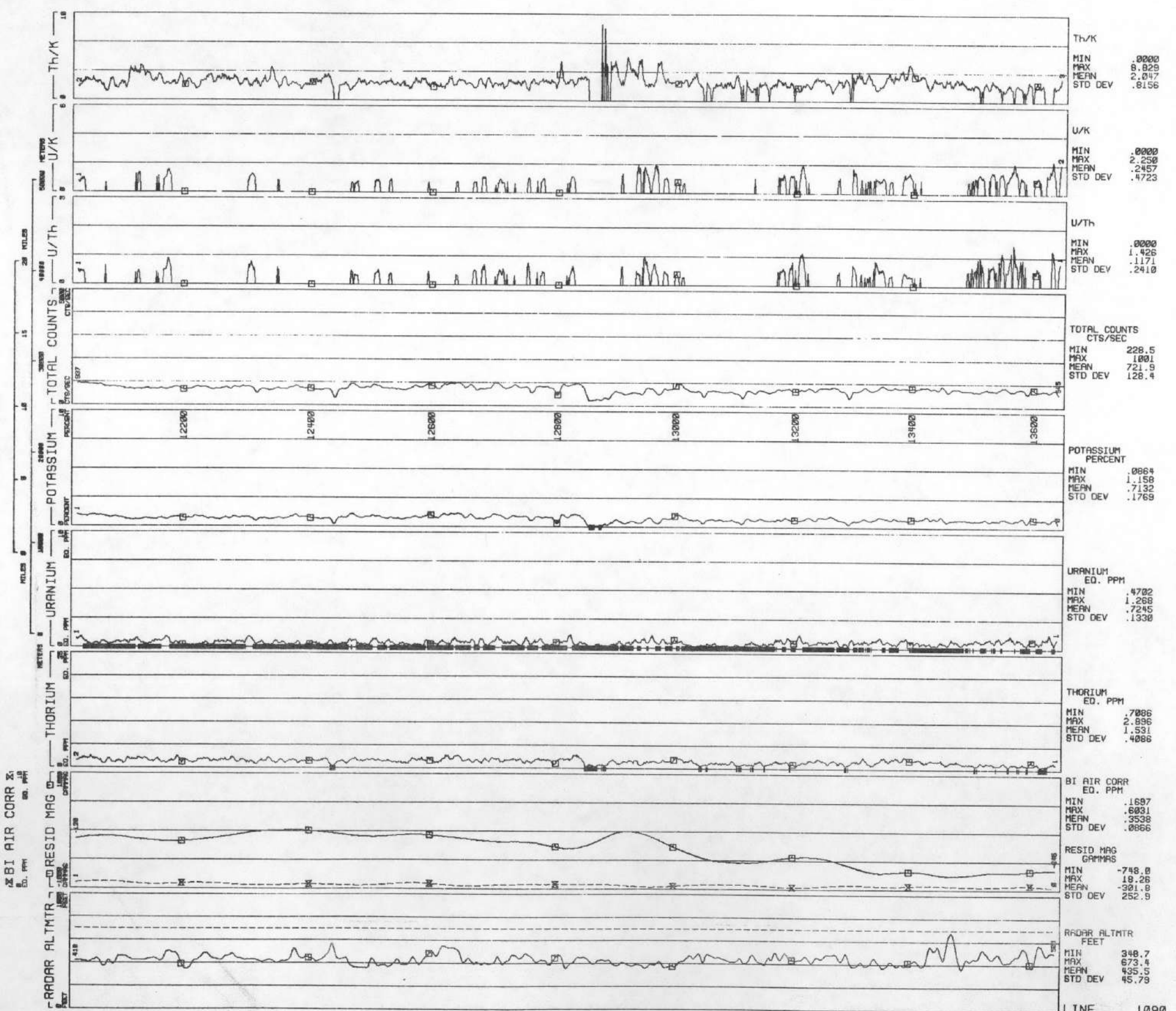


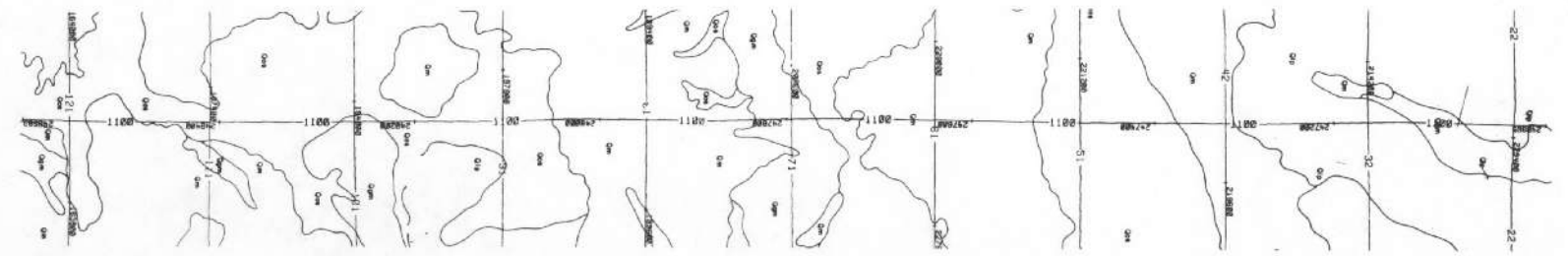
LINE 120
 TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
 DATA ACQUIRED 81160



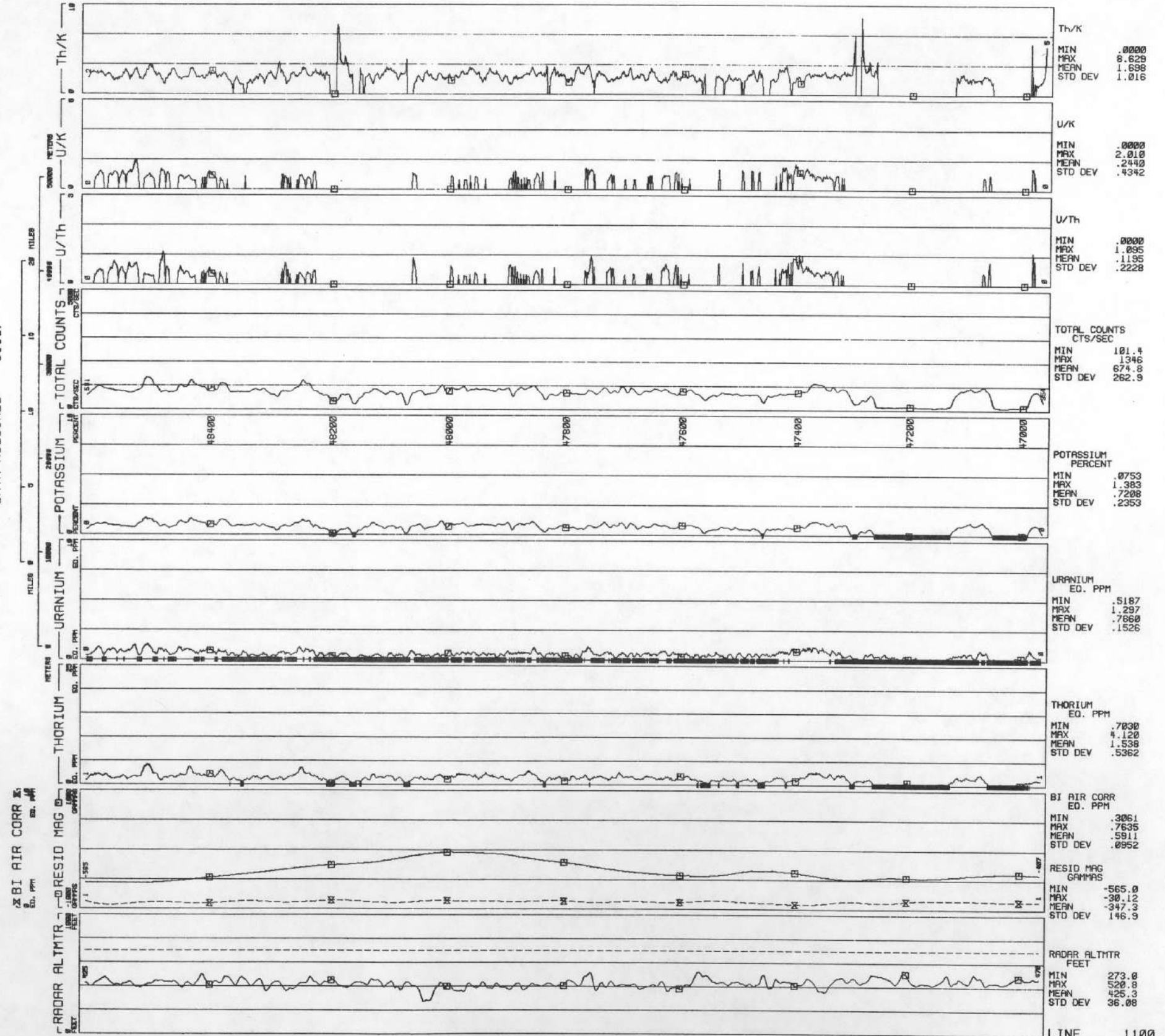


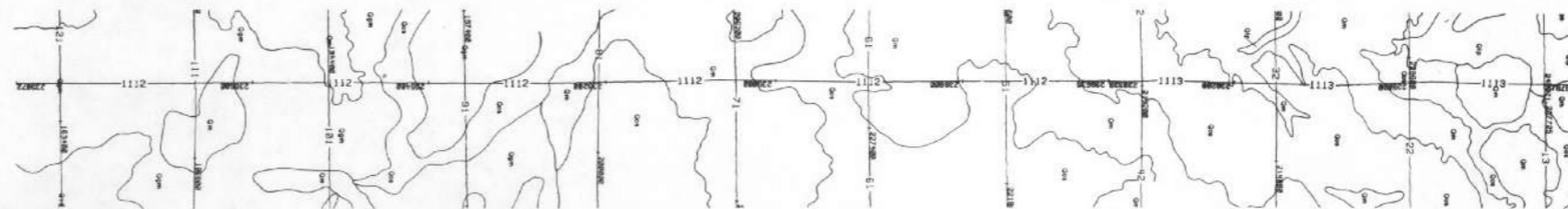
LINE 1090
 TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
 DATA ACQUIRED 811166



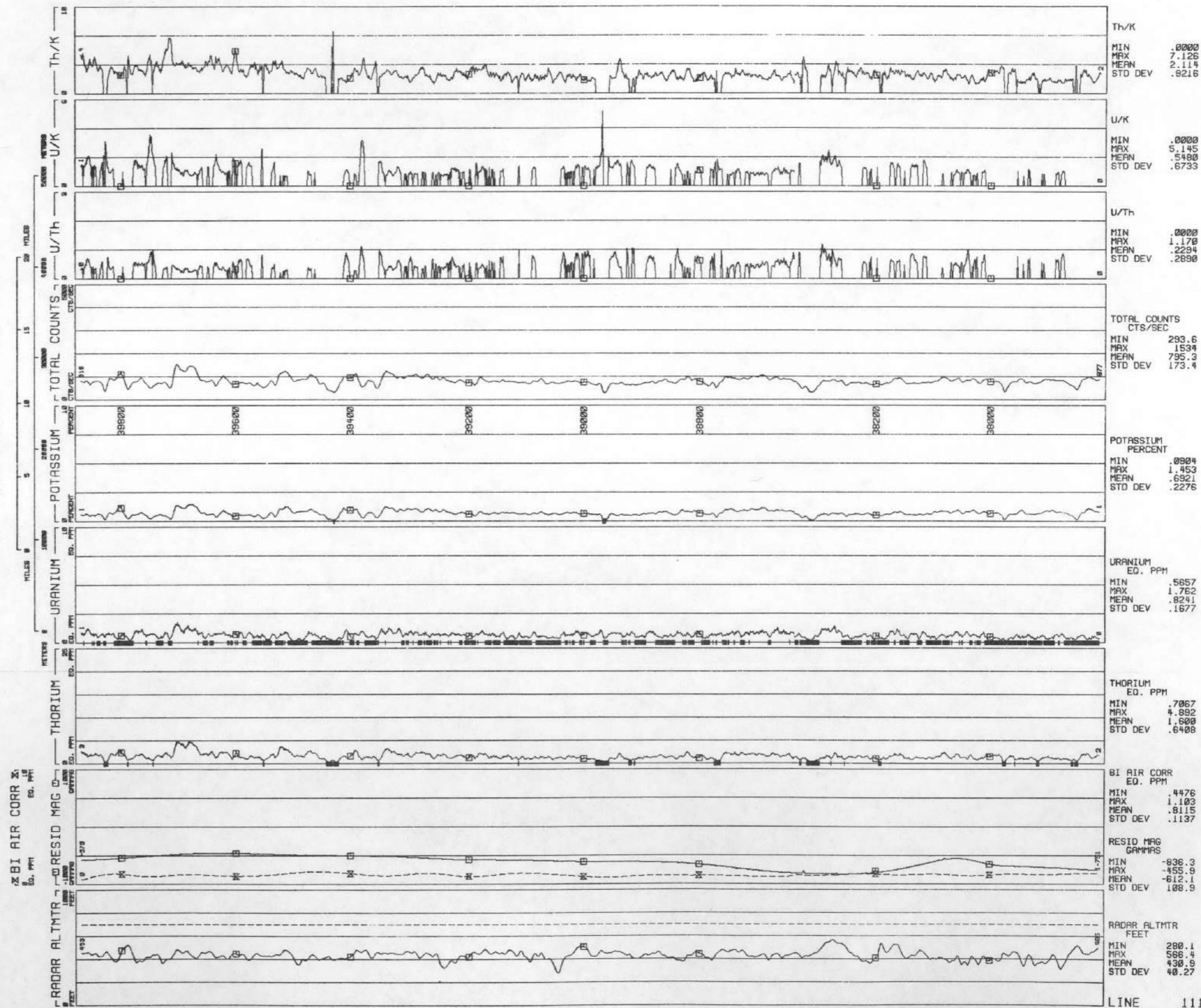


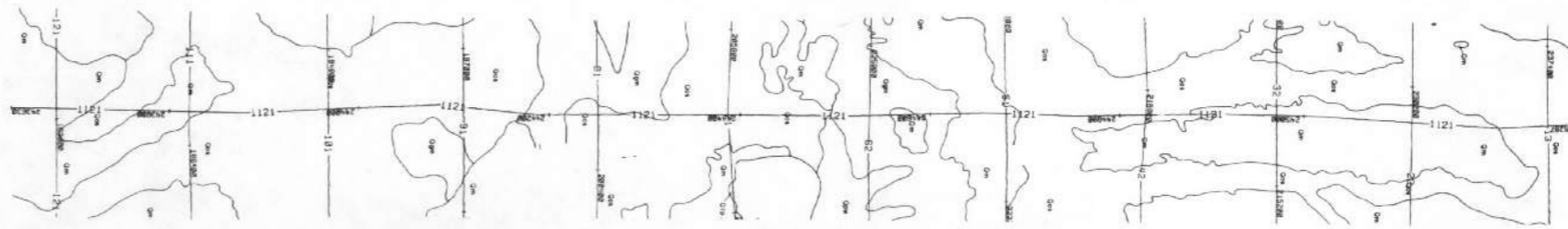
LINE 1100
 TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
 DATA ACQUIRED 81167





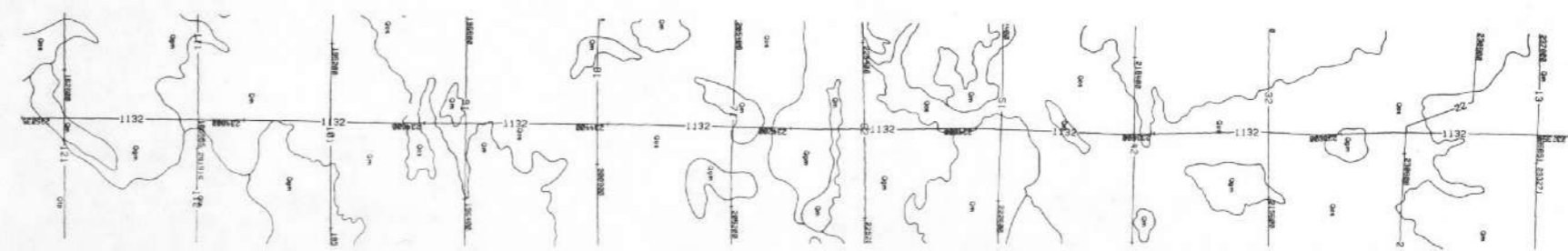
TRaverse CITY QUADRANGLE - NTMS NL 16-12
 LINE 1110
 DATA ACQUIRED 81167



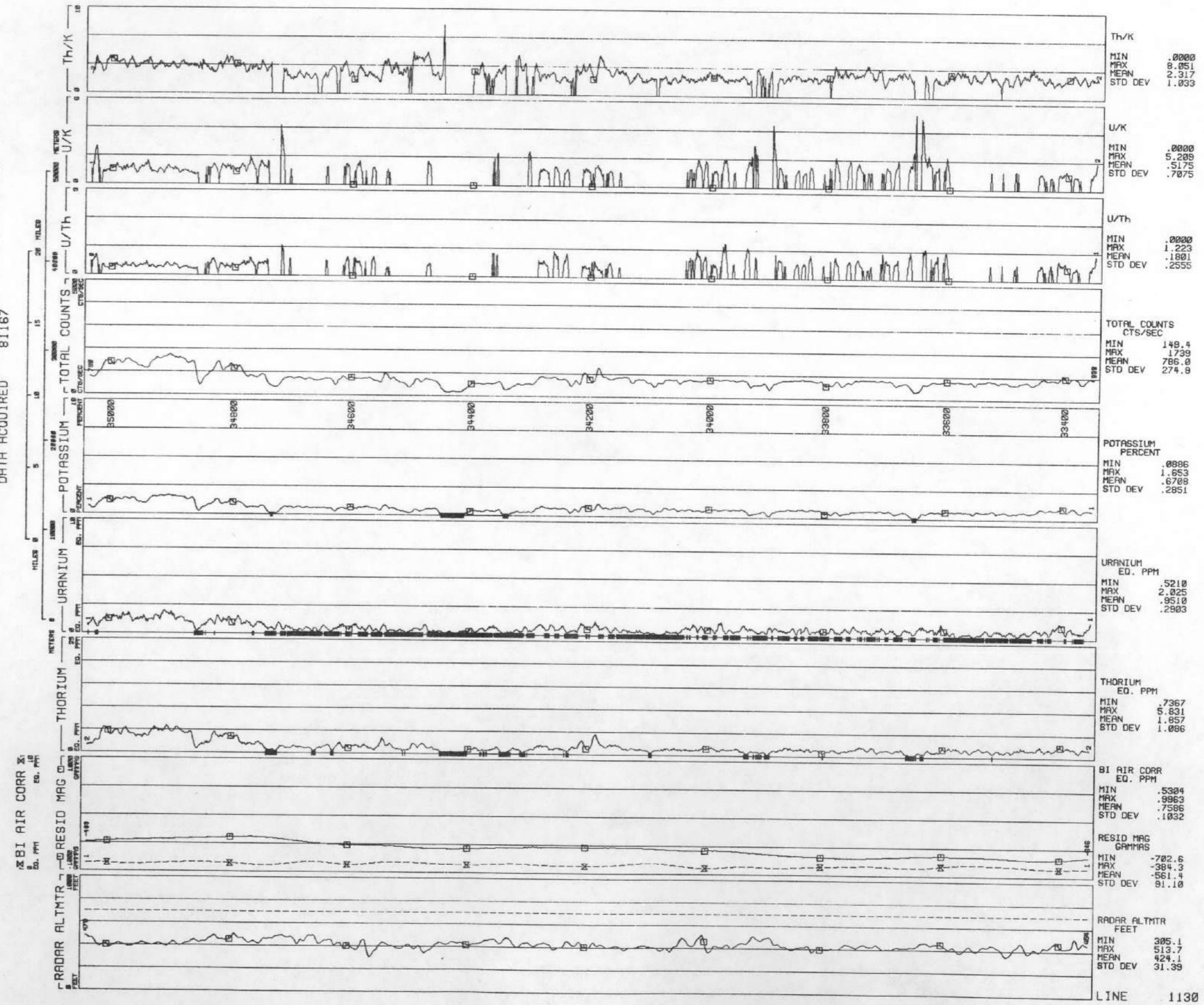


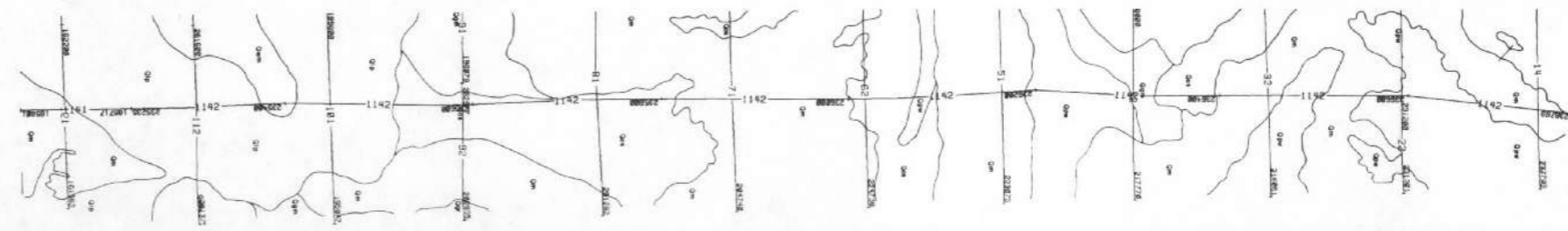
LINE 1120
 TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
 DATA ACQUIRED 81167



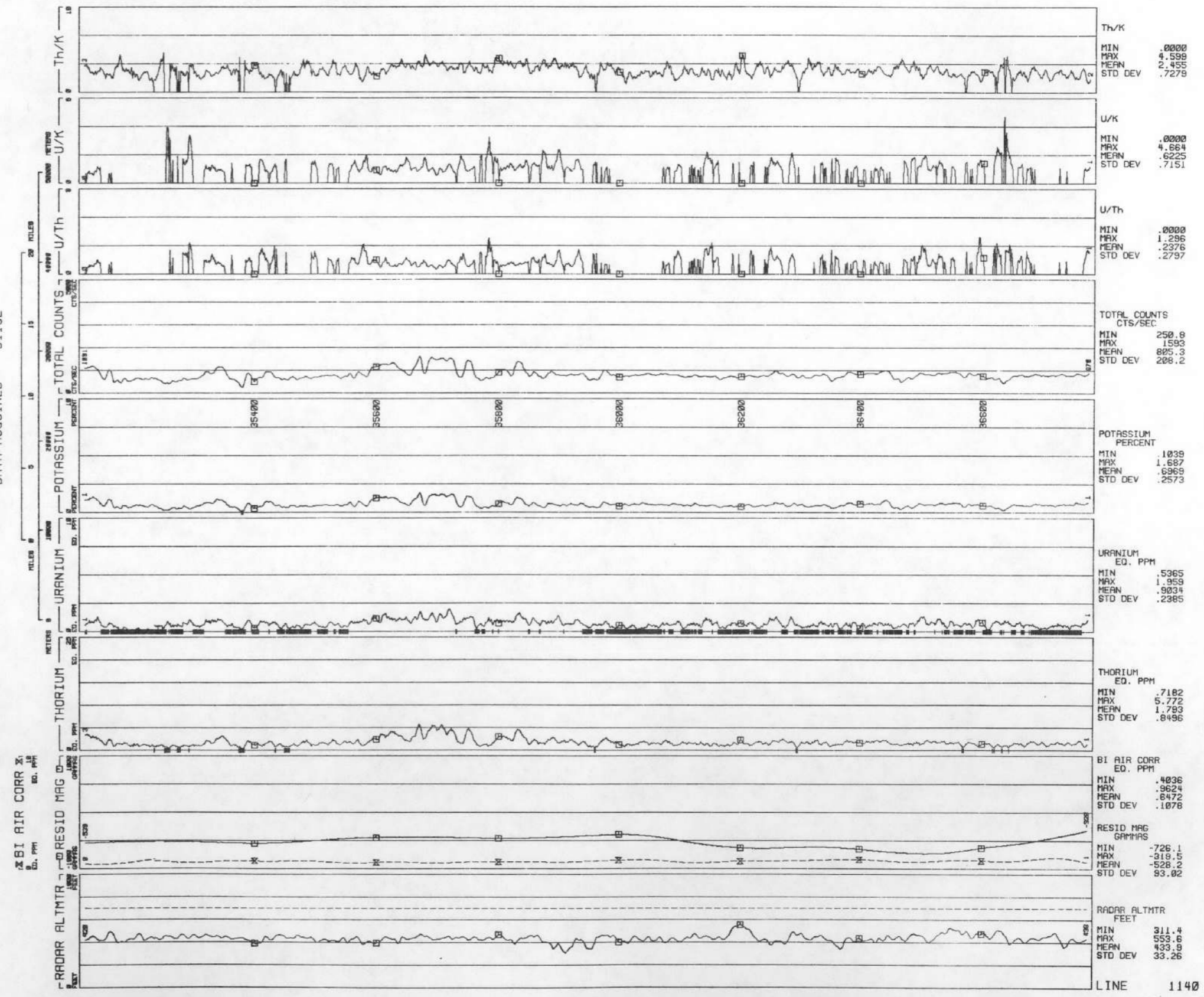


LINE 1130
 TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
 DATA ACQUIRED 81167

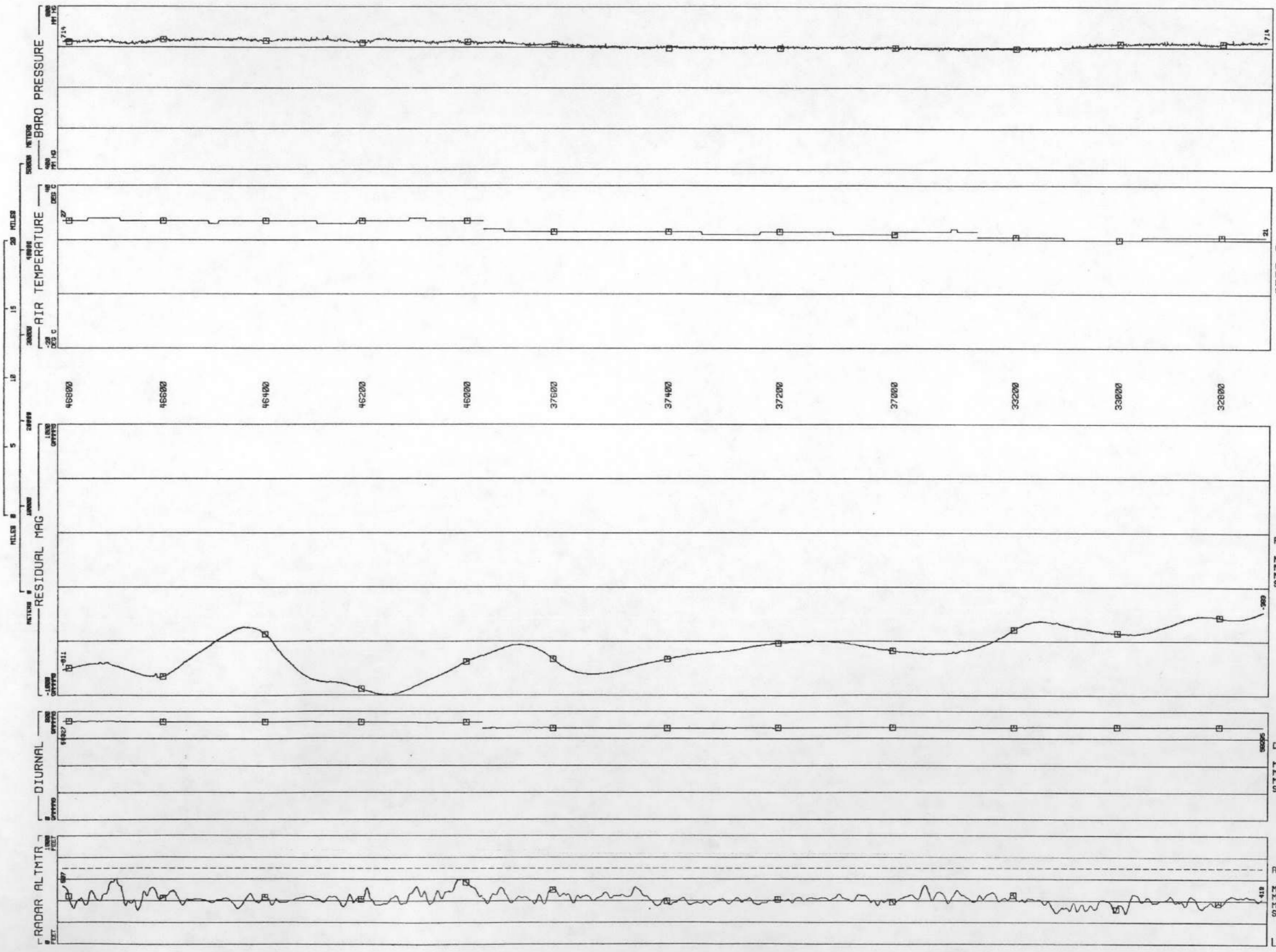
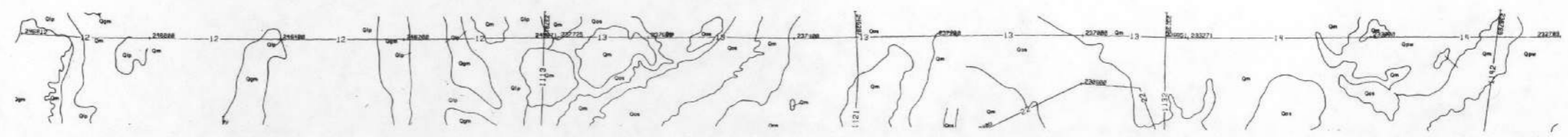




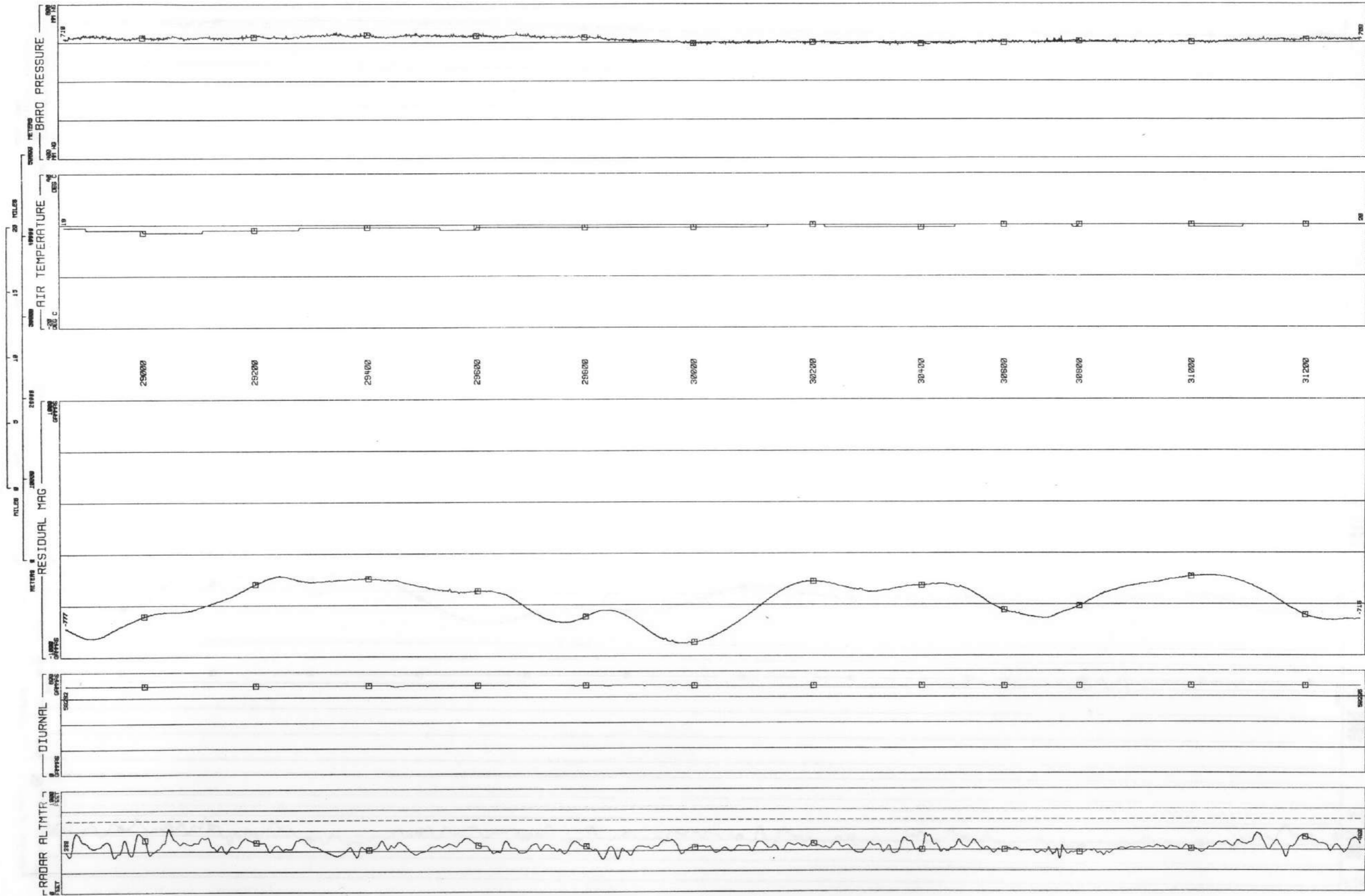
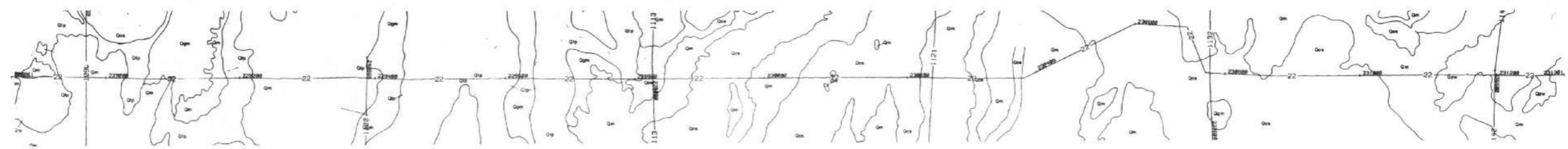
LINE 1140
 TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
 DATA ACQUIRED 81162



LINE 10
TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
DATA ACQUIRED 811158



LINE 20
TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
DATA ACQUIRED 81158



BARO PRESSURE
MM HG
MIN 692.0
MAX 727.7
MEAN 706.8
STD DEV 7.735

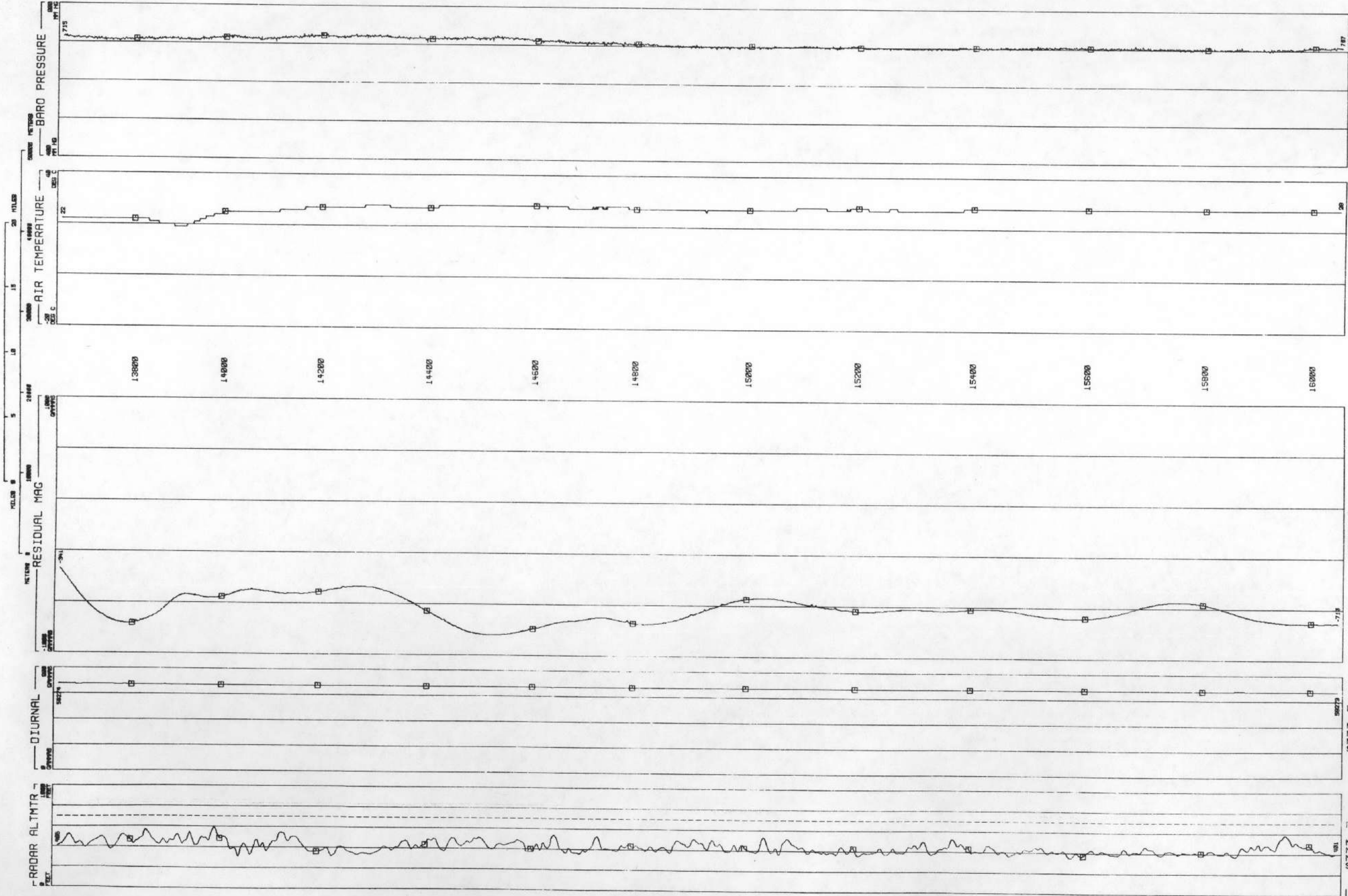
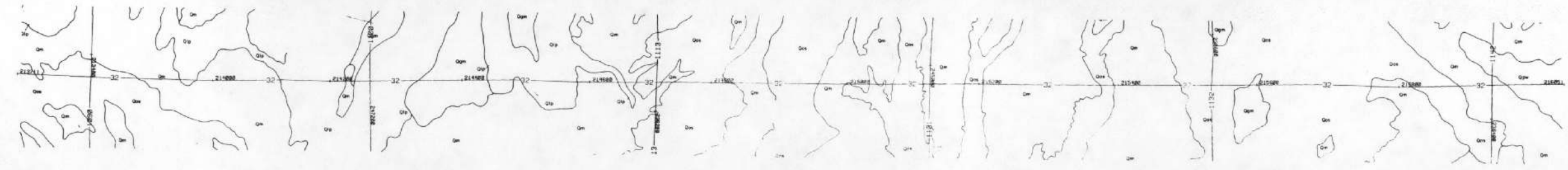
AIR TEMPERATURE
DEG C
MIN 17.00
MAX 20.00
MEAN 19.11
STD DEV .8028

RESIDUAL MAG
GAMMAS
MIN -801.5
MAX -373.0
MEAN -572.5
STD DEV 143.4

DIURNAL
GAMMAS
MIN 58262
MAX 58282
MEAN 58262
STD DEV 7.060

RADAR ALTMTR
FEET
MIN 328.1
MAX 348.4
MEAN 334.8
STD DEV 46.89

LINE 30
TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
DATA ACQUIRED 81158



BARO PRESSURE
MM HG
MIN 694.4
MAX 725.8
MEAN 707.0
STD DEV 7.043

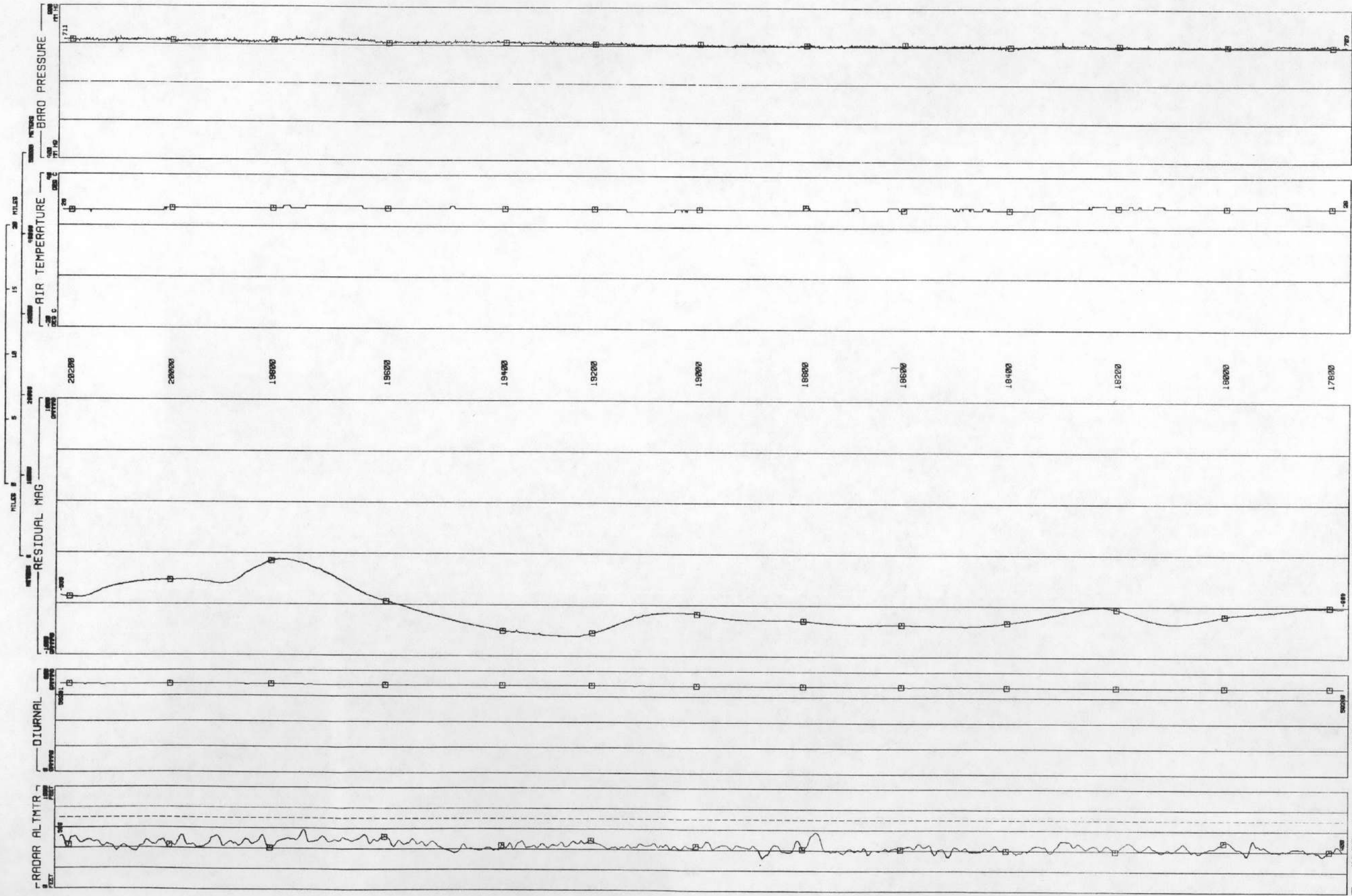
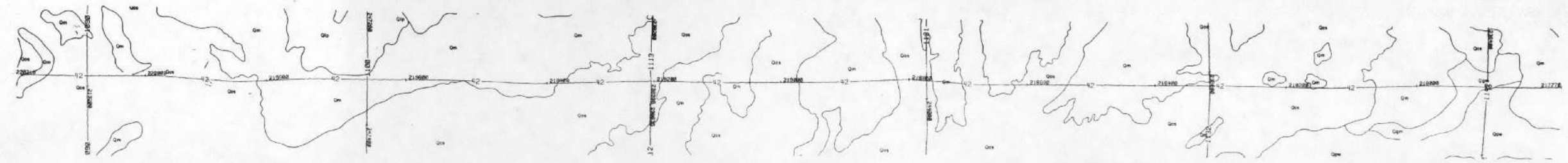
AIR TEMPERATURE
DEG C
MIN 19.00
MAX 28.00
MEAN 26.67
STD DEV 2.145

RESIDUAL MAG
GAMMAS
MIN -841.9
MAX -340.6
MEAN -635.0
STD DEV 93.16

DIURNAL
GAMMAS
MIN 58269
MAX 58275
MEAN 58266
STD DEV 6.539

RADAR ALTMTR
FEET
MIN 311.0
MAX 588.9
MEAN 428.1
STD DEV 47.13

LINE 40
TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
DATA ACQUIRED 81158



BARO PRESSURE
MM HG
MIN 694.4
MAX 721.0
MEAN 705.4
STD DEV 4.106

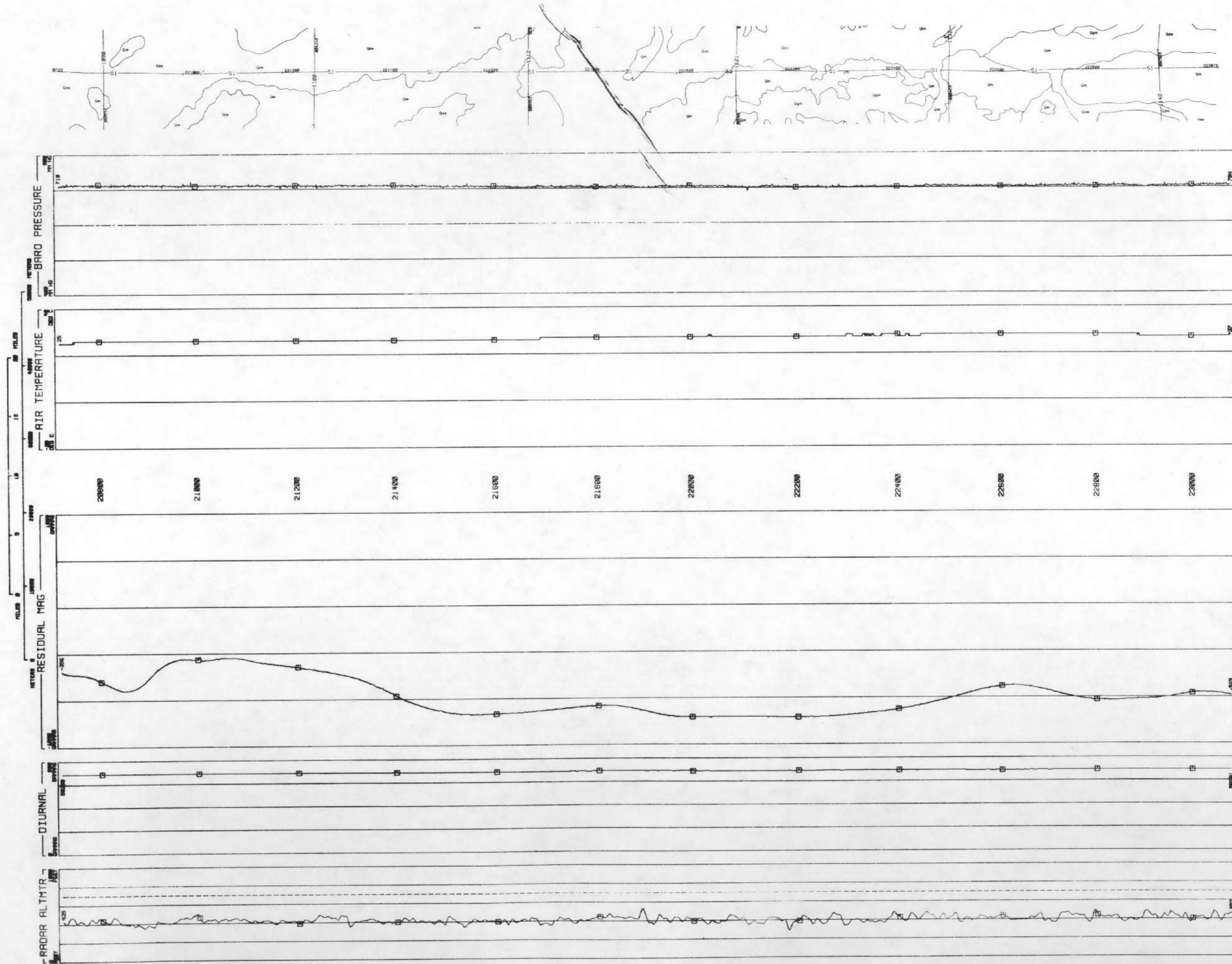
AIR TEMPERATURE
DEG C
MIN 25.00
MAX 29.00
MEAN 27.28
STD DEV .7366

RESIDUAL MAG
GAMMAS
MIN -844.2
MAX -247.2
MEAN -638.6
STD DEV 147.4

DIURNAL
GAMMAS
MIN 58278
MAX 58292
MEAN 58279
STD DEV 7.702

RADAR ALTMTR
FEET
MIN 322.5
MAX 584.7
MEAN 434.8
STD DEV 38.94

LINE 50
TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
DATA ACQUIRED 811158



BARO PRESSURE
MM HG
MIN 691.6
MAX 720.8
MEAN 705.9
STD DEV 3.549

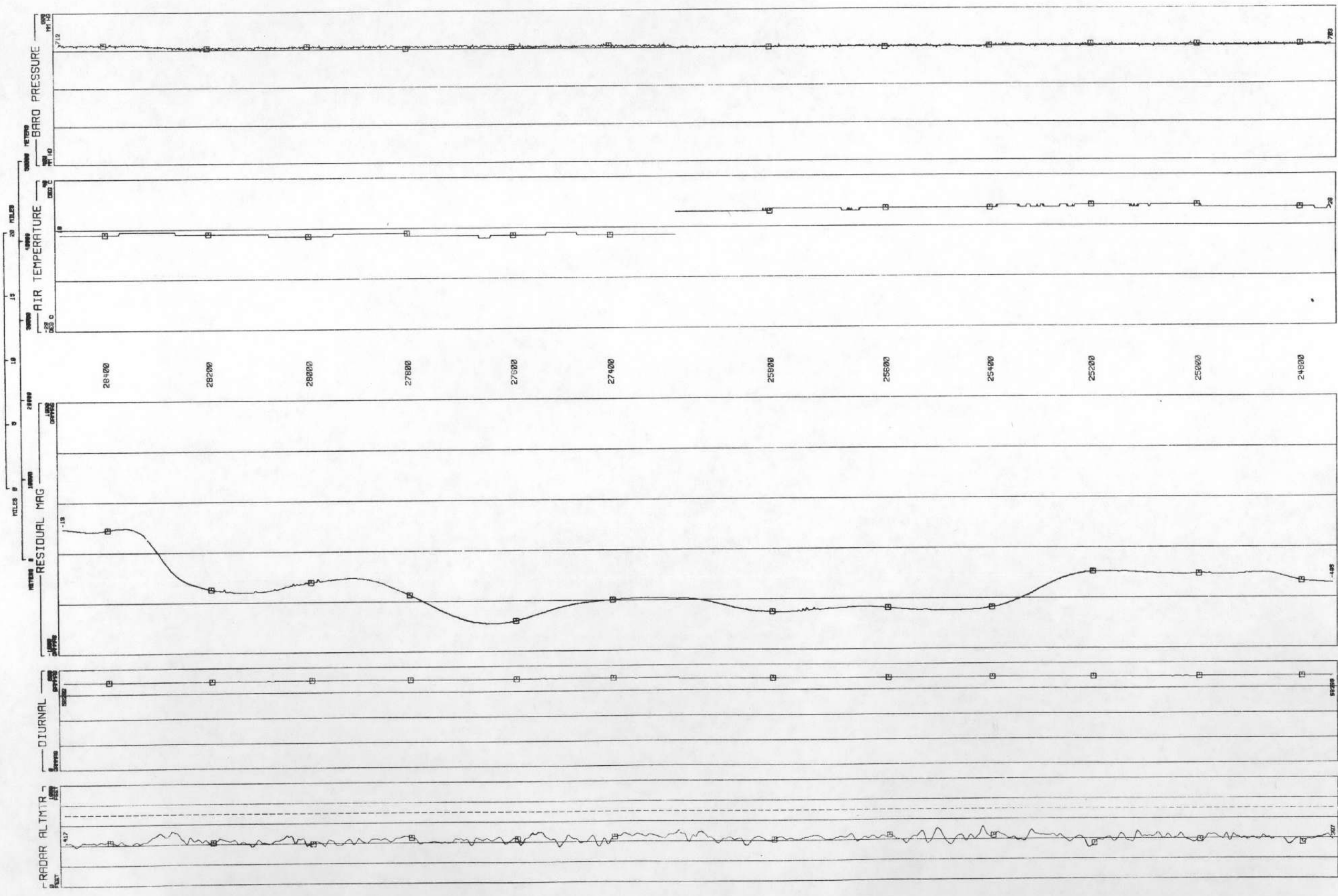
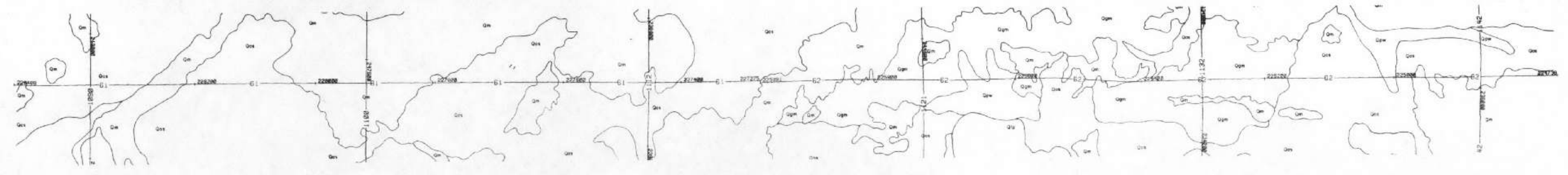
AIR TEMPERATURE
DEG C
MIN 25.00
MAX 26.00
MEAN 26.00
STD DEV .7916

RESIDUAL MAG
GAMMAS
MIN -769.4
MAX -228.6
MEAN -580.1
STD DEV 162.1

DIURNAL
GAMMAS
MIN 5828
MAX 5829
MEAN 5828
STD DEV 2.350

RADAR ALTMTR
FEET
MIN 288.6
MAX 528.6
MEAN 415.1
STD DEV 30.35

LINE 60
TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
DATA ACQUIRED 81158



BARO PRESSURE
MM HG
MIN 694.1
MAX 717.5
MEAN 704.0
STD DEV 3.669

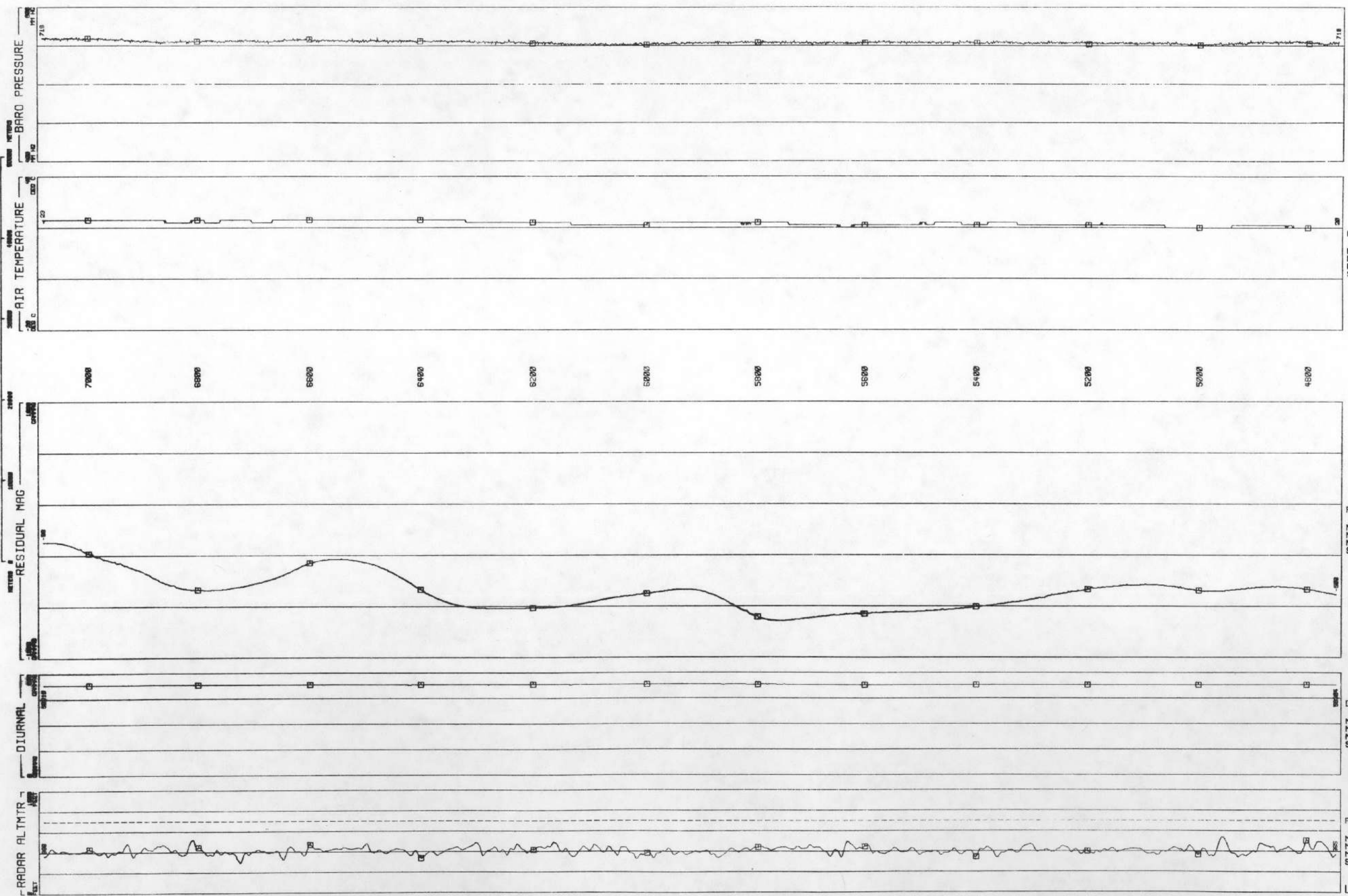
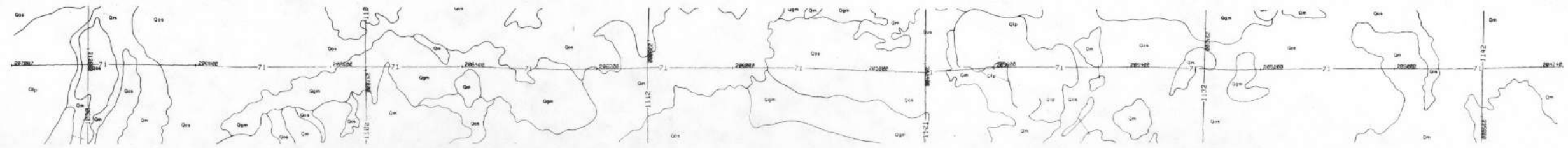
AIR TEMPERATURE
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MAX 28.00
MEAN 22.38
STD DEV 4.775

RESIDUAL MAG
GAMMAS
MIN -781.3
MAX -5.477
MEAN -518.9
STD DEV 181.2

DIURNAL
GAMMAS
MIN 58290
MAX 58300
MEAN 58289
STD DEV 5.175

RADAR ALTMTR
FEET
MIN 313.8
MAX 526.9
MEAN 422.9
STD DEV 31.40

LINE 70
TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
DATA ACQUIRED 81160



BARO PRESSURE
MM HG
MIN 698.5
MAX 721.8
MEAN 706.6
STD DEV 3.904

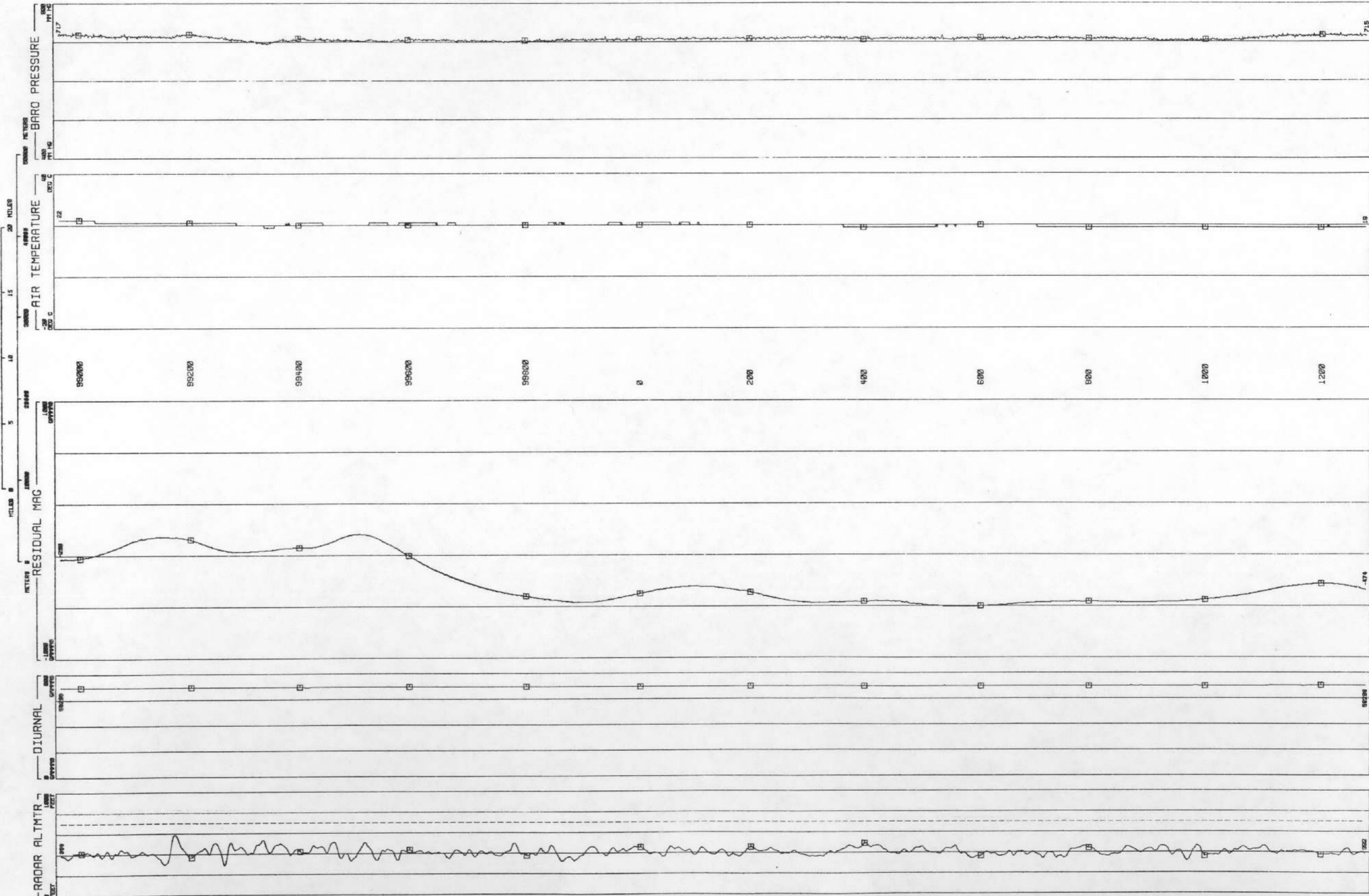
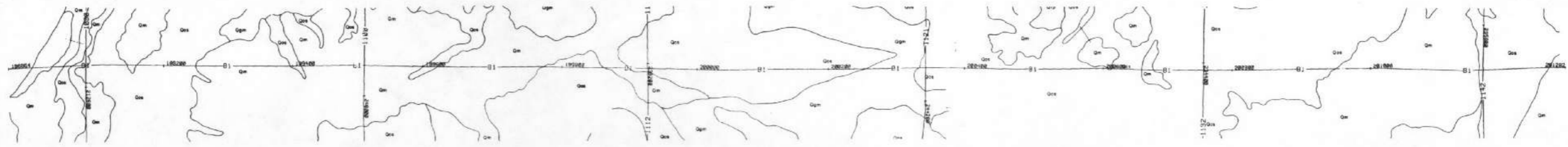
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MIN 20.00
MAX 23.00
MEAN 21.74
STD DEV .8771

RESIDUAL MAG
GAMMAS
MIN -715.3
MAX -94.73
MEAN -404.6
STD DEV 143.0

DIURNAL
GAMMAS
MIN 56303
MAX 56310
MEAN 56303
STD DEV 3.716

RADAR ALTMTR
FEET
MIN 295.3
MAX 538.1
MEAN 409.7
STD DEV 32.60

LINE 80
TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
DATA ACQUIRED 81160



BARO PRESSURE
MM HG
MIN 693.4
MAX 723.7
MEAN 707.9
STD DEV 4.744

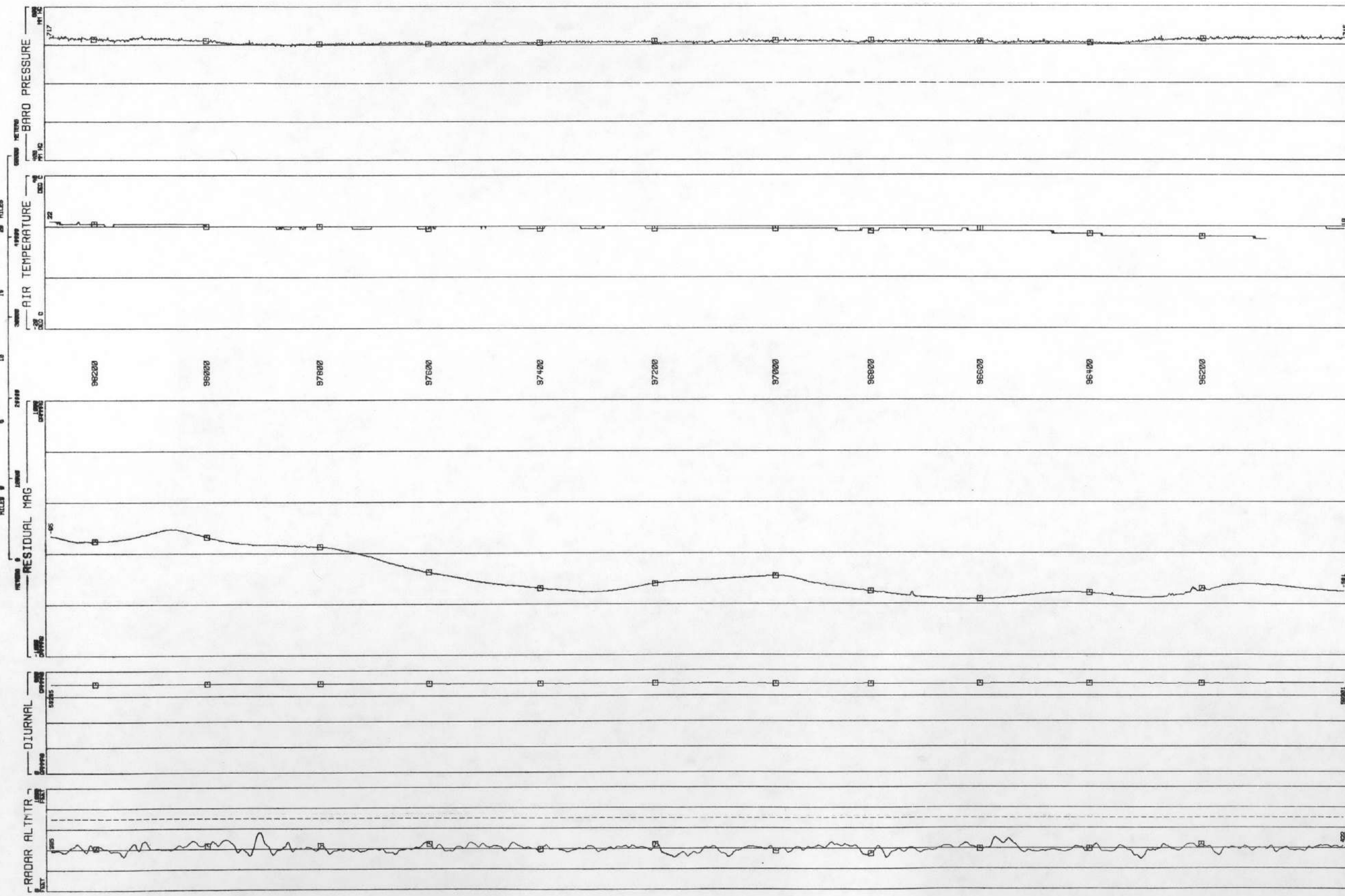
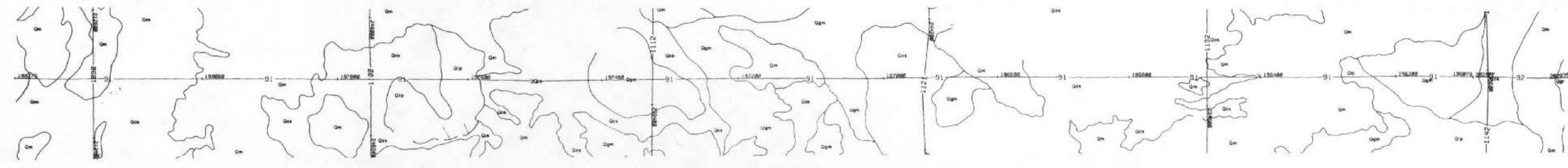
AIR TEMPERATURE
DEG C
MIN 19.00
MAX 22.00
MEAN 19.96
STD DEV .8133

RESIDUAL MAG
GAMMAS
MIN -604.1
MAX -37.00
MEAN -410.7
STD DEV 188.2

DIURNAL
GAMMAS
MIN 58293
MAX 58299
MEAN 58296
STD DEV 6.773

RADAR ALTMTR
FEET
MIN 290.0
MAX 585.1
MEAN 410.8
STD DEV 37.69

LINE 90
TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
DATA ACQUIRED 81160



BARO PRESSURE
MM HG
MIN 695.7
MAX 725.8
MEAN 708.3
STD DEV 5.004

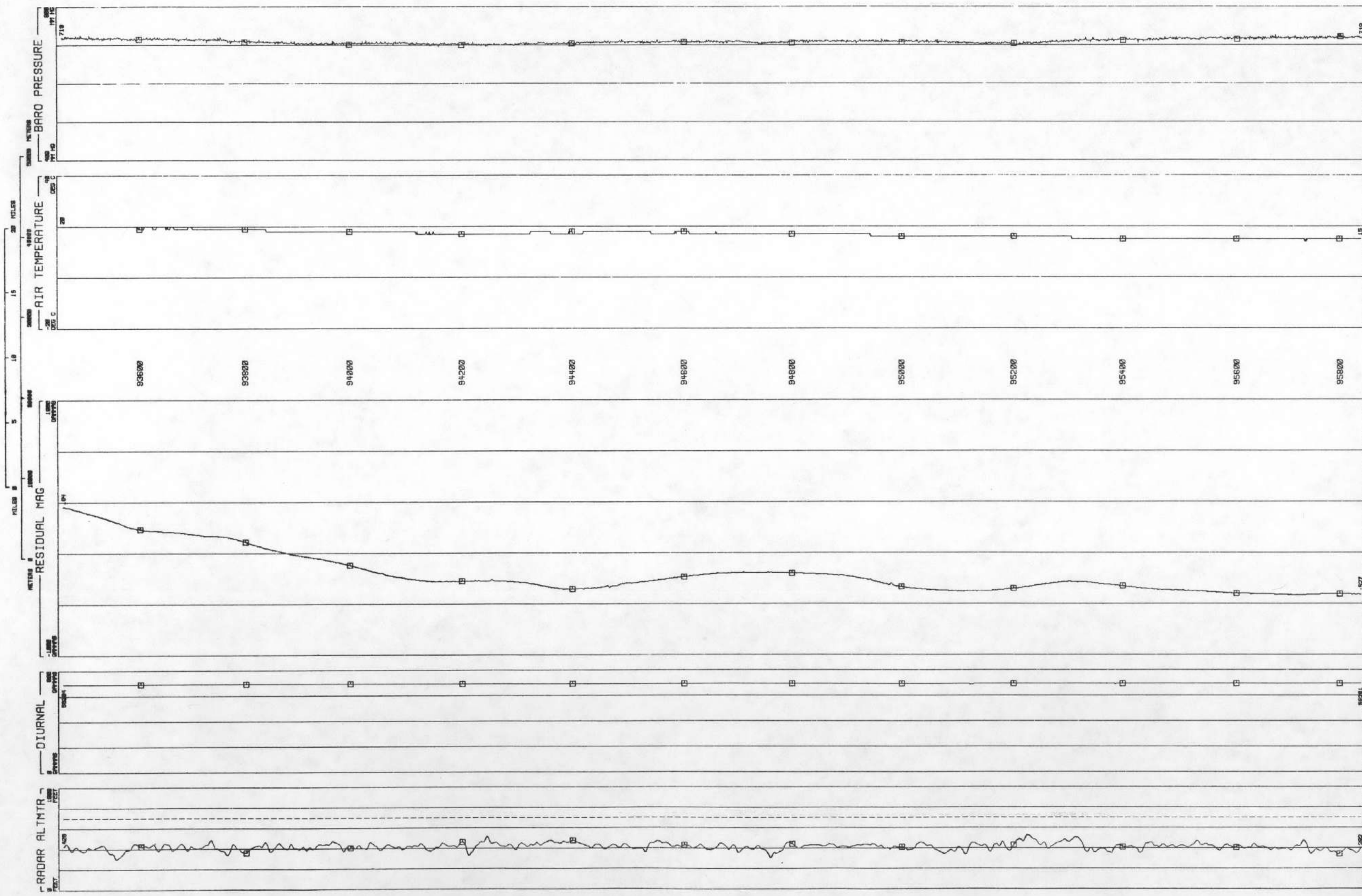
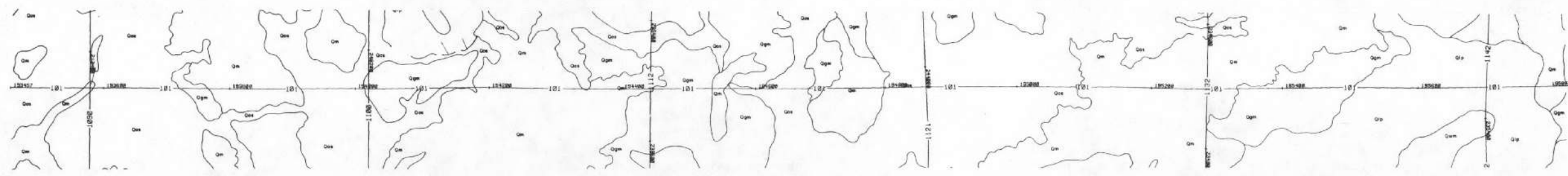
AIR TEMPERATURE
DEG C
MIN 15.00
MAX 22.00
MEAN 18.96
STD DEV 1.515

RESIDUAL MAG
GAMMAS
MIN -562.6
MAX -9.266
MEAN -378.6
STD DEV 167.3

DIURNAL
GAMMAS
MIN 58293
MAX 58302
MEAN 58288
STD DEV 6.056

RADAR ALTMTR
FEET
MIN 294.5
MAX 561.8
MEAN 481.5
STD DEV 33.39

LINE 100
TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
DATA ACQUIRED 81160



BARO PRESSURE
MM HG
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MAX 725.1
MEAN 709.6
STD DEV 5.492

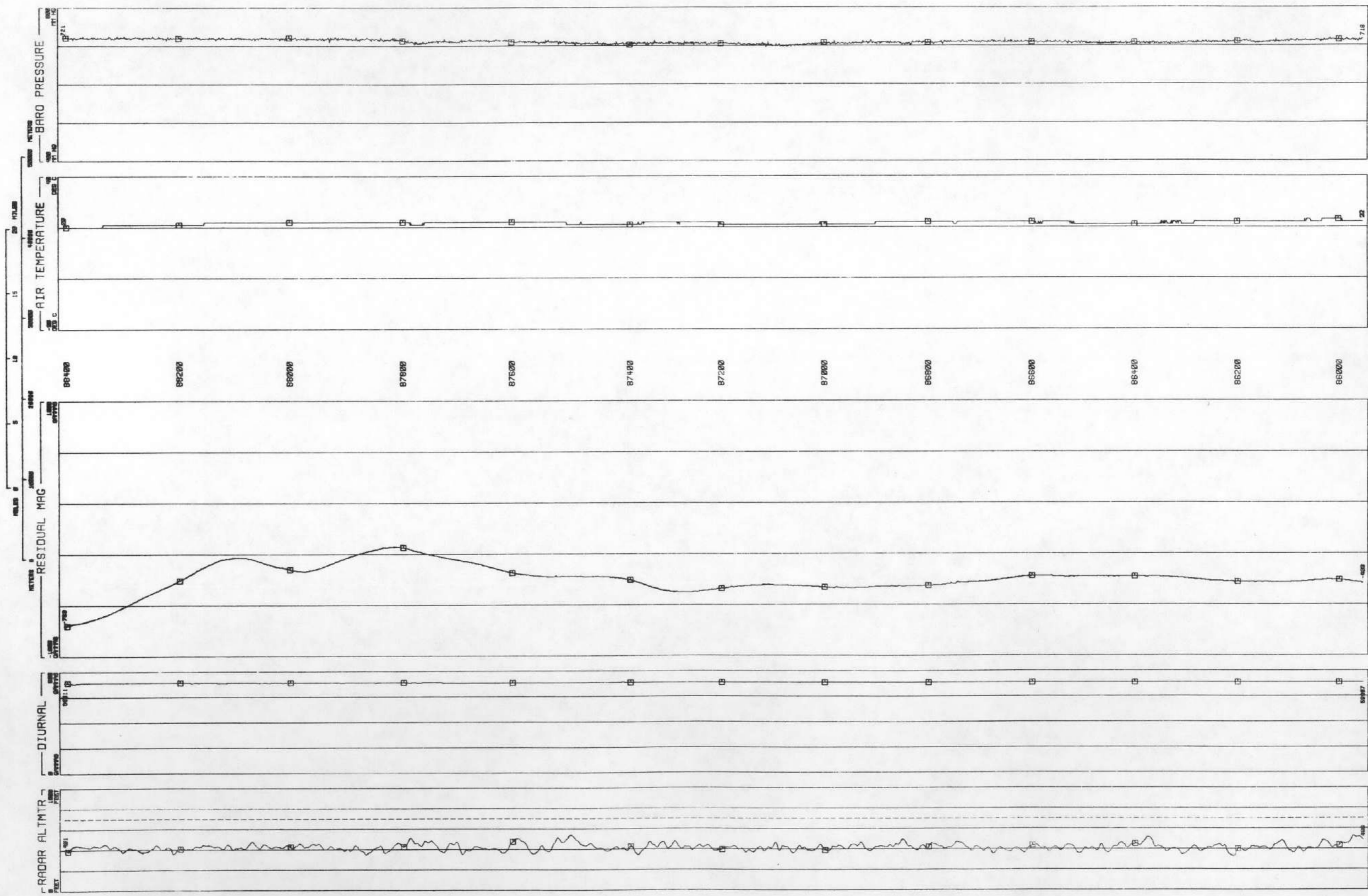
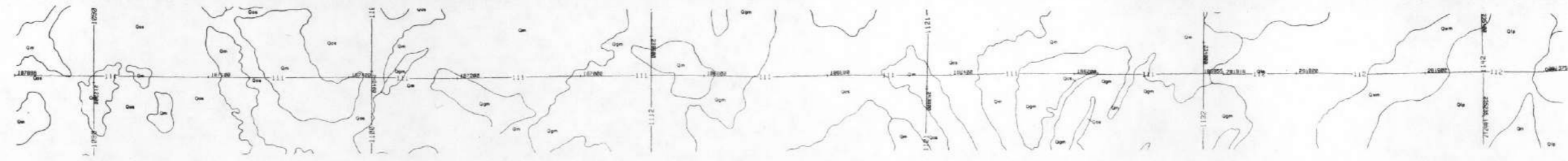
AIR TEMPERATURE
DEG C
MIN 14.00
MAX 20.00
MEAN 17.00
STD DEV 1.514

RESIDUAL MAG
GAMMAS
MIN -531.8
MAX 153.5
MEAN -369.5
STD DEV 172.2

DIURNAL
GAMMAS
MIN 58289
MAX 58294
MEAN 58289
STD DEV 3.667

RADAR ALTMTR
FEET
MIN 300.6
MAX 527.9
MEAN 414.9
STD DEV 32.48

LINE 110
TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
DATA ACQUIRED 8:11:00



BARO PRESSURE
MM HG
MIN 686.2
MAX 725.8
MEAN 710.7
STD DEV 5.818

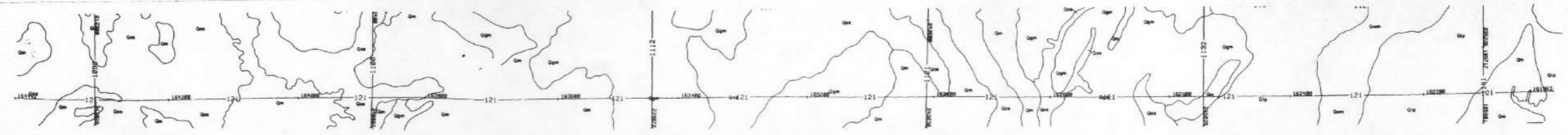
AIR TEMPERATURE
DEG C
MIN 20.00
MAX 23.00
MEAN 21.61
STD DEV .5765

RESIDUAL MAG
GAMMAS
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MEAN -397.3
STD DEV 109.6

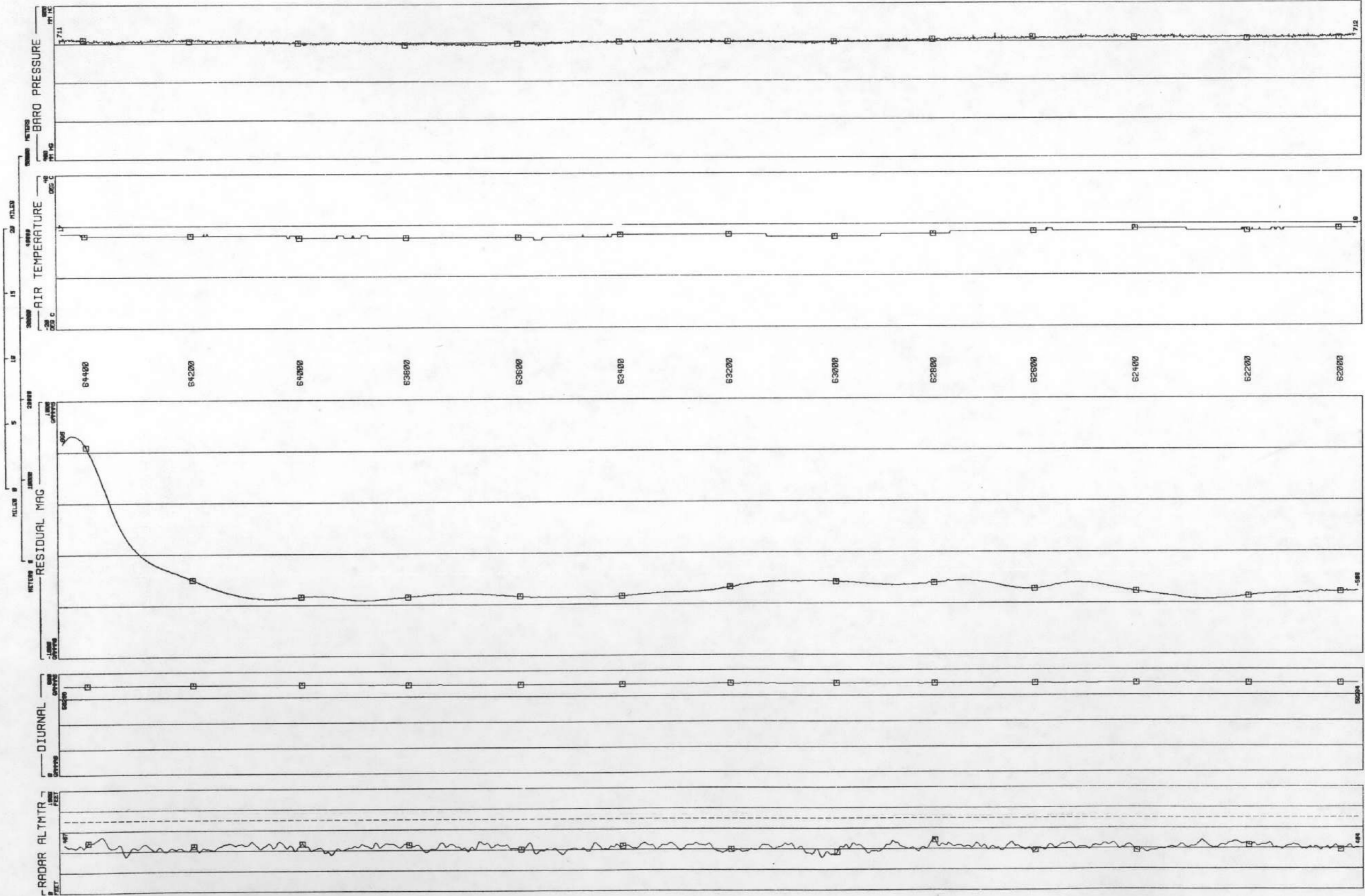
DIURNAL
GAMMAS
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MAX 58311
MEAN 58305
STD DEV 4.290

RADAR ALTIMTR
FEET
MIN 326.3
MAX 541.6
MEAN 418.6
STD DEV 32.61

LINE 120
 TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
 DATA ACQUIRED 811160



D62 mt



BARO PRESSURE
 MM HG
 MIN 690.8
 MAX 718.8
 MEAN 703.9
 STD DEV 4.862

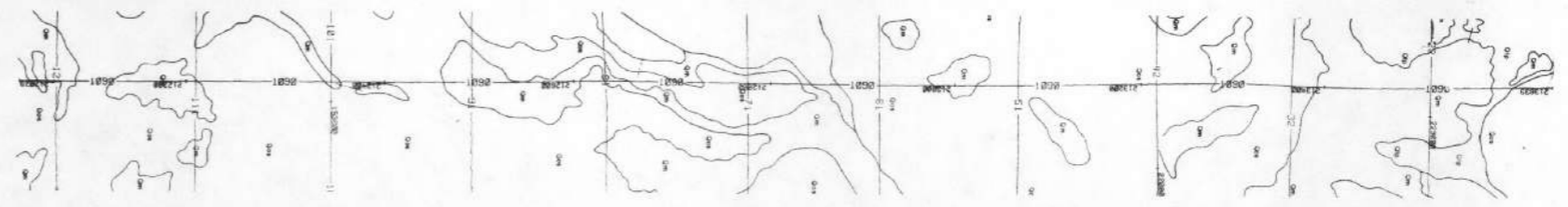
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 DEG C
 MIN 14.00
 MAX 18.00
 MEAN 16.13
 STD DEV 1.003

RESIDUAL MAG
 GAMMAS
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 MAX 727.1
 MEAN 445.8
 STD DEV 213.7

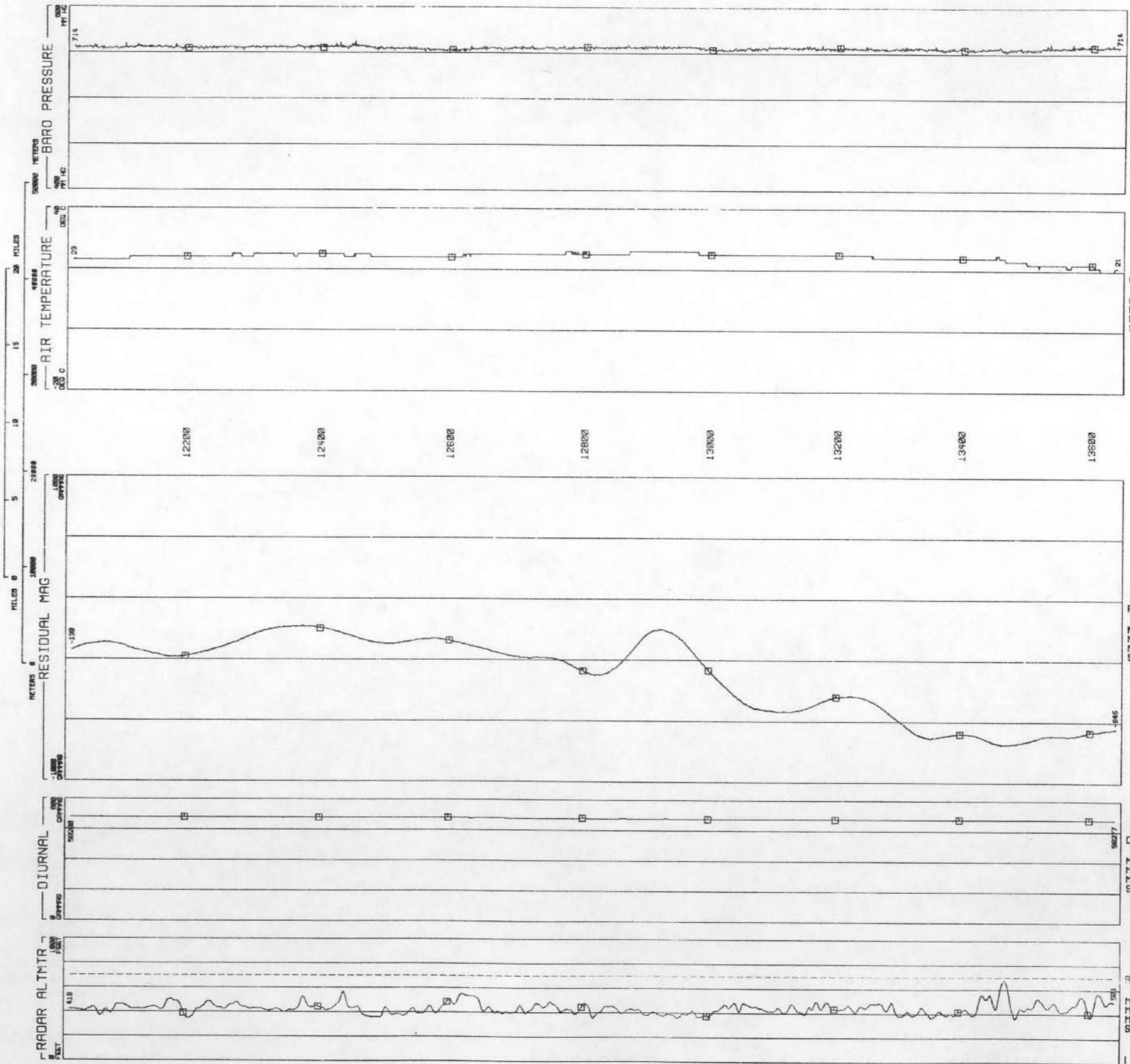
DIURNAL
 GAMMAS
 MIN 58292
 MAX 58298
 MEAN 58288
 STD DEV 6.071

RADAR ALTMTR
 FEET
 MIN 319.4
 MAX 541.8
 MEAN 422.8
 STD DEV 29.33

LINE 120



LINE 1090
 TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
 DATA ACQUIRED 81166



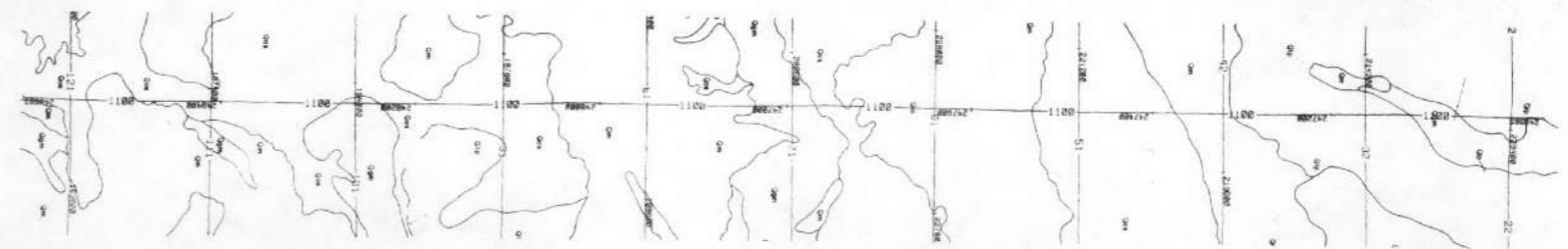
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 MM HG
 MIN 702.7
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 MEAN 711.1
 STD DEV 2.621

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 MAX 26.00
 MEAN 24.29
 STD DEV 1.146

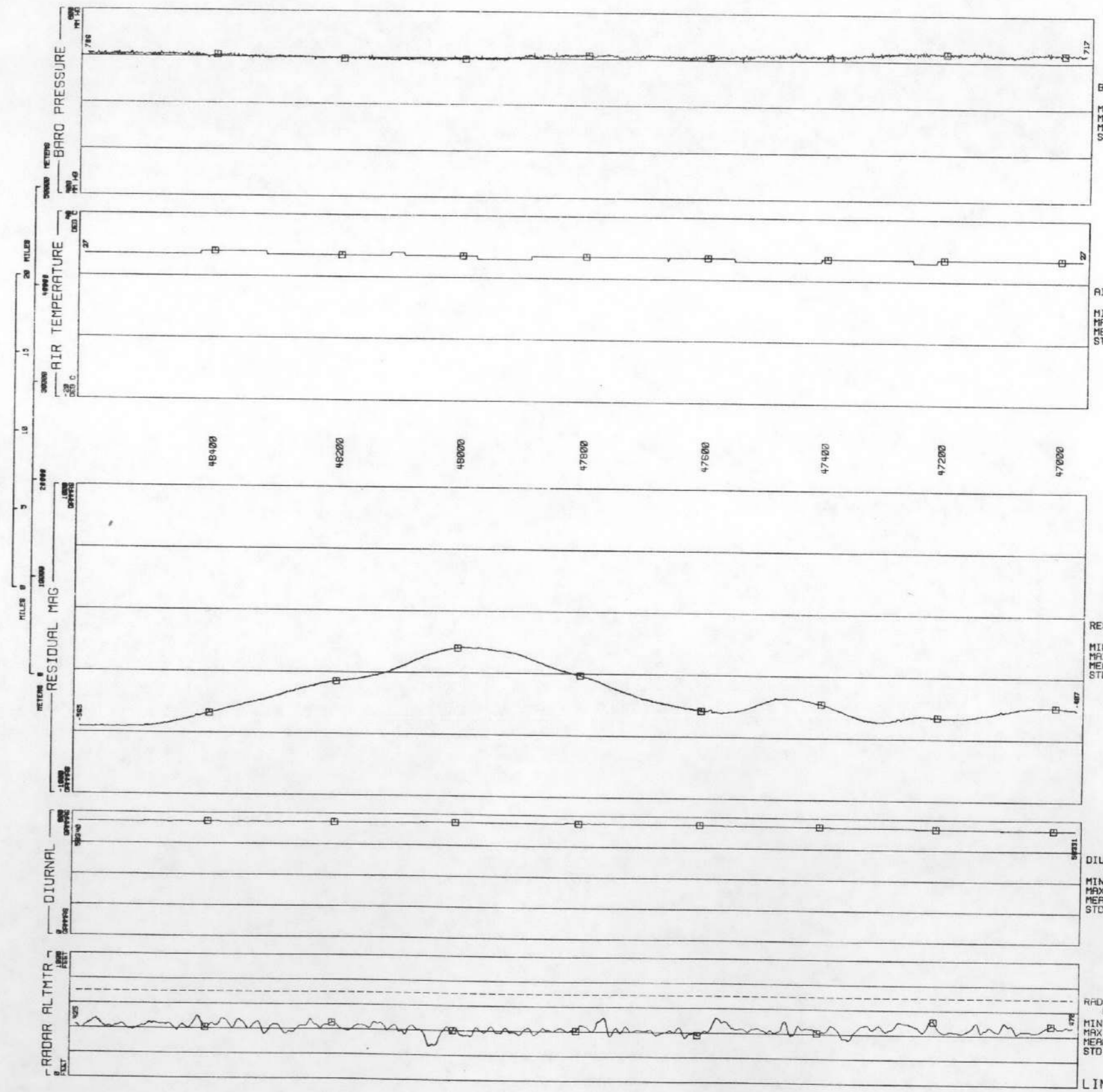
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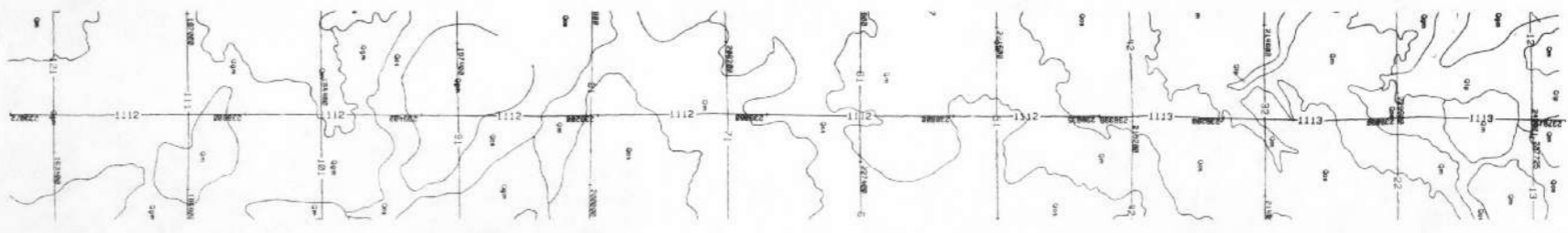
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 GAMMAS
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 MAX 56280
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RADAR ALTMTR
 FEET
 MIN 348.7
 MAX 673.4
 MEAN 435.5
 STD DEV 45.78

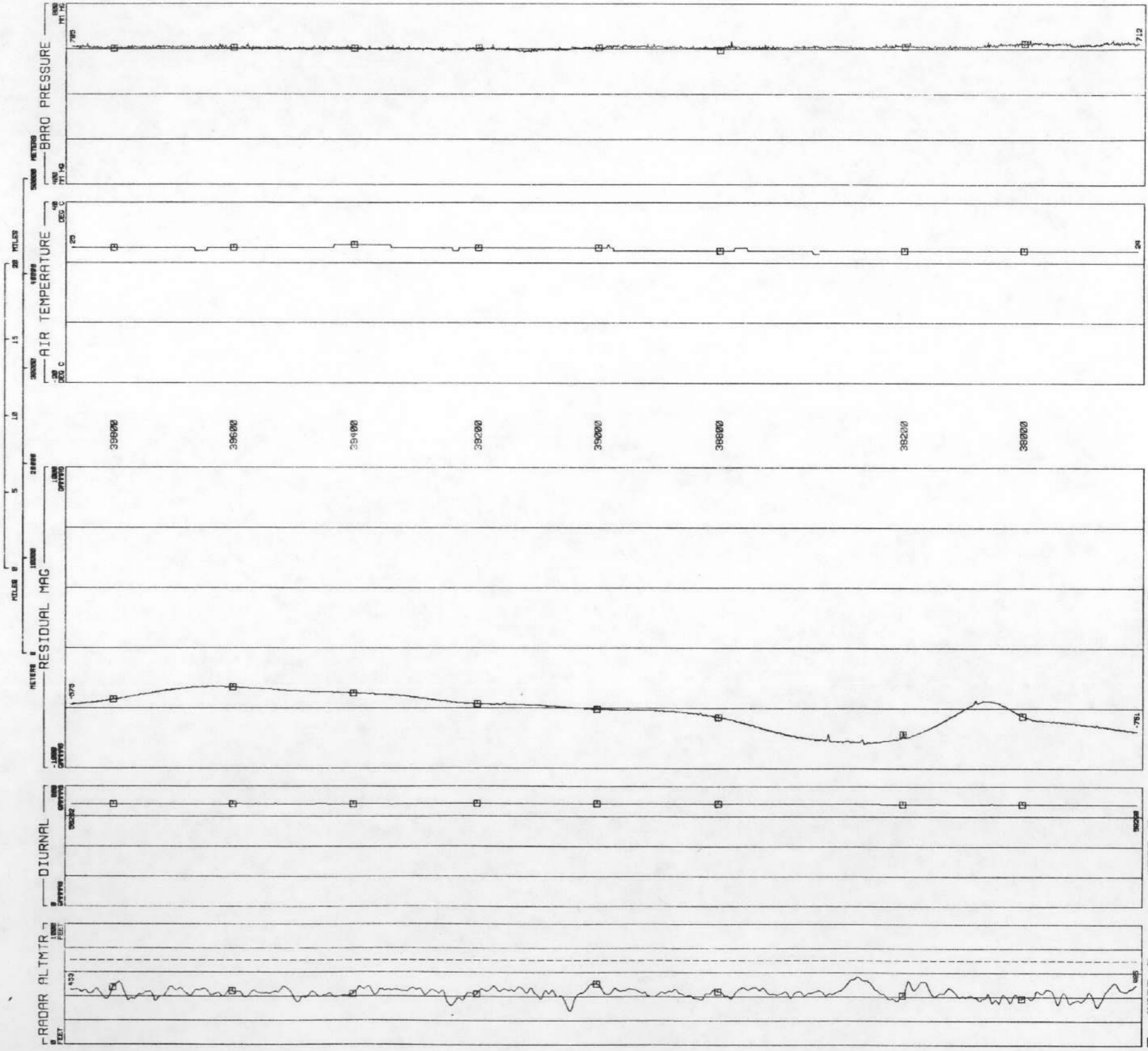


LINE 1100
 TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
 DATA ACQUIRED 81167





LINE 1110
 TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
 DATA ACQUIRED 81167



BARO PRESSURE
 MM HG
 MIN 693.4
 MAX 719.6
 MEAN 703.9
 STD DEV 4.057

AIR TEMPERATURE
 DEG C
 MIN 23.00
 MAX 25.00
 MEAN 24.55
 STD DEV .6037

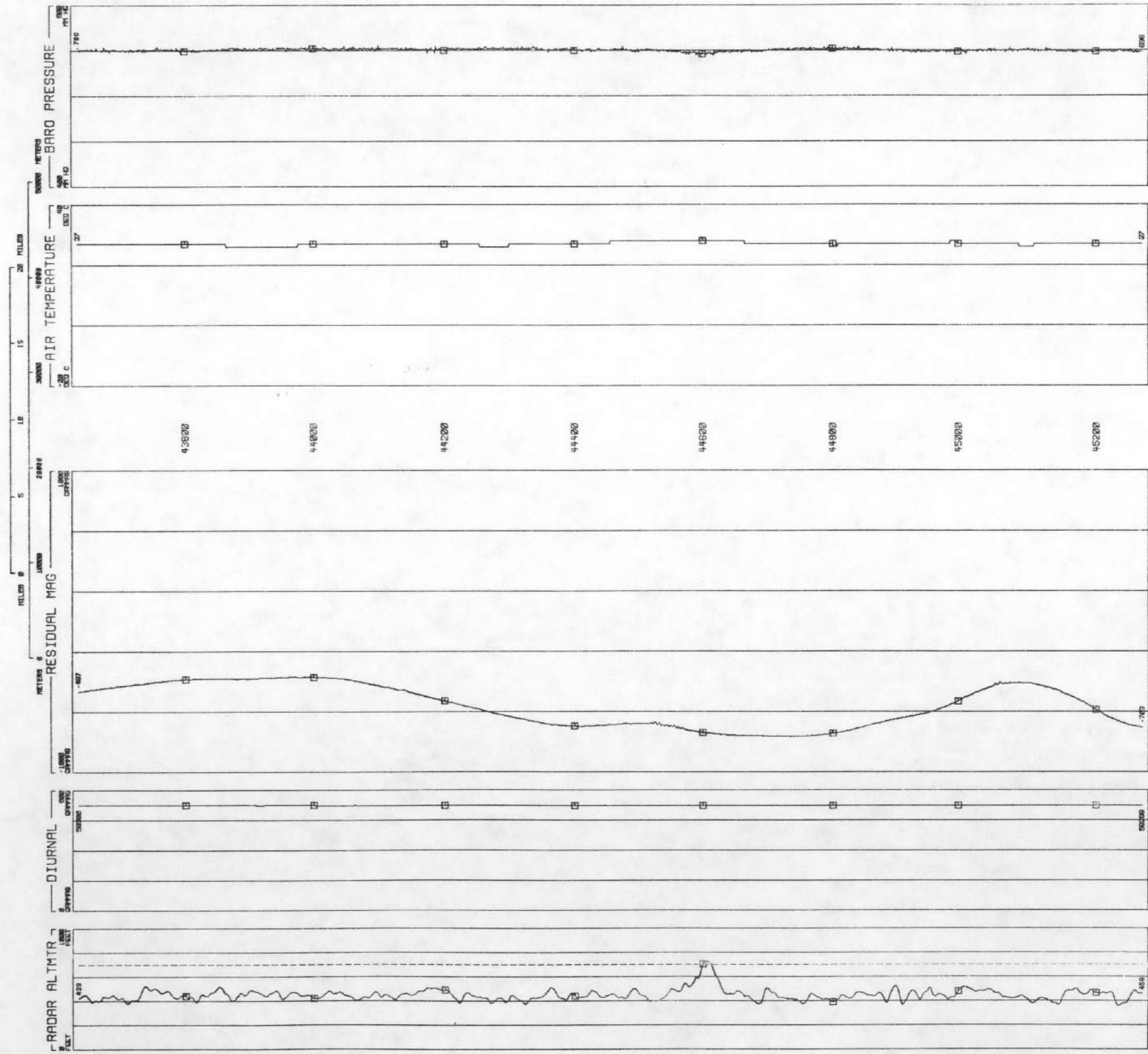
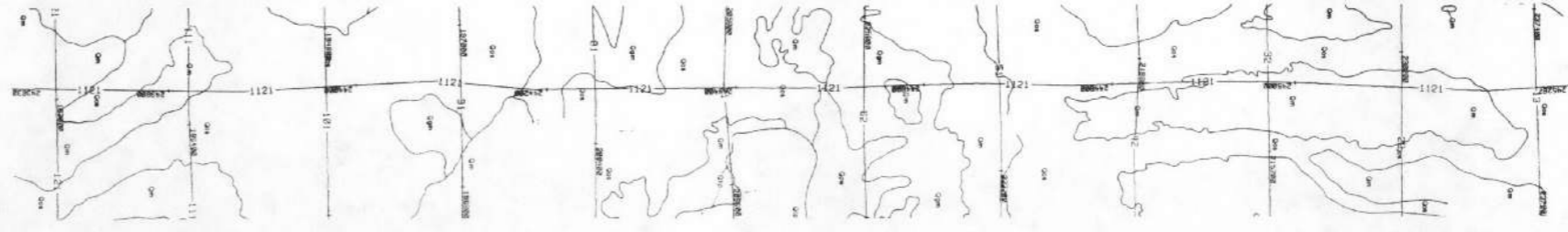
RESIDUAL MAG
 GAMMAS
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 MAX -455.9
 MEAN -612.1
 STD DEV 188.9

DIURNAL
 GAMMAS
 MIN 58279
 MAX 59279
 MEAN 59277
 STD DEV 5.238

RADAR ALTMTR
 FEET
 MIN 280.1
 MAX 566.4
 MEAN 430.9
 STD DEV 48.27

LINE 1110

LINE 1120
TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
DATA ACQUIRED 81167



BARO PRESSURE
MM HG
MIN 687.9
MAX 710.1
MEAN 700.9
STD DEV 3.003

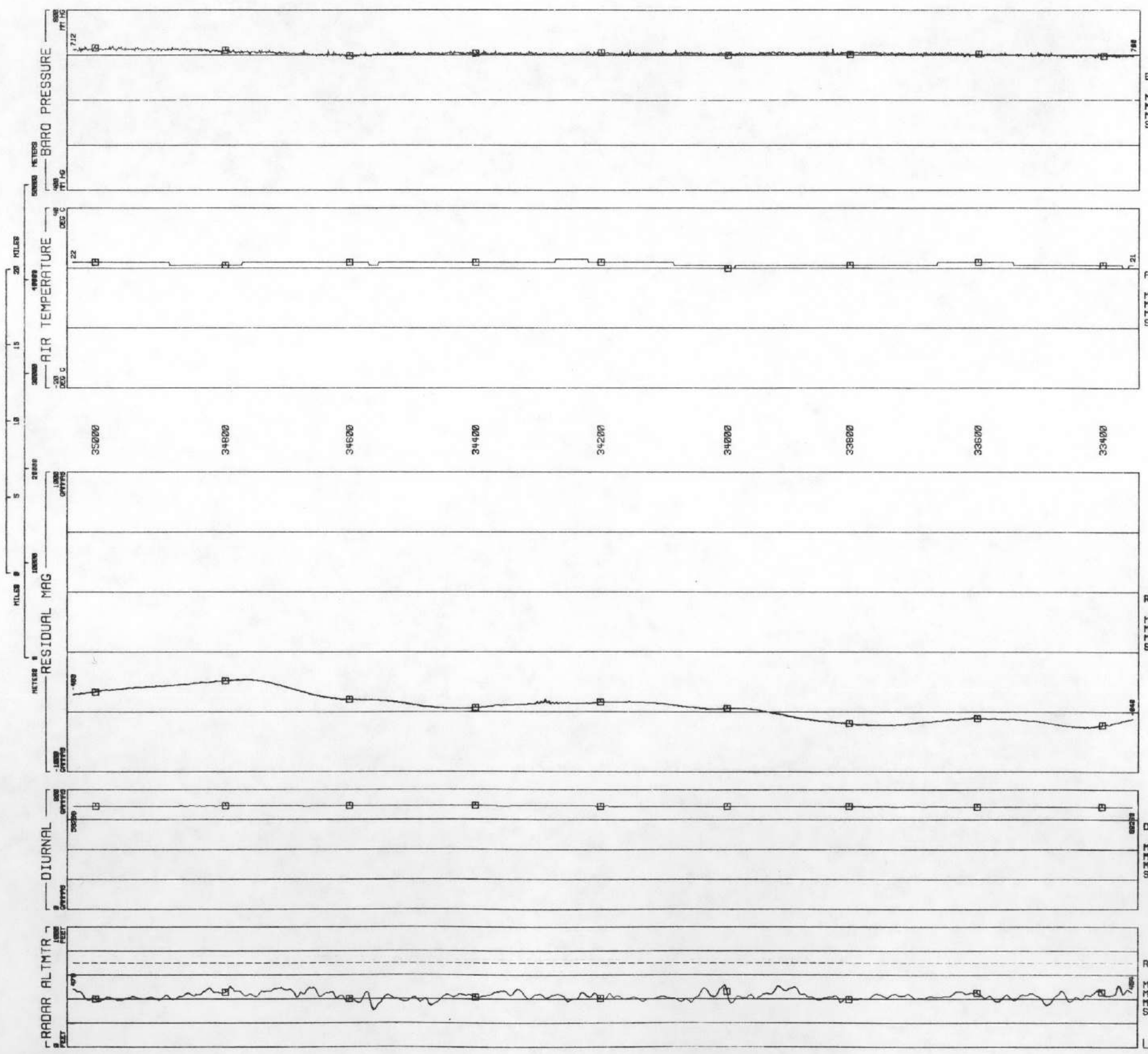
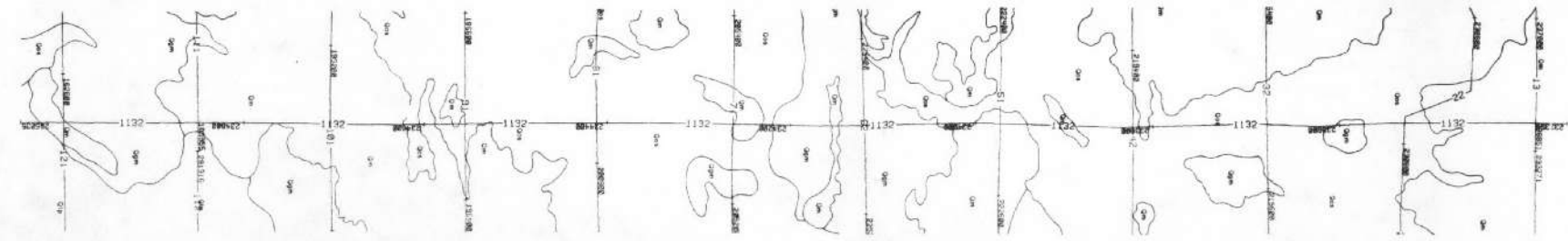
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MAX 28.00
MEAN 27.02
STD DEV .4931

RESIDUAL MAG
GAMMAS
MIN -766.2
MAX -368.1
MEAN -561.3
STD DEV 139.9

DIURNAL
GAMMAS
MIN 58294
MAX 58300
MEAN 58293
STD DEV 4.282

RADAR ALTMTR
FEET
MIN 359.2
MAX 725.6
MEAN 449.4
STD DEV 47.03

LINE 1130
TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
DATA ACQUIRED 81167



BARO PRESSURE
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MAX 720.2
MEAN 703.9
STD DEV 4.352

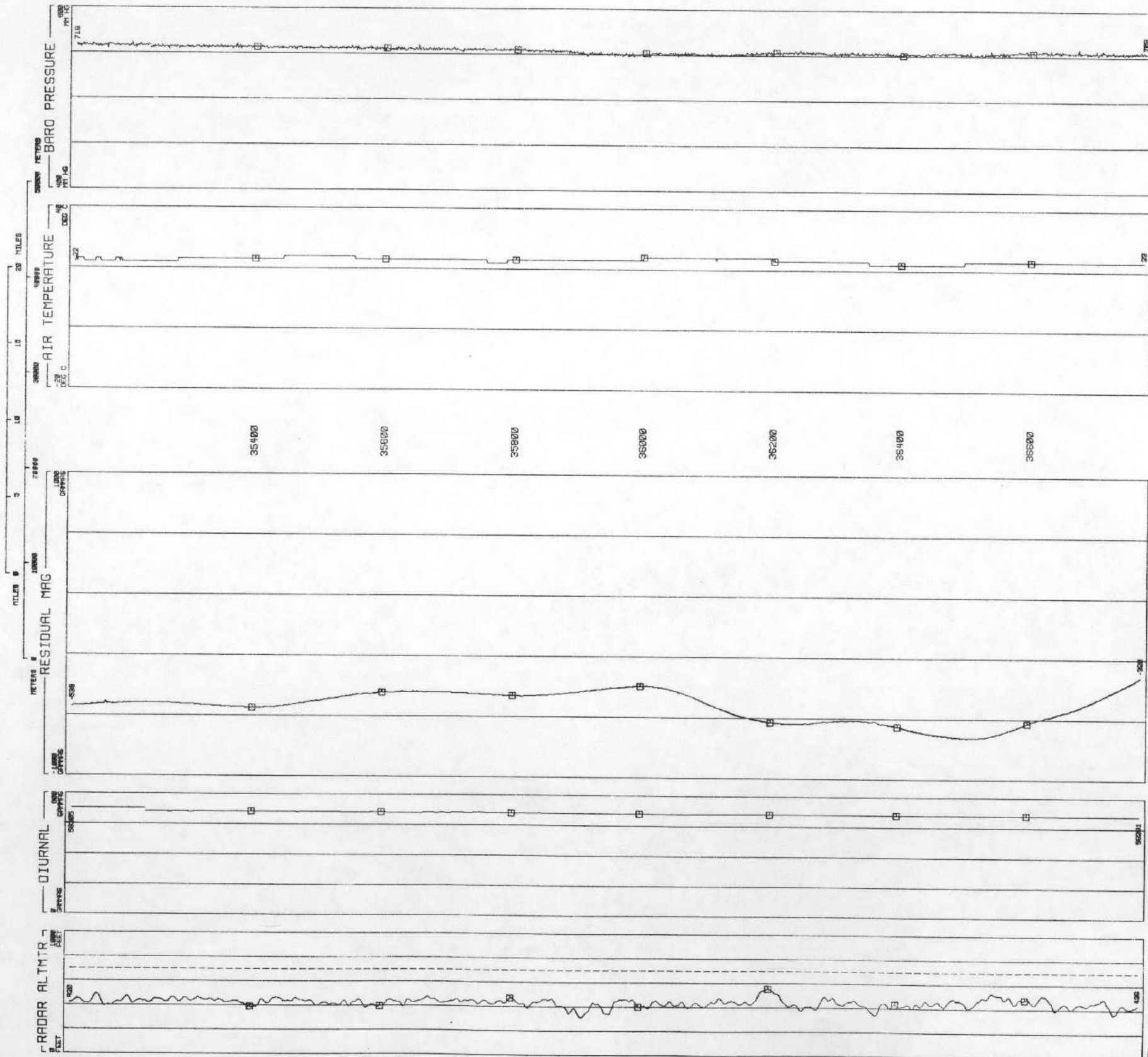
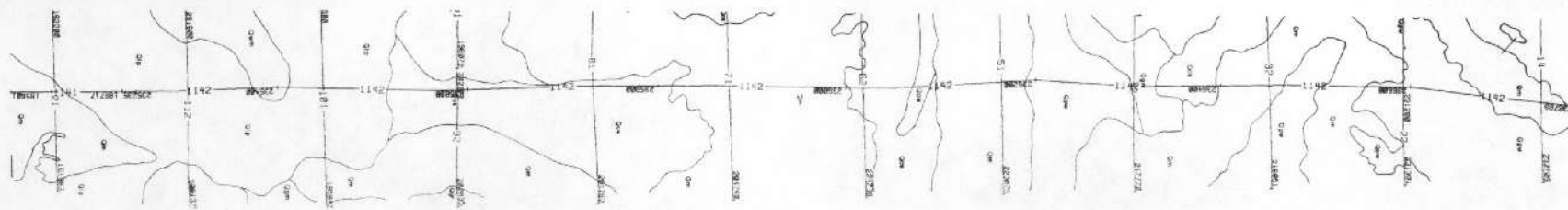
AIR TEMPERATURE
DEG C
MIN 20.00
MAX 23.00
MEAN 21.58
STD DEV .5763

RESIDUAL MAG
GAMMAS
MIN -702.6
MAX -384.3
MEAN -561.4
STD DEV 91.10

DIURNAL
GAMMAS
MIN 58283
MAX 58292
MEAN 58283
STD DEV 6.234

RADAR ALTMTR
FEET
MIN 305.1
MAX 513.7
MEAN 424.1
STD DEV 31.39

LINE 1140
TRAVERSE CITY QUADRANGLE - NTMS NL 16-12
DATA ACQUIRED 81162



BARO PRESSURE
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MAX 721.8
MEAN 708.0
STD DEV 4.733

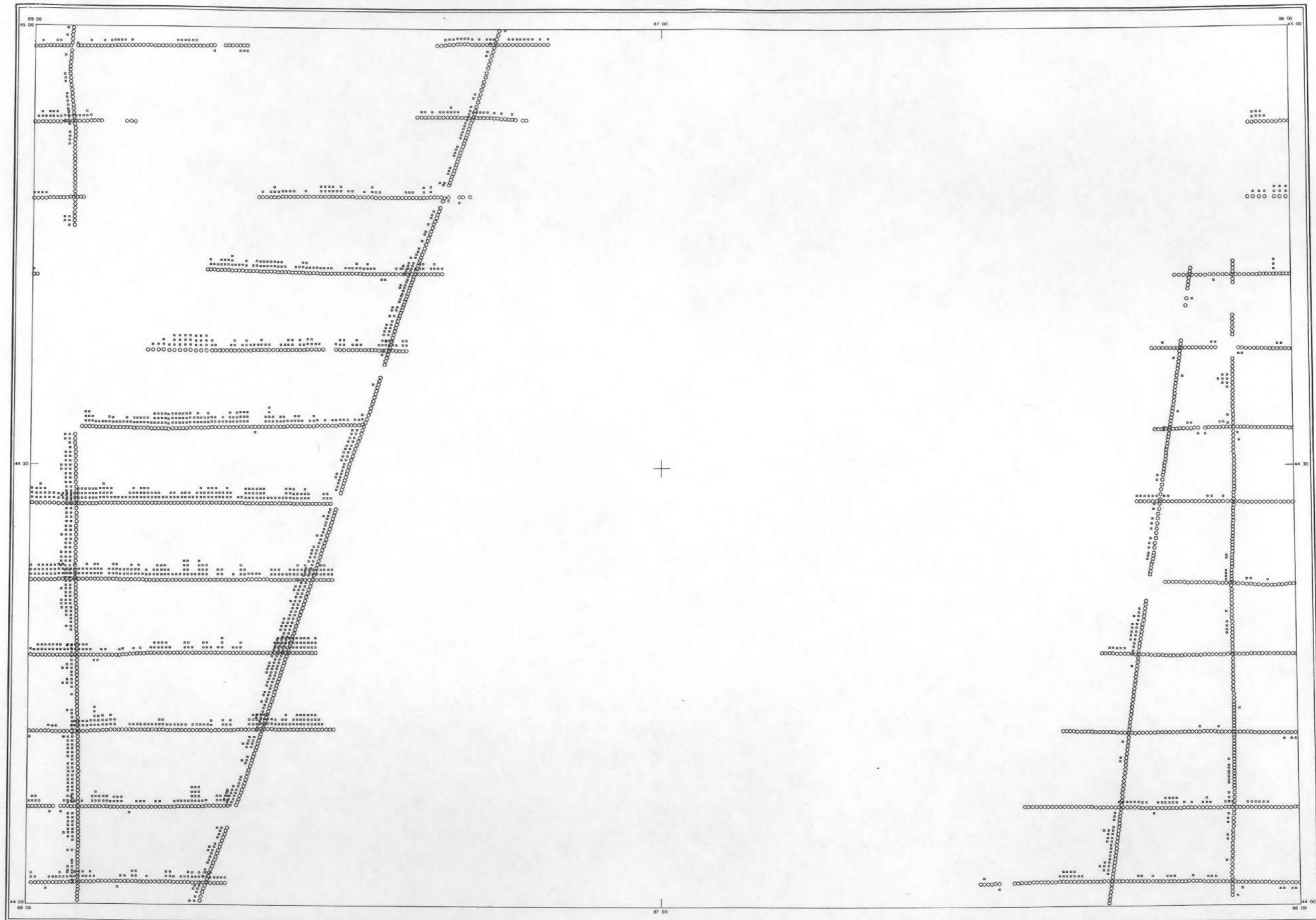
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DEG C
MIN 22.00
MAX 24.00
MEAN 23.00
STD DEV .6161

RESIDUAL MAG
GAMMAS
MIN -726.1
MAX -319.5
MEAN -528.2
STD DEV 93.02

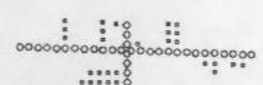
DIURNAL
GAMMAS
MIN 58279
MAX 58305
MEAN 58279
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RADAR ALTMTR
FEET
MIN 311.4
MAX 553.6
MEAN 433.9
STD DEV 33.26

APPENDIX E - Standard Deviation Maps

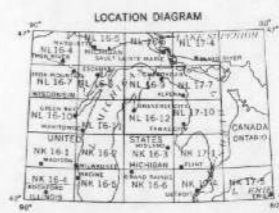


SCALE 1:500,000



○ - DATA STATISTICALLY ADEQUATE
 BLANK - DATA STATISTICALLY INADEQUATE
 × - 1 σ ABOUT MEASURE OF CENTRAL TENDENCY

NOTE: ON E-W LINES, +σ TO NORTH, -σ TO SOUTH
 ON N-S LINES, +σ TO WEST, -σ TO EAST.

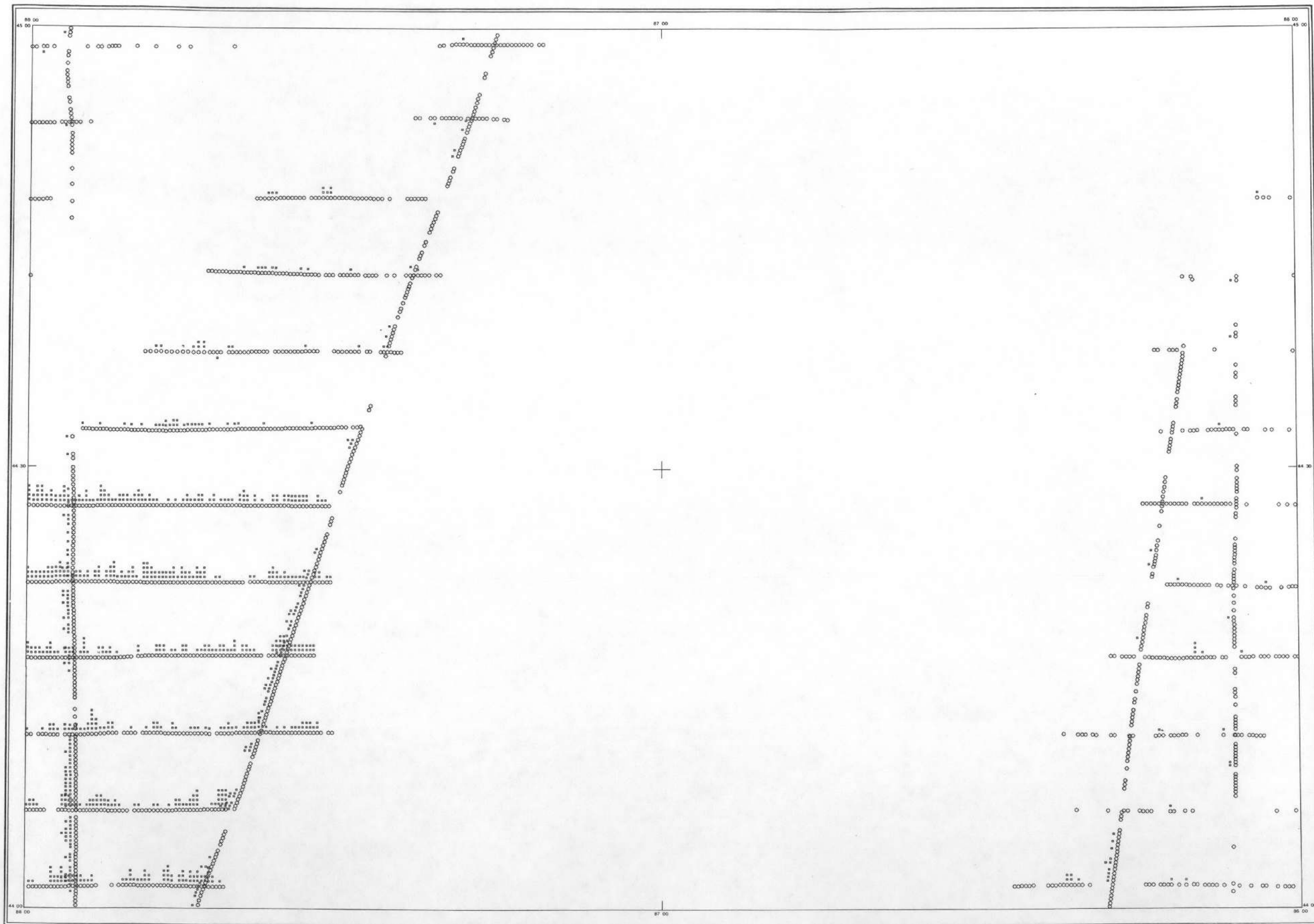


POTASSIUM STANDARD DEVIATION MAP

GREAT LAKES PROJECT

U. S. DEPARTMENT OF ENERGY

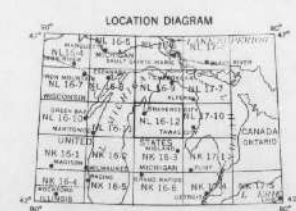
SURVEY AND
 COMPILED BY:
 EGG GEOMETRICS



SCALE 1:500,000



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 □ - DATA STATISTICALLY INADEQUATE
 * - 1 σ ABOUT MEASURE OF CENTRAL TENDENCY
 NOTE: ON E-W LINES, +σ TO NORTH, -σ TO SOUTH.
 ON N-S LINES, +σ TO WEST, -σ TO EAST.

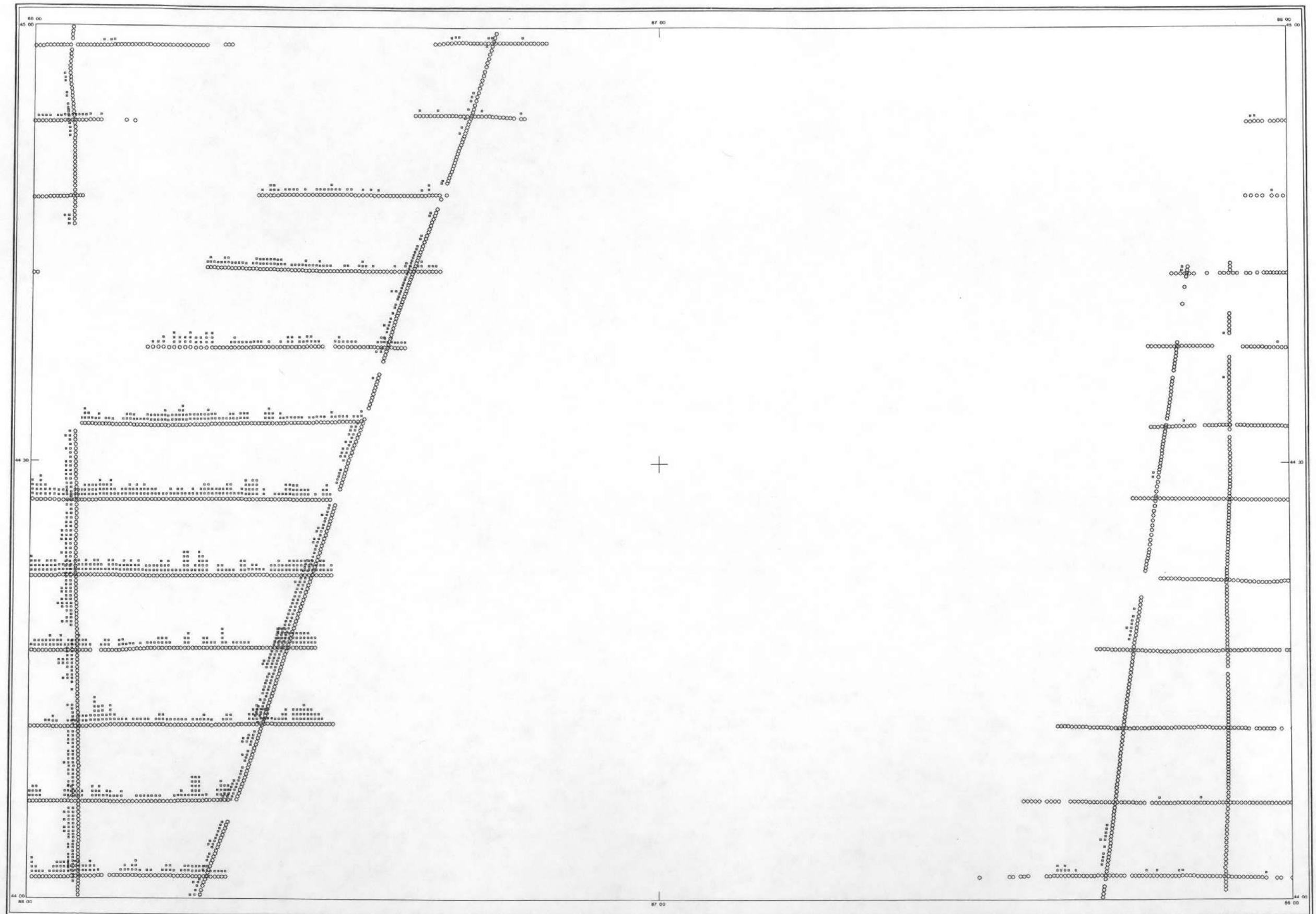


URANIUM STANDARD DEVIATION MAP

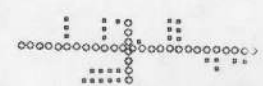
GREAT LAKES PROJECT

U. S. DEPARTMENT OF ENERGY

SURVEY AND
 COMPILED BY:
EG&G GEOMETRICS

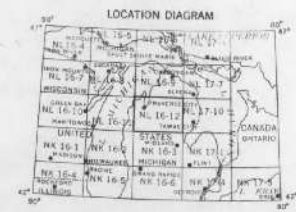


SCALE 1:500,000



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 ✕ - DATA STATISTICALLY INADEQUATE
 • - 1 σ ABOUT MEASURE OF CENTRAL TENDENCY

NOTE: ON E-W LINES, +σ TO NORTH, -σ TO SOUTH.
 ON N-S LINES, +σ TO WEST, -σ TO EAST.



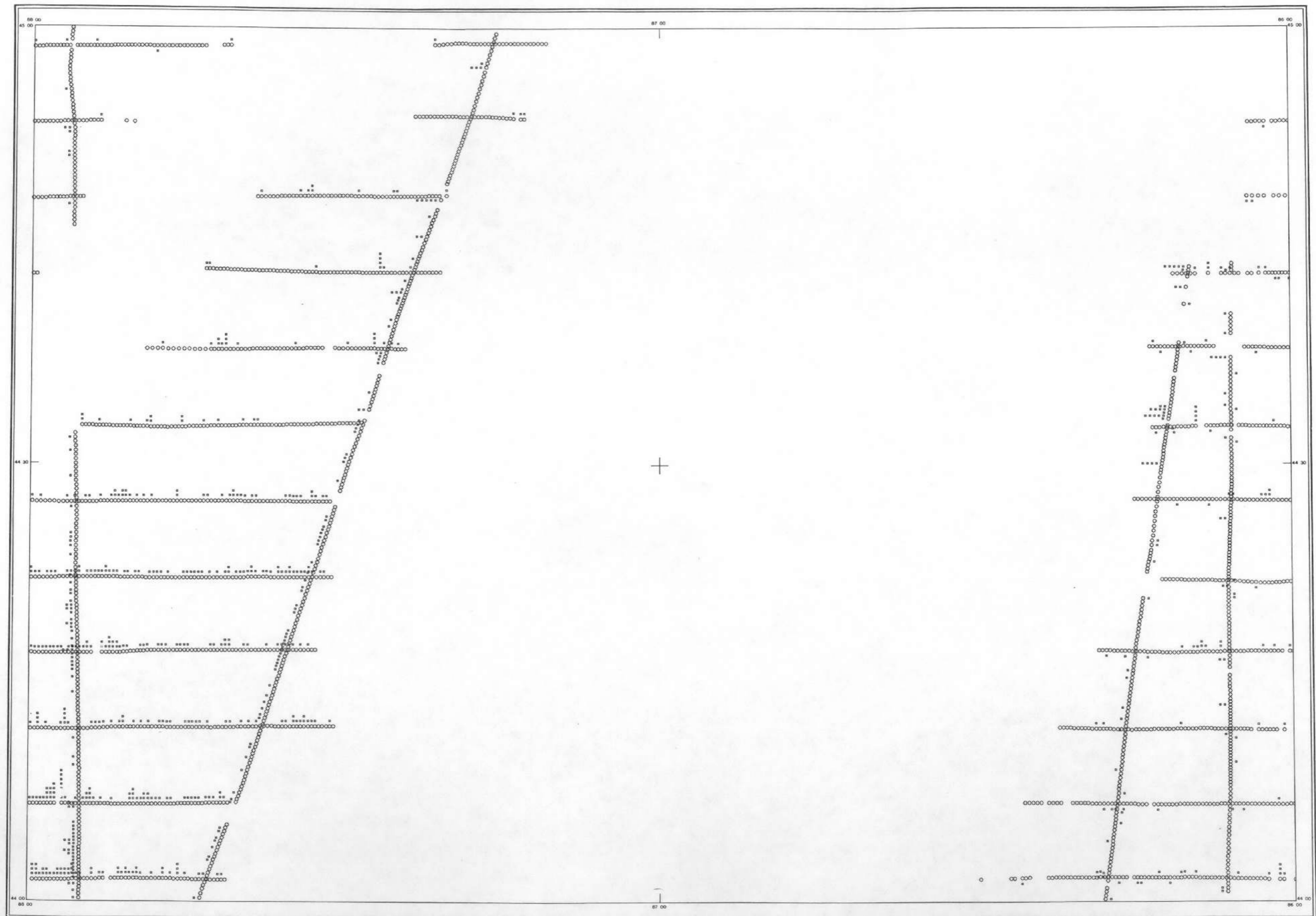
THORIUM STANDARD DEVIATION MAP

GREAT LAKES PROJECT

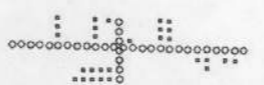
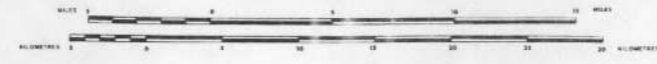
U. S. DEPARTMENT OF ENERGY

SURVEY AND
 COMPILED BY:
EG&G GEOMETRICS

MANITOWOC

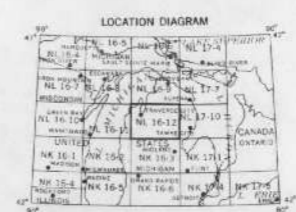


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 ■ - 1 σ ABOUT MEASURE OF CENTRAL TENDENCY

NOTE: ON E-W LINES, +σ TO NORTH, -σ TO SOUTH.
 ON N-S LINES, +σ TO WEST, -σ TO EAST.

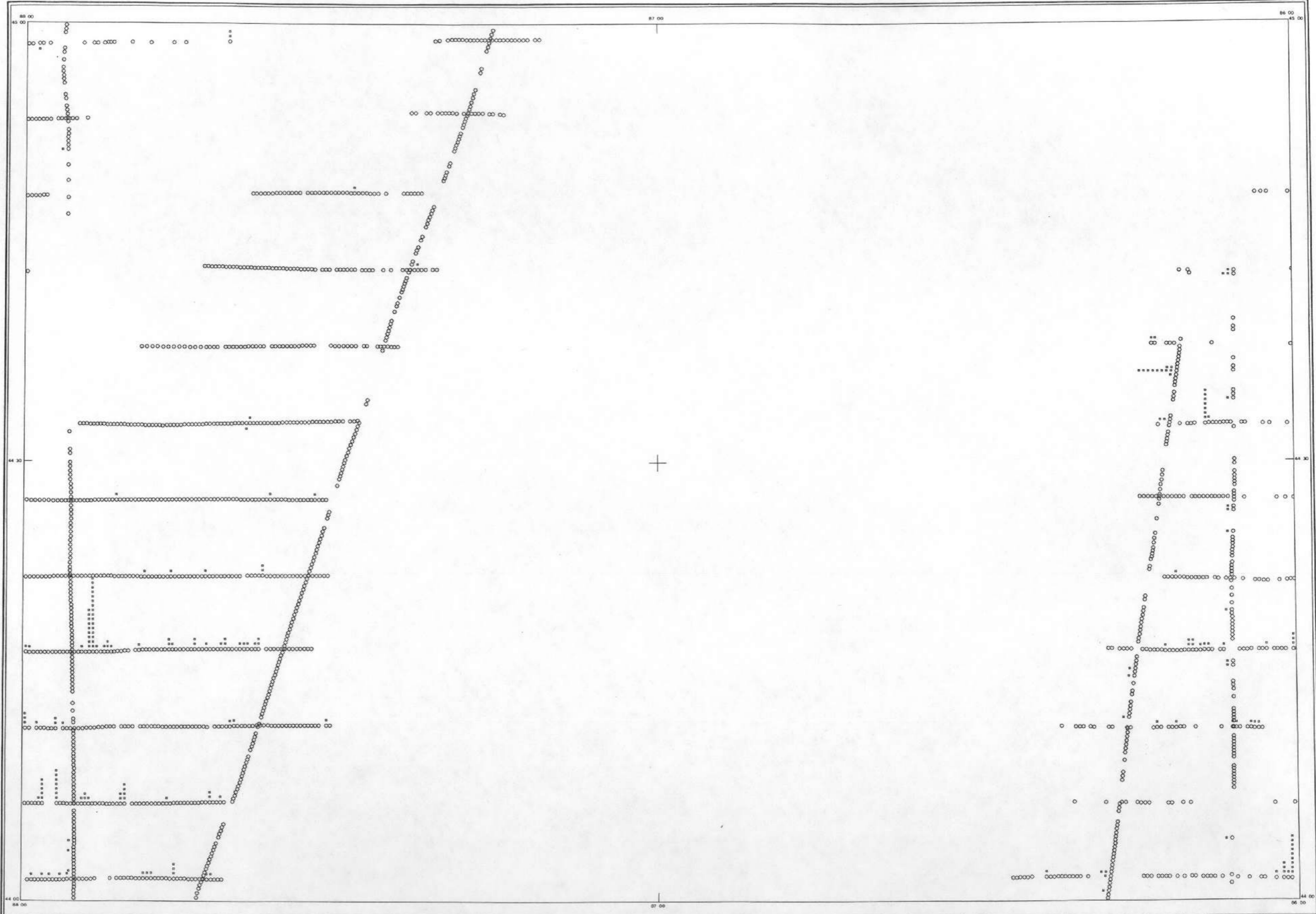


THORIUM / POTASSIUM STANDARD DEVIATION MAP

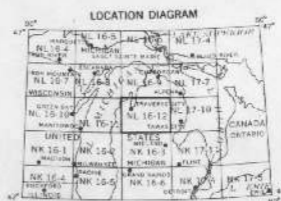
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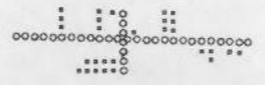


URANIUM / POTASSIUM STANDARD DEVIATION MAP

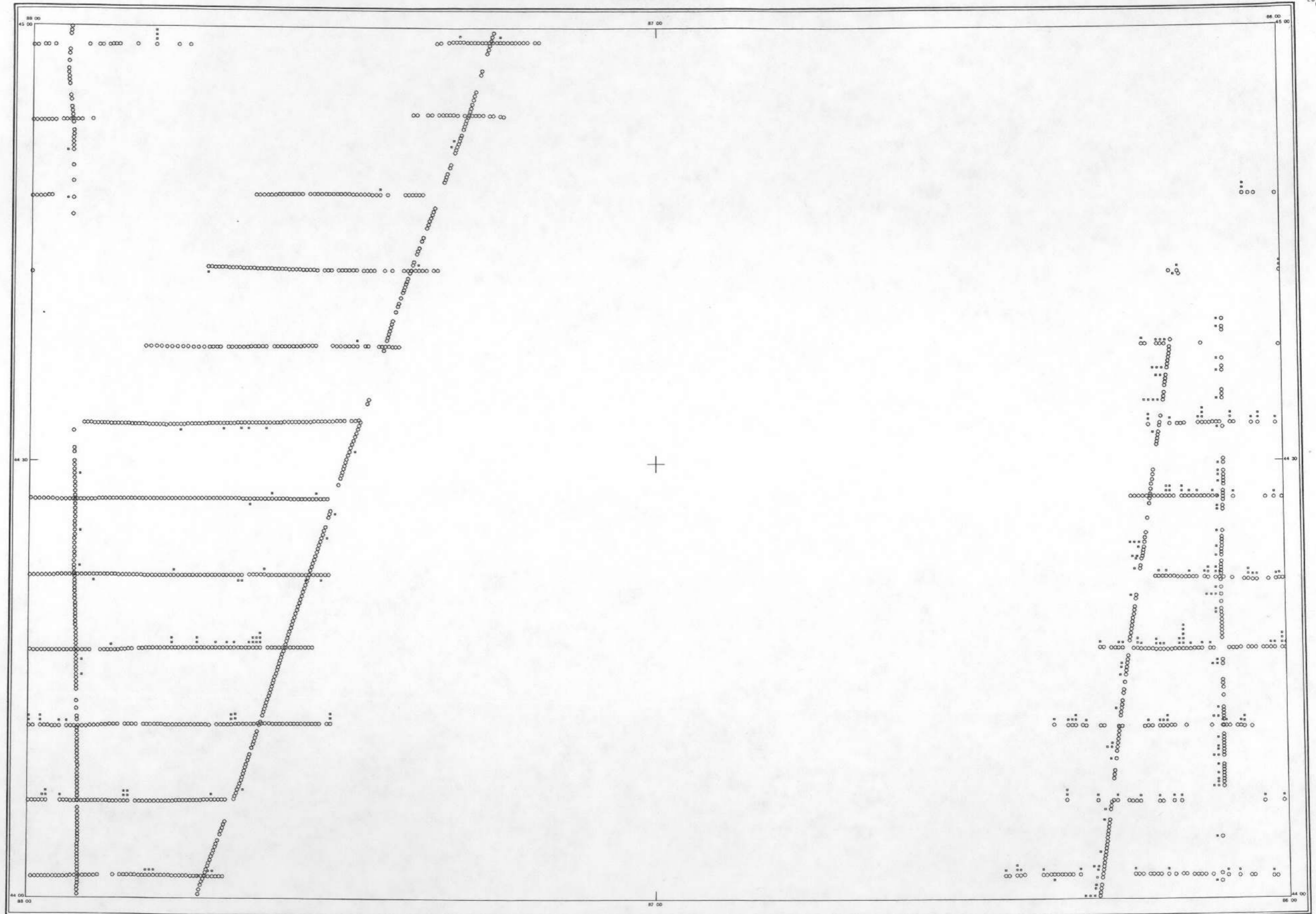
GREAT LAKES PROJECT

U. S. DEPARTMENT OF ENERGY

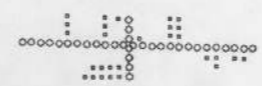
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EG&G GEOMETRICS



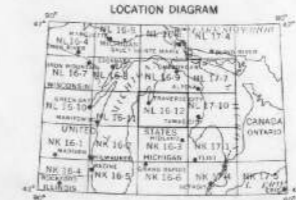
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ON N-S LINES, +σ TO WEST, -σ TO EAST.



SCALE 1:500,000



NOTE: ON E-W LINES, +σ TO NORTH, -σ TO SOUTH.
ON N-S LINES, +σ TO WEST, -σ TO EAST.



URANIUM / THORIUM STANDARD DEVIATION MAP

GREAT LAKES PROJECT

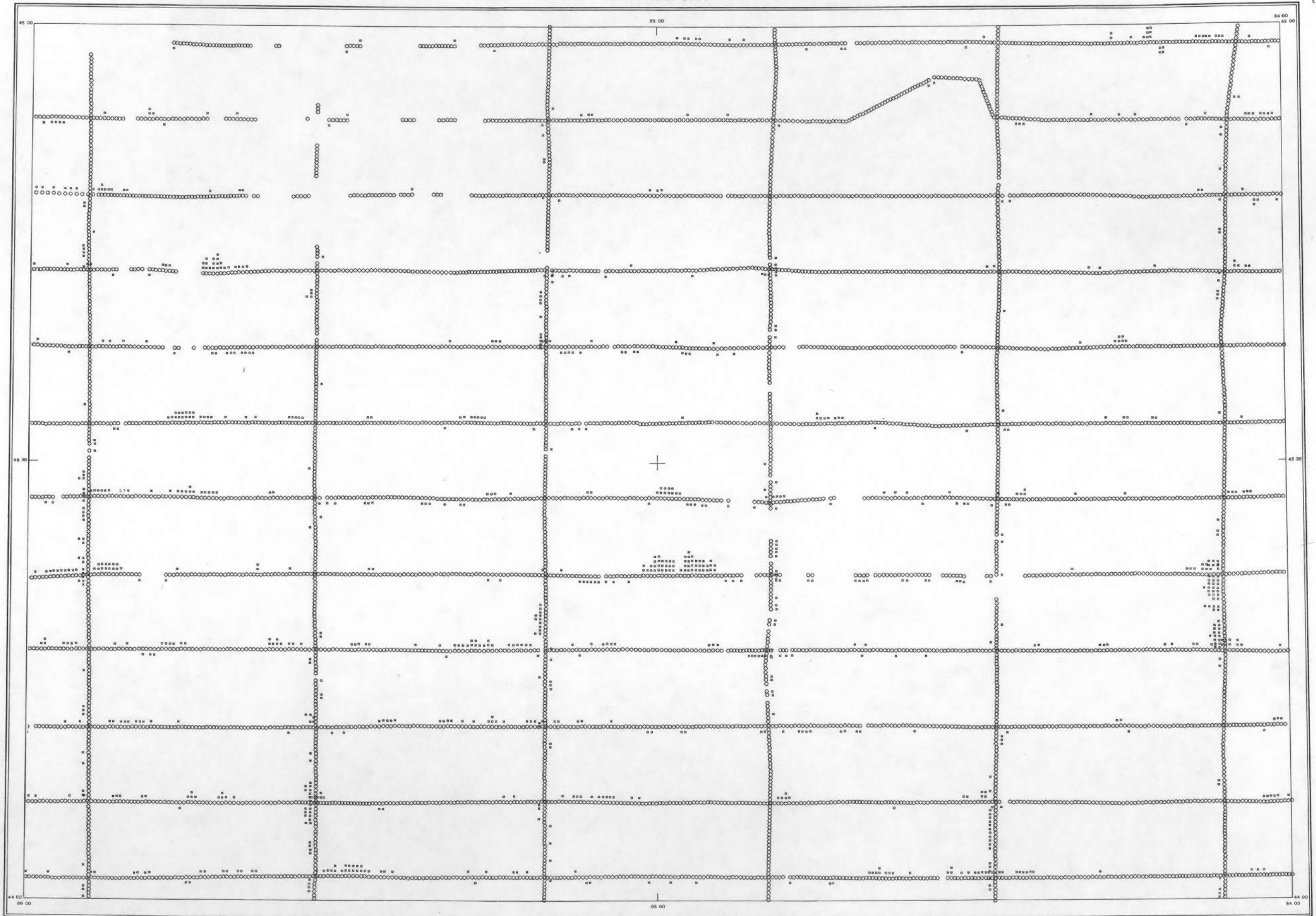
U. S. DEPARTMENT OF ENERGY

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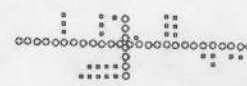


TRAVERSE CITY

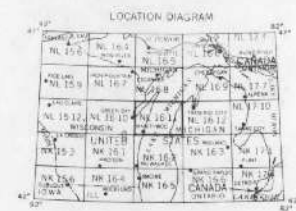
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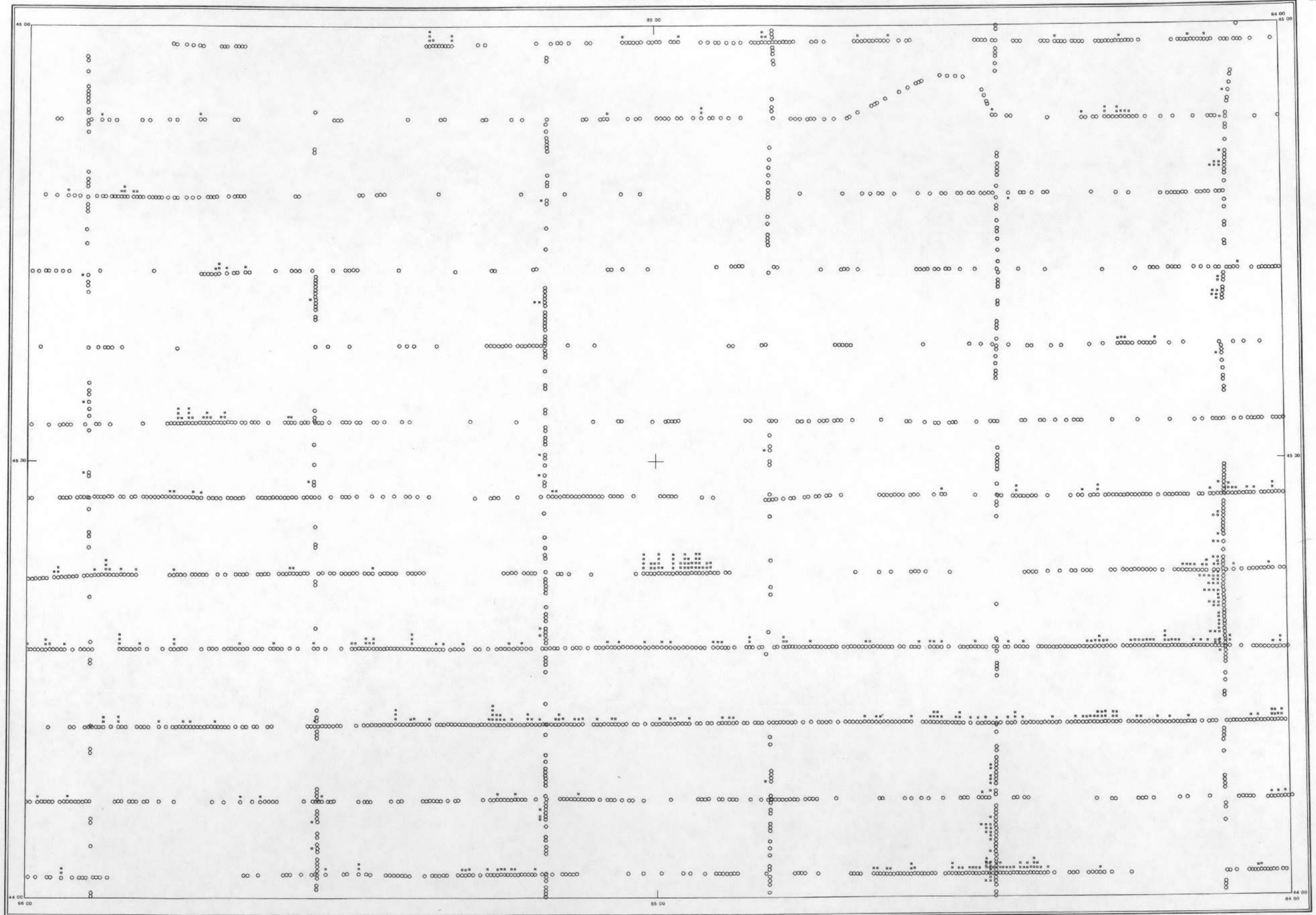
POTASSIUM STANDARD DEVIATION MAP

GREAT LAKES PROJECT

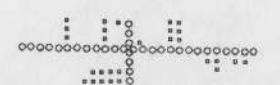
U. S. DEPARTMENT OF ENERGY

SURVEY AND
 COMPILED BY
 EG&G GEOMETRICS

TRAVERSE CITY



SCALE 1:500,000



○ DATA STATISTICALLY ADEQUATE
 ✕ DATA STATISTICALLY INADEQUATE
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 NOTE: ON E-W LINES, + TO NORTH, - TO SOUTH.
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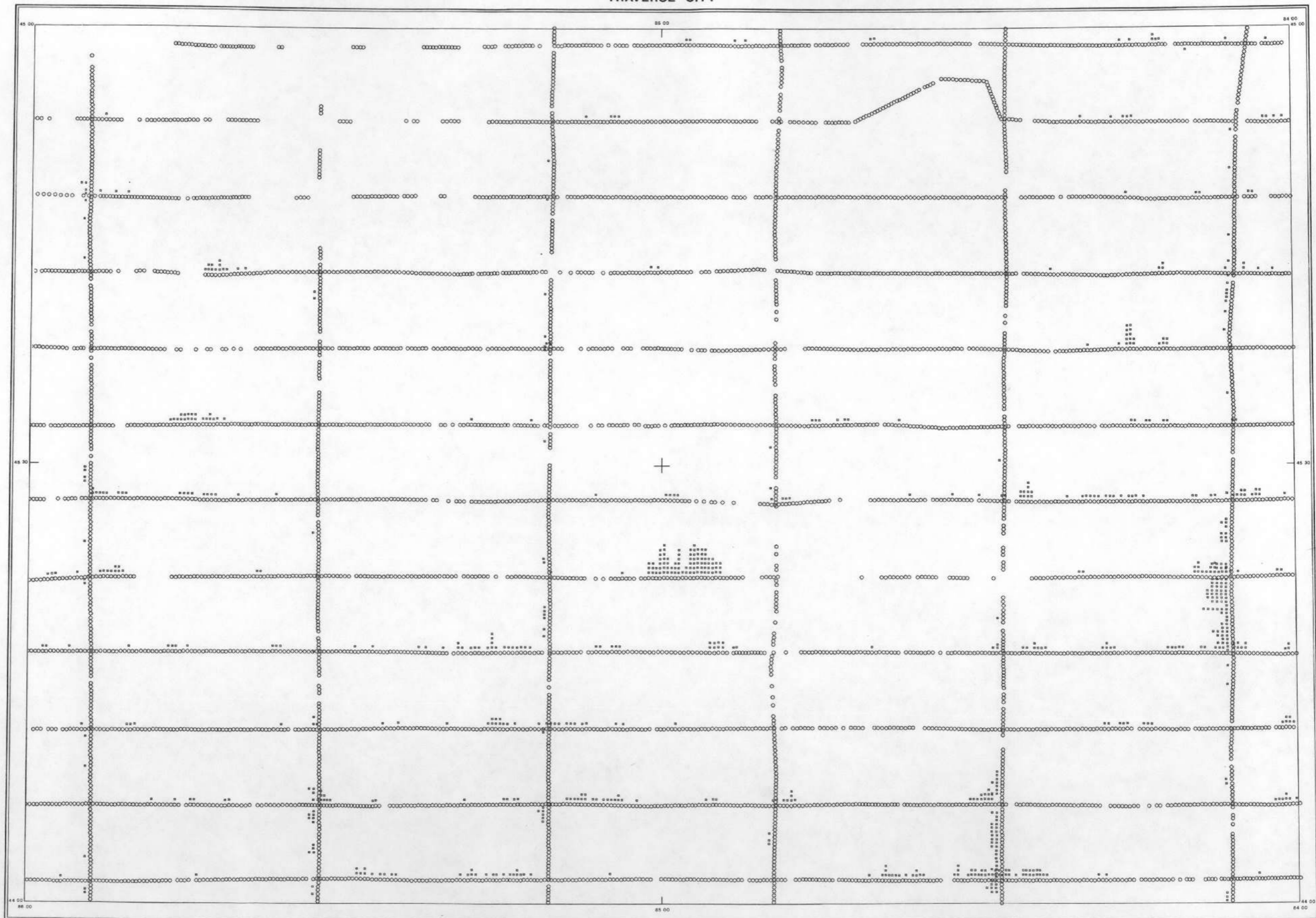
URANIUM STANDARD DEVIATION MAP

GREAT LAKES PROJECT

U. S. DEPARTMENT OF ENERGY

TRAVERSE CITY

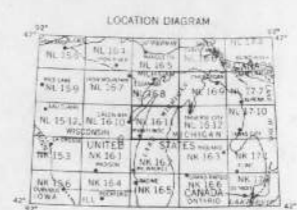
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SCALE 1:500,000



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 ON N-S LINES, +σ TO WEST, -σ TO EAST.



THORIUM STANDARD DEVIATION MAP

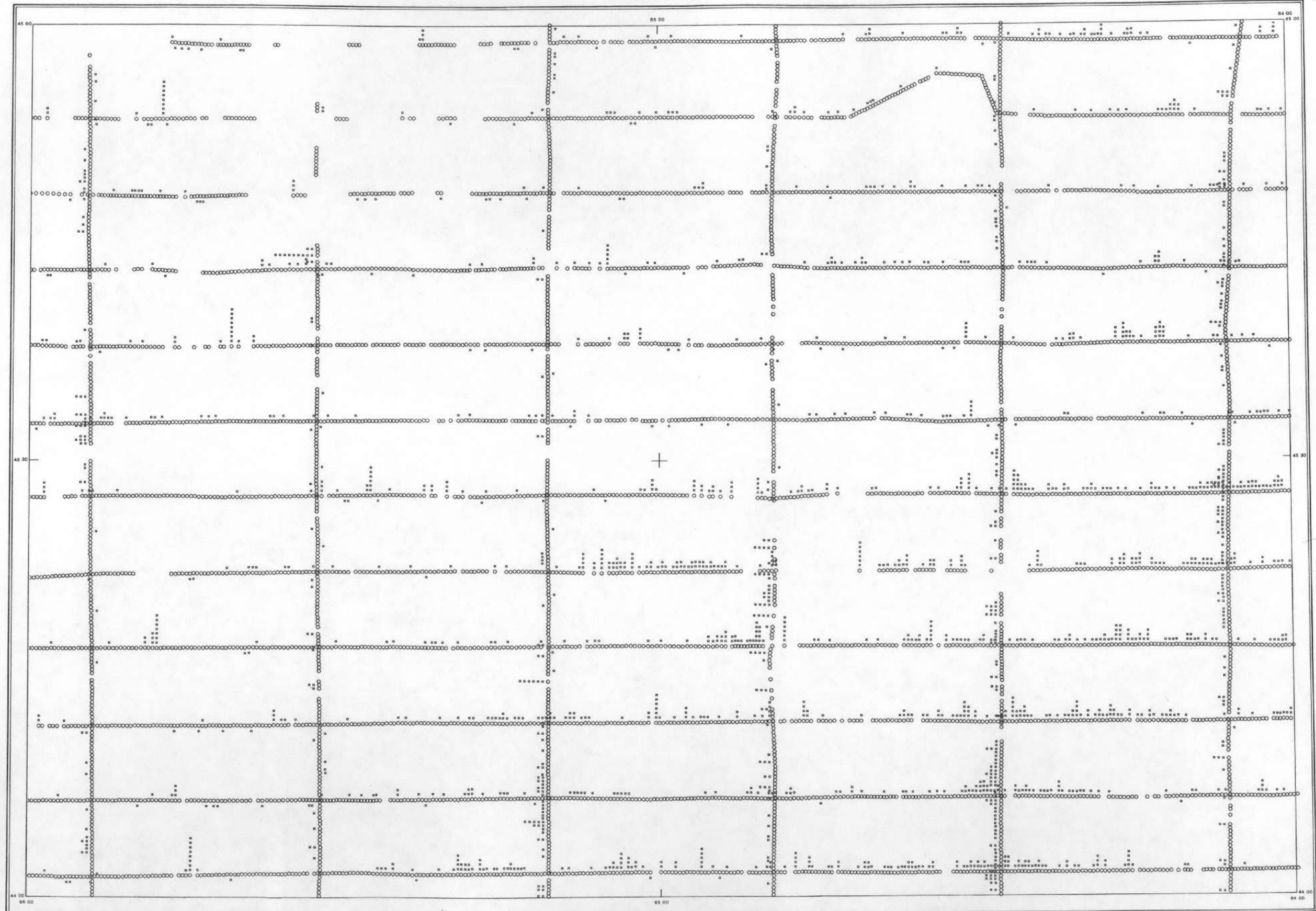
GREAT LAKES PROJECT

U. S. DEPARTMENT OF ENERGY

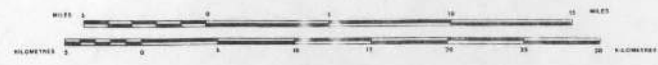
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TRAVERSE CITY

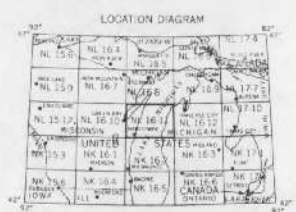
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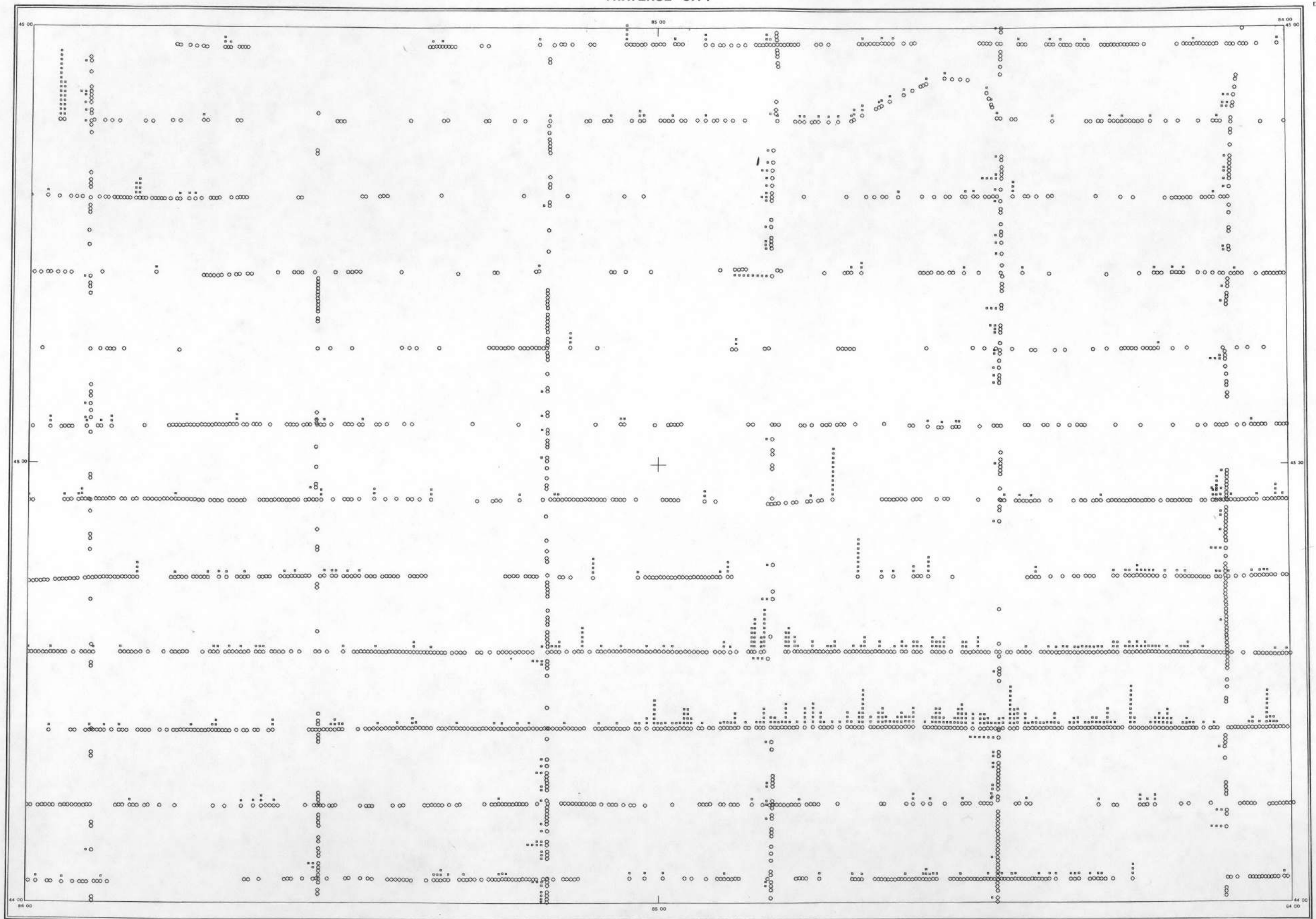


THORIUM / POTASSIUM STANDARD DEVIATION MAP

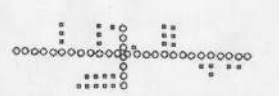
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U. S. DEPARTMENT OF ENERGY

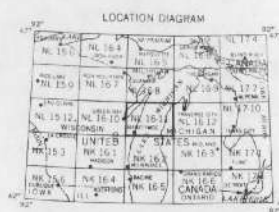
SURVEY AND
 COMPILATION BY
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SCALE 1:500,000



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 + MEASURE OF CENTRAL TENDENCY
 NOTE: ON E-W LINES, + TO NORTH, - TO SOUTH
 ON N-S LINES, + TO WEST, - TO EAST.



URANIUM / POTASSIUM STANDARD DEVIATION MAP

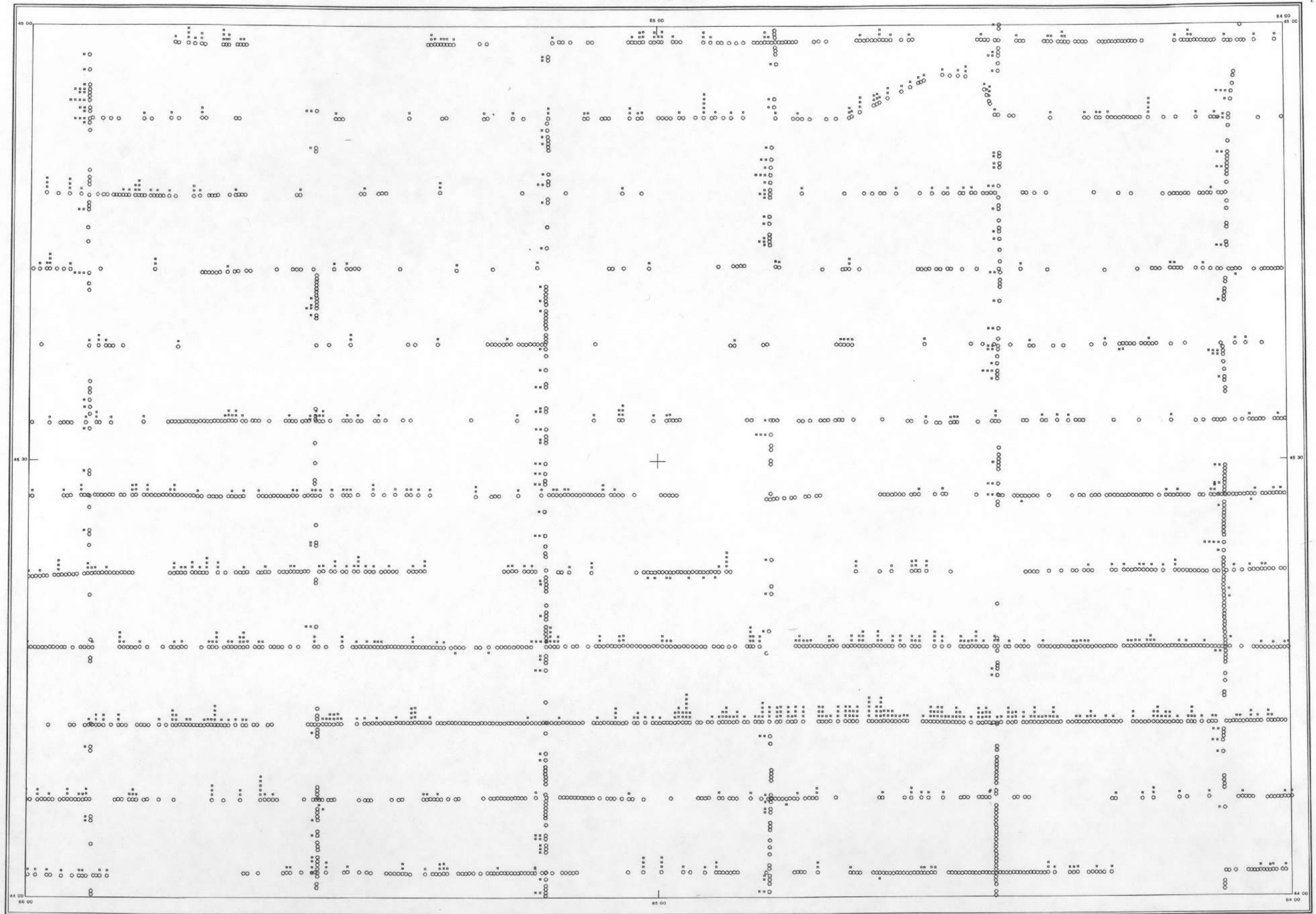
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U. S. DEPARTMENT OF ENERGY

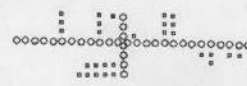
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TRAVERSE CITY

E12

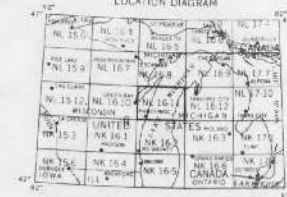


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○ - DATA STATISTICALLY ADEQUATE
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 + - 1 σ ABOUT MEASURE OF CENTRAL TENDENCY
 NOTE: ON E-W LINES, +σ TO NORTH, -σ TO SOUTH.
 ON N-S LINES, +σ TO WEST, -σ TO EAST.

LOCATION DIAGRAM



URANIUM / THORIUM STANDARD DEVIATION MAP

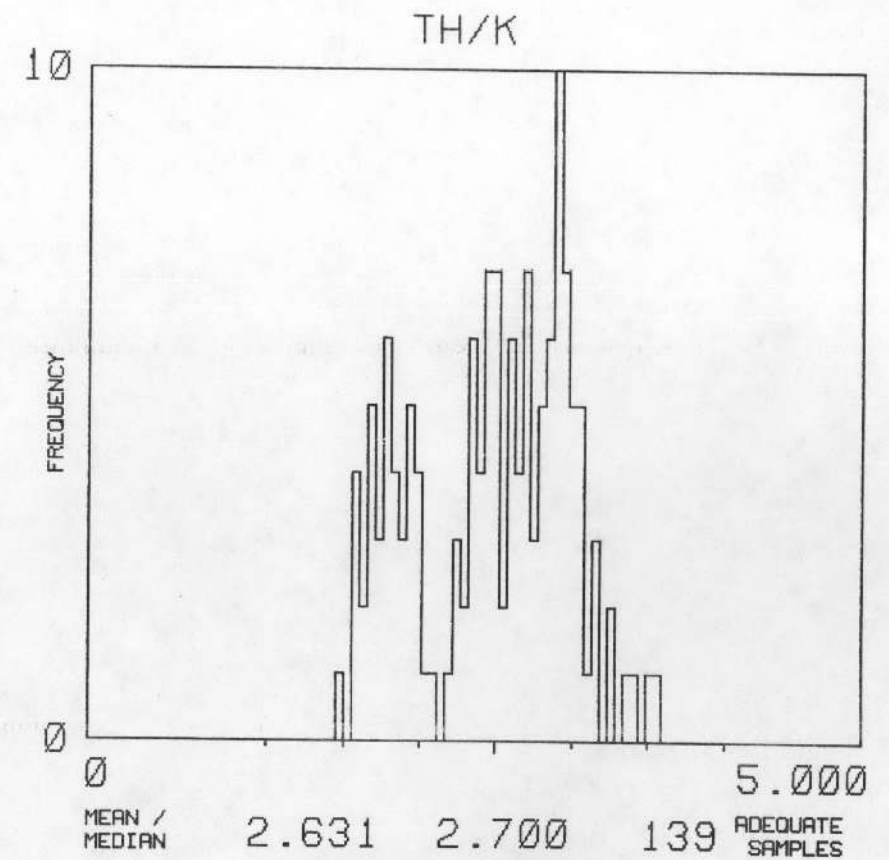
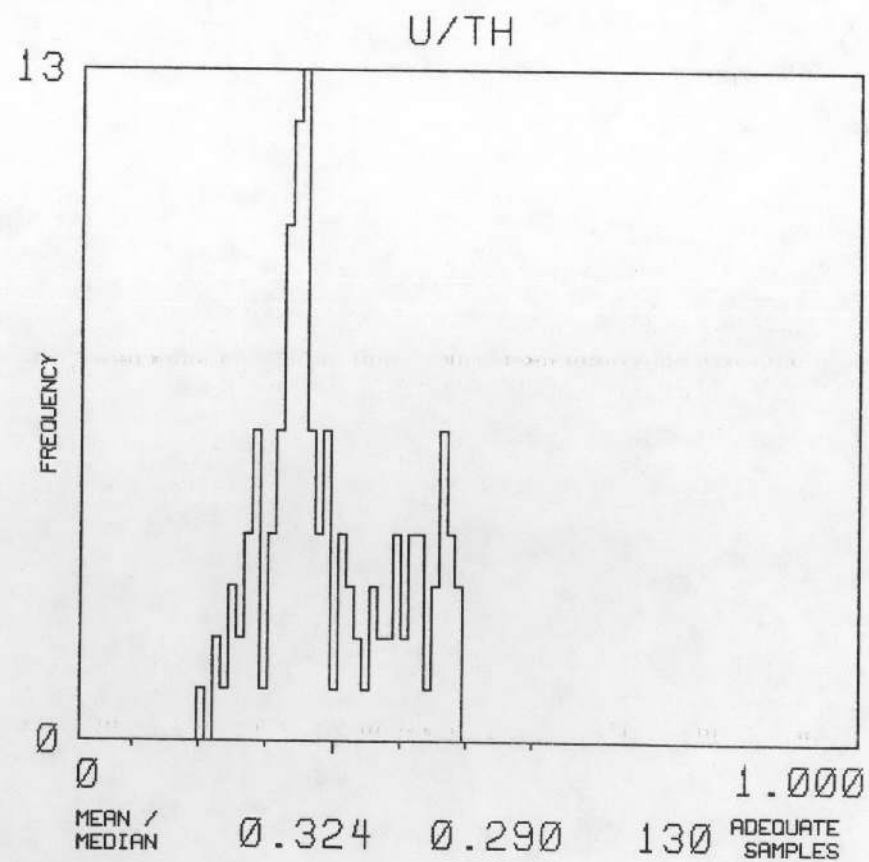
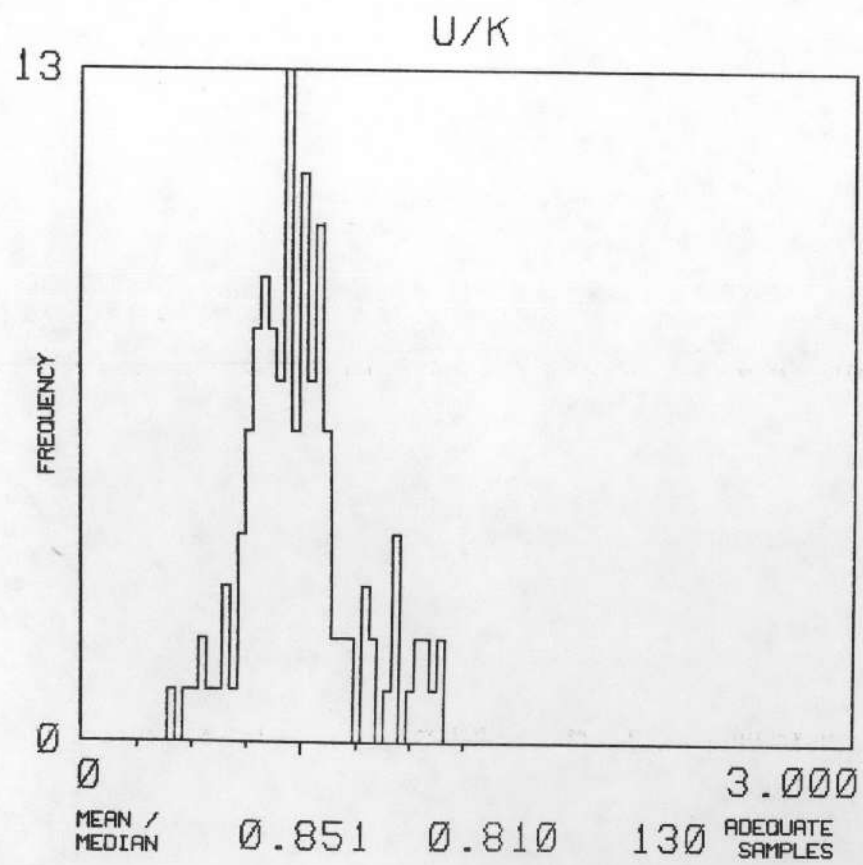
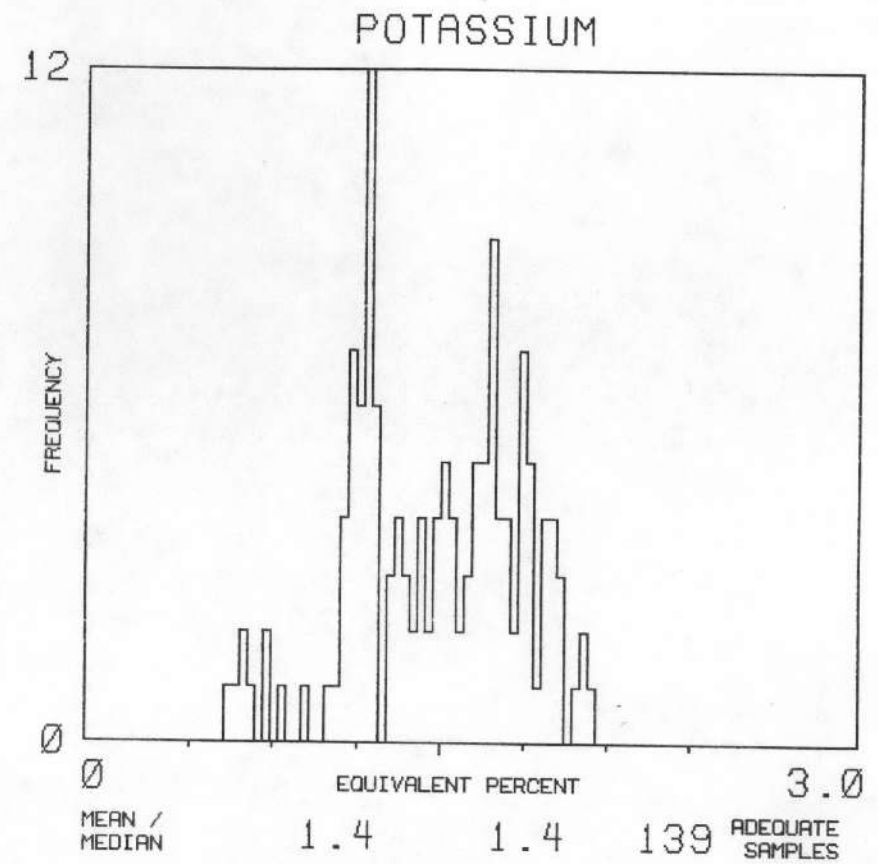
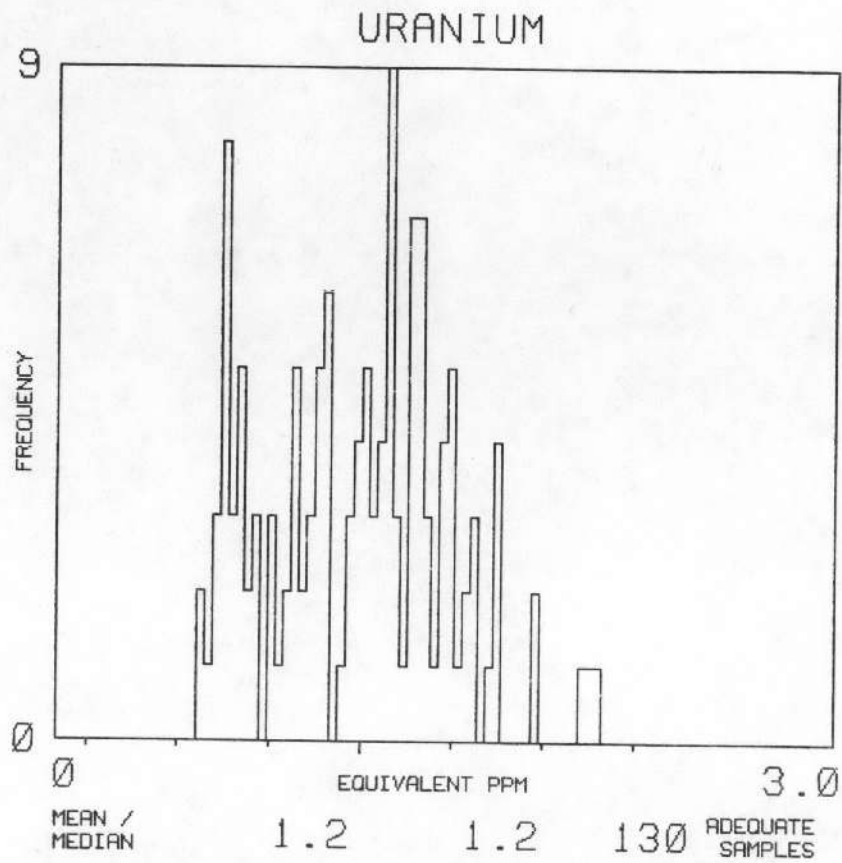
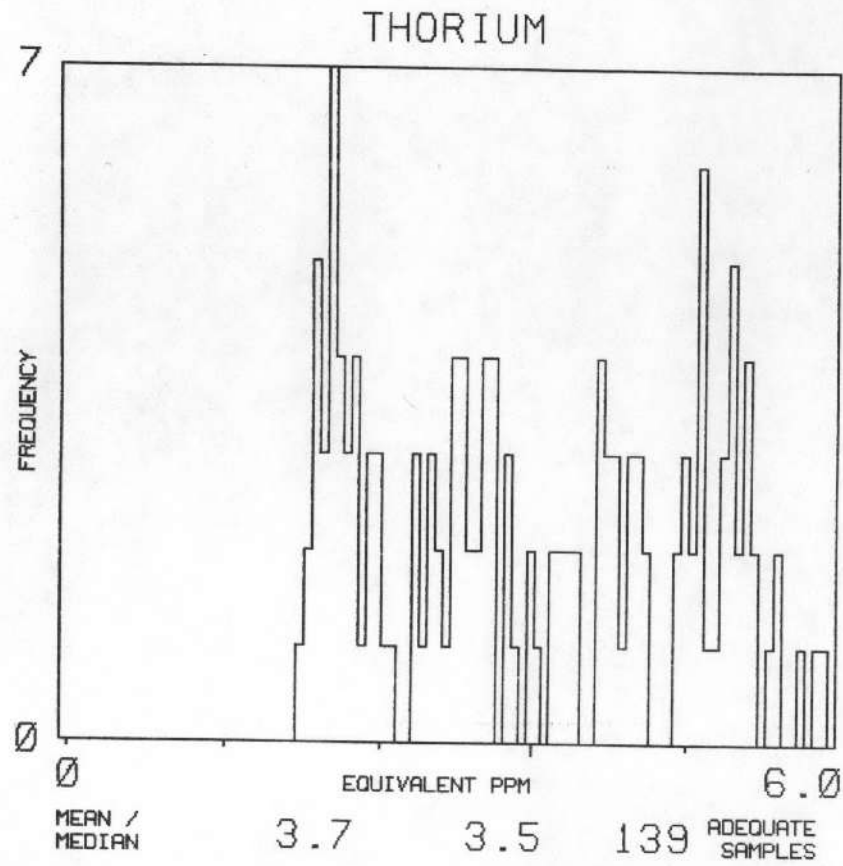
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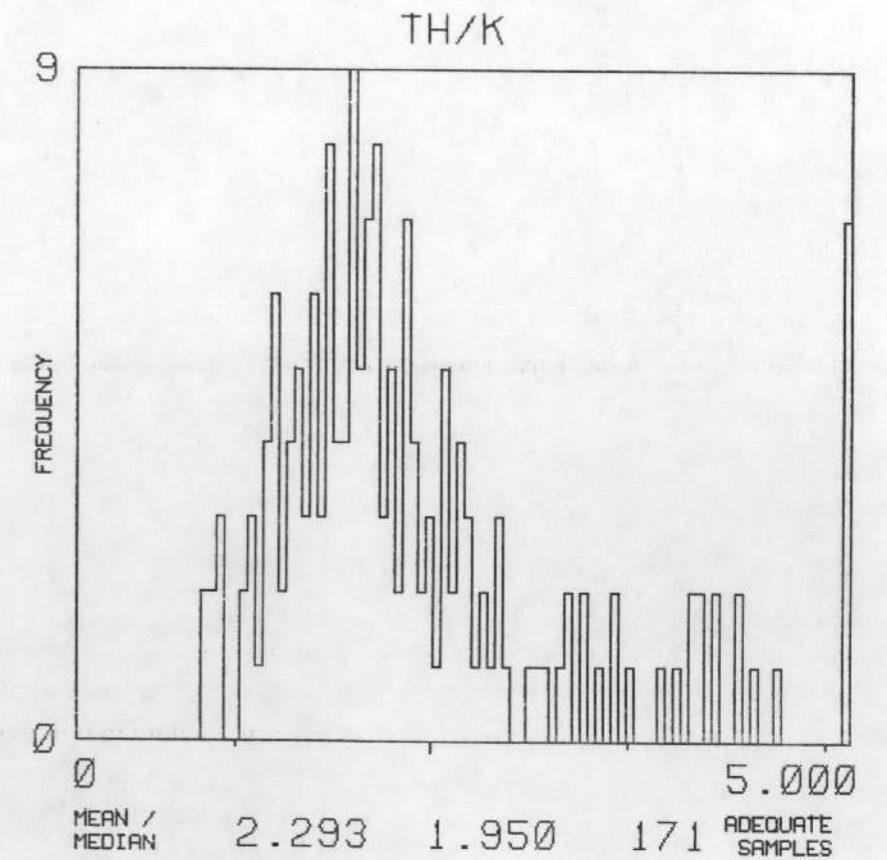
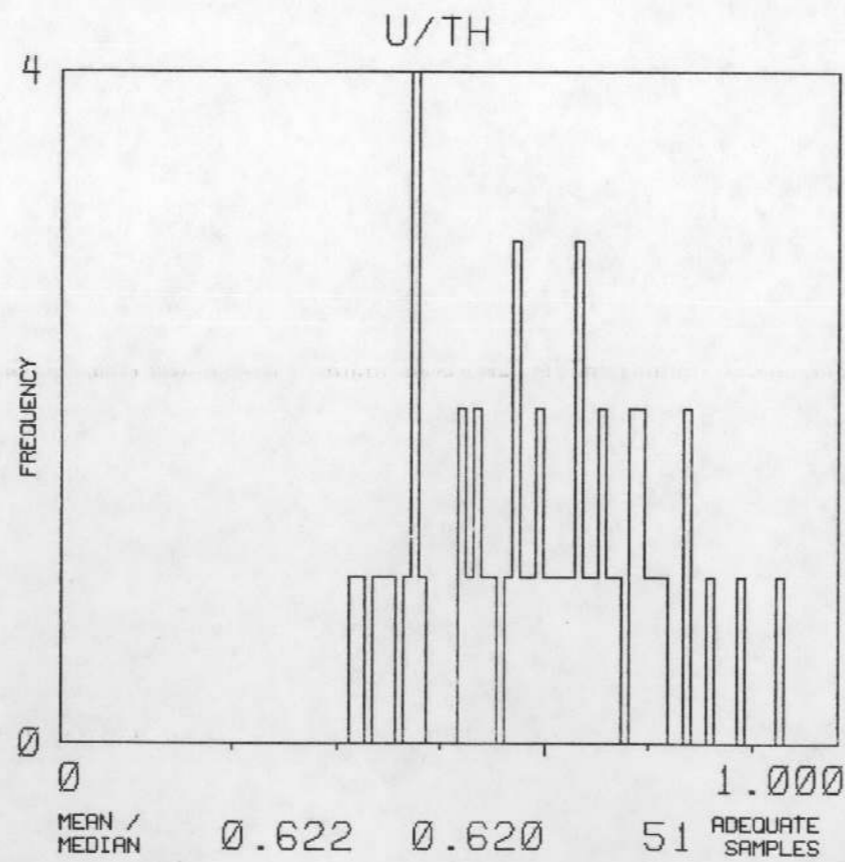
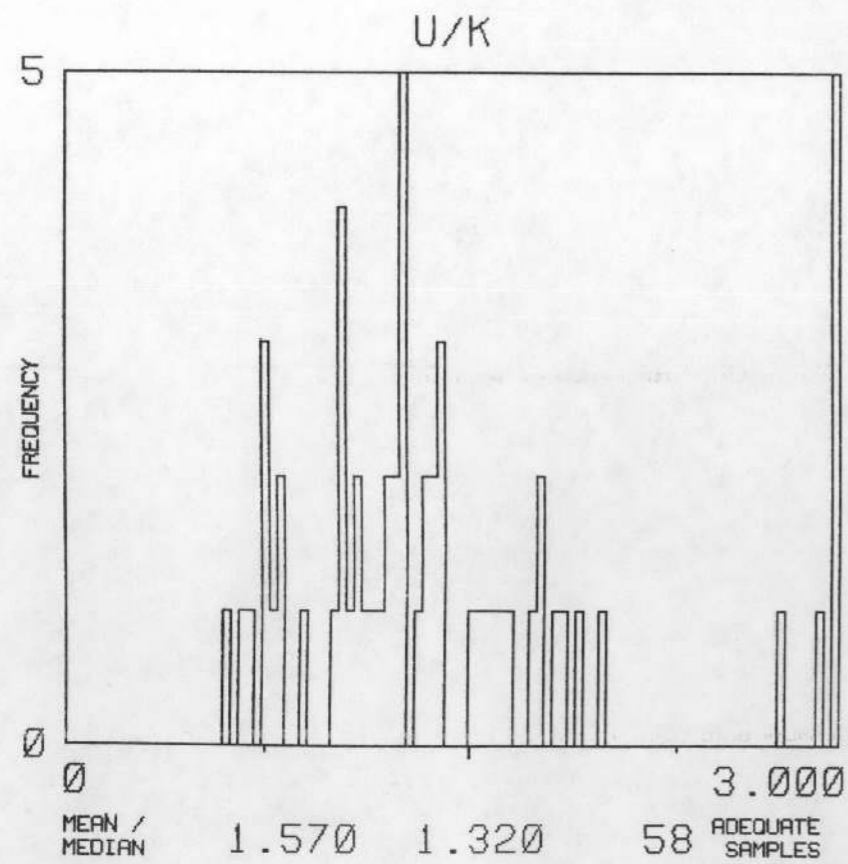
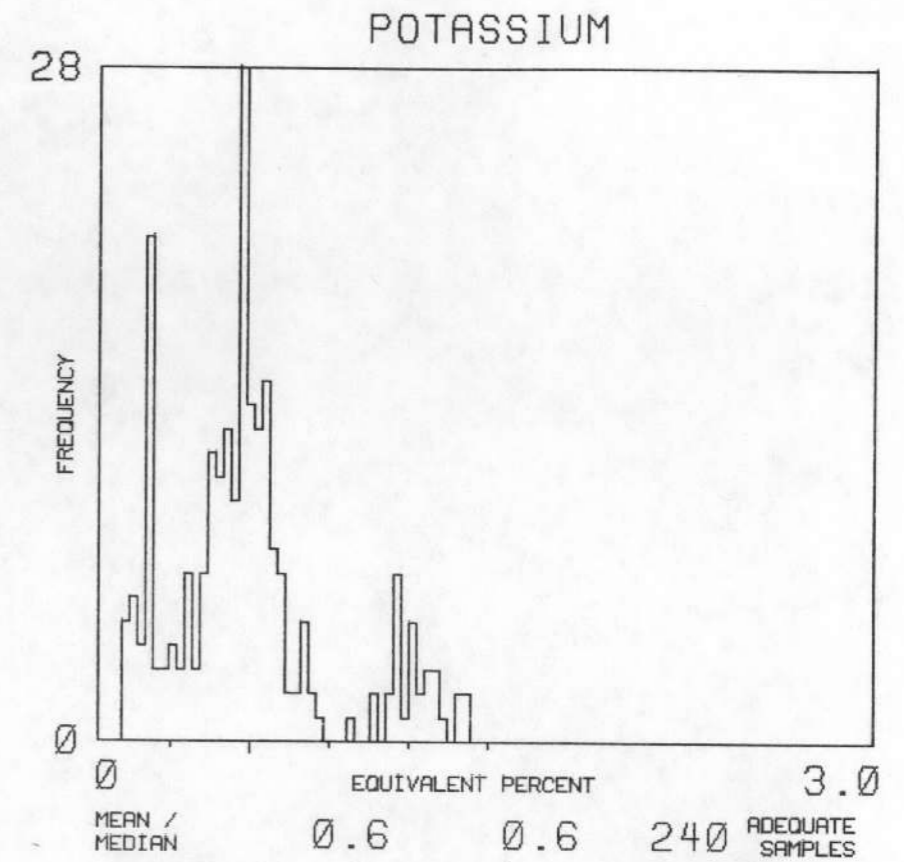
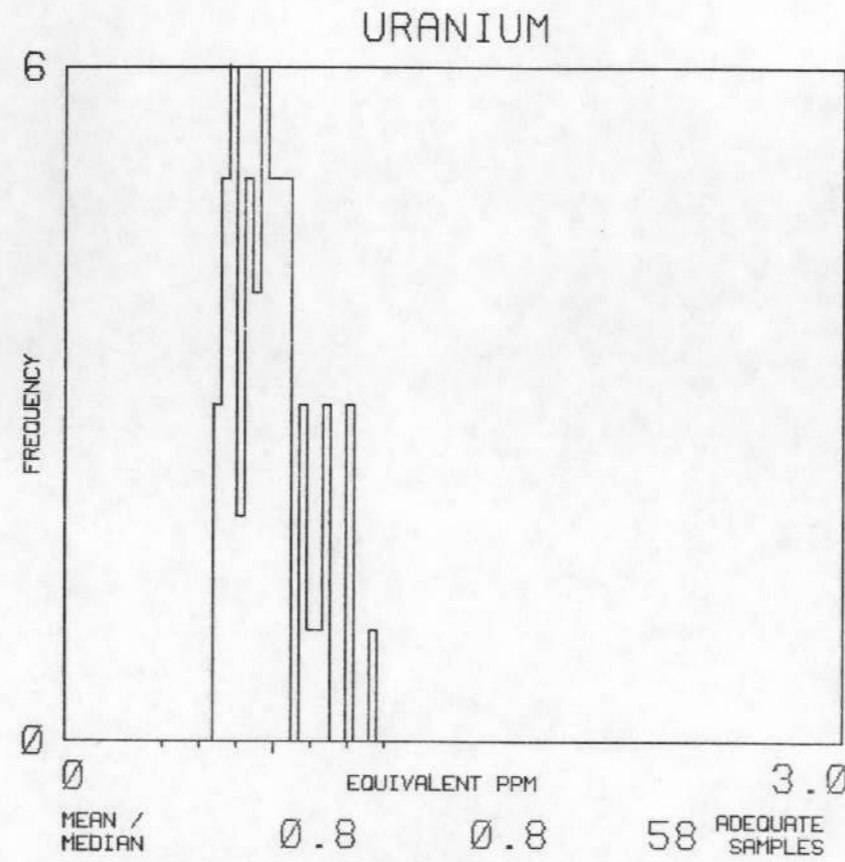
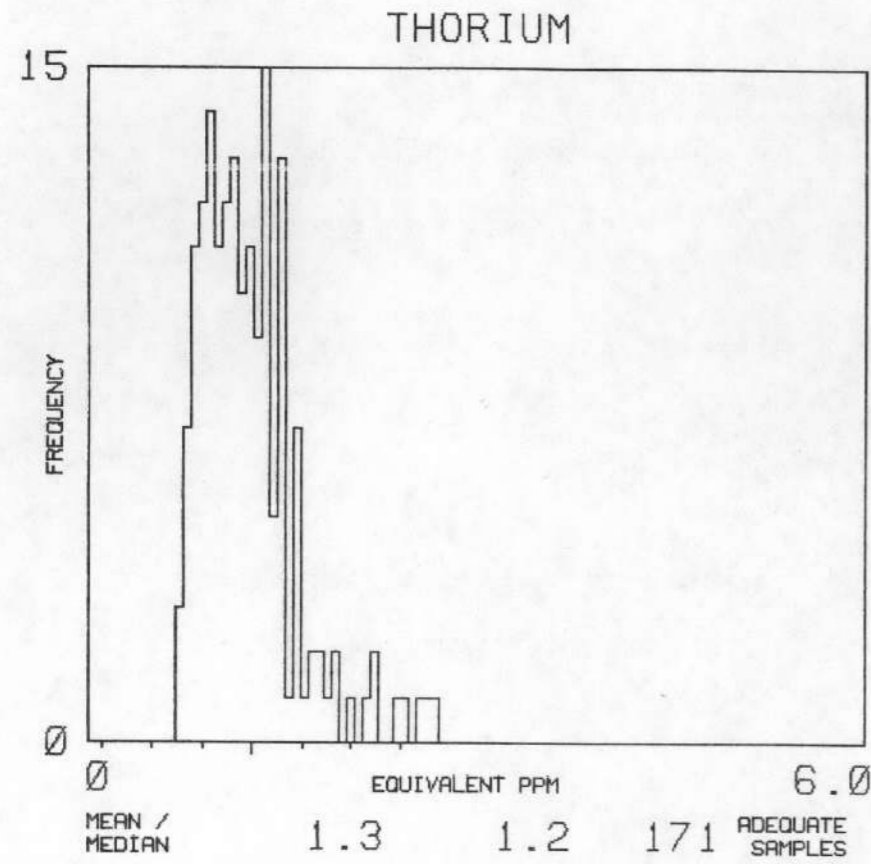
U. S. DEPARTMENT OF ENERGY

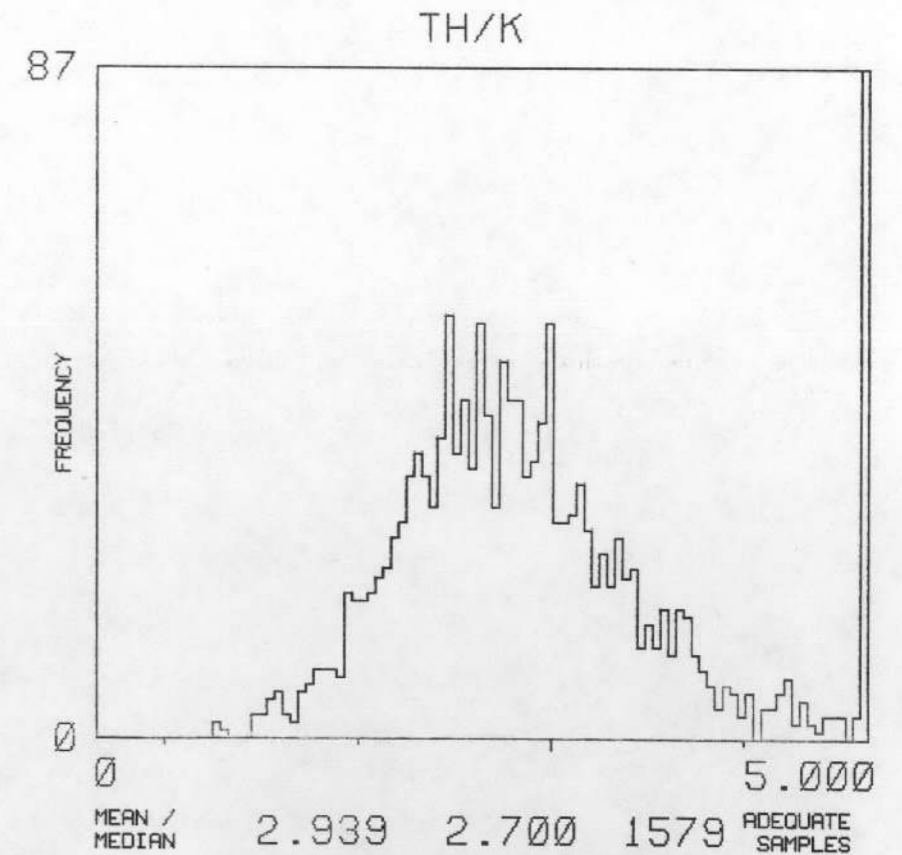
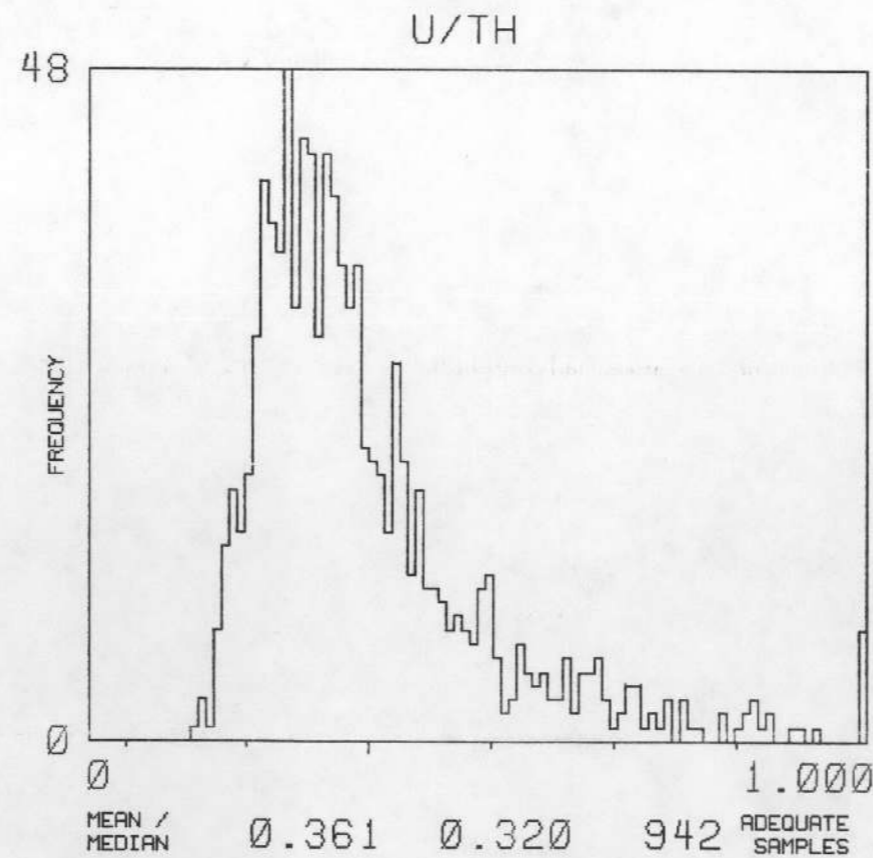
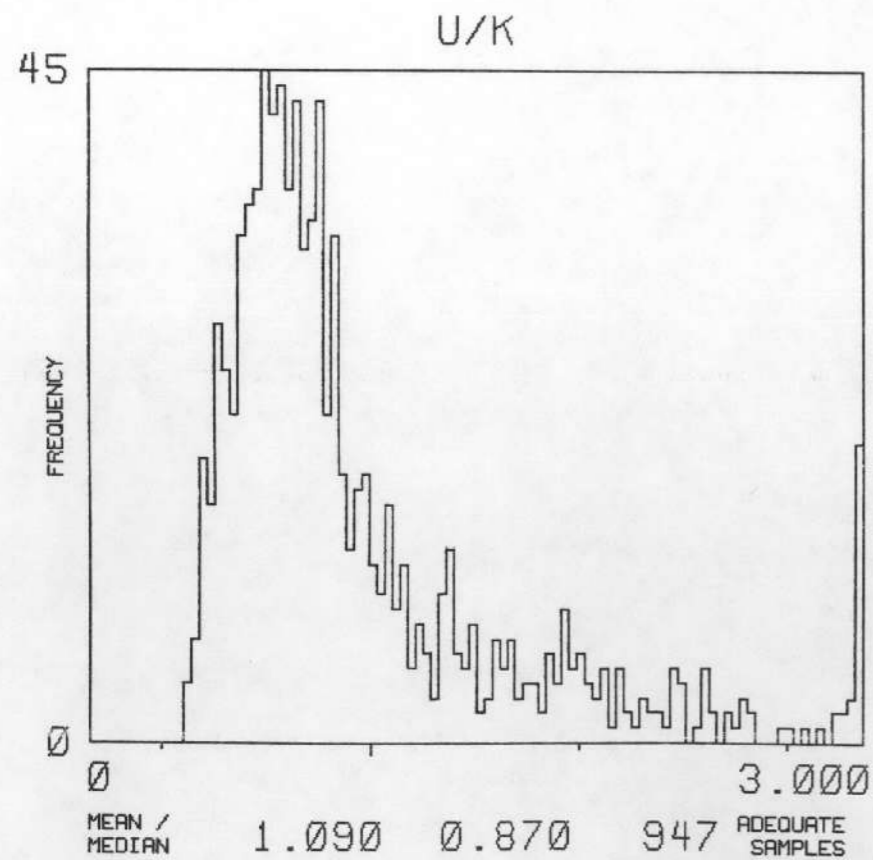
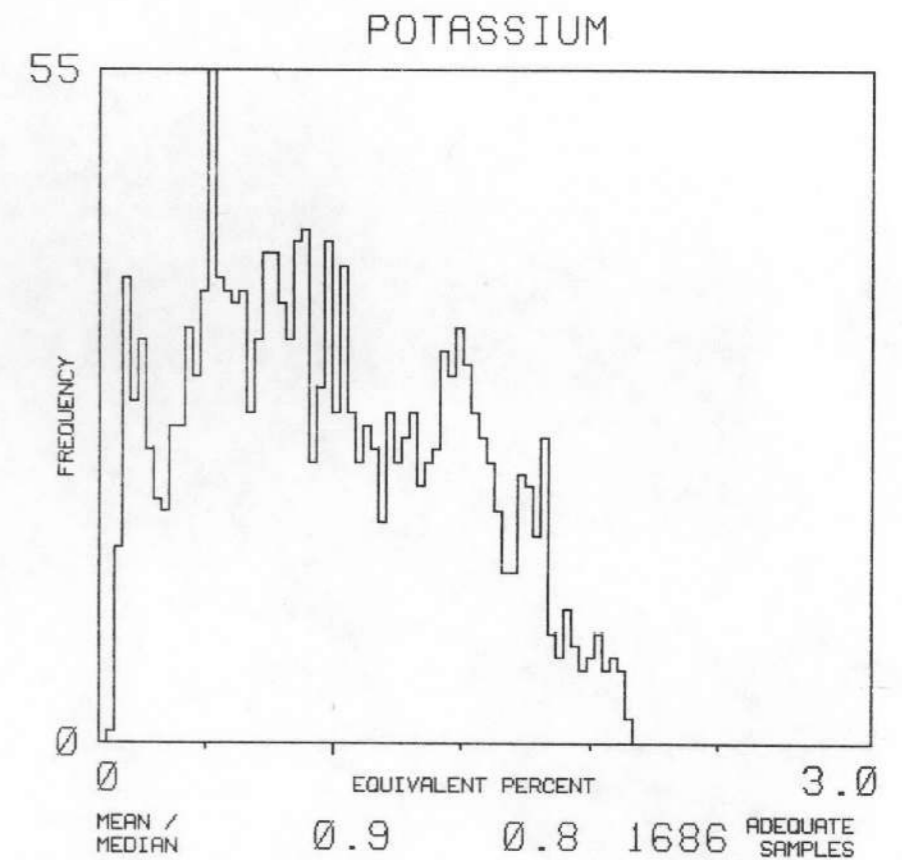
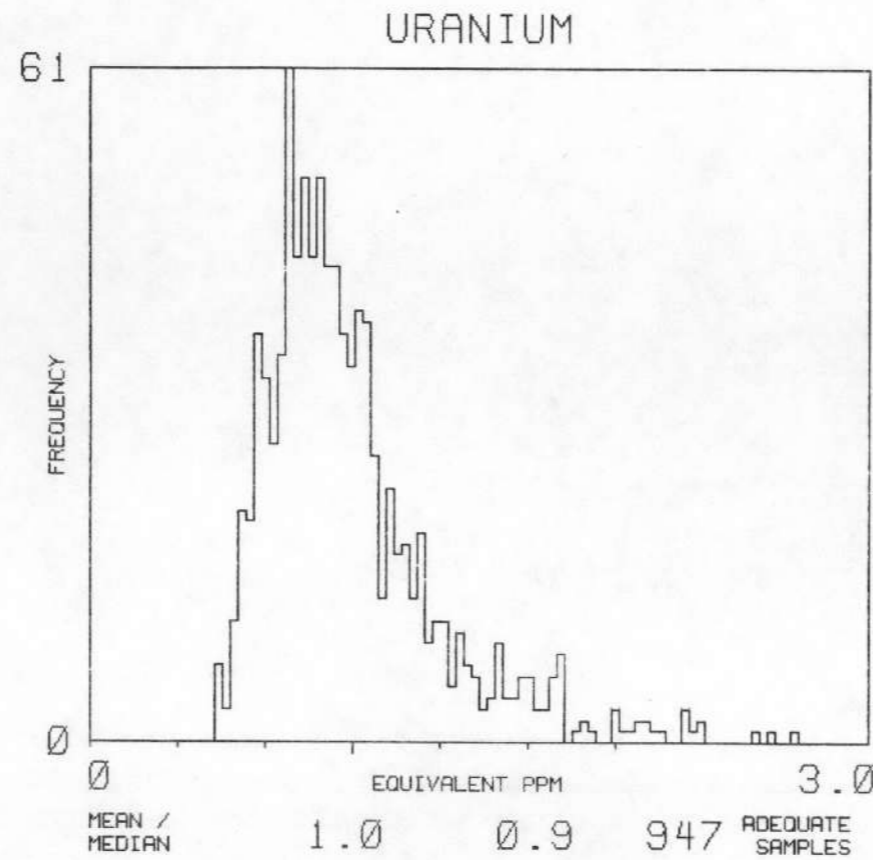
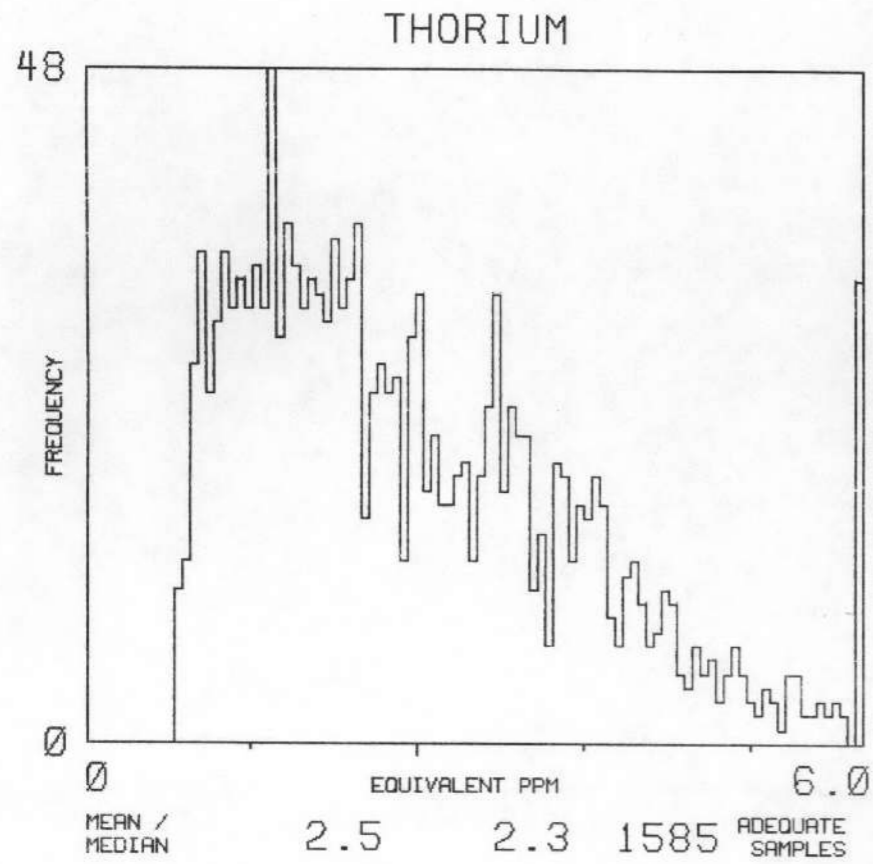
SURVEY AND
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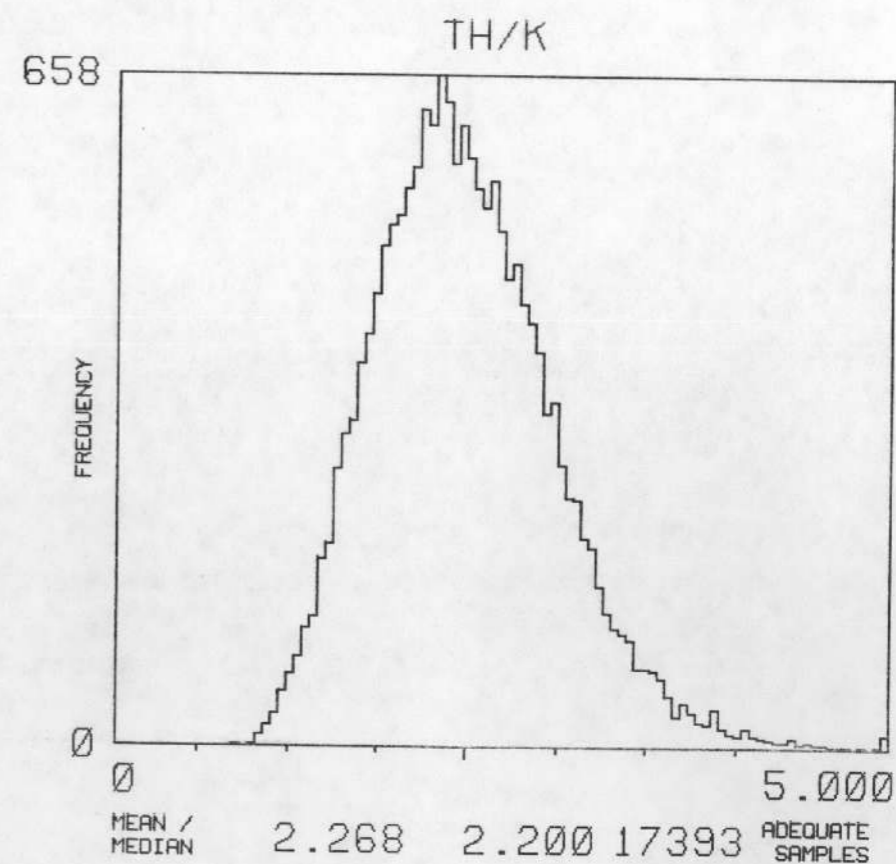
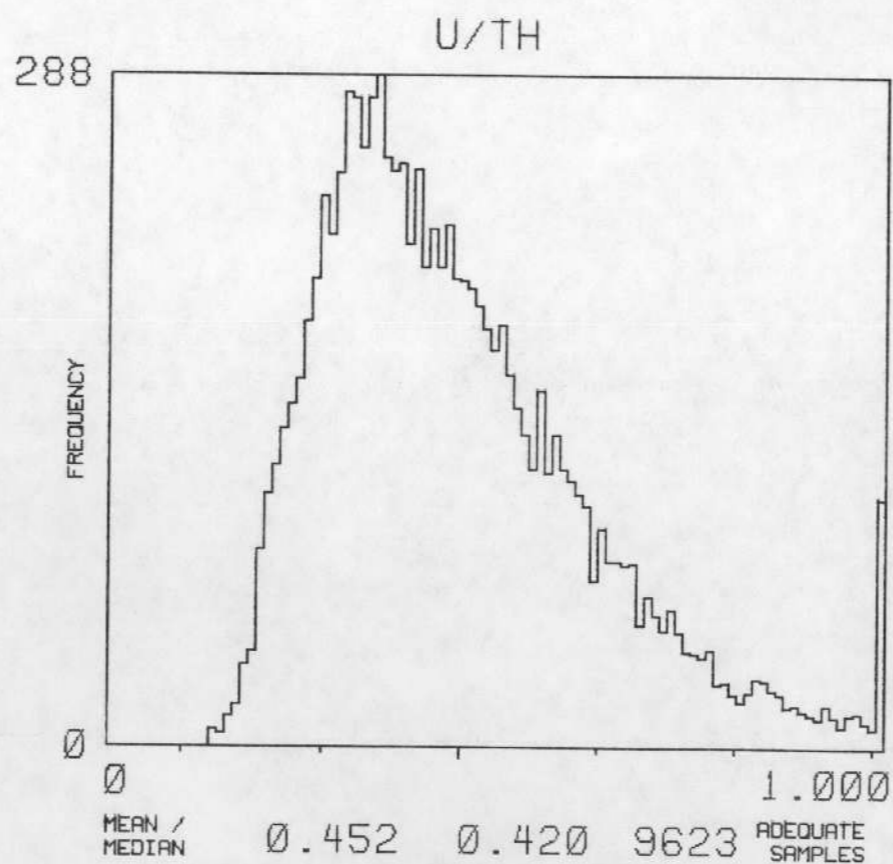
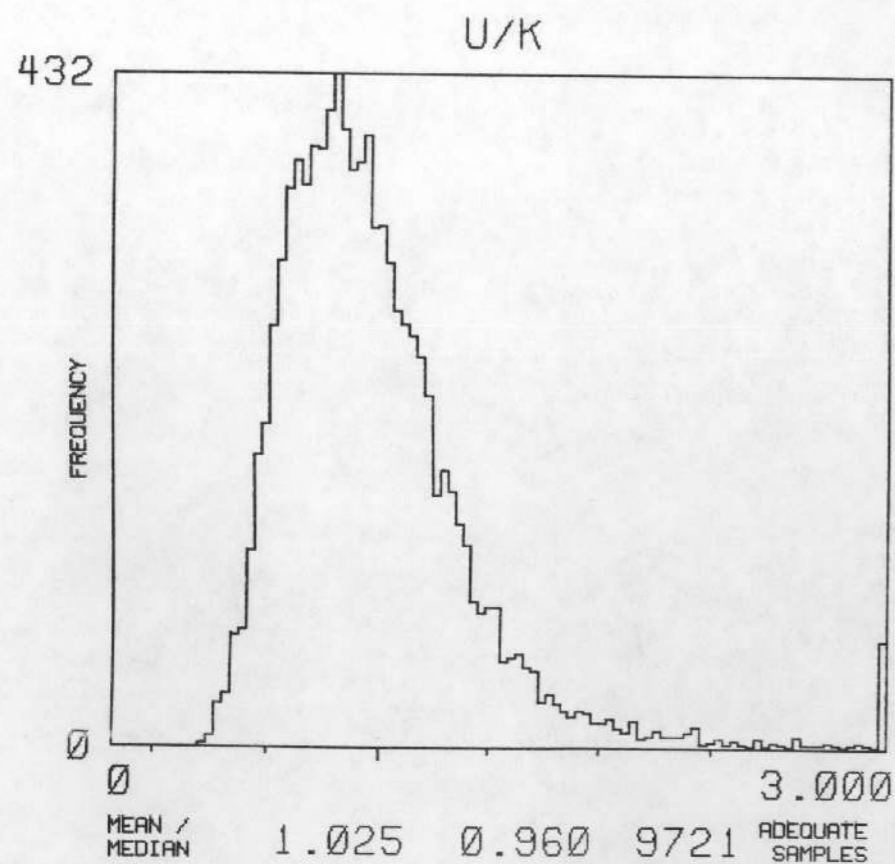
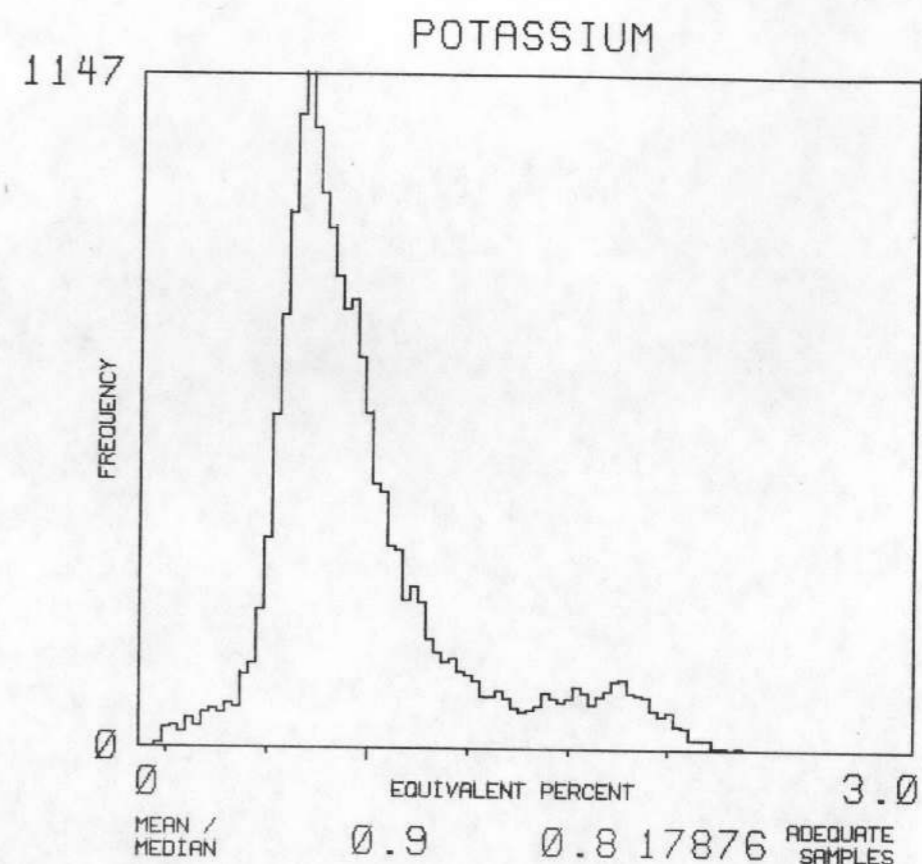
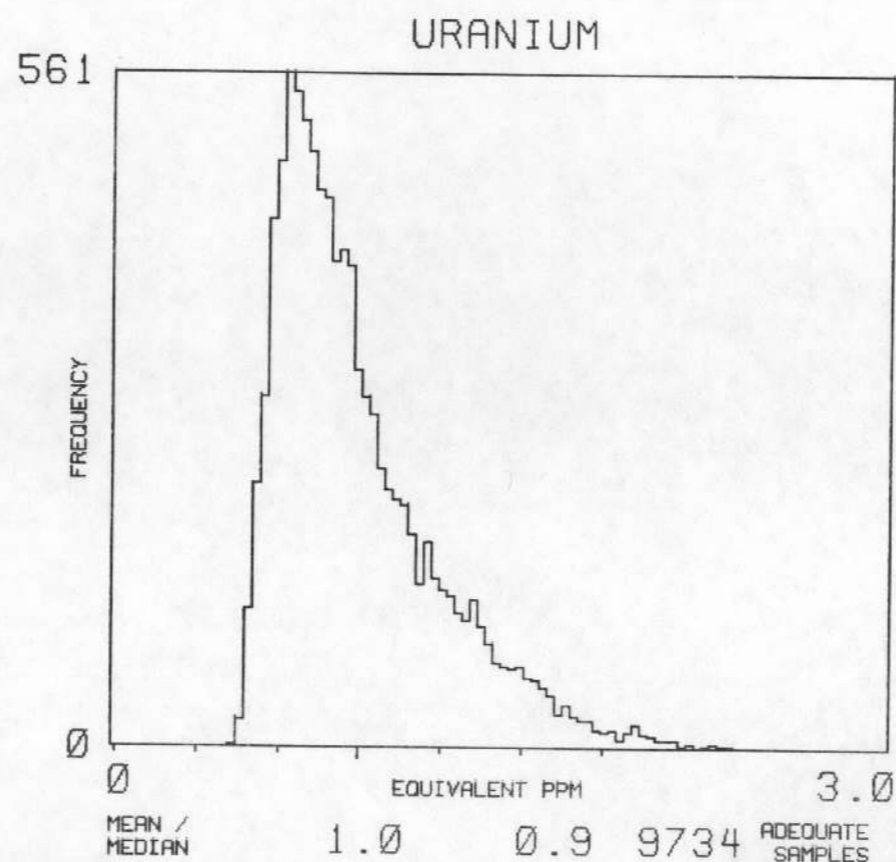
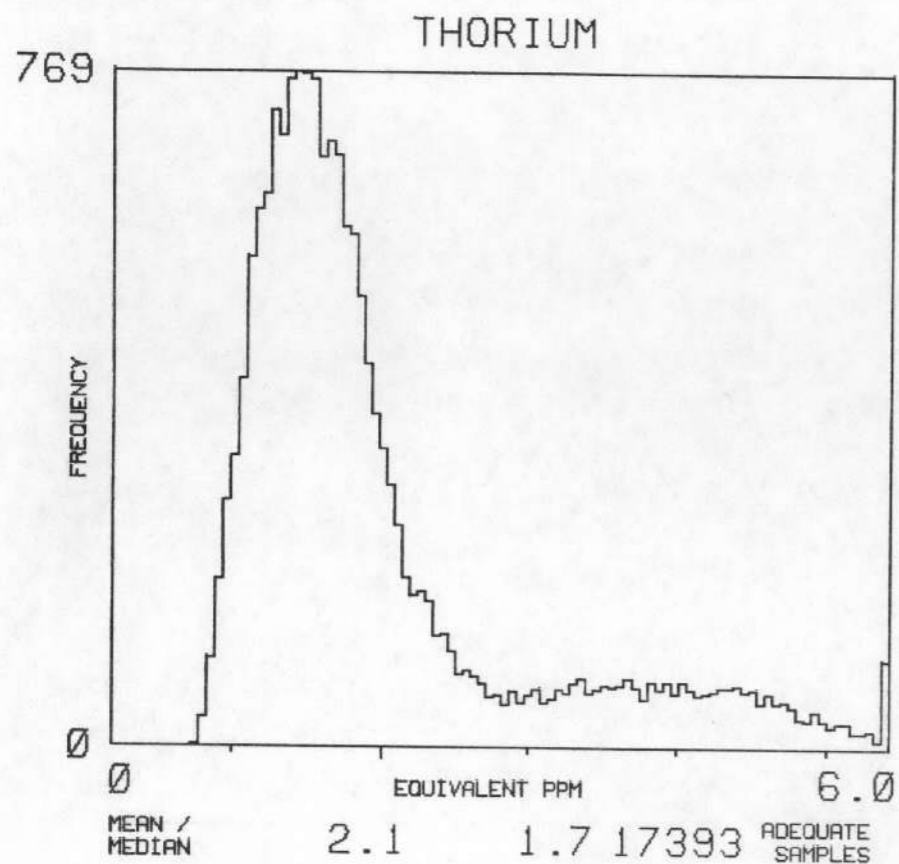
EG&G GEOMETRICS

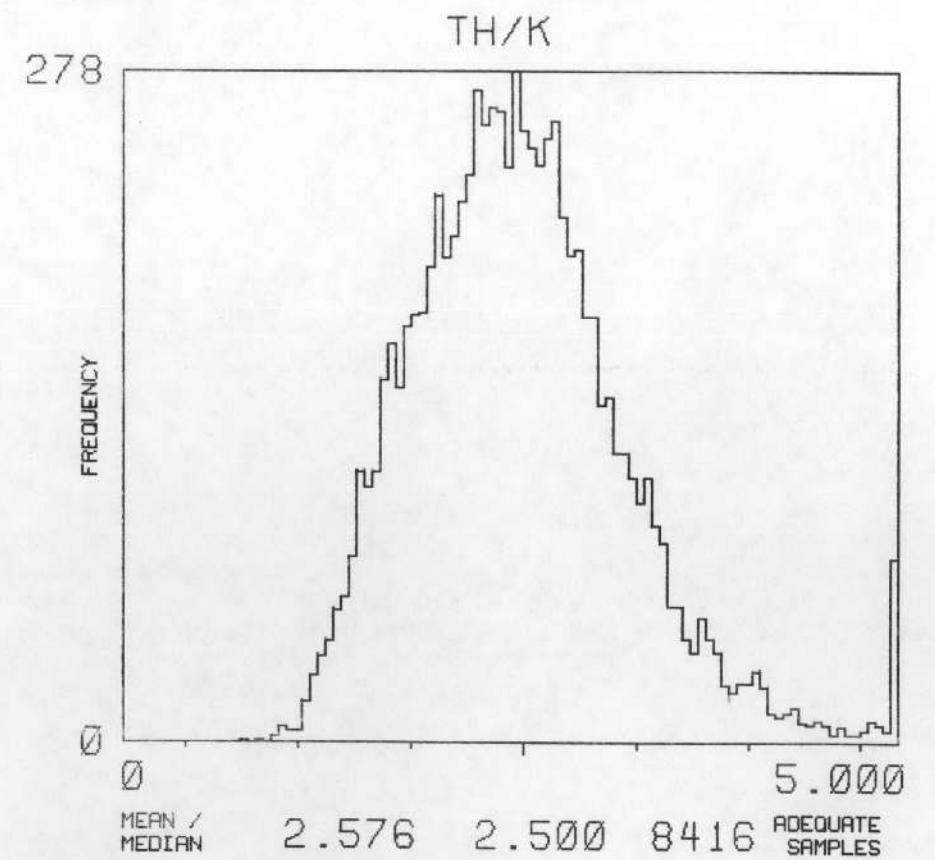
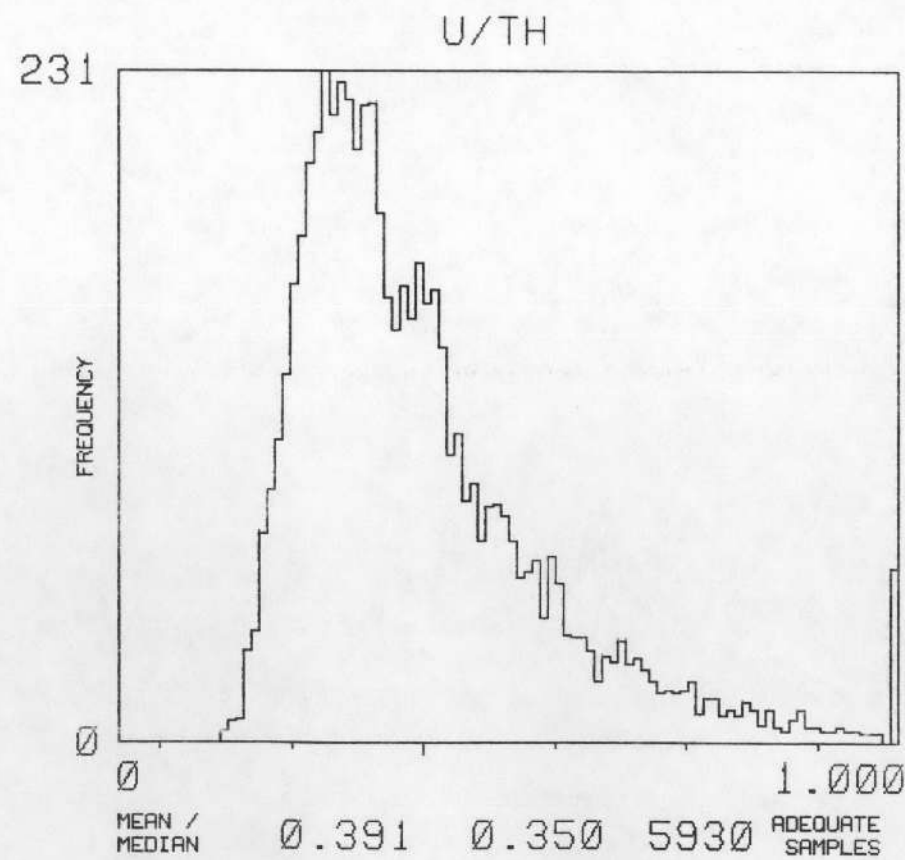
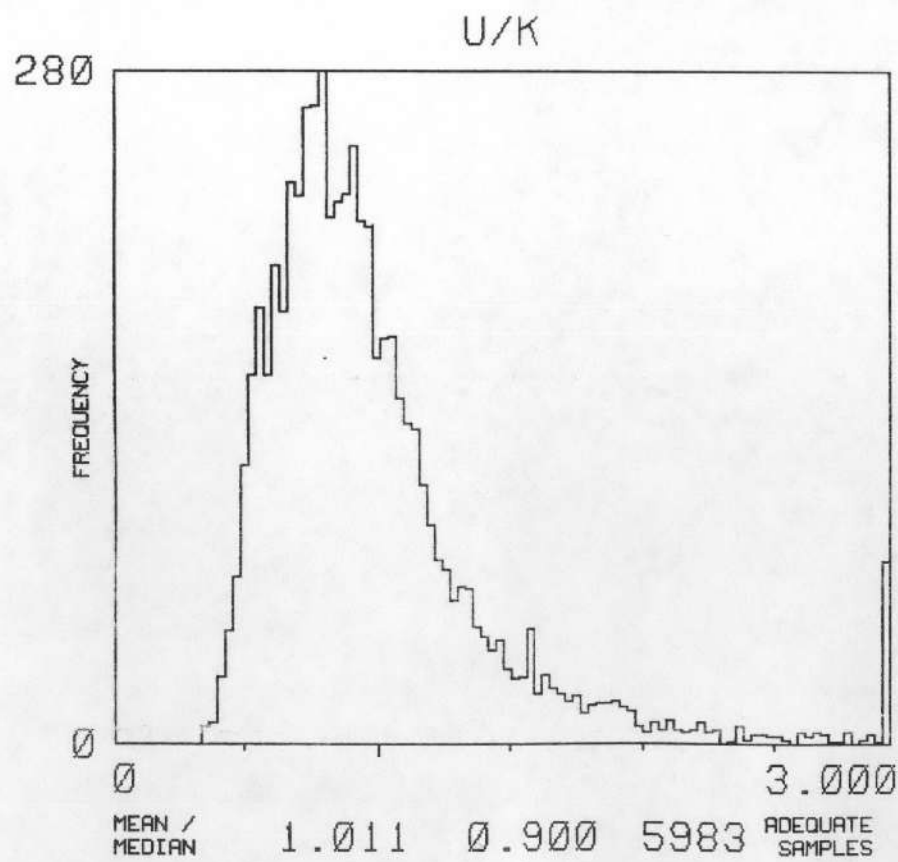
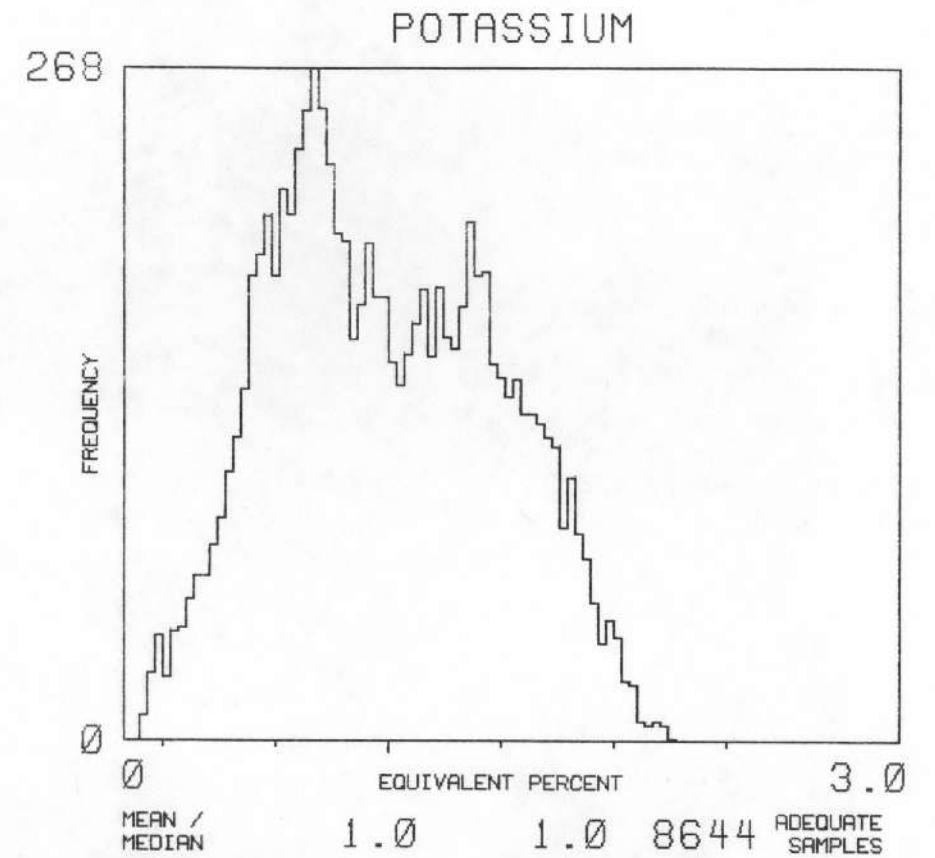
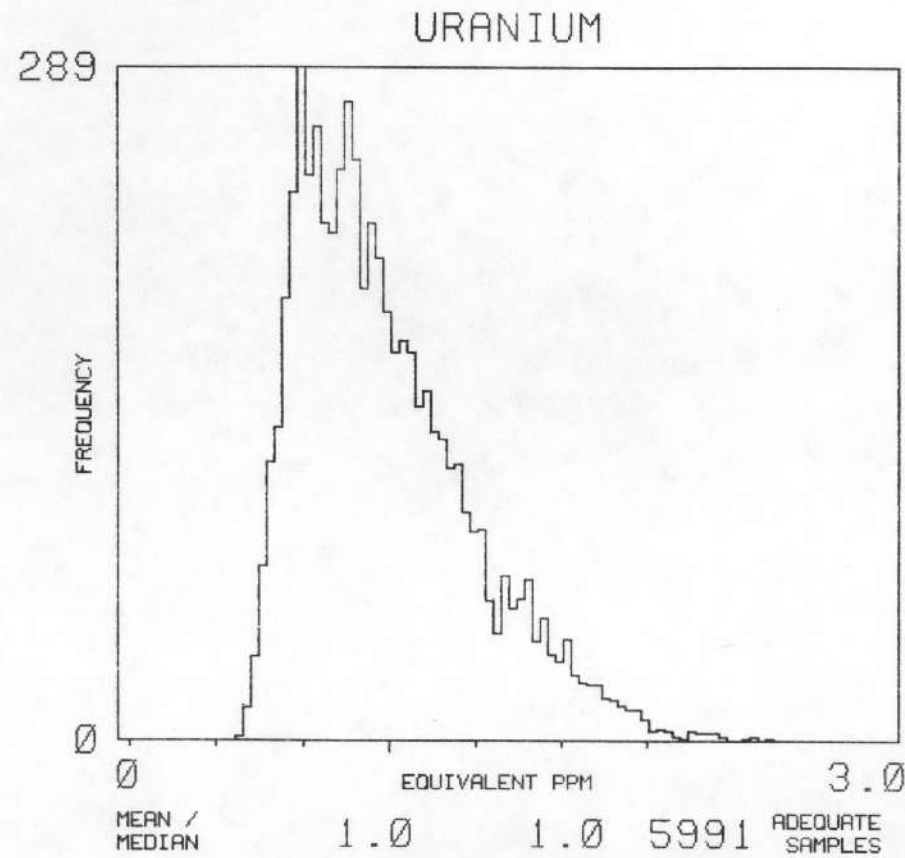
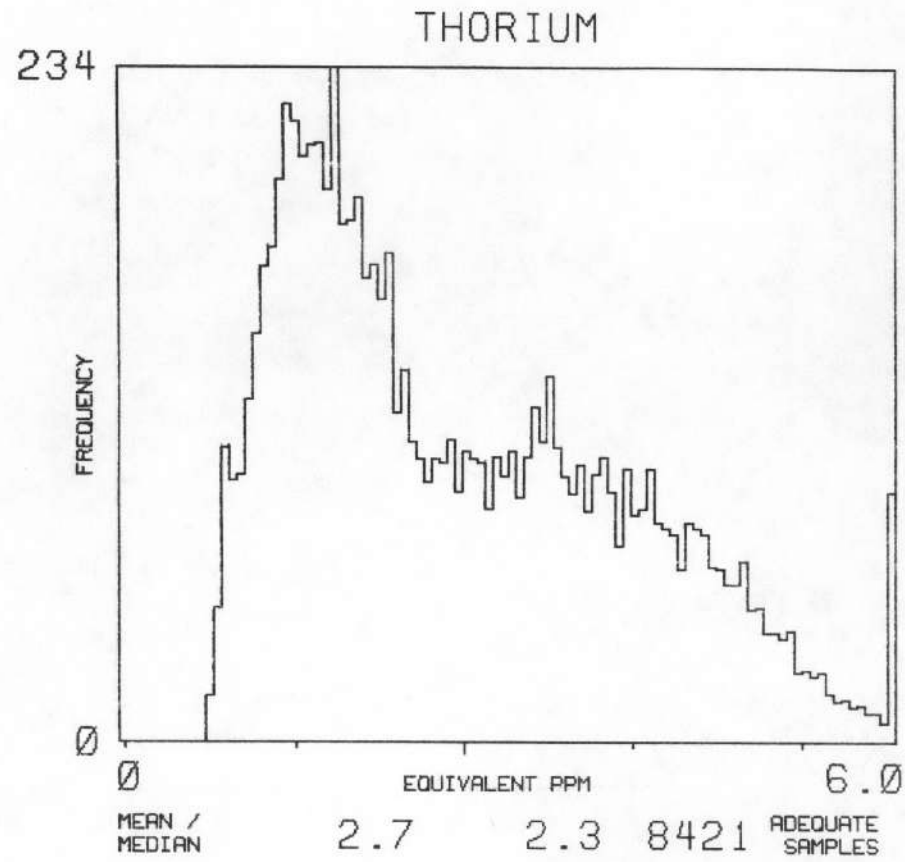
**APPENDIX F - Histograms and Map Unit Conversion
Table**

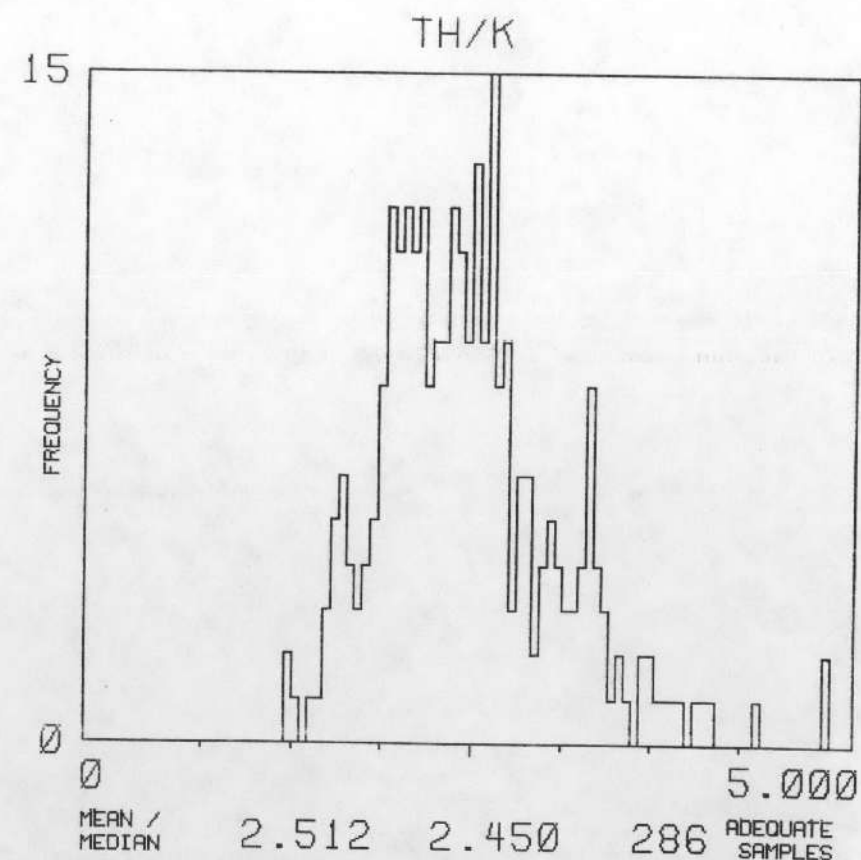
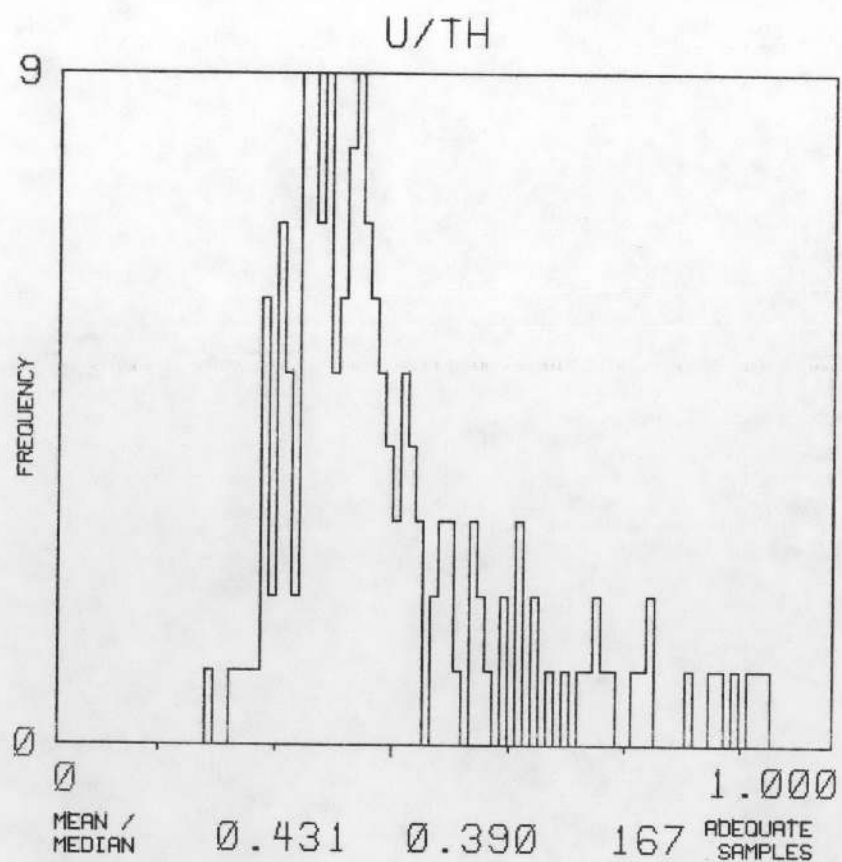
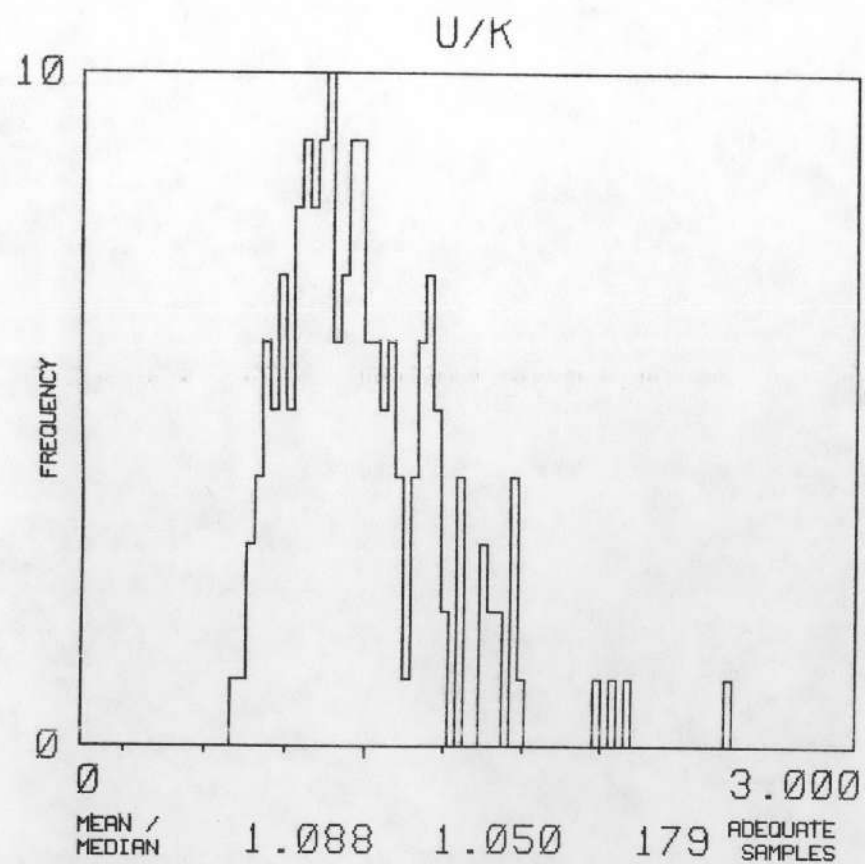
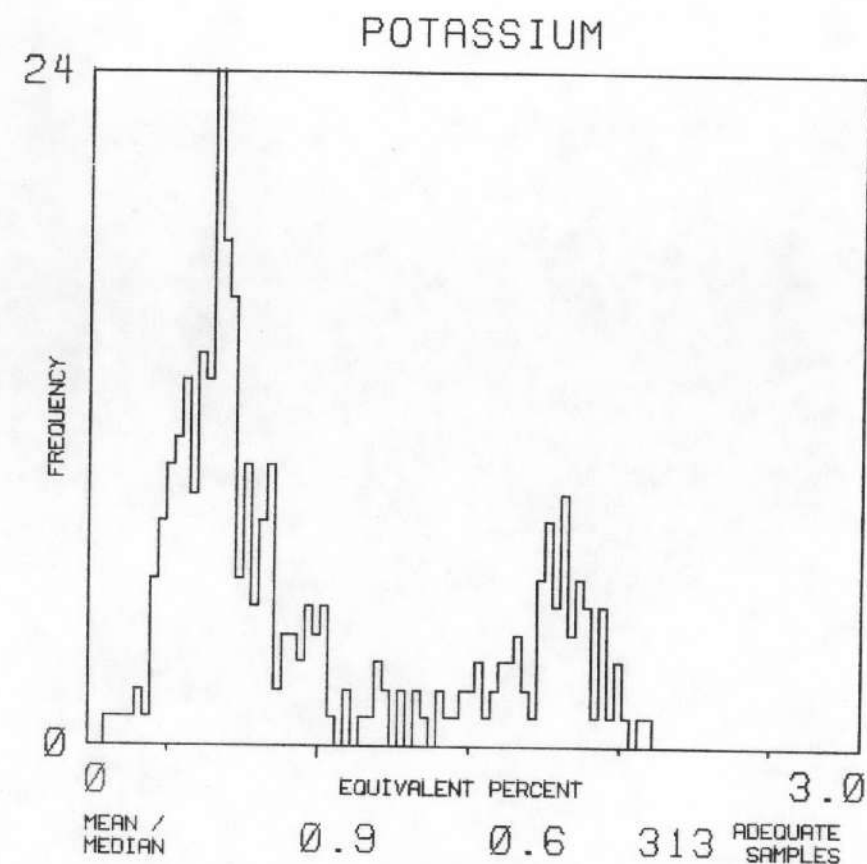
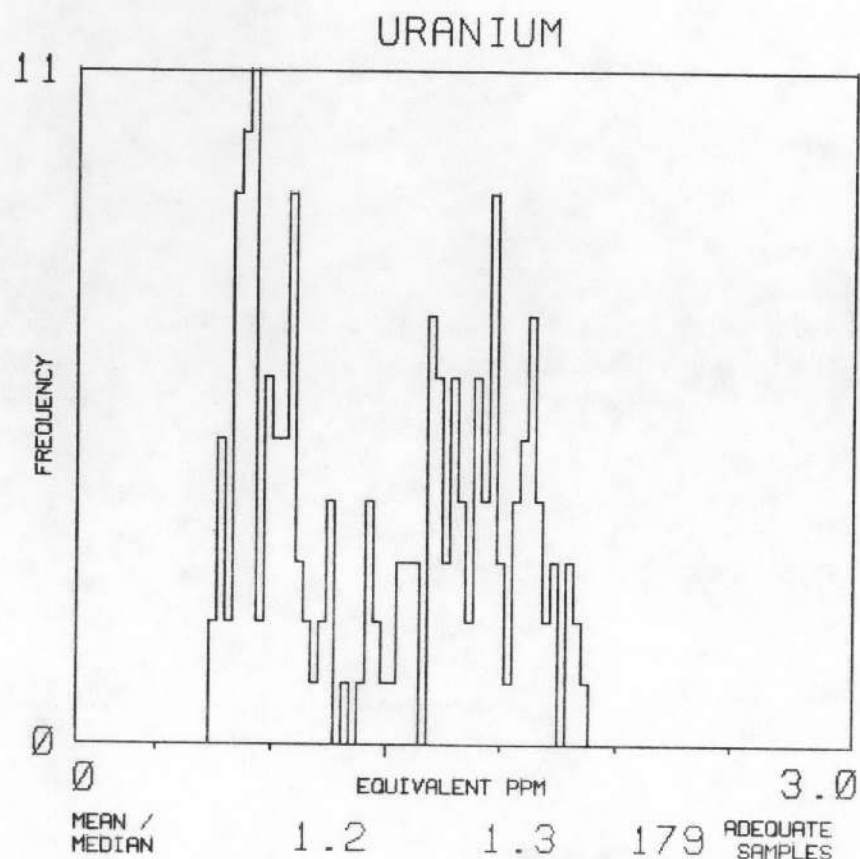
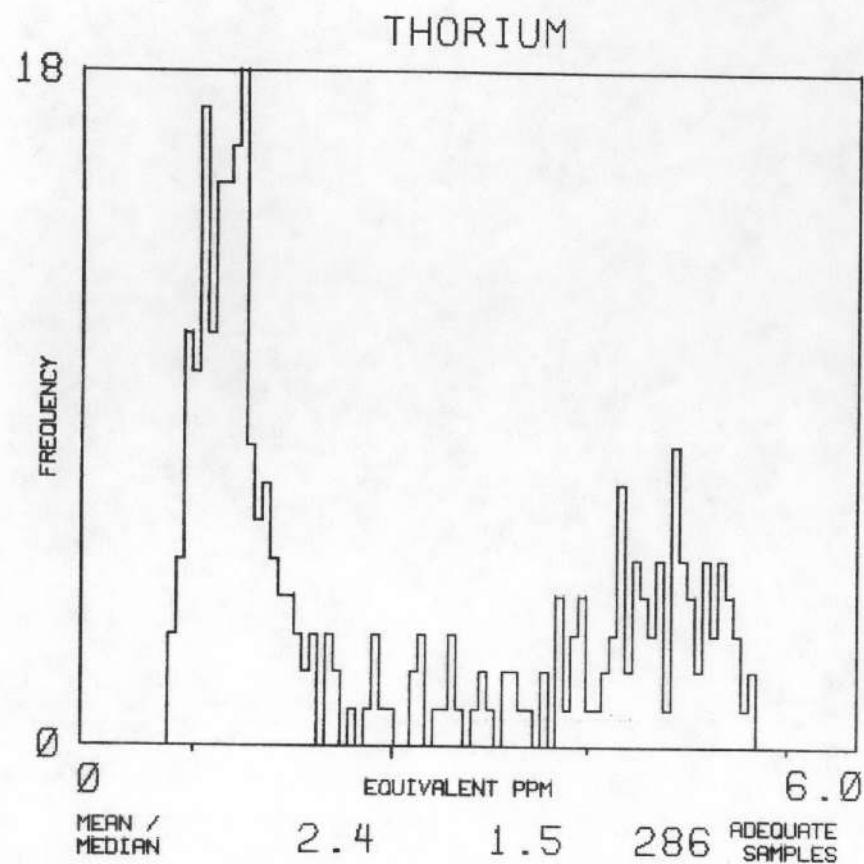


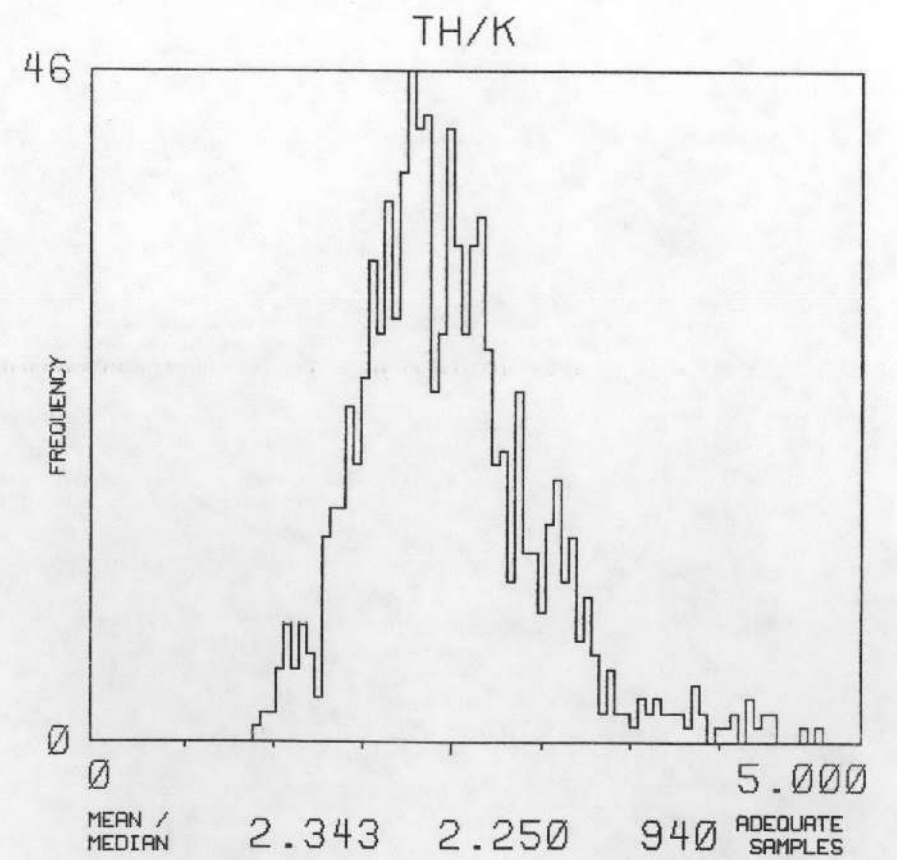
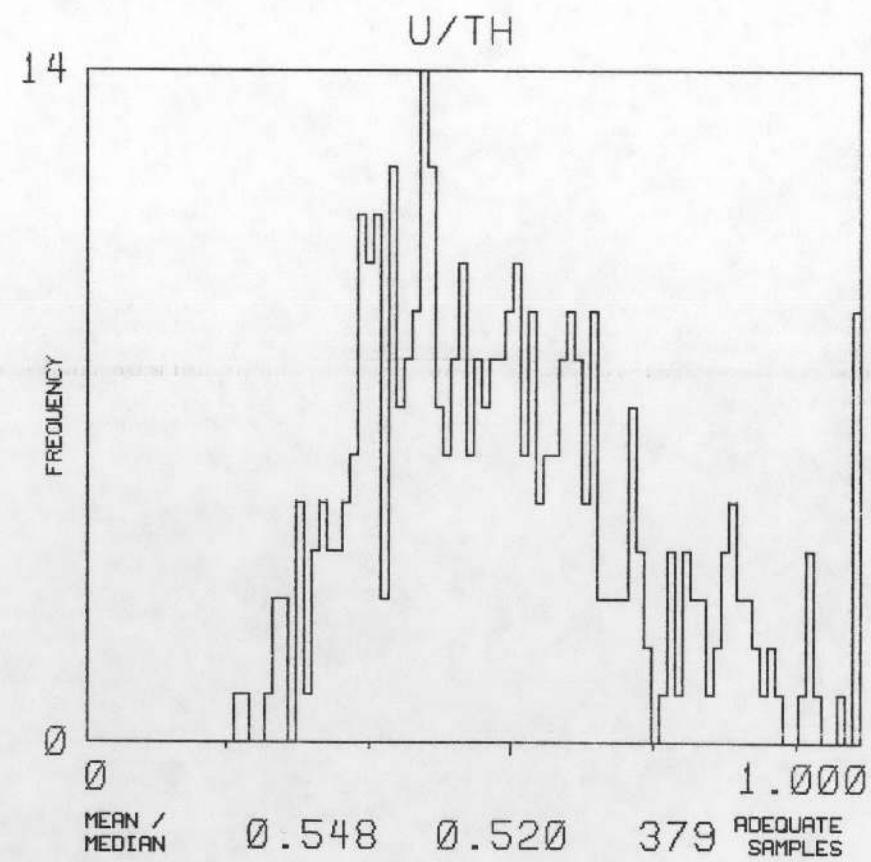
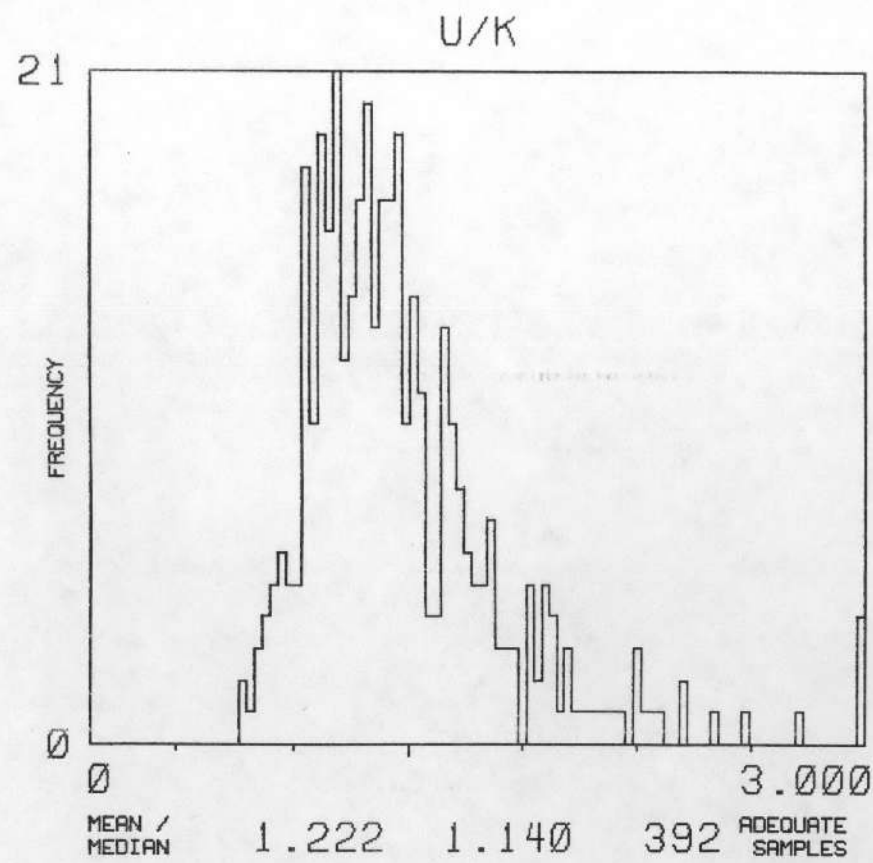
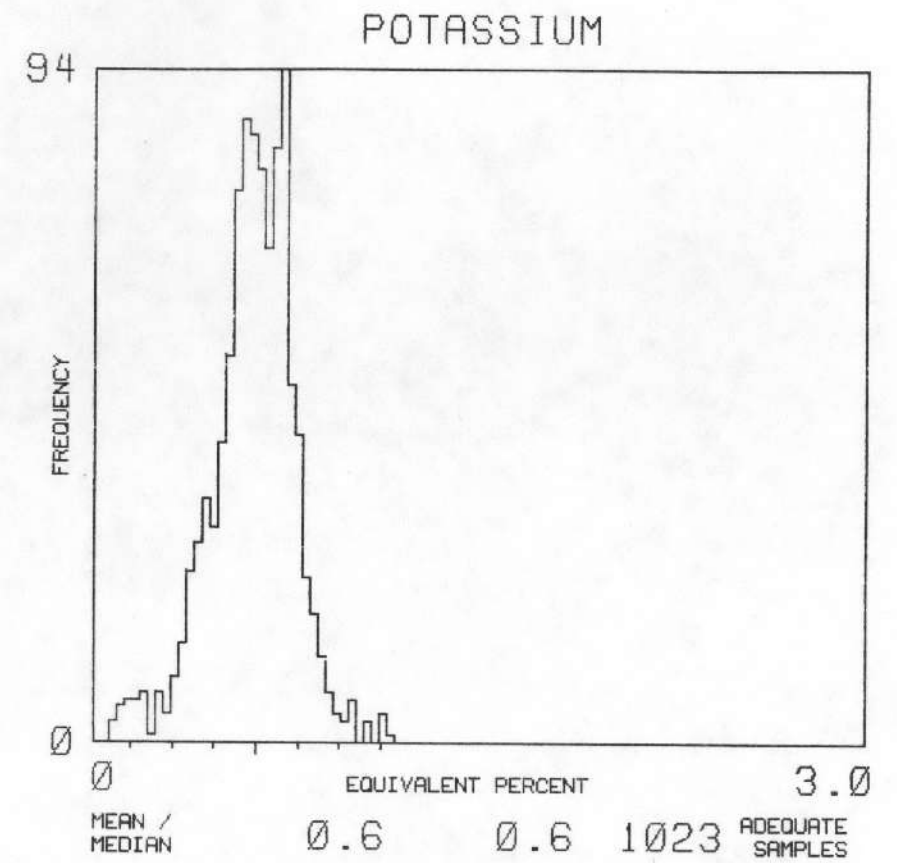
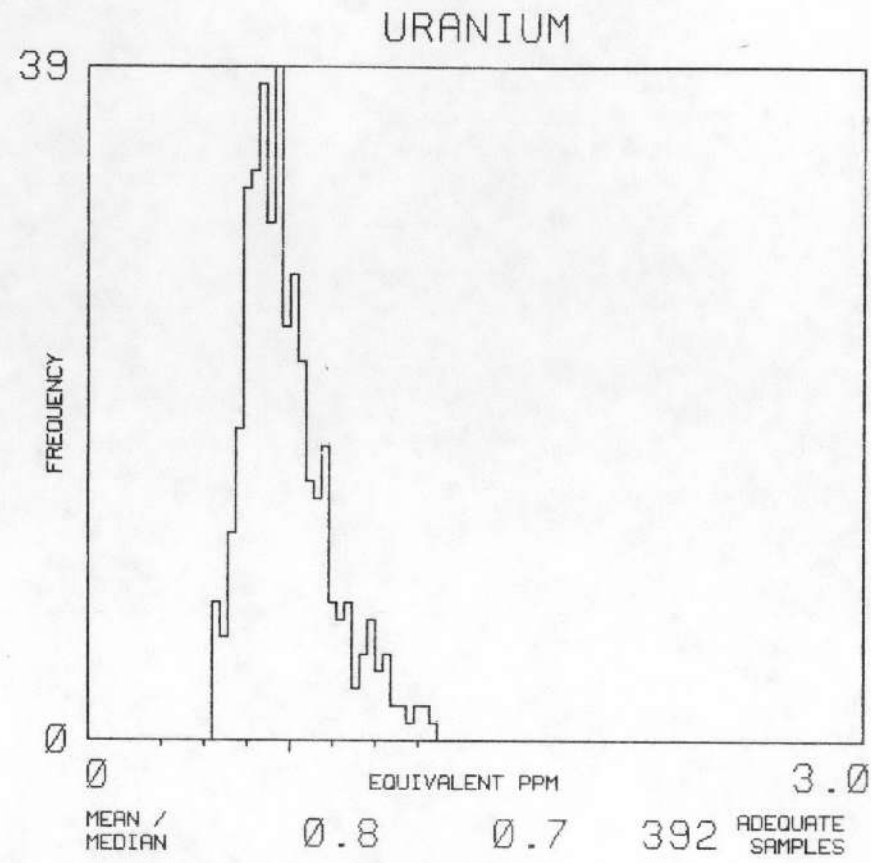
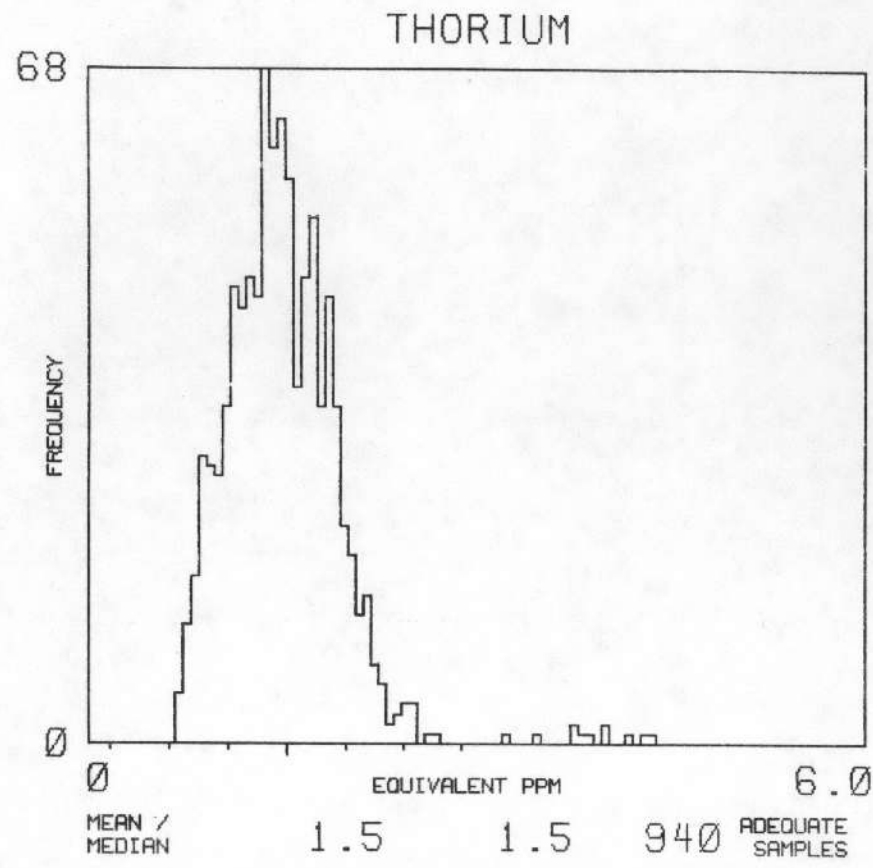


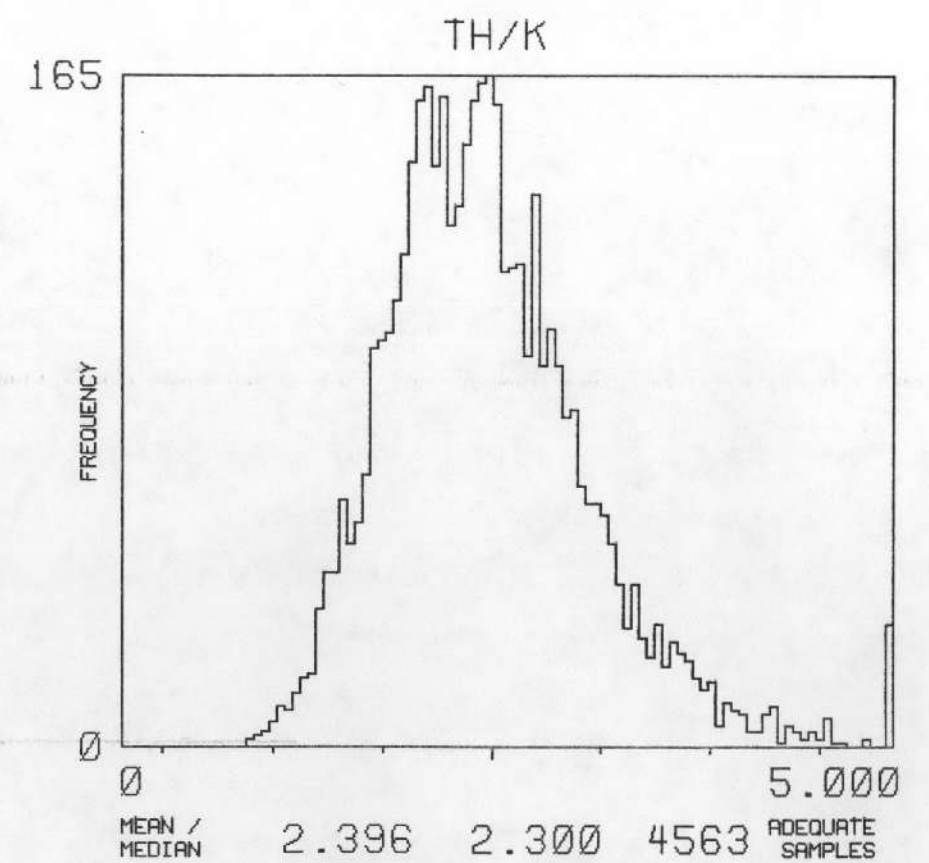
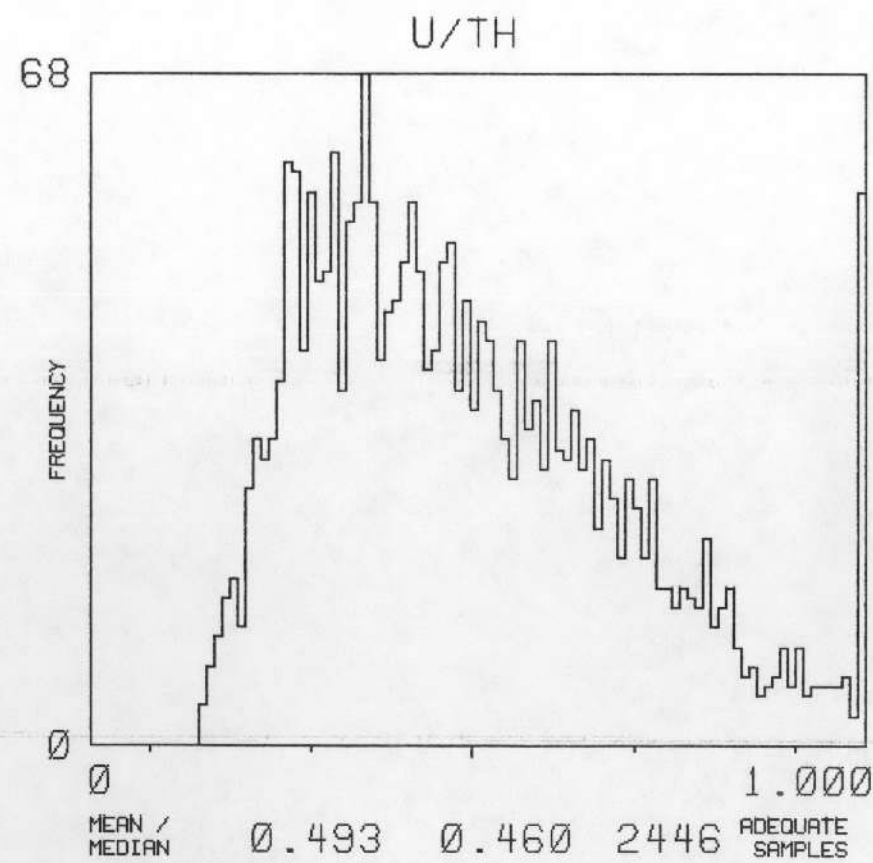
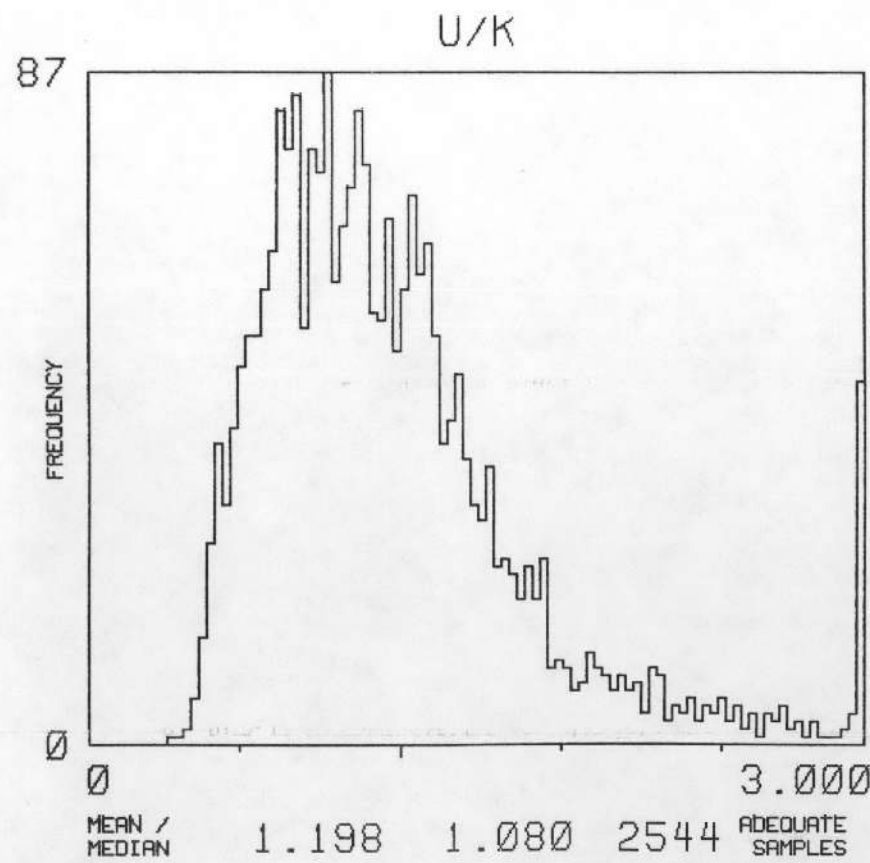
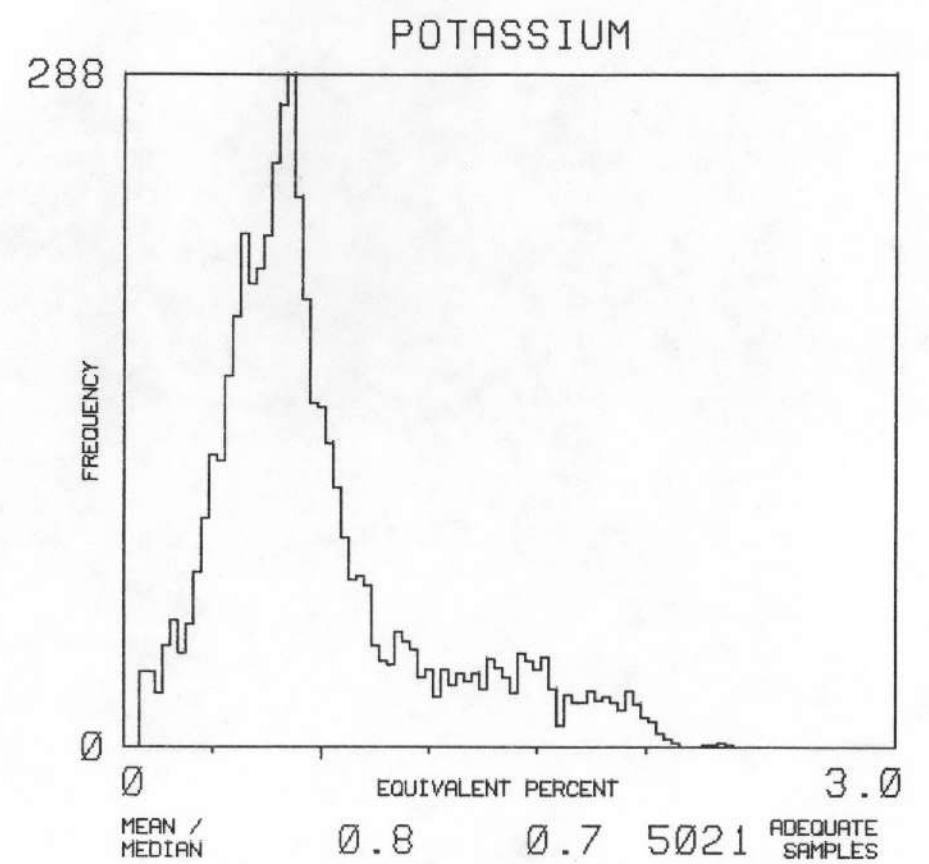
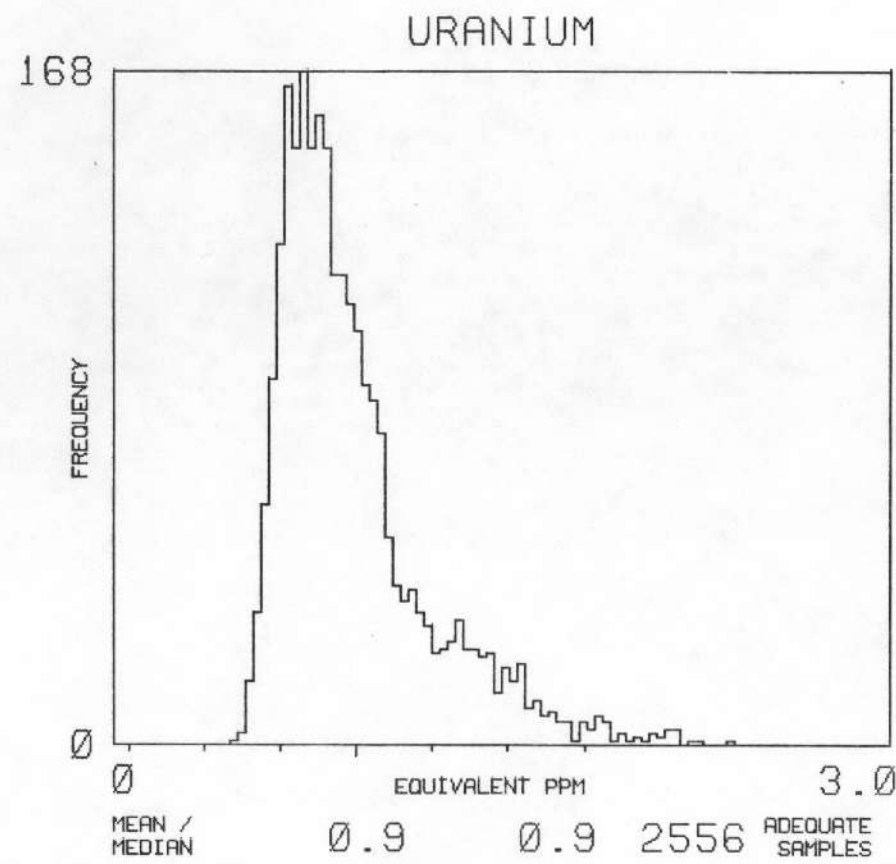
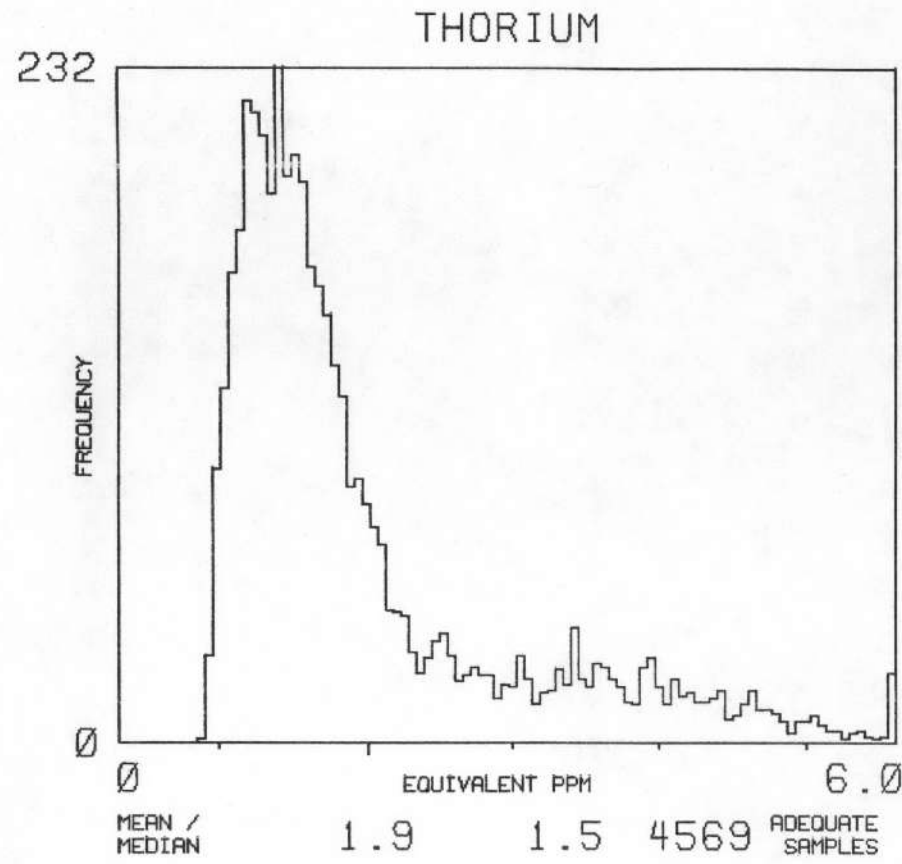


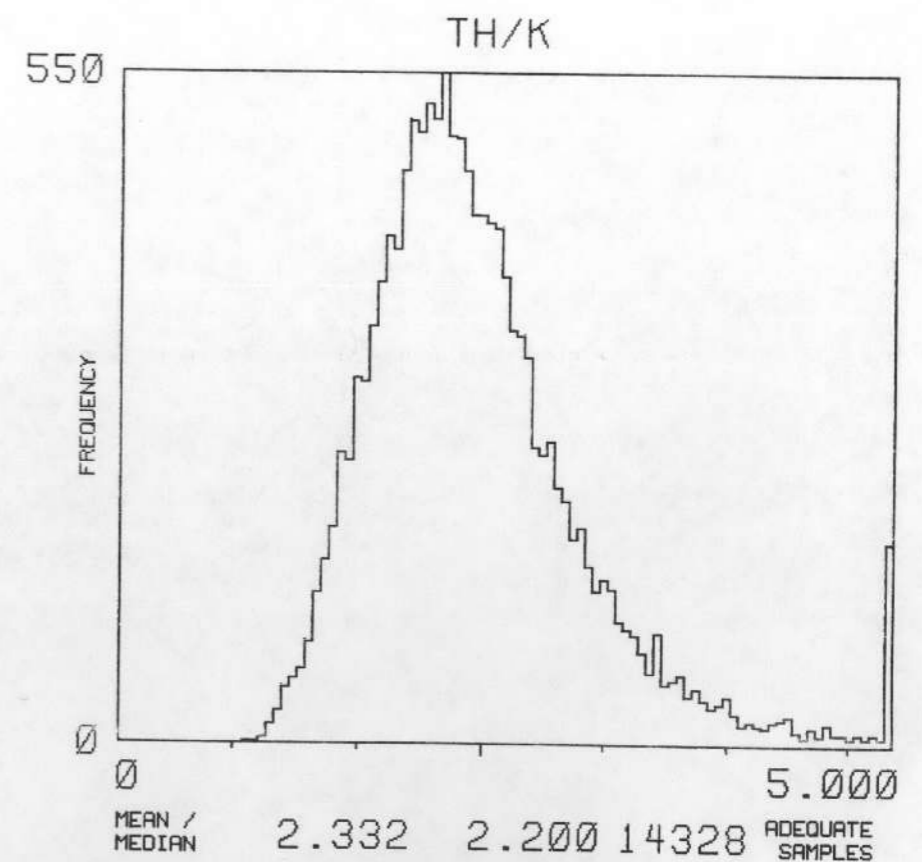
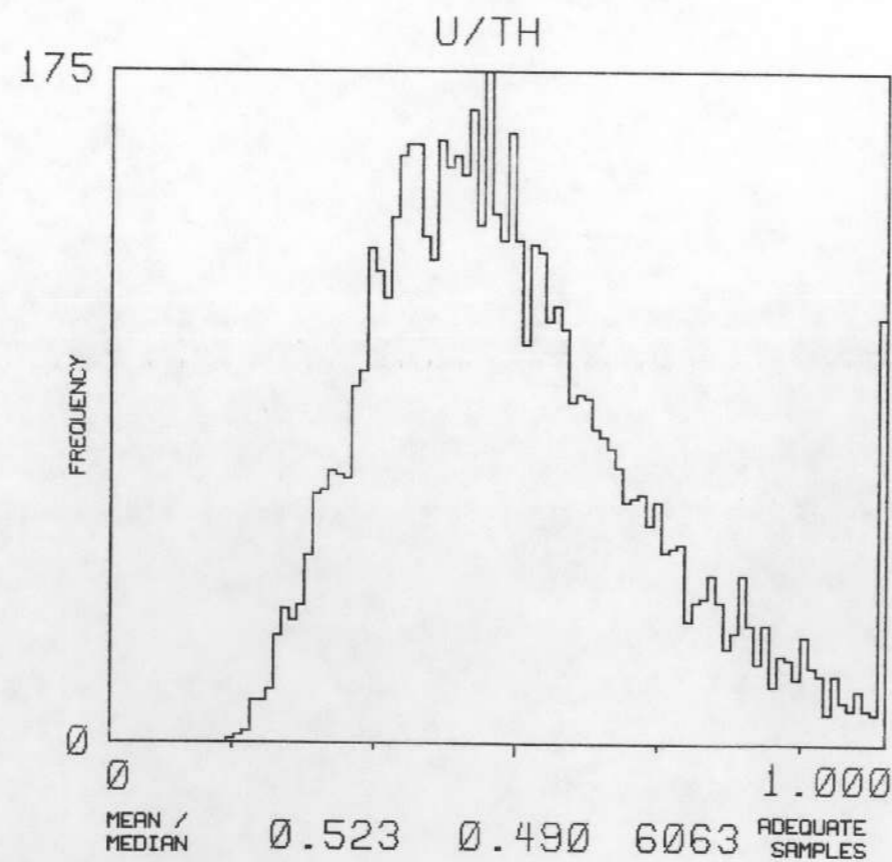
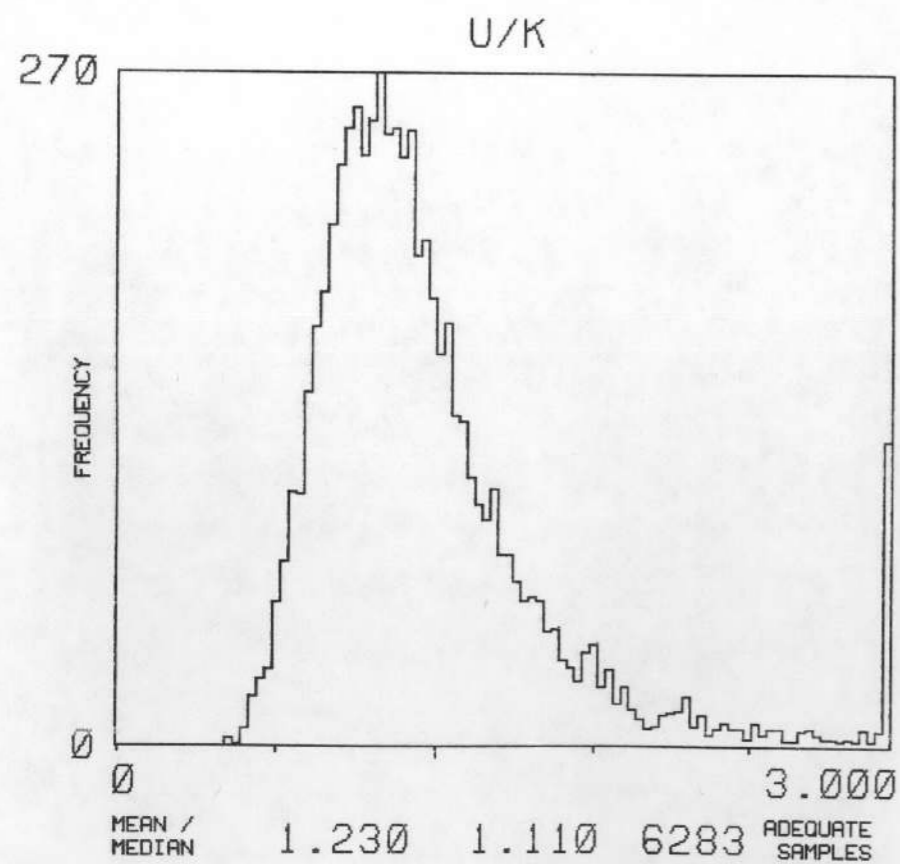
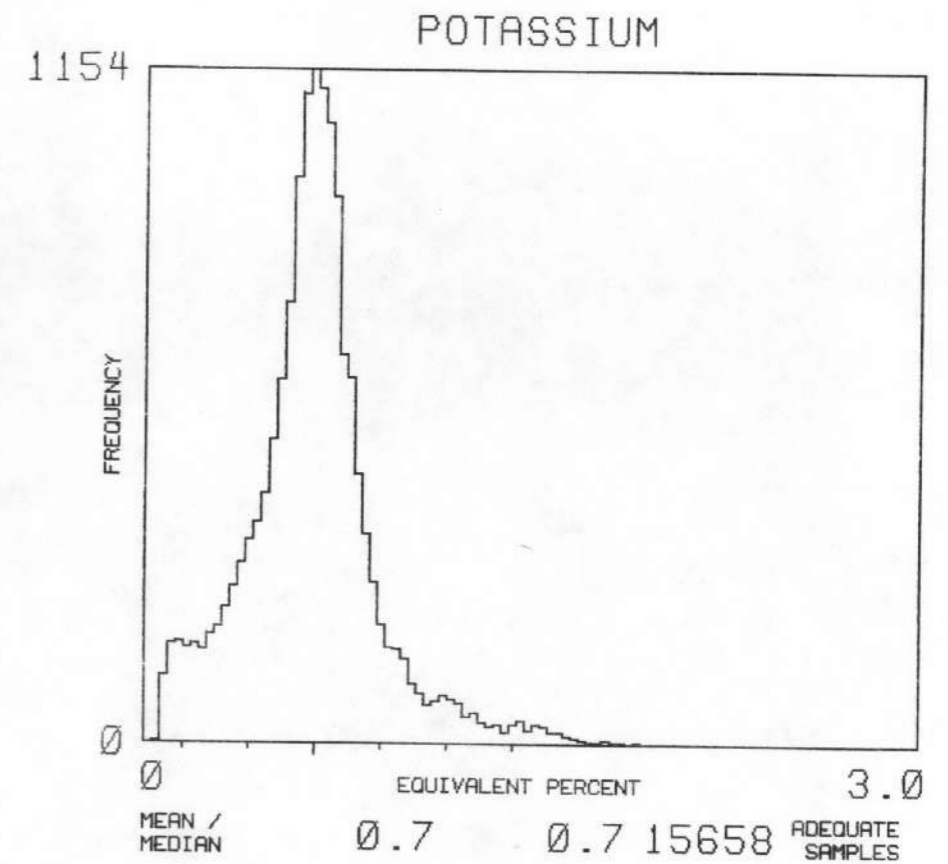
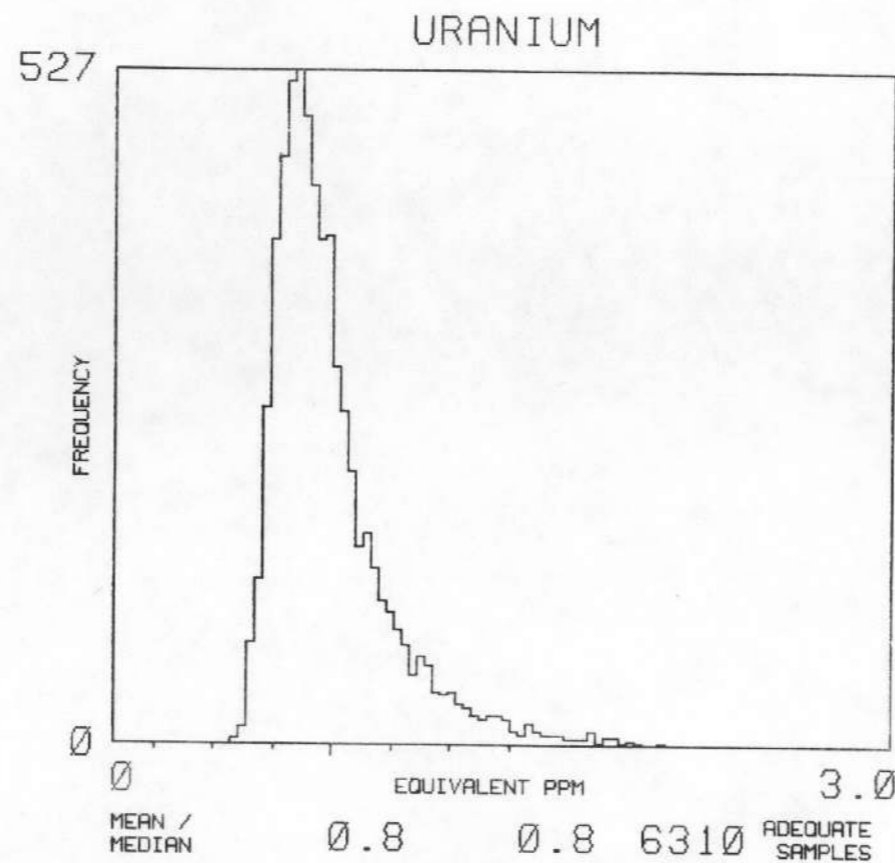
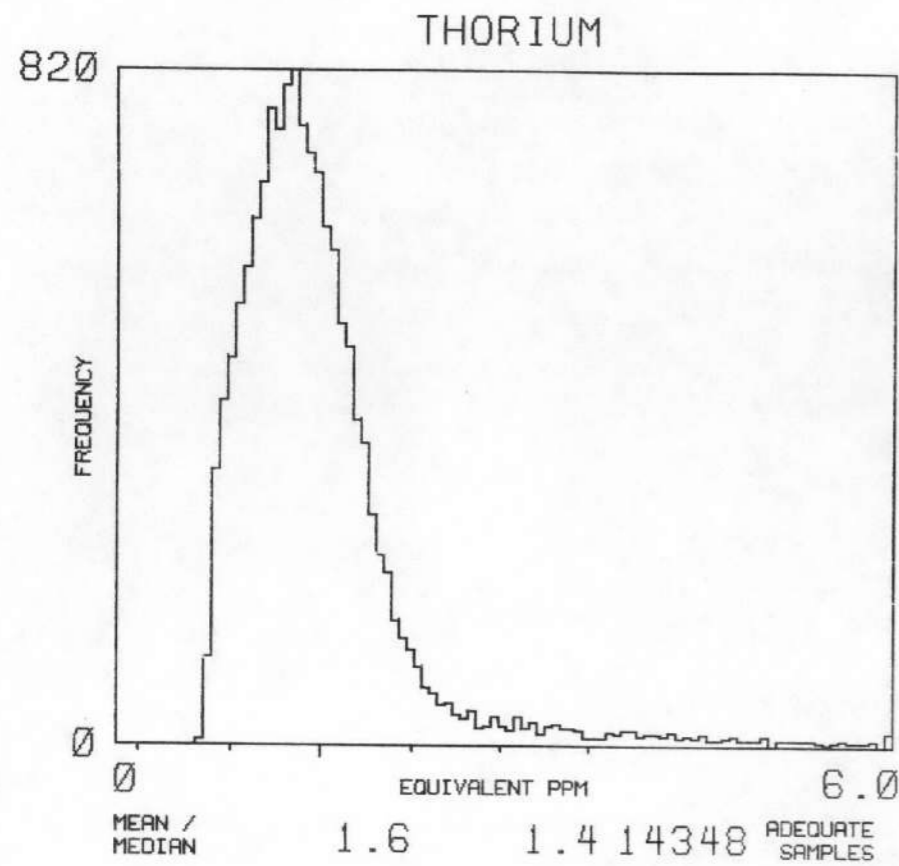


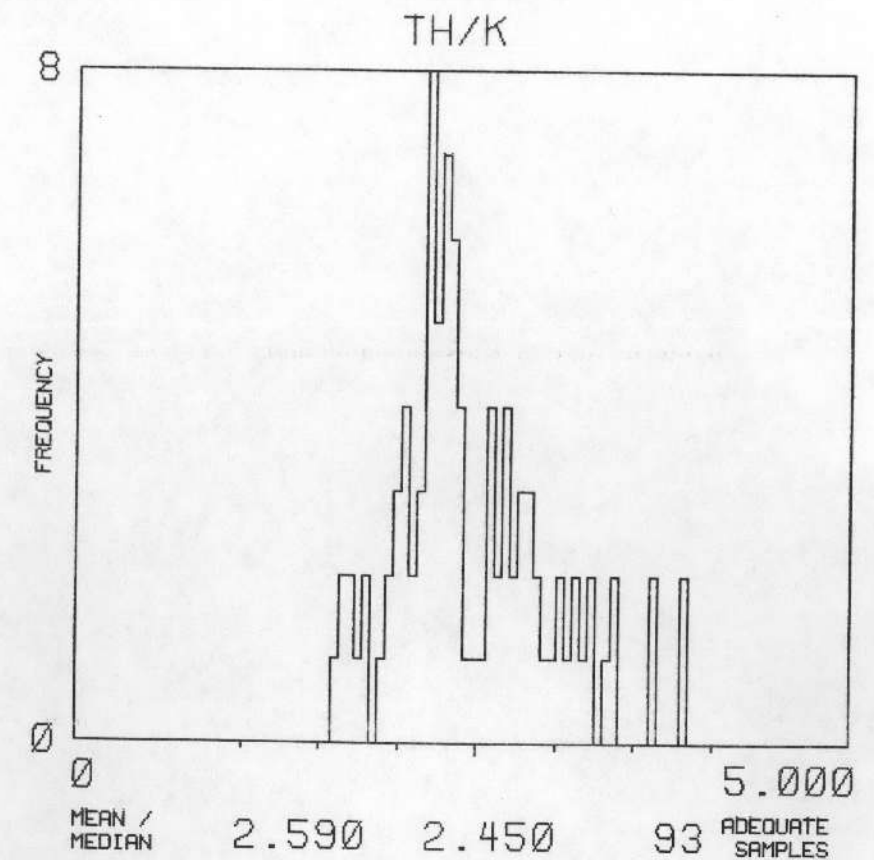
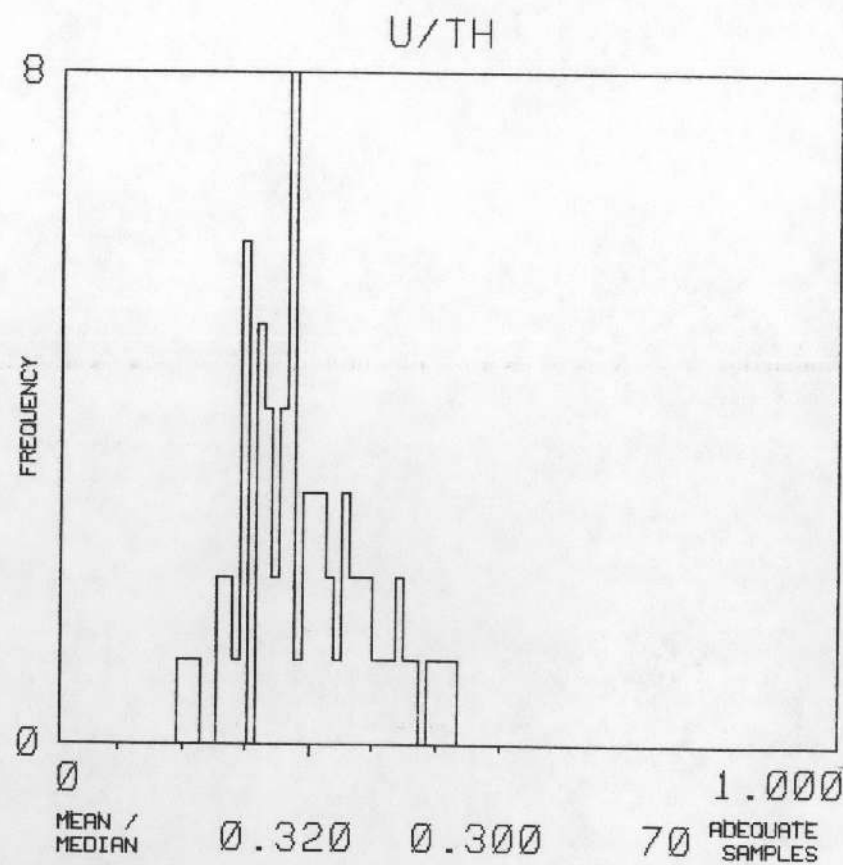
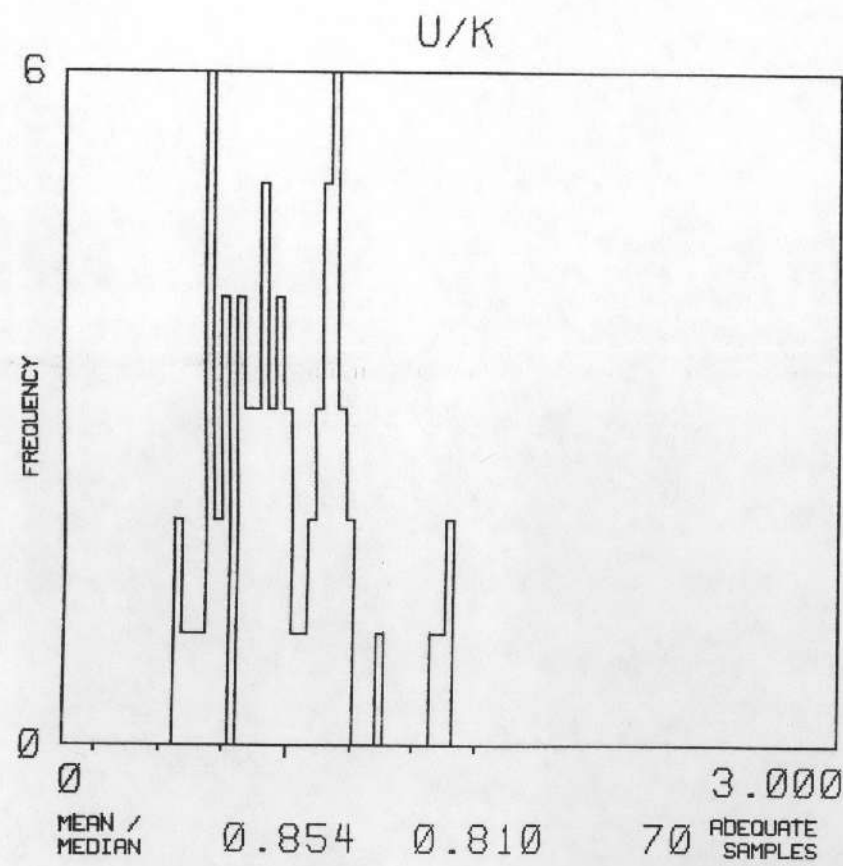
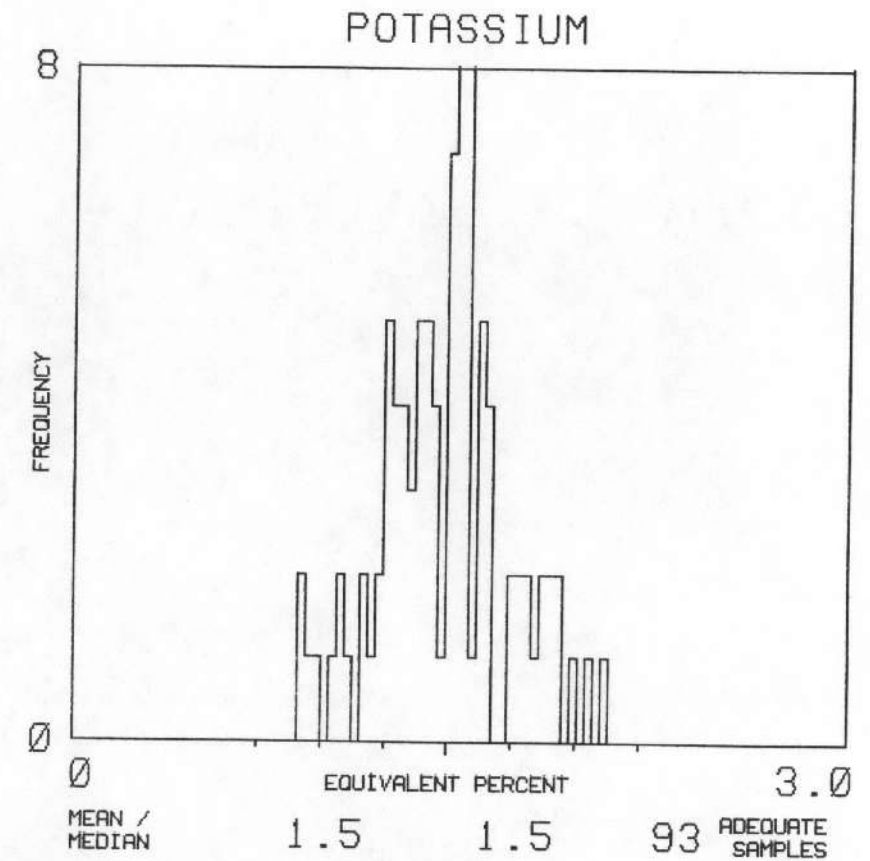
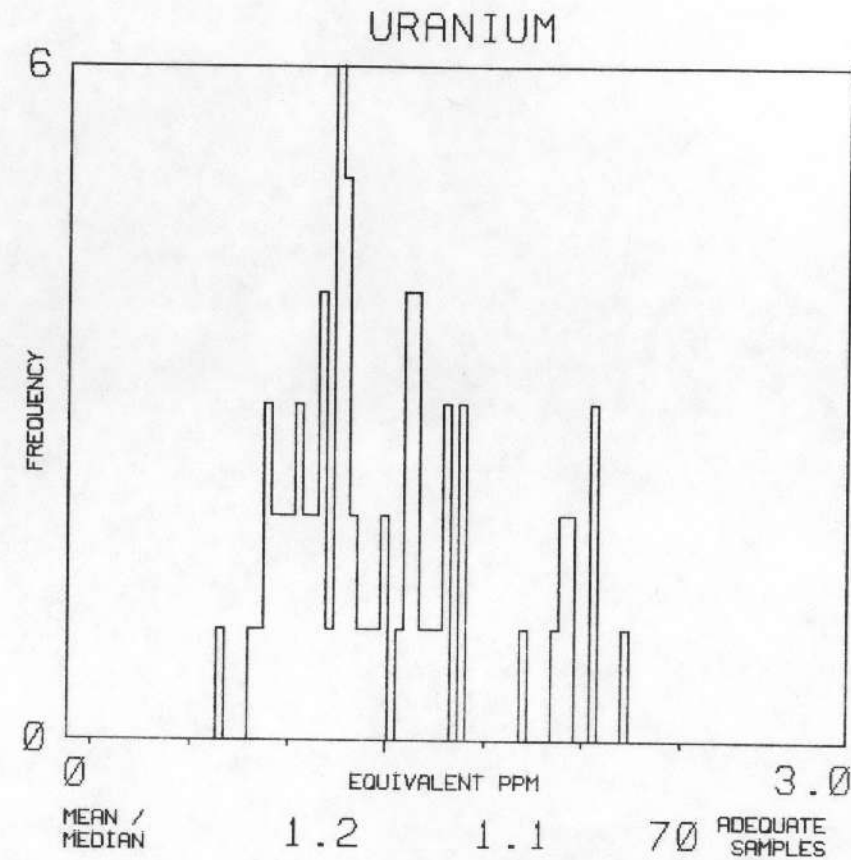
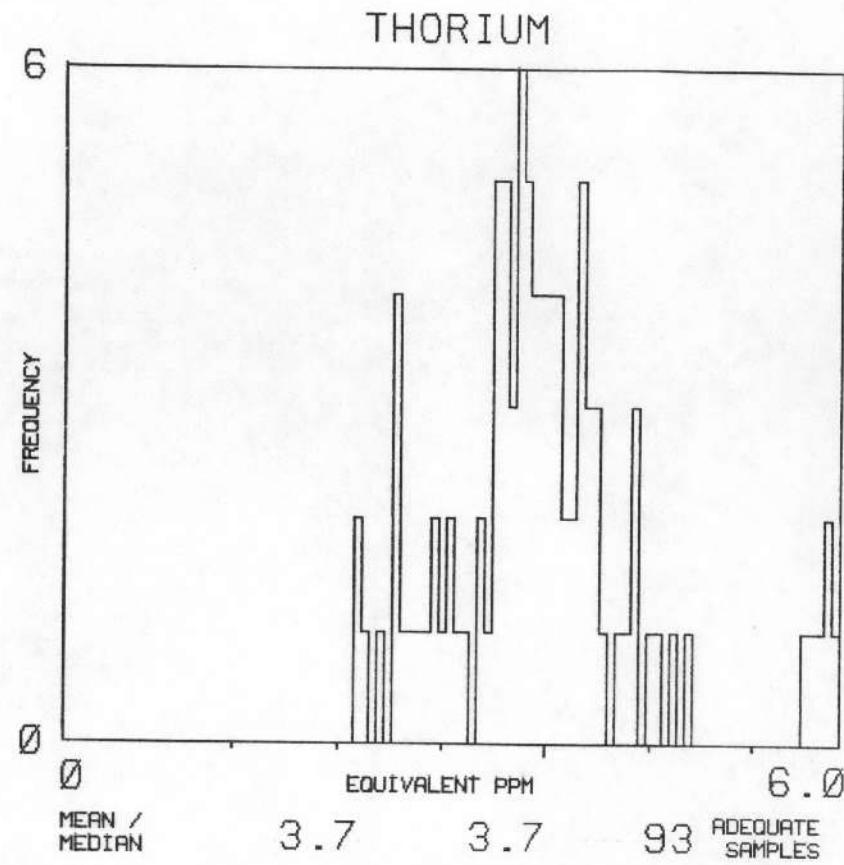












MANITOWOC AND TRAVERSE CITY QUADRANGLESComputer Map Unit Symbol Conversion Table

<u>Computer Map Unit Symbol</u>	<u>Geologic Map Unit Symbol</u>
QAL	Qa1
QB	Qb
QMA	Qma
QM	Qm
QGM	Qgm
QWM	Qwm
QPW	Qpw
QL	Ql
QO	Qo
QDE	Drumlins and Eskers

NOTES:

On the following pages, histograms for each computer map unit are included in the same order as they appear on the above list.

Geologic descriptions of original geologic map units are in Appendix C.

Areas over water or cultural features were assigned separate map unit symbols and were removed from the data block during processing.

**APPENDIX G - Uranium Anomaly Summary and
Statistical Tables**

ANOMALY SUMMARY TABLE																				
ANOMALY	FLIGHT	COMPUTER	MAP UNIT AND NO.			PEAK PPM	NUMBER OF SAMPLES WITH A STANDARD DEVIATION OF :													
			ANOMALOUS SAMPLES IN UNIT				1	2	3	4	5	6	7	GT7						
1 C	80	QGM	/	1	/	0	/	0	/	0	2.0	0	0	1	0	0	0	0	0	0
2 C	90	QGM	/	1	/	0	/	0	/	0	2.0	0	0	1	0	0	0	0	0	0
3 C	90	QMA	/	1	/	0	/	0	/	0	2.1	0	0	1	0	0	0	0	0	0
4 C	100	QD	/	1	/	0	/	0	/	0	1.4	0	0	1	0	0	0	0	0	0
5 C	100	QM	/	3	/	0	/	0	/	0	1.7	1	2	0	0	0	0	0	0	0
6 C	100	QM	/	1	/	0	/	0	/	0	1.8	0	0	1	0	0	0	0	0	0
7 C	120	QGM	/	2	/	0	/	0	/	0	2.0	0	1	1	0	0	0	0	0	0
8 C	120	QGM	/	2	/	0	/	0	/	0	2.4	0	1	0	1	0	0	0	0	0
9 C	1140	QPW	/	1	/	0	/	0	/	0	1.2	0	0	1	0	0	0	0	0	0

NOTES: M INDICATES THAT THE ANOMALY LIES OVER
A URANIUM MINE OR PROSPECT.

C INDICATES THAT THE ANOMALY LIES OVER A CULTURAL FEATURE.

W INDICATES POSSIBLE INTERFERENCE BY WEATHER PHENOMENA.

			MAP UNIT GAL						
			-3	-2	-1	0	+1	+2	+3
POTASIAM	DIST	NORMAL	0.4061	0.7301	1.0541	1.3781	1.7021	2.0261	2.3501
URANIUM	DIST	NORMAL	0.1163	0.4681	0.8199	1.1717	1.5235	1.8753	2.2271
THURIUM	DIST	NORMAL	0.0668	1.2613	2.4558	3.6503	4.8448	6.0393	7.2338
U/K	DIST	NORMAL	0.2170	0.4283	0.6396	0.8509	1.0622	1.2735	1.4848
U/TH	DIST	NORMAL	0.0671	0.1527	0.2383	0.3239	0.4095	0.4951	0.5807
TH/K	DIST	NORMAL	1.1527	1.6454	2.1381	2.6308	3.1235	3.6162	4.1089

			MAP UNIT QB						
			-3	-2	-1	0	+1	+2	+3
POTASIAM	DIST	NORMAL	-0.3349	-0.0281	0.2787	0.5855	0.8923	1.1991	1.5059
URANIUM	DIST	NORMAL	0.3730	0.5164	0.6598	0.8032	0.9466	1.0900	1.2334
THURIUM	DIST	NORMAL	0.1035	0.4859	0.8683	1.2507	1.6331	2.0155	2.3979
U/K	DIST	NORMAL	-0.8543	-0.0462	0.7619	1.5700	2.3781	3.1862	3.9943
U/TH	DIST	NORMAL	0.2211	0.3548	0.4885	0.6222	0.7559	0.8896	1.0233
TH/K	DIST	NORMAL	-1.5275	-0.2541	1.0193	2.2927	3.5661	4.8395	6.1129

			MAP UNIT QMA						
			-3	-2	-1	0	+1	+2	+3
POTASIAM	DIST	NORMAL	-0.5872	-0.0891	0.4090	0.9071	1.4052	1.9033	2.4014
URANIUM	DIST	NORMAL	-0.0000	0.3375	0.6750	1.0125	1.3500	1.6875	2.0250
THURIUM	DIST	NORMAL	-1.3568	-0.0580	1.2408	2.5396	3.8384	5.1372	6.4360
U/K	DIST	NORMAL	-1.3390	-0.5292	0.2806	1.0904	1.9002	2.7100	3.5198
U/TH	DIST	NORMAL	-0.1108	0.0464	0.2036	0.3608	0.5180	0.6752	0.8324
TH/K	DIST	NORMAL	-0.8066	0.4418	1.6902	2.9386	4.1870	5.4354	6.6838

			MAP UNIT QM						
			-3	-2	-1	0	+1	+2	+3
POTASIAM	DIST	NORMAL	-0.2796	0.1086	0.4968	0.8850	1.2732	1.6614	2.0496
URANIUM	DIST	NORMAL	0.0128	0.3271	0.6414	0.9557	1.2700	1.5843	1.8986
THURIUM	DIST	NORMAL	-1.3902	-0.2389	0.9124	2.0637	3.2150	4.3663	5.5176
U/K	DIST	NORMAL	-0.2753	0.1580	0.5913	1.0246	1.4579	1.8912	2.3245
U/TH	DIST	NORMAL	-0.0820	0.0960	0.2740	0.4520	0.6300	0.8080	0.9860
TH/K	DIST	NORMAL	0.5257	1.1064	1.6871	2.2678	2.8485	3.4292	4.0099

			MAP UNIT QGM						
			-3	-2	-1	0	+1	+2	+3
POTASIAM	DIST	NORMAL	-0.2810	0.1532	0.5874	1.0216	1.4558	1.8900	2.3242
URANIUM	DIST	NORMAL	0.0468	0.3782	0.7096	1.0410	1.3724	1.7038	2.0352
THURIUM	DIST	NORMAL	-1.2697	0.0402	1.3501	2.6600	3.9699	5.2798	6.5897
U/K	DIST	NORMAL	-0.5311	-0.0171	0.4969	1.0109	1.5249	2.0389	2.5529
U/TH	DIST	NORMAL	-0.1158	0.0530	0.2218	0.3906	0.5594	0.7282	0.8970
TH/K	DIST	NORMAL	0.3979	1.1240	1.8501	2.5762	3.3023	4.0284	4.7545

		MAP UNIT QWM						
		-3	-2	-1	0	+1	+2	+3
POTASium	DIST NORMAL	-0.8590	-0.2741	0.3108	0.8957	1.4806	2.0655	2.6504
URANIUM	DIST NORMAL	-0.1337	0.3093	0.7523	1.1953	1.6383	2.0813	2.5243
THORIUM	DIST NORMAL	-2.2235	-0.6875	0.8485	2.3845	3.9205	5.4565	6.9925
U/K	DIST NORMAL	0.1676	0.4744	0.7812	1.0880	1.3948	1.7016	2.0084
U/TH	DIST NORMAL	-0.0210	0.1297	0.2804	0.4311	0.5818	0.7325	0.8832
TH/K	DIST NORMAL	0.7598	1.3439	1.9280	2.5121	3.0962	3.6803	4.2644

		MAP UNIT QPW						
		-3	-2	-1	0	+1	+2	+3
POTASium	DIST NORMAL	0.1438	0.3061	0.4684	0.6307	0.7930	0.9553	1.1176
URANIUM	DIST NORMAL	0.2880	0.4529	0.6178	0.7827	0.9476	1.1125	1.2774
THORIUM	DIST NORMAL	0.1620	0.6131	1.0642	1.5153	1.9664	2.4175	2.8686
U/K	DIST NORMAL	-0.1141	0.3313	0.7767	1.2221	1.6675	2.1129	2.5583
U/TH	DIST NORMAL	-0.0046	0.1796	0.3638	0.5480	0.7322	0.9164	1.1006
TH/K	DIST NORMAL	0.6104	1.1879	1.7654	2.3429	2.9204	3.4979	4.0754

		MAP UNIT QL						
		-3	-2	-1	0	+1	+2	+3
POTASium	DIST NORMAL	-0.4959	-0.0751	0.3457	0.7665	1.1873	1.6081	2.0289
URANIUM	DIST NORMAL	0.0590	0.3523	0.6456	0.9389	1.2322	1.5255	1.8188
THORIUM	DIST NORMAL	-1.5015	-0.3672	0.7671	1.9014	3.0357	4.1700	5.3043
U/K	DIST NORMAL	-0.6689	-0.0465	0.5759	1.1983	1.8207	2.4431	3.0655
U/TH	DIST NORMAL	-0.1315	0.0767	0.2849	0.4931	0.7013	0.9095	1.1177
TH/K	DIST NORMAL	0.2643	0.9747	1.6851	2.3955	3.1059	3.8163	4.5267

		MAP UNIT QO						
		-3	-2	-1	0	+1	+2	+3
POTASium	DIST NORMAL	-0.1053	0.1499	0.4051	0.6603	0.9155	1.1707	1.4259
URANIUM	DIST NORMAL	0.1557	0.3844	0.6131	0.8418	1.0705	1.2992	1.5279
THORIUM	DIST NORMAL	-0.5235	0.1722	0.8679	1.5636	2.2593	2.9550	3.6507
U/K	DIST NORMAL	-0.6049	0.0068	0.6185	1.2302	1.8419	2.4536	3.0653
U/TH	DIST NORMAL	-0.0263	0.1568	0.3399	0.5230	0.7061	0.8892	1.0723
TH/K	DIST NORMAL	-0.0519	0.7426	1.5371	2.3316	3.1261	3.9206	4.7151

		MAP UNIT QDE						
		-3	-2	-1	0	+1	+2	+3
POTASium	DIST NORMAL	0.7133	0.9590	1.2047	1.4504	1.6961	1.9418	2.1875
URANIUM	DIST NORMAL	0.0903	0.4688	0.8473	1.2258	1.6043	1.9828	2.3613
THORIUM	DIST NORMAL	1.2961	2.1030	2.9099	3.7168	4.5237	5.3306	6.1375
U/K	DIST NORMAL	0.1191	0.3642	0.6093	0.8544	1.0995	1.3446	1.5897
U/TH	DIST NORMAL	0.0750	0.1565	0.2380	0.3195	0.4010	0.4825	0.5640
TH/K	DIST NORMAL	1.0732	1.5789	2.0846	2.5903	3.0960	3.6017	4.1074

MAP UNIT QMA

	10	20	30	40	50	60	70	80	90	100	110	120	1010	1060	1070
POTASIAM	0.866	0.536	0.912	0.726	1.225	1.441	1.370	1.073	0.600	1.041	0.941	0.589	0.914	0.461	0.803
URANIUM	0.766	0.757	0.966	0.828	0.970	0.963	0.970	0.925	1.054	1.335	1.408	1.011	1.064	0.824	0.865
THURIUM	1.986	1.786	2.502	2.106	3.422	3.668	2.831	3.483	1.764	3.179	3.314	2.155	2.658	1.414	2.217
U/K	0.701	0.616	0.794	0.772	0.725	0.696	0.711	0.940	1.809	1.213	2.049	1.280	0.991	1.830	0.790
U/TH	0.318	0.250	0.306	0.291	0.273	0.268	0.344	0.273	0.607	0.374	0.439	0.373	0.333	0.592	0.319
TH/K	2.271	3.076	2.735	2.460	2.730	2.609	2.068	3.395	3.120	3.395	4.861	3.749	2.922	3.077	2.920

	1080	1090	1100	1110	1120	1130	1140
POTASIAM	0.539	0.000	0.000	0.000	0.000	0.000	0.000
URANIUM	0.911	0.000	0.000	0.000	0.000	0.000	0.000
THURIUM	1.528	0.000	0.000	0.000	0.000	0.000	0.000
U/K	1.632	0.000	0.000	0.000	0.000	0.000	0.000
U/TH	0.552	0.000	0.000	0.000	0.000	0.000	0.000
TH/K	3.398	0.000	0.000	0.000	0.000	0.000	0.000

MAP UNIT QM

	10	20	30	40	50	60	70	80	90	100	110	120	1010	1060	1070
POTASIAM	0.696	0.679	0.734	0.734	0.799	0.963	1.098	1.100	1.031	0.866	0.845	0.879	1.700	0.847	1.481
URANIUM	0.792	0.822	0.773	0.759	0.795	0.914	1.097	1.116	1.111	1.042	0.839	0.984	1.224	0.812	1.066
THURIUM	1.535	1.507	1.502	1.618	1.713	2.104	2.762	2.771	2.603	2.116	2.002	2.107	4.458	1.662	3.787
U/K	1.094	1.301	1.003	0.911	0.851	0.858	0.999	1.003	1.141	1.365	0.976	1.065	0.728	0.920	0.676
U/TH	0.526	0.562	0.508	0.435	0.420	0.417	0.408	0.429	0.464	0.558	0.450	0.453	0.277	0.491	0.269
TH/K	2.197	2.202	2.066	2.189	2.093	2.120	2.507	2.428	2.453	2.431	2.357	2.363	2.638	1.981	2.562

	1080	1090	1100	1110	1120	1130	1140
POTASIAM	1.047	0.764	0.796	0.766	0.580	0.704	0.709
URANIUM	0.849	0.714	0.776	0.769	0.769	0.940	0.860
THURIUM	2.010	1.610	1.702	1.491	1.263	1.895	1.779
U/K	0.813	0.997	0.903	1.004	1.328	1.220	1.185
U/TH	0.445	0.522	0.435	0.518	0.620	0.458	0.460
TH/K	1.877	2.118	2.078	1.969	2.171	2.508	2.513

MAP UNIT QPW

	10	20	30	40	50	60	70	80	90	100	110	120	1010	1060	1070
POTASIAM	0.617	0.609	0.513	0.780	0.651	0.749	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
URANIUM	0.734	0.714	0.717	0.818	0.804	0.706	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
THURIUM	1.374	1.442	1.396	1.781	1.733	1.752	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
U/K	1.120	1.099	1.201	1.006	1.060	0.918	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
U/TH	0.555	0.529	0.615	0.434	0.389	0.421	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
TH/K	2.188	2.195	2.330	2.270	2.589	2.372	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

	1080	1090	1100	1110	1120	1130	1140
POTASIAM	0.000	0.000	0.000	0.000	0.000	0.000	0.622
URANIUM	0.000	0.000	0.000	0.000	0.000	0.000	0.849
THURIUM	0.000	0.000	0.000	0.000	0.000	0.000	1.511
U/K	0.000	0.000	0.000	0.000	0.000	0.000	1.465
U/TH	0.000	0.000	0.000	0.000	0.000	0.000	0.623
TH/K	0.000	0.000	0.000	0.000	0.000	0.000	2.465

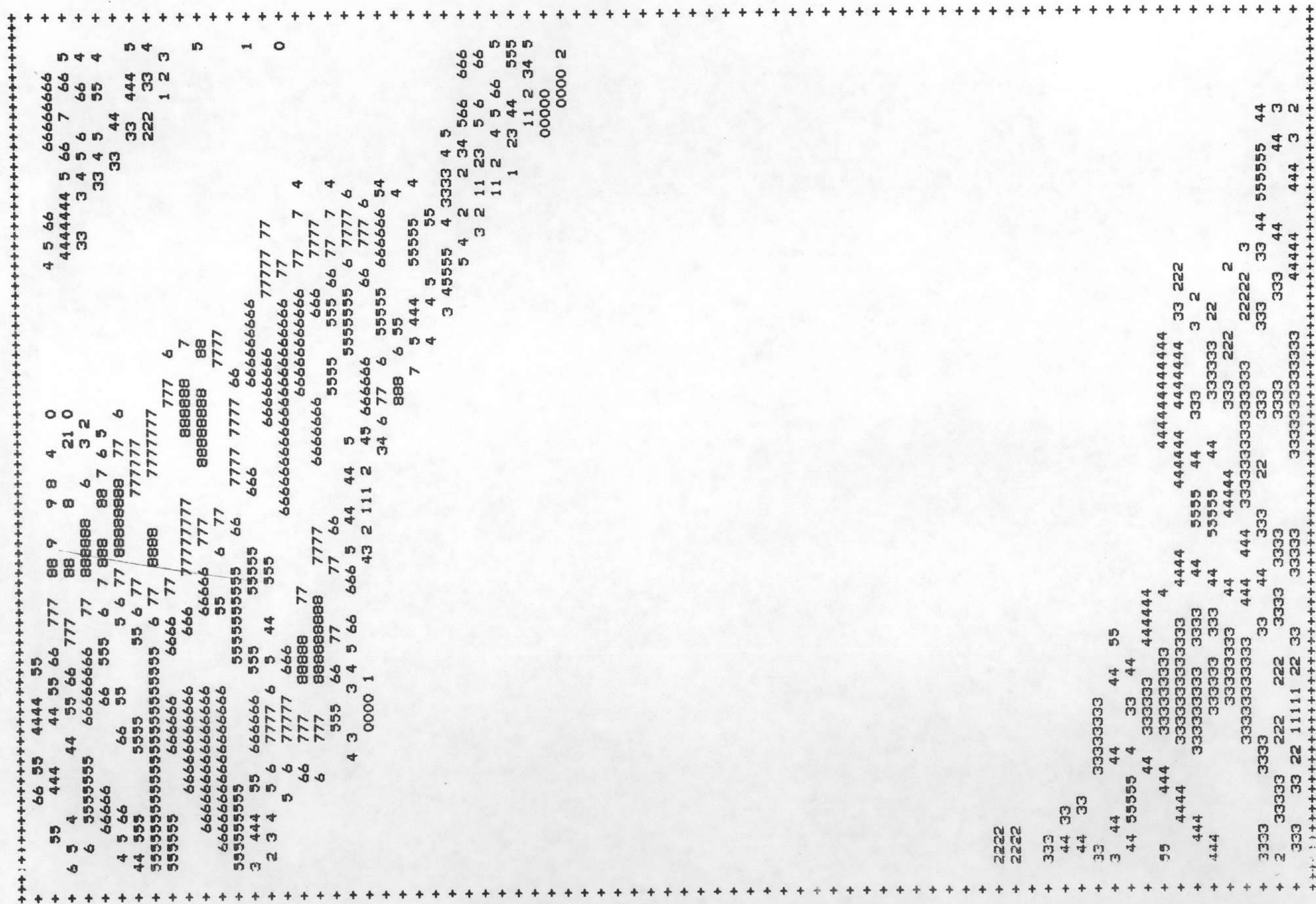
MAP UNIT QL

	10	20	30	40	50	60	70	80	90	100	110	120	1010	1060	1070
POTASIAM	0.687	0.674	0.772	0.866	1.650	1.407	0.831	0.779	0.762	0.746	0.557	0.683	1.461	0.530	1.304
URANIUM	0.871	0.781	0.860	0.814	0.946	1.016	1.116	0.830	0.947	0.993	0.691	0.974	1.118	0.803	1.044
THURIUM	1.629	1.559	1.741	2.369	3.830	3.881	2.211	1.498	1.832	1.957	1.310	1.679	3.567	1.350	3.500
U/K	1.142	1.093	0.881	0.712	0.573	0.564	1.260	1.109	1.353	1.581	1.183	1.262	0.720	2.167	0.759
U/TH	0.510	0.516	0.432	0.311	0.242	0.240	0.473	0.597	0.542	0.602	0.538	0.532	0.301	0.528	0.295
TH/K	2.325	2.182	2.038	2.376	2.335	2.621	2.598	1.923	2.503	2.581	2.424	2.294	2.436	2.375	2.640

	1080	1090	1100	1110	1120	1130	1140
POTASIAM	0.788	0.521	0.495	0.479	0.000	0.560	0.562
URANIUM	0.871	0.738	0.788	0.000	0.000	0.786	0.808
THURIUM	1.537	1.078	1.093	1.208	0.000	1.386	1.343
U/K	1.248	0.973	1.082	0.000	0.000	1.546	1.442
U/TH	0.597	0.683	0.888	0.000	0.000	0.614	0.573
TH/K	2.183	1.684	2.605	2.109	0.000	2.401	2.372

APPENDIX H - Pseudo Contour Maps

MANITOWOC



Potassium Pseudo-Contour Map - Manitowoc Quadrangle

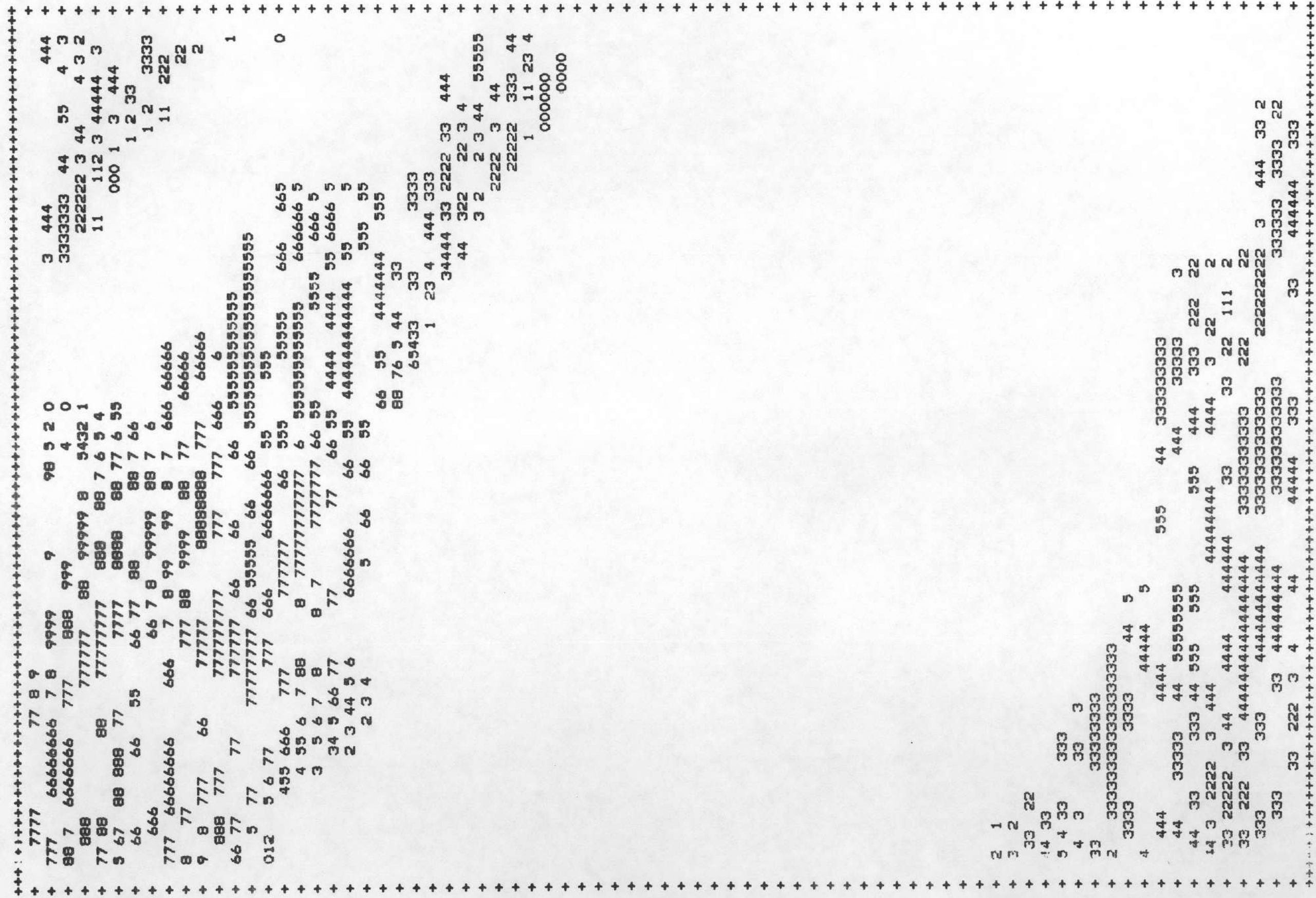
EXPLANATION

PRINT CHARACTER	VALUE
0	0.0000
1	0.1250
2	0.2500
3	0.3750
4	0.5000
5	0.6250
6	0.7500
7	0.8750
8	1.0000
9	1.1250
0	1.2500
1	1.3750
2	1.5000
3	1.6250
4	1.7500
5	1.8750
6	2.0000
7	2.1250
8	2.2500
9	2.3750
0	2.5000

SCALE IN EQUIVALENT PERCENT



MANITOWOC

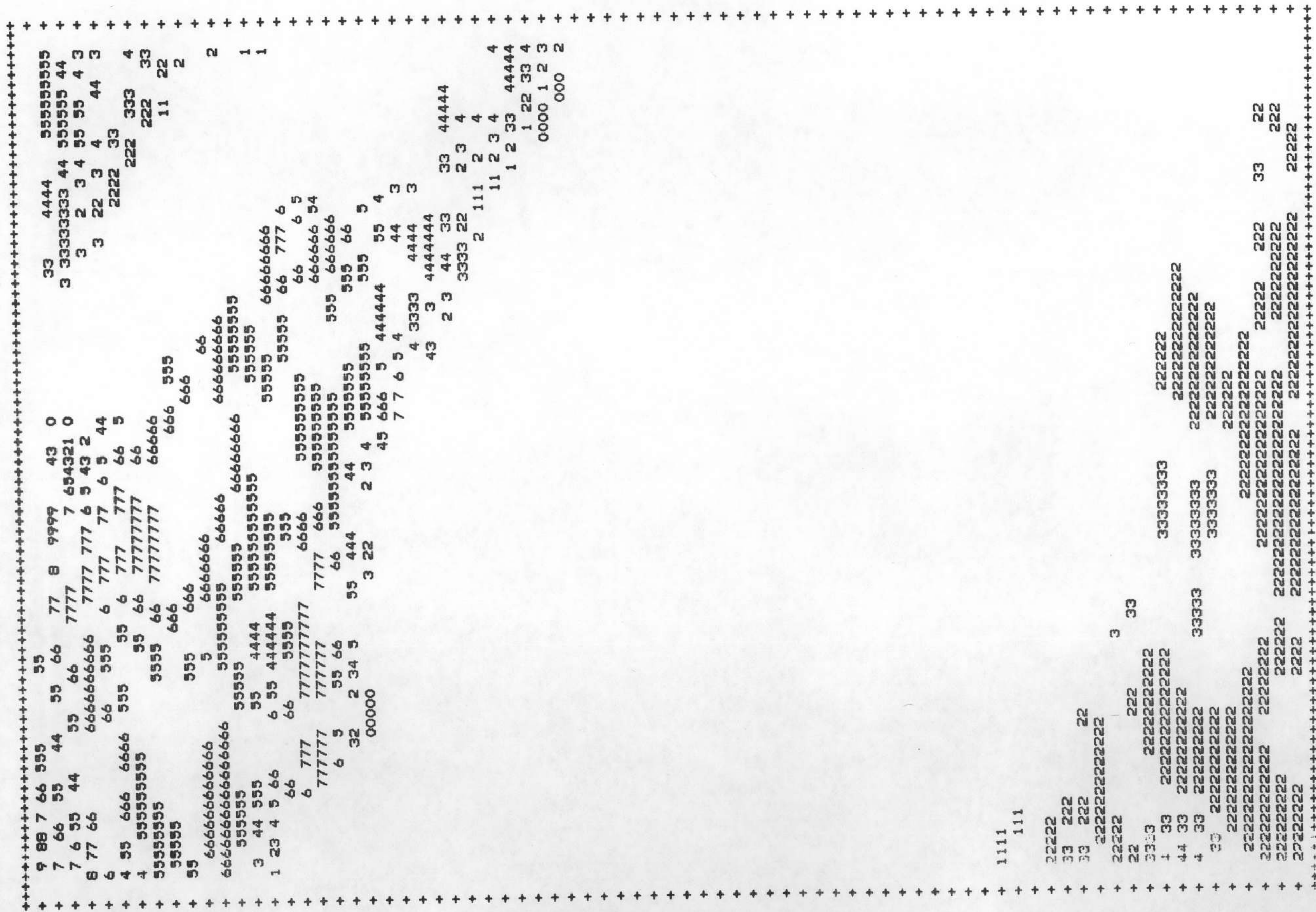


PRINT CHARACTER	EXPLANATION	VALUE
0	LE	0.0000
1		0.0000
1		0.1000
1		0.2000
2		0.3000
2		0.4000
2		0.5000
2		0.6000
2		0.7000
2		0.8000
2		0.9000
3		1.0000
3		1.1000
3		1.2000
3		1.3000
3		1.4000
3		1.5000
3		1.6000
3		1.7000
3		1.8000
4		1.8000

Uranium Pseudo-Contour Map - Manitowoc Quadrangle

SCALE IN EQUIVALENT PPM

MANITOWOC



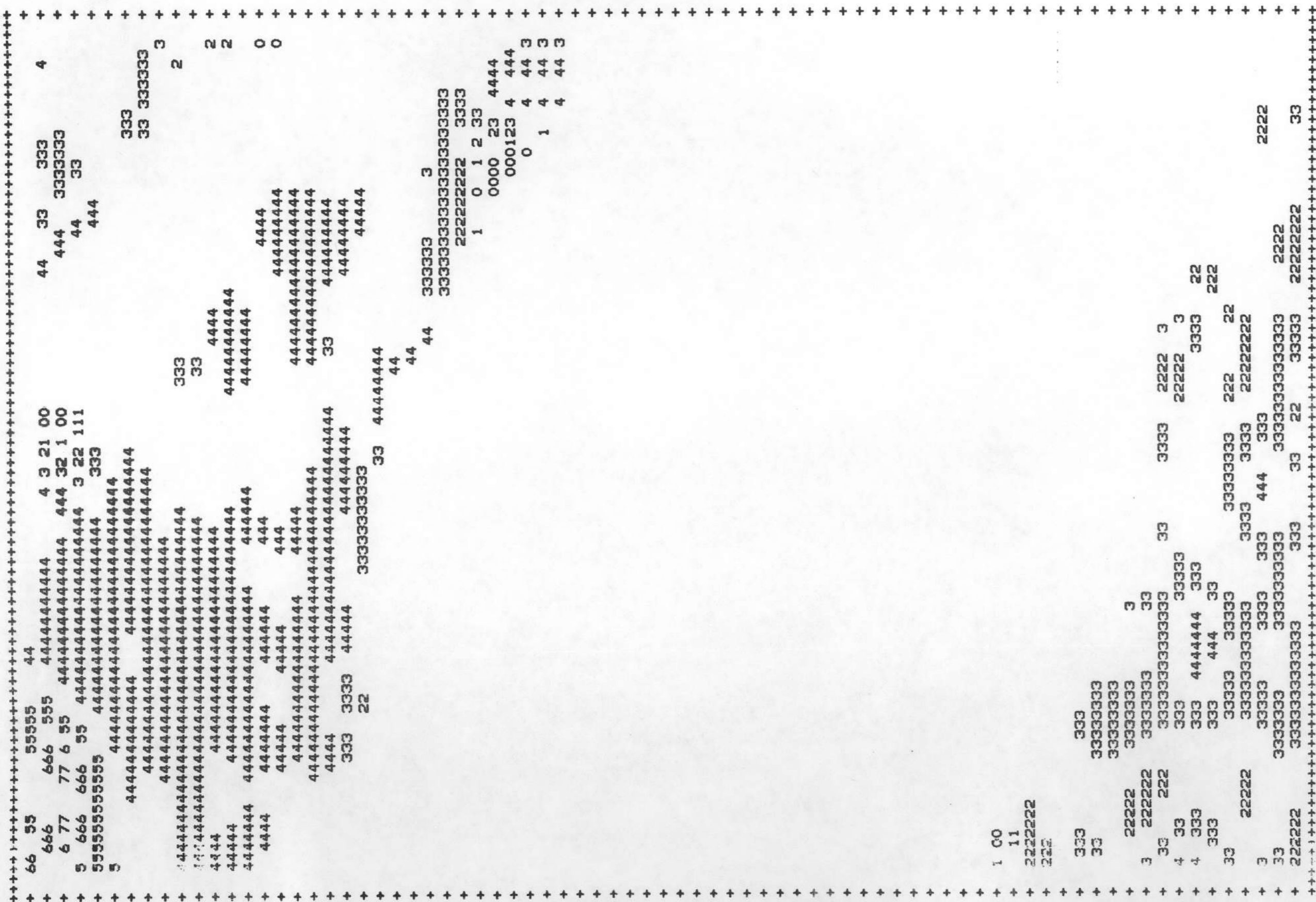
Thorium Pseudo-Contour Map - Manitowoc Quadrangle

EXPLANATION

PRINT CHARACTER	VALUE
0	LE 0.0000
1	0.0000 0.3750
2	0.3750 0.7500
3	0.7500 1.1250
4	1.1250 1.5000
5	1.5000 1.8750
6	1.8750 2.2500
7	2.2500 2.6250
8	2.6250 3.0000
9	3.0000 3.3750
GT	3.3750 3.7500

SCALE IN EQUIVALENT PPM

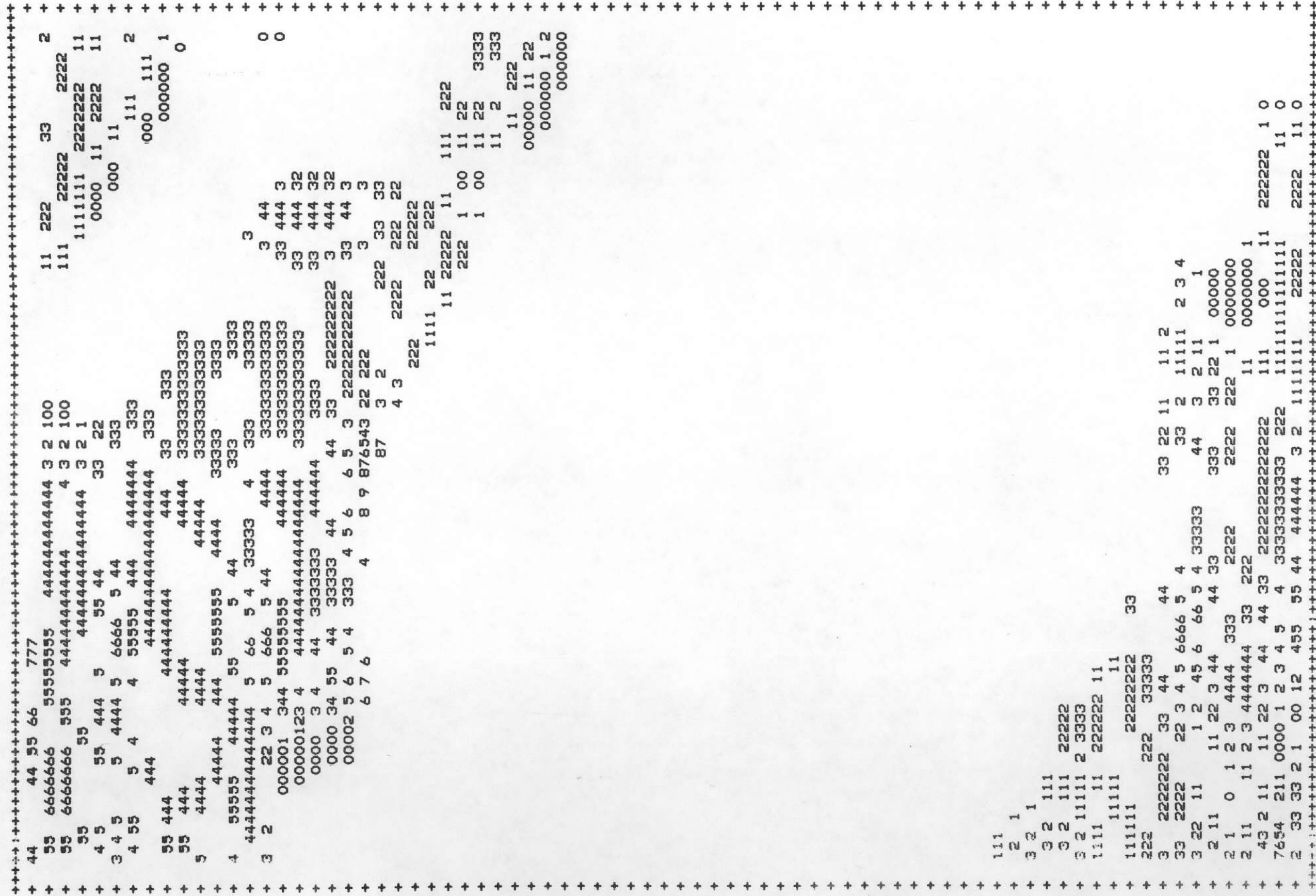
MANITOWOC



Thorium/Potassium Pseudo-Contour Map - Manitowoc Quadrangle

EXPLANATION		
PRINT CHARACTER	VALUE	
0	LE	0.0000
1	0.0000	0.3750
2	0.3750	0.7500
3	0.7500	1.1250
4	1.1250	1.5000
5	1.5000	1.8750
6	1.8750	2.2500
7	2.2500	2.6250
8	2.6250	3.0000
9	3.0000	3.3750
GT	3.3750	3.7500

MANITOWOC

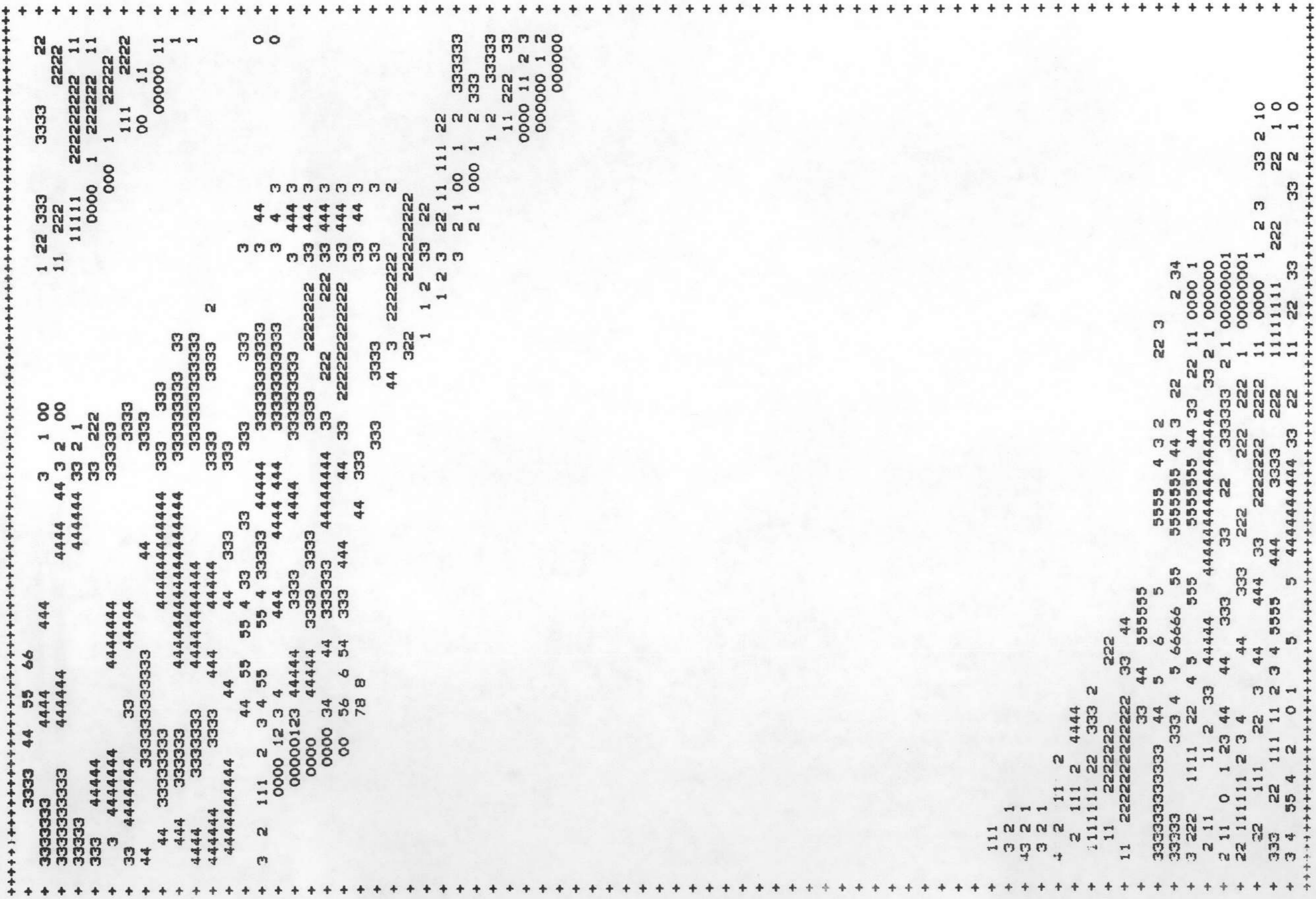


EXPLANATION

PRINT CHARACTER	VALUE
0	LE 0.0000
1	0.0000 0.1250
2	0.1250 0.2500
3	0.2500 0.3750
4	0.3750 0.5000
5	0.5000 0.6250
6	0.6250 0.7500
7	0.7500 0.8750
8	0.8750 1.0000
9	1.0000 1.1250
	1.1250 1.2500
	1.2500 1.3750
	1.3750 1.5000
	1.5000 1.6250
	1.6250 1.7500
	1.7500 1.8750
	1.8750 2.0000
	2.0000 2.1250
	2.1250 2.2500
	2.2500 2.3750
	2.3750 2.5000
	2.5000 2.6250
	2.6250 2.7500
	2.7500 2.8750
	2.8750 3.0000
	3.0000 3.1250
	3.1250 3.2500
	3.2500 3.3750
	3.3750 3.5000
	3.5000 3.6250
	3.6250 3.7500
	3.7500 3.8750
	3.8750 4.0000
	4.0000 4.1250
	4.1250 4.2500
	4.2500 4.3750
	4.3750 4.5000
	4.5000 4.6250
	4.6250 4.7500
	4.7500 4.8750
	4.8750 5.0000
	5.0000 5.1250
	5.1250 5.2500
	5.2500 5.3750
	5.3750 5.5000
	5.5000 5.6250
	5.6250 5.7500
	5.7500 5.8750
	5.8750 6.0000
	6.0000 6.1250
	6.1250 6.2500
	6.2500 6.3750
	6.3750 6.5000
	6.5000 6.6250
	6.6250 6.7500
	6.7500 6.8750
	6.8750 7.0000
	7.0000 7.1250
	7.1250 7.2500
	7.2500 7.3750
	7.3750 7.5000
	7.5000 7.6250
	7.6250 7.7500
	7.7500 7.8750
	7.8750 8.0000
	8.0000 8.1250
	8.1250 8.2500
	8.2500 8.3750
	8.3750 8.5000
	8.5000 8.6250
	8.6250 8.7500
	8.7500 8.8750
	8.8750 9.0000
	9.0000 9.1250
	9.1250 9.2500
	9.2500 9.3750
	9.3750 9.5000
	9.5000 9.6250
	9.6250 9.7500
	9.7500 9.8750
	9.8750 10.0000



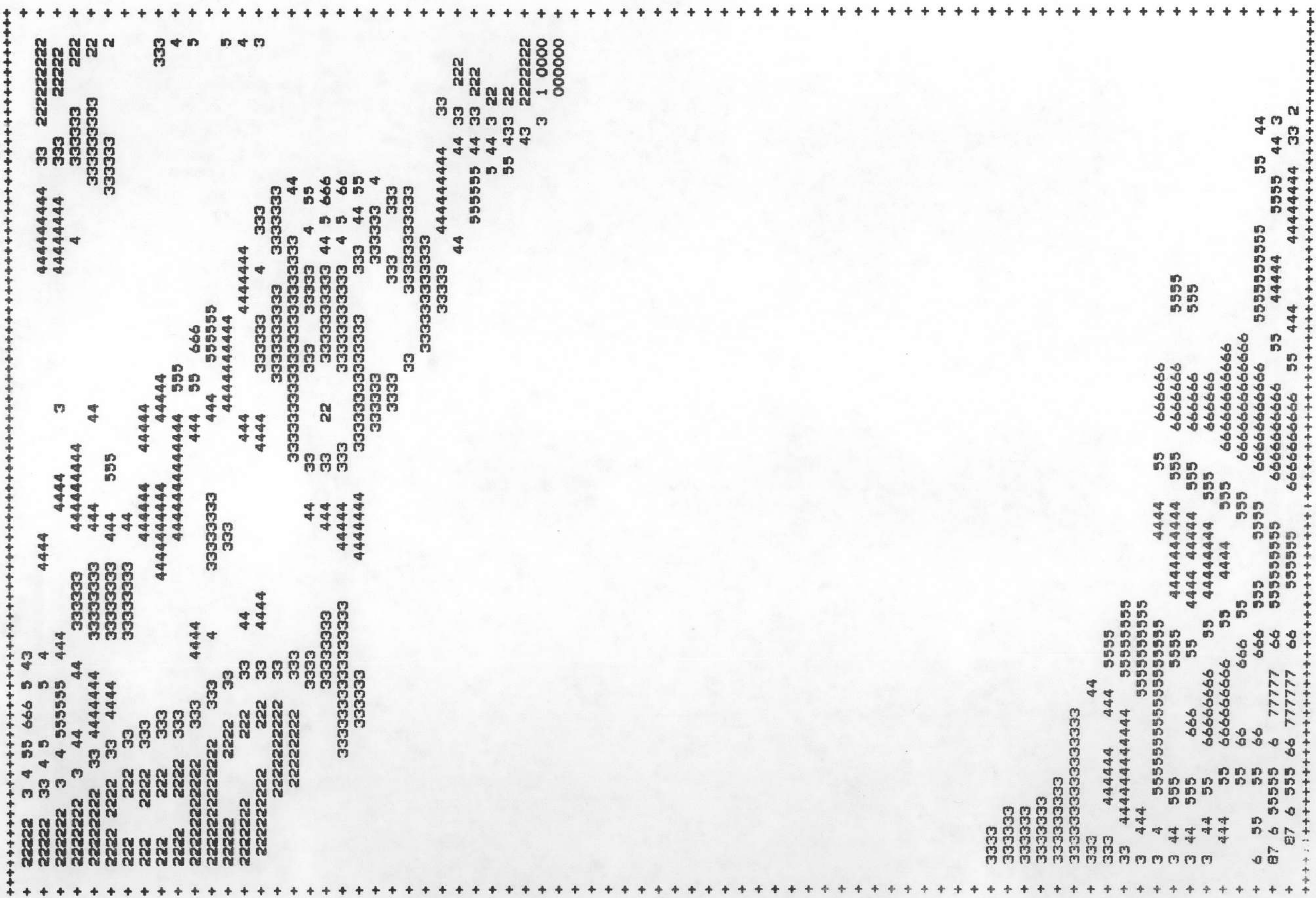
MANITOWOC



PRINT CHARACTER		EXPLANATION	VALUE
0	LE		0.0000
1			0.0500
2			0.1000
3			0.1500
4			0.2000
5			0.2500
6			0.3000
7			0.3500
8			0.4000
9			0.4500
	GT		0.9000

Uranium/Thorium Pseudo-Contour Map - Manitowoc Quadrangle

MANITOWOC

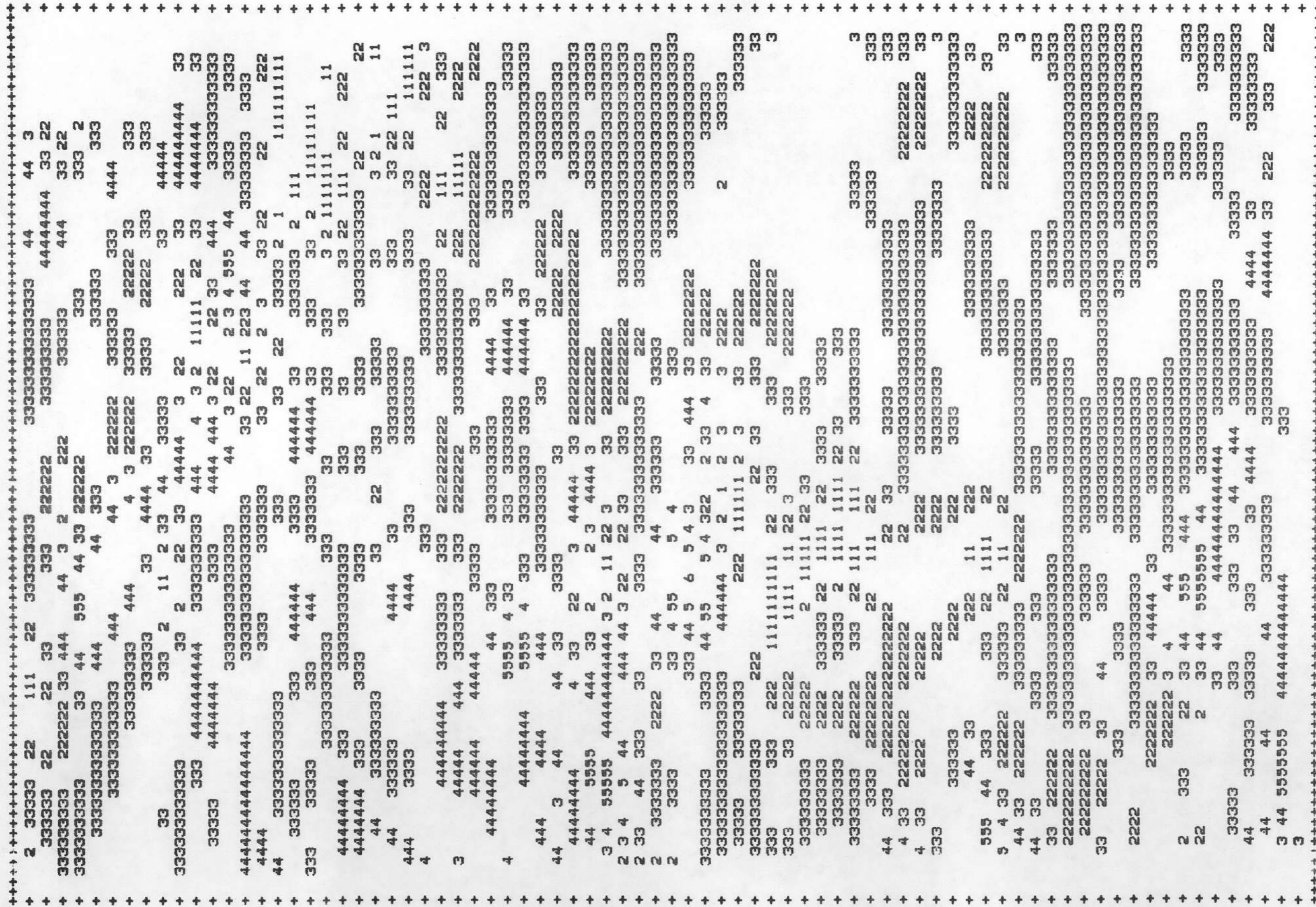


EXPLANATION

PRINT CHARACTER	VALUE
0	LE-1200.0000
-1200.0000-1100.0000	
1-1100.0000-1000.0000	
-1000.0000 -900.0000	
2 -900.0000 -800.0000	
-800.0000 -700.0000	
3 -700.0000 -600.0000	
-600.0000 -500.0000	
4 -500.0000 -400.0000	
-400.0000 -300.0000	
5 -300.0000 -200.0000	
-200.0000 -100.0000	
6 -100.0000 0.0000	
0.0000 100.0000	
7 100.0000 200.0000	
200.0000 300.0000	
8 300.0000 400.0000	
400.0000 500.0000	
9 500.0000 600.0000	
GT 600.0000	

SCALE IN GAMMAS

TRAVERSE CITY



EXPLANATION

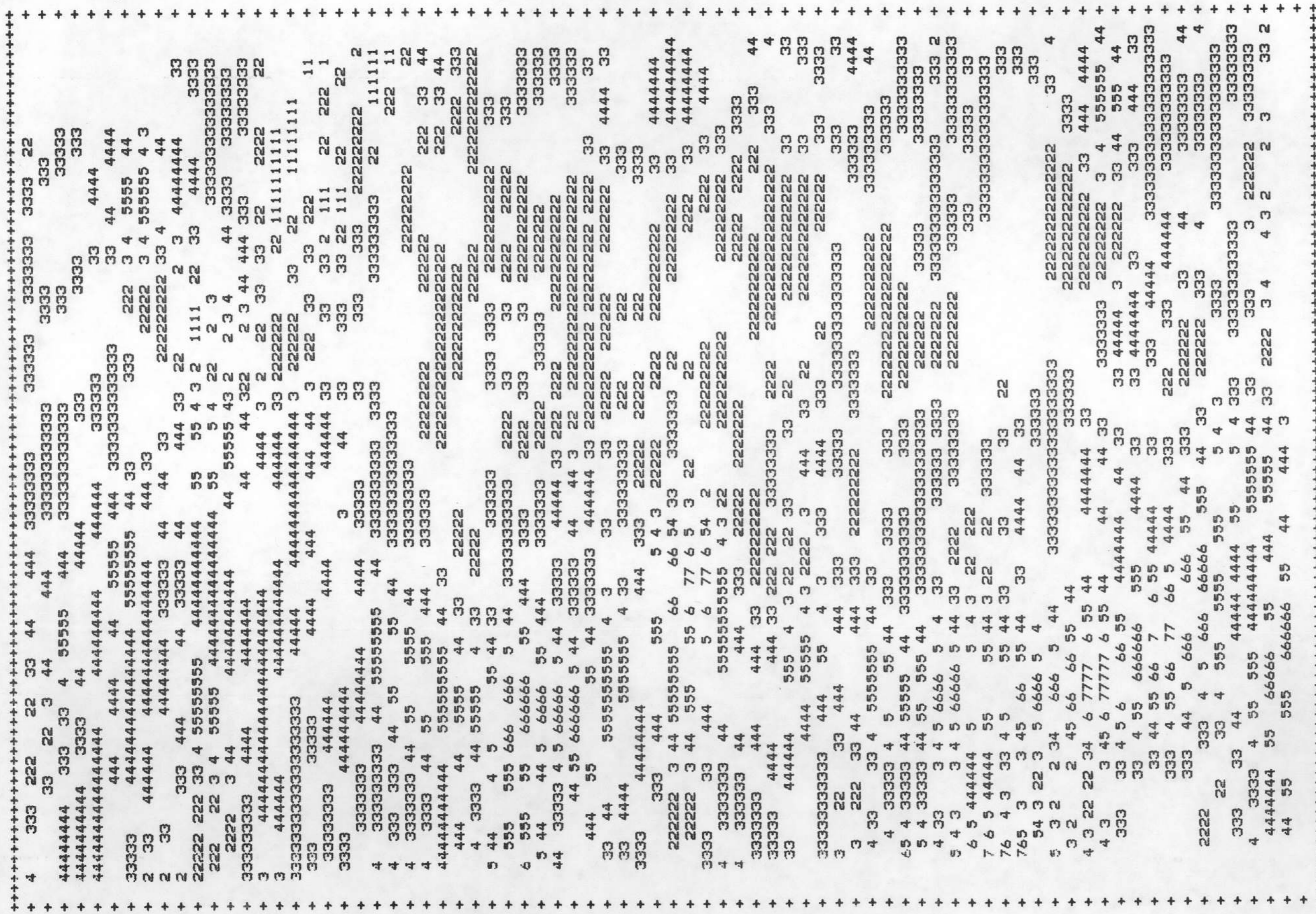
PRINT CHARACTER	VALUE
0	LE 0.0000
1	0.0000 0.1250 0.2500 0.3750 0.5000 0.6250 0.7500 0.8750 1.0000 1.1250 1.2500 1.3750 1.5000 1.6250 1.7500 1.8750 2.0000 2.1250 2.2500
2	0.0000 0.1250 0.2500 0.3750 0.5000 0.6250 0.7500 0.8750 1.0000 1.1250 1.2500 1.3750 1.5000 1.6250 1.7500 1.8750 2.0000 2.1250 2.2500
3	0.0000 0.1250 0.2500 0.3750 0.5000 0.6250 0.7500 0.8750 1.0000 1.1250 1.2500 1.3750 1.5000 1.6250 1.7500 1.8750 2.0000 2.1250 2.2500
4	0.0000 0.1250 0.2500 0.3750 0.5000 0.6250 0.7500 0.8750 1.0000 1.1250 1.2500 1.3750 1.5000 1.6250 1.7500 1.8750 2.0000 2.1250 2.2500
5	0.0000 0.1250 0.2500 0.3750 0.5000 0.6250 0.7500 0.8750 1.0000 1.1250 1.2500 1.3750 1.5000 1.6250 1.7500 1.8750 2.0000 2.1250 2.2500
6	0.0000 0.1250 0.2500 0.3750 0.5000 0.6250 0.7500 0.8750 1.0000 1.1250 1.2500 1.3750 1.5000 1.6250 1.7500 1.8750 2.0000 2.1250 2.2500
7	0.0000 0.1250 0.2500 0.3750 0.5000 0.6250 0.7500 0.8750 1.0000 1.1250 1.2500 1.3750 1.5000 1.6250 1.7500 1.8750 2.0000 2.1250 2.2500
8	0.0000 0.1250 0.2500 0.3750 0.5000 0.6250 0.7500 0.8750 1.0000 1.1250 1.2500 1.3750 1.5000 1.6250 1.7500 1.8750 2.0000 2.1250 2.2500
9	0.0000 0.1250 0.2500 0.3750 0.5000 0.6250 0.7500 0.8750 1.0000 1.1250 1.2500 1.3750 1.5000 1.6250 1.7500 1.8750 2.0000 2.1250 2.2500

Potassium Pseudo-Contour Map - Traverse City Quadrangle

SCALE IN EQUIVALENT PERCENT

6T

TRAVERSE CITY



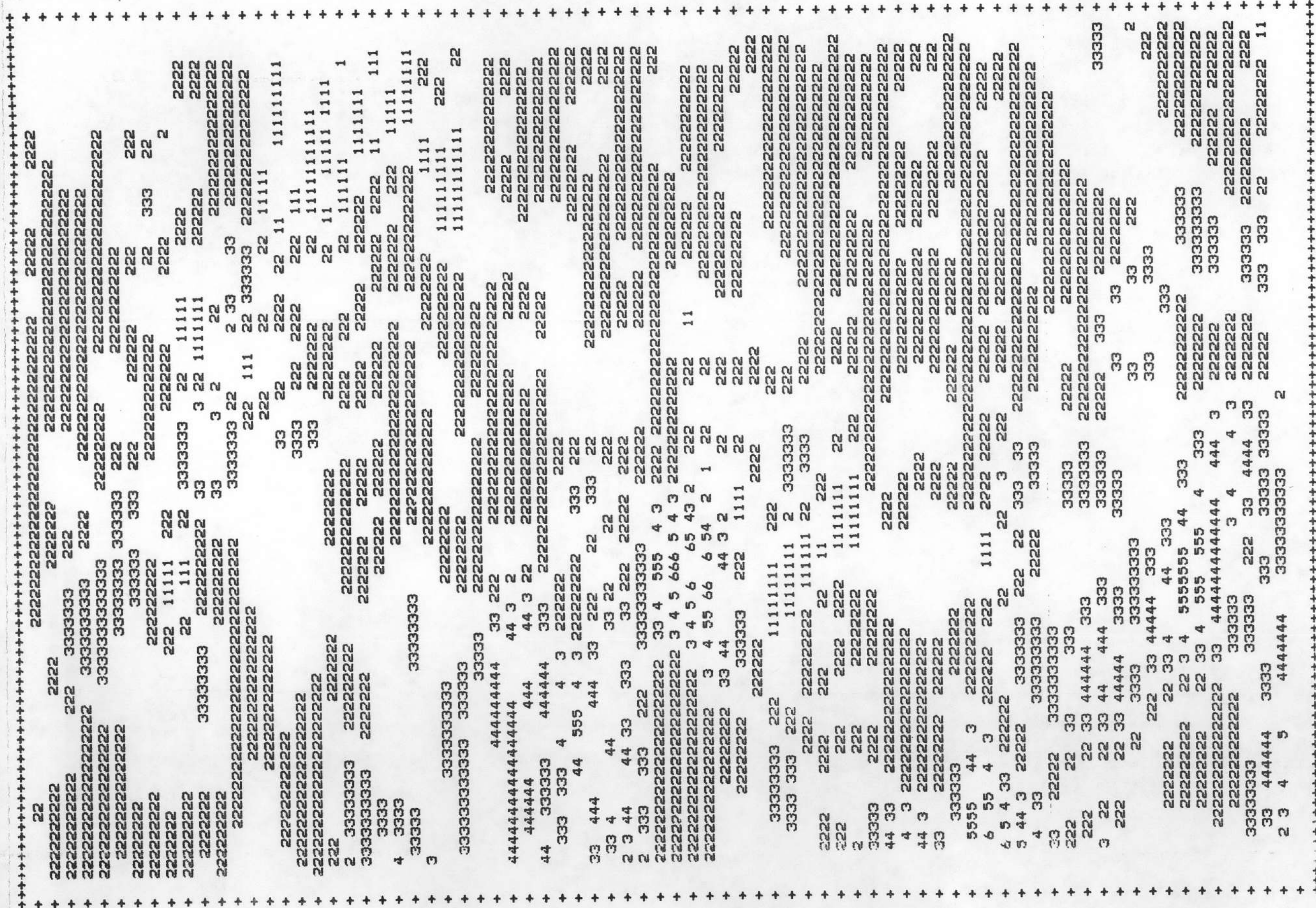
Uranium Pseudo-Contour Map - Traverse City Quadrangle

PRINT CHARACTER	EXPLANATION	VALUE
0	LE	0.0000
1		0.1000
2		0.2000
3		0.3000
4		0.4000
5		0.5000
6		0.6000
7		0.7000
8		0.8000
9		0.9000
		1.0000
		1.1000
		1.2000
		1.3000
		1.4000
		1.5000
		1.6000
		1.7000
		1.8000
GT		1.8000

SCALE IN EQUIVALENT PPM



TRAVERSE CITY

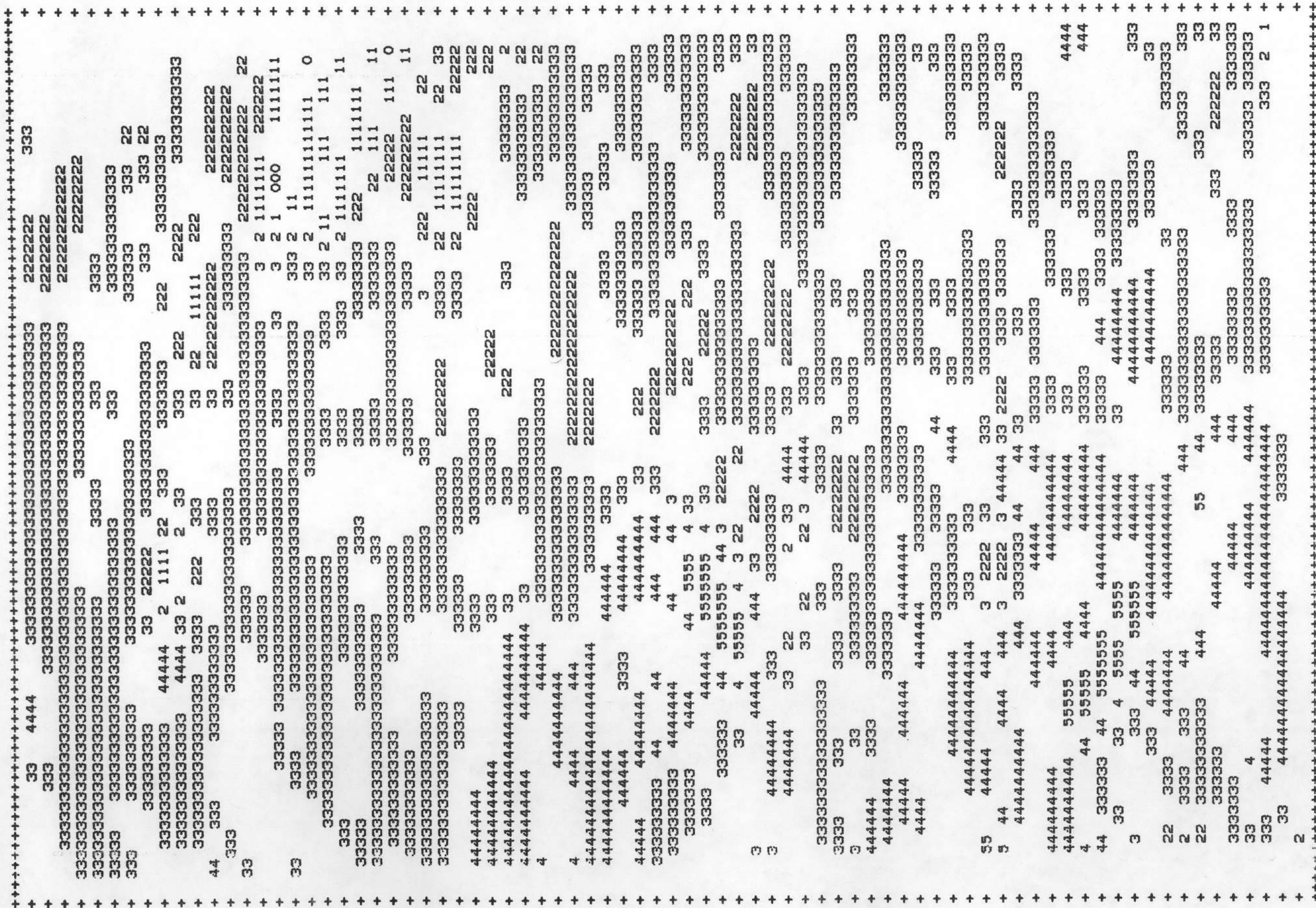


PRINT CHARACTER		EXPLANATION	VALUE
0	LE		0.0000
1	0.0000		0.3750
2	0.3750		0.7500
3	0.7500		1.1250
4	1.1250		1.5000
5	1.5000		1.8750
6	1.8750		2.2500
7	2.2500		2.6250
8	2.6250		3.0000
9	3.0000		3.3750
	3.3750		3.7500
	3.7500		4.1250
	4.1250		4.5000
	4.5000		4.8750
	4.8750		5.2500
	5.2500		5.6250
	5.6250		6.0000
	6.0000		6.3750
	6.3750		6.7500
	6T		6.7500

Thorium Pseudo-Contour Map - Traverse City Quadrangle

SCALE IN EQUIVALENT PPM

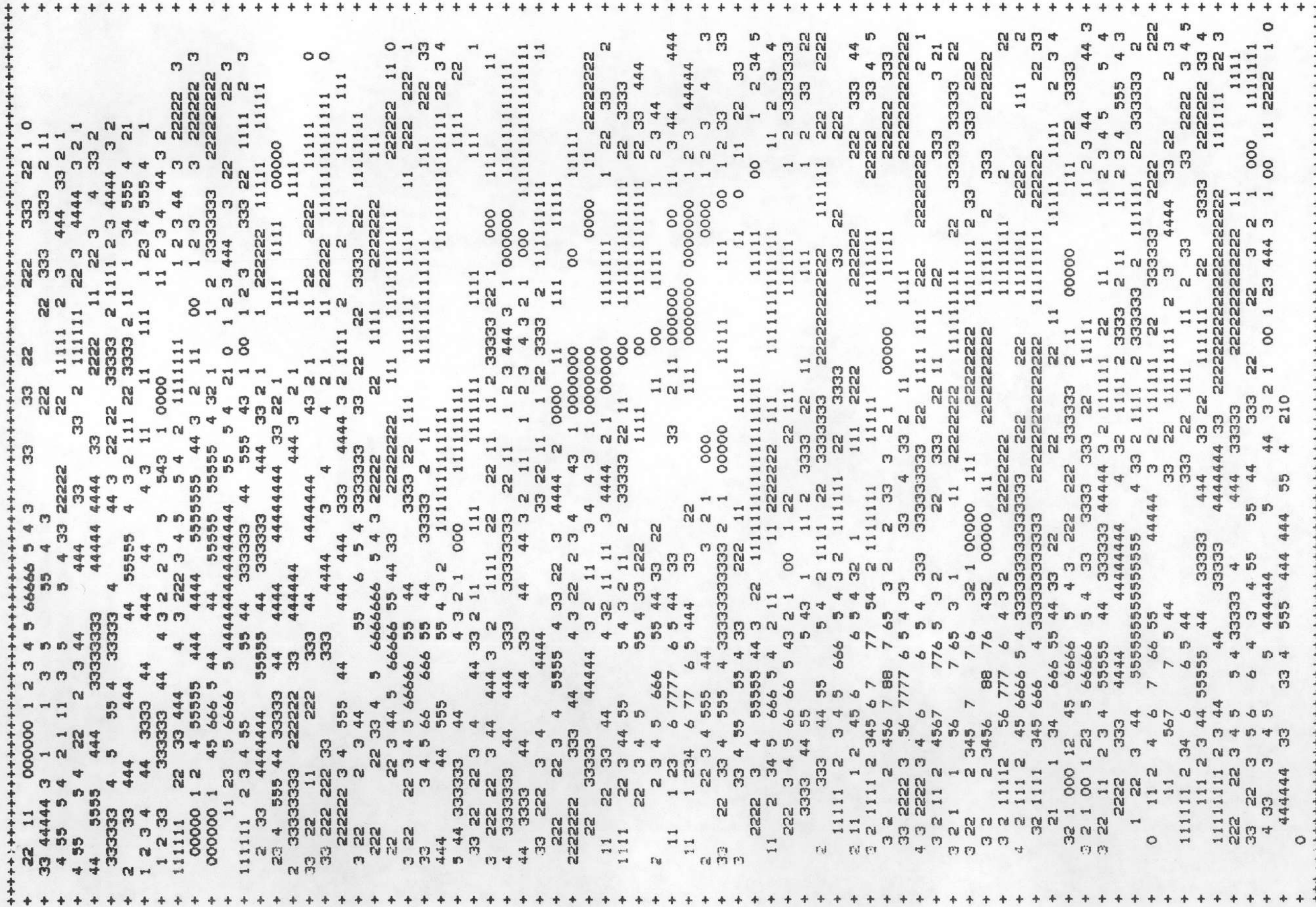
TRAVERSE CITY



PRINT CHARACTER		EXPLANATION
0	LE	0.0000
1	0.0000	0.3750
1	0.3750	0.7500
2	0.7500	1.1250
2	1.1250	1.5000
3	1.5000	1.8750
3	1.8750	2.2500
4	2.2500	2.6250
4	2.6250	3.0000
5	3.0000	3.3750
5	3.3750	3.7500
6	3.7500	4.1250
6	4.1250	4.5000
7	4.5000	4.8750
7	4.8750	5.2500
8	5.2500	5.6250
8	5.6250	6.0000
9	6.0000	6.3750
9	6.3750	6.7500
GT	6.7500	

Thorium/Potassium Pseudo-Contour Map - Traverse City Quadrangle

TRAVERSE CITY

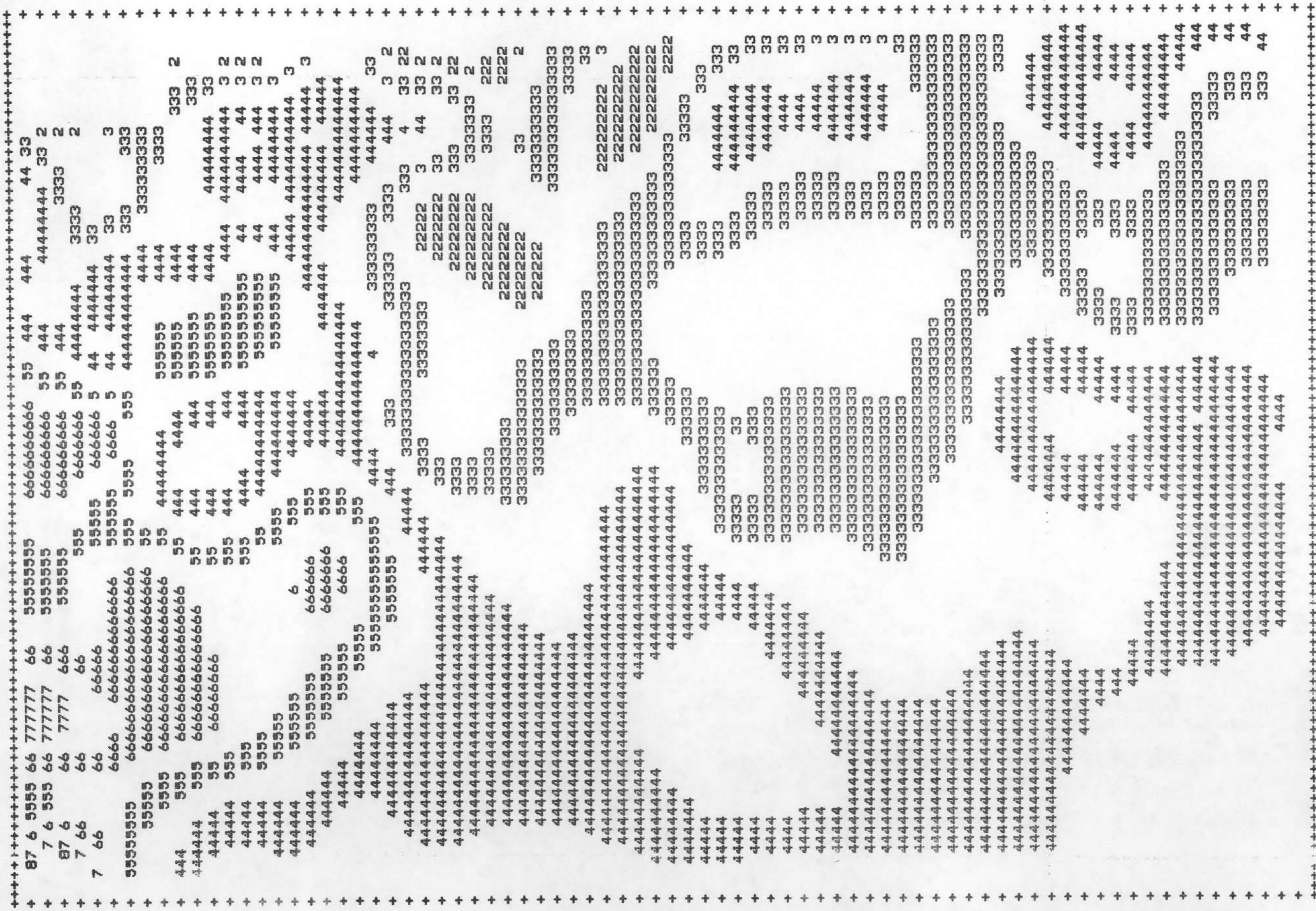


EXPLANATION

PRINT CHARACTER	VALUE
0	LE 0.0000
1	0.0500 0.1000
2	0.1000 0.1500
3	0.1500 0.2000
4	0.2000 0.2500
5	0.2500 0.3000
6	0.3000 0.3500
7	0.3500 0.4000
8	0.4000 0.4500
9	0.4500 0.5000
	0.5000 0.5500
	0.5500 0.6000
	0.6000 0.6500
	0.6500 0.7000
	0.7000 0.7500
	0.7500 0.8000
	0.8000 0.8500
	0.8500 0.9000
GT	0.9000

Uranium/Thorium Pseudo-Contour Map - Traverse City Quadrangle

TRAVERSE CITY



EXPLANATION

PRINT CHARACTER	VALUE
0	LE-1200. 0000
-	-1200. 0000-1100. 0000
1-	1100. 0000-1000. 0000
-	-1000. 0000 -900. 0000
2-	900. 0000 -800. 0000
-	-800. 0000 -700. 0000
3-	700. 0000 -600. 0000
-	-600. 0000 -500. 0000
4-	500. 0000 -400. 0000
-	-400. 0000 -300. 0000
5-	300. 0000 -200. 0000
-	-200. 0000 -100. 0000
6-	100. 0000 0. 0000
-	0. 0000 100. 0000
7	100. 0000 200. 0000
8	300. 0000 400. 0000
9	500. 0000 600. 0000
GT	600. 0000

Residual Magnetic Pseudo-Contour Map - Traverse City Quadrangle

SCALE IN GAMMAS



