

GENERALIZED DIFFUSION THEORY OF MICROMORPHICLY DEFORMABLE PARTICLE-FLUID CONTINUUM AND BUBBLE-LIQUID TWO-PHASE FLOWS

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ABSTRACT. In the paper [1] the basic concepts and equations were derived for the micromorphically deformable particle-fluid two-phase flows, the constitutive equations have been constructed. The flow of fluid with deformable spherical particles, when the particle only expands radially, rotates and translates, is considered in this paper. For this case one can obtain the full motion's equations system. These equations together with the constitutive equations are sufficient to determine all of unknowns, and they can be used to study the bubble-liquid two-phase flow. The problems of kinematic wave and acoustic wave propagation in the bubble-liquid two-phase flow is studied.

INTRODUCTION

The problem of multiphase flow of fluids or gases with deformable particles is attracting the great attention of scientists.

In the paper [1] a general continuum theory has been developed for two-phase flows of fluid with deformable particles, where the relative motion between phases and the micro-deformation of particles are taken into account.

In this paper the generalized diffusion theory, developed in [2] has been used to study the relative motion between constituent phases. The micromotion has been taken into account by generalizing the Eringen's theory [3, 4] of mixtures for micromorphic materials, where the micromotion of particles is considered as simple micromotion, but the micromotion of carrier fluid is kinematically dependent of particles micromotion and it is determined by extending the theory of potential motion of fluid with moving and deformable bodies [5].

The simplest case of developed theory, when the particles of spherical form only expand radially, rotate and translate is considered now.

1. THE MOTION EQUATIONS SYSTEM

We will consider two-phase flows of a liquid with deformable spherical particles. Suppose that during a micro-deformation process a particle can only expand radially, rotate and translate. It means [1]

$$\begin{aligned}\bar{\nu} &= \nu_0 \bar{G} + \bar{\nu}_1 \cdot \bar{E}, \\ \bar{I} &= I_0 \bar{G}\end{aligned}\tag{1.1}$$

where $\bar{\nu}$ is tensor of micro-velocity gradient, characterizing the deformation rate of the micro-volume of particle, $\bar{\nu}_0$ - scalar, characterizing the radial extension rate of particle, $\bar{\nu}_1$ - vector of particle rotation velocity, \bar{G} - unit tensor of 2nd order, \bar{E} - permutation tensor, \bar{I} - tensor, characterizing the micro-inertia of particle of arbitrary form, I_0 - scalar, characterizing the micro-inertia of spherical particle.

In this case it can be shown [1] that Φ - the potential of fluid micro-motion induced in a moving spherical particle has a form:

$$\begin{aligned}\Phi &= (\bar{U}_1 - \bar{U}_2) \cdot \bar{\Phi}_u + \nu_0 \Phi_{\nu_0}, \\ \bar{\Phi}_u &= -\frac{1}{2} \bar{\xi} \frac{R^3}{r^3}, \\ \Phi_{\nu_0} &= -\frac{R^3}{r}, \quad r = |\bar{\xi}|.\end{aligned}\tag{1.2}$$

In the expressions (1.2) \bar{U}_1 and \bar{U}_2 are translating velocity vector of particles and liquid respectively, $\bar{\Phi}_u$ - potential of fluid micro-motion induced in a translation of spherical particle, Φ_{ν_0} - a radially extension, R - radius of particle, $\bar{\xi}$ - relative position vector of the considered fluid point with respect to the position of center mass of particle, r - its absolute value.

Taking into account the results of [1] we can obtain the following expressions for the generalized induced mass tensors

$$\begin{aligned}\bar{M} &= M_0 \bar{G}, \quad M_0 = \frac{2}{3} \pi R^3 \rho_2; \\ \bar{L} &= 0; \\ \bar{N} &= N_0 \bar{G} \bar{G}, \quad N_0 = \frac{4}{3} \pi R^5 \rho_2;\end{aligned}\tag{1.3}$$

where ρ_2 - mass density of liquid.

It can be shown that I_0 has the form

$$I_0 = \frac{4}{3} \pi R^5 \rho_1\tag{1.4}$$

where ρ_1 - mass density of particle.

The micro-pressure tensor $\bar{\pi}^*$ can be written in the form

$$\bar{\pi}^* = \pi_0^* \bar{G}\tag{1.5}$$

Then, we obtain the following motion equations system

$$\begin{aligned}\frac{d^{(a)} n}{dt} + n(\bar{\nabla} \cdot \bar{U}_a) &= -\bar{\nabla} \cdot \left(n \frac{\bar{J}^a}{\rho_1^*} \right), \\ \frac{d^{(a)} \rho}{dt} + \rho(\bar{\nabla} \cdot \bar{U}_a) &= -\bar{\nabla} \cdot \left(1 - \frac{a_1 \rho_2^*}{a_2 \rho_1^*} \right) \bar{J}^a, \\ \frac{d^{(a)}}{dt} (\rho_1 \varphi) + \rho_1 \varphi (\bar{\nabla} \cdot \bar{U}_a) &= -\bar{\nabla} \cdot \bar{J}^a, \\ \rho \frac{d^{(a)} \bar{U}_a}{dt} &= \rho \bar{f} - \bar{\nabla} p + \bar{\nabla} \tau_0 - \bar{\nabla} \times \bar{\tau}_1^a + \bar{\nabla} \cdot \bar{\tau}_2^a - \\ &\quad - \frac{D^{(a)}}{Dt} \left(\frac{a_2 \rho_1^* - a_1 \rho_2^*}{a_2 \rho_1^*} \bar{J}^a \right) - \bar{\nabla} \cdot \left[\frac{\bar{J}^a \bar{J}^a}{\rho_1^*} \left(1 + \frac{a_1^2 \rho_2^*}{a_2^2 \rho_1^*} \right) \right],\end{aligned}$$

$$\begin{aligned}
& \frac{a_2^2 \rho_1^* + a_1^2 \rho_2^*}{a_2^2 \rho_1^*} \frac{D^{(a)} \bar{J}^a}{Dt} + \frac{a_2^3 \rho_1^* - a_1^3 \rho_2^*}{a_2^3 \rho_1^*} \bar{\nabla} \cdot \left(\frac{\bar{J}^a \bar{J}^a}{\rho_1^*} \right) + \frac{a_1}{a_2} \bar{J}^a \frac{d^{(a)}}{dt} \left(\frac{a_1 \rho_2^*}{a_2 \rho_1^*} \right) - \\
& - \frac{a_1}{a_2} \frac{\bar{J}^a}{\rho_1^*} (\bar{J}^a \cdot \bar{\nabla}) \left(\frac{a_1^2 \rho_2^*}{a_2^2 \rho_1^*} \right) + n \left(1 + \frac{a_1}{a_2} \right) M_0 \left\{ \frac{d^{(a)}}{dt} \left[\left(1 + \frac{a_1}{a_2} \right) \frac{\bar{J}^a}{\rho_1^*} \right] + \right. \\
& + \left. \left(\frac{\bar{J}^a}{\rho_1^*} \cdot \bar{\nabla} \right) \left[\left(1 + \frac{a_1}{a_2} \right) \frac{\bar{J}^a}{\rho_1^*} \right] \right\} + \frac{n}{2} \left[\frac{d^{(a)} M_0}{dt} + \left(\frac{\bar{J}^a}{\rho_1^*} \cdot \bar{\nabla} \right) M_0 \right] \bar{J}^a = \\
& = \rho_1^* \left(\bar{f}_1 - \frac{a_1 \rho_2^*}{a_2 \rho_1^*} \bar{f}_2 \right) - \rho_1^* \left(1 - \frac{a_1 \rho_2^*}{a_2 \rho_1^*} \right) \frac{d^{(a)} \bar{U}_a}{dt} - \\
& - \rho_1^* \left(1 + \frac{a_1}{a_2} \right) (\bar{\nabla} \mu_1)_{p, \pi_0, T} - \varphi \left[1 - \frac{a_1 (1 - \varphi)}{a_2 \varphi} \right] \bar{\nabla} p - \\
& - \rho_1^* \left(1 - \frac{\rho}{\rho_1^*} - \frac{a_1 \rho_2^*}{a_2 \rho_1^*} \right) (\bar{\nabla} I_0) \pi_0 - \rho_1^* \bar{F}_a^*; \tag{1.6}
\end{aligned}$$

$$\begin{aligned}
& n N_0 \left(\frac{d^{(a)} \nu_0}{dt} + \frac{5}{2} \nu_0 \right) + n I_0 \left(\frac{d^{(a)} \nu_0}{dt} + \nu_0^2 \right) + n (N_0 + I_0) \left(\frac{\bar{J}^a}{\rho_1^*} \cdot \bar{\nabla} \right) \nu_0 = \\
& = \rho_1^* \bar{\ell}_0 + \pi_0^* - \chi_0 + \bar{\nabla} \cdot \bar{\lambda}_{12}, \\
& n I_0 \left(\frac{d^{(a)} \bar{\nu}_1}{dt} + \nu_0 \bar{\nu}_1 \right) + n I_0 \left(\frac{\bar{J}^a}{\rho_1^*} \cdot \bar{\nabla} \right) \bar{\nu}_1 = \\
& = \rho_1^* \bar{\ell}_1 + \bar{\tau}_1^a + \bar{\nabla} \lambda_0 - \frac{1}{2} \bar{\nabla} \times \bar{\lambda}_{11} + \bar{\nabla} \cdot \bar{\lambda}_{21};
\end{aligned}$$

In the equations system (1.6), the first is particle number conservation equation, the 2nd - mixture mass conservation, 3th - particle mass conservation, 4th - mixture momentum balance, 5th - particle generalized diffusion, 6th - particle volume change, 7th - particle rotation one.

In obtaining equations (1.6) we suppose that

$$\begin{aligned}
\rho_2 &= \text{const}; \\
\frac{4}{3} \pi R^3 \rho_1 &= \text{const}; \tag{1.7}
\end{aligned}$$

Moreover we have the following relationships

$$\begin{aligned}
\nu_0 &= \frac{1}{R} \left[\frac{d^{(a)} R}{dt} + \left(\frac{\bar{J}^a}{\rho_1^*} \cdot \bar{\nabla} \right) R \right]; \\
\varphi &= \frac{4}{3} \pi R^3 n. \tag{1.8}
\end{aligned}$$

In (1.6) - (1.8) n is number of particles in a unit volume of the flow; \bar{U}_a - certain characteristic mean velocity, expressed linearly in terms of liquid and particles velocities by some system of normalized weighing factors a_k ; \bar{J}^a - generalized diffusion flux of particles; ρ_1^* and ρ_2^* - fictive mass densities of particle and liquid respectively; ρ - mean mass density of mixture; φ - volume concentration of particles; \bar{f} - density of the external body force acting on mixture; \bar{f}_1 and \bar{f}_2 - density of the external body force acting on particles and liquid respectively; μ_1 - generalized chemical potential; p - thermodynamical pressure; $\bar{\tau}_1^a$, $\bar{\tau}_2^a$, $\bar{F} - a^*$, χ_0 , λ_0 , $\bar{\lambda}_{11}$, $\bar{\lambda}_{12}$, $\bar{\lambda}_{21}$ - generalized thermodynamical forces; $d^{(a)}/dt$ - full time derivative determining the change over time with respect to a coordinate system moving at the characteristic velocity \bar{U}_a ; the operator $D^{(a)}/Dt$ - time derivative determining the change over time with respect to a generalized Lagrangian coordinate system moving and deforming at velocity \bar{U}_a [1]; the operator (\cdot) - scalar product and (\times) - vector product between two closest indices of tensor quantities.

Together with the constitutive equations [1], the equations system (1.6) - (1.8) can be considered as the equations of motion of the fluid-deformable spherical particle two-phase media. In particular they can be used for predicting the bubble-liquid two-phase flows. This equations system will be analyzed in the next chapter.

2. SIMPLE CASED OF BUBBLE-LIQUID TWO-PHASE FLOWS

a) Case 1:

Consider the case when there is no relative motion between phases, the spherical particle only expands radially, the liquid mass density and the total mass of a particle are constant, the motion is isothermal, and the dissipative terms can be neglected. Then, it can be shown that the equations of motion have the form

$$\begin{aligned}
 \frac{dn}{dt} + n \bar{\nabla} \cdot \bar{U} &= 0; \\
 \frac{d}{dt}(\rho_1 \varphi) + \rho_1 \varphi (\bar{\nabla} \cdot \bar{U}) &= 0; \\
 \varphi &= \frac{4}{3} \pi R^3 n; \quad \rho_2 = \text{const}; \\
 \frac{4}{3} \pi R^3 \rho_1 &= \text{const}; \quad \frac{d}{dt}(\dots) = \frac{\partial}{\partial t}(\dots) + (\bar{U} \cdot \bar{\nabla})(\dots), \\
 \frac{d\bar{U}}{dt} &= \rho \bar{f} - \bar{\nabla} p; \\
 \frac{4}{3} \pi R^3 n \rho_2 \left[R \frac{d^2 R}{dt^2} + \frac{3}{2} \left(\frac{dR}{dt} \right)^2 \right] + \frac{4}{3} \pi R^3 n \rho_1 \frac{R d^2 R}{dt^2} &= \pi_0^*.
 \end{aligned} \tag{2.1}$$

In (2.1) the last equation determines the change of the particle radius R . It is necessary to note that the micropressure π_0^* has to be determined by giving a concrete form of the internal energy of two-phase flow [1]. But, here in comparing with the Rayleigh's equation [6] we can set

$$\pi_0^* = \frac{4}{3} \pi R^3 n = \left(p_1 - p - \frac{2\sigma}{R} \right) \tag{2.2}$$

where p_1 is the gas (or vapor) pressure inside a particle, σ - the surface tension.

In addition, it is necessary to consider the equation of state for the gas (or vapor) inside the particle. As usual [6], we may assume the following state equation

$$\frac{p_1}{\rho_1} = \text{const} \tag{2.3}$$

Equations (2.1) - (2.3) are sufficient to determine all the unknowns.

b. Case 2:

When there is no particle rotation, the mean - volume velocity of the two-phase. Flow is used, the volume concentration of particles is small, the mass density of gas (or vapor) can be neglected with respect to the liquid mass density, the dissipative terms in the momentum balance equation and the particle radial expansion equation can be neglected, then the equations of motion will have the following form

$$\begin{aligned}
 \frac{d^{(\nu)}}{dt}(\rho_1 \varphi) + \rho_1 \varphi \bar{\nabla} \cdot \bar{U}_\nu &= -\bar{\nabla} \cdot \bar{J}^\nu; \\
 \bar{\nabla} \cdot \bar{U}_\nu &= \frac{1}{1-\varphi} \left(\frac{d^{(\nu)} \varphi}{dt} + \bar{\nabla} \cdot \frac{\bar{J}^\nu}{\rho_1} \right);
 \end{aligned}$$

$$\begin{aligned}
(1-\rho)\rho_2 \frac{d^{(\nu)}\bar{U}_\nu}{dt} &= (1-\varphi)\rho_2\bar{g} - \bar{\nabla}p + \rho_2 \frac{R^{(\nu)}}{Dt} \left(\frac{\bar{J}^\nu}{\rho_1} \right); \\
\frac{d^{(\nu)}\bar{J}^\nu}{dt} + \left(\frac{\bar{J}^\nu}{\rho_1\varphi} \cdot \bar{\nabla} \right) \bar{J}^\nu &= -2\varphi\rho_1 \left(\bar{g} - \frac{d^{(\nu)}\bar{U}_\nu}{dt} \right) - \frac{2\varphi\rho_1^2}{\rho_2} (\bar{\nabla}\mu_1)_{p,\pi_0,T} - \frac{2\varphi\rho_1^2}{\rho_2} \alpha \bar{J}^\nu; \\
R\ddot{R} + \frac{3}{2}\dot{R}^2 + R \left(\frac{\bar{J}^\nu}{\rho_1\varphi} \cdot \bar{\nabla} \right) \dot{R} + \frac{3}{2} \left(\frac{\bar{J}^\nu}{\rho_1\varphi} \cdot \bar{\nabla} \right) R &= \frac{1}{\rho_2} \left(p_1 - p - \frac{2\sigma}{R} \right), \\
\varphi = \frac{4}{3}\pi R^3 n; \quad \frac{4}{3}\pi R^3 \rho_1 = \text{const}; \quad \frac{t_1}{\rho_1} &= \text{const}
\end{aligned} \tag{2.4}$$

where

$$\begin{aligned}
\bar{U}_\nu &= \varphi\bar{U}_1 + (1-\varphi)\bar{U}_2; \quad \bar{J}^\nu = \rho_1\varphi(\bar{U}_1 - \bar{U}_2); \\
\dot{R} &= \frac{d^{(\nu)}R}{dt}; \quad \ddot{R} = \frac{d^{(\nu)}\dot{R}}{dt}; \quad \frac{d^{(\nu)}}{dt}(\dots) = \frac{\partial}{\partial t}(\dots) + (\bar{U}_\nu \cdot \bar{\nabla})(\dots); \\
\frac{D^{(\nu)}}{Dt}(\dots) &= \frac{d^{(\nu)}}{dt}(\dots) + [(\dots) \cdot \bar{\nabla}]\bar{U}_\nu + (\dots)(\bar{\nabla} \cdot \bar{U}_\nu);
\end{aligned} \tag{2.5}$$

3. THE PROPAGATION OF KINEMATIC WAVE AND ACOUSTIC WAVE IN THE BUBBLE-LIQUID TWO-PHASE FLOWS

To determine the velocities of a kinematic and acoustic waves propagation in the bubble-fluid two-phase flows we suppose that [4]

$$(\bar{\nabla}\mu_1)_{p,\pi_0,T} = 0, \quad p_1 = p$$

Then, the one-dimensional equation system (2.4) can be shown to have the following form

$$\begin{aligned}
\frac{\partial\varphi}{\partial t} + u \frac{\partial\varphi}{\partial x} + \frac{\varphi}{p} \frac{\partial p}{\partial t} + \frac{\varphi u}{p} \frac{\partial p}{\partial x} + \varphi \frac{\partial u}{\partial x} + \frac{1}{Ap} \frac{\partial J}{\partial x} &= 0, \\
\frac{\partial\varphi}{\partial t} + u \frac{\partial\varphi}{\partial x} - \frac{J}{Ap^2} \frac{\partial p}{\partial x} - (1-\varphi) \frac{\partial u}{\partial x} + \frac{1}{Ap} \frac{\partial J}{\partial x} &= 0, \\
\frac{J\rho_2}{Ap^2} \frac{\partial p}{\partial t} + \left(1 + \frac{\rho_2 u J}{Ap^2} \right) \frac{\partial p}{\partial x} + (1-\varphi)\rho_2 \frac{\partial u}{\partial t} + \left[(1-\varphi)\rho_2 u - \frac{2\rho_2 J}{Ap} \right] \frac{\partial u}{\partial x} - \\
- \frac{\rho_2}{Ap} \frac{\partial J}{\partial t} - \frac{\rho_2 u}{Ap} \frac{\partial J}{\partial x} &= (1-\varphi)\rho_2 g; \\
- 2\varphi Ap \frac{\partial u}{\partial t} - 2\varphi Ap u \frac{\partial u}{\partial x} + \frac{\partial J}{\partial t} + \left(u + \frac{J}{Ap\varphi} \right) \frac{\partial J}{\partial x} &= - \frac{2\varphi A^2 p^2}{\rho_2} \alpha J - 2\varphi Ap g,
\end{aligned} \tag{3.1}$$

where, we put $\frac{p_1}{\rho_1} = \frac{1}{A}$, $A = \text{const}$.

The characteristic equation of the system (3.1) has a form

$$(u-\lambda) \left[- \frac{\varphi(1-3\varphi)\rho_2}{p} (u-\lambda)^3 - \frac{(1-4\varphi)\rho_2 J}{Ap^2} (u-\lambda)^2 + \left(1 + \frac{\rho_2 J^2}{A^2 p^3} \right) (u-\lambda) + \frac{J}{Ap\varphi} \right] = 0 \tag{3.2}$$

From the equation (3.2) one can see that the first characteristic velocity of equations system (3.1) is equal

$$\lambda_1 = u \tag{3.3}$$

When there is no relative motion between bubbles and the carrier liquid (that means $J = \sigma$) from the characteristic equation (3.2) we can obtain the following characteristic velocities:

$$\lambda_{2,3}^0 = u \pm a_0, \quad (3.4)$$

where

$$a_0 = \sqrt{\frac{p}{\varphi(1-3\varphi)\rho_2}}; \quad (3.5)$$

It is obvious that a_0 is the velocity of acoustic wave propagation in motionless bubble-liquid two-phase media. It is coincided with the know result [6].

Taking into account of (3.3) and (3.5) the characteristic equation (3.2) can be transformed into following equation

$$Z^3 + \frac{1-4\varphi}{1-3\varphi}\varepsilon Z^2 - \left(1 + \frac{\varphi}{1-3\varphi}\varepsilon^2\right)Z - \varepsilon = 0 \quad (3.6)$$

where we put

$$Z = \frac{u-\lambda}{a_0}; \quad \varepsilon = \frac{J}{Ap\varphi a_0}; \quad (3.7)$$

In general the dimensionless parameter ε is small, and the equation (3.6) can be solved by the following expanding

$$Z = Z_0 + \varepsilon Z_1,$$

By this way it can be shown that the equation (3.6) has 3 following characteristic velocities

$$\begin{aligned} \lambda_{2,3} &= u + \frac{J}{2(1-3\varphi)\rho_1} \pm a_0, \\ \lambda_4 &= u - \frac{J}{(1-3\varphi)\rho_1}, \end{aligned} \quad (3.8)$$

From (3.8) the characteristic velocities $\lambda_{2,3}$ can be considered as the velocities of acoustic wave propagation, λ_4 - the velocity of kinematic wave propagation in bubble-liquid two-phase flows.

The problem of damping or amplification of these waves during the propagation in bubble-liquid two-phase flows will be the subject of further investigations.

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