

11-19-2019

## Investigations regarding the pumping process of wet-mix shotcrete improvement and upgrading of underground traffic structures

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### Recommended Citation

Johannes Flotzinger, Maria Thumann, Florian Steindl, Florian Mittermayr, Benedikt Lindlar, and Wolfgang Kusterle, "Investigations regarding the pumping process of wet-mix shotcrete improvement and upgrading of underground traffic structures" in "Shotcrete for Underground Support XIV", Matthias Beisler, ILF Consulting Engineers Asia, Ltd., Thailand Preedee Ngamsantikul, Thailand Underground and Tunneling Group (TUTG), Thailand Herbert Klapperich, TU Freiberg, Germany Eds, ECI Symposium Series, (2019). [https://dc.engconfintl.org/shotcrete\\_xiv/6](https://dc.engconfintl.org/shotcrete_xiv/6)

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# Investigations regarding the pumping process of wet-mix shotcrete

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# Outline

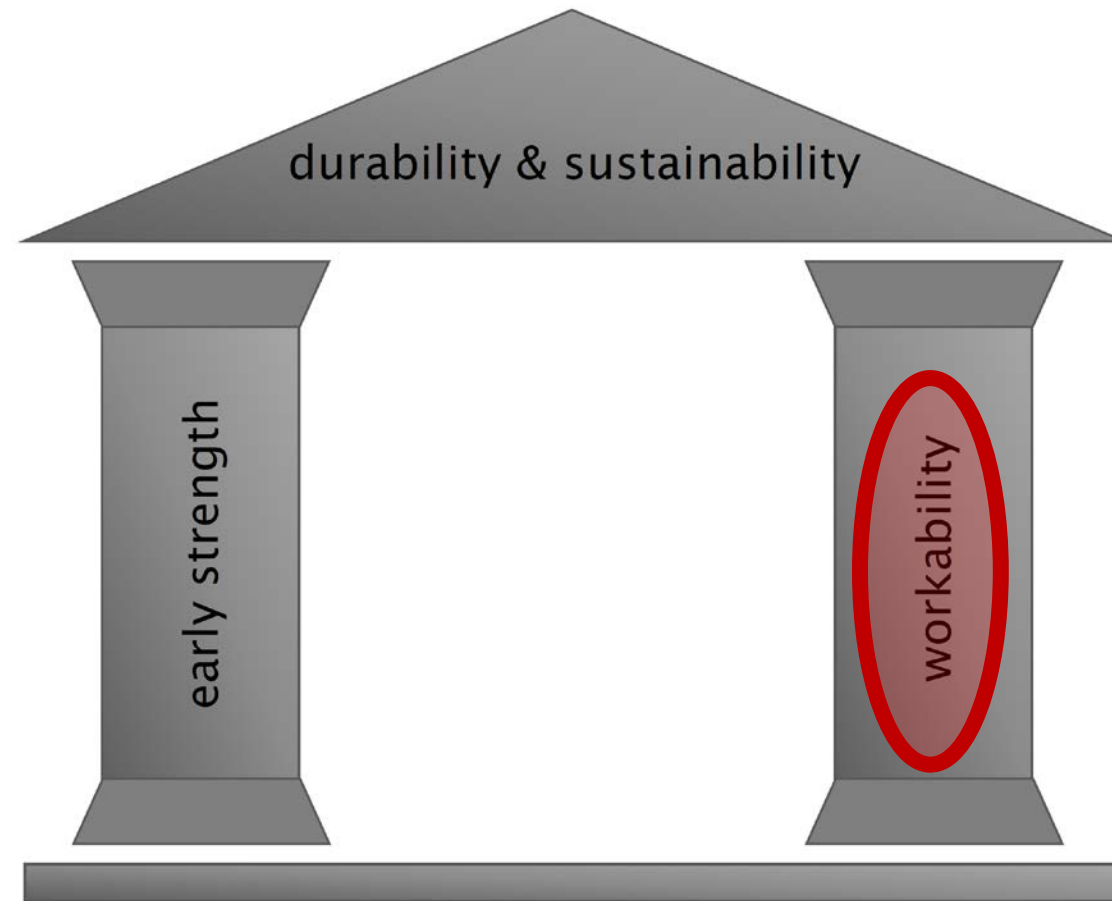
1. ASSpC
2. Stability and rheology
3. Shotcrete rig and sensors
4. Results
5. Resume
6. Outlook

# ASSpC (Advanced and Sustainable Sprayed Concrete)

- Increase of durability of construction/shotcrete
  - Use of sustainable materials
  - Reduction of environmental footprint
- Low maintenance costs
- Good life cycle performance



# ASSpC



# Goals

Fresh concrete tests:

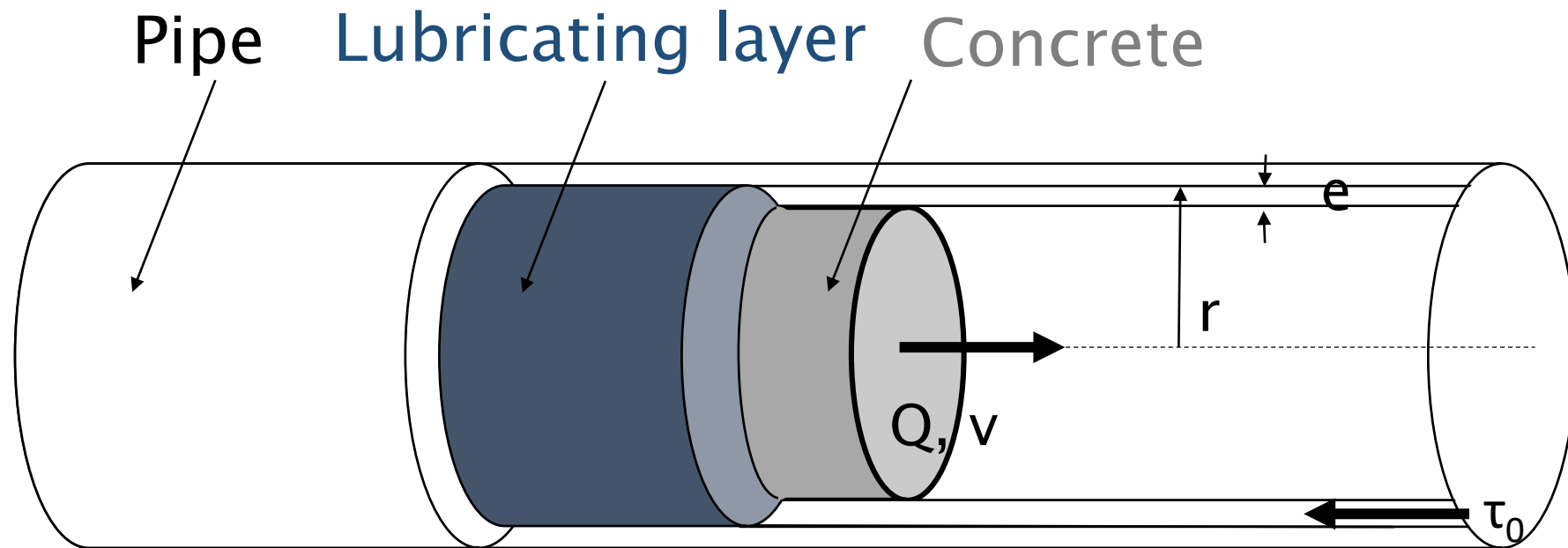
- What measurements can be made to determine the rheology and stability of the shotcrete?

Pressure tests:

- How do the flow rate and hence the pressures affect the quality of the spray pattern?

→ Can the pumping pressure be determined before the spraying process by fresh concrete properties?

# Schematic illustration



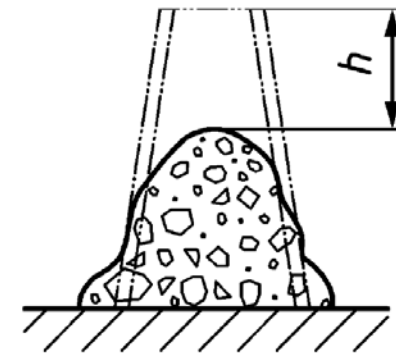
Source: Kasten, K.: Gleitrohr-Rheometer. Ein Verfahren zur Bestimmung der Fließeigenschaften von Dickstoffen in Rohrleitungen. Dissertation. Dresden 2009.



# Experimental setup

Common tests for describing the fresh concrete properties:

- Flow table spread or slump flow
- The Austrian guideline for shotcrete recommends a flow spread of  $600 \pm 50$  mm
- The segregation, the demand of water and the dosage of super-plasticiser must be taken into account
- Investigations of *Reinhold, Secrieru et al., Kasten, Jacobsen and Ngo* showed that flow spread and slump flow are insufficient for describing the pumpability of concrete



EN 12350-2:2019

# Test methods of the fresh concrete



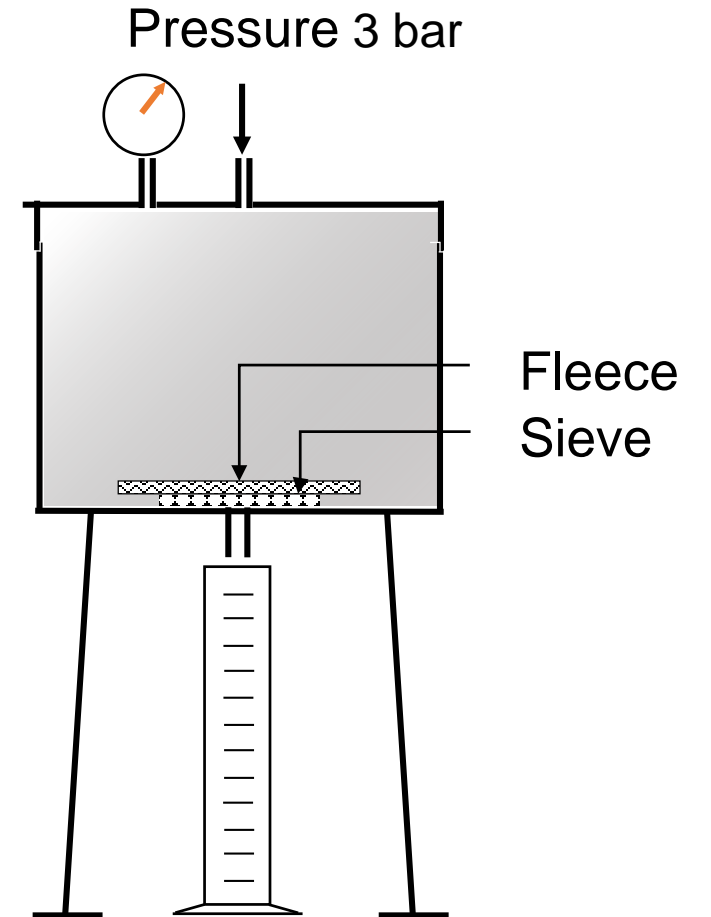
- Flow table spread
- Filter pressing test
- SLIPER (SLiding PipE Rheometer)

Flow table spread

# Stability



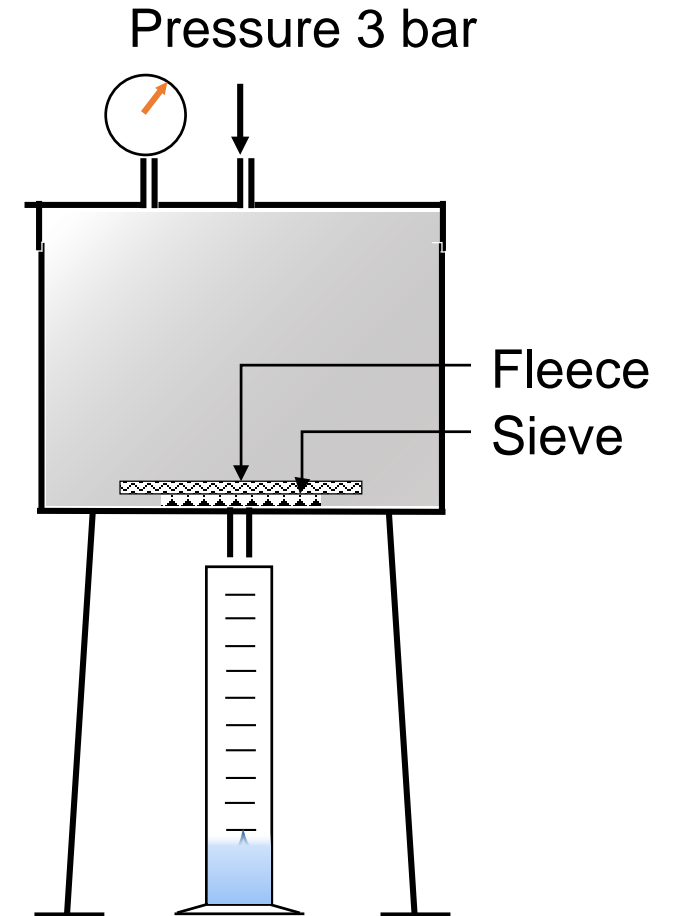
Filter press



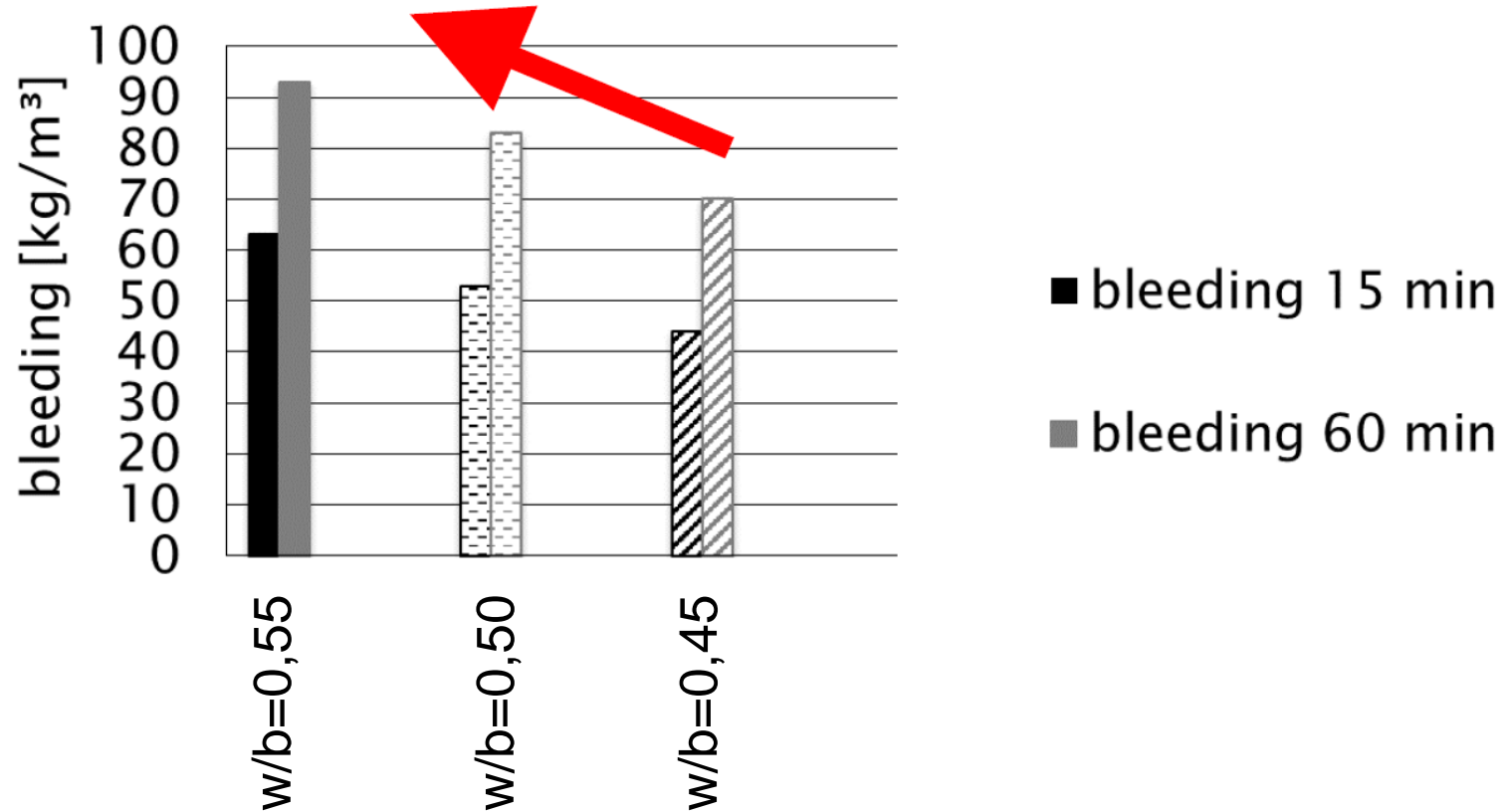
# Stability



Filter press



# Stability

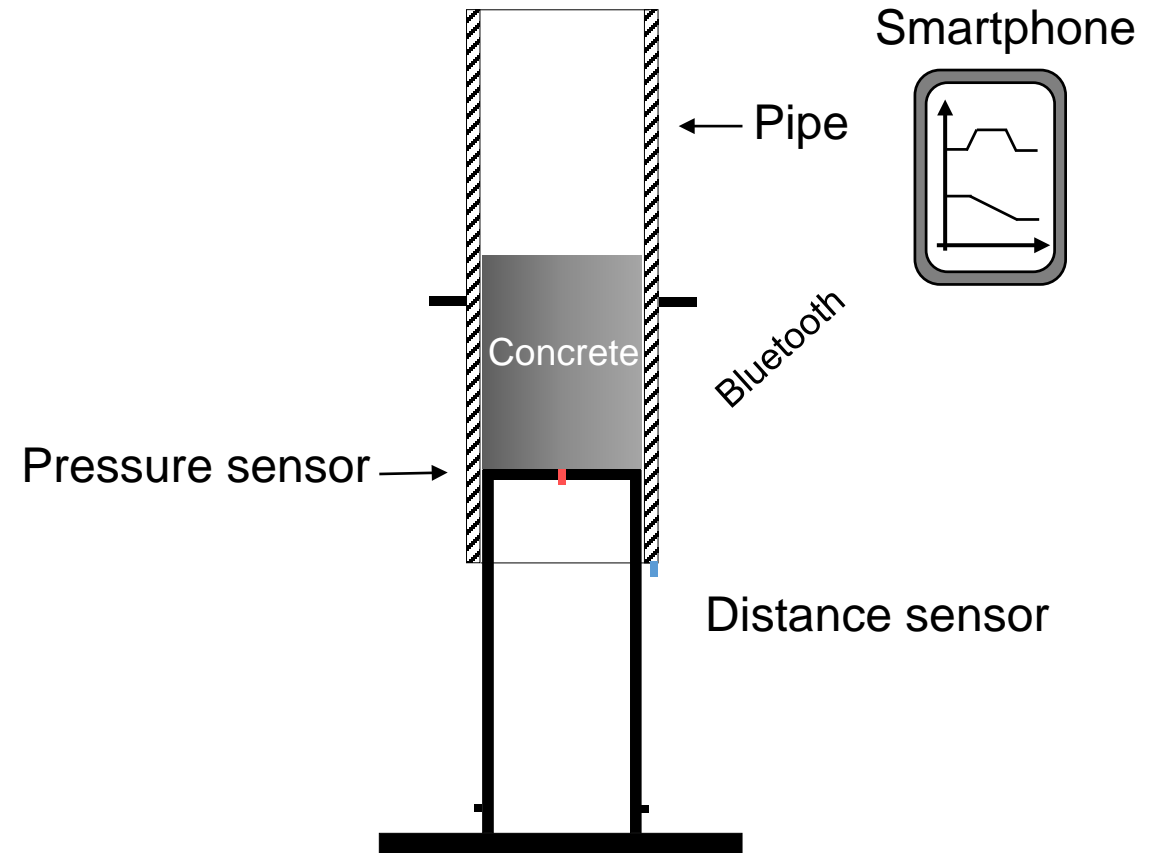


Filter press results at different w/b ratios

# SLIPER (SLIding PipE Rheometer)



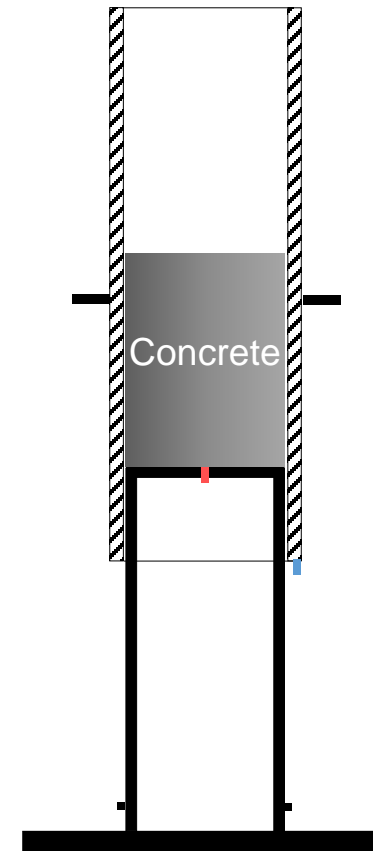
Sliper



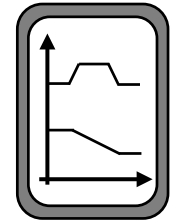
# SLIPER (SLIding PipE Rheometer)



Sliper



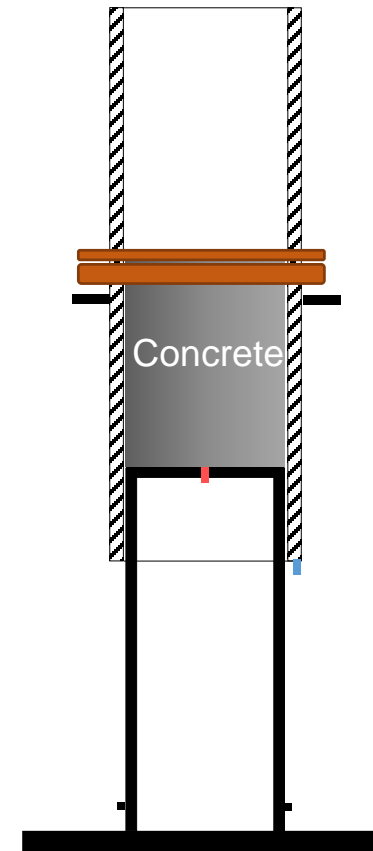
Smartphone



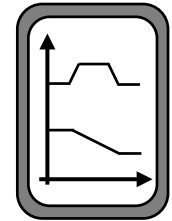
# SLIPER (SLIding PipE Rheometer)



Sliper

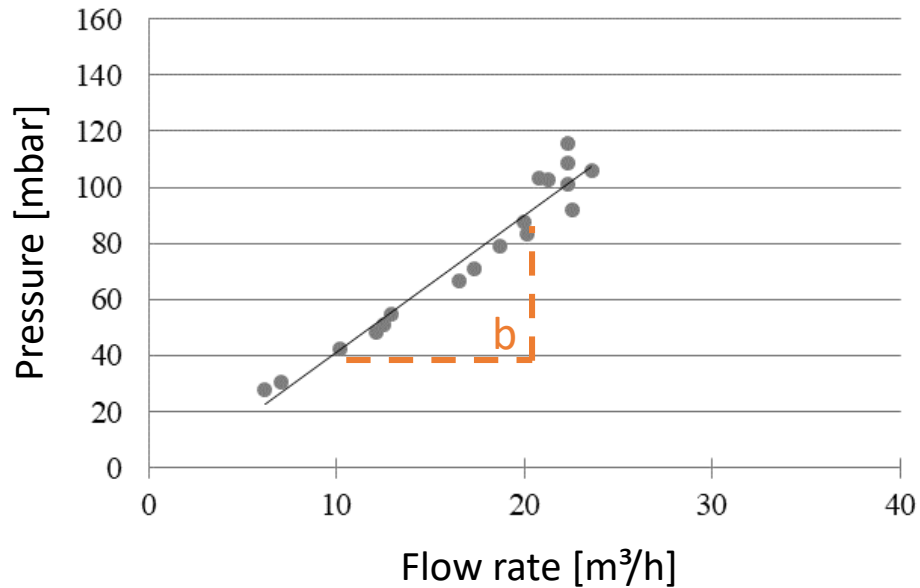


Smartphone





# Sliper measurement



— Example

- Y-axis: The maximum pressure
  - measured by the sensor
- X-axis: Flow rate
  - Velocity\*Cross section
- Two parameters of the lubricant layer can be obtained:
  - a represents the „yield stress“
  - b represents the „viscosity“

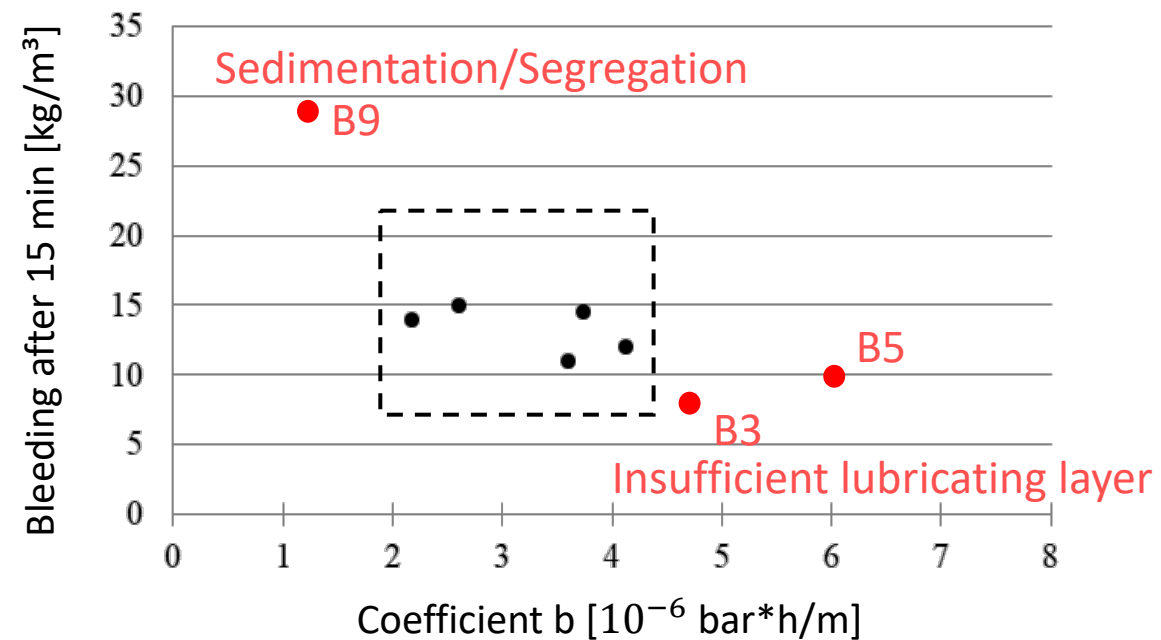
# Formula for calculating the concrete pressure ( $p_s$ )

$$p_s = a \cdot 4 \cdot \frac{L_{\bar{a}}}{D} + b \cdot 16 \cdot Q \cdot \frac{L_{\bar{a}}}{\pi \cdot D^3} + \rho \cdot g \cdot H$$

Depends on:

- a (Sliper-Yield stress)
- b (Sliper-Viscosity)
- Diameter of the pipe
- Flow rate
- Density of the concrete
- Delivery head (assumed 5m)

# Stability and Rheology



# Shotcrete rig

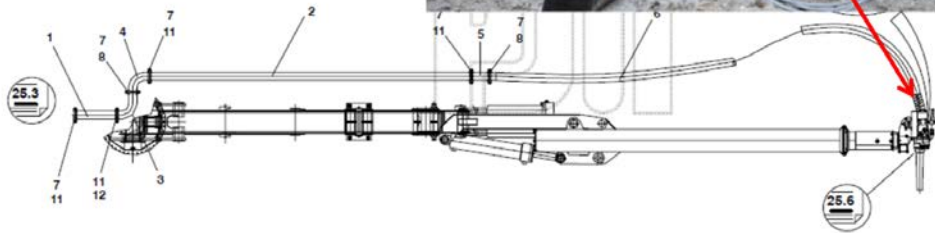


Filling of the shotcrete pump



Checking the sensors

# The sensors



Sensors at the nozzle



Data logger



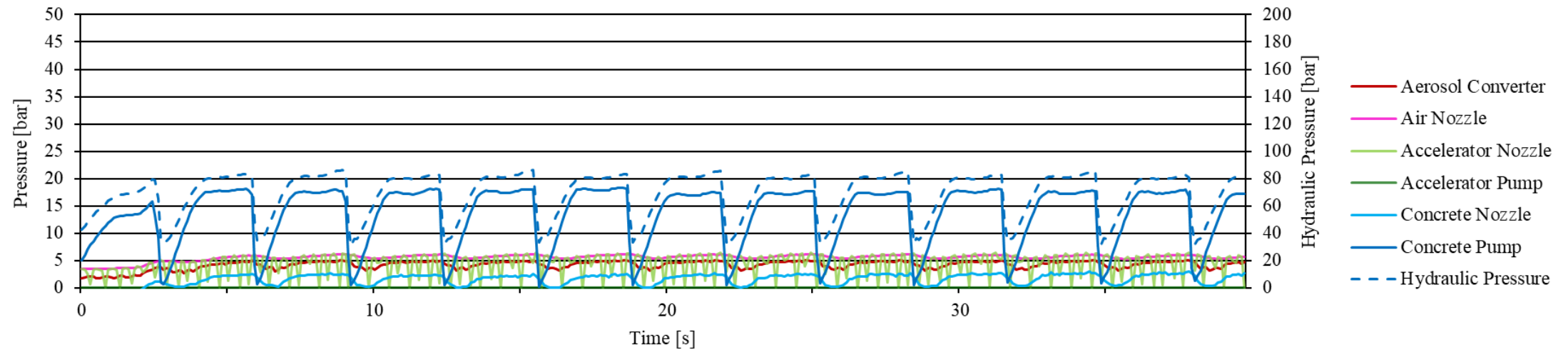
# Results

Mix-Design		Reference	w/b-High
w/b	[-]	0,47	<b>0,52</b>
Water	[dm <sup>3</sup> /m <sup>3</sup> ]	189	204
Fines*	[dm <sup>3</sup> /m <sup>3</sup> ]	170	159
Air void content (measured)	[dm <sup>3</sup> /m <sup>3</sup> ]	8	10
Total paste volume	[dm <sup>3</sup> /m <sup>3</sup> ]	367	373

\*cement+aggregates < 0.125mm+additives

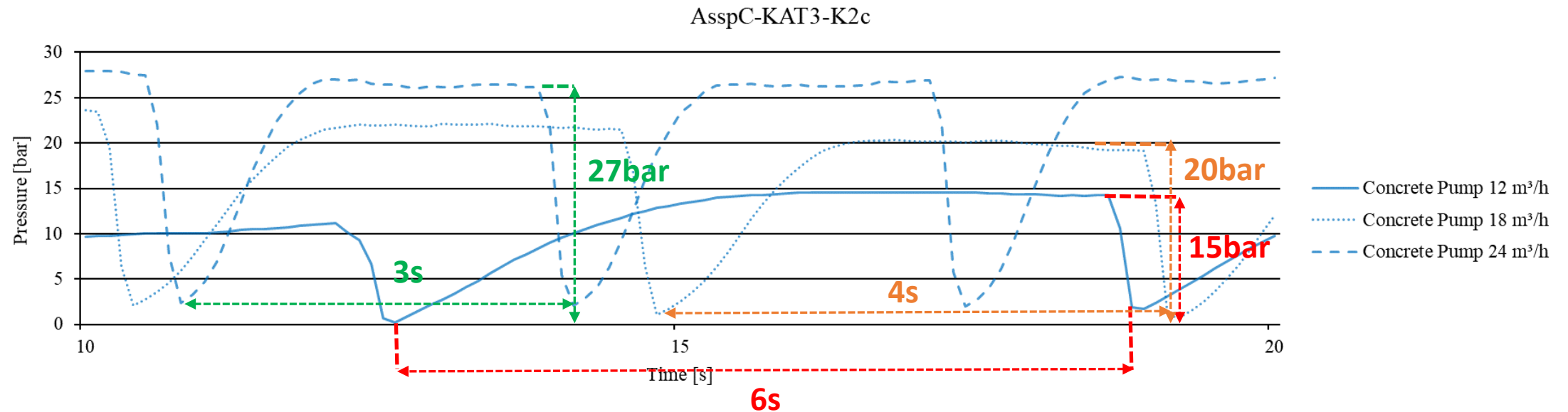
# Results

AsspC-KAT3-190306-150745



Pressures of all sensors during one Measurement (Reference)

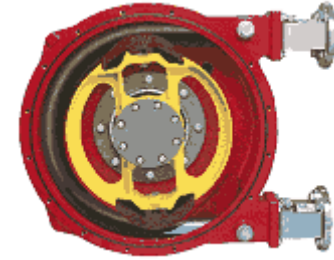
# Results



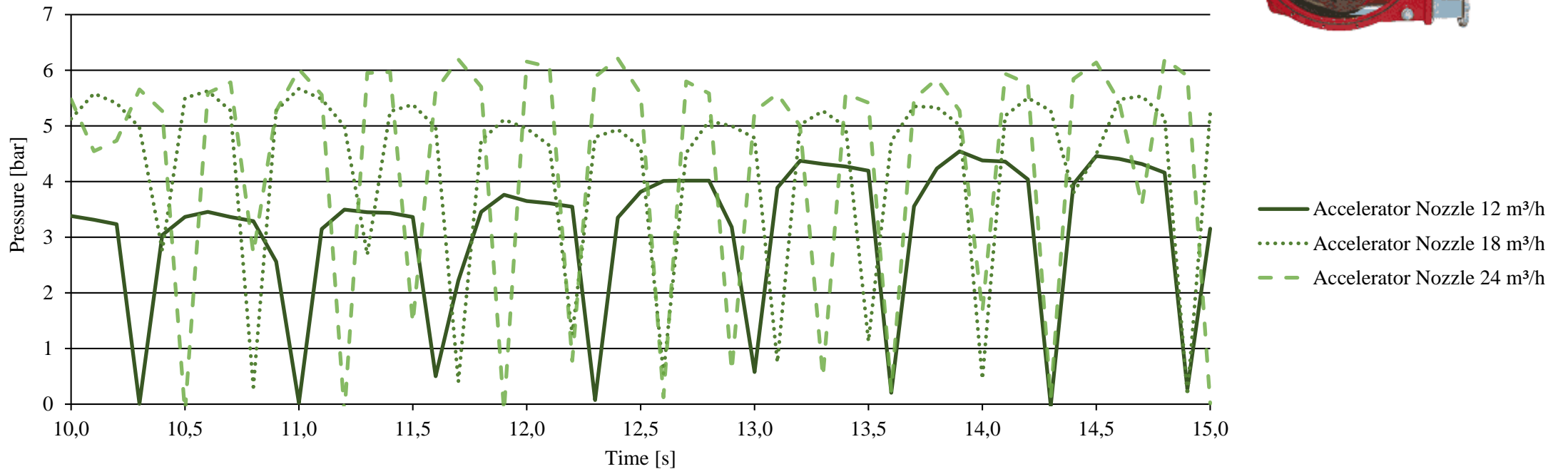
Comparison of the concrete pump pressures at different flow rates but with the same mixture (Reference)



# Results



AsspC-KAT3-190306-150340/K7

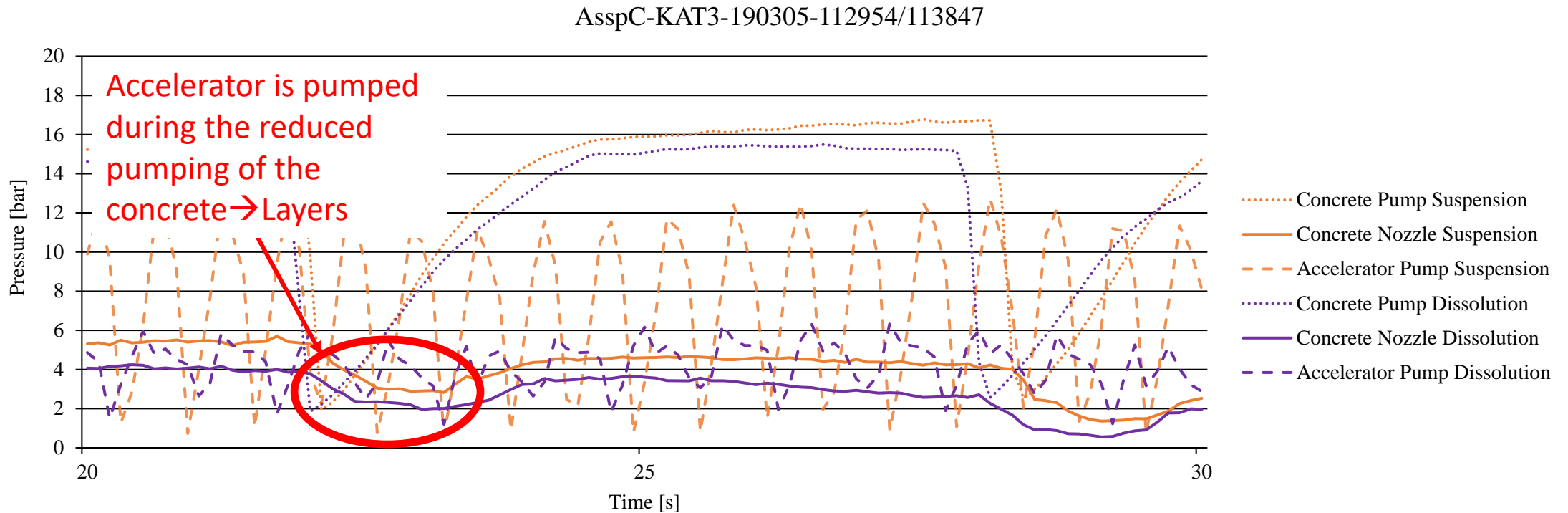


Comparison of the accelerator nozzle pressures at different flow rates

# Results

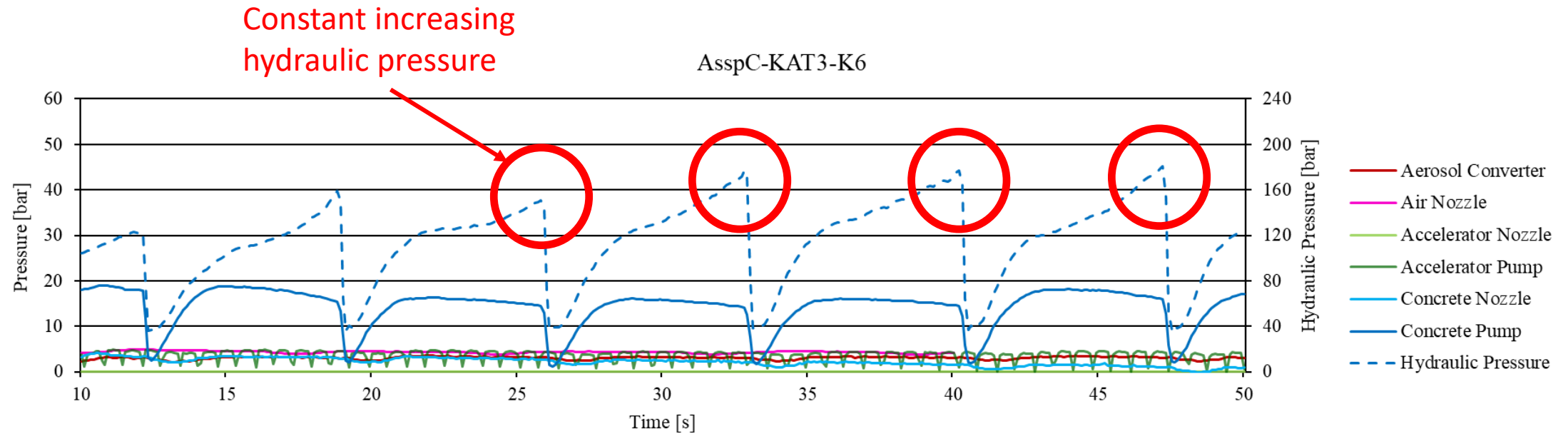


# Results



Comparison of the concrete and accelerator pump pressures with a suspension and a dissolution accelerator

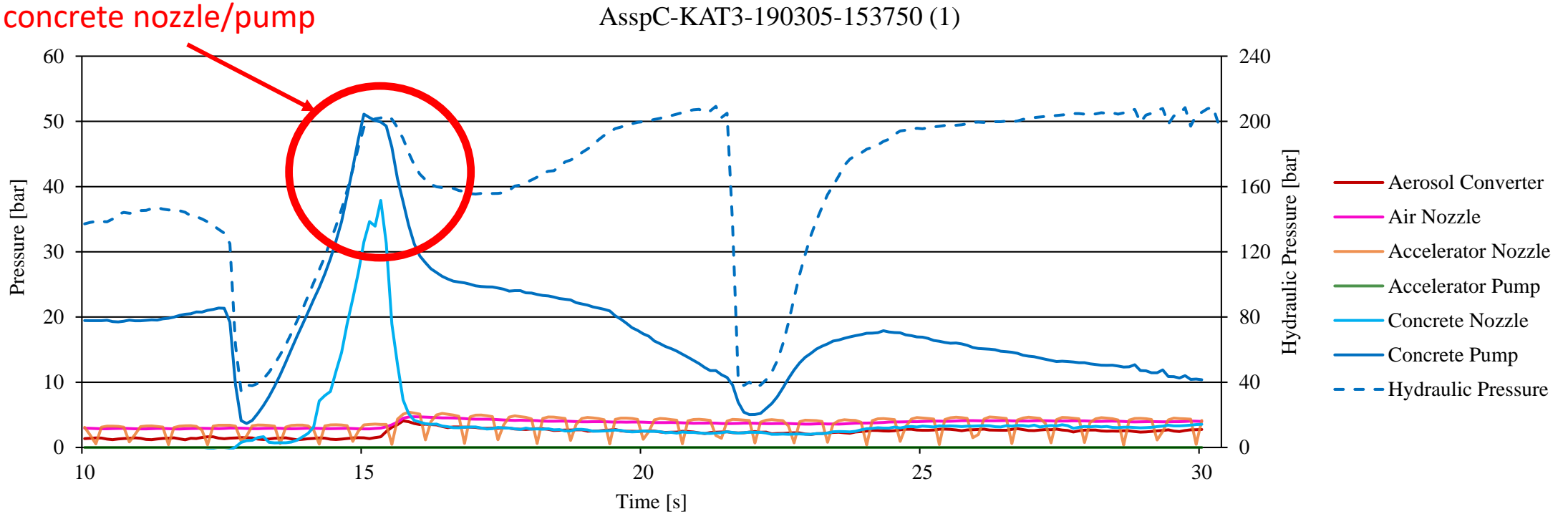
# Results



Indications for an arising blockage

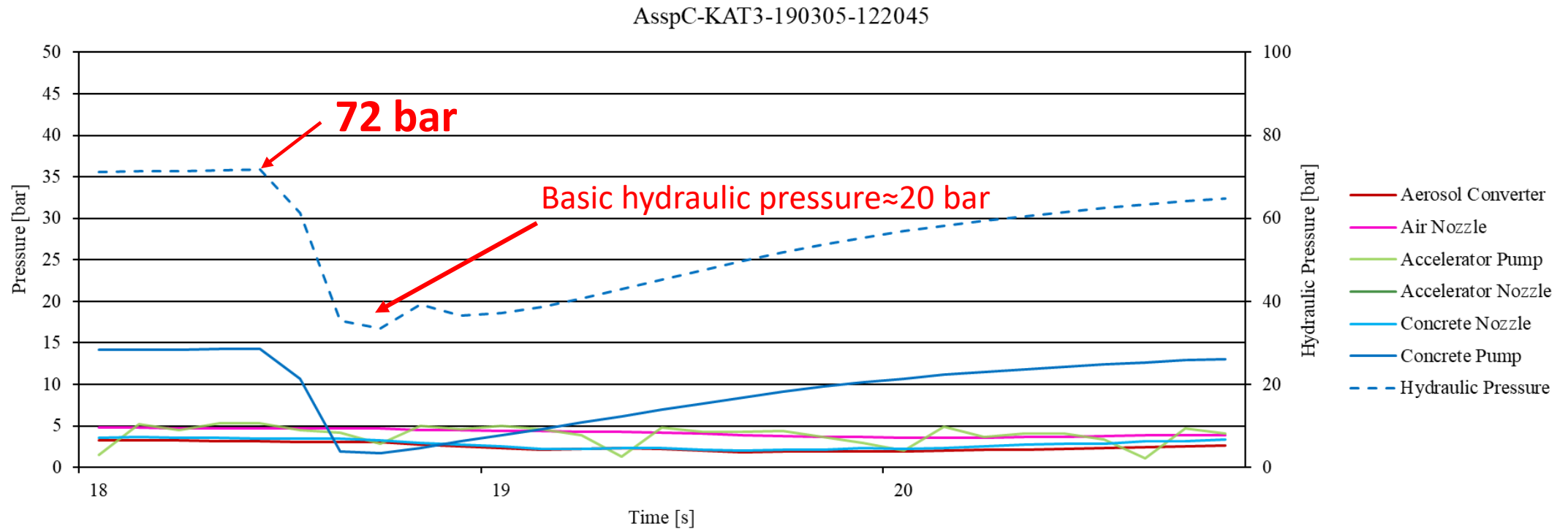
# Results

Huge peak at the  
concrete nozzle/pump



The occurring blockage

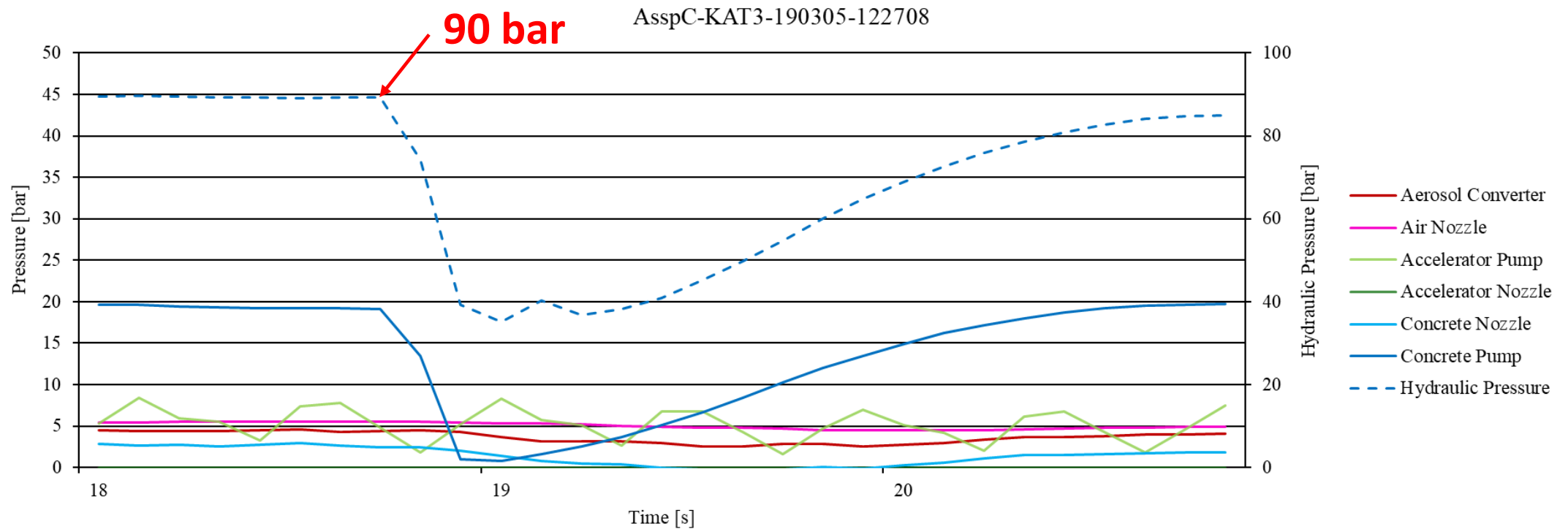
# Pressure drop



Pressure drop between two strokes at a flow rate of 12 m<sup>3</sup>/h of the reference mix

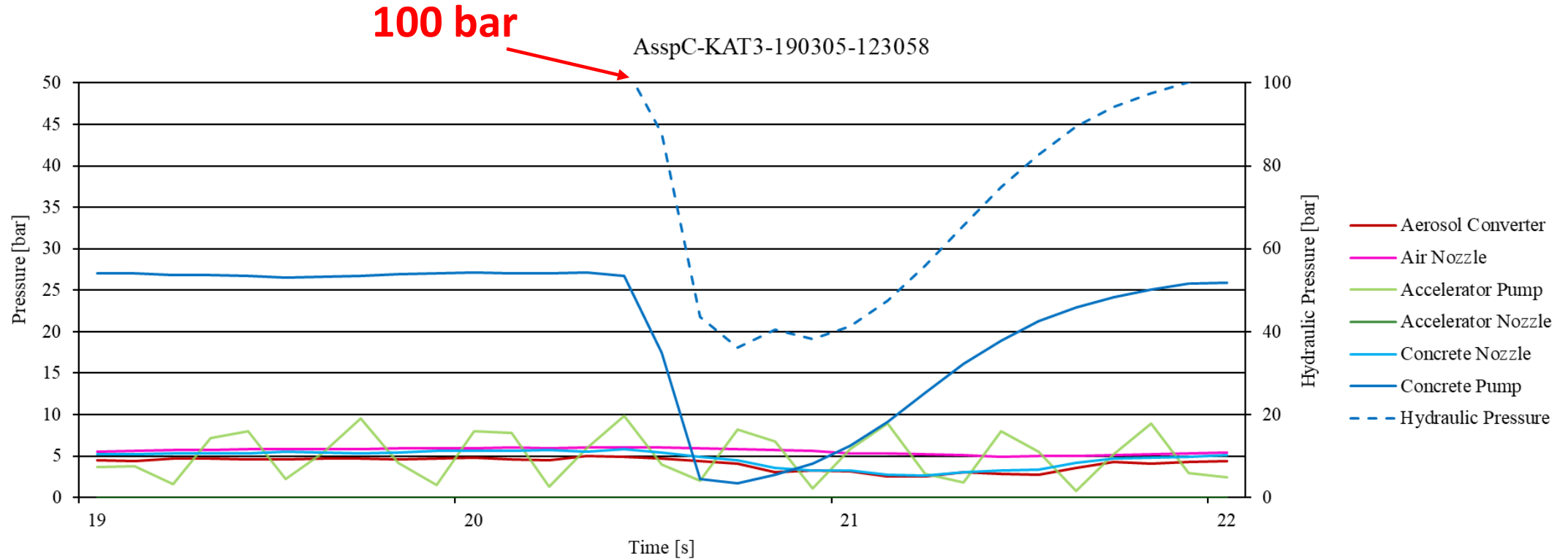


# Pressure drop



Pressure drop between two strokes at a flow rate of 18 m<sup>3</sup>/h of the reference mixture

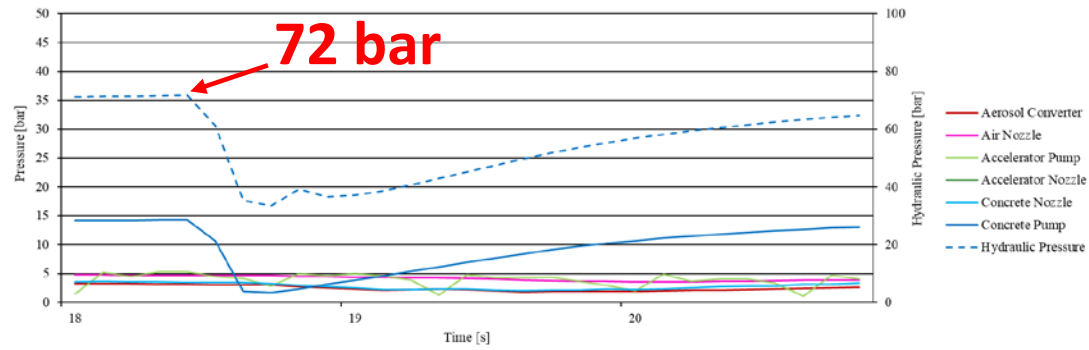
# Pressure drop



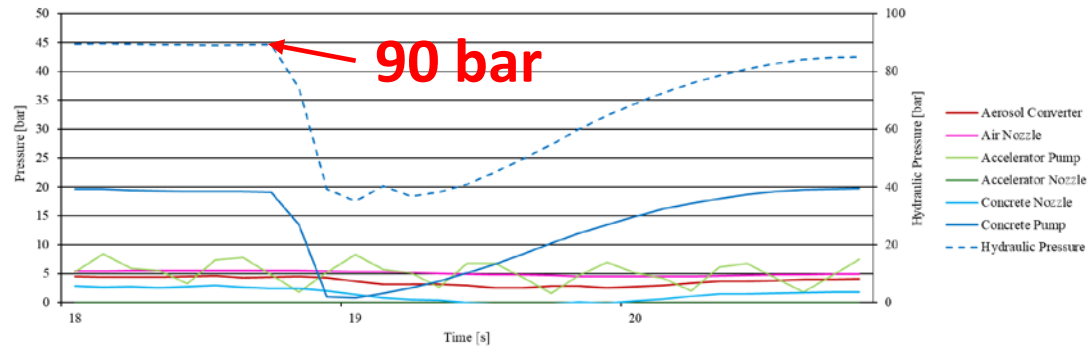
Pressure drop between two strokes at a flow rate of 24 m<sup>3</sup>/h of the reference mixture



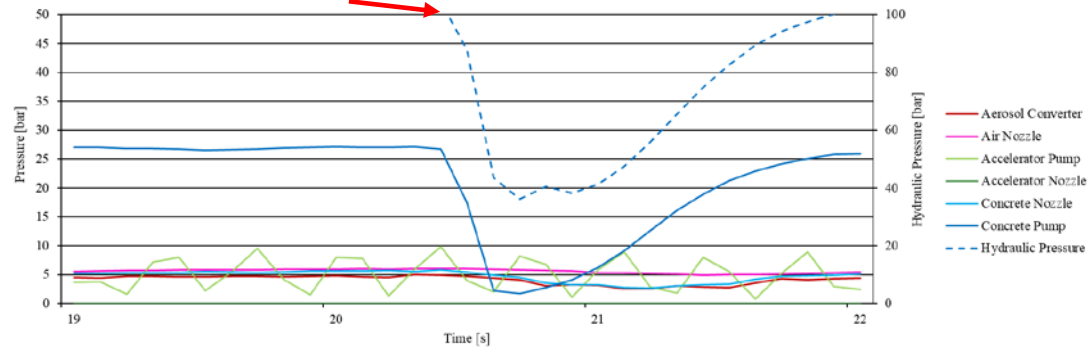
12 m<sup>3</sup>/h



18 m<sup>3</sup>/h

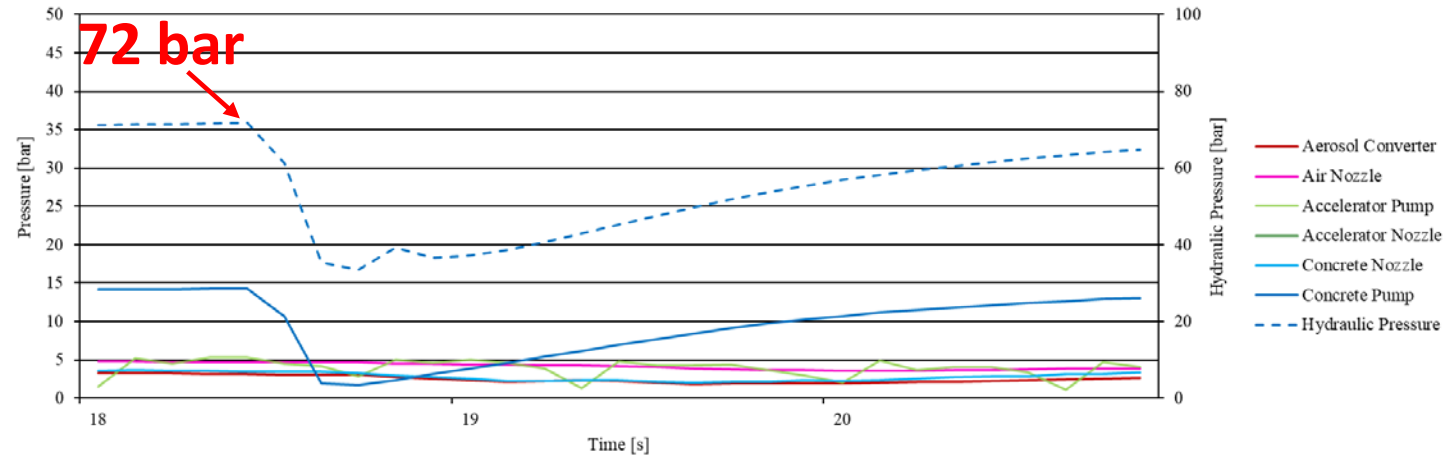


100 bar 24 m<sup>3</sup>/h

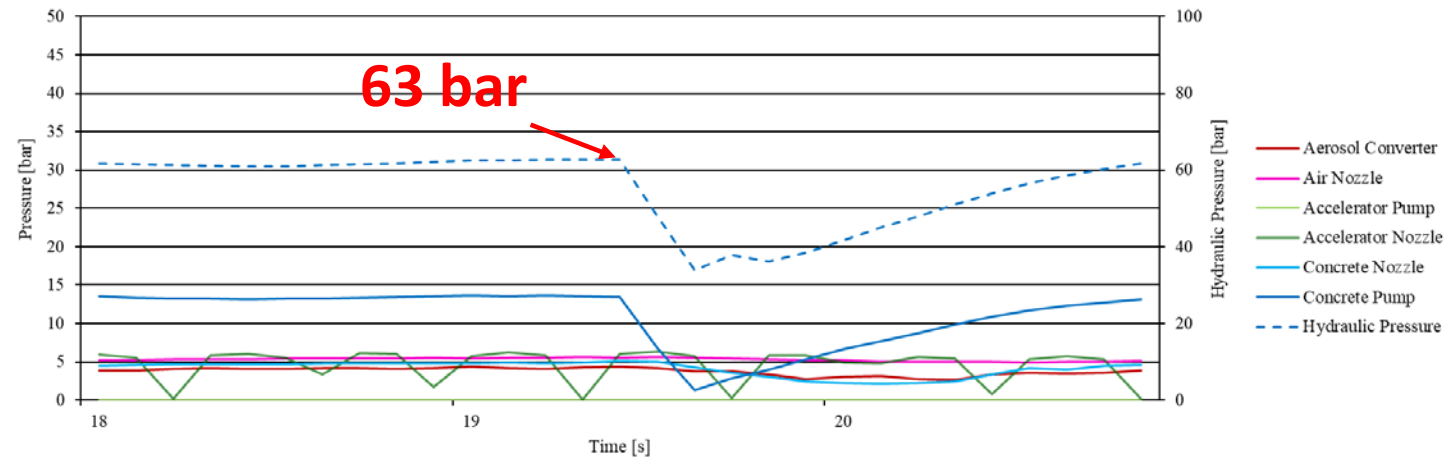


Pressure history during a pressure drop at different flow rates (reference mix)

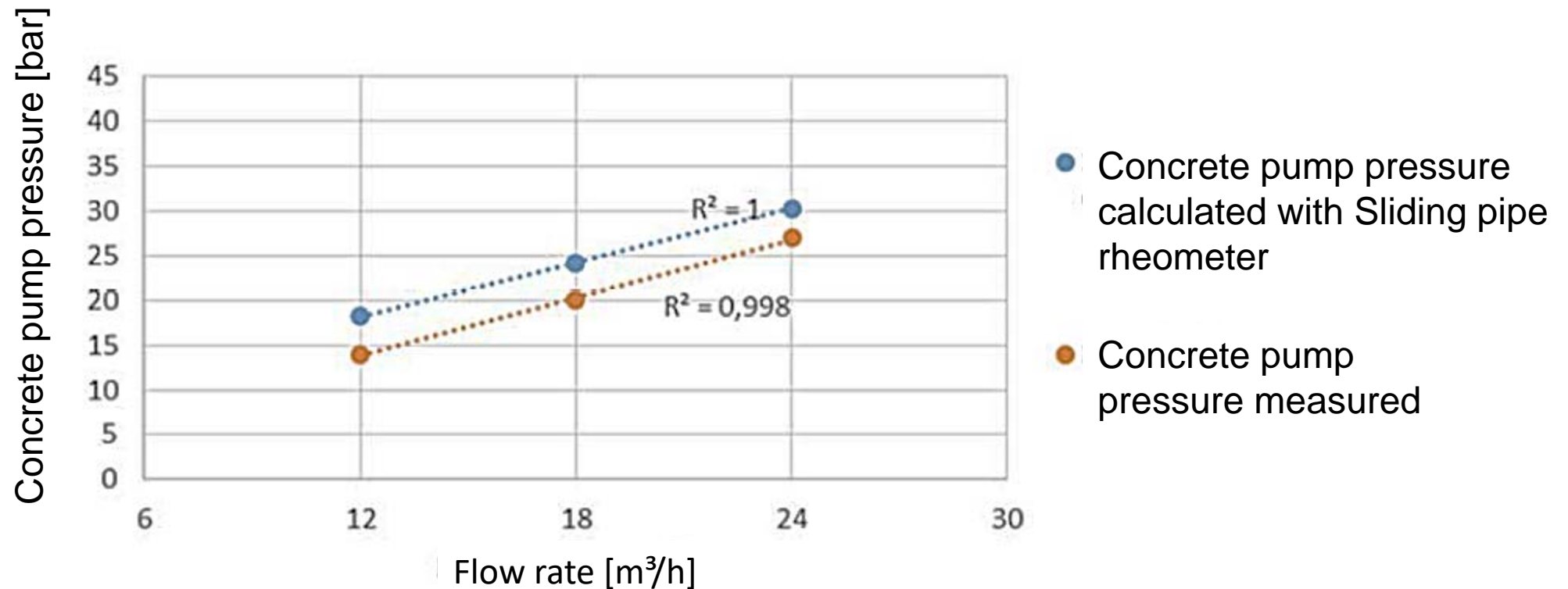
## Reference 12 m<sup>3</sup>/h



## w/b\_High 24 m<sup>3</sup>/h



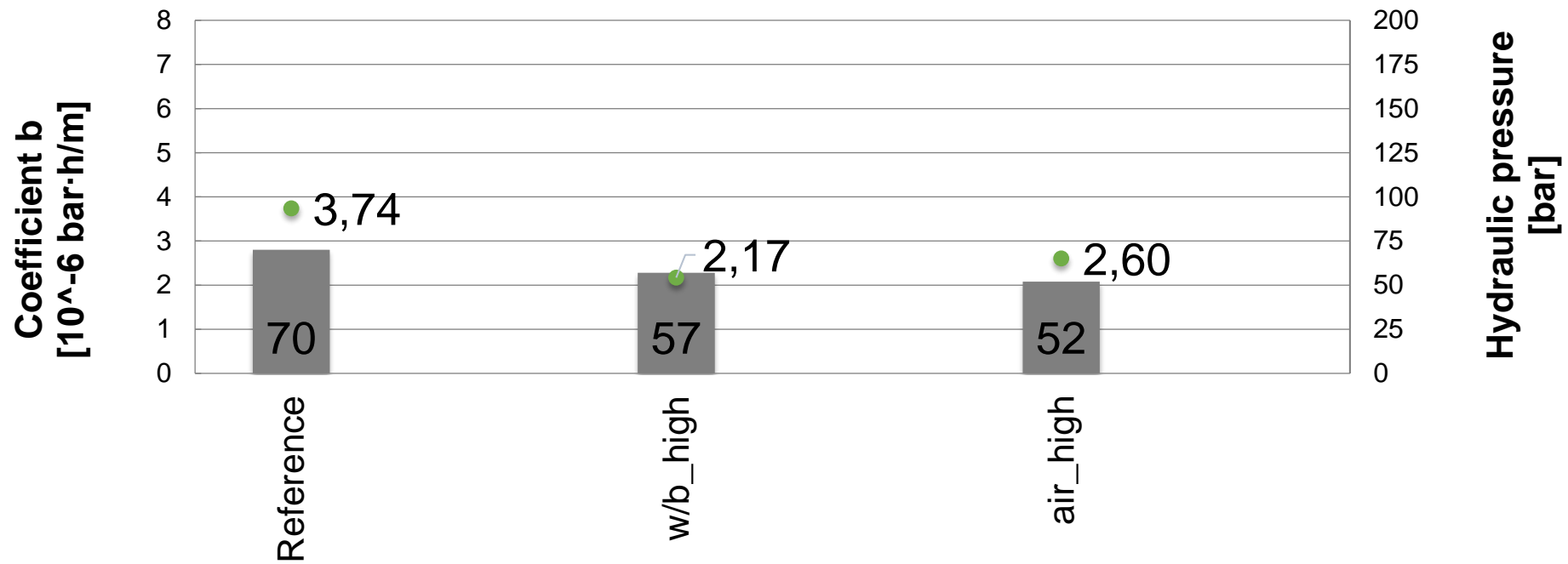
# Sliper viscosity vs. Concrete pump pressure



# Sliper viscosity vs. Hydraulic pressure

Mix-Design		Reference	w/b_high	air_high
w/b		0,49	0,52	0,49
CEM II	[dm <sup>3</sup> /m <sup>3</sup> ]	131	132	133
Water	[dm <sup>3</sup> /m <sup>3</sup> ]	197	<b>208</b>	196
Aggregate ≤ 0,125 mm	[dm <sup>3</sup> /m <sup>3</sup> ]	46	46	42
Air void content	[dm <sup>3</sup> /m <sup>3</sup> ]	32	15	<b>90</b>
Paste volume	[dm <sup>3</sup> /m <sup>3</sup> ]	406	401	461

# Sliper viscosity vs. Hydraulic pressure



# Resume

- Pumpability/Workability of shotcrete depends on:
  - Stability of the mix-design
  - Paste volume
  - Rheology of the paste
- Higher flow rates result in higher pumping pressures
- Measurements of the pumping pressures confirm that the pumpability can be estimated by using results from:
  - Filterpress
  - Sliding Pipe Rheometer

# Outlook

The section of the pressure drop might be optimized

- The interrupted concrete flow, when changing between the two pistons pushing the concrete, should be optimized
- Accelerator dosing has to be adapted during the switch between the two pistons
- Uniform material streams would result in better and more homogeneous hardened shotcrete properties (strength, modulus of elasticity, chemical resistance, etc.)



# Thank you for your attention!

