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Effect of anisotropic elasticity on dislocation pile-ups at grain boundaries

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Objectives:

The current context of miniaturization of objects involves the development of experimental and numerical multi-scale techniques taking into account the effects of internal lengths inherent to the microstructure (crystallographic slip)

- Analytical and numerical calculations of stresses due to different **dislocation pile-up** configurations in a **bi-crystal** considering or not grain boundary properties and **free surface** effects in the context of heterogeneous **anisotropic elasticity**
- Characterization by AFM of the slip behavior at grain boundaries of during compression tests on micron-sized **FCC bi-crystals** (Ni)
- Comparisons between the theoretical calculations and the experimental results for the height of slip lines due to a dislocation pile-up
- Estimation of the resistance of different **grain boundaries** and quantification of the contribution of anisotropic elasticity on **slip transmission**

Micromechanical calculations of dislocation and pile up stress fields in anisotropic bi-materials and tri-materials with/without free surfaces (LEM3)

-- Two different methods of calculations based on Stroh's formalism [1] were used:

- Method of Choi [2] for tri-material configurations
- Use of standard analytic continuation arguments and alternating technique to satisfy boundary conditions at the two interfaces.

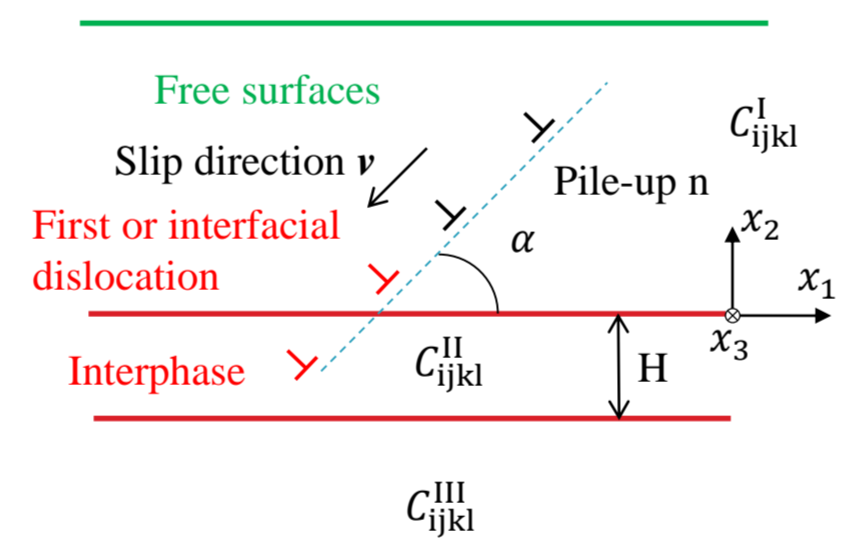
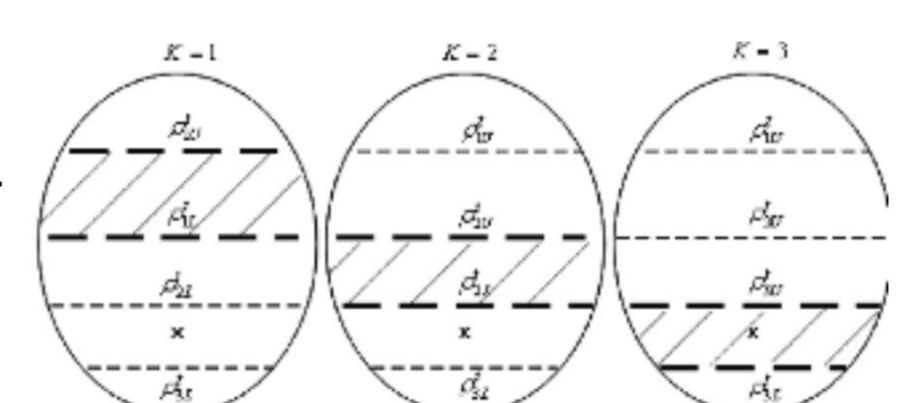
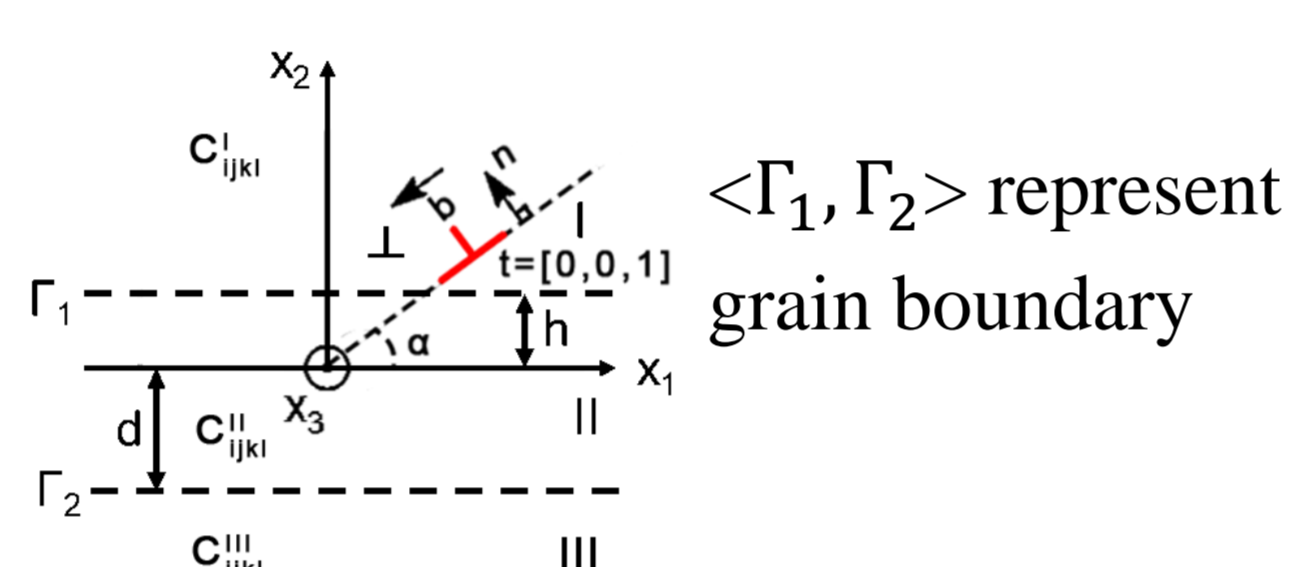
$$u_i = 2\text{Re} [A_{ij} f_j(z_j)]$$

$$f_i(z_i) = \begin{cases} f_i^0(z_i) + f_i^{10}(z_i) + \sum_{n=1}^{\infty} f_i^{In}(z_i) & z \in \text{I} \\ \sum_{n=1}^{\infty} f_i^n(z_i) + \sum_{n=1}^{\infty} f_i^{In}(z_i) & z \in \text{II} \\ \sum_{n=1}^{\infty} f_i^{In}(z_i) & z \in \text{III} \end{cases}$$

- Modeling compliant or rigid grain boundary in tri-materials: $c_{ijkl}^{\text{II}} = \frac{\lambda}{2}(c_{ijkl}^{\text{I}} + c_{ijkl}^{\text{III}})$
- Method of image dislocation density of Wu [3] for an infinite number of layers
- Decomposition of a K-layer problem into K infinite homogeneous sub-problems.
- Summing the contributions of the source (homogeneous) and all image dislocation densities in sub-problems 1, 2 and 3, respectively.

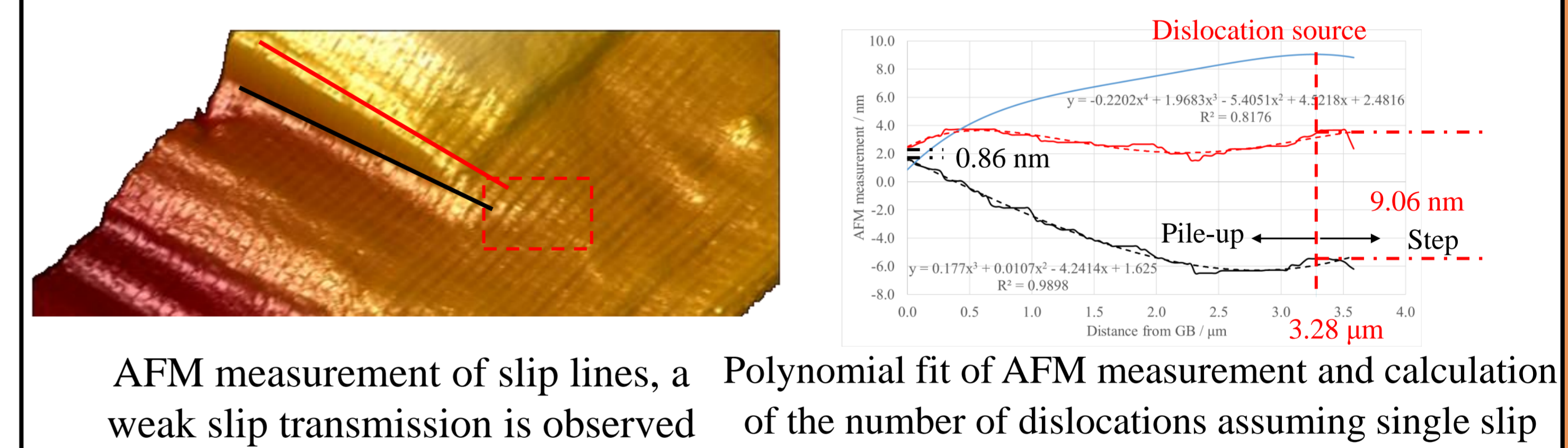
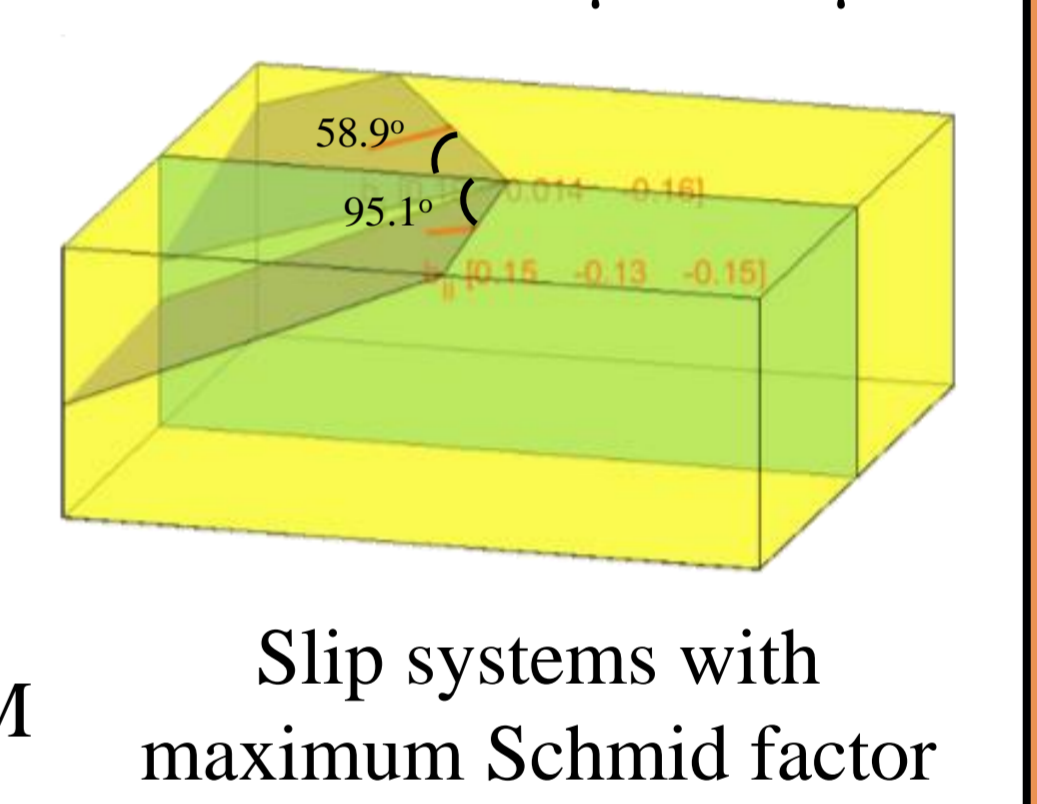
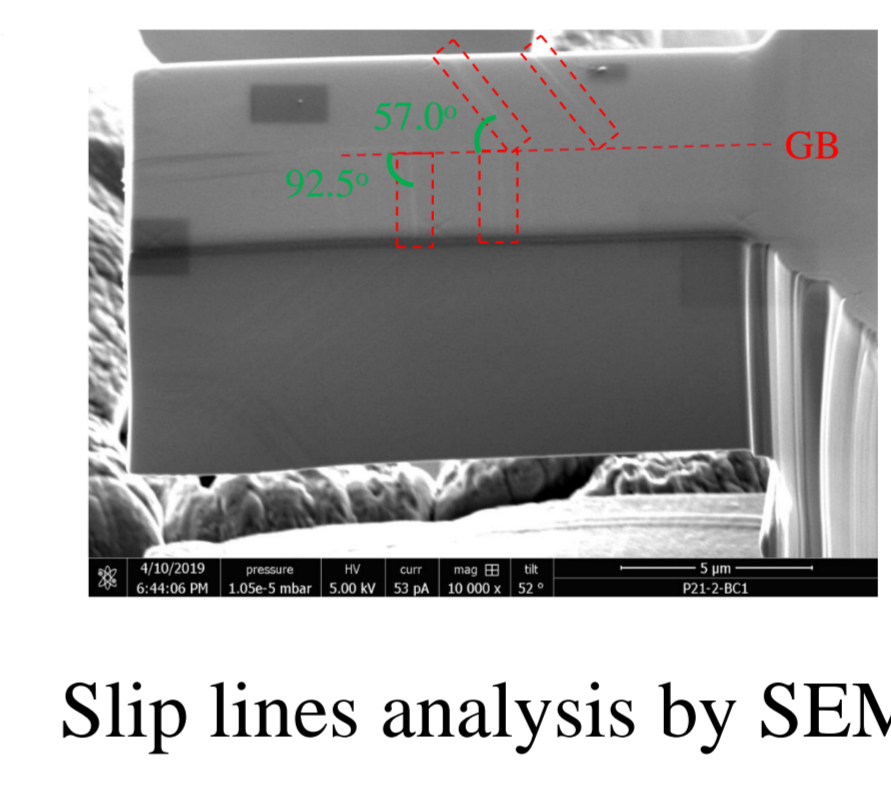
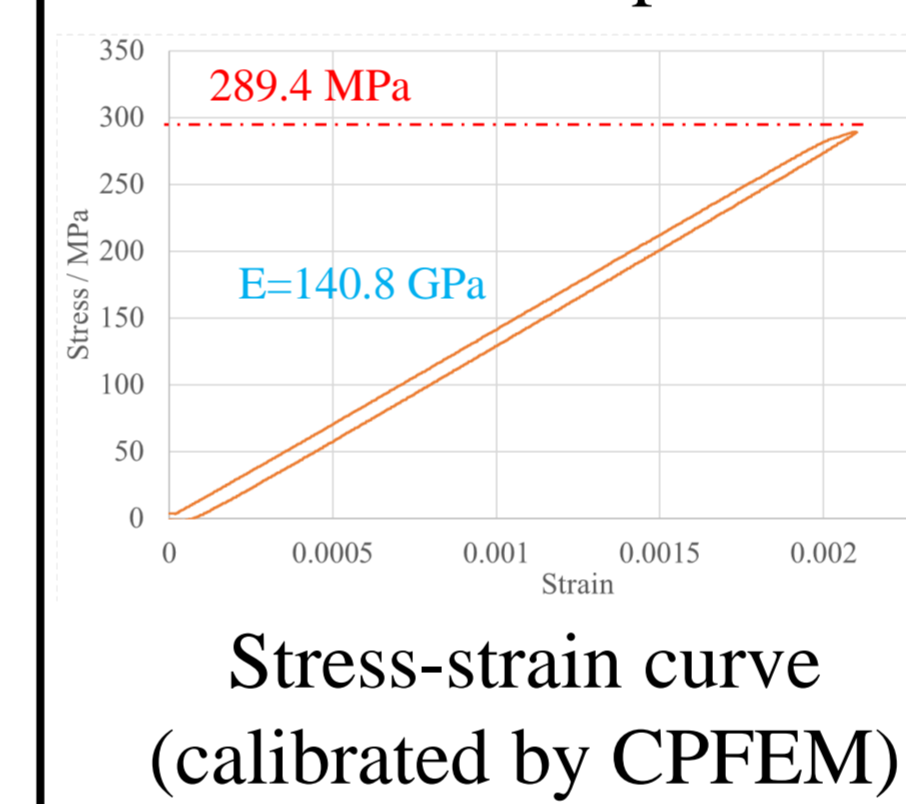
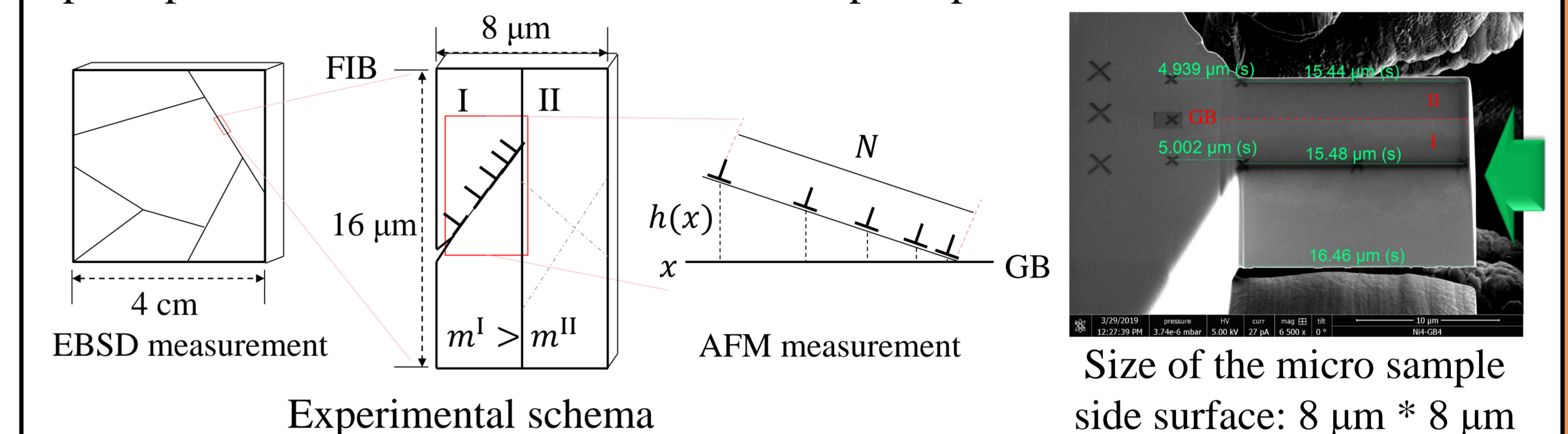
$$\sigma_{ij}(K, \rho_{JK}^t, x_1, \Delta x_2) = \int_{-\infty}^{\infty} 2 \sum_{\alpha=1}^3 (\xi_{K\alpha ij}^{\text{TR}} P(\Delta x_1, p_{K\alpha}^R \Delta x_2, p_{K\alpha}^L \Delta x_2) + \dots)$$

- Dislocation positions in an equilibrated pile-up computed by an iterative relaxation scheme that minimizes the Peach-Koehler force on each dislocation [4]:



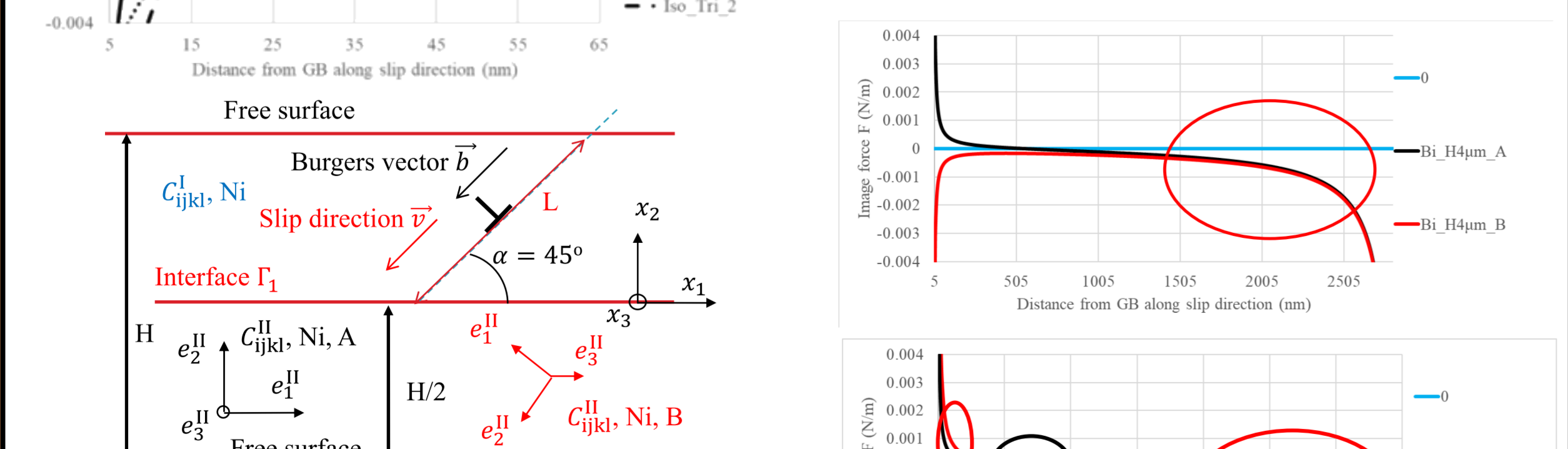
In-situ micromechanical experiments (MWW)

- Bi-crystals (Ni) made out of poly-crystalline sheets by FIB
- Micro-compression tests to test dislocation – grain boundary interactions.
- Observations of bi-crystal plasticity using SEM, AFM and EBSD
- From slip height $h(x)$ determined by AFM, the number of dislocations N in the pile up is obtained and feeds the numerical pile up calculations.



Application: effect of misorientation, GB stiffness and free surfaces on image force along slip direction [5]

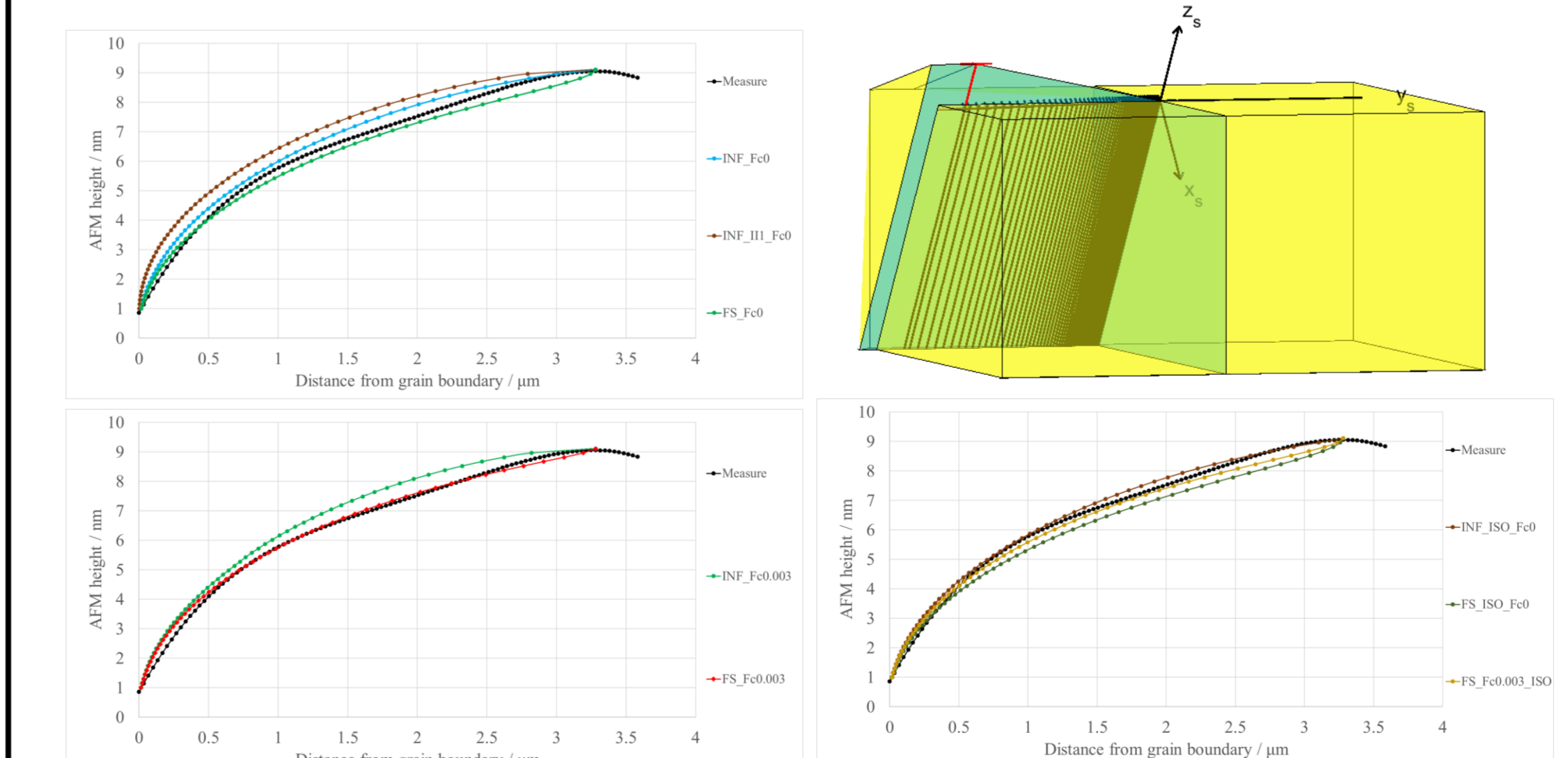
Fixed orientation of crystal I ($\phi_1 = 45^\circ, \Phi = 324.7^\circ, \phi_2 = 135^\circ$); Attractive orientation A ($\phi_1 = 0^\circ, \Phi = 0^\circ, \phi_2 = 0^\circ$) of crystal III and stiff interphase ($\lambda = 2.0$); Repulsive orientation B ($\phi_1 = 90^\circ, \Phi = 45^\circ, \phi_2 = 45^\circ$) of crystal III and compliant interphase ($\lambda = 0.5$)



Free surfaces always attract dislocations; Size effect; Normalized equilibrium positions are close

Application: slip step heights due to a dislocation pile-up in heterogeneous anisotropic elasticity

- $H = N \times b_{\text{unit}} \times |b_s^{\text{Ni}}|, b_{\text{unit}} \times |b_s^{\text{Ni}}| = [0.15, -0.13, -0.15] \text{ nm}$
- $N_T \approx 6, N_S \approx 61 \rightarrow N_P \approx 55$ with $\sigma_{\text{ext}} \approx 289.4 \text{ MPa}, \lambda=1, H=0.9 \text{ nm}$
- A dislocation locked at $L = 3.28 \mu\text{m}$ as dislocation source
- An interfacial dislocation of $6b$ locked in GB to account for transmitted dislocations



Simulation considering grains misorientation, free surfaces, critical force for dislocation glide ($F_C=0.003 \text{ N/m}, 12 \text{ MPa}$ for Ni) and transmitted dislocations across to GB fits very well with AFM measurement of dislocation pile-up heights.

Outlook

- Direct observations of discrete dislocations by ECCI
- Use molecular dynamics simulations to study the elastic stiffness of GB
- Use molecular dynamics simulations to study dislocation-GB interactions at atomic scale
- Estimate GB strength and improve slip transmission criteria

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