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Improvements in a Hybrid Stochastic/Deterministic Method for Transient Three-Dimensional Neutron Transport

Charles L. Bentley
University of Tennessee - Knoxville

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To the Graduate Council:

I am submitting herewith a dissertation written by Charles L. Bentley entitled "Improvements in a Hybrid Stochastic/Deterministic Method for Transient Three-Dimensional Neutron Transport." I have examined the final electronic copy of this dissertation for form and content and recommend that it be accepted in partial fulfillment of the requirements for the degree of Doctor of Philosophy, with a major in Nuclear Engineering.

H. L. Dodds, Major Professor

We have read this dissertation and recommend its acceptance:

L. F. Miller, R. E. Pevey, M. Pace

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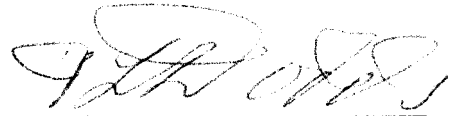
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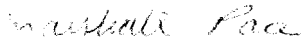
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Improvements in a Hybrid
Stochastic/Deterministic Method for Transient,
Three-Dimensional Neutron Transport

A Dissertation

Presented for the

Doctor of Philosophy

Degree

The University of Tennessee, Knoxville

Charles L. Bentley

December 1996

Dedication

This dissertation is dedicated to my parents, Jane Ellen Bentley and the late William Dean Bentley, and to my wife, Lisa Lynn Bentley.

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I would like to thank my advisor, Dr. H.L. Dodds, for his encouragement and guidance. This work could not have been completed without his supervision. I would also like to thank my committee members, Dr. L.F. Miller, Dr. R.E. Pevey and Dr. M. Pace, for their advice and assistance. I also wish to thank the members, past and present, of the Nuclear Criticality Safety Group at the University of Tennessee, Knoxville; particularly, B. Basoglu, R. Demeglio, M. Dunn, S. Goluoglu, K. Norton, L. Paschal, W. Waddell and T. Yamamoto. I also wish to recognize the U.S. Department of Energy and Oak Ridge Institute for Science and Education for the financial support of this work via the Nuclear Engineering/Health Physics Fellowship Program. Finally, I would like to express thanks to the members of my family, Lisa Bentley, Jane Bentley, Jenny Griffith, Danny Griffith and Doris Reynolds.

Abstract

This research develops an improved methodology (and corresponding code) for solving the time-dependent, three-dimensional Boltzmann Transport Equation with explicit representation of delayed neutrons. These improvements are incorporated in a modified version of the code TDKENO, entitled TDKENO-M. Specifically, these improvements are:

1. Incorporate the improved quasistatic methodology into an existing quasistatic framework. Specifically, include the flux shape derivative in the fixed source term instead of being neglected. Also, compute the point kinetics parameters deterministically by their inner product definitions.
2. Incorporate a hierarchy of three different integration time intervals for the numerical solution of the coupled set of ordinary differential equations. The shape function is assumed to vary linearly over the largest time interval. The second largest time interval is used for determining the point kinetics parameters. Finally, the smallest time step is used for solving the point kinetics equations.
3. Apply TDKENO-M to benchmark problems to determine the accuracy of the method. Particularly, TDKENO-M is applied to one- and three-dimensional benchmark problems to evaluate its neutronic capabilities.
4. Combine input requirements into a single input file so that TDKENO-M is less cumbersome to execute.
5. Develop the ability to restart a calculation at an intermediate problem time.
6. Develop a "user-friendly" manual for using TDKENO-M which describes in detail the input requirements as well as the output files, subroutines, modules, and the calculational flow.

Results show that TDKENO-M is quite accurate in comparison with benchmark calculations (less than 2% error in power trace for ANL Benchmark 16-A1) with as much as a factor of 500 reduction in CPU time relative to TDKENO.

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Chapter One

Introduction

1.1 Background

The transient simulation of neutronic systems is of extreme importance for new reactor system design, emergency response planning for inadvertent criticality excursions, and also for the safety analysis of existing systems. The transient neutronic behavior of a system can be modeled using methods ranging in complexity from simple point kinetics algorithms to three-dimensional nodal methods using space-time kinetics.

Point kinetics¹ algorithms were initially used to perform transient reactor calculations. This method ignores the spatial distribution of the neutron flux during the transient. Point kinetics algorithms are usually adequate for modeling small reactors (i.e., a few mean free paths thick) in which the spatial distribution of flux is relatively time-independent. However, the validity of using point kinetics for large reactor systems with loosely coupled regions is questionable and, therefore, the spatial dependence of the flux should be modeled.¹

To incorporate the spatial dynamics of a reactor system, two methods exist, transport theory and diffusion theory. Diffusion theory, in which the angular dependence is assumed to be linear, is an approximation to transport theory.² The time-dependent, three-dimensional Boltzmann transport equation with explicit representation of delayed

neutrons is as follows:

$$\begin{aligned}
& \frac{1}{v} \frac{\partial \phi(\bar{r}, \bar{\Omega}, E, t)}{\partial t} + \bar{\Omega} \cdot \bar{\nabla} \phi + \Sigma_t \phi = \\
& \iint \Sigma_s(\bar{r}; \bar{\Omega}', E' \rightarrow \bar{\Omega}, E; t) \phi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' \\
& + \iint \chi_p(E) (1-\beta) \nu \Sigma_f(\bar{r}, E', t) \phi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' \\
& + \sum_j \lambda_j C_j(\bar{r}, t) \chi_j + Q
\end{aligned} \tag{1}$$

and

$$\frac{\partial C_j(\bar{r}, t)}{\partial t} + \lambda_j C_j = \iint \beta_j \nu \Sigma_f(\bar{r}, E', t) \phi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' \quad j=1, N \tag{2}$$

where,

- v = particle speed,
- ϕ = time-dependent angular flux,
- \bar{r} = spatial variable,
- E = energy,
- $\bar{\Omega}$ = unit vector describing particle direction,
- t = time,
- Σ_t = total cross section,
- Σ_s = differential scattering cross section,
- Q = external source,
- χ_p = normalized energy spectrum of prompt neutrons,
- χ_j = normalized energy spectrum for precursor group j ,
- β = delayed neutron fraction,
- ν = total number of neutrons emitted per fission,
- Σ_f = fission cross section,
- λ_j = decay constant for delayed neutron precursor group j ,
- C_j = density of delayed neutron precursors for group j ,
- N = number of precursor groups.

Also, the time-dependent three-dimensional diffusion equation with explicit representation of delayed neutrons is given by:

$$\begin{aligned}
\frac{1}{v} \frac{\partial}{\partial t} \phi(\bar{r}, E, t) + \Sigma_t \phi &= \bar{\nabla} \cdot D(\bar{r}, E, t) \bar{\nabla} \phi(\bar{r}, E, t) \\
&+ \int \Sigma_s(\bar{r}; E' \rightarrow E; t) \phi(\bar{r}, E', t) dE' \\
&+ \int \chi_p(E) (1 - \beta) v \Sigma_f(\bar{r}, E', t) \phi(\bar{r}, E', t) dE' \\
&+ \sum_j \lambda_j C_j(\bar{r}, t) \chi_j + Q
\end{aligned} \tag{3}$$

and

$$\frac{\partial C_j(\bar{r}, t)}{\partial t} + \lambda_j C_j = \int \beta_j v \Sigma_f(\bar{r}, E', t) \phi(\bar{r}, E', t) dE' \quad j=1, N \tag{4}$$

1.2 Previous Work

Due to the complexity of the equations, neither the transport method or the diffusion method can be solved analytically for complicated geometries. However, analytical solutions can be determined for some simple geometries (e.g., homogeneous spheres, rectangular parallelepipeds, etc.) and therefore, numerical techniques are needed to solve the spatial and temporal dependent equations for realistic geometries. Techniques which address the spatial variable include modal, finite element, nodal, and

direct integration.³ Methods which treat the time variable include direct integration and flux factorization methods. The direct methods use temporal approximation techniques such as fully implicit, fully explicit, Crank-Nicholson, and semi-implicit techniques. Flux factorization methods include exponential transformation, point kinetics, adiabatic, quasistatic and improved quasistatic methods.⁴ Note that the adiabatic, quasistatic, and improved quasistatic methods are often generically referred to as the quasistatic method without denoting the intrinsic differences between the three methods.

The modal expansion technique^{5,6,7,8} involves the expansion of the solution into specified functions of one or more of the independent variables by using combining coefficients. Thus, the number of independent variables for a problem is reduced. Codes which use modal expansion techniques to solve the time-dependent diffusion equations include one-dimensional RAUMZEIT⁹, two-dimensional RADYVAR¹⁰, and three-dimensional SMOKIN.¹¹

The nodal method^{12,13,14,15} divides the reactor into subregions or nodes. The flux in each node is determined using a single polynomial and the interaction between nodes is included by using coupling coefficients. Diffusion codes which use the nodal method include a one-dimensional code by Alcouffe and Albrecht¹⁶ as well as three-dimensional codes NEM¹⁷, CUBBOX¹⁸, IQSBOX¹⁹, CONQUEST¹⁵, QUANDRY²⁰, and NIKE.²¹

The most straight forward method is the direct integration technique²² in which either the transport equations or the diffusion equations are directly integrated. There are several methods for integrating the time variable which range in complexity from fully explicit, in which the flux is an explicit function of variables at the previous time step, to fully implicit, in which the flux depends on variables at the present time step and leads to iterative solutions. In general, direct numerical integration methods are quite time consuming when applied to three-dimensional multigroup problems. Codes which solve the time-dependent diffusion equations using finite difference methods include one-dimensional WIGLE²³, two-dimensional TWIGL²⁴ and DISCOTHEQUE²⁵, and three-dimensional 3DKIN²⁶ and MEKIN.²⁷ Further, three-dimensional CRONOS²⁸ uses finite elements. Codes which solve the time-dependent transport equations using direct numerical integration include one dimensional TDA²⁹ and TIMEX³⁰, and two-dimensional TRANZIT.³¹ TDA is a time-dependent version of the one-dimensional, multigroup discrete ordinates transport code ANISN.³² TIMEX is a one-dimensional, multigroup transport code which uses a finite element method to treat the spatial variable, and conventional discrete ordinates to treat the angular variable. TRANZIT is a multigroup, time-dependent, two-dimensional discrete ordinates code in cylindrical geometry which uses diamond difference approximation techniques.

Finally, the quasistatic method^{33,34} treats the spatial dynamics of a calculation by factoring the flux into an amplitude and a shape function such that the time variation of the shape function is more slowly varying than the time variation of the amplitude

function.³⁵ This factorization of the flux results in splitting the neutronics equation into two coupled equations; an amplitude equation having the form of the point kinetics equation and a shape equation. The accuracy of the quasistatic method based on diffusion theory has been investigated for a wide range of excursions in fast and thermal systems by comparison with full numerical solutions. The results of these investigations show that the quasistatic method can describe even extreme excursions in both fast and thermal systems very accurately.^{4,36,37,38} Deterministic diffusion codes which use the quasistatic method to solve the time-dependent diffusion equations include one-dimensional QX1³⁸, two-dimensional FX2³⁹ and TWODQD⁴⁰, and three dimensional CERBERUS⁴¹, QUANDRY²⁰, and CONQUEST.¹⁵ Further, TDKENO^{42,43,44} was the first successful attempt at modeling time-dependent transport theory with explicit representation of delayed neutrons using a hybrid stochastic/deterministic method embedded in a quasistatic framework. The quasistatic method is described in more detail in the following chapter of this document.

1.3 Objective

The objective of this work is to develop an improved hybrid/stochastic method for transient, three-dimensional neutron transport. These improvements are incorporated in a modified version of the code TDKENO, entitled TDKENO-M. Specifically, these improvements are:

1. Incorporate the improved quasistatic methodology into an existing quasistatic framework. Specifically, include the flux shape derivative in the fixed source term instead of being neglected. Also, compute the point kinetics parameters deterministically by their inner product definitions.
2. Incorporate a hierarchy of three different integration time intervals for the numerical solution of the coupled set of ordinary differential equations. The shape function is assumed to vary linearly over the largest time interval. The second largest time interval is used for determining the point kinetics parameters. Finally, the smallest time step is used for solving the point kinetics equations.
3. Apply TDKENO-M to benchmark problems to determine the accuracy of the method. Particularly, TDKENO-M is applied to one-dimensional and three-dimensional benchmark problems to evaluate its neutronic capabilities.
4. Combine input requirements into a single input file so that TDKENO-M is less cumbersome to execute.
5. Develop the ability to restart a calculation at an intermediate problem time.
6. Develop a "user-friendly" manual for using TDKENO-M which describes in detail the input requirements as well as the output files, subroutines, modules, and the calculational flow.

TDKENO-M is verified by applying the code to Benchmark Problems 14-A2, 16-A1, 16-A2, 16-A3, 16-A6, and 16-A7 contained in the ANL-7416 Supplement 3 Benchmark Problem Book.⁴⁵ Problem 14-A2 is a prompt-critical transient in three dimensions with adiabatic heatup and Doppler feedback. Problems 16-A1, 16-A2, 16-A3, 16-A6, and 16-A7 are one-dimensional, two-group transient problems for which solutions have been determined using the one-dimensional transport codes TDA²⁹ and TIMEX³⁰. Finally, comparisons between TDKENO and TDKENO-M are made whenever possible in order to evaluate the improvements in TDKENO-M.

1.4 Originality and Importance of Work

As mentioned, TDKENO^{42,43,44} was the first successful attempt at modeling time dependent, three-dimensional transport theory with explicit representation of delayed neutrons using a hybrid stochastic/deterministic method embedded in a quasistatic framework. Therefore, to the best of my knowledge, TDKENO-M will be the first hybrid stochastic/deterministic code that solves the time dependent, three-dimensional transport equation with explicit representation of delayed neutrons using the improved quasistatic methodology. The method not only incorporates the improved quasistatic methodology, it also involves other improvements (i.e., three time steps instead of two, deterministic rather than stochastic calculation of point kinetics parameters, etc.). These improvements will allow TDKENO-M to serve as a benchmark of comparison for other more approximate and less CPU intensive codes without the prohibitive computing times encountered with TDKENO.

1.5 Scope and Organization

This dissertation contains seven chapters. The first chapter provides background information, a summary of relevant previous work, the objectives of this work as well as a description of the originality and importance of this work.

Chapter Two describes in detail the improved quasistatic methodology. Chapter Three contains information related to the numerical solution algorithms used in this work. Chapter Four describes the transient, three-dimensional transport code, TDKENO-M.

Chapter Five describes the results obtained using TDKENO-M to model various benchmark problems.

Chapter Six describes the sensitivity and parametric studies for the numerical solution algorithms. Finally, Chapter Seven contains the conclusions and suggestions for future work.

Chapter Two

Improved Quasistatic Methodology

2.1 Introduction

The quasistatic approach is a method of treating the spatial dynamics of a transport calculation by factoring the flux into an amplitude and a shape function such that the time variation of the shape function is more slowly varying than the time variation of the amplitude function. This factorization of the flux results in splitting the neutronics equation into two coupled equations; an amplitude equation having the form of the point kinetics equation and a shape equation. The improved quasistatic method replaces the time derivative of the shape function by a first order backward difference approximation thus allowing the improved quasistatic method to be applied more accurately. Note that a complete derivation of the quasistatic equations is given in Appendix A.

The development of the improved quasistatic method begins with the time-dependent Boltzmann transport equation with explicit representation of delayed neutrons as given by equations 1 and 2 on page 2 of this document. Also, the time-independent k_{eff} adjoint form of the transport equation is given by:

$$\begin{aligned}
-\bar{\Omega} \cdot \bar{\nabla} \phi^* + \Sigma_t \phi^* &= \iint \Sigma_s(\bar{r}; \bar{\Omega}, E \rightarrow \bar{\Omega}', E') \phi^*(\bar{r}, \bar{\Omega}', E') d\Omega' dE' \\
&+ \frac{1}{k_{eff}} \iint \chi(E') \nu \Sigma_f(\bar{r}, E) \phi^*(\bar{r}, \bar{\Omega}', E') d\Omega' dE'
\end{aligned} \tag{5}$$

where,

$$\phi^* = \text{adjoint flux.}$$

Next, the flux is factored into an amplitude function, $P(t)$, and a shape function, Ψ , such that the flux is given by:

$$\phi(\bar{r}, \bar{\Omega}, E, t) = P(t) \psi(\bar{r}, \bar{\Omega}, E, t) \tag{6}$$

This factorization requires an additional separation constraint for $t > 0$ in order to become a unique definition.³⁵ There are many conditions that could be used, all of which involve constraining some space-energy integral of $\Psi(r, E, t)$ to a constant value for all $t > 0$. The only basic requirement is that $\Psi(r, E, t)$ remain positive and bounded at all points in space (r, E) for all time. According to Henry, the following equation fulfills the requirements for the constraint condition and has the added advantage that it facilitates the transition to the point kinetics formulation:^{46,47}

$$\iiint \frac{1}{V} \psi(\bar{r}, \bar{\Omega}, E, t) \phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dE dV = \text{constant} \tag{7}$$

2.2 Flux Amplitude Equation

The flux amplitude equation is determined by combining equations 1, 2, and 5 through 7 and integrating over space, energy and angle to produce the following expression:

$$\frac{dP(t)}{dt} = \frac{\rho(t) - \bar{\beta}(t)}{\Lambda(t)} P(t) + \sum_j \lambda_j C_j(t) + \bar{Q}(t) \quad (8)$$

with the following parameter definitions:

$$\begin{aligned} \rho(t) = & - \frac{1}{F(t)} \iiint (\Sigma_t(\bar{r}, E, t) - \Sigma_t(\bar{r}, E)) \Psi(\bar{r}, \bar{\Omega}, E, t) \Phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dE dV \\ & + \frac{1}{F(t)} \iiint \iiint \Phi^*(\bar{r}, \bar{\Omega}, E) [(\Sigma_s(\bar{r}; \bar{\Omega}', E' \rightarrow \bar{\Omega}, E; t) - \Sigma_s(\bar{r}; \bar{\Omega}', E' \rightarrow \bar{\Omega}, E)) \\ & + \chi_p(E) (\nu \Sigma_f(\bar{r}, E', t) - \nu \Sigma_f(\bar{r}, E'))] \Psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' d\Omega dE dV \end{aligned} \quad (9)$$

$$\bar{\beta}(t) = \sum_j \bar{\beta}_j(t) \quad (10)$$

$$\begin{aligned} \bar{\beta}_j(t) = & \frac{1}{F(t)} \iiint \iiint \chi(E) \beta_j \nu \Sigma_f(\bar{r}, E') \Psi(\bar{r}, \bar{\Omega}', E', t) \\ & \times \Phi^*(\bar{r}, \bar{\Omega}, E) d\Omega' dE' d\Omega dE dV \end{aligned} \quad (11)$$

$$\Lambda(t) = \frac{1}{F(t)} \iiint \frac{1}{V} \Psi(\bar{r}, \bar{\Omega}, E, t) \phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dE dV \quad (12)$$

$$C_j(t) = \frac{(1/F(t))}{\Lambda} \iiint \phi^*(\bar{r}, \bar{\Omega}, E) C_j(\bar{r}, t) \chi_j(E) d\Omega dE dV \quad (13)$$

$$\bar{Q}(t) = \frac{(1/F(t))}{\Lambda} \iiint \phi^*(\bar{r}, \bar{\Omega}, E) Q(\bar{r}, \bar{\Omega}, E) d\Omega dE dV \quad (14)$$

$$F(t) = \iiint \iiint \chi(E) v \Sigma_f(\bar{r}, E') \Psi(\bar{r}, \bar{\Omega}', E', t) \phi_0^*(\bar{r}, \bar{\Omega}, E) d\Omega' dE' d\Omega dE dV \quad (15)$$

where,

$$\phi_0^* = \text{steady-state } k_{\text{eff}} \text{ adjoint flux.}$$

Note that $\Lambda(t)$ is called the prompt neutron lifetime in Reference 33, but is called the generation time in this work as well as other references.

2.3 Delayed Neutron Precursor Equations

The delayed neutron precursor equations are obtained by multiplying equation 2 by $\chi_j(E)\phi^*$, integrating over space, energy and angle, and using the separability condition given in equation 6 to yield the following equation for each precursor group:

$$\frac{\partial C_j(t)}{\partial t} + \lambda_j C_j(t) = \frac{\bar{\beta}_j(t)}{\Lambda} P(t) \quad j=1, N \quad (16)$$

2.4 Shape Equation

The shape equation is obtained by substituting the separability condition (equation 6) into the time-dependent Boltzmann transport equation and dividing by $P(t)$ to yield the following:

$$\begin{aligned} & \frac{1}{v} \cdot \frac{1}{P(t)} \cdot \frac{\partial P(t)}{\partial t} \cdot \Psi(\bar{r}, \bar{\Omega}, E, t) + \frac{1}{v} \frac{\partial \Psi(\bar{r}, \bar{\Omega}, E, t)}{\partial t} \\ & + \bar{\Omega} \cdot \bar{\nabla} \Psi(\bar{r}, \bar{\Omega}, E, t) + \Sigma_t(\bar{r}, E, t) \Psi(\bar{r}, \bar{\Omega}, E, t) \\ & = \iint \Sigma_s(\bar{r}; \bar{\Omega}', E' \rightarrow \bar{\Omega}, E; t) \Psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' \\ & + \iint \chi_p(E) (1-\beta) v \Sigma_f(\bar{r}, E', t) \Psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' \\ & \quad + \frac{Q_d(\bar{r}, E, t)}{P(t)} + \frac{Q}{P(t)} \end{aligned} \quad (17)$$

where,

$$\begin{aligned} Q_d(\bar{r}, E, t) &= \int_{-\infty}^t \int_{E'} \int_{\bar{\Omega}'} v \Sigma_f(\bar{r}, E', t) P(t') \Psi(\bar{r}, \bar{\Omega}', E', t) \\ &\quad \times \sum_j \beta_j \chi_j \lambda_j e^{-\lambda_j(t-t')} d\Omega' dE' dt' \end{aligned} \quad (18)$$

The quasistatic method, as originally applied in TDKENO, computes Q_a from equation 18 and uses this in equation 17 with $\partial\Psi/\partial t$ set equal to zero. The $[\partial P(t)/\partial t]/P(t)$ term is determined from the solution of the point kinetics equation (equation 8).

The improved quasistatic method, as applied in TDKENO-M, solves the full shape equation (equation 17) by replacing the time derivative of the shape function with a backward difference approximation of first order:

$$\frac{\partial}{\partial t} \psi(\bar{x}, \bar{\Omega}, E, t) = \frac{\psi(\bar{x}, \bar{\Omega}, E, t) - \psi(\bar{x}, \bar{\Omega}, E, t - \Delta t)}{\Delta t} \quad (19)$$

where,

$$\begin{aligned} t - \Delta t &= \text{time of the last shape calculation,} \\ \Delta t &= \text{time interval for shape calculations.} \end{aligned}$$

Since the shape function is usually slowly varying in time, this approximation is valid over a much larger time range than is acceptable for the total flux. Using the backward difference approximation for the time derivative of the shape function yields the following shape equation:

$$\begin{aligned}
& \frac{1}{v} \cdot \frac{1}{P(t)} \cdot \frac{\partial P(t)}{\partial t} \cdot \Psi(\bar{I}, \bar{\Omega}, E, t) + \frac{1}{v} \left(\frac{\Psi(\bar{I}, \bar{\Omega}, E, t) - \Psi(\bar{I}, \bar{\Omega}, E, t - \Delta t)}{\Delta t} \right) \\
& + \bar{\Omega} \cdot \bar{\nabla} \Psi(\bar{I}, \bar{\Omega}, E, t) + \Sigma_{\epsilon}(\bar{I}, E, t) \Psi(\bar{I}, \bar{\Omega}, E, t) \\
& = \iint \Sigma_s(\bar{I}; \bar{\Omega}', E' \rightarrow \bar{\Omega}, E; t) \Psi(\bar{I}, \bar{\Omega}', E', t) d\Omega' dE' \\
& + \iint \chi_p(E) (1 - \beta) v \Sigma_f(\bar{I}, E', t) \Psi(\bar{I}, \bar{\Omega}', E', t) d\Omega' dE' \\
& + \frac{Q_d(\bar{I}, E, t)}{P(t)} + \frac{Q}{P(t)}
\end{aligned} \tag{20}$$

which can be rearranged as:

$$\begin{aligned}
& \frac{1}{v} \left(\frac{1}{P(t)} \cdot \frac{\partial P(t)}{\partial t} + \frac{1}{\Delta t} \right) \Psi(\bar{I}, \bar{\Omega}, E, t) \\
& + \bar{\Omega} \cdot \bar{\nabla} \Psi(\bar{I}, \bar{\Omega}, E, t) + \Sigma_{\epsilon}(\bar{I}, E, t) \Psi(\bar{I}, \bar{\Omega}, E, t) \\
& - \iint \Sigma_s(\bar{I}; \bar{\Omega}', E' \rightarrow \bar{\Omega}, E; t) \Psi(\bar{I}, \bar{\Omega}', E', t) d\Omega' dE' \\
& - \iint \chi_p(E) (1 - \beta) v \Sigma_f(\bar{I}, E', t) \Psi(\bar{I}, \bar{\Omega}', E', t) d\Omega' dE' \\
& = \frac{Q_d(\bar{I}, E, t)}{P(t)} + \frac{Q}{P(t)} + \frac{\Psi(\bar{I}, \bar{\Omega}, E, t - \Delta t)}{v \Delta t}
\end{aligned} \tag{21}$$

This shape equation is an inhomogeneous partial differential equation. As with the quasistatic method, Q_d is computed from equation 18 and the $[\partial P(t)/\partial t]/P(t)$ term is determined from the solution of the point kinetics equation (equation 8). With the improved quasistatic method, there is now an additional $1/\Delta t$ term as well as an additional source term from the backward difference approximation of the shape derivative which is incorporated as described below.

The right hand side of the backward difference approximation (equation 19) is used to modify the source distribution in KENO V.a for each generation of neutrons. A random selection is made based on the cumulative distribution functions to determine whether each neutron is prompt, delayed, or contributes to the flux shape derivative. If a neutron is selected to be delayed, the starting energy, angle, and position are determined from the delayed source distribution. If the neutron is determined to contribute to the flux shape derivative, the starting parameters are selected based on the source distribution calculated from the numerical integration of the right hand side of the backward difference approximation. Note that prompt neutrons are tracked by KENO V.a without any modifications.

2.5 System Power

The system power can be represented by:

$$\begin{aligned}
 Power(t) &= \epsilon_f \iiint \Sigma_f(\bar{r}, E) \phi(\bar{r}, \bar{\Omega}, E, t) d\Omega dEdV \\
 &= P(t) \epsilon_f \iiint \Sigma_f(\bar{r}, E) \psi(\bar{r}, \bar{\Omega}, E, t) d\Omega dEdV
 \end{aligned}
 \tag{22}$$

where,

$$\epsilon_f = \text{average energy release per fission.}$$

2.6 Point Kinetics Parameters

The original version of TDKENO determines the point kinetics parameters (reactivity, generation time, etc.) during the random walk using the concept of

tracklength estimation to determine the following contribution to reactivity and generation time at every collision point and at every boundary crossing during the random walk of a Monte Carlo calculation:^{42,43,44}

$$\begin{aligned}
 \rho = & l \times wate [-\Delta \Sigma_t(\bar{r}, E', t) \phi_0^*(\bar{r}, \bar{\Omega}', E')] \\
 & + \iint \Delta \Sigma_s(\bar{r}; \bar{\Omega}', E' \rightarrow \bar{\Omega}, E; t) \phi_0^*(\bar{r}, \bar{\Omega}, E) d\Omega dE \quad (23) \\
 & + \iint \chi(E) \Delta v \Sigma_f(\bar{r}, E', t) \phi_0^*(\bar{r}, \bar{\Omega}, E) d\Omega dE]
 \end{aligned}$$

and

$$\Lambda = l \times wate \times \frac{1}{V} \phi_0^*(\bar{r}, \bar{\Omega}, E) \quad (24)$$

where,

l = tracklength
 $wate$ = neutron weight.

TDKENO-M determines the point kinetics parameters deterministically using their inner product definitions as given by equations 9-15 with an interpolated shape function. This allows the point kinetics parameters to be calculated at times intermediate to the flux shape calculations and, therefore, should provide improved accuracy relative to TDKENO for many transients of interest. This procedure should also be much more efficient than TDKENO since the additional histories required by TDKENO to have a small uncertainty in reactivity is avoided in TDKENO-M due to the fact that the reactivity is computed deterministically.

Chapter Three

Numerical Solution

3.1 Time-step Hierarchy

The shape equation (21), point kinetics equations (8 & 16), normalization constraint equation (7), and inner product definitions (9 through 15) are solved numerically using a hierarchy of three different integration time intervals as shown in Figure 1.

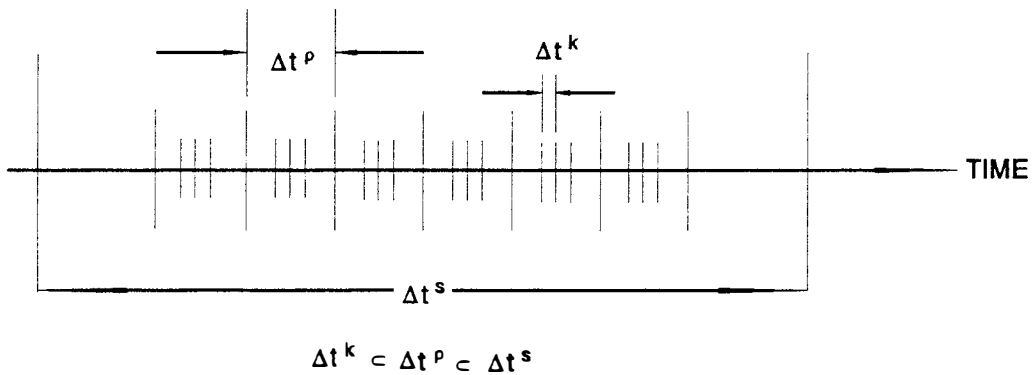


Figure 1: Time-step Hierarchy in the Improved Quasistatic Method

The shape function is assumed to vary linearly over the largest time interval, Δt^s , where for the n^{th} time interval, $\Delta t_n^s = t_n^s - t_{n-1}^s$. The reactivity, delayed neutron fraction, and the generation time are calculated using the Δt^p time intervals with linearly interpolated flux shapes. The Δt^k time intervals are used for solving the point kinetics equations as well as the delayed neutron spatial precursor concentrations with

quadratically (second order) interpolated point kinetics parameters.

3.2 Solution Algorithm

A general description of the solution algorithm for the improved quasistatic method is given below:

1. Assume everything is known at time t_{n-1}^s .
2. Extrapolate the shape function, $\Psi(\bar{r}, \bar{\Omega}, E, t)$, linearly with respect to time from $\Psi(\bar{r}, \bar{\Omega}, E, t_{n-1}^s)$ to $\Psi(\bar{r}, \bar{\Omega}, E, t_n^s)$.
3. Evaluate reactivity, generation time, and delayed neutron fraction at the t_n^s points out to t_n^s using equations 9-15 with an interpolated shape function.
4. Interpolate reactivity, generation time and delayed neutron fraction quadratically (second order) between t_{n-1}^s and t_n^s at the t^k points.
5. Solve the point kinetics equations and update the delayed neutron precursor spatial distribution using LSODE out to t_n^s at the t^k points using interpolated point kinetics parameters.
6. If the problem considers thermalhydraulic feedback (i.e., Benchmark 14-A2), compute the temperature distribution out to t_n^s at the t^k points using the adiabatic heatup model.
7. If $t_n^s < t_n^s$, go to the next t_n^s time point and repeat Steps 4 through 7.
8. If $t_n^s = t_n^s$, calculate a new flux shape.
9. Normalize the flux shape to satisfy the normalization constraint equation.
10. Repeat steps 3 through 7 until $t_n^s = t_n^s$ using a shape function, $\Psi(\bar{r}, \bar{\Omega}, E, t)$, which is linearly interpolated with respect to time from $\Psi(\bar{r}, \bar{\Omega}, E, t_{n-1}^s)$ to $\Psi(\bar{r}, \bar{\Omega}, E, t_n^s)$.
11. Go to the next Δt^s time interval and repeat Steps 2 through 10.

Chapter Four

TDKENO-M

4.1 Introduction

TDKENO-M is a Fortran code which solves the time-dependent, three-dimensional Boltzmann transport equation with explicit representation of delayed neutrons as given by equations 1 and 2. The code consists of several large subroutines which perform specific functions as described below:

1. KENO V.a Modified to perform a fixed source calculation with user-defined angular binning and to explicitly track delayed neutrons based on the distribution function given by equation 18. KENO V.a was also modified to include the flux shape derivative with the fixed source term using a backward difference approximation of first order (equation 19). Note that the modified version of KENO V.a uses both AMPX and Monte Carlo formatted binary cross section libraries.³²
2. RHO Determines the point kinetics parameters (reactivity, generation time and effective delayed neutron fraction) from their inner product definitions as given by equations 9 through 15.
3. PTKIN Solves the point kinetics equations using the Livermore Solver of Ordinary Differential Equations (LSODE).
4. CDELAY Calculates the delayed neutron precursor spatial distribution (equation 18) as well as the cumulative distribution functions used to incorporate the flux shape derivative.
5. POWER Determines the power history using equation 22.

Refer to the user's manual as well as the code listing given in Appendix B for greater detail on the individual subroutines as well as the input and output files for a sample problem.

4.2 Computational Flow

The computational flow for a typical TDKENO-M calculation is given in Figure 2. Initially, a steady-state adjoint calculation is performed using the modified version of KENO V.a. This steady state adjoint flux is used for all subsequent calculations of the point kinetics parameters. Next, a steady-state forward KENO V.a calculation is performed to determine the initial flux shape as well as the effective multiplication factor. Next, subroutines RHO and PTKIN are called to determine the initial values of the point kinetics parameters and the flux amplitude, respectively. In the case of thermalhydraulic feedback (i.e., Benchmark 14-A2), subroutine FEEDBACK is called to calculate the system temperature from the adiabatic heatup model described in Appendix C as well as the system power. Note that the system power calculated by subroutine FEEDBACK is only used intermediately to calculate the system temperature and is not written as output. The subroutine CDELAY is then called by TDKENO-M to determine the delayed neutron source distribution as well as the cumulative distribution functions needed for the implementation of the flux shape derivative for the transient calculations.

TDKENO-M next calls KENO V.a to perform the first flux shape calculation of the perturbed system. Subsequently, subroutines RHO, PTKIN and CDELAY are called again to update the system parameters and the amplitude as described above. This sequence is continued until the desired cutoff time is reached for the transient calculation. Upon the completion of the transient calculation, subroutine POWER is used to determine the power trace for the system.

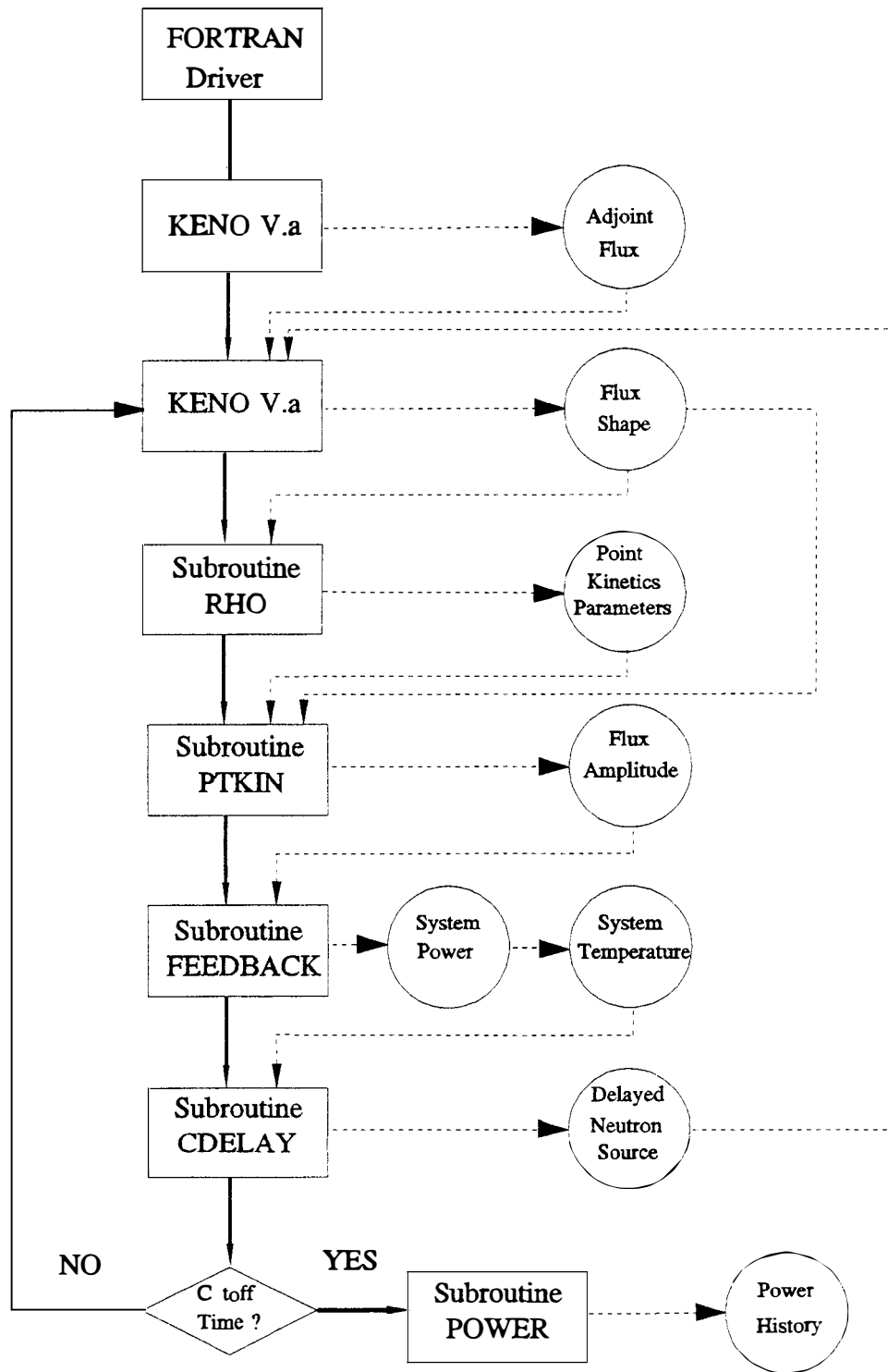


Figure 2: Computational Flow for TDKENO-M

Chapter Five

Results

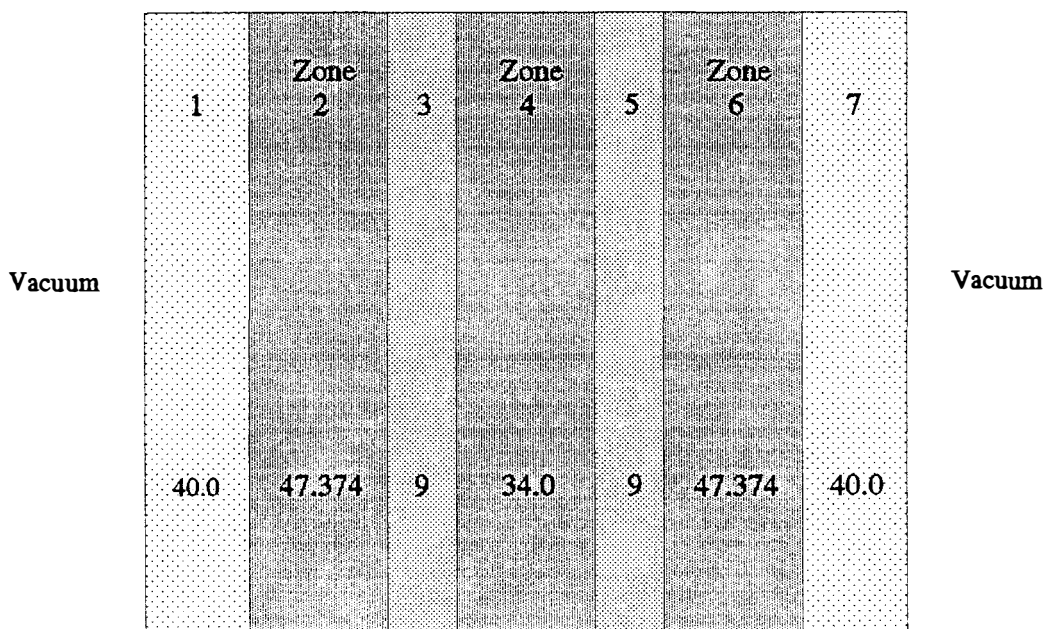
5.1 Introduction

To verify that TDKENO-M accurately solves the three-dimensional, time-dependent Boltzmann transport equation with explicit representation of delayed neutrons, TDKENO-M was used to model benchmark problems 16-A1, 16-A2, 16-A3, 16-A6^a, 16-A7^a, and 14-A2 in the Argonne National Laboratory Benchmark Problem Book⁴⁵ using a Hewlett-Packard 9000 model 730 workstation. Problems 16-A1, 16-A2, 16-A3, 16-A6 and 16-A7 are one-dimensional, two-group transient problems for which solutions have been determined using the one-dimensional transport codes TDA²⁹ and TIMEX³⁰. Problem 14-A2 is a prompt-critical transient in three dimensions with adiabatic heatup and Doppler feedback designed to test codes based on two-group diffusion theory. Note that one-dimensional transport benchmarks and three-dimensional diffusion benchmarks are used in this work since transient, three-dimensional transport benchmarks do not exist. Further, even though the 16A series of benchmark problems are one-dimensional problems, TDKENO-M still performs all calculations in three dimensions. A complete description of the benchmark problems is given in Appendix B.

a Benchmark problems 16-A6 and 16-A7 are unpublished benchmark problems which use the same geometrical configuration and data as Benchmark problem 16-A1.

5.2 Benchmark Problem 16-A1

Problem 16-A1 is a seven region, one-dimensional slab liquid metal fast breeder reactor (LMFBR). The configuration consists of three core regions (zones 2, 4, and 6) containing core material and sodium, two control rod regions (zones 3 and 5) containing control rod material and sodium, and two fuel blanket regions (zones 1 and 7) containing blanket material and sodium. Refer to Figure 3 for a schematic representation of the problem. Two neutron energy groups and six delayed neutron groups are used (Tables 1 and 2). The initiating perturbation is caused by a 5% increase in density of the material in zone 2 and a 5% decrease in density of the material in zone 6 resulting in a delayed supercritical transient.



Note: All Dimensions are in Centimeters

Figure 3: Schematic Diagram of Benchmark Problem 16-A1

Table 1: Benchmark Problem 16-A1 Initial Two-Group Data

Zone	Group	$\nu\Sigma_f^i$	Σ_t^i	$\Sigma_s^{i\rightarrow i}$	$\Sigma_s^{i\rightarrow j}$
1,7	1	8.3441×10^{-4}	2.411×10^{-1}	2.336×10^{-1}	3.598×10^{-3}
	2	3.2776×10^{-4}	4.172×10^{-1}	4.070×10^{-1}	0.0
2,4,6	1	7.4518×10^{-3}	1.849×10^{-1}	1.777×10^{-1}	2.085×10^{-3}
	2	1.1061×10^{-2}	3.668×10^{-1}	3.537×10^{-1}	0.0
3,5	1	0.0	9.432×10^{-2}	8.571×10^{-2}	1.717×10^{-3}
	2	0.0	1.876×10^{-1}	1.713×10^{-1}	0.0

Table 2: Benchmark Problem 16-A1 Delayed Neutron Parameters^a

Delayed Neutron Group	Delayed Neutron Fraction, β	Decay Constant, λ
1	8.10×10^{-5}	1.29×10^{-2}
2	6.87×10^{-4}	3.11×10^{-2}
3	6.12×10^{-4}	1.34×10^{-1}
4	1.14×10^{-3}	3.31×10^{-1}
5	5.12×10^{-4}	1.26
6	1.70×10^{-4}	3.21

^aPrompt and delayed neutron spectra are identical with $\chi_1 = 1.0$ and $\chi_2 = 0.0$.
 Also, $1/v_1 = 1.851 \times 10^{-9}$ sec/cm and $1/v_2 = 1.088 \times 10^{-8}$ sec/cm.

Results obtained with TDKENO-M as well as TIMEX and TDA for Benchmark Problem 16-A1 are given in Figures 4-6 and Table 3. Figure 4 is a plot of normalized power versus time (power trace). Figures 5 and 6 are plots of the normalized flux distribution for neutron energy groups one and two, respectively. Table 3 is a tabular representation of the CPU time and the error (as compared to TIMEX and TDA) associated with both TDKENO and TDKENO-M due to a reduction of the total number of histories for each flux shape calculation. As the number of histories decreases, the accuracy of TDKENO-M is much better than TDKENO. This is because TDKENO-M computes reactivity and generation time deterministically rather than using the stochastic method (i.e., boundary crossing estimation) used by TDKENO which requires a huge number of histories to obtain acceptable uncertainties.

The results show that TDKENO-M is quite accurate in comparison with Benchmark Problem 16-A1 (approximately 2% error in power trace) with as much as a factor of 400 reduction in CPU time relative to TDKENO. Note that the results presented were obtained by performing shape calculations at 0.0, 10^{-6} , 10^{-5} , and 10^{-2} seconds. Further, ten intermediate calculations of the point kinetics parameters are performed between each shape calculation and ten flux amplitude calculations are performed between each calculation of the point kinetics parameters. Also, 21 spatial mesh intervals are used for modeling Benchmark Problem 16-A1 as described in Appendix D.

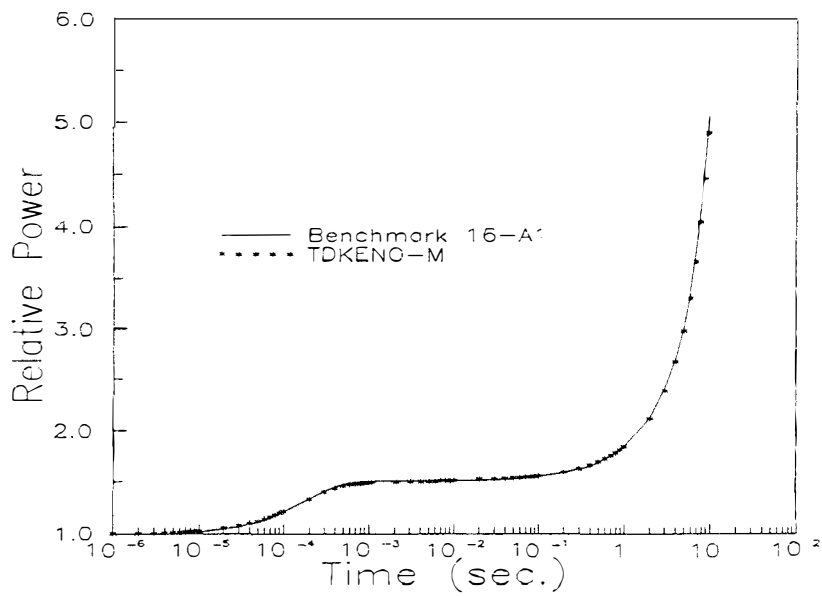


Figure 4: Relative Power vs Time for Benchmark Problem 16-A1

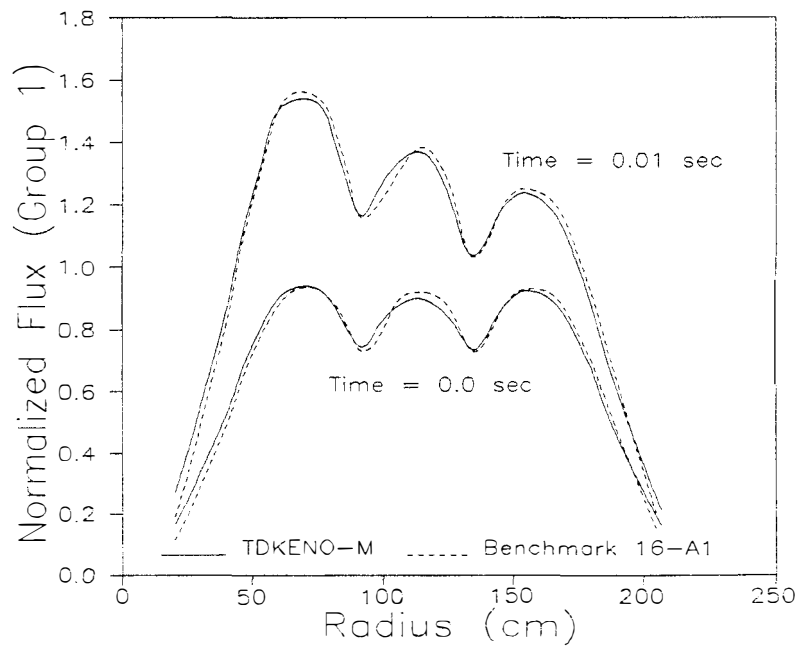


Figure 5: Normalized Group 1 Flux vs Radial Position for Problem 16-A1

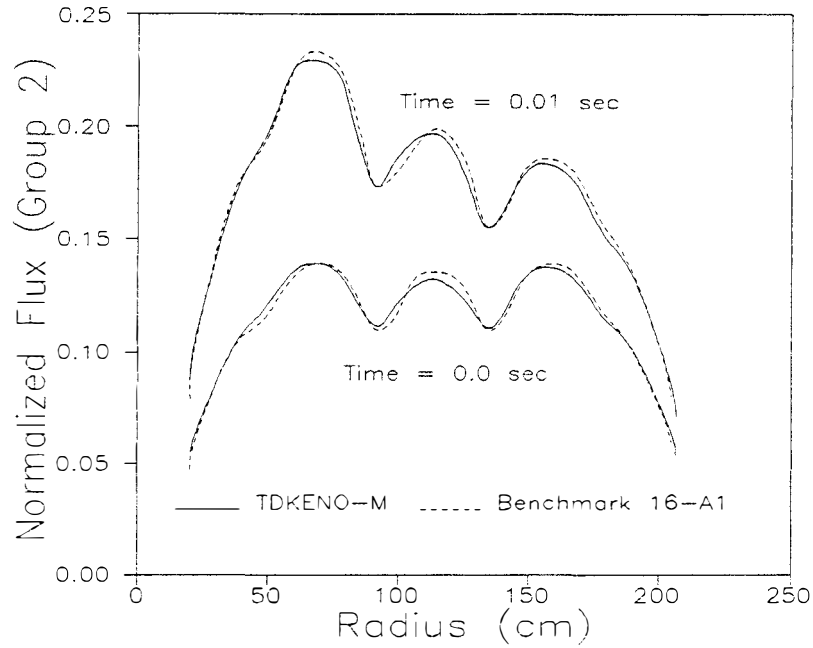


Figure 6: Normalized Group 2 Flux vs Radial Position for Problem 16-A1

Table 3: Results for Benchmark Problem 16-A1

Fraction of Original Histories	CPU Time* (min.)	Average Shape* Deviation (%)	Average Power Deviation (%) TDKENO	Average Power Deviation (%) TDKENO-M
1	2023	0.25	0.41	0.13
1/2	1019	0.51	2.02	0.16
1/4	509	0.72	3.64	0.21
1/10	213	0.86	12.62	0.39
1/100	23.6	2.13	69.23	1.02
1/1000	4.8	7.24	154.3	2.14

*Values of CPU Time and Average Flux Deviation are for both TDKENO and TDKENO-M since these parameters depend primarily on the total number of histories and not the solution methodology.

5.3 Benchmark Problem 16-A2

Problem 16-A2 is identical to Benchmark 16-A1 except for the initiating perturbation which is a 10% increase in density in core zone 2 and a 10% decrease in density of core zone 6 (refer to Figure 3 on page 25). These perturbations result in a prompt supercritical transient.

Results obtained with TDKENO-M as well as TIMEX and TDA for Benchmark Problem 16-A2 are given in Figure 7 and Table 4. Figure 7 is a plot of normalized power versus time (power trace). Table 4 is a tabular representation of the CPU time and the error (as compared to TIMEX and TDA) associated with both TDKENO and TDKENO-M. Similar to Benchmark Problem 16-A1, as the number of histories decreases, the accuracy of TDKENO-M is much better than TDKENO.

Results show that TDKENO-M is quite accurate in comparison with Benchmark Problem 16-A2 (approximately 2.4% error in power trace) with as much as a factor of 700 reduction in CPU time relative to TDKENO. Note that the results presented were obtained by performing flux shape calculations at 0.0, 10^{-4} , and 1.1×10^{-3} seconds. Further, ten intermediate calculations of the point kinetics parameters are performed between each shape calculation and ten flux amplitude calculations are performed between each calculation of the point kinetics parameters. Also, 32 spatial mesh intervals are used for modeling Benchmark Problem 16-A2 as described in Appendix D.

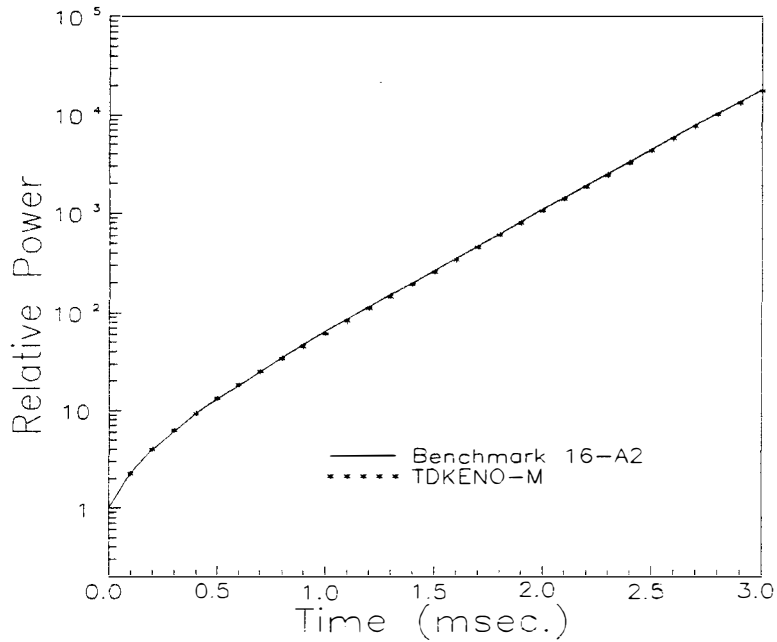


Figure 7: Relative Power vs Time for Benchmark Problem 16-A2

Table 4: Results for Benchmark Problem 16-A2

Fraction of Original Histories	CPU Time* (min.)	Average Shape* Deviation (%)	Average Power Deviation (%) TDKENO	Average Power Deviation (%) TDKENO-M
1	7201	0.23	0.37	0.25
1/2	3604	0.49	1.84	0.32
1/4	1805	0.76	3.96	0.38
1/10	725	0.88	10.73	0.43
1/100	75.4	2.52	58.80	1.38
1/1000	9.75	6.03	136.9	2.43

*Values of CPU Time and Average Flux Deviation are for both TDKENO and TDKENO-M since these parameters depend primarily on the total number of histories and not the solution methodology.

5.4 Benchmark Problem 16-A3

Benchmark Problem 16-A3 simulates the complete ejection of a control rod from the reactor followed by a complete control rod insertion at a different location. Initially, the material in zone 5 is changed from a mixture of sodium and control rod material to complete sodium. Then, at 0.0001 sec, the material in zone 3 is changed from a mixture of sodium and control rod material to 100% control rod material.

Results obtained with TDKENO-M as well as TIMEX and TDA for Benchmark Problem 16-A3 are given in Figure 8 and Table 5. Figure 8 is a plot of normalized power versus time. Table 5 gives the CPU time and the error (as compared to TIMEX and TDA) associated with both TDKENO and TDKENO-M. Results show that TDKENO-M is quite accurate in comparison with Benchmark Problem 16-A3 (approximately 2.5% error in power trace) with as much as a factor of 350 reduction in CPU time relative to TDKENO. The results presented were obtained by performing shape calculations at 0.0, 2×10^{-6} , 5×10^{-5} , 9×10^{-5} , 1×10^{-4} , 1.01×10^{-4} and 1.5×10^{-3} seconds using 29 mesh intervals as described in Appendix D.

It should be noted that the power trace discrepancy after the control rod insertion as encountered with TDKENO⁴⁴ (see Figure 8) is not present using TDKENO-M. This is due to the fact that the flux shape derivative term is included in TDKENO-M while it is ignored in TDKENO. Thus, the flux shape derivative creates a retardation time which, if not modeled, causes the power trace to be shifted towards larger times.

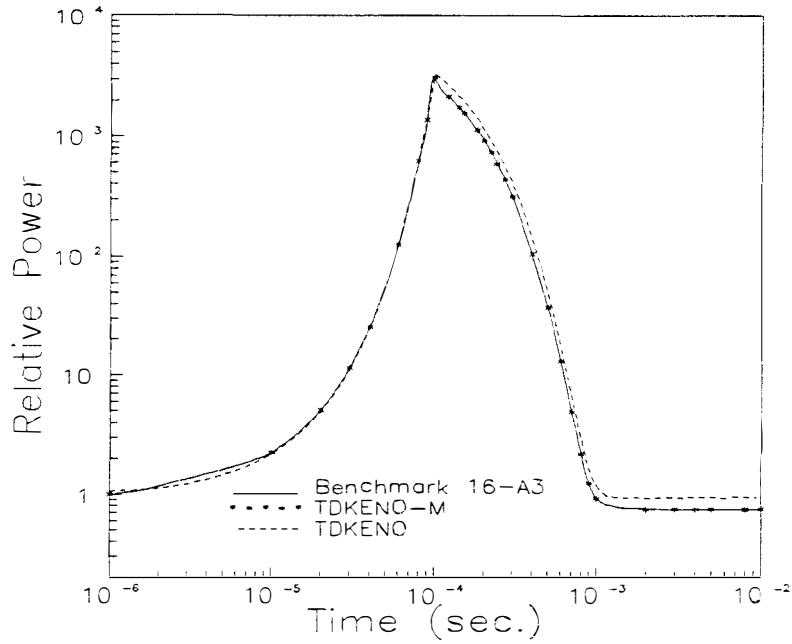


Figure 8: Relative Power vs Time for Benchmark Problem 16-A3

Table 5: Results for Benchmark Problem 16-A3

Fraction of Original Histories	CPU Time* (min.)	Average Shape* Deviation (%)	Average Power Deviation (%) TDKENO	Average Power Deviation (%) TDKENO-M
1	3145	0.32	0.71	0.15
1/2	1575	0.64	3.74	0.18
1/4	789	0.89	4.96	0.24
1/10	319	0.96	15.30	0.45
1/100	35.2	2.53	79.48	1.13
1/1000	8.42	8.82	217.8	2.56

*Values of CPU Time and Average Flux Deviation are for both TDKENO and TDKENO-M since these parameters depend primarily on the total number of histories and not the solution methodology.

5.5 Benchmark Problem 16-A6

Problem 16-A6 simulates both control rod movement and material motion. The transient is initiated by a decrease in control rod material and an increase in sodium in zone 5 resulting in the cross sections for zone 5 at $t \geq 0.0$ seconds given in Table 6. Also, for the time interval between $t = 0.0$ and $t = 0.5$ seconds, the densities of the materials in zones 1, 2, 4, 6, and 7 are changed linearly (i.e., material motion) resulting in final cross sections for each zone at $t = 0.5$ sec as shown in Table 7.

Results obtained with TDKENO-M as well as TIMEX and TDA for Benchmark Problem 16-A6 are given in Figure 9 and Table 8. Figure 9 is a plot of normalized power versus time. Table 8 is a tabular representation of the CPU time and the error (as compared to TIMEX and TDA) associated with both TDKENO and TDKENO-M.

Results show that TDKENO-M is quite accurate in comparison with Benchmark Problem 16-A6 (approximately 2.1% error in power trace) with as much as a factor of 90 reduction in CPU time relative to TDKENO. Note that the results presented were obtained by performing flux shape calculations at 0.0, 10^{-5} , 10^{-2} , 10^{-1} , 2×10^{-1} , and 5×10^{-1} seconds using 36 mesh intervals as described in Appendix D. Further, ten intermediate calculations of the point kinetics parameters are performed between each shape calculation and ten flux amplitude calculations are performed between each calculation of the point kinetics parameters.

Table 6: Two-Group Constants for Step Perturbation in Zone 5

Energy Group	Σ_t^i	$\Sigma_s^{i \rightarrow i}$	$\Sigma_s^{i \rightarrow j}$
1	9.05399×10^{-2}	8.24499×10^{-2}	1.6550×10^{-3}
2	1.7860×10^{-1}	1.640×10^{-1}	0.0

Table 7: Two-Group Constants for Ramp Perturbations

Zone	Group	$\nu \Sigma_f^i$	Σ_t^i	$\Sigma_s^{i \rightarrow i}$	$\Sigma_s^{i \rightarrow j}$
1	1	1.71696×10^{-3}	2.62999×10^{-1}	2.54691×10^{-1}	3.8449×10^{-3}
	2	1.63779×10^{-3}	4.60642×10^{-1}	4.48897×10^{-1}	0.0
2	1	6.70661×10^{-3}	1.6641×10^{-1}	1.5994×10^{-1}	1.8765×10^{-3}
	2	9.95507×10^{-3}	3.3012×10^{-1}	3.18349×10^{-1}	0.0
4,6	1	2.98072×10^{-3}	7.39599×10^{-2}	7.10843×10^{-2}	8.3399×10^{-3}
	2	4.42448×10^{-3}	1.4672×10^{-1}	1.41488×10^{-1}	0.0
7	1	9.93014×10^{-3}	4.66791×10^{-1}	4.50559×10^{-1}	6.1429×10^{-3}
	2	1.38292×10^{-2}	8.64919×10^{-1}	8.38759×10^{-1}	0.0

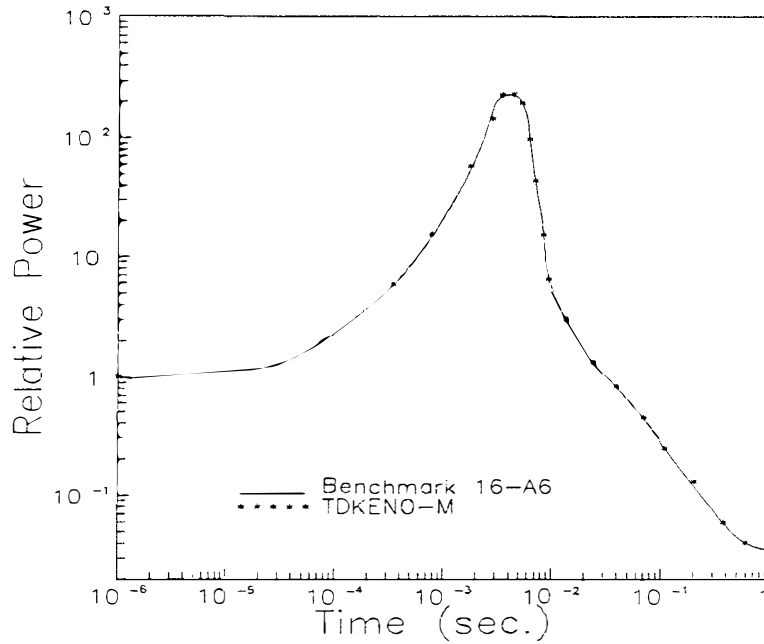


Figure 9: Relative Power vs Time for Benchmark Problem 16-A6

Table 8: Results for Benchmark Problem 16-A6

Fraction of Original Histories	CPU Time* (min.)	Average Shape* Deviation (%)	Average Power Deviation (%) TDKENO	Average Power Deviation (%) TDKENO-M
1	866	0.53	0.62	0.31
1/2	435	1.17	4.49	0.42
1/4	219	1.62	8.69	0.69
1/10	88.2	1.95	39.83	0.93
1/100	9.23	4.58	204.72	2.13

*Values of CPU Time and Average Flux Deviation are for both TDKENO and TDKENO-M since these parameters depend primarily on the total number of histories and not the solution methodology.

5.6 Benchmark Problem 16-A7

Benchmark Problem 16-A7 is identical to Benchmark Problem 16-A6 except that the ramp representing material motion is replaced with a step perturbation at 0.01 seconds. Results obtained with TDKENO-M as well as TIMEX and TDA for Benchmark Problem 16-A7 are given in Figure 10 and Table 9. Figure 10 is a plot of normalized power versus time (power trace). Table 9 is a tabular representation of the CPU time and the error (as compared to TIMEX and TDA) associated with both TDKENO and TDKENO-M. Also, 36 spatial mesh intervals are used for modeling Benchmark Problem 16-A7 as described in Appendix D.

Results show that TDKENO-M is quite accurate in comparison with Benchmark Problem 16-A7 (approximately 3.1% error in the power trace) with as much as a factor of 95 reduction in the CPU time relative to TDKENO. Note that the results presented were obtained by performing flux shape calculations at 0.0, 5×10^{-5} , 1×10^{-4} , 10^{-2} , 1.1×10^{-2} , 2×10^{-2} , and 10^{-1} seconds using 36 mesh intervals as described in Appendix D. Further, ten intermediate calculations of the point kinetics parameters are performed between each flux shape calculation and ten flux amplitude calculations are performed between each calculation of the point kinetics parameters.

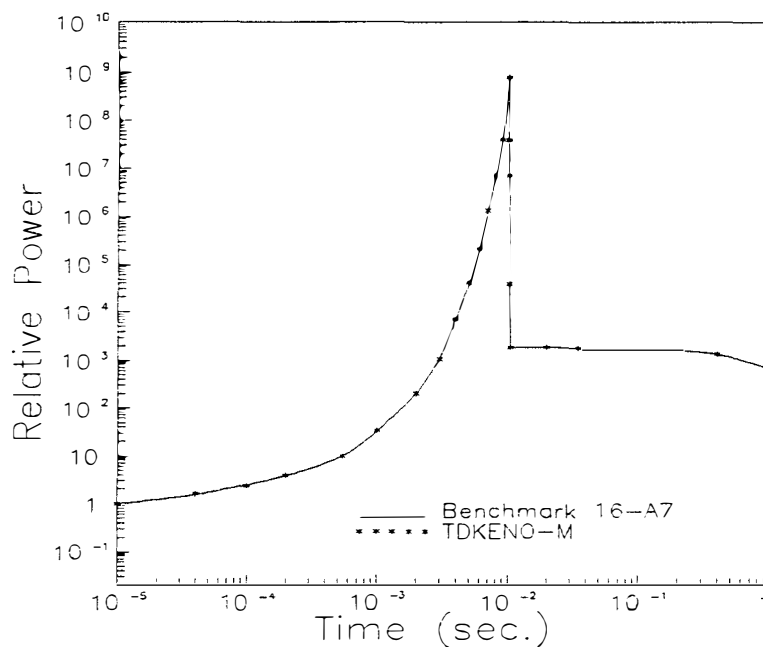


Figure 10: Relative Power vs Time for Benchmark Problem 16-A7

Table 9: Results for Benchmark Problem 16-A7

Fraction of Original Histories	CPU Time* (min.)	Average Shape* Deviation (%)	Average Power Deviation (%) TDKENO	Average Power Deviation (%) TDKENO-M
1	398	0.64	0.66	0.43
1/2	200	1.41	4.80	0.55
1/4	101	1.96	9.25	0.86
1/10	40.5	2.35	97.3	1.29
1/100	4.21	5.53	500.2	3.14

*Values of CPU Time and Average Flux Deviation are for both TDKENO and TDKENO-M since these parameters depend primarily on the total number of histories and not the solution methodology.

5.7 Benchmark Problem 14-A2

Benchmark Problem 14-A2 is a three-dimensional model of a Boiling Water Reactor (BWR) in which the initiating perturbation is the complete withdrawal of a control rod resulting in a super-prompt transient. Refer to Figures 11 and 12 for a schematic representation of the problem as well as material/region assignments. Note that the region denoted by R is the location of the control rod to be withdrawn. Two neutron energy groups and two delayed neutron groups are used for Benchmark Problem 14-A2 (Tables 10 and 11). Finally, the problem includes a feedback model with adiabatic heatup and Doppler feedback as described in Appendix C.

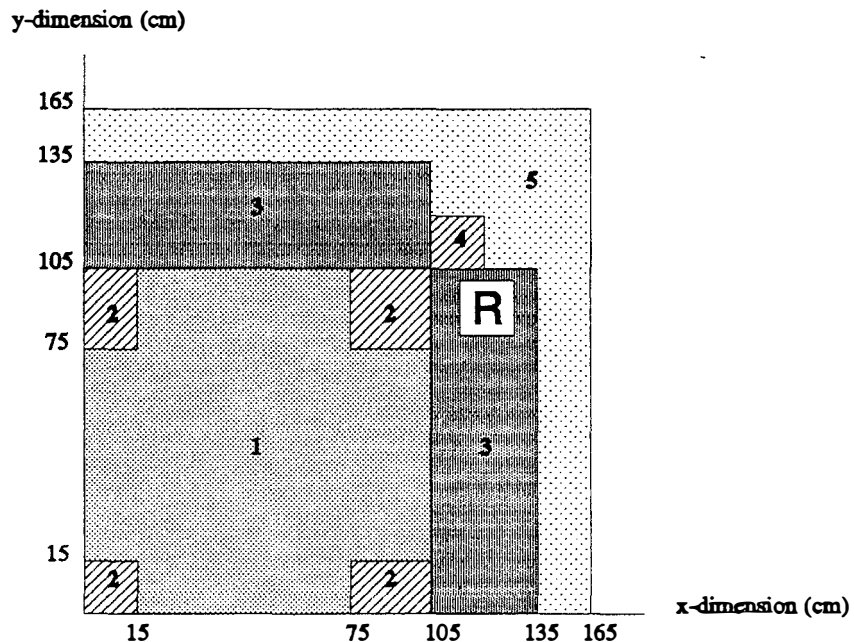


Figure 11: Quadrant of Reactor Horizontal Cross Section for Benchmark 14-A2

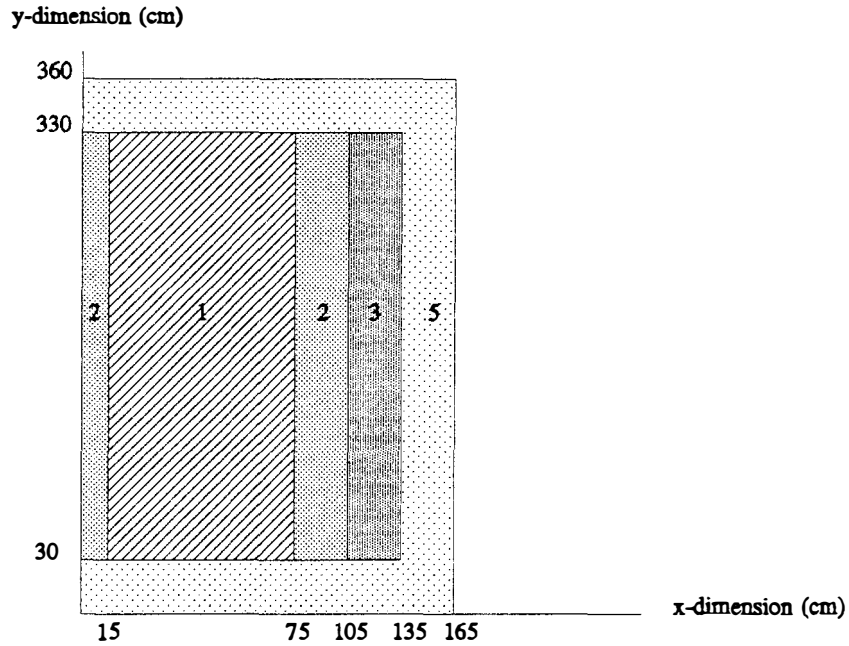


Figure 12: Reactor Vertical Cross Section for Benchmark 14-A2

Table 10: Benchmark Problem 14-A2 Delayed Neutron Parameters^a

Delayed Neutron Group	Delayed Neutron Fraction, β	Decay Constant, λ
1	5.40×10^{-3}	6.54×10^{-3}
2	1.087×10^{-3}	1.35

^aPrompt and delayed neutron spectra are identical with $\chi_1=1.0$ and $\chi_2=0.0$. Also, $1/v_1 = 3.333 \times 10^{-6}$ sec/cm and $1/v_2 = 3.333 \times 10^{-4}$ sec/cm.

Table 11: Benchmark Problem 14-A2 Initial Two-Group Data

Zone	Material	Group	D_i	Σ_a^i	$\nu\Sigma_f^i$	$\Sigma_s^{1\rightarrow 2}$
1	Fuel 1 with rod	1	1.255	8.252×10^{-3}	4.602×10^{-3}	2.533×10^{-2}
		2	0.211	1.003×10^{-1}	1.091×10^{-1}	
2	Fuel 2 without rod	1	1.268	7.181×10^{-3}	4.609×10^{-3}	2.767×10^{-2}
		2	0.1902	7.047×10^{-2}	8.675×10^{-2}	
3	Fuel 2 with rod	1	1.259	8.002×10^{-3}	4.663×10^{-3}	2.617×10^{-2}
		2	0.2091	8.344×10^{-2}	1.021×10^{-1}	
4	Fuel 2 without rod	1	1.259	8.002×10^{-3}	4.663×10^{-3}	2.617×10^{-2}
		2	0.2091	7.332×10^{-2}	1.021×10^{-1}	
5	Reflector	1	1.257	6.034×10^{-4}	0.0	4.754×10^{-2}
		2	0.1592	1.911×10^{-2}	0.0	

Problem 14-A2 was designed for testing diffusion codes; therefore, diffusion coefficients are given rather than total cross sections. The cross sections are obtained from the diffusion coefficients using the following equation:²²

$$D = \frac{1}{3 \Sigma_s (1 - \overline{\cos \psi})}$$

where,

- D = diffusion coefficient,
- Σ_s = scattering cross section,
- ψ = scattering angle in the laboratory system.

Isotropic scattering in the laboratory system is assumed which causes the average cosine term to vanish. The total cross section is then obtained from the addition of the scattering and absorption cross sections.

Results obtained with TDKENO-M as well as IQSBOX⁴⁸ for Benchmark Problem 14-A2 are given in Figures 13 and 14 and Table 12. Figure 13 is a plot of normalized power versus time (power trace). Figure 14 is a plot of the average core temperature versus time. Table 12 is a tabular representation of the CPU time and the error (as compared to IQSBOX) associated with both TDKENO and TDKENO-M due to a reduction of the total number of histories for each flux shape calculation.

Results show that TDKENO-M provides adequate accuracy in comparison with Benchmark Problem 14-A2 (less than 6.5% error in power trace) with as much as a factor of 9.4 reduction in CPU time relative to TDKENO. Note that the results presented were obtained by performing 30 flux shape calculations. Further, ten intermediate calculations of the point kinetics parameters are performed between each flux shape calculation and ten flux amplitude calculations are performed between each calculation of the point kinetics parameters. Also, 217 spatial mesh intervals are used for both the neutronic and thermalhydraulic modeling of Benchmark Problem 14-A2 as described in Appendix D.

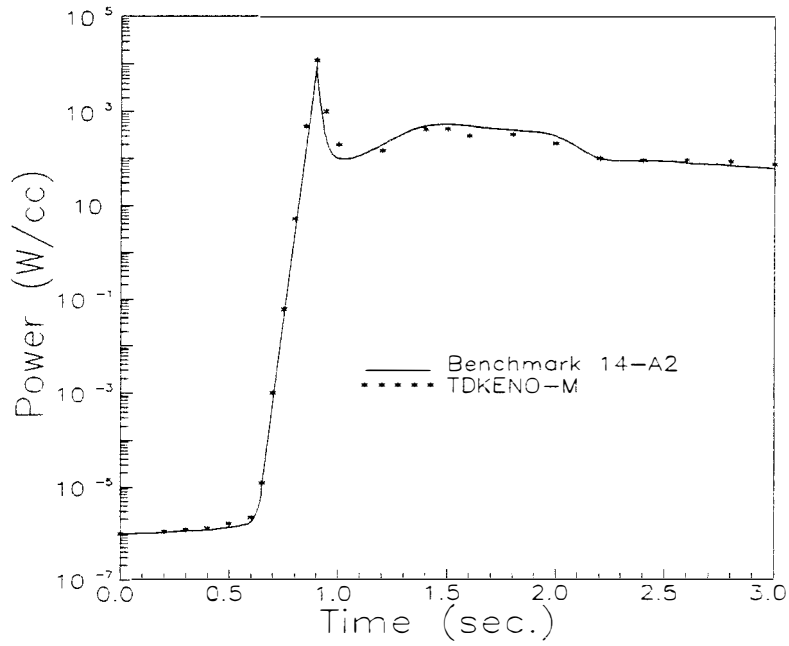


Figure 13: Power vs Time for Benchmark Problem 14-A2

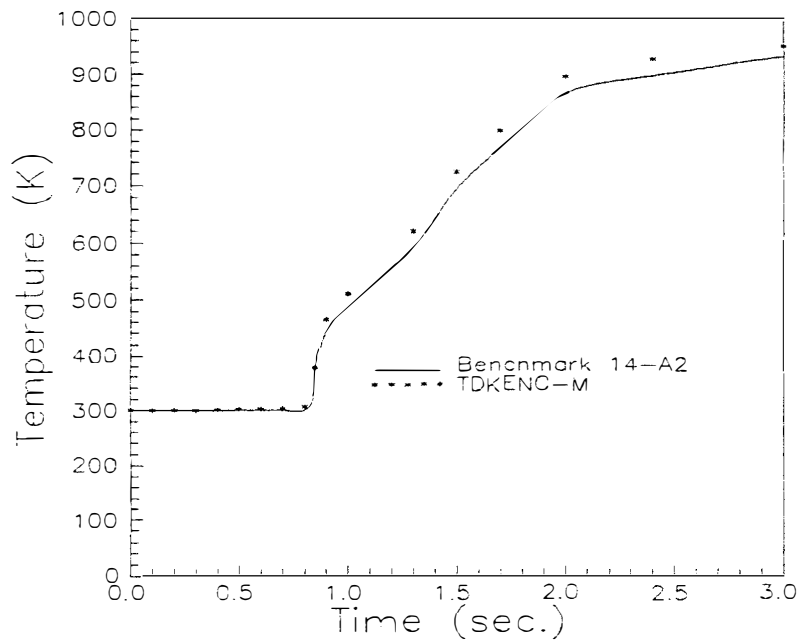


Figure 14: Average Temperature vs Time for Benchmark Problem 14-A2

Table 12: Results for Benchmark Problem 14-A2

Fraction of Original Histories	CPU Time* (min.)	Average Shape* Deviation (%)	Average Power Deviation (%) TDKENO	Average Power Deviation (%) TDKENO-M
1	2339	0.97	29.5	1.64
1/2	1198	2.19	105	1.83
1/4	605	5.45	133	2.20
1/10	249	10.5	285	6.38

*Values of CPU Time and Average Flux Deviation are for both TDKENO and TDKENO-M since these parameters depend primarily on the total number of histories and not the solution methodology.

Chapter Six

Sensitivity Studies

6.1 Introduction

Several of the user-specified input parameters used by TDKENO-M are somewhat arbitrary. Therefore, the sensitivity which these parameters have on the results is investigated in this chapter. Parameters considered in this investigation include 1.) the total number of histories per shape calculation, 2.) the number of shape calculations, and 3.) the number of reactivity and point kinetics time steps. Note that all sensitivity studies presented in this chapter are for Benchmark Problem 16-A1.

6.2 Sensitivity to Total Histories

As described in Chapter 5, as the number of histories decreases, the accuracy of TDKENO-M is much better than TDKENO. This is because TDKENO-M computes reactivity and generation time deterministically rather than using the stochastic method (i.e., boundary crossing estimation) used by TDKENO which requires a huge number of histories to obtain acceptable uncertainties. Table 3 (page 29) is a tabular representation of the CPU time and the error (as compared to TIMEX and TDA) associated with both TDKENO and TDKENO-M due to a reduction of the total number of histories for each flux shape calculation.

Results show that the average power deviation as calculated by TDKENO-M is approximately 2% error in comparison with Benchmark Problem 16-A1 with as much as a factor of 400 reduction in CPU time relative to TDKENO.

6.3 Sensitivity to Number of Shape Calculations

The effect of a reduction in the total number of shape calculations is investigated in this section. Since TDKENO-M determines the point kinetics parameters using their inner product definitions, they can be calculated at times intermediate to the flux shape calculations. The ability to calculate point kinetics parameters at intermediate times should reduce the number of shape calculations for many transients of interest.

Figure 15 is a plot of normalized power versus time for Problem 16-A1 without a shape calculation at 10^{-5} seconds. Results of this calculation show that the power trace calculated by TDKENO-M differs from the benchmark results by approximately 3%. Figure 16 is a power trace for Benchmark Problem 16-A1 without a shape calculation at 10^{-2} seconds. Results of this calculation show that the power trace calculated by TDKENO-M differs from the benchmark results by approximately 26%. The large error for this calculation can be attributed to the errors produced by extrapolating the flux shape from 10^{-5} seconds to 10.0 seconds. Thus, the user should be careful to ensure that the total number of shape calculations as well as the spacing of the flux shape calculations is appropriate for the problem of interest.

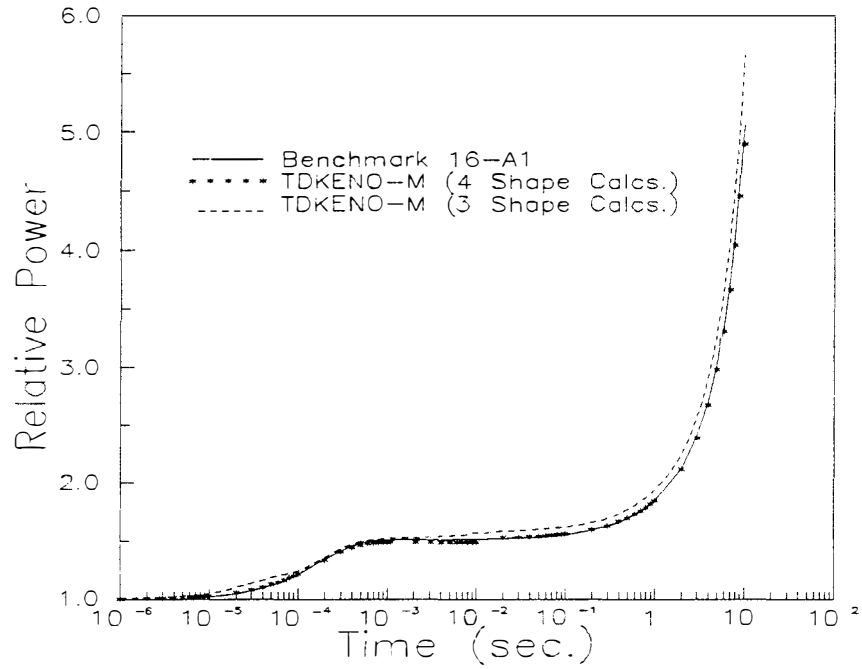


Figure 15: Power Trace for Benchmark Problem 16-A1 without Flux Shape Calculation at 10^{-5} Seconds

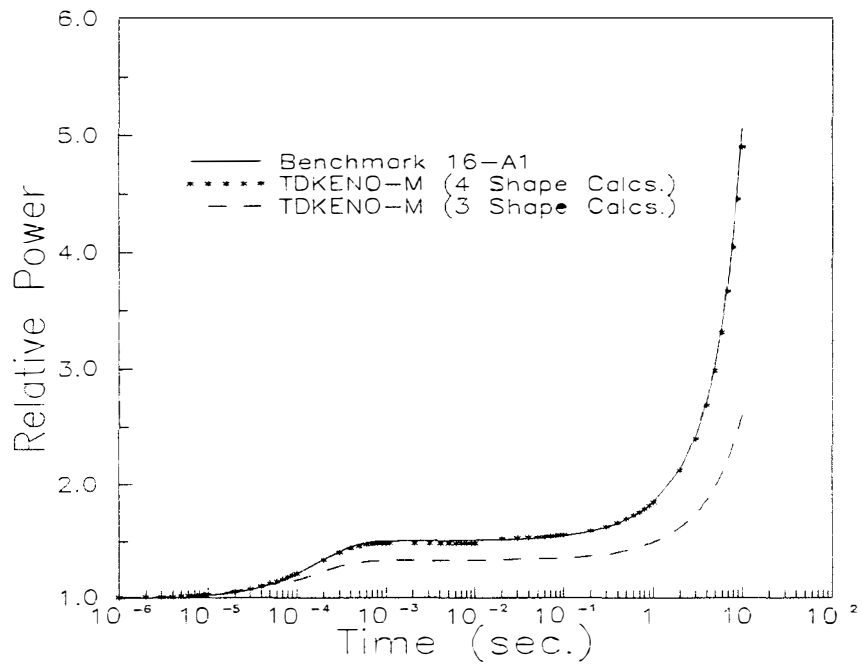


Figure 16: Power Trace for Benchmark Problem 16-A1 without Flux Shape Calculation at 10^{-2} Seconds

6.4 Sensitivity to Time Steps

This section investigates the effect of changing the number of reactivity calculations between shape calculations as well as the number of point kinetics calculations between reactivity calculations. Table 13 is a tabular representation of the number of time steps used between each calculation of flux shape and the point kinetics parameters along with the error associated with each transient calculation.

Results show that the time step spacing is of extreme importance. Particularly, the effect of increasing the number of intermediate reactivity calculations between each shape calculation is of greater importance than increasing the number of amplitude calculations between reactivity calculations. For example, if the number of intermediate amplitude calculations remains fixed at zero while the number of intermediate reactivity calculations is increased from 0 to 100, the average power deviation is reduced from 0.685% to 0.152%. In contrast, if the number of intermediate reactivity calculations remains fixed at 10 while the number of intermediate amplitude calculations is increased from 0 to 100, the average power deviation is only reduced from 0.158 to 0.129.

It should be noted that the number of intermediate calculations of either amplitude or the point kinetics parameters reaches a threshold value after which an increase in the number of intermediate calculations causes only negligible improvement in the average power deviation.

Table 13: Results of Time Step Sensitivity Studies

Number of Intermediate Reactivity Calculations	Number of Intermediate Amplitude Calculations	Average Power Deviation (%)
0	0	0.685
0	10	0.478
0	100	0.452
10	0	0.158
10	10	0.134
10	100	0.129
100	0	0.152
100	10	0.131
100	100	0.129

Chapter Seven

Conclusions and Future Work

7.1 Conclusions

An improved hybrid stochastic/deterministic method for transient, three-dimensional neutron transport has been developed. The method, as incorporated in TDKENO-M, provides a mechanism for benchmarking more approximate and less CPU intensive codes without the prohibitive computing times encountered with TDKENO. Finally, the method has been verified by comparisons with several benchmark problems to ensure that TDKENO-M accurately solves the three-dimensional, time-dependent Boltzmann transport equation with explicit representation of delayed neutrons.

TDKENO-M is verified by applying the code to Benchmark Problems 14-A2, 16-A1, 16-A2, 16-A3, 16-A6, and 16-A7 contained in the ANL-7416 Benchmark Problem Book.⁴⁵ Results show that TDKENO-M is quite accurate in comparison with benchmark calculations (less than 2% error in power trace for ANL Benchmark 16-A1) with as much as a factor of 500 reduction in CPU time relative to TDKENO.

In conclusion, the transport code as well as the methodology developed in this work is an extremely important new tool for the transient simulation of neutronic systems. Thus, the user has the ability to model the three-dimensional transient behavior of fissile systems using an exact transport treatment.

7.2 Future Work

The primary area where future work is recommended is with respect to the thermalhydraulic feedback models which are utilized for the systems being modeled. The current version of TDKENO-M considers only simple adiabatic heatup with Doppler broadening of the absorption cross sections. Thus, a better mechanism for including thermalhydraulic feedback would be to use deterministic models for conduction, convection, and radiation of heat for the system as well as any other physical phenomena that affects reactivity.

Work is also recommended in the testing and evaluation of TDKENO-M. Particularly, more testing should be performed to identify the types of problems for which TDKENO-M is best (as well as least) suited. It would also be beneficial to apply TDKENO-M to additional three-dimensional benchmark problems (e.g., problem 17-A2) as further evaluation of the neutronic capabilities of TDKENO-M.

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Appendices

Appendix A: Derivation of Improved Quasistatic Equations

The quasistatic approach is a method of treating the spatial dynamics of the time-dependent Boltzmann transport calculation by factoring the flux into an amplitude and a shape function such that the time variation of the shape function is more slowly varying than the time variation of the amplitude function. This factorization of the flux results in splitting the neutronics equation into two coupled equations; an amplitude equation having the form of the point kinetics equation and a shape equation. The improved quasistatic method replaces the time derivative of the shape function by a first order backward difference approximation thus allowing the improved quasistatic method to be applied more accurately.

The development of the improved quasistatic method begins with the time-dependent Boltzmann transport equation with explicit representation of delayed neutrons:

$$\begin{aligned} \frac{1}{v} \frac{\partial \phi(\bar{r}, \bar{\Omega}, E, t)}{\partial t} + \bar{\Omega} \cdot \bar{\nabla} \phi + \Sigma_t \phi = \int \int \Sigma_s(\bar{r}, \bar{\Omega}', E' \rightarrow \bar{\Omega}, E, t) \phi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' \\ + \int \int \chi_p(E) (1 - \beta) v \Sigma_f(\bar{r}, E', t) \phi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' + \sum_j \lambda_j C_j(\bar{r}, t) \chi_j + Q \end{aligned} \quad (\text{a.1})$$

and

$$\frac{\partial C_j(\bar{r}, t)}{\partial t} + \lambda_j C_j = \int \int \beta_j v \Sigma_f(\bar{r}, E', t) \phi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' \quad \text{for } j=1, N \quad (\text{a.2})$$

where,

v	=	particle speed,
ϕ	=	time-dependent angular flux,
\bar{r}	=	spatial variable,
E	=	energy,
$\bar{\Omega}$	=	unit vector describing particle direction,
t	=	time,
Σ_t	=	total cross section,
Σ_s	=	differential scattering cross section,
Q	=	external source,
χ_p	=	normalized energy spectrum of prompt neutrons,
χ_j	=	normalized energy spectrum for precursor group j,
β	=	delayed neutron fraction,
ν	=	total number of neutrons emitted per fission,
Σ_f	=	fission cross section,
λ_j	=	decay constant for delayed neutron precursor group j,
C_j	=	density of delayed neutron precursors for group j,
N	=	number of precursor groups.

The time-independent adjoint form of the transport equation is given by:

$$\begin{aligned}
 -\bar{\Omega} \cdot \bar{\nabla} \phi^* + \Sigma_t \phi^* &= \int \int \Sigma_s(\bar{r}; \bar{\Omega}, E \rightarrow \bar{\Omega}', E') \phi^*(\bar{r}, \bar{\Omega}', E') d\Omega' dE' \\
 &+ \int \int \chi(E') \nu \Sigma_f(\bar{r}, E) \phi^*(\bar{r}, \bar{\Omega}', E') d\Omega' dE'
 \end{aligned}
 \tag{a.3}$$

where,

$$\phi^* = \text{adjoint flux.}$$

Next, the flux is factored into an amplitude function, $P(t)$, and a shape function, Ψ , such that the flux is given by:

$$\phi(\bar{r}, \bar{\Omega}, E, t) = P(t) \Psi(\bar{r}, \bar{\Omega}, E, t)
 \tag{a.4}$$

This factorization requires an additional separation condition for $t > 0$ in order to become a unique definition.³⁵ There are many conditions that could be used, all of which involve constraining some space-energy integral of $\Psi(r,E,t)$ to a constant value for all $t > 0$. The only basic requirement is that $\Psi(r,E,t)$ remain positive and bounded at all points in space (r,E) for all time. According to Henry, the following equation fulfills the requirements for the constraint condition and has the added advantage that it facilitates the transition to the point kinetics formulation:^{45,46}

$$\iiint \frac{1}{v} \Psi(\bar{r}, \bar{\Omega}, E, t) \phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dE dV = \text{constant} \quad (\text{a.5})$$

Substituting the separability assumption given in equation a.4 into the time-dependent Boltzmann transport equation and multiplying by ϕ^* yields the following equation:

$$\begin{aligned} & \frac{1}{v} \frac{\partial P(t) \Psi(\bar{r}, \bar{\Omega}, E, t)}{\partial t} \phi^* + \bar{\Omega} \cdot \bar{\nabla} [P(t) \Psi(\bar{r}, \bar{\Omega}, E, t)] \phi^* \\ & + \Sigma_t(\bar{r}, E, t) P(t) \Psi(\bar{r}, \bar{\Omega}, E, t) \phi^* \\ = & \phi^* \iint \Sigma_s(\bar{r}; \bar{\Omega}', E' \rightarrow \bar{\Omega}, E; t) P(t) \Psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' \\ & + \phi^* \iint \chi_p(E) (1 - \beta) v \Sigma_f(\bar{r}, E', t) P(t) \Psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' \\ & + \phi^* \sum_j \lambda_j C_j(\bar{r}, t) \chi_j + \phi^* Q \end{aligned} \quad (\text{a.6})$$

Next, the time-independent adjoint form of the transport equation (equation a.3) is multiplied by ϕ and the separability assumption (equation a.4) is again used to yield the following:

$$\begin{aligned}
& -(\bar{\Omega} \cdot \bar{\nabla} \phi^*) P(t) \psi(\bar{r}, \bar{\Omega}, E, t) + \Sigma_t(\bar{r}, E) \phi^* P(t) \psi(\bar{r}, \bar{\Omega}, E, t) \\
& = P(t) \psi(\bar{r}, \bar{\Omega}, E, t) \iint \Sigma_s(\bar{r}, \bar{\Omega}, E \rightarrow \bar{\Omega}', E') \phi^* d\Omega' dE' \\
& \quad + P(t) \psi(\bar{r}, \bar{\Omega}, E, t) \iint \chi(E') \nu \Sigma_f(\bar{r}, E) \phi^* d\Omega' dE'
\end{aligned} \tag{a.7}$$

The flux-weighted adjoint equation (equation a.7) is subtracted from the adjoint-weighted forward equation (equation a.6) to give:

$$\begin{aligned}
& \frac{1}{\nu} \frac{\partial P(t) \psi(\bar{r}, \bar{\Omega}, E, t)}{\partial t} \phi^* + \bar{\Omega} \cdot \bar{\nabla} [P(t) \psi(\bar{r}, \bar{\Omega}, E, t)] \phi^* \\
& \quad + (\bar{\Omega} \cdot \bar{\nabla} \phi^*) P(t) \psi(\bar{r}, \bar{\Omega}, E, t) \\
& + \Sigma_t(\bar{r}, E, t) P(t) \psi(\bar{r}, \bar{\Omega}, E, t) \phi^* - \Sigma_t(\bar{r}, E, t) \phi^* P(t) \psi(\bar{r}, \bar{\Omega}, E, t) \\
& = \phi^* \iint \Sigma_s(\bar{r}, \bar{\Omega}', E' \rightarrow \bar{\Omega}, E, t) P(t) \psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' \\
& \quad - P(t) \psi(\bar{r}, \bar{\Omega}, E, t) \iint \Sigma_s(\bar{r}, \bar{\Omega}, E \rightarrow \bar{\Omega}', E') \phi^*(\bar{r}, \bar{\Omega}', E') d\Omega' dE' \\
& \quad + \phi^* \iint \chi_p(E) (1 - \beta) \nu \Sigma_f(\bar{r}, E', t) P(t) \psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' \\
& \quad - P(t) \psi(\bar{r}, \bar{\Omega}, E, t) \iint \chi(E') \nu \Sigma_f(\bar{r}, E) \phi^*(\bar{r}, \bar{\Omega}', E') d\Omega' dE' \\
& \quad + \phi^* \sum_j \lambda_j C_j(\bar{r}, t) \chi_j + \phi^* Q
\end{aligned} \tag{a.8}$$

Integration of this equation over space, energy and angle gives:

$$\begin{aligned}
& \iiint \frac{1}{v} \frac{\partial P(t) \psi(\bar{r}, \bar{\Omega}, E, t)}{\partial t} \phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dE dV \\
& + \iiint \bar{\Omega} \cdot \bar{\nabla} P(t) \psi(\bar{r}, \bar{\Omega}, E, t) \phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dE dV \\
& + \iiint \bar{\Omega} \cdot \bar{\nabla} \phi^*(\bar{r}, \bar{\Omega}, E) P(t) \psi(\bar{r}, \bar{\Omega}, E, t) d\Omega dE dV \\
& + \iiint (\Sigma_s(\bar{r}, E, t) - \Sigma_a(\bar{r}, E)) P(t) \psi(\bar{r}, \bar{\Omega}, E, t) \phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dE dV \\
= & \iiint \phi^*(\bar{r}, \bar{\Omega}, E) \iiint \Sigma_s(\bar{r}, \bar{\Omega}', E' \rightarrow \bar{\Omega}, E, t) P(t) \psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' d\Omega dE dV \quad (\text{a.9}) \\
& - \iiint P(t) \psi(\bar{r}, \bar{\Omega}, E, t) \iiint \Sigma_s(\bar{r}, \bar{\Omega}, E \rightarrow \bar{\Omega}', E') \phi^*(\bar{r}, \bar{\Omega}', E') d\Omega' dE' d\Omega dE dV \\
& + \iiint \phi^*(\bar{r}, \bar{\Omega}, E) \iiint \chi_p(E) (1 - \beta) v \Sigma_f(\bar{r}, E', t) P(t) \psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' d\Omega dE dV \\
& - \iiint P(t) \psi(\bar{r}, \bar{\Omega}, E, t) \iiint \chi(E') v \Sigma_f(\bar{r}, E) \phi^*(\bar{r}, \bar{\Omega}', E') d\Omega' dE' d\Omega dE dV \\
& + \iiint \phi^*(\bar{r}, \bar{\Omega}, E) \sum_j \lambda_j C_j(\bar{r}, t) \chi_j d\Omega dE dV + \iiint \phi^*(\bar{r}, \bar{\Omega}, E) Q d\Omega dE dV
\end{aligned}$$

The first term in equation a.9 can be rewritten as follows:

$$\begin{aligned}
& \iiint \frac{1}{v} \frac{\partial P(t) \psi(\bar{r}, \bar{\Omega}, E, t)}{\partial t} \phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dE dV \\
= & P(t) \frac{\partial}{\partial t} \iiint \frac{1}{v} \psi(\bar{r}, \bar{\Omega}, E, t) \phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dE dV \quad (\text{a.10}) \\
& + \iiint \frac{1}{v} \psi(\bar{r}, \bar{\Omega}, E, t) \frac{\partial P(t)}{\partial t} \phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dE dV
\end{aligned}$$

Using the space-energy integral constraint given in equation a.5 it is obvious that the first term on the right hand side of equation a.10 vanishes. Thus, the first term in equation a.9 can be written as:

$$\begin{aligned} & \iiint_{\mathbf{v}} \frac{1}{v} \frac{\partial P(t) \psi(\bar{r}, \bar{\Omega}, E, t)}{\partial t} \phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dE dV \\ & = \frac{\partial P(t)}{\partial t} \iiint_{\mathbf{v}} \frac{1}{v} \psi(\bar{r}, \bar{\Omega}, E, t) \phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dE dV \end{aligned} \quad (\text{a.11})$$

Since the gradient in the second and third terms of equation a.9 is invariant with respect to the angular variable, those two terms can be respectively simplified as follows:

$$\begin{aligned} & \iiint \bar{\Omega} \cdot \bar{\nabla} (P(t) \psi(\bar{r}, \bar{\Omega}, E, t)) \phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dE dV \\ & = \iiint \bar{\nabla} \cdot \bar{\Omega} (P(t) \psi(\bar{r}, \bar{\Omega}, E, t)) \phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dE dV \end{aligned} \quad (\text{a.12})$$

and

$$\begin{aligned} & \iiint \bar{\Omega} \cdot \bar{\nabla} \phi^*(\bar{r}, \bar{\Omega}, E) P(t) \psi(\bar{r}, \bar{\Omega}, E, t) d\Omega dE dV \\ & = \iiint \bar{\nabla} \cdot \bar{\Omega} \phi^*(\bar{r}, \bar{\Omega}, E) P(t) \psi(\bar{r}, \bar{\Omega}, E, t) d\Omega dE dV \end{aligned} \quad (\text{a.13})$$

Next, the divergence theorem is used to change these volume integrals (equations a.12 and a.13) into surface integrals as follows:⁴⁸

$$\begin{aligned}
 & \iiint_V \bar{\nabla} \cdot \bar{\Omega} (P(t) \Psi(\bar{r}, \bar{\Omega}, E, t)) \phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dE dV \\
 &= \iint_S \bar{n} \cdot \bar{\Omega} (P(t) \Psi(\bar{r}, \bar{\Omega}, E, t)) \phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dE dV
 \end{aligned} \tag{a.14}$$

and

$$\begin{aligned}
 & \iiint_V \bar{\nabla} \cdot \bar{\Omega} \phi^*(\bar{r}, \bar{\Omega}, E) P(t) \Psi(\bar{r}, \bar{\Omega}, E, t) d\Omega dE dV \\
 &= \iint_S \bar{n} \cdot \bar{\Omega} \phi^*(\bar{r}, \bar{\Omega}, E) P(t) \Psi(\bar{r}, \bar{\Omega}, E, t) d\Omega dE dV
 \end{aligned} \tag{a.15}$$

If the boundary conditions for Ψ and ϕ^* are assumed such that $\Psi \phi^*$ is zero on the surface, which is the usual assumption, then the second and third terms of equation a.9 vanish.

The first two terms on the right hand side of equation a.9 can be rearranged by interchanging the dummy variables of integration and combined to be rewritten as:⁴⁸

$$\begin{aligned}
& \int \int \int \phi^*(\bar{r}, \bar{\Omega}, E) \int \int \Sigma_s(\bar{r}, \bar{\Omega}', E' \rightarrow \bar{\Omega}, E, t) P(t) \psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' d\Omega dEdV \\
& - \int \int \int P(t) \psi(\bar{r}, \bar{\Omega}, E, t) \int \int \Sigma_s(\bar{r}, \bar{\Omega}, E \rightarrow \bar{\Omega}', E', t) \phi^*(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' d\Omega dEdV \\
& = P(t) \int \int \int \int \phi^*(\bar{r}, \bar{\Omega}, E) \left(\Sigma_s(\bar{r}, \bar{\Omega}', E' \rightarrow \bar{\Omega}, E, t) - \Sigma_s(\bar{r}, \bar{\Omega}, E \rightarrow \bar{\Omega}', E', t) \right) \\
& \quad \times \psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' d\Omega dEdV
\end{aligned} \tag{a.16}$$

If the assumption is now made that the energy spectrum of prompt neutrons is identical to the energy spectrum of total neutrons (i.e., $\chi = \chi_p$), the two fission terms on the right hand side of equation a.9 (minus the β term) can be combined and rewritten as:

$$\begin{aligned}
& \int \int \int \phi^*(\bar{r}, \bar{\Omega}, E) \int \int \chi_p(E) \nu \Sigma_f(\bar{r}, E', t) P(t) \psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' d\Omega dEdV \\
& - \int \int \int P(t) \psi(\bar{r}, \bar{\Omega}, E, t) \int \int \chi(E') \nu \Sigma_f(\bar{r}, E) \phi^*(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' d\Omega dEdV \\
& = P(t) \int \int \int \int \phi^*(\bar{r}, \bar{\Omega}, E) \chi_p(E) \left(\nu \Sigma_f(\bar{r}, E', t) - \nu \Sigma_f(\bar{r}, E) \right) \\
& \quad \times \psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' d\Omega dEdV
\end{aligned} \tag{a.17}$$

The fission term containing β on the right hand side of equation a.9 can also be written as:

$$\begin{aligned}
& - \iiint \phi^*(\bar{r}, \bar{\Omega}, E) \iiint \chi_p(E) \beta \nu \Sigma_f(\bar{r}, E', t) P(t) \psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' d\Omega dEdV \\
& = -P(t) \iiint \iiint \phi^*(\bar{r}, \bar{\Omega}, E) \chi_p(E) \left(\sum_j \beta_j \right) \nu \Sigma_f(\bar{r}, E', t) \\
& \quad \times \psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' d\Omega dEdV
\end{aligned} \tag{a.18}$$

Substituting equations a.11, a.14, a.15, a.16, a.17, and a.18 into equation a.9 yields the following equation:

$$\begin{aligned}
& \frac{\partial P(t)}{\partial t} \iiint \frac{1}{\nu} \psi(\bar{r}, \bar{\Omega}, E, t) \phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dEdV \\
& = - \iiint (\Sigma_t(\bar{r}, E, t) - \Sigma_t(\bar{r}, E)) P(t) \psi(\bar{r}, \bar{\Omega}, E, t) \phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dEdV \\
& + P(t) \iiint \iiint \phi^*(\bar{r}, \bar{\Omega}, E) (\Sigma_s(\bar{r}, \bar{\Omega}', E' - \bar{\Omega}, E; t) - \Sigma_s(\bar{r}, \bar{\Omega}', E' - \bar{\Omega}, E)) \\
& \quad \times \psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' d\Omega dEdV \\
& + P(t) \iiint \iiint \phi^*(\bar{r}, \bar{\Omega}, E) \chi_p(E) (\nu \Sigma_f(\bar{r}, E', t) - \nu \Sigma_f(\bar{r}, E')) \\
& \quad \times \psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' d\Omega dEdV \\
& - P(t) \iiint \iiint \phi^*(\bar{r}, \bar{\Omega}, E) \chi_p(E) \left(\sum_j \beta_j \right) \nu \Sigma_f(\bar{r}, E', t) \\
& \quad \times \psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' d\Omega dEdV \\
& + \iiint \phi^*(\bar{r}, \bar{\Omega}, E) \sum_j \lambda_j C_j(\bar{r}, t) \chi_j d\Omega dEdV + \iiint \phi^*(\bar{r}, \bar{\Omega}, E) Q d\Omega dEdV
\end{aligned} \tag{a.19}$$

Equation a.19 can be greatly simplified by introducing the following notation:

$$A = \iiint \frac{1}{v} \Psi(\bar{r}, \bar{\Omega}, E, t) \Phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dE dV \quad (\text{a.20})$$

$$\begin{aligned} B = & - \iiint (\Sigma_t(\bar{r}, E, t) - \Sigma_f(\bar{r}, E)) \Psi(\bar{r}, \bar{\Omega}, E, t) \Phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dE dV \\ & + \iiint \iiint \Phi^*(\bar{r}, \bar{\Omega}, E) [\Sigma_s(\bar{r}, \bar{\Omega}', E' - \bar{\Omega}, E, t) - \Sigma_s(\bar{r}, \bar{\Omega}', E' - \bar{\Omega}, E)] \\ & + \chi_p(E) (v \Sigma_f(\bar{r}, E', t) - v \Sigma_f(\bar{r}, E')) \Psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' d\Omega dE dV \end{aligned} \quad (\text{a.21})$$

$$\begin{aligned} C = & \iiint \iiint \Phi^*(\bar{r}, \bar{\Omega}, E) \chi_p(E) \left(\sum_j \beta_j \right) v \Sigma_f(\bar{r}, E', t) \\ & \times \Psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' d\Omega dE dV \end{aligned} \quad (\text{a.22})$$

Using equations a.20, a.21, and a.22, equation a.19 can be written as:

$$\begin{aligned} \frac{\partial P(t)}{\partial t} = & \frac{B - C}{A} P(t) + \frac{1}{A} \iiint \Phi^*(\bar{r}, \bar{\Omega}, E) \left(\sum_j \lambda_j C_j(\bar{r}, t) \chi_j \right) d\Omega dE dV \\ & + \frac{1}{A} \iiint \Phi^*(\bar{r}, \bar{\Omega}, E) Q d\Omega dE dV \end{aligned} \quad (\text{a.23})$$

Next, an arbitrary normalization factor, $F(t)$, is introduced so that the various parameters in the point kinetics equation have physical interpretations. Note that this normalization factor has no effect on the solution of equation a.23 since it always cancels in the numerator and the denominator of each term. Bell & Glasstone suggest that the most appropriate normalization factor is:⁴

$$F(t) = \iiint \int \chi(E) \nu \Sigma_f(\bar{r}, E') \Psi(\bar{r}, \bar{\Omega}', E', t) \phi_0^*(\bar{r}, \bar{\Omega}, E) d\Omega' dE' d\Omega dE dV \quad (\text{a.24})$$

where,

$$\phi_0^* = \text{steady-state adjoint flux.}$$

Using this normalization factor, equation a.23 can be rewritten as:

$$\frac{dP(t)}{dt} = \frac{\rho(t) - \bar{\beta}(t)}{\Lambda(t)} P(t) + \sum_j \lambda_j C_j(t) + \bar{Q}(t) \quad (\text{a.25})$$

with the following parameter definitions:

$$\begin{aligned} \rho(t) = & - \frac{1}{F(t)} \iiint \int (\Sigma_t(\bar{r}, E, t) - \Sigma_t(\bar{r}, E)) \Psi(\bar{r}, \bar{\Omega}, E, t) \phi_0^*(\bar{r}, \bar{\Omega}, E) d\Omega dE dV \\ & + \frac{1}{F(t)} \iiint \int \int \phi_0^*(\bar{r}, \bar{\Omega}, E) [(\Sigma_s(\bar{r}, \bar{\Omega}', E' \rightarrow \bar{\Omega}, E; t) - \Sigma_s(\bar{r}, \bar{\Omega}', E' \rightarrow \bar{\Omega}, E)) \\ & + \chi_p(\nu \Sigma_f(\bar{r}, E', t) - \nu \Sigma_f(\bar{r}, E'))] \Psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' d\Omega dE dV \end{aligned} \quad (\text{a.26})$$

$$\bar{\beta}(t) = \sum_j \bar{\beta}_j(t) \quad (\text{a.27})$$

$$\begin{aligned} \bar{\beta}_j(t) = & \frac{1}{F(t)} \iiint \iiint \chi(E) \beta_{j\nu} \Sigma_f(\bar{r}, E') \Psi(\bar{r}, \bar{\Omega}', E', t) \\ & \times \phi_0^*(\bar{r}, \bar{\Omega}, E) d\Omega' dE' d\Omega dEdV \end{aligned} \quad (\text{a.28})$$

$$\Lambda(t) = \frac{1}{F(t)} \iiint \frac{1}{v} \Psi(\bar{r}, \bar{\Omega}, E, t) \phi^*(\bar{r}, \bar{\Omega}, E) d\Omega dEdV \quad (\text{a.29})$$

$$C_j(t) = \frac{(1/F(t))}{\Lambda} \iiint \phi^*(\bar{r}, \bar{\Omega}, E) C_j(\bar{r}, t) \chi_j(E) d\Omega dEdV \quad (\text{a.30})$$

$$\bar{Q}(t) = \frac{(1/F(t))}{\Lambda} \iiint \phi^*(\bar{r}, \bar{\Omega}, E) Q(\bar{r}, \bar{\Omega}, E) d\Omega dEdV \quad (\text{a.31})$$

The delayed neutron precursor equations are obtained by multiplying equation a.2 by $\chi_j(E)\phi^*$ and using the separability condition given in equation a.4 to yield the following equation for each precursor group:

$$\begin{aligned} & \frac{\partial(\chi_j(E)\phi^*(\bar{r}, \bar{\Omega}, E)C_j(\bar{r}, t))}{\partial t} + \lambda_j \chi_j(E)\phi^*(\bar{r}, \bar{\Omega}, E)C_j(\bar{r}, t) \\ & = \iiint \chi_j(E) \beta_{j\nu} \Sigma_f(\bar{r}, E', t) P(t) \Psi(\bar{r}, \bar{\Omega}, E, t) \phi^*(\bar{r}, \bar{\Omega}, E) d\Omega' dE' \end{aligned} \quad (\text{a.32})$$

Integrating equation a.32 over space, energy and angle yields the following equation:

$$\begin{aligned}
& \iiint \frac{\partial(\chi_j(E)\phi^*(\bar{r},\bar{\Omega},E)C_j(\bar{r},t))}{\partial t} d\Omega dE dV \\
& + \iiint \lambda_j \chi_j(E)\phi^*(\bar{r},\bar{\Omega},E)C_j(\bar{r},t) d\Omega dE dV \\
& = \iiint \iiint \chi_j(E)\beta_{j,v}\Sigma_f(\bar{r},E',t)P(t)\psi(\bar{r},\bar{\Omega},E,t) \\
& \quad \times \phi^*(\bar{r},\bar{\Omega},E)d\Omega' dE' d\Omega dE dV
\end{aligned} \tag{a.33}$$

Rearranging equation a.30 and substituting into equation a.33 gives:

$$\begin{aligned}
\frac{\partial C_j(t)}{\partial t} + \lambda_j C_j(t) &= \frac{P(t)}{\Lambda} \cdot \frac{1}{F(t)} \iiint \iiint \beta_{j,v}\Sigma_f(\bar{r},E',t) \\
& \times \psi(\bar{r},\bar{\Omega}',E',t)\phi^*(\bar{r},\bar{\Omega},E)d\Omega' dE' d\Omega dE dV
\end{aligned} \tag{a.34}$$

Using the parameter definition of $\bar{\beta}_j(t)$ (equation a.28), equation a.34 can be written as:

$$\frac{\partial C_j(t)}{\partial t} + \lambda_j C_j(t) = \frac{\bar{\beta}_j(t)}{\Lambda} P(t) \tag{a.35}$$

The shape equation is obtained by substituting the separability condition (equation a.4) into the time-dependent Boltzmann transport equation and dividing by $P(t)$ to yield the following:

$$\begin{aligned}
& \frac{1}{v} \cdot \frac{1}{P(t)} \cdot \frac{\partial P(t)}{\partial t} \cdot \psi(\bar{r}, \bar{\Omega}, E, t) + \frac{1}{v} \frac{\partial \psi(\bar{r}, \bar{\Omega}, E, t)}{\partial t} + \bar{\Omega} \cdot \bar{\nabla} \psi(\bar{r}, \bar{\Omega}, E, t) \\
& + \Sigma_t(\bar{r}, E, t) \psi(\bar{r}, \bar{\Omega}, E, t) = \iint \Sigma_s(\bar{r}, \bar{\Omega}', E' \rightarrow \bar{\Omega}, E; t) \psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' \\
& + \iint \chi_p(E) (1 - \beta) v \Sigma_f(\bar{r}, E', t) \psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' \\
& + \frac{Q_d(\bar{r}, E, t)}{P(t)} + \frac{Q}{P(t)}
\end{aligned} \tag{a.36}$$

where,

$$\begin{aligned}
Q_d(\bar{r}, E, t) &= \int_{-\infty}^t \int_{E'} \int_{\bar{\Omega}'} v \Sigma_f(\bar{r}, E', t) P(t') \psi(\bar{r}, \bar{\Omega}', E', t) \\
&\times \sum_j \beta_j \chi_j \lambda_j e^{-\lambda_j(t-t')} d\Omega' dE' dt'
\end{aligned} \tag{a.37}$$

The improved quasistatic method, as applied to TDKENO-M, solves the full shape equation (equation a.36) by replacing the time derivative of the shape function with a backward difference approximation of first order:

$$\frac{\partial}{\partial t} \psi(\bar{r}, \bar{\Omega}, E, t) = \frac{\psi(\bar{r}, \bar{\Omega}, E, t) - \psi(\bar{r}, \bar{\Omega}, E, t - \Delta t)}{\Delta t} \quad (\text{a.38})$$

where,

$$\begin{aligned} t - \Delta t &= \text{time of the last shape calculation,} \\ \Delta t &= \text{time interval for shape calculations.} \end{aligned}$$

Since the rate of change of the shape function is determined essentially by a slow variation of system parameters, this approximation is valid over a much larger time range than is acceptable for the total flux. Using the backward difference approximation for the time derivative of the shape function yields the following shape equation:

$$\begin{aligned} & \frac{1}{v} \frac{1}{P(t)} \frac{\partial P(t)}{\partial t} \psi(\bar{r}, \bar{\Omega}, E, t) + \frac{1}{v} \left(\frac{\psi(\bar{r}, \bar{\Omega}, E, t) - \psi(\bar{r}, \bar{\Omega}, E, t - \Delta t)}{\Delta t} \right) \\ & + \bar{\Omega} \cdot \bar{\nabla} \psi(\bar{r}, \bar{\Omega}, E, t) + \Sigma_t(\bar{r}, E, t) \psi(\bar{r}, \bar{\Omega}, E, t) \\ & = \iint \Sigma_s(\bar{r}, \bar{\Omega}', E' \rightarrow \bar{\Omega}, E, t) \psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' \\ & + \iint \chi_p(E) (1 - \beta) v \Sigma_f(\bar{r}, E', t) \psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' \\ & + \frac{Q_d(\bar{r}, E, t)}{P(t)} + \frac{Q}{P(t)} \end{aligned} \quad (\text{a.39})$$

Equation a.39 can be rearranged to be written as:

$$\begin{aligned}
& \frac{1}{v} \left(\frac{1}{P(t)} \cdot \frac{\partial P(t)}{\partial t} + \frac{1}{\Delta t} \right) \psi(\bar{r}, \bar{\Omega}, E, t) \\
& + \bar{\Omega} \cdot \bar{\nabla} \psi(\bar{r}, \bar{\Omega}, E, t) + \Sigma_s(\bar{r}, E, t) \psi(\bar{r}, \bar{\Omega}, E, t) \\
& - \int \int \Sigma_s(\bar{r}, \bar{\Omega}', E' \rightarrow \bar{\Omega}, E; t) \psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' \\
& - \int \int \chi_p(E) (1 - \beta) v \Sigma_f(\bar{r}, E', t) \psi(\bar{r}, \bar{\Omega}', E', t) d\Omega' dE' \\
& = \frac{Q_d(\bar{r}, E, t)}{P(t)} + \frac{Q}{P(t)} + \frac{\psi(\bar{r}, \bar{\Omega}, E, t - \Delta t)}{v \Delta t}
\end{aligned} \tag{a.40}$$

This shape equation is of inhomogeneous partial differential form. As with the quasistatic method, Q_d is computed from equation a.37 and the $[\partial P(t)/\partial t]/P(t)$ term is determined from the solution of the point kinetics equation (equation a.25). With the improved quasistatic method, there is now an additional source term from the backward difference approximation of the shape derivative as well as an additional $1/\Delta t$ term which is incorporated as shown in equation a.40.

Appendix B: TDKENO-M

TDKENO-M Code Listing

```

program tdkenom
*****
*
*   TTTTTTTTTT   DDDD   K   K   EEEEE   N   N   OOO   M   M
*   T           D   D   K   K   E       NN   N   O   O   MM   MM
*   T           D   D   K   K   E       NN   N   O   O   M M   M M
*   T           D   D   KK      EEEEE   N   N   N   O   O   M   MM   M
*   T           D   D   K   K   E       N   NN   O   O   M   M
*   T           D   D   K   K   E       N   NN   O   O   M   M
*   T           DDDD   K   K   EEEEE   N   N   OOO   M   M
*
*****
*
*                               VARIABLES
*
*****
*
*   a(1)-a(nadjp1) = phi angle bins
*   a(nadjp1)-a(i) = theta andle bins
*   abeta(i)       = fraction of delayed neutrons for group i
*   abeta2(i)      = total abeta(i)
*   abeta3(i)      = variance of abeta(i)
*   adj            = flag for doing adjoint calculation
*   adjfis        = adjoint flux
*   adjin         = adjoint in incoming direction
*   alambda(i)    = fraction of delayed neutrons for group i
*   albb          = albedo
*   amp(i)        = flux amplitude
*   ampti(i)      = time of flux amplitude calculation
*   amx           = flag for printing all mixture X-sections
*   atol         = tolerance used by LSODE
*   beta(i)       = delayed neutron fraction for group i
*   betat        = total delayed neutron fraction
*   betatot      = total delayed neutron fraction
*   binu(i)       = boundaries of phi bins
*   binv(i)       = boundaries of theta bins
*   c(i)          = precursor concentration for group i
*   c0(i)         = initial concentration for group i
*   ccons         = constraint integral
*   ccons2        = total constraint integral
*   ccons3        = variance of constraint integral
*   chi(i,j)      = fission spectrum
*   conp2b        = conversion factor to btu/sec
*   const         = constraint constant
*   delmin        = minimum time step
*   delt          = time step
*   deltat        = time step
*   dpdt          = (1/pow)*(dp/dt)
*   eb            = conversion factor from energy to velocity
*   etamin        = cosine of scattering angle in COM
*   exprn()       = exponential random number
*   fap           = absorption probability
*   fk(i)         = pdf for delayed neutron source
*   fkig(i)       = pdf for delayed neutron source
*   flux(i)       = adjoint flux for bin i
*   flux(i,j)     = flux shape
*   flux(i,j,1)   = flux shape
*   flux(i,j,2)   = percent deviation flux shape
*   flux(i,j,3)   = variance of flux shape
*   fluxti        = time of flux shape calculation

```

```

*      flx          = flag for collecting and printing fluxes      *
*      fnap        = scatter probability                          *
*      fnfp        = fission probability                        *
*      fs          = flux shift/(delayed + flux shift)          *
*      fsp        = p0 angles                                  *
*      gen         = generation time (also # of generations)    *
*      gfis       = fission weighted energy group              *
*      iadjfl     = file identifier for adjoint file            *
*      icexs0     = file identifier for ft434001                *
*      icon,iconf = flag for determining perturbation of X's    *
*      id         = id number for mixture                       *
*      idelay     = file identifier for delay.dat               *
*      ifixsc     = pointer for fixed source data              *
*      iflux      = file identifier for flux.dat                *
*      iflux0     = file identifier for flux.out                *
*      ig         = energy group number (also flags EOF)        *
*      igg        = flag for gammas                            *
*      igen     = file identifier for general.dat              *
*      igen     = generation number (also)                     *
*      igfis     = energy group of fission                      *
*      ikin      = file identifier for kinetics.dat             *
*      iline     = dummy variable to count line numbers         *
*      inn       = file identifier for power.in                 *
*      iopt      = parameter used by LSODE                      *
*      iout      = file identifier for output files              *
*      iphi     = phi bin number                                *
*      isec     = section number of general.dat file            *
*      isigf    = file identifier for nusigf.dat                *
*      isort    = flag used to sort values                      *
*      istrate = parameter used by LSODE                        *
*      istop    = flag used for last iteration                  *
*      itask    = parameter used by LSODE                       *
*      itheta   = theta bin number                              *
*      itime    = file identifier for timen.dat                  *
*      itime0   = file identifier for time0.dat                 *
*      itimen   = file identifier for timen.dat                  *
*      itol     = tolerance used for LSODE                      *
*      ixsst    = pointer for steady state X-sections           *
*      kmax     = number of geometry regions                    *
*      kmax0    = number of geometry regions                    *
*      knew     = region number of fixed source neutron        *
*      lamp     = pointer for flux amplitude                    *
*      lampt    = pointer for flux amplitude times              *
*      lchi     = pointer for flux spectrum                     *
*      lcon     = pointer for constraint constant                *
*      lend     = pointer for end of array                       *
*      lf       = pointer for flux shift                        *
*      lfk      = pointer for flux shift spatial pdf            *
*      lfkig    = pointer for flux shift pdf                     *
*      lflux    = pointer for flux shapes                       *
*      lfulxt   = pointer for flux times                        *
*      lib      = logical unit number for AMPX library          *
*      lim      = maximum number of delayed groups              *
*      limmem   = maximum number of array values                *
*      liw      = parameter used by LSODE                       *
*      ll       = lower limit                                    *
*      lmt      = maximum number of mixtures                    *
*      lncor    = pointer for mixture i.d. numbers              *
*      lnexttr  = number of entries of extra data from EXTRA   *
*      lntegr   = pointer for integrand values of qd            *
*      lpow     = pointer for flux amplitudes                   *
*      lpowt    = pointer for flux amplitude times              *
*      lrw      = parameter used by LSODE                       *
*      lqd      = pointer for delayed neutron source            *
*      lqdk     = pointer for pdf of delayed neutron source     *
*      lqdkig   = pointer for pdf of delayed neutron source     *
*      lsigf    = pointer for nusigf                            *
*      lsigft   = pointer for nusigf times                      *
*      ltime    = pointer for time                              *
*      lu       = upper limit                                    *
*      lvel     = pointer for energy boundaries                  *
*      lvol     = pointer for volumes                            *
*      m        = mixture id number (also flags crossings)     *

```



```

*      matt      = number of mixtures in geometry      *
*      mf        = parameter used by LSODE             *
*      mix       = mixture id number                  *
*      mixnum    = number of mixtures                  *
*      mwa       = magic word array (2-D scatter transfer) *
*      n1d       = number of 1-D X-sections on ICE tape *
*      n1m       = length of p0 array for primaries    *
*      nadj      = flag for adjoint calculations (true) *
*      nadjph    = number of phi angle bins            *
*      nadjth    = number of theta angle bins          *
*      namp      = maximum number of times on timen.dat file *
*      ncork(i)  = mixture id number for region i      *
*      ndg       = number of delayed neutron groups    *
*      ndglim    = maximum number of delayed neutron groups *
*      ndxadj    = pointer for adjoint flux            *
*      neq       = number of equations solved by LSODE *
*      neut      = neutron number                     *
*      newbar    = flag for calculation average nu     *
*      ngp       = number of energy groups             *
*      ngp1      = ngp + 1                             *
*      ngp0      = number of energy groups             *
*      nmat      = number of cross-section mixtures    *
*      nnamp     = number of time steps on timen.dat file *
*      nntmef    = number of time steps on flux.dat    *
*      nntmes    = number of time steps on nusigf.dat  *
*      nnpow     = number of time steps on timen.dat  *
*      np1       = order of expansion of p-set         *
*      npg       = neutrons per generation            *
*      npow      = maximum number of times on timen.dat file *
*      nrec      = number of records/section on general.dat *
*      nsk       = number of generations omitted       *
*      nskip     = number of generations skipped       *
*      ntegr     = maximum number of integrand values  *
*      ntime     = number of time intervals           *
*      ntimef    = maximum number of flux shape calculations *
*      ntimes    = maximum number of times on nusigf.dat file *
*      nx        = number of secondary 1-D X-sections  *
*      pi        = 3.14159265                          *
*      plt       = flag for drawing pictures of problem geo *
*      pow(i)    = flux amplitude                      *
*      powini    = initial power                       *
*      powti(i)  = time of flux amplitude calculation  *
*      pth       = particle pathlength                 *
*      qd(i,j)   = delayed neutron source              *
*      qdk(i)    = pdf for delayed neutron source     *
*      qdkig(i,j) = pdf for delayed neutron source    *
*      r1        = prompt/(prompt + delayed)          *
*      r2        = flux shift/(prompt + delayed)      *
*      r3        = prompt/delayed                     *
*      react     = contribution to reactivity          *
*      react2    = total reactivity                    *
*      react3    = variance of reactivity             *
*      rho       = reactivity                          *
*      rhotot    = reactivity                          *
*      rnd       = hexadecimal random number           *
*      rtol      = tolerance used by LSODE             *
*      sct       = number of discrete scattering angles *
*      sigcon    = contribution to reactivity due to perturb *
*      sigf(i,j,k) = nusigf                            *
*      sigf0     = unperturbed fission X-section      *
*      sigs      = scattering X-section                *
*      sigt      = total X-section                    *
*      sigt0     = unperturbed total X-section        *
*      sold      = beginning point of TRACK           *
*      ssfiss    = nusigf*flux at t=0                 *
*      sum,sumf  = dummy variable used for summation  *
*      t         = time                                 *
*      tba       = time for each generation (min)     *
*      tcool1    = coolant temperature                 *
*      tcool2    = coolant temperature                 *
*      tfisn     = average fission X-section          *
*      tfuel     = fuel temperature                   *
*      time      = time                                 *

```

```

*      time2      = current time
*      tme       = execution time (min)
*      tout      = time at end of an iteration
*      trial     = convergence parameter
*      tstop     = time of end of interval
*      twopi     = 2*pi
*      u,v,w     = direction cosines
*      vel(i)    = velocity (energy) boundary for group i
*      vinv      = inverse velocity
*      vol(i)    = volume of region i
*      wt        = particle weight
*      wtavg     = average particle weight
*      wtxlen    = wt*xlen
*      x1        = x-coordinate
*      x1d       = extra 1-D X-sections
*      xap       = flag for printing discrete scatter angles
*      xc        = interpolated precursor concentration
*      xcc(i)    = precursor concentration of group i
*      xflux     = interpolated flux shape
*      xgen,xgent = generation time
*      xgen2     = total generation time
*      xgen3     = variance of generation time
*      xntegr(i) = integrand values of qd
*      xpow      = interpolated flux amplitude
*      xsc       = logical unit number for X-section library
*      xtime     = last time on timen.dat
*      y1        = y-coordinate
*      y1d(i,j)  = X-sections
*      y1d(i,1)  = total X-sections
*      y(1)      = normalized flux amplitude
*      y(2)-y(ndgp1) = normalized precursor concentrations
*      ydot(i)   = time derivative of y(i)
*      x1        = z-coordinate
*      xc        = interpolated precursor concentration
*      xflux     = interpolated flux shape
*      xlen      = component of pathlength in x-direction
*      xnormc    = normalization factor for constraint const
*      xnormp    = normalization factor for flux amplitude
*      xpow      = interpolated flux amplitude
*      xsig      = interpolated nusigf
*      xtra(1)-(i) = boundaries of phi bins
*      xtra(i)-(i+j) = boundaries of theta bins
*      xtra(ndxadj) = adjoint flux

```

```

*****
*
*
*              SUBROUTINES
*
*
*****

```

```

*      CDELAY    calculates delayed neutron source.
*      CONMWA   converts 2-D scatter array to KENO format
*      CONRHO   makes contribution to reactivity and
*              generation time at every collision site and
*              every boundary crossing.
*      DATAIN  controls most of data input.  Calls EXTRA.
*      EXTRA    inputs angle bins for adjoint case.
*      FISFLX   calculates statistics for k-eff, reactivity,
*              generation time, etc.
*      FITFLX   prints fluxes to interface file.
*      GUIDE    controls tracking.
*      INITAL   initializes and opens interface files.
*      MASTER   controlling subroutine of KENO.
*      NORM     merges and reformats flux output of KENO into
*              flux shape interface file.
*      NSTART   generates the fission source for a generation.
*      PRTFLX   outputs fluxes to interface file.
*      PTKIN    solves the point kinetics equations.
*      POWER    calculates the normalized power from the flux
*              amplitude and shape.  Also, determines the
*              normalized flux distribution.
*      REMVID   removes reaction type id's for 1-D X-sections.
*      TRACK    tracks each neutron through the geometry.

```

```

*      WWFITF      edits adjoint fluxes.      *
*      WWINF      reads adjoint fluxes from file.      *
*      WWOUTF     outputs adjoint fluxes to an interface file.      *
*      WWRETR     retrieves steady-state scatter X-sections.      *
*      WWRHO      outputs reactivity to an interface file.      *
*      WWSTAT     calculates statistics for adjoint flux.      *
*      WSTRSU     selects starting position of fixed source n's.      *
*      WWTAPE     reads steady-state cross sections.      *
*      WWXSEC     reads steady state cross sections from file.      *
*
*****
      integer iadj,imeth,iss,inumtfs,irhonum,ipknum
      common/flags/irhonum,ipknum
c
c-----Find initial time of calculation
c
      call jstime(iim)
      diii = iim
c
c-----Make symbolic links to executables
c
      call slinks
c
c-----Create interface files
c
      call interfiles(iadj,imeth,iss,inumtfs,iouttt)
c
      write(iouttt,*)('Adjoint calculation flag =      ',iadj)
      write(iouttt,*)('Forward calculation method flag =      ',imeth)
      write(iouttt,*)('Forward calculation flag =      ',iss)
      write(iouttt,*)('Number of transient calcs =      ',iss)
      write(iouttt,*)('Number of reactivities per shape =      ',irhonum)
      write(iouttt,*)('Number of point kinetics per shape =      ',ipknum)
c
c-----Perform steady-state adjoint calculation
c
c      NOTE: A steady-state adjoint calculation must be performed unless
c            an adjoint file already exists and is saved in the
c            local directory as ft42f001.
c
      if (iadj.eq.1) then
          call adjoint
      end if
c
c-----Perform steady-state forward calculation
c
c      NOTE: A steady-state forward calculation must be performed unless
c            a forward flux file already exists and is saved in the
c            local directory as flux.dat.
c
      if (iss.eq.1) then
          call ssforward
      end if
c
c-----Extrapolate reactivity and flux amplitude to first transient
c            flux shape calculation
c
      call extrap
c
c-----Perform transient calculations
c
      do i=1,inumtfs
c
c-----Perform shape calculation
c
          call transhape
c
c-----Perform reactivity and point kinetics calculations
c
          call extrap
c
      end do
c

```

```

c-----Calculate the power trace and the normalized flux distribution
c
c      call power
c
c-----Find final time of calculation and determine total time
c
c      call jstime(ii)
c      diim = ii
c      dtme = (diii-diim)/6000.0
c      write(iouttt,101)dtme
c      write(6,101)dtme
c
c      close(ioutt)
c      close(61)
c
c-----Cleanup the job
c
c      call cleanup
c
c-----End TDKENOM program
c
101 format(' You have successfully completed TDKENO-M in ',f10.5,
*         ' minutes !!')
c      stop
c      end
c
c      subroutine slinks
c      character*60 link1,link2
c
c      link1='ln -s $HOME/tdkeno/tdkeno      tdkeno      '
c      link2='ln -s $HOME/KENO/load/tdkenoadj  tdkenoadj  '
c
c      status=system(link1)
c      if (status.ne.0) stop
c      status=system(link2)
c      if (status.ne.0) stop
c      return
c      end
c
c
c      subroutine interfiles(iadj,imeth,iss,inumtfs,iouttt)
c      common/flags/irhonum,ipknum
c      dimension beta(20),alamda(20),xcc(20),vol(1000)
c      dimension chi(20),ebound(21),ncor(1000),sigfti(20)
c      dimension sigf(20,5,20),fluxti(40),in1(7),re1(7)
c      integer iadj,imeth,iss,inumtfs,irhonum,ipknum
c      character title*60
c      character*60 link1,link2,link3
c      iouttt = 61
c      ntimes = 20
c
c      open(41,file='time0.dat',status='new')
c      open(47,file='delay.dat',status='new')
c      open(49,file='kinetics.dat',status='new')
c      open(44,file='rho.out',status='new')
c      open(45,file='general.dat',status='new')
c      open(54,file='nusigf.dat',status='new')
c      open(55,file='flux.dat',status='unknown')
c      open(46,file='timen.dat',status='new')
c      open(50,file='keno.meth',status='new')
c      open(58,file='infile',status='old')
c      open(51,file='rho.dat',status='new')
c      open(52,file='cdelay.dat',status='new')
c      open(53,file='outfile',status='new')
c      open(61,file='tmeout',status='new')
c
c      link1='cp timen.dat ft46f001      '
c      link2='cp delay.dat ft47f001      '
c      link3='cp kinetics.dat ft49f001   '
c
c      rewind 41
c      rewind 47

```

```

rewind 54
rewind 44
rewind 45
rewind 46
rewind 55
rewind 58
rewind 49
rewind 50
rewind 51
rewind 52
rewind 53
rewind 61
c
read(58,*) iadj, imeth, iss, inumtfs, irhonum, ipknum
write(50,*) imeth
read(58,801) kmax,ngp
read(58,802) dpf2t, f2dpf, d2p, xdelt
if(iss.eq.1) then
  write(55,801) kmax,ngp
end if
write(47,801) kmax,ngp
write(47,802) dpf2t, f2dpf, d2p, xdelt
read(58,*) iflag1
write(44,*) iflag1
read(58,805) ndg
read(58,806) (beta(i), i=1,ndg)
read(58,806) (alamda(i), i=1,ndg)
write(49,805) ndg
write(49,806) (beta(i), i=1,ndg)
write(49,806) (alamda(i), i=1,ndg)
read(58,803) time, pow, tfuel, tcool1, tcool2
write(46,803) time, pow, tfuel, tcool1, tcool2
read(58,810) (xcc(i), i=1,ndg)
write(46,804) (xcc(i), i=1,ndg)
read(58,807) kmax0, ngp0, nmat
write(54,807) kmax0, ngp0, nmat
if(kmax0 .ne. kmax) then
  write(6,950) kmax, kmax0
  stop
end if
if(ngp0 .ne. ngp) then
  write(6,960) ngp, ngp0
  stop
end if
read(58,808) (vol(k), k=1, kmax)
read(58,808) (chi(ig), ig=1, ngp)
read(58,808) (ebound(ig), ig=1, ngp+1)
read(58,809) (ncor(k), k=1, kmax)
write(54,808) (vol(k), k=1, kmax)
write(54,808) (chi(ig), ig=1, ngp)
write(54,808) (ebound(ig), ig=1, ngp+1)
write(54,809) (ncor(k), k=1, kmax)
c
i2 = 0
30 continue
c
i = 0
40 continue
c
i = i + 1
if(i .gt. ntimes) then
  write(*,910) ntimes
  stop
end if
c
read(58,808) sigfti(i),
* ((sigf(ig,m,i), ig=1,ngp), m=1,nmat)
write(54,808) sigfti(i),
* ((sigf(ig,m,i), ig=1,ngp), m=1,nmat)
if(sigfti(i) .lt. 0.0) then
  i = i - 1
  go to 50
end if

```

```

        go to 40
50 continue
c
c-----just read nusigf, go back for sigf
c
    if(i2 .eq. 0)then
        i2 = 1
        go to 30
    end if
c
    nntmes = i
    if(nntmes .le. 0) then
        write(iout,990)
        stop
    end if
c
    read(58,902)isec,nrec
    write(45,902)isec,nrec
    do 120 ic=1,nrec
        read(58,900)title
        write(45,900)title
120 continue
c
c-----skip section #2 of general interface file
c
    read(58,902)isec,nrec
    write(45,902)isec,nrec
    read(58,805)(in1(i),i=1,5)
    write(45,805)(in1(i),i=1,5)
    read(58,805)(in1(i),i=1,6)
    write(45,805)(in1(i),i=1,6)
    read(58,*)in4,in5,re4,re5
    write(45,815)in4,in5,re4,re5
    read(58,805)(in1(i),i=1,7)
    write(45,805)(in1(i),i=1,7)
    read(58,805)in2
    write(45,805)in2
    read(58,805)in2
    write(45,805)in2
    read(58,806)(re1(i),i=1,7)
    write(45,806)(re1(i),i=1,7)
    read(58,806)re2
    write(45,806)re2
    read(58,806)(re1(i),i=1,2)
    write(45,806)(re1(i),i=1,2)
    read(58,806)(re1(i),i=1,2)
    write(45,806)(re1(i),i=1,2)
    read(58,806)(re1(i),i=1,4)
    write(45,806)(re1(i),i=1,4)
    read(58,806)(re1(i),i=1,4)
    write(45,806)(re1(i),i=1,4)
    read(58,806)(re1(i),i=1,4)
    write(45,806)(re1(i),i=1,4)
    read(58,806)(re1(i),i=1,4)
    write(45,806)(re1(i),i=1,4)
c
c-----skip section 3 of interface file
c
    read(58,902)isec,nrec
    write(45,902)isec,nrec
    read(58,805)(in1(i),i=1,3)
    write(45,805)(in1(i),i=1,3)
    read(58,805)(in1(i),i=1,7)
    write(45,805)(in1(i),i=1,7)
    read(58,806)(re1(i),i=1,3)
    write(45,806)(re1(i),i=1,3)
    do i=1,3
        read(58,*) in4,in5,re4
        write(45,816) in4,in5,re4
    end do
c
c-----read time data section #4
c

```

```

        read(58,902)isec,nrec
        write(45,902)isec,nrec
        itimes = nrec
        n=0
101 continue
        read(58,903)fluxti(n+1)
        write(45,903)fluxti(n+1)
        n=n+1
        nlft=nrec-n
        if(nlft.gt.0)go to 101
c
c-----read time data section #5
c
100 continue
        read(58,902)isec,nrec
        write(45,902)isec,nrec
        read(58,902)ntime
        write(45,902)ntime
        do 200 ic=1,ntime
            read(58,903)tstop,delt
            write(45,903)tstop,delt
200 continue
c
        close(41)
        close(47)
        close(54)
        close(44)
        close(45)
        close(46)
        close(55)
        close(58)
        close(49)
        close(50)
        close(51)
        close(52)
c
        status=system(link1)
        if (status.ne.0) stop
        status=system(link2)
        if (status.ne.0) stop
        status=system(link3)
        if (status.ne.0) stop
c
c
801 format(10i5)
802 format(6e11.4)
803 format(7e11.4)
810 format(6e11.4)
804 format(11x,6e11.4)
805 format(10i5)
806 format(7e11.4)
807 format(3i5)
808 format(6e11.4)
809 format(12i5)
815 format(2i5,2e11.4)
816 format(2i5,1e11.4)
900 format(a60)
902 format(15i5)
903 format(7e11.4)
904 format(1x,21hend of problem time=,f7.2)
910 format(1x,'more times on nusigf.dat than allowed',i11)
950 format(1x,'kmax not consistent in interface files in norm',2i5)
960 format(1x,'ngp not consistent in interface files in norm',2i5)
990 format(1x,'no data on nusigf.dat')
c
        return
        end
c
c
        subroutine adjoint
        character*60 link2,link3,link4,link5,link6,link7
        character*60 link8,link9,link11,link12
c

```

```

link2='cp xs ft02f001      '
link3='mv input input.forward '
link4='cp input.adj input  '
link5='tdkenoadj          '
link6='cat _out* input > output.adj '
link7='rm _out* input _p*   '
link8='mv output.adj      output '
link9='mv input.forward  input  '
link11='rm ft08f001 ft09f001 ft14f001 '
link12='rm tdkenoadj      '
c
status=system(link2)
if (status.ne.0) stop
status=system(link3)
if (status.ne.0) stop
status=system(link4)
if (status.ne.0) stop
status=system(link5)
if (status.ne.0) stop
status=system(link6)
if (status.ne.0) stop
status=system(link7)
status=system(link8)
if (status.ne.0) stop
status=system(link9)
if (status.ne.0) stop
status=system(link11)
status=system(link12)
c
return
end
c
c
subroutine ssforward
character*60 link1,link2,link4,link5,link6,link7
character*60 link8,link9,link10
c
link9='cp input.for input      '
link1='cp xspmc ft43f001      '
link2='cp xsmc ft02f001      '
link4='cat norm.out >> outfile '
link10='rm norm.out          '
link5='mv fluxnew.dat flux.dat '
link6='mv ft46f001 timen.dat  '
link7='cp flux.dat flux.ss    '
link8='mv flux.ss output      '
c
status=system(link9)
if (status.ne.0) stop
status=system(link1)
if (status.ne.0) stop
status=system(link2)
if (status.ne.0) stop
call kenova
call norm
status=system(link4)
status=system(link10)
status=system(link5)
status=system(link6)
status=system(link7)
status=system(link8)
c
return
end
c
subroutine transhape
character*60 link1,link2,link3,link4,link5,link6,link7
character*60 link8,link9
c
link9='cp input.for input      '
link1='mv timen.dat ft46f001   '
link2='mv delay.dat ft47f001   '
link3='cat norm.out >> outfile '

```



```

link4='rm norm.out           '
link5='mv fluxnew.dat flux.dat '
link6='cat rho.out >> rho.dat '
link7='cat ptkin.out >> outfile '
link8='rm ptkin.out         '
c
status=system(link1)
if (status.ne.0) stop
status=system(link2)
if (status.ne.0) stop
call kenova
call norm
status=system(link3)
status=system(link4)
status=system(link5)
call rho
status=system(link6)
if (status.ne.0) stop
call ptkin
status=system(link7)
if (status.ne.0) stop
status=system(link8)
if (status.ne.0) stop
c
return
end
c
subroutine extrap
character*60 link1,link2,link3,link4,link5,link6,link7
character*60 link8,link9
c
link8='cp xsmc ft43f001       '
link9='cp xspmc ft02f001     '
link7='mv timen.dat time0.dat '
link1='cat rho.out >> rho.dat '
link2='cat ptkin.out >> outfile '
link3='rm ptkin.out         '
link4='cat delay.dat >> cdelay.dat '
link5='cat cdelay.out >> outfile '
link6='rm cdelay.out         '
c
status=system(link8)
status=system(link9)
status=system(link7)
if (status.ne.0) stop
call rho
status=system(link1)
if (status.ne.0) stop
call ptkin
status=system(link2)
if (status.ne.0) stop
status=system(link3)
if (status.ne.0) stop
call cdelay
status=system(link4)
if (status.ne.0) stop
status=system(link5)
if (status.ne.0) stop
status=system(link6)
if (status.ne.0) stop
c
return
end
*****
*                               *
*               SUBROUTINE RHO   *
*                               *
*****
subroutine rho
c-----
c
c calculate point kinetics parameters including: reactivity,
c generation time, effective betas, F(t), precursor densities,

```

```

c      and extraneous source.
c
c      nntmef = no. of time steps on flux.dat
c      nntmes = no. of time steps on nusigf.dat
c      nnamp  = no. of time steps on timen.dat
c      ntimef = max no of flux shape calcs
c      ntimes = max no of times on nusigf.dat file
c      namp   = max no of times on timen.dat file
c      nproca = max no of processes on ampx file
c      irhonum =no. of intermediate reactivity calculations
c      ipknum = no. of intermediate point kinetics calculations
c-----
c
c      common/flags/irhonum, ipknum
c      common/unitsrho/iout, isigf, iflux, ikin, iadjoint, icexss, icexsp,
* itimen, iflux0, igen
c      common/paramrho/kmax, ngp, ntimef, ntimes, namp, nadjph, nadjth,
* nntmef, nntmes, nnamp, nmat, ndg, nadjn, ngp1, iflag
c      double precision d
c      dimension d(500000)
c      data limmem/500000/
c      integer nadjn, nadjph, nadjth, iflag
c
c
c      ntimef = 40
c      ntimes = 20
c      namp   = 10000
c      nproca = 6
c
c      call ofilerho
c
c      rewind iflux
c      rewind isigf
c      rewind ikin
c      rewind itimen
c      rewind iout
c
c      read(iflux,940)kmax,ngp
c      write(iout,*)('kmax from flux file = ',kmax)
c      write(iout,*)('ngp from flux file = ',ngp)
c
c      read(isigf,940)kmax0,ngp0,nmat
c      write(iout,*)
c      write(iout,*)('kmax from nusigf file = ',kmax0)
c      write(iout,*)('ngp from nusigf file = ',ngp0)
c      write(iout,*)('nmat from nusigf file = ',nmat)
c      if(kmax0 .ne. kmax)then
c          write(iout,950)kmax,kmax0
c          stop
c      end if
c      if(ngp0 .ne. ngp)then
c          write(iout,960)ngp,ngp0
c          stop
c      end if
c
c      read(ikin,941) ndg
c      write(iout,*)
c      write(iout,*)('ndg from kinetics file = ',ndg)
c
c
c      read(iout,*) iflag
c      write(6,*)('Iflag = ',iflag)
c
c-----input adjoint data
c
c      rewind iadjoint
c      read(iadjoint)nadjph,nadjth
c      write(iout,*)('nadjph and nadjth from adjoint file = ',
c      * nadjph,nadjth)
c      nadjn=nadjph*nadjth
c
c-----generate array pointers
c      ngp1 = ngp + 1

```

```

lflux = 1
lsigf = lflux + kmax*ngp*ntimef
lalamda = lsigf + nmat*ngp*ntimes
lbeta = lalamda + ndg
lfluxti = lbeta + ndg
lsigfti = lfluxti + ntimef
lncor = lsigfti + ntimes
lvol = lncor + kmax
lcon = lvol + kmax
lbin = lcon + ntimef
lvel = lbin + nadjn
lc = lvel + ngp1
lci = lc + ndg
ladflux = lci + ndg
lchi = ladflux + ngp*kmax
lds = lchi + ngp
lids = lds + nproca
lxs = lids + 50
lys = lxs + kmax*nmat
ldp = lys + nmat*nmat
lidp = ldp + nproca
lxp = lidp + 50
lyp = lxp + kmax*nmat
ldelx = lyp + nmat*nmat
lscats = ldelx + kmax*nmat
lscatp = lscats + nmat*ngp1
ldelscat = lscatp + nmat*ngp1
lbetaeff = ldelscat + nmat*ngp1
lid3s = lbetaeff + ndg*(irhonum + 1)
lid3p = lid3s + nmat*nmat*ngp
lid4s = lid3p + nmat*nmat*ngp
lid4p = lid4s + nproca
lrhoti = lid4p + nproca
lgen = lrhoti + (irhonum + 1)
lrho = lgen + (irhonum + 1)
lbetai = lrho + (irhonum + 1)
iend = lbetai + ndg
c write(6,*)(iend = ',iend)
if(iend .gt.limmem)then
    write(iout,900)limmem,iend
    stop
end if
c
c call mastrho(d(lflux),d(lsigf),d(lalamda),d(lbeta),d(lfluxti),
* d(lsigfti),d(lncor),d(lvol),d(lcon),d(lbin),d(lvel),d(lc),
* d(lci),d(ladflux),d(lchi),d(lds),d(lids),d(lxs),d(lys),
* d(ldp),d(lidp),d(lxp),d(lyp),d(ldelx),d(lscats),d(lscatp),
* d(ldelscat),d(lbetaeff),d(lid3s),d(lid3p),d(lid4s),d(lid4p),
* d(lrhoti),d(lgen),d(lrho),d(lbetai))
c
c close (iout)
close (lsigf)
close (lflux)
close (lkin)
close (iadjoint)
close (icexss)
close (icexsp)
close (itimen)
close (lflux0)
close (igen)
c
c return
900 format(1x,'insufficient memory',2i10)
940 format(3i5)
941 format(2i5)
942 format(7e11.4)
950 format(1x,'kmax not consistent in interface files in main',2i5)
960 format(1x,'ngp not consistent in interface files in main',2i5)
end
c
c
c subroutine mastrho(flux,sigf,alamda,beta,fluxti,sigfti,ncor,
* vol,con,bin,vel,c,ci,adflux,chi,ds,ids,xs,ys,dp,idp,xp,

```

```

* yp,delx,scats,scatp,delscat,betaeff,id3s,id3p,id4s,id4p
* rhoti,gen,rho,betaeffi)
-----
c
c   mastrho is the controlling subroutine
c
-----
c
common/flags/irhonum,ipknum
common/unitsrho/iout,isigf,iflux,ikin,iadjoin,icexss,icexsp,
* itimen,iflux0,igen
common/paramrho/kmax,ngp,ntimef,ntimes,namp,nadjph,nadjth,
* nntmf,nntmes,nnamp,nmat,ndg,nadjn,ngp1,iflag
dimension flux(ngp,kmax,ntimef),sigf(ngp,nmat,ntimes)
dimension alanda(ndg),beta(ndg),betaeffi(ndg)
dimension fluxti(ntimef),sigfti(ntimes),ncor(kmax)
dimension vol(kmax),con(ntimef),bin(nadjn),vel(ngp+1)
dimension c(ndg),ci(ndg),adflux(ngp,kmax),chi(ngp)
dimension ds(6),ids(50),xs(21,5),ys(5,5),dp(6),idp(50)
dimension xp(21,5),yp(5,5),delx(5,21),scats(nmat,3)
dimension scatp(nmat,3),delscat(nmat,3),betaeff(irhonum+1,ndg)
dimension rho(irhonum+1),gen(irhonum+1),rhoti(irhonum+1)
integer id3s(10,5),id3p(10,5),id4s(6),id4p(6)
real time,pow

c
c-----input delayed neutron data
c
read(ikin,945)(alanda(i),i=1,ndg)
read(ikin,945)(beta(i),i=1,ndg)
c   write(6,*)('ndg = ',ndg)
c   do 801 i=1,ndg
c     write(6,*)('beta from kinetics file = ',beta(i),
c * ' for group ',i)
c 801 continue
c
c-----input precursor densities
c
101 continue
read(itimen,901,end=201) time,pow,xlum,xlum,xlum
read(itimen,902,end=201) (c(i),i=1,ndg)
go to 101
201 continue
c   write(iout,*)('time of flux shape = ',time)
c   write(iout,*)('amplitude = ',pow)
c   do 802 i=1,ndg
c     write(iout,*)('precursor concentrations = ',c(i),
c * 'for group',i)
c 802 continue
c
c-----input steady state adjoint fluxes and angular bins
c
call inadj(bin,adflux)
c
c-----input cross sections and calculate deltas
c
rewind icexss
rewind icexsp
c-----input unperturbed cross-section data
read(icexss) ids
c   write(iout,*) (ids(j),j=1,14)
read(icexss) ds
c   write(iout,*) ds
do 100 i=1,ids(2)
read(icexss) ids
c   write(iout,10300) ids(19),(ids(n),n=1,18)
c   write(iout,*) (ids(n),n=20,48),ids(50)
10300 format (i2,4x,18a4)
read(icexss) (id3s(o,i),xs(2*o-1,i),xs(2*o,i),o=1,ids(28))
do 110 k=1,ids(28)
c   write(iout,*) ('MT = ',id3s(k,i))
c   write(iout,10400) xs(2*k-1,i),xs(2*k,i)
110 continue
10400 format ('Group 1= ',E16.8,2x,'Group2= ',E16.8)

```

```

j=0
l=ids(23)
read(icexss) id4s
c   write(iout,*) ('Transfer Matrix Pointers are ',id4s)
read(icexss) (ys(j,i),j=1,ids(23))
c   write(iout,*) ('Scatter Probs are ',(ys(j,i),j=1,ids(23)))
100 continue
c-----input perturbed cross-section data
read(icexsp) idp
c   write(iout,*) (idp(j),j=1,14)
read(icexsp) dp
c   write(iout,*) dp
do 103 i=1,idp(2)
read (icexsp) idp
c   write(iout,10300) idp(19),(idp(n),n=1,18)
c   write(iout,*) (idp(n),n=20,48),idp(50)
read(icexsp) (id3p(o,i),xp(2*o-1,i),xp(2*o,i),o=1,idp(28))
do 113 k=1,idp(28)
c   write(iout,*) ('MT = ',id3p(k,i))
c   write(iout,10400) xp(2*k-1,i),xp(2*k,i)
113 continue
j=0
l=idp(23)
read(icexsp) id4p
c   write(iout,*) ('Transfer Matrix Pointers are ',id4s)
read(icexsp) (yp(j,i),j=1,idp(23))
c   write(iout,*) ('Scatter Probs are ',(yp(j,i),j=1,idp(23)))
103 continue
c-----calculate delta cross-sections
c-----note that the cross-sections are loaded as follows:
c   i=1,2 for total cross-section (group 1 and 2)
c   i=3,4 for nu*sigf (group 1 and 2)
c   i=5,6 for chi spectrum (group 1 and 2)
c   i=7,8 for absorption cross-section (group 1 and 2)
c   i=9,10 not used
c   i=11,12 for average nu (group 1 and 2)
c   i=13,14 for total non-absorption cross-section (group 1 and 2)
c-----note that the scatter probabilities are loaded as follows:
c   i=1 for group 1 to group 1
c   i=2 for group 1 to group 2
c   i=3 for group 2 to group 2
i2times = 2*ids(28)
do 114 i=1,nmat
do 115 j=1,i2times
delx(i,j) = xp(j,i) - xs(j,i)
c   write(iout,*)('Delta cross-section for material ',i,
c   * ' process ',j,' = ',delx(i,j))
115 continue
114 continue
c-----construct transfer matrix
do 126 i=1,nmat
do 127 j=1,ngp
scaterms = (xs(j,i) - xs(6+j,i))
scatermp = (xp(j,i) - xp(6+j,i))
if(j.eq.1) then
do 128 k=1,2
scats(i,k) = scaterms*ys(k,i)
scatp(i,k) = scatermp*yp(k,i)
128 continue
else
scats(i,3) = scaterms
scatp(i,3) = scatermp
end if
127 continue
126 continue
do 129 i=1,nmat
do 131 k=1,3
c   write(iout,*)('Unperturbed scatter for material ',i,
c   * ' process ',k,' = ',scats(i,k))
c   write(iout,*)('Perturbed scatter for material ',i,
c   * ' process ',k,' = ',scatp(i,k))
131 continue
129 continue

```

```

c-----calculate deltas for transfer matrix
  do 132 i=1,nmat
    do 133 j=1,3
      delscat(i,j) = scatp(i,j) - scats(i,j)
c      write(iout,*)('Delta scatter for material ',i,' process ',
c      * j,' = ',delscat(i,j))
      133 continue
    132 continue
c
c-----input flux shapes and times
c
  call nfluxrho(flux,rhoww,genww)
c
  call gettimrho(fluxti,itimes)
c
  do 830 i=1,itimes
c  write(iout,999)(fluxti(i))
  do 831 j=1,ngp
    do 832 k=1,kmax
c    write(iout,*)('Flux shape for material ',k,' group ',j,
c    * ' = ',flux(j,k,i))
    832 continue
  831 continue
  830 continue
  999 format(1x,'Fluxti = ',7e11.4)
c  write(6,*)('Time = ',fluxti(nntmef))
  do 833 i=1,ndg
c    write(iout,*)('Delayed neutron fraction for group ',
c    * i,' = ',beta(i))
  833 continue
c
c-----calculate times of reactivity calculations
c
  if (iflag.eq.-2) then
    nntmefp1 = nntmef + 1
  else
    nntmefp1 = nntmef
  end if
c
  if(nntmef.gt.0) then
    rhoti(irhonum+1) = fluxti(nntmefp1)
    do it=1,irhonum
      rhoti(it) = fluxti(nntmefp1 - 1) +
*      ((fluxti(nntmefp1) - fluxti(nntmefp1 - 1))/
*      irhonum)*(it-1)
    end do
  else
    write(iout,*)('Not enough data on flux file!')
    stop
  end if
c  write(iout,*)('Time0 = ',fluxti(nntmef - 1))
  do iw=1,irhonum+1
c    write(6,*)('Rhoti = ',rhoti(iw))
  end do
c
c-----input sigf, volumes, chi, times, velocities, and ncor
c
  call nsigfrho(sigf,sigfti,ncor,vol,chi,vel)
c
  do 834 k=1,kmax
c    write(iout,*)('Volume for region ',k,' = ',vol(k))
  834 continue
  do 835 j=1,ngp
c    write(iout,*)('Chi for energy group ',j,' = ',chi(j))
  835 continue
  do 836 j=1,ngp
c    write(iout,*)('Velocity for energy group ',j,' = ',vel(j))
  836 continue
  do 837 k=1,kmax
c    write(iout,*)('Corresponding index # for region ',k,' = ',ncor(k))
  837 continue
  do 838 i=1,nntmes
c    write(iout,*)('Sigf time = ',sigfti(i))

```

```

        do 839 k=1,nmat
          do 840 j=1,ngp
c           write(iout,*)('Nusigf for material ',k,' group ',j,
c            *          ' = ',sigf(j,k,i))
            840 continue
            839 continue
            838 continue
c
c-----begin iteration over shape time step
c
          do 111 i=1,irhonum+1
c
c-----calculate F(t)
c
            fterm = 0.0
            geni = 0.0
            rhoi = 0.0
            t = 0.0
            do iini = 1,ndg
              betaeffi(iini) = 0.0
            end do
            t = rhoti(i)
c
c          call calcf(fterm,flux,sigf,ncor,chi,adflux,vol,t,fluxti)
c          write(6,*)('Rhoti = ',t)
c          write(6,*)('F(t) = ',fterm)
c
c-----calculate generation time
c
            call calclam(adflux,flux,vel,geni,fterm,vol,t,fluxti)
            gen(i) = geni
c          write(6,*)('Gen = ',geni)
c
c-----calculate reactivity
c
            call calcrho(adflux,flux,fterm,deltx,delscat,
            * ncor,chi,rhoi,vol,t,fluxti)
            rho(i) = rhoi
c
c-----calculate effective betas
c
            call calcbeta(flux,sigf,ncor,adflux,chi,
            * beta,betaeffi,vol,fterm,t,fluxti)
c
            betaefft = 0.0
            do 181 ib = 1,ndg
              betaeff(i,ib) = betaeffi(ib)
c              write(6,*)('Betaeff = ',betaeff(i,ib),' i & group = ',i,ib)
              betaefft = betaefft + betaeffi(ib)
            181 continue
c            write(6,*)('Betaefft = ',betaefft)
c
c-----calculate effective precursor densities
c
            call calcpd(c,ci,flux,ncor,adflux,chi,vol,fterm,geni)
c
            111 continue
c
c-----end iteration over shape time step
c
c-----write parameters to interface file
c
            call uploadrho(gen,betaeff,rho,c,rhoti)
c
            return
c
c-----End of master
c
            945 format(6e11.4)
            901 format(5e11.4)
            902 format(11x,6e11.4)
            end

```

```

c
  subroutine ofilerho
  common/unitsrho/iout, isigf, iflux, ikin, iadjoint, icexss, icexsp,
  * itimen, iflux0, igen
c
  iout   = 44
  isigf  = 54
  iflux  = 55
  ikin   = 49
  iadjoint = 42
  icexss = 43
  icexsp = 2
  itimen = 41
  igen  = 45
c
c-----open files
c
  open(44, file='rho.out', status='old', form='formatted')
  open(54, file='nusigf.dat', status='old', form='formatted')
  open(55, file='flux.dat', status='old', form='formatted')
  open(49, file='kinetics.dat', status='old', form='formatted')
  open(42, file='ft42f001', status='old', form='unformatted')
  open(43, file='ft43f001', status='old', form='unformatted')
  open(2, file='ft02f001', status='old', form='unformatted')
  open(41, file='time0.dat', status='old', form='formatted')
  open(45, file='general.dat', status='old', form='formatted')
c
  rewind 44
  rewind 54
  rewind 55
  rewind 49
  rewind 42
  rewind 43
  rewind 2
  rewind 41
  rewind 45
  return
  end
c
  subroutine nfluxrho(flux, rhoww, genww)
c-----
c
c   input flux shapes
c-----
c
  common/flags/irhonum, ipknum
  common/unitsrho/iout, isigf, iflux, ikin, iadjoint, icexss, icexsp,
  * itimen, iflux0, igen
  common/paramrho/kmax, ngp, ntimef, ntimes, namp, nadjph, nadjth,
  * nntmef, nntmes, nnamp, nmat, ndg, nadjn, ngp1, iflag
  dimension flux(ngp, kmax, ntimef), fluxti(ntimef), beta(ndg)
  dimension con(ntimef)
  integer ig, ix
c
  ix = 0
40 continue
c
  ip1 = ix + 1
  ip2 = ix + 2
  if(ip2 .gt. ntimef)then
    write(iout, 910)ntimef
    stop
  end if
c
  read(iflux, 970, end=50)fluxti(ip1), rhoww, genww, con(ip1)
  read(iflux, 930, end=50)((flux(ig, k, ip1), ig=1, ngp), k=1, kmax)
  read(iflux, 930, end=50)(xdum, j=1, ndg)
  ix = ix + 1
  go to 40
50 continue
c
  nntmef = ix

```



```

        if(nntmef .le. 0) then
            write(iout,990)
            stop
        end if
c
c-----For first pass, linearly extrapolate the flux
c
        if (iflag.eq.-2) then
            nntmefp1 = nntmef + 1
c
            write(6,*)('nntmef = ',nntmef)
            do ig=1,ngp
                do k=1,kmax
                    flux(ig,k,nntmefp1) = flux(ig,k,nntmef)
                end do
            end do
        end if
c
c
        return
910 format(1x,'more times on flux.dat than allowed',i11)
930 format(6e11.4)
940 format(i5)
970 format(4e11.4)
990 format(1x,'no data on flux.dat')
        end
c
        subroutine nsigfrho(sigf,sigfti,ncor,vol,chi,vel)
c-----
c
c    input sigf, volumes
c-----
c
c
        common/unitsrho/iout,isigf,iflux,ikin,iadjoin,icexss,icexsp,
        * itimen,iflux0,igen
        common/paramrho/kmax,ngp,ntimef,ntimes,namp,nadjph,nadjth,
        * nntmef,nntmes,nnamp,nmat,ndg,nadjn,ngp1,iflag
        common/flags/irhonum,ipknum
        dimension sigf(ngp,nmat,ntimes),sigfti(ntimes)
        dimension ncor(kmax),vol(kmax),chi(ngp)
        dimension vel(ngp1)
c
        read(isigf,930)(vol(k),k=1,kmax)
        read(isigf,915)(chi(ig),ig=1,ngp)
        read(isigf,916)(vel(ig),ig=1,ngp1)
c
        write(6,*)('ngp1 = ',ngp1)
        read(isigf,950)(ncor(k),k=1,kmax)
c
c
        i2 = 0
30 continue
c
        i = 0
40 continue
c
        i = i + 1
        if(i .gt. ntimes)then
            write(iout,910)ntimes
            stop
        end if
c
        read(isigf,930)sigfti(i),
        * ((sigf(ig,m,i),ig=1,ngp),m=1,nmat)
        if(sigfti(i) .lt. 0.0)then
            i = i - 1
            go to 50
        end if
        go to 40
50 continue
c
c
c-----just read nusigf, go back for sigf
c

```

```

        if(i2 .eq. 0)then
            i2 = 1
            go to 30
        end if
c
        nntmes = i
        if(nntmes .le. 0) then
            write(iout,990)
            stop
        end if
c
c-----convert energy boundaries to velocities
c
        ig = 0
    80 continue
            ig = ig + 1
            eb = sqrt(vel(ig)*vel(ig+1))
            vel(ig) = 1.3859e+6*sqrt(eb)
            if(ig.lt.ngp) then
                go to 80
            end if
c
        return
    910 format(1x,'more times on nusigf.dat than allowed',i11)
    915 format(2e11.4)
    916 format(3e11.4)
    930 format(6e11.4)
    940 format(2i5)
    950 format(12i5)
    990 format(1x,'no data on nusigf.dat')
        end
c
        subroutine inadj(bin,adflux)
        common/unitsrho/iout,isigf,iflux,ikin,iadjoint,icexss,icexsp,
        * itimen,iflux0,igen
        common/paramrho/kmax,ngp,ntimef,ntimes,namp,nadjph,nadjth,
        * nntmef,nntmes,nnamp,nmat,ndg,nadjn,ngp1,iflag
        common/flags/irhonum,ipknum
        dimension bin(nadjn),adflx(ngp*nadjn,kmax)
        dimension adflux(ngp,kmax)
c
        nadjt1 = nadjth + 1
        nadjp1 = nadjph + 1
        read(iadjoint)(bin(i),i=1,nadjp1)
        do 803 i=1,nadjp1
c
            write(iout,*)('phi bins = ',bin(i))
    803 continue
            read(iadjoint)(bin(i+nadjp1),i=1,nadjt1)
            do 804 i=1,nadjt1
c
                write(iout,*)('theta bins = ',bin(i+nadjp1))
    804 continue
                do 111 k=1,kmax
                    do 112 j=1,ngp
                        ipoint=(j-1)*nadjn
                        read(iadjoint)(adflx(ipoint+i,k),i=1,nadjn)
    112 continue
    111 continue
                    do 805 k=1,kmax
                        do 806 j=1,ngp
                            do 807 i=1,nadjn
                                ipoint=(j-1)*nadjn
                                write(iout,*)('Adjoint flux for material ',k,' group ',
c
                                * j,' and bin ',i,' = ',adflx(ipoint+i,k))
c
    807 continue
    806 continue
    805 continue
                    do 810 j=1,ngp
                        do 811 k=1,kmax
                            adflux(j,k)=0.0
    811 continue
    810 continue
c
                do 116 k=1,kmax

```

```

        do 117 j=1,ngp
            ipoint=(j-1)*nadjn
            do 118 i=1,nadjn
                adflux(j,k)=adflux(j,k)+adflx(i+ipoint,k)
            118 continue
        c        write(iout,*)('Adjoint flux for ',k,' group ',
        c        *      j,' = ',adflux(j,k))
        117 continue
        116 continue
        return
    end

c
    subroutine calcf(fterm,flux,sigf,ncor,chi,adflux,vol,t,
    * fluxti)
    common/paramrho/kmax,ngp,ntimef,ntimes,namp,nadjph,nadjth,
    * nntmef,nntmes,nnamp,nmat,ndg,nadjn,ngp1,iflag
    common/flags/irhonum,ipknum
    dimension flux(ngp,kmax,nntmef+1)
    dimension sigf(ngp,nmat,nntmes),ncor(kmax)
    dimension term1(kmax),term2(kmax*ngp),chi(ngp)
    dimension adflux(ngp,kmax),vol(kmax),fluxti(nntmef+1)
c-----perform the integral over all other energies first
    do 100 i=1,kmax
        term1(i) = 0.0
        do 110 ig=1,ngp
            d = ncor(i)
            call intflrho(flux,t,xflux,fluxti,ig,i)
            term1(i) = term1(i) + xflux*
            *      sigf(ig,d,nntmes)
        110 continue
    100 continue
c-----multiply by spectrum and adjoint flux
    do 120 ig=1,ngp
        do 130 i=1,kmax
            l = i + kmax*(ig-1)
            term2(l) = 0.0
            term2(l) = term1(i)*chi(ig)*adflux(ig,i)
        130 continue
    120 continue
c-----perform integration over volume and energy
    do 140 ig=1,ngp
        do 150 i=1,kmax
            l = i + kmax*(ig-1)
            fterm = fterm + term2(l)*vol(i)
        150 continue
    140 continue
c-----end calculating F(t)
    return
    end

c
    subroutine calclam(adflux,flux,vel,gen,fterm,vol,
    * t,fluxti)
    common/paramrho/kmax,ngp,ntimef,ntimes,namp,nadjph,nadjth,
    * nntmef,nntmes,nnamp,nmat,ndg,nadjn,ngp1,iflag
    common/flags/irhonum,ipknum
    dimension adflux(ngp,kmax),flux(ngp,kmax,nntmef+1)
    dimension vel(ngp+1),term2(kmax*ngp),vol(kmax)
    dimension fluxti(nntmef+1)

c
c-----multiply forward flux and adjoint flux and velocities
    do 120 ig=1,ngp
        do 130 i=1,kmax
            l = i + kmax*(ig-1)
            call intflrho(flux,t,xflux,fluxti,ig,i)
            term2(l) = 0.0
            term2(l) = (adflux(ig,i)*xflux)/vel(ig)
        130 continue
    120 continue
c-----perform integration over volume and energy
    do 140 ig=1,ngp
        do 150 i=1,kmax
            l = i + kmax*(ig-1)
            gen = gen + term2(l)*vol(i)

```

```

150 continue
140 continue
    gen = gen/fterm
    return
    end
c
    subroutine calcrho(adflux,flux,fterm,delx,delscat,
* ncor,chi,rho,vol,t,fluxti)
    common/unitsrho/iout,isigf,iflux,ikin,iadjoint,icexss,icexsp,
* itimen,iflux0,igen
    common/paramrho/kmax,ngp,ntimef,ntimes,namp,nadjph,nadjth,
* nntmef,nntmes,nnamp,nmat,ndg,nadjn,ngp1,iflag
    common/flags/irhonum,ipknum
    dimension adflux(ngp,kmax),flux(ngp,kmax,nntmef+1)
    dimension delx(nmat,kmax),delscat(nmat,ngp1+1)
    dimension chi(ngp),vol(kmax),fluxti(nntmef+1)
    dimension term1(kmax*ngp),ncor(kmax),term5(kmax*ngp)
    dimension term2(kmax*ngp),term4(kmax),term6(kmax*ngp)
    do 10 ig=1,ngp
        do 20 i=1,kmax
            d = i + kmax*(ig-1)
            id = ncor(i)
            term1(d) = 0.0
            call intflrho(flux,t,xflux,fluxti,ig,i)
            term1(d) = delx(id,ig)*adflux(ig,i)*xflux
c            write(iout,*)('Term1= ',term1(d),' id= ',id,' k= ',i)
20 continue
10 continue
c
        do 21 i=1,nmat
            delscat(i,4) = 0.0
21 continue
c
        do 30 ig=1,ngp
            do 40 i=1,kmax
                d = i + kmax*(ig-1)
                term2(d) = 0.0
                id = ncor(i)
                call intflrho(flux,t,xflux,fluxti,ig,i)
                do 50 ig1=1,ngp
                    if(ig.eq.1) then
                        b = ig1
                    else
                        b = ig1 + 2
                    end if
                    term2(d) = term2(d) +
*                    delscat(id,b)*xflux
c            write(iout,*)('Delscat= ',delscat(id,b),' ig= ',ig,' b=',b)
50 continue
                term2(d) = term2(d)*adflux(ig,i)
c            write(iout,*)('Term2= ',term2(d),' id= ',id,' k= ',i)
40 continue
30 continue
c
            do 60 i=1,kmax
                term4(i) = 0.0
                do 70 ig=1,ngp
                    id = ncor(i)
                    call intflrho(flux,t,xflux,fluxti,ig,i)
                    c = ig + 2
                    term4(i) = term4(i) +
*                    delx(id,c)*xflux
70 continue
c            write(iout,*)('Term4= ',term4(i),' ig= ',ig,' k= ',i)
60 continue
c
            do 61 ig=1,ngp
                do 71 i=1,kmax
                    d = i + kmax*(ig-1)
                    term6(d) = 0.0
                    term6(d) = term4(i)*chi(ig)*adflux(ig,i)
c            write(iout,*)('Term6= ',term6(d),' ig= ',ig,' k= ',i)
71 continue

```

```

61 continue
c
do 80 ig=1,ngp
do 90 i=1,kmax
d = i + kmax*(ig-1)
term5(d) = 0.0
term5(d) = - term1(d) + term2(d) + term6(d)
c write(iout,*)('Term5= ',term5(d),' ig= ',ig,' k= ',i)
90 continue
80 continue
c
do 140 ig=1,ngp
do 150 i=1,kmax
l = i + kmax*(ig-1)
rho = rho + term5(l)*vol(i)
150 continue
140 continue
rho = rho/fterm
c write(6,*)('Rho = ',rho)
c
return
end
c
subroutine calcbeta(flux,sigf,ncor,adflux,chi,
* beta,betaeff,vol,fterm,t,fluxti)
common/unitsrho/iout,isigf,iflux,ikin,iadjoin,icexss,icexsp,
* itimen,iflux0,igen
common/paramrho/kmax,ngp,ntimef,ntimes,namp,nadjph,nadjth,
* nntmef,nntmes,nnamp,rmat,ndg,nadjn,ngp1,iflag
common/flags/irhonum,ipknum
dimension term1(kmax),flux(ngp,kmax,nntmef+1)
dimension sigf(ngp,rmat,nntmes),ncor(kmax)
dimension adflux(ngp,kmax),chi(ngp),term2(ngp*kmax)
dimension beta(ndg),betaeff(ndg),vol(kmax)
dimension fluxti(nntmef+1)
do 10 id=1,ndg
do 100 i=1,kmax
term1(i) = 0.0
do 110 ig=1,ngp
d = ncor(i)
call intflrho(flux,t,xflux,fluxti,ig,i)
term1(i) = term1(i) + xflux*
* sigf(ig,d,nntmes)
110 continue
100 continue
c-----multiply by spectrum and adjoint flux
do 120 ig=1,ngp
do 130 i=1,kmax
l = i + kmax*(ig-1)
term2(l) = 0.0
term2(l) = term1(i)*chi(ig)*adflux(ig,i)*beta(id)
130 continue
120 continue
c
do 140 ig=1,ngp
do 150 i=1,kmax
l = i + kmax*(ig-1)
betaeff(id) = betaeff(id) + term2(l)*vol(i)
150 continue
140 continue
betaeff(id) = betaeff(id)/fterm
c write(6,*)('Betaeff = ',betaeff(id),' for group ',id)
c
10 continue
return
end
c
subroutine calcpd(c,ci,flux,ncor,adflux,chi,vol,fterm,gen)
common/unitsrho/iout,isigf,iflux,ikin,iadjoin,icexss,icexsp,
* itimen,iflux0,igen
common/paramrho/kmax,ngp,ntimef,ntimes,namp,nadjph,nadjth,
* nntmef,nntmes,nnamp,rmat,ndg,nadjn,ngp1,iflag
common/flags/irhonum,ipknum

```

```

dimension flux(ngp,kmax,nntmef+1)
dimension ncor(kmax)
dimension adflux(ngp,kmax),chi(ngp),term2(ngp*kmax)
dimension vol(kmax),c(ndg),ci(ndg)
do 10 id=1,ndg
c-----multiply by spectrum and adjoint flux
do 120 ig=1,ngp
do 130 i=1,kmax
l = i + kmax*(ig-1)
term2(l) = 0.0
term2(l) = chi(ig)*adflux(ig,i)*c(id)
130 continue
120 continue
c
do 140 ig=1,ngp
do 150 i=1,kmax
l = i + kmax*(ig-1)
ci(id) = ci(id) + term2(l)*vol(i)
150 continue
140 continue
ci(id) = ci(id)/(fterm*gen)
c write(6,*)('C = ',c(id),' for group ',id)
c
10 continue
return
end
c
c
subroutine uploadrho(gen,betaeff,rho,c,rhoti)
common/unitsrho/iout, isigf, iflux, ikin, iadjoint, icexss, icexsp,
* itimen, iflux0, igen
common/paramrho/kmax, ngp, ntimef, ntimes, namp, nadjph, nadjth,
* nntmef, nntmes, nnamp, nmat, ndg, nadjn, ngp1, iflag
common/flags/irhonum, ipknum
dimension betaeff(irhonum+1,ndg),c(ndg),rhoti(irhonum+1)
dimension gen(irhonum+1),rho(irhonum+1)
rewind iout
if (iflag.eq.-1) then
iflag = -2
else
iflag = -1
end if
write(iout,*) iflag
do 100 i=1,irhonum+1
write(iout,800) rhoti(i),gen(i),rho(i)
write(iout,810)(c(in),in=1,ndg)
write(iout,810)(betaeff(i,in),in=1,ndg)
100 continue
c
800 format(3e14.7)
810 format(6e14.7)
return
end
c
subroutine intflrho(flux,t,x,fluxti,ig,k)
c-----
c
c interpolate flux values
c-----
c
common/paramrho/kmax, ngp, ntimef, ntimes, namp, nadjph, nadjth,
* nntmef, nntmes, nnamp, nmat, ndg, nadjn, ngp1, iflag
common/flags/irhonum, ipknum
dimension flux(ngp,kmax,nntmef+1)
dimension fluxti(nntmef+1)
c
if (iflag.eq.-2) then
nntmefp1 = nntmef + 1
else
nntmefp1 = nntmef
end if
c

```

```

        if(nntmef.le.0)then
            write(iout,*)('Not enough data on flux file!')
            stop
        else
            x=flux(ig,k,nntmefp1-1)+(flux(ig,k,nntmefp1)-
                flux(ig,k,nntmefp1-1))*
            * (t-fluxti(nntmefp1-1))/(fluxti(nntmefp1)-
            * fluxti(nntmefp1-1))
            end if
            return
        end
    c
    subroutine gettimrho(fluxti,itimes)
        common/unitsrho/iout,isigf,iflux,ikin,iadjoin,icexss,icexsp,
        * itimen,iflux0,igen
        common/paramrho/kmax,ngp,ntimef,ntimes,namp,nadjph,nadjth,
        * nntmef,nntmes,nnamp,nmat,ndg,nadjn,ngp1,iflag
        common/flags/irhonum,ipknum
        dimension fluxti(ntimef)
        integer itimes
    c-----
    c   gettim reads tstop,delt, tin of general interface file
    c-----
    c
    c-----initial variables
    c
        rewind igen
    c
    c-----skip section #1
    c
        read(igen,902)isec,nrec
        do 20 ic=1,nrec
            read(igen,900)
        20 continue
    c
    c-----skip section #2 of general interface file
    c
        read(igen,902)isec,nrec
        do 30 ic=1,nrec
            read(igen,902)
        30 continue
    c
    c-----skip section 3 of interface file
    c
        read(igen,902)isec,nrec
        do 50 ic=1,nrec
            read(igen,902)
        50 continue
    c
    c-----read time data section #4
    c
        read(igen,902)isec,nrec
        itimes = nrec
        n=0
        100 continue
        read(igen,903)fluxti(n+1)
        n=n+1
        nlft=nrec-n
        if(nlft.gt.0)go to 100
    c
        900 format(80a1)
        902 format(15i5)
        903 format(7e11.4)
        904 format(1x,21hend of problem time=,f7.2)
    c
        return
        end
    c
    c
    *****
    *
    *           SUBROUTINE PTKIN
    *
    *****

```

```

*****
      subroutine ptkin
c-----
c
c   point kinetics code- no feedback
c
c-----
      common/flags/irhonum,ipknum
      common/rdata/rho(1000+1),gen(1000+1),pow,time,
      * betat(1000+1),tfuel,
      * tcool1,tcool2,tin,rhon,genn,betatn,iter,
      * tfuel0,tcol10,tcol20,pow0,rhoti(1000+1),
      * betaeff(1000+1,100)
      common/idata/inn,iout,ikin,itime0,ndg,itime0,ndg,itime0,ndg,itime0,ndg
      common/betdat/beta(100),alanda(100)
      external f
      double precision y,rtol,atol,tout,dtime,rwork,delt
c
      dimension c(100),c0(100),y(200)
      dimension rwork(500),iwork(100)
      integer iflag,iter
      data itol/1/
      data rtol/1.0d-04/
      data atol/0.0d0/
      data itask/1/
      data istate/1/
      data iopt/0/
      data lrw/500/
      data liw/100/
      data mf/22/
c
c-----assign logical unit #'s and open files
c
      call ofilepk
c
c-----input kinetics data
c
      call nkinpk(iflag,c)
c
      write(iout,*)('iflag = ',iflag)
      do 313 i=1,irhonum+1
c         write(iout,998)rhoti(i),gen(i),rho(i),betat(i)
c         write(iout,999)(betaeff(i,in),in=1,ndg)
c         write(iout,999)(c(in),in=1,ndg)
313 continue
998 format(4e14.7)
999 format(6e14.7)
c
c-----get power, c's, and last time
c
      call getpowpk(c,c0)
      write(iout,999)(c0(in),in=1,ndg)
c
c
c-----calculate system equation constants and initial conditions
c
      neq=1+ndg
      call calconpk(c,c0)
c
c-----initialize
c
      rhon  = rho(1)
      genn  = gen(1)
      betatn = betat(1)
      delt  = (rhoti(2) - rhoti(1))/ipknum
      tout  = time + delt
c
c-----load dependent variables into y array and normalize
c
      call dloadpk(y,neq,c,c0)
c
c-----begin iteration over tj points
c

```



```

do 100 iter=1,irhonum
c
tk    = rhoti(iter + 1)
delt  = (rhoti(iter + 1) - rhoti(iter))/ipknum
tstop = rhoti(irhonum+1)
betatn = betat(iter)
c
c   write(iout,*)('iter = ',iter)
c   write(iout,997)time,tstop,delt,tout
c 997 format('Time,tstop,delt,tout = ',4e11.4)
c
c-----integrate
c
170 continue
c
c-----time must be double precision
c
dtim = time
c
c
call lsode(f,neq,y,dtim,tout,itol,rtol,atol,itask,istate,
* iopt,rwork,lrw,iwork,liw,jac,mf)
c
time = dtim
if(istate.lt.0)go to 775
c
c-----unload y array and unnormalize
c
call unloadpk(y,neq,c)
c
c-----save to time file
c
call savpowpk(c)
c
c-----interpolate point kinetics parameters
c
if(time.ge.rhoti(1)) then
call intrhopk(xnew,time)
if (xnew.ge.0.0) then
rhon = xnew
end if
call intgenpk(xnew,time)
if (xnew.ge.0.0) then
genn = xnew
end if
end if
c
write(iout,*)('Time = ',time,' Reactivity = ',rhon)
c
write(iout,*)('Betatn = ',betatn,' Gen = ',genn)
c
write(iout,*)('Beta = ',betaeff(iter,ig),ig=1,ndg)
c
write(iout,*)('lamda = ',alamda(ig),ig=1,ndg)
c
if(time.ge.tstop)go to 700
if(time.ge.tk)go to 100
tout = time + delt
go to 170
c
100 continue
c
c
700 continue
c
c
write(iout,701)tstop
701 format(1x,'ptkin finished at time=',e11.4)
write(iout,702)pow
702 format(5x,'last power=',e11.4)
c
c
close (iout)
close (ikin)
close (itime0)
close (itimen)
close (igen)

```

```

        close (iflux)
        close (irho)
c
c
        return
775 continue
        write(iout,776)istate
776 format(1x,'error.....istate=',i4)
        stop
        end
c
c
        subroutine ofilepk
c-----
c
c   ofile assigns logical unit # & open files
c-----
c
        common/idata/inn,iout,ikin,itime0,ndg,itimen,igen,iflux,irho
c
        igen = 45
        itime0 = 41
        itimen = 46
        iout = 40
        ikin = 49
        iflux = 55
        irho = 44
c
        open(40,file='ptkin.out',status='unknown',form='formatted')
        open(45,file='general.dat',status='old',form='formatted')
        open(41,file='time0.dat',status='old',form='formatted')
        open(46,file='timen.dat',status='new',form='formatted')
        open(49,file='kinetics.dat',status='old',form='formatted')
        open(55,file='flux.dat',status='old',form='formatted')
        open(44,file='rho.out',status='old',form='formatted')
c
        rewind 40
        rewind 45
        rewind 41
        rewind 46
        rewind 49
        rewind 55
        rewind 44
c
        return
        end
        subroutine nkinpk(iflag,c)
c-----
c   nkin reads kinetics data
c-----
c
        common/flags/irhonum,ipknum
        common/betdat/beta(100),alamda(100)
        common/rdata/rho(1000+1),gen(1000+1),pow,time,
* betat(1000+1),tfuel,
* tcool1,tcool2,tin,rhon,genn,betatn,iter,
* tfuel0,tcol10,tcol20,pow0,rhoti(1000+1),
* betaeff(1000+1,100)
        common/idata/inn,iout,ikin,itime0,ndg,itimen,igen,iflux,irho
        dimension c(100)
        integer iflag
c
c
c
        read(ikin,802)ndg
        read(ikin,803)(alamda(i),i=1,ndg)
c
c-----input effective beta's at latest time step
c
        read(iflux,940)kmax,ngp
c
        rewind irho
        read(irho,*)iflag

```

```

do 113 i=1,irhonum+1
  read(irho,930)rhoti(i),gen(i),rho(i)
  read(irho,940)(c(in),in=1,ndg)
  read(irho,940)(betaeff(i,j),j=1,ndg)
113 continue
c
c
c-----calculate total beta
c
do 101 i=1,irhonum+1
  do 100 j=1,ndg
    betat(i) = betat(i) + betaeff(i,j)
  100 continue
101 continue
c
802 format(10i5)
803 format(7e11.4)
930 format(3e14.7)
940 format(6e14.7)
970 format(4e11.4)
990 format(1x,'effective betas not found on flux.dat file')
return
end
c
subroutine getpowpk(c,c0)
c-----
c getpow reads initial conditions of time file
c-----
c
common/rdata/rho(1000+1),gen(1000+1),pow,time,
* betat(1000+1),tfuel,
* tcool1,tcool2,tin,rhon,genn,betatn,iter,
* tfuel0,tcol10,tcol20,pow0,rhoti(1000+1),
* betaeff(1000+1,100)
common/flags/irhonum,ipknum
common/idata/inn,iout,ikin,itime0,ndg,itime1,igen,iflux,irho
dimension c0(100),c(100),c2(100)
c
c-----read variables at last time and save on new time file
c
rewind itime0
rewind itimen
c
100 continue
read(itime0,900,end=200)time,pow,tfuel,tcool1,tcool2
write(itimen,900)time,pow,tfuel,tcool1,tcool2
read(itime0,907,end=200)(c2(i),i=1,ndg)
write(itimen,907)(c2(i),i=1,ndg)
go to 100
c
200 continue
c
c-----initial variables
c
if (time.eq.0.0) then
  time = (rhoti(2) - rhoti(1))/irhonum
end if
pow0 = pow
tfuel0 = tfuel
tcol10 = tcool1
tcol20 = tcool2
do 300 i=1,ndg
  c0(i) = c(i)
300 continue
c
901 format(1e11.4)
900 format(7e11.4)
907 format(11x,6e11.4)
return
end
c
c
subroutine gettim(tstop,delt)

```

```

c-----
c   gettim reads tstop,delt, tin of general interface file
c-----
c
c       common/idata/inn,iout,ikin,itime0,ndg,itime0,igen,iflux,irho
c
c-----initial variables
c
c       rewind igen
c
c-----skip section #1
c
c       read(igen,902)isec,nrec
c       do 20 ic=1,nrec
c         read(igen,900)
c       20 continue
c
c-----skip section #2 of general interface file
c
c       read(igen,902)isec,nrec
c       do 30 ic=1,nrec
c         read(igen,902)
c       30 continue
c
c-----skip section 3 of interface file
c
c       read(igen,902)isec,nrec
c       do 50 ic=1,nrec
c         read(igen,902)
c       50 continue
c
c-----read t/h data section #4
c
c       read(igen,902)isec,nrec
c       n=0
c       read(igen,903)tin
c       n=n+1
c       nlft=nrec-n
c       if(nlft.le.0)go to 100
c       do 60 ic=1,nlft
c         read(igen,902)
c       60 continue
c
c-----read time data section #5
c
c       100 continue
c       read(igen,902)isec,nrec
c       read(igen,902)ntime
c       do 200 ic=1,ntime
c         read(igen,903)tstop,delt
c         if(time.lt.tstop)go to 300
c       200 continue
c
c-----end of problem
c
c       write(iout,904)time
c       return
c
c
c       900 format(80a1)
c       902 format(15i5)
c       903 format(7e11.4)
c       904 format(1x,21hend of problem time=,f7.2)
c
c       300 continue
c       return
c       end
c
c       subroutine calconpk(c,c0)
c-----
c       calcon calculates equation constants and initial conditions.
c-----
c
c       common/rdata/rho(1000+1),gen(1000+1),pow,time,

```



```

        sum=0.0
        do 100 i=1,ndg
            sum = sum + alanda(i)*y(i+1)
100    continue
        ydot(1) = (rhon-betatn)*y(1)/genn + sum
c
c-----equations 2-ndg+1: precursors
c
        do 200 i=1,ndg
            ydot(i+1) = betaeff(iter,i)*y(1)/genn - alanda(i)*y(i+1)
200    continue
c
c    write(iout,*)('iter = ',iter,'Time = ',t)
c    write(iout,999)(rhon,genn,betatn,sum)
c    write(iout,998)(alanda(ig),ig=1,ndg)
c    write(iout,998)(betaeff(iter,ig),ig=1,ndg)
998    format(6e17.4)
999    format(4e17.4)
        return
        end
c
        subroutine unloadpk(y,neq,c)
c-----
c    unload takes dependent variables out of y array
c-----
c
        common/idata/inn,iout,ikin,itime0,ndg,itime1,igen,iflux,irho
        common/rdata/rho(1000+1),gen(1000+1),pow,time,
        * betat(1000+1),tfuel,
        * tcool1,tcool2,tin,rhon,genn,betatn,iter,
        * tfuel0,tcol10,tcol20,pow0,rhoti(1000+1),
        * betaeff(1000+1,100)
        common/flags/irhonum,ipknum
        double precision y
        dimension y(101),c(100)
c
c-----y(1)=power/initial power
c
        pow = pow0*y(1)
c
        do 100 i=1,ndg
            c(i) = y(i+1)*pow0
100    continue
c
        return
        end
c
c
        subroutine savpowpk(c)
c-----
c    savpow writes dependent variables to the time file
c-----
c
        common/rdata/rho(1000+1),gen(1000+1),pow,time,
        * betat(1000+1),tfuel,
        * tcool1,tcool2,tin,rhon,genn,betatn,iter,
        * tfuel0,tcol10,tcol20,pow0,rhoti(1000+1),
        * betaeff(1000+1,100)
        common/flags/irhonum,ipknum
        common/idata/inn,iout,ikin,itime0,ndg,itime1,igen,iflux,irho
        dimension c(100)
        data iline/0/
c
c
c-----save variables
c
        write(itimen,900)time,pow,tfuel,tcool1,tcool2
        write(itimen,907)(c(i),i=1,ndg)
900    format(7e11.4)
907    format(11x,6e11.4)
c
c
        iline = iline + 2

```

```

        if(iline .gt. 20000)then
            write(iout,700)
700      format(1x,'exceeded 20000 lines in ptkin')
            stop
        end if
c
        return
        end
c
        subroutine intrhopk(xnew,tk)
            common/rdata/rho(1000+1),gen(1000+1),pow,time,
            * betat(1000+1),tfuel,
            * tcool1,tcool2,tin,rhon,genn,betatn,iter,
            * tfuel0,tcol10,tcol20,pow0,rhoti(1000+1),
            * betaeff(1000+1,100)
            common/flags/irhonum,ipknum
            common/idata/inn,iout,ikin,itime0,ndg,itime1,igen,iflux,irho
            integer imethod
            real x0,x1,x2,xnew,t0,t1,t2,tk,dt1,dt2,dtk,dtk2
c
c imethod = 1 if linear interpolation
c imethod = 2 if quadratic interpolation
c x0,x1,x2 are last three values of parameter being interpolated
c t0,t1,t2 are the associated times
c xnew is the interpolated value
c tk is the time the parameter is being interpolated at
c
            if (iter.eq.1) then
                imethod = 1
                t0 = rhoti(iter)
                t1 = rhoti(iter+1)
                x0 = rho(iter)
                x1 = rho(iter+1)
            else
                imethod = 2
                t0 = rhoti(iter-1)
                t1 = rhoti(iter)
                t2 = rhoti(iter+1)
                x0 = rho(iter-1)
                x1 = rho(iter)
                x2 = rho(iter+1)
            end if
c
            dt1 = t1 - t0
            dt2 = t2 - t1
            dtk = tk - t0
            dtk2 = tk - t1
            if(imethod.eq.1) then
                xnew = x0 + ((x1 - x0)*dtk)/(dt1)
            end if
            if(imethod.eq.2) then
                xnew = x0 + ((x1 - x0)*(dtk))/(dt1) + ((dtk)*(dtk2))*
            * (((x2 - x1)/dt2) - ((x1 - x0)/dt1))/(dt2 + dt1)
            end if
c
            write(6,*) (' xnew = ',xnew,' x0 = ',x0,
c * ' x1 = ',x1,' x2 = ',x2)
c
            write(6,*) (' tk = ',tk,' t0 = ',t0,' t1 = ',t1,
c * ' t2 = ',t2)
            return
            end
c
        subroutine intgenpk(xnew,tk)
            common/rdata/rho(1000+1),gen(1000+1),pow,time,
            * betat(1000+1),tfuel,
            * tcool1,tcool2,tin,rhon,genn,betatn,iter,
            * tfuel0,tcol10,tcol20,pow0,rhoti(1000+1),
            * betaeff(1000+1,100)
            common/flags/irhonum,ipknum
            common/idata/inn,iout,ikin,itime0,ndg,itime1,igen,iflux,irho
            integer imethod
            real x0,x1,x2,xnew,t0,t1,t2,tk,dt1,dt2,dtk,dtk2
c
c imethod = 1 if linear interpolation

```

```

c imethod = 2 if quadratic interpolation
c x0,x1,x2 are last three values of parameter being interpolated
c t0,t1,t2 are the associated times
c xnew is the interpolated value
c tk is the time the parameter is being interpolated at
c
  if (iter.eq.1) then
    imethod = 1
    t0 = rhoti(iter)
    t1 = rhoti(iter+1)
    x0 = gen(iter)
    x1 = gen(iter+1)
  else
    imethod = 2
    t0 = rhoti(iter-1)
    t1 = rhoti(iter)
    t2 = rhoti(iter+1)
    x0 = gen(iter-1)
    x1 = gen(iter)
    x2 = gen(iter+1)
  end if
c
  dt1 = t1 - t0
  dt2 = t2 - t1
  dtk = tk - t0
  dtk2 = tk - t1
  if(imethod.eq.1) then
    xnew = x0 + ((x1 - x0)*dtk)/(dt1)
  end if
  if(imethod.eq.2) then
    xnew = x0 + ((x1 - x0)*(dtk))/(dt1) + ((dtk)*(dtk2))*
* (((x2 - x1)/dt2) - ((x1 - x0)/dt1))/(dt2 + dt1)
  end if
c  write(6,*) (' xnew = ',xnew,' x0 = ',x0,
c * ' x1 = ',x1,' x2 = ',x2)
c  write(6,*) (' tk = ',tk,' t0 = ',t0,' t1 = ',t1,
c * ' t2 = ',t2)
  return
end
*****
*                               *
*                               SUBROUTINE NORM                               *
*                               *
*****
subroutine norm
c-----
c
c  merge & reformat flux output of keno into flux shape
c  interface file.
c-----
  dimension flux(300,300)
  dimension beta(20)
  data lim/20/
  data ifluxi/48/
  data ifluxo/55/
  data inew/57/
  data iout/56/
  data ikin/49/
c
c
c-----open files
c
  open(56,file='norm.out',status='unknown',form='formatted')
  open(49,file='kinetics.dat',status='old',form='formatted')
  open(48,file='ft48f001',status='old',form='unformatted')
  open(55,file='flux.dat',status='old',form='formatted')
  open(57,file='fluxnew.dat',status='new',form='formatted')
c
  rewind 56
  rewind 49
  rewind 48
  rewind 57

```



```

rewind 55
c
c
c-----input no. of delayed neutron groups
read(ikin,940)ndg
if (ndg .gt. lim)then
write(iout,980)ndg,lim
stop
end if
c
read(iflux1)kmax,ngp
read(iflux1)time2
c
if(kmax.gt.300)then
write(iout,900)kmax
stop
end if
c
if(ngp.gt.300)then
write(iout,910)ngp
stop
end if
c
read(ifluxo,940)kmaxo,ngpo
c
if(kmax.ne.kmaxo)then
write(iout,950)kmax,kmaxo
stop
end if
c
if(ngp.ne.ngpo)then
write(iout,960)ngp,ngpo
stop
end if
c
c-----transfer data from old flux.dat to new flux.dat.
c first const on file will be the constant value of the integral.
c
write(inew,940)kmax,ngp
40 continue
read(ifluxo,970,end=50)time,rho,xgen,const
c
c-----replace time step (iteration), do not append time step
c
iyes = 1
if(time2 .eq. time)then
iyes = 0
end if
c
if(iyes .eq. 1)then
write(inew,970)time,rho,xgen,const
end if
read(ifluxo,930,end=50)((flux(ig,k),ig=1,ngp),k=1,kmax)
if(iyes .eq. 1)then
write(inew,930)((flux(ig,k),ig=1,ngp),k=1,kmax)
end if
read(ifluxo,930,end=50)(beta(j),j=1,ndg)
if(iyes .eq. 1)then
write(inew,930)(beta(j),j=1,ndg)
end if
go to 40
50 continue
c
100 continue
c
c-----input fluxes
c
read(iflux1)ig,ll,lu
if(ig .eq. -1)then
go to 200
end if
read(iflux1)(flux(ig,k),k=ll,lu)
go to 100

```

```

c
200 continue
c
c-----output latest data
c
      read(ifluxi)rho,xgen,const
      write(inew,970)time2,rho,xgen,const
      write(inew,930)((flux(ig,k),ig=1,ngp),k=1,kmax)
      read(ifluxi)(beta(j),j=1,ndg)
      write(inew,930)(beta(j),j=1,ndg)
c
      write(iout,1000)time2
1000 format(1x,'flux.dat file updated by norm, time=',e11.4)
      write(iout,1100)rho,xgen
1100 format(1x,'reactivity=',e11.4,/,1x,'generation time=',e11.4)
      write(iout,1200)const
1200 format(1x,'constraint constant=',e11.4)
c
      close (56)
      close (49)
      close (48)
      close (57)
      close (55)
c
      return
900 format(1x,'kmax exceeds 300, kmax=',i7)
910 format(1x,'ngp exceeds 300, ngp=',i7)
920 format(1x,'time=',e11.4)
930 format(6e11.4)
940 format(2i5)
950 format(1x,'kmax not consistent in interface files in norm',2i5)
960 format(1x,'ngp not consistent in interface files in norm',2i5)
970 format(4e11.4)
980 format(1x,'ndg exceeds lim, ndg,lim=',2i5)
      end
*****
*
*              SUBROUTINE CDELAY
*
*****
      subroutine cdelay
c-----
c
c      calculate delayed neutron shape
c
c      nntmef = no. of time steps on flux.dat
c      nntmes = no. of time steps on nusigf.dat
c      nnpow = no. of time steps on timen.dat
c      ndglim = max no of delayed neutron groups
c      ntimef = max no of flux shape calcs
c      ntimes = max no of times on nusigf.dat file
c      npow = max no of times on timen.dat file
c      ntegr = max no of integrand values
c-----
c
      common/unitscd/iout,ikin,isigf,itime,iflux,idelay
      common/paramcd/kmax,ngp,ntimef,ntimes,npow,ndglim,ntegr,
* nntmef,nntmes,nnpow,ndg,nmat
      dimension d(100000)
      dimension beta(20),alamda(20)
      data limmem/100000/
c
      ndglim = 20
      ntimef = 40
      ntimes = 20
      npow = 10000
      ntegr = 3000
c
      call ofilecd
c
      read(iflux,940)kmax,ngp
c
      read(isigf,940)kmax0,ngp0,nmat

```

```

        if(kmax0 .ne. kmax)then
            write(iout,950)kmax,kmax0
            stop
        end if
        if(ngp0 .ne. ngp)then
            write(iout,960)ngp,ngp0
            stop
        end if
c
c
c-----generate array pointers
ngp1 = ngp + 1
lflux = 1
lfluxt = lflux + kmax*ngp*ntimef
lsigf = lfluxt + ntimef
lsigft = lsigf + nmat*ngp*ntimes
lncor = lsigft + ntimes
lpow = lncor + kmax
lpowt = lpow + npow
lchi = lpowt + npow
lntegr = lchi + ngp*ndglim
ltime = lntegr + ntegr
lqd = ltime + ntegr
lqdk = lqd + kmax*ngp
lqdkig = lqdk + kmax
lvol = lqdkig + kmax*ngp
lvel = lvol + kmax
lf = lvel + ngp1
lfk = lf + kmax*ngp
lfkig = lfk + kmax
iend = lfkig + kmax*ngp
if(iend .gt. limmem)then
    write(iout,900)limmem,iend
    stop
end if
c
    call master1(d(lflux),d(lfluxt),d(lsigf),d(lpow),d(lchi),
* d(lntegr),d(ltime),d(lqd),d(lsigft),d(lpowt),beta,alamda,
* d(lncor),d(lqdk),d(lqdkig),d(lvol),d(lvel),d(lf),
* d(lfk),d(lfkig),ngp1)
c
    close (iout)
    close (ikin)
    close (isigf)
    close (itime)
    close (iflux)
    close (idelay)
c
    return
900 format(1x,'insufficient memory',2i10)
940 format(3i5)
950 format(1x,'kmax not consistent in interface files in main',2i5)
960 format(1x,'ngp not consistent in interface files in main',2i5)
end
subroutine master1(flux,fluxti,sigf,pow,chi,xntegr,time,qd,
* sigfti,powti,beta,alamda,ncor,qdk,
* qdkig,vol,vel,f, fk, fkig,ngp1)
c-----
c
c    master1 is the controlling subroutine
c-----
c
common/unitscd/iout,ikin,isigf,itime,iflux,idelay
common/paramcd/kmax,ngp,ntimef,ntimes,npow,ndglim,ntegr,
* nntimef,nntmes,nnpow,ndg,nmat
dimension flux(ngp,kmax,ntimef),sigf(ngp,nmat,ntimes)
dimension pow(npow),xntegr(ntege),time(ntege),qd(ngp,kmax)
dimension beta(ndglim),alamda(ndglim),chi(ngp,ndglim)
dimension fluxti(ntimef),sigfti(ntimes),powti(npow),ncor(kmax)
dimension qdk(kmax),qdkig(ngp,kmax),vol(kmax),vel(ngp1)
dimension f(ngp,kmax),fk(kmax),fkig(ngp,kmax)
logical istop

```

```

      data delmin/.001/
c
c-----input no. of delayed neutron groups
      read(ikin,940)ndg
      if (ndg .gt. ndglim)then
        write(iout,980)ndg,ndglim
        stop
      end if
      read(ikin,803)(alamda(i),i=1,ndg)
      read(ikin,803)(beta(i),i=1,ndg)
c
c-----input flux shapes
      call nflux(flux,fluxti)
c
c-----input nusigf & chi's & velocities & volumes
      call nsigf(sigf,chi,sigfti,ncor,vol,vel,ngp1)
c
c-----input powers
c      xtime = last time on timen.dat file and will be time integrated
c      to
c      power = last amplitude on timen.dat file
c      call inpow(pow,xtime,powti,power)
c
c
      do 55 k=1,kmax
        qdk(k) = 0.0
        fk(k) = 0.0
        do 50 ig=1,ngp
          qd(ig,k) = 0.0
          qdkig(ig,k) = 0.0
          f(ig,k) = 0.0
          fkig(ig,k) = 0.0
50      continue
55      continue
c
      do 95 k=1,kmax
        m = ncor(k)
        do 91 j=1,ndg
c
c-----steady-state fissions (assumes first time step on timen.dat,
c      flux.dat, nusigf.dat files is steady-state.)
c
          ssfiss = 0.0
          do 80 ig=1,ngp
            ssfiss = ssfiss + sigf(ig,m,1)*pow(1)*flux(ig,k,1)
80          continue
c
          do 90 ignew=1,ngp
c-----following assumes all chi's are the same for
c      all j's
            qd(ignew,k) = qd(ignew,k) + ssfiss*chi(ignew,1)*
            *      alamda(j)*beta(j)*exp(-alamda(j)*xtime)
90          continue
c
91          continue
95          continue
c
c
c-----integrate
      do 500 j=1,ndg
        deltat = delmin
        t = xtime
        i = 1
        time(i) = t
        xntegr(i) = 1.0
        istop = .false.
c
c
100      continue
        t = t - deltat
c
        if(t .le. 0.0)then
          t = 0.0

```

```

        istop = .true.
    end if
c
    i = i + 1
c
    if(i .gt. ntegr)then
        write(iout,990)ntegr
        stop
    end if
c
    xntegr(i) = exp(-alamda(j)*(xtime-t))
c
    trial = abs(xntegr(i)-xntegr(i-1))
    if(trial .gt. .005)then
        deltat = deltat/2.0
        i = i - 1
    else if(trial .lt. .001)then
        if(.not. istop)then
            deltat = deltat*2.0
            i = i - 1
        endif
    else
        time(i) = t
    end if
c
    if(istop)then
        if(i .eq. 1)then
            i = 2
            time(i) = t
        end if
        go to 200
    else
        go to 100
    end if
200    continue
c
c-----add times from timen.dat file
    ii = i + nnpow
c
    if(ii .gt. ntegr)then
        write(iout,990)ntegr
        stop
    end if
c
    call addmor(time,i,powti,xntegr,alamda(j),xtime)
c
c
c-----finished with time mesh for group j
c    now fold other terms of the integrand in
c
    do 450 k=1,kmax
        sum = 0.0
        do 400 ig=1,ngp
c
            do 300 ii=1,i
c
c-----interpolate values
c
                call intflx(flux,time(ii),xflux,fluxti,ig,k)
c
                call intsig(sigf,time(ii),xsig,sigfti,ig,k,ncor)
c
                call intpow(pow,time(ii),xpow,powti)
c
                fact = xflux*xsig*xpow*alamda(j)*beta(j)
                xntegr(ii) = fact*exp(-alamda(j)*(xtime-time(ii)))
300    continue
c
            do 310 ii=2,i
c
c-----integrate using trapezoid rule
c
c

```

```

                del = abs(time(ii)-time(ii-1))/2.0
                sum = sum + (xntegr(ii) + xntegr(ii-1))*del
310          continue
400          continue
c
          do 410 ignew=1,ngp
c-----following assumes all chi's are the same for
c          all j's
                qd(ignew,k) = qd(ignew,k) + sum*chi(ignew,1)
410          continue
450          continue
500          continue
c
c
c-----calculate (1/vdelt)*flux(t-delt) part of shape derivative.
c
          call fluxsh(flux,fluxti,f,vel,ngp1,xtime)
c
c
c-----d = ratio of delayed & flux shift source neutrons to total source
c-----fs = ratio of flux shift source neutrons to delayed + flux shift
c          source neutrons
c
          fs = 0.0
          d = 0.0
          do 520 k=1,kmax
                sumf = 0.0
                sum = 0.0
                do 510 ig=1,ngp
                        sumf = sumf + f(ig,k)
                        sum = sum + qd(ig,k)
510          continue
                fs = fs + sumf*vol(k)
                d = d + sum*vol(k)
520          continue
c
c
c-----calculate pdf's for spatial & energy distributions of fixed
c          source neutrons
c
          do 540 k=1,kmax
                sumf = 0.0
                sum = 0.0
                do 530 ig=1,ngp
                        sumf = sumf + f(ig,k)
                        sum = sum + qd(ig,k)
530          continue
                do 535 ig=1,ngp
                        if(sum .gt. 0.0)then
                                qdkig(ig,k) = qd(ig,k)/sum
                        end if
                        if(sumf .gt. 0.0)then
                                fkig(ig,k) = f(ig,k)/sumf
                        end if
535          continue
                if(d .gt. 0.0)then
                        qdk(k) = sum*vol(k)/d
                end if
                if(fs .gt. 0.0)then
                        fk(k) = sumf*vol(k)/fs
                end if
540          continue
                d = d/pow(nnpow)
c
c
c-----Flux used to calculate prompt fission neutrons is that at the
c          latest time on flux.dat file.
c
          betat = 0.0
          do 550 j=1,ndg
                betat = betat + beta(j)
550          continue
c

```

```

xtime2 = fluxti(nntmef)
p = 0.0
c
do 700 k=1,kmax
  sum = 0.0
  do 600 ig=1,ngp
    call intsig(sigf,xtime2,xsig,sigfti,ig,k,ncor)
    sum = sum + chi(ig,1)*(1.0-betat)*xsig*flux(ig,k,nntmef)
600  continue
    p = p + sum*vol(k)
700 continue
c
r1 = (d + fs)/(d + fs + p)
r2 = fs/(d + fs)
r3 = d/p
write(idelay,940)kmax,ngp
write(idelay,930)r1,r2,r3,fluxti(nntmef)
write(idelay,930)(qdk(k),k=1,kmax)
write(idelay,930)((qdkig(ig,k),ig=1,ngp),k=1,kmax)
write(idelay,930)(fk(k),k=1,kmax)
write(idelay,930)((fkig(ig,k),ig=1,ngp),k=1,kmax)
c
write(iout,1000)xtime
write(iout,1100)r1
write(iout,1200)r2
write(iout,1300)r3
c
803 format(7e11.4)
930 format(6e11.4)
940 format(2i5)
980 format(1x,'ndg exceeds lim, ndg,lim=',2i5)
990 format(1x,'number of intrgrand values exceeds limit',i6)
1000 format(1x,'cdelay calc. ended at time=',e11.4)
1100 format(1x,'ratio of fixed source to total source=',e11.4)
1200 format(1x,'ratio of flux shift to total fixed source=',e11.4)
1300 format(1x,'ratio of delayed n. source to prompt source=',e11.4)
return
end
subroutine ofilecd
common/unitscd/iout,ikin,isigf,itime,iflux,idelay
c
iout = 59
ikin = 49
isigf = 54
itime = 46
iflux = 55
idelay = 47
c
c
c-----open files
c
open(59,file='cdelay.out',status='new',form='formatted')
open(49,file='kinetics.dat',status='old',form='formatted')
open(54,file='nusigf.dat',status='old',form='formatted')
open(46,file='timen.dat',status='old',form='formatted')
open(55,file='flux.dat',status='old',form='formatted')
open(47,file='delay.dat',status='unknown',form='formatted')
rewind 59
rewind 49
rewind 54
rewind 46
rewind 55
rewind 47
c
return
end
c
subroutine nflux(flux,fluxti)
c-----
c
c input flux shapes
c-----

```

```

c
common/unitscd/iout,ikin,isigf,itime,iflux,idelay
common/paramcd/kmax,ngp,ntimef,ntimes,npow,ndglim,nTEGR,
* nntmef,nntmes,nnpow,ndg,nmat
dimension flux(ngp,kmax,ntimef),fluxti(ntimef)
c
c
i = 0
40 continue
c
ip1 = i + 1
if(ip1 .gt. ntimef)then
write(iout,910)ntimef
stop
end if
c
read(iflux,970,end=50)fluxti(ip1),rho,gen,xdum
read(iflux,930,end=50)((flux(ig,k,ip1),ig=1,ngp),k=1,kmax)
read(iflux,930,end=50)(xdum,j=1,ndg)
i = i + 1
go to 40
50 continue
c
nntmef = i
if(nntmef .le. 0) then
write(iout,990)
stop
end if
c
c
if(fluxti(1) .ne. 0.0) then
write(iout,980)
stop
end if
c
c
return
910 format(1x,'more times on flux.dat than allowed',i11)
930 format(6e11.4)
970 format(4e11.4)
980 format(1x,'first time on flux.dat file must be 0')
990 format(1x,'no data on flux.dat')
end
c
subroutine nsigf(sigf,chi,sigfti,ncor,vol,vel,ngp1)
c-----
c
c input nusigf, chi, volumes, and velocities
c
c-----
c
common/unitscd/iout,ikin,isigf,itime,iflux,idelay
common/paramcd/kmax,ngp,ntimef,ntimes,npow,ndglim,nTEGR,
* nntmef,nntmes,nnpow,ndg,nmat
dimension sigf(ngp,nmat,ntimes),sigfti(ntimes),chi(ngp,ndglim)
dimension ncor(kmax),vel(ngp1),vol(kmax)
c
c-----following assumes all chi's are the same for
c all j's
c read(isigf,930)(vol(k),k=1,kmax)
c read(isigf,930)(chi(ig,1),ig=1,ngp)
c read(isigf,930)(vel(ig),ig=1,ngp1)
c read(isigf,950)(ncor(k),k=1,kmax)
c
c
i = 0
40 continue
c
i = i + 1
if(i .gt. ntimes)then
write(iout,910)ntimes
stop
end if
c

```



```

        read(isigf,930)sigfti(i),
*          ((sigf(ig,m,i),ig=1,ngp),m=1,nmat)
        if(sigfti(i).lt. 0.0)then
            i = i - 1
            go to 50
        end if
        go to 40
50 continue
c
        nntmes = i
        if(nntmes .le. 0) then
            write(iout,990)
            stop
        end if
c
c-----convert energies to velocities
c
        ig = 0
80 continue
        ig = ig + 1
        eb = sqrt(vel(ig)*vel(ig+1))
        vel(ig) = 1.3859e+6*sqrt(eb)
        if(ig .lt. ngp)then
            go to 80
        end if
c
        return
910 format(1x,'more times on nusigf.dat than allowed',i11)
930 format(6e11.4)
940 format(2i5)
950 format(12i5)
990 format(1x,'no data on nusigf.dat')
end
c
        subroutine inpow(pow,xtime,powti,power)
        common/unitscd/iout,ikin,isigf,itime,iflux,idelay
        common/paramcd/kmax,ngp,ntimef,ntimes,npow,ndglim,nTEGR,
*          nntmef,nntmes,nnpow,ndg,nmat
        dimension pow(npow),powti(npow)
c
        i = 0
100 continue
c
        ip1 = i + 1
        if(ip1 .gt. npow)then
            write(iout,910)npow
            stop
        end if
c
        read(itime,900,end=200)powti(ip1),pow(ip1),tfuel,
*          tcool1,tcool2
        read(itime,907,end=200)(xdum,j=1,ndg)
        i = ip1
        go to 100
c
200 continue
c
        nnpow = i
        if(nnpow .le. 0) then
            write(iout,990)
            stop
        end if
c
        xtime = powti(nnpow)
        power = pow(nnpow)
c
c
900 format(7e11.4)
907 format(11x,6e11.4)
910 format(1x,'more times on timen.dat than allowed',i11)
990 format(1x,'no data on timen.dat')
        return
        end

```

```

subroutine addmor(time,i,powti,xntegr,alamda,xtime)
c-----
c
c   add times from timen.dat file
c
c-----
c
common/paramcd/kmax,ngp,ntimef,ntimes,npow,ndglim,ntegr,
* nntmef,nntmes,nnpow,ndg,nmat
dimension xntegr(ntegr),time(ntegr)
dimension powti(npow)
logical isort
c
if(nnpow .le. 1)then
  i = i + 1
  time(i) = powti(1)
else
  do 100 j=1,nnpow
    time(i+j) = powti(j)
100  continue
  i = i + nnpow
end if
c
c-----sort times
c
150 continue
isort = .false.
do 200 j=2,i
  if(time(j) .lt. time(j-1))then
    a = time(j)
    time(j) = time(j-1)
    time(j-1) = a
    isort = .true.
  end if
200 continue
c
if(isort)then
  go to 150
end if
c
c-----times have been sorted
c
do 300 ii=1,i
  xntegr(ii) = exp(-alamda*(xtime-time(ii)))
300 continue
c
return
end
subroutine intflx(flux,t,x,fluxti,ig,k)
c-----
c
c   interpolate flux values
c
c-----
c
common/paramcd/kmax,ngp,ntimef,ntimes,npow,ndglim,ntegr,
* nntmef,nntmes,nnpow,ndg,nmat
dimension flux(ngp,kmax,ntimef)
dimension fluxti(ntimef)
c
if(nntmef .le. 1)then
  x = flux(ig,k,1)
else
  do 100 i=1,nntmef
    if(t .le. fluxti(i))then
      go to 200
    end if
100  continue
c
c-----time is > than any time on flux file. set equal to
c   flux at last flux file time step
c
x = flux(ig,k,nntmef)

```

```

        go to 300
c
200    continue
      if(i .le. 1)then
        x = flux(ig,k,1)
      else
        *   x = flux(ig,k,i-1) + (flux(ig,k,i) - flux(ig,k,i-1))*
          (t - fluxti(i-1))/(fluxti(i) - fluxti(i-1))
        end if
300    continue
c
      end if
      return
      end
      subroutine intsig(sigf,t,x,sigfti,ig,k,ncor)
c-----
c
c   interpolate nusig values
c-----
c
      common/paramcd/kmax,ngp,ntimef,ntimes,npow,ndglim,ntegr,
      * nntmef,nntmes,nnpow,ndg,rmat
      dimension sigf(ngp,rmat,ntimes)
      dimension sigfti(ntimes),ncor(kmax)
c
      m = ncor(k)
      if(nntmes .le. 1)then
        x = sigf(ig,m,1)
      else
        do 100 i=1,nntmes
          if(t .le. sigfti(i))then
            go to 200
          end if
100    continue
c
c-----time is > than any time on sigf file. set equal to
c       sigf at last sigf file time step
c
      x = sigf(ig,m,nntmes)
      go to 300
c
200    continue
      if(i .le. 1)then
        x = sigf(ig,m,1)
      else
        *   x = sigf(ig,m,i-1) + (sigf(ig,m,i) - sigf(ig,m,i-1))*
          (t - sigfti(i-1))/(sigfti(i) - sigfti(i-1))
        end if
300    continue
c
      end if
      return
      end
      subroutine intpow(pow,t,x,powti)
c-----
c
c   interpolate power values
c-----
c
      common/paramcd/kmax,ngp,ntimef,ntimes,npow,ndglim,ntegr,
      * nntmef,nntmes,nnpow,ndg,rmat
      dimension pow(npow)
      dimension powti(npow)
c
      if(nnpow .le. 1)then
        x = pow(1)
      else
        do 100 i=1,nnpow
          if(t .le. powti(i))then
            go to 200
          end if

```

```

100    continue
c
c-----time is > than any time on time file. set equal to
c      pow at last time file time step
c
c      x = pow(nnpow)
c      go to 300
c
200    continue
c      if(i .le. 1)then
c        x = pow(1)
c      else
c        x = pow(i-1) + (pow(i) - pow(i-1))*
*      (t - powti(i-1))/(powti(i) - powti(i-1))
c      end if
300    continue
c
c      end if
c      return
c      end
c      subroutine fluxsh(flux,fluxti,f,vel,ngp1,xtime)
c-----
c
c      calculate (1/(delt*vel)) * flux(t-delt)
c      t = xtime = last time on timen.dat file
c      t - delt = last time on flux.dat file
c-----
c
c      common/paramcd/kmax,ngp,ntimef,ntimes,npow,ndglim,ntegr,
*      nntmef,nntmes,nnpow,ndg,nmat
c      common/unitscd/iout,ikin,isigf,itime,iflux,idelay
c      dimension flux(ngp,kmax,ntimef)
c      dimension fluxti(ntimef)
c      dimension f(ngp,kmax),vel(ngp1)
c
c
c      delt = xtime - fluxti(nntmef)
c      write(6,*)('delt =',delt)
c      if(delt .le. 0.0)then
c        write(iout,950)
c        stop
c      end if
c
c      do 500 k=1,kmax
c        do 400 ig=1,ngp
c          f(ig,k) = 0.0
c          f(ig,k) = (1.0/vel(ig))*flux(ig,k,nntmef)/delt
c
c      400    continue
c      500    continue
c
c
c      950 format(1x,'delt le 0 in fluxsh')
c      return
c      end
*****
*
*          SUBROUTINE POWER
*
*****
subroutine power
c-----
c
c      calculate power from amplitude and shape functions
c      also determine normalized flux distribution
c
c      nntmef = no. of time steps on flux.dat
c      nntmes = no. of time steps on nusigf.dat
c      nnamp = no. of time steps on timen.dat
c      ntimef = max no of flux shape calcs
c      ntimes = max no of times on nusigf.dat file
c      namp = max no of times on timen.dat file

```

```

c-----
c
  common/units2/inn,iout,isingf,itime,iflux,ikin,ifluxo
  common/param2/kmax,ngp,ntimef,ntimes,namp,
  * nntimef,nntmes,nnamp,nmat,ndg
  dimension d(50000)
  data limmem/50000/
c
  ntimef = 40
  ntimes = 20
  namp = 10000
c
  call ofiles2
c
  read(iflux,940)kmax,ngp
c
  read(isingf,940)kmax0,ngp0,nmat
  if(kmax0 .ne. kmax)then
    write(iout,950)kmax,kmax0
    stop
  end if
  if(ngp0 .ne. ngp)then
    write(iout,960)ngp,ngp0
    stop
  end if
c
c
c-----generate array pointers
  ngp1 = ngp + 1
  lflux = 1
  lfluxt = lflux + kmax*ngp*ntimef
  lsigf = lfluxt + ntimef
  lsigft = lsigf + nmat*ngp*ntimes
  lncor = lsigft + ntimes
  lamp = lncor + kmax
  lamp1 = lamp + namp
  lvol = lamp1 + namp
  lcon = lvol + kmax
  iend = lcon + ntimef
  if(iend .gt.limmem)then
    write(iout,900)limmem,iend
    stop
  end if
c
  call master2(d(lflux),d(lfluxt),d(lsigf),d(lamp),
  * d(lsigft),d(lamp1),d(lncor),d(lvol),d(lcon),ngp1)
c
  close (inn)
  close (iout)
  close (isingf)
  close (itime)
  close (iflux)
  close (ikin)
  close (ifluxo)
c
  return
900 format(1x,'insufficient memory',2i10)
940 format(3i5)
950 format(1x,'kmax not consistent in interface files in main',2i5)
960 format(1x,'ngp not consistent in interface files in main',2i5)
  end
  subroutine master2(flux,fluxti,sigf,amp,
  * sigfti,ampti,ncor,vol,con,ngp1)
c-----
c
c  master2 is the controlling subroutine
c
c-----
c
  common/units2/inn,iout,isingf,itime,iflux,ikin,ifluxo
  common/param2/kmax,ngp,ntimef,ntimes,namp,
  * nntimef,nntmes,nnamp,nmat,ndg
  dimension flux(ngp,kmax,ntimef),sigf(ngp,nmat,ntimes)

```

```

        dimension amp(namp)
        dimension fluxti(ntimef),sigfti(ntimes),ampti(namp),ncor(kmax)
        dimension vol(kmax),con(ntimef)
c
c-----input flux shapes
        call nflux2(flux,fluxti,con)
c
c-----input sigf & volumes
        call nsigf2(sigf,sigfti,ncor,vol,ngp1)
c
c-----input amplitudes
        call inamp(amp,ampti)
c
c-----determine power normalization factor
c      defaults to 1.0 if the file power.in does not exist.
c
        powini = 1.0
        read(inn,803,end=50)powini
50    continue
c
        p = 0.0
        do 200 k=1,kmax
            sum = 0.0
            do 100 ig=1,ngp
                m = ncor(k)
                sum = sum + sigf(ig,m,1)*flux(ig,k,1)
100    continue
            p = p + sum*vol(k)
200    continue
        p = p*amp(1)
        xnormp = powini/p
c
c-----determine powers
c
        do 500 i=1,nnamp
            p = 0.0
            do 400 k=1,kmax
                sum = 0.0
                do 300 ig=1,ngp
c
c-----interpolate values
c
                call intflx2(flux,ampti(i),xflux,fluxti,ig,k,con,xc)
                call intsig2(sigf,ampti(i),xsig,sigfti,ig,k,ncor)
                xnormc = con(1)/xc
c
                sum = sum + xsig*xflux
300    continue
            p = p + sum*vol(k)
400    continue
            pow = p*amp(i)*xnormc*xnormp
            write(iout,803)ampti(i),pow,amp(i)
500    continue
c
c-----determine normalized flux distribution
c
        do 800 i=1,nntmef
            call intamp(amp,fluxti(i),x,ampti)
            do 700 k=1,kmax
                do 600 ig=1,ngp
                    flux(ig,k,i) = flux(ig,k,i)*x*xnormp*con(1)/con(i)
600    continue
700    continue
800    continue
c
c-----output flux distribution
        call oflux(flux,fluxti)
c
803    format(3e11.4)
        return
        end
        subroutine ofiles2
        common/units2/inn,iout,isigf,itime,iflux,ikin,ifluxo

```

```

c
inn = 63
iout = 60
isigf = 54
itime = 46
iflux = 55
ikin = 49
ifluxo = 62

c
c-----open files
c
open(63,file='power.in',status='unknown',form='formatted')
open(60,file='power.out',status='new',form='formatted')
open(54,file='nusigf.dat',status='old',form='formatted')
open(46,file='timen.dat',status='old',form='formatted')
open(55,file='flux.dat',status='old',form='formatted')
open(49,file='kinetics.dat',status='old',form='formatted')
open(62,file='flux.out',status='new',form='formatted')

c
rewind 63
rewind 60
rewind 54
rewind 46
rewind 55
rewind 49
rewind 62

c
return
end

c
subroutine nflux2(flux,fluxti,con)
c-----
c
c   input flux shapes
c-----
c
common/units2/inn,iout,isigf,itime,iflux,ikin,ifluxo
common/param2/kmax,ngp,ntimef,ntimes,namp,
* nntmef,nntmes,nnamp,nmat,ndg
dimension flux(ngp,kmax,ntimef),fluxti(ntimef)
dimension con(ntimef)

c
c-----input no. of delayed neutron groups
read(ikin,940)ndg

c
i = 0
40 continue

c
ip1 = i + 1
if(ip1 .gt. ntimef)then
write(iout,910)ntimef
stop
end if

c
read(iflux,970,end=50)fluxti(ip1),rho,gen,con(ip1)
read(iflux,930,end=50)((flux(ig,k,ip1),ig=1,ngp),k=1,kmax)
read(iflux,930,end=50)(xdum,j=1,ndg)
i = i + 1
go to 40

50 continue

c
nntmef = i
if(nntmef .le. 0) then
write(iout,990)
stop
end if

c
return
910 format(1x,'more times on flux.dat than allowed',i11)
930 format(6e11.4)
940 format(i5)
970 format(4e11.4)

```

```

990 format(1x,'no data on flux.dat')
end
c
c      subroutine nsigf2(sigf,sigfti,ncor,vol,ngp1)
c-----
c
c      input sigf, volumes
c-----
c
c      common/units2/inn,iout,isigf,itime,iflux,ikin,ifluxo
common/param2/kmax,ngp,ntimef,ntimes,namp,
* nntmef,nntmes,nnamp,nmat,ndg
dimension sigf(ngp,nmat,ntimes),sigfti(ntimes)
dimension ncor(kmax),vol(kmax)
c
c      read(isigf,930)(vol(k),k=1,kmax)
read(isigf,930)(xdum,ig=1,ngp)
read(isigf,930)(xdum,ig=1,ngp1)
read(isigf,950)(ncor(k),k=1,kmax)
c
c      i2 = 0
30 continue
c
c      i = 0
40 continue
c
c      i = i + 1
if(i .gt. ntimes)then
write(iout,910)ntimes
stop
end if
c
c      read(isigf,930)sigfti(i),
* ((sigf(ig,m,i),ig=1,ngp),m=1,nmat)
if(sigfti(i) .lt. 0.0)then
i = i - 1
go to 50
end if
go to 40
50 continue
c
c-----just read nusigf, go back for sigf
c
c      if(i2 .eq. 0)then
i2 = 1
go to 30
end if
c
c      nntmes = i
if(nntmes .le. 0) then
write(iout,990)
stop
end if
c
c      return
910 format(1x,'more times on nusigf.dat than allowed',i11)
930 format(6e11.4)
940 format(2i5)
950 format(12i5)
990 format(1x,'no data on nusigf.dat')
end
c
c      subroutine inamp(amp,ampti)
c-----
c
c      input amplitude function
c-----
c
c      common/units2/inn,iout,isigf,itime,iflux,ikin,ifluxo
common/param2/kmax,ngp,ntimef,ntimes,namp,
* nntmef,nntmes,nnamp,nmat,ndg

```



```

        dimension amp(namp), ampti(namp)
c
    i = 0
100 continue
c
        ip1 = i + 1
        if(ip1 .gt. namp)then
            write(iout,910)namp
            stop
        end if
c
        read(itime,900,end=200)ampti(ip1),amp(ip1),tfuel,
*         tcool1,tcool2
        read(itime,907,end=200)(xdum,j=1,ndg)
        i = ip1
        go to 100
c
200 continue
c
        nnamp = i
        if(nnamp .le. 0) then
            write(iout,990)
            stop
        end if
c
c
900 format(7e11.4)
907 format(11x,6e11.4)
910 format(1x,'more times on timen.dat than allowed',i11)
990 format(1x,'no data on timen.dat')
        return
        end
        subroutine intflx2(flux,t,x,fluxti,ig,k,con,xc)
c-----
c
c     interpolate flux values
c-----
c
c
        common/param2/kmax,ngp,ntimef,ntimes,namp,
*         nntmef,nntmes,nnamp,nmat,ndg
        dimension flux(ngp,kmax,ntimef)
        dimension fluxti(ntimef),con(ntimef)
c
        if(nntmef .le. 1)then
            x = flux(ig,k,1)
            xc = con(1)
        else
            do 100 i=1,nntmef
                if(t .le. fluxti(i))then
                    go to 200
                end if
100         continue
c
c-----time is > than any time on flux file. set equal to
c         flux at last flux file time step
c
        x = flux(ig,k,nntmef)
        xc = con(nntmef)
        go to 300
c
200         continue
        if(i .le. 1)then
            x = flux(ig,k,1)
            xc = con(1)
        else
            x = flux(ig,k,i-1) + (flux(ig,k,i) - flux(ig,k,i-1))*
*             (t - fluxti(i-1))/(fluxti(i) - fluxti(i-1))
            xc = con(i-1) + (con(i) - con(i-1))*
*             (t - fluxti(i-1))/(fluxti(i) - fluxti(i-1))
        end if
300         continue
c

```

```

        end if
        return
    end
    subroutine intsig2(sigf,t,x,sigfti,ig,k,ncor)
c-----
c
c   interpolate nusigf values
c-----
c
    common/param2/kmax,ngp,ntimef,ntimes,namp,
* nntmef,nntmes,nnamp,rmat,ndg
    dimension sigf(ngp,rmat,ntimes)
    dimension sigfti(ntimes),ncor(kmax)
c
    m = ncor(k)
    if(nntmes .le. 1)then
        x = sigf(ig,m,1)
    else
        do 100 i=1,nntmes
            if(t .le. sigfti(i))then
                go to 200
            end if
100        continue
c
c-----time is > than any time on sigf file. set equal to
c         sigf at last sigf file time step
c
        x = sigf(ig,m,nntmes)
        go to 300
c
200        continue
        if(i .le. 1)then
            x = sigf(ig,m,1)
        else
            *   x = sigf(ig,m,i-1) + (sigf(ig,m,i) - sigf(ig,m,i-1))*
              (t - sigfti(i-1))/(sigfti(i) - sigfti(i-1))
        end if
300        continue
c
    end if
    return
    end
    subroutine oflux(flux,fluxti)
c-----
c
c   output flux distribution
c-----
c
    common/units2/inn,iout,isigf,itime,iflux,ikin,ifluxo
    common/param2/kmax,ngp,ntimef,ntimes,namp,
* nntmef,nntmes,nnamp,rmat,ndg
    dimension flux(ngp,kmax,ntimef),fluxti(ntimef)
c
c
    do 200 i=1,nntmef
        do 100 ig=1,ngp
            write(ifluxo,910)fluxti(i),ig
            write(ifluxo,930)(flux(ig,k,i),k=1,kmax)
100        continue
200    continue
c
    return
910    format(1x,'flux at time=',1pe10.4,4x,'group=',i3)
930    format(6e11.4)
    end
    subroutine intamp(amp,t,x,ampiti)
c-----
c
c   interpolate amplitude values
c-----

```



```

call opnfil(outpt, 'new', 'formatted', '$out')
call opnfil(inpt, 'old', 'formatted', 'input')
rewind(inpt)
bfalse = .true.
btrue = .false.
call inital(lng)
call alocat(master, lng, *100)
call closda(direct(1))
call closda(direct(2))
call closda(direct(3))
close(inpt)
return
100 continue
call stop ('keno message number k5-213'//
*          ' *** error *** insufficient space allocation.'//
*          ' master was not called.$', 162, 0, 1)
return
end
c
c
c
subroutine cleanup

character*60 link1, link2, link3, link4, link5, link6, link7
character*60 link8, link9, link10, link11, link12, link13
character*60 link14, link15, link16, link17, link18
character*60 link19, link20, link21
c
link1='cat _out* > keno.out           '
link2='cat infile >> outfile          '
link3='cat input input.adj >> outfile '
link4='rm ft08f001 ft09f001 ft14f001 '
link19='rm ft46f001 ft47f001 ft49f001 '
link5='rm _out*_P* tdkeno tdkenoadj   '
link20='cat tmeout >> outfile         '
link21='rm tmeout                    '
link7='mv rho.dat output              '
link8='mv cdelay.dat output           '
link9='cp flux.dat output             '
link10='mv power.out output          '
link11='mv timen.dat output           '
link12='rm kinetics.dat delay.dat    '
link13='mv flux.out output            '
link14='rm general.dat               '
link15='mv power.in output            '
link16='rm keno.meth rho.out          '
link17='rm time0.dat nusigf.dat      '
link18='mv keno.out output            '
link6='mv outfile output              '
c
status=system(link1)
status=system(link2)
status=system(link3)
status=system(link4)
status=system(link19)
status=system(link5)
status=system(link20)
status=system(link21)
status=system(link7)
status=system(link8)
status=system(link9)
status=system(link10)
status=system(link11)
status=system(link12)
status=system(link13)
status=system(link14)
status=system(link15)
status=system(link16)
status=system(link17)
status=system(link18)
status=system(link6)
return
end

```

Appendix B:
TDKENO-M User's Manual

TDKENO-M User's Manual

by

Charles L. Bentley

The University of Tennessee, Knoxville

Department of Nuclear Engineering

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1. Introduction

TDKENO-M is a Fortran code which solves the time-dependent, three-dimensional Boltzmann transport equation with explicit representation of delayed neutrons as given by equations 1 and 2. The code consists of several large subroutines which perform specific functions as described below:

1. KENO V.a Modified to perform a fixed source calculation and to explicitly track delayed neutrons based on the distribution function given by equation 18. KENO V.a was also modified to include the flux shape derivative with the fixed source terms using a backwards difference approximation of first order (equation 19).
2. RHO Determines the point kinetics parameters (reactivity, generation time and effective delayed neutron fraction) from their inner product definitions as given by equations 9 through 15.
3. PTKIN Solves the point kinetics equations using the Livermore Solver of Ordinary Differential Equations (LSODE).
4. CDELAY Calculates the delayed neutron distribution (equation 18) as well as the cumulative distribution functions used to incorporate the flux shape derivative.
5. POWER Determines the power history using equation 22.

The calculational flow as well as the subroutines mentioned above are described in greater detail in the subsequent chapters of the user's manual.

2. Calculational Flow

The calculational flow for a typical TDKENO-M calculation is given in Figure 1. Initially, a steady-state adjoint calculation is performed using the modified version of KENO V.a. This steady state adjoint flux is used for all subsequent calculations of the point kinetics parameters as well as for the calculation of the system power. Next, a steady-state forward KENO V.a calculation is performed to determine the initial flux shape as well as the effective multiplication factor and the constraint integral (equation 7). Next, subroutines RHO and PTKIN are called to determine the initial values of the point kinetics parameters and the flux amplitude, respectively. In the case of thermalhydraulic feedback (i.e., Benchmark 14-A2), subroutine FEEDBACK is called to calculate the system temperature using the adiabatic heatup model described in Appendix C. The subroutine CDELAY is then called by TDKENO-M to determine the delayed neutron source distribution as well as the cumulative distribution functions needed for the implementation of the flux shape derivative for the transient calculations.

TDKENO-M next calls KENO V.a to perform the first flux shape calculation of the perturbed system. Subsequently, subroutines RHO, PTKIN and CDELAY are called again to update the system parameters and the amplitude as described above. This sequence is continued until the desired cutoff time is reached for the transient calculation. Upon the completion of the transient calculation, subroutine POWER is used to determine the power trace for the system.

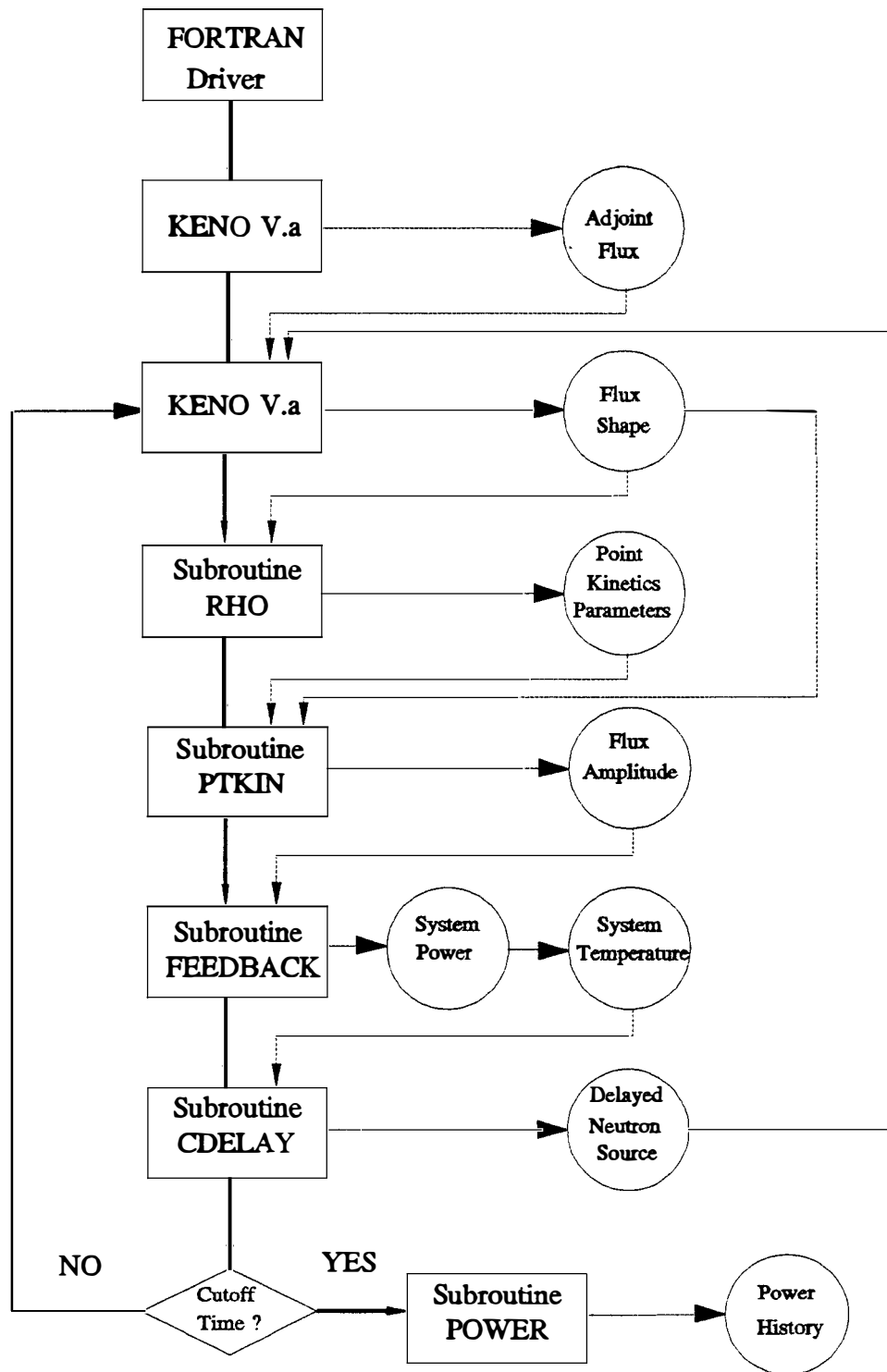


Figure 1: Computational Flow for TDKENO-M

3. Subroutines

3.1 KENO V.a

The three-dimensional transport code KENO V.a was modified to solve the inhomogeneous shape equation (equation 18) which includes the delayed neutron source, the amplitude derivative as well as the shape derivative.^{42,43,44} Several KENO V.a subroutines were modified so that the fission source for a generation would explicitly represent the delayed neutrons as well as those neutrons contributing to the flux shape derivative (i.e., the right hand side of the backwards difference approximation). KENO V.a selects the energy, angle and direction of the delayed neutrons based on the delayed neutron source distribution given by equation 18. The energy, angle and direction of the neutrons contributing to the flux shape derivative term are selected based on cumulative distribution functions calculated by subroutine CDELAY as described below.

3.2 RHO

Subroutine RHO calculates the point kinetics parameters including reactivity, generation time and effective delayed neutron fraction using an interpolated flux shape. The point kinetics parameters are calculated based on their inner product definitions. Subroutine RHO uses the steady-state adjoint fluxes and the flux shapes produced by KENO V.a to numerically integrate the appropriate equations. The cross sections, fission spectra and delayed neutron data are read from interface files as described in the following chapter of this manual.

3.3 PTKIN

Subroutine **PTKIN** solves the point kinetics equations using the Livermore Solver of Ordinary Differential Equations (**LSODE**). **LSODE** solves initial value problems for either stiff or non-stiff systems of first order differential equations. Integration time steps are selected automatically by **LSODE** based on user-specified tolerance parameters.

PTKIN uses quadratically interpolated (second order) point kinetics parameters with linearly interpolated cross sections. Subroutine **PTKIN** outputs the flux amplitude as well as the delayed precursor concentrations and the flux amplitude derivative.

3.4 CDELAY

Subroutine **CDELAY** solves the delayed neutron spatial distribution using a numerical integration technique with linearly interpolated flux shapes and cross sections. **CDELAY** selects the integration time step automatically using an algorithm to minimize integration errors.

CDELAY also determines cumulative distribution density functions used by **KENO V.a** to incorporate the flux shape derivative. Specifically, the right hand side of the backwards difference approximation is used to modify the source distribution in **KENO V.a** for each generation of neutrons. A random selection is made based on the cumulative distribution functions to determine whether each neutron is prompt, delayed, or contributes to the flux shape derivative. If a neutron is selected to be delayed, the

starting energy, angle, and position are determined from the delayed source distribution. If the neutron is determined to contribute to the flux shape derivative, the starting parameters are selected based on the source distribution calculated from the numerical integration of the backwards difference approximation term. Note that prompt neutrons are tracked by KENO V.a without any modifications.

3.5 POWER

Subroutine POWER determines the power history for a calculation by numerically integrating the product of the shape, amplitude, and fission cross sections divided by the particle speed. POWER uses linearly interpolated flux shapes and cross sections. The time, flux amplitude, and power are all written to an output file as describe later in the manual.

4. Description of Input Files

TDKENO-M uses several input files for a calculation including cross section files, standard KENO V.a input files, and a single input file which includes all other necessary data to perform a TDKENO-M calculation. Note that the standard KENO V.a input (except angular input) and the KENO V.a cross section files are not described in this manual since a complete description exists in the SCALE manuals. Described below is the TDKENO-M input file format followed by a sample input file for Benchmark 16-A1:

4.1 Global Parameters

<u>Record</u>	<u>Format</u>	<u>Input Variable</u>
1	6I5	<p>iadj Flags TDKENO-M to perform an adjoint calculation if set equal to 1. Otherwise, TDKENO-M does not perform an adjoint calculation and uses a user-specified adjoint file.</p> <p>imeth Determines the method used to calculate the flux shape. If set equal to 1, TDKENO-M performs a point kinetics calculation. For imeth=2, TDKENO-M performs an adiabatic calculation. For imeth=3, TDKENO-M does a quasistatic calculation. Finally, for imeth=4, TDKENO-M performs an improved quasistatic calculation.</p> <p>iss Flags TDKENO-M to perform a steady-state forward calculation. If iss=1, TDKENO-M does a steady-state calculation. Otherwise, TDKENO-M uses a user specified steady-state flux file.</p> <p>itfs The number of transient flux shape calculations to be performed.</p> <p>irho The number of reactivity calculations to be performed between flux shape calculations.</p>

<u>Record</u>	<u>Format</u>	<u>Input Variable</u>	
		ipk	The number of point kinetics calculations to be performed between each reactivity calculation.
2	NI5	icor	This record contains N entries where N is the number of transient shape calculations. The parameter icor corresponds to the standard KENO V.a input file to be used for each flux shape calculation.
3	2I5	kmax	The number of geometry regions.
		ngp	The number of energy groups.
4	4I5	dpr	The initial ratio of delayed neutrons to total neutrons.
		f2d	The initial ratio of neutrons contributing to the flux shape derivative to delayed plus flux shape contributing neutrons.
		d2p	The initial ratio of delayed neutrons to prompt neutrons.
		xdelt	The initial time of a delayed neutron source distribution calculation.
5	1I5	ifr	A flag used for the initial point kinetics calculation. This parameter should be set equal to -2 if the first calculation is a steady-state forward calculation.
6	1I5	ndg	The number of delayed neutron groups.
7	NI5	beta	The initial delayed neutron fraction for each delayed neutron group where N is the total number of groups.
8	NI5	alam	The initial delayed neutron decay constants where N is the number of delayed neutron groups.
9	6E7.4	time	The initial time of the calculation.
		pow	The initial power of the system.
		tfuel	The initial fuel temperature of the system.
		tcool1	The initial temperature of coolant 1.

<u>Record</u>	<u>Format</u>	<u>Input Variable</u>	
		tcool2	The initial temperature of coolant 2.
		dpdt	The initial amplitude derivative.
10	NE11.4	c(i)	The initial delayed neutron precursor concentrations, where N is the number of delayed neutron groups.
11	3I5	kmax	The number of geometrical regions.
		ngp	The number of energy groups.
		nmat	The number of materials.
12	NE11.4	vol(i)	The volumes for each region, where N is the number of geometrical regions.
13	NE11.4	chi(i)	The fission spectrum for each energy group, where N is the number of energy groups.
14	NE11.4	eb(i)	The energy boundaries for each energy group, where N is the number of energy groups plus one.
15	NE11.4	nc(i)	The material identification number corresponding to each geometrical region, where N is the number of geometrical regions.
16	6E11.4	time	The time of the first fission cross-section entry.
		sf(i,j)	The fission cross section at the specified time where i denotes the energy group and j denotes the geometrical region.
17	E11.4	xdum	This variable is set equal to -1.0 to flag a new sequence of fission cross section data.
18	6E11.4	sf(i,j)	These entries are the same as record 16 and are repeated for each time where fission cross section data is entered.

4.2 General Parameters

These parameters are specific to each problem and allow the user to input specific data used during a calculation. Each section starts with a record giving the section number and the number of entries in the section. The format of this series of data is:

<u>Record</u>	<u>Format</u>	<u>Input Variable</u>	
1	2I5	isec	The section number.
		nrec	The number of entries for this section.
2-6	80A1	title	These five lines can be used to give a descriptive title for the problem being modeled.
7-28			These 21 lines are not used in the current version of TDKENO-M.
29	2I5	isec	The section number for the time step data.
		istep	The number of time steps given in the time step data.
30	E11.4	tstep	The time for each flux shape calculation.

For the current version of TDKENO-M the first section is used to enter title data in a series of five lines. The second and third sections are used for thermalhydraulic data (Benchmark Problem 14-A2 only). Finally, the fourth section is used to enter time interval data.

Refer to the following section of this document for a sample TDKENO-M input file. Note that all of the sample files presented in this manual are for the modeling of ANL Benchmark Problem 16-A1.⁴⁵

4.3 Sample TDKENO-M Input File

```

0 4 1 3 10 10
1 1 1
21 2
.0000E+00 .0000E+00 .0000E+00 .0000E+00
-2
6
.1290E-01 .3110E-01 .1340E+00 .3310E+00 .1260E+01 .3210E+01
.8100E-04 .6870E-03 .6120E-03 .1138E-02 .5120E-03 .1700E-03
.0000E+00 .1000E+01 .0000E+00 .0000E+00 .0000E+00 .0000E+00
.1680E+05 .5912E+05 .1223E+05 .9215E+04 .1094E+04 .1439E+03
21 2 5
.4000E+02 .3000E+01 .7000E+01 .9100E+01 .9100E+01 .9174E+01
.7000E+01 .3000E+01 .9000E+01 .5000E+01 .2400E+02 .5000E+01
.9000E+01 .3000E+01 .7000E+01 .9126E+01 .9100E+01 .9148E+01
.7000E+01 .3000E+01 .4000E+02
.1000E+01 .0000E+00
.1194E+07 .1934E+05 .1000E+04
1 4 4 4 4 4 4 3 2 2 2
3 5 5 5 5 5 5 5 1
.0000E+00 .8344E-03 .3278E-03 .7452E-02 .1106E-01 .0000E+00
.0000E+00 .7452E-02 .1106E-01 .7452E-02 .1106E-01
.1000E-08 .8344E-03 .3278E-03 .7452E-02 .1106E-01 .0000E+00
.0000E+00 .7824E-02 .1161E-01 .7079E-02 .1051E-01
.1500E+02 .8344E-03 .3278E-03 .7452E-02 .1106E-01 .0000E+00
.0000E+00 .7824E-02 .1161E-01 .7079E-02 .1051E-01
-.1000E+01 .0000E+00 .0000E+00 .0000E+00 .0000E+00 .0000E+00
.0000E+00 .0000E+00 .0000E+00 .0000E+00 .0000E+00
.0000E+00 .8344E-03 .3278E-03 .7452E-02 .1106E-01 .0000E+00
.0000E+00 .7452E-02 .1106E-01 .7452E-02 .1106E-01
.1000E-08 .8344E-03 .3278E-03 .7452E-02 .1106E-01 .0000E+00
.0000E+00 .7824E-02 .1161E-01 .7079E-02 .1051E-01
.1500E+02 .8344E-03 .3278E-03 .7452E-02 .1106E-01 .0000E+00
.0000E+00 .7824E-02 .1161E-01 .7079E-02 .1051E-01
-.1000E+01 .0000E+00 .0000E+00 .0000E+00 .0000E+00 .0000E+00
.0000E+00 .0000E+00 .0000E+00 .0000E+00 .0000E+00
1 5
BENCHMARK PROBLEM 16-A1
P. 26 OF ORNL/TM-7086

2 14
4 7 1 1 0
0 0 0 0 0 0
10 10 .1000E-02 .1000E-02
20 24 5 16 5 24 20
1
.0000E+00 .4000E+02 .8737E+02 .9637E+02 .1304E+03 .1394E+03 .1867E+03
.2267E+03
.1000E+01 .1000E+01
.1000E+01 .1000E+01
.2500E+00 .2500E+00 .2500E+00 .2500E+00
-.7887E+00 -.2113E+00 .2113E+00 .7887E+00
.1000E+01 .1000E+01 .1000E+01 .1000E+01
.1000E+01 .1000E+01 .1000E+01 .1000E+01
3 6
3 3 2
1 2 3 2 3 2 1
.0000E+00 .0000E+00 .0000E+00
1 1 .1000E+01
2 2 .1000E+01
3 3 .1000E+01
4 5
.0000E+00
.1000E-05
.1000E-04
.1000E-01
.1000E+02

```

4.4 KENO V.a Angular Input

The KENO V.a input is identical to a normal KENO V.a input file with the exception that angular data is appended to the end of the standard input file. The angular data is entered in the KENO V.a extra data form (i.e., READ EXTRA data END EXTRA) where data is in the form:

nphi	The number of phi angle bins.
ntheta	The number of theta (azimuthal) angle bins.
phi(i)	The boundaries for the phi angles. The first angle entered must be 0.0 and the last angle must be twice the variable pi.
theta(i)	The boundaries for the theta (azimuthal) angles. The first angle entered must be 0.0 and the last angle must be pi.

Refer to the following section of this manual for a sample KENO V.a input file with angular data.

4.5 Sample KENO V.a Input File

```
benchmark problem 16-a1 steady state adjoint k16a1a
read parm tme=450 tba=10.0 gen=706 npg=2500 nsk=6 flx=yes
rnd=2bc38cfe126d amx=yes xap=yes plt=no adj=yes
lib=2 end parm
read geom
cuboid 1 1 40.000 0.0 1000.0 -1000.0 1000.0 -1000.0
cuboid 4 1 43.000 0.0 1000.0 -1000.0 1000.0 -1000.0
cuboid 4 1 50.000 0.0 1000.0 -1000.0 1000.0 -1000.0
cuboid 4 1 59.100 0.0 1000.0 -1000.0 1000.0 -1000.0
cuboid 4 1 68.200 0.0 1000.0 -1000.0 1000.0 -1000.0
cuboid 4 1 77.374 0.0 1000.0 -1000.0 1000.0 -1000.0
cuboid 4 1 84.374 0.0 1000.0 -1000.0 1000.0 -1000.0
cuboid 4 1 87.374 0.0 1000.0 -1000.0 1000.0 -1000.0
cuboid 3 1 96.374 0.0 1000.0 -1000.0 1000.0 -1000.0
cuboid 2 1 101.374 0.0 1000.0 -1000.0 1000.0 -1000.0
cuboid 2 1 125.374 0.0 1000.0 -1000.0 1000.0 -1000.0
cuboid 2 1 130.374 0.0 1000.0 -1000.0 1000.0 -1000.0
cuboid 3 1 139.374 0.0 1000.0 -1000.0 1000.0 -1000.0
cuboid 5 1 142.374 0.0 1000.0 -1000.0 1000.0 -1000.0
cuboid 5 1 149.374 0.0 1000.0 -1000.0 1000.0 -1000.0
cuboid 5 1 158.500 0.0 1000.0 -1000.0 1000.0 -1000.0
cuboid 5 1 167.600 0.0 1000.0 -1000.0 1000.0 -1000.0
```

```
cuboid 5 1 176.748 0.0 1000.0 -1000.0 1000.0 -1000.0
cuboid 5 1 183.748 0.0 1000.0 -1000.0 1000.0 -1000.0
cuboid 5 1 186.748 0.0 1000.0 -1000.0 1000.0 -1000.0
cuboid 1 1 226.748 0.0 1000.0 -1000.0 1000.0 -1000.0
end geom
read boun yzf=specular end boun
read mixt sct=0 mix=1 1 1.0
           mix=2 2 1.0
           mix=3 3 1.0
           mix=4 2 1.0
           mix=5 2 1.0
end mixt
read extr
20 1
0.0 0.314 0.628 0.942 1.257 1.571 1.885 2.199 2.513 2.827
3.142 3.456 3.770 4.084 4.398 4.712 5.027 5.341 5.655 5.969 6.283
0.0 3.14159
end extr
end data
```

5. Description of Output Files

The output from TDKENO-M consists of six files. Each of these files is described below and excerpts from sample output files are given.

5.1 Output file power.out

This output file consists of three columns and contains the power history as well as the flux amplitudes. The first column is the time each flux amplitude was calculated. The second and third columns are the power and flux amplitude, respectively.

5.1.1 Sample power.out file

```
0.000000E+00 1.000000E+00 1.000000E+00
5.000000E-08 1.000793E+00 1.000000E+00
1.000000E-07 1.001144E+00 1.000010E+00
1.500000E-07 1.001485E+00 1.000010E+00
2.000000E-07 1.001827E+00 1.000010E+00
2.500000E-07 1.002179E+00 1.000020E+00
3.000000E-07 1.002521E+00 1.000020E+00
3.500000E-07 1.002864E+00 1.000020E+00
4.000000E-07 1.003216E+00 1.000030E+00
4.500000E-07 1.003559E+00 1.000030E+00
5.000000E-07 1.003902E+00 1.000030E+00
5.500000E-07 1.004255E+00 1.000040E+00
6.000000E-07 1.004599E+00 1.000040E+00
6.500000E-07 1.004942E+00 1.000040E+00
7.000000E-07 1.005296E+00 1.000050E+00
7.500000E-07 1.005640E+00 1.000050E+00
8.000000E-07 1.005984E+00 1.000050E+00
8.500000E-07 1.006339E+00 1.000060E+00
9.000000E-07 1.006684E+00 1.000060E+00
9.500000E-07 1.007038E+00 1.000070E+00
1.000000E-06 1.007384E+00 1.000070E+00
2.080000E-06 1.007588E+00 1.002140E+00
3.070000E-06 1.007756E+00 1.004030E+00
4.150000E-06 1.007904E+00 1.006070E+00
5.230000E-06 1.008028E+00 1.008100E+00
6.310000E-06 1.008129E+00 1.010120E+00
7.030000E-06 1.008171E+00 1.011450E+00
8.020000E-06 1.008221E+00 1.013280E+00
9.010000E-06 1.008240E+00 1.015090E+00
1.000000E-05 1.008247E+00 1.016900E+00
2.098000E-04 1.198779E+00 1.208920E+00
3.097000E-04 1.231955E+00 1.242200E+00
4.096000E-04 1.249170E+00 1.259380E+00
5.095000E-04 1.258157E+00 1.268260E+00
```

5.2 Output file outfile

This output file contains the status from each subroutine upon its completion. Information in this file includes the time of completion of each subroutine, the status of the completion, and the final values from the calculation. The final five lines of this output file contains information describing the computational method used for the calculation (i.e., point kinetics, adiabatic, quasistatic, or improved quasistatic) as well as the CPU time for the problem.

5.2.1 Sample outfile file

```
*****
Time,tstop,delt,tout,tk = .0000E+00 .1000E-05 .1000E-07 .1000E-07 .1000E-06
iter = 1  istate = 1
Reactivity = 2.58012E-05
Gen = 3.74433E-07
Beta = 8.10000E-05
Beta = 6.86999E-04
Beta = 6.11999E-04
Beta = 1.13800E-03
Beta = 5.11999E-04
Beta = 1.69999E-04
Betatn = 3.19999E-03
Lamda = 1.29000E-02
Lamda = 3.10999E-02
Lamda = .134
Lamda = .331
Lamda = 1.26
Lamda = 3.21
*****
Time,tstop,delt,tout,tk = .1000E-06 .1000E-05 .1000E-07 .1100E-06 .2000E-06
iter = 2  istate = 2
Reactivity = 2.58012E-05
Gen = 3.74433E-07
Beta = 8.10000E-05
Beta = 6.86999E-04
Beta = 6.11999E-04
Beta = 1.13800E-03
Beta = 5.11999E-04
Beta = 1.69999E-04
Betatn = 3.19999E-03
Lamda = 1.29000E-02
Lamda = 3.10999E-02
Lamda = .134
Lamda = .331
Lamda = 1.26
Lamda = 3.21
*****
Time,tstop,delt,tout,tk = .9900E-06 .1000E-05 .1000E-07 .1000E-05 .1000E-05
iter = 10  istate = 2
Reactivity = 2.58012E-05
Gen = 3.74433E-07
```

```

Beta = 8.10000E-05
Beta = 6.86999E-04
Beta = 6.11999E-04
Beta = 1.13800E-03
Beta = 5.11999E-04
Beta = 1.69999E-04
Betatn = 3.19999E-03
Lamda = 1.29000E-02
Lamda = 3.10999E-02
Lamda = .134
Lamda = .331
Lamda = 1.26
Lamda = 3.21
*****
ptkin finished at time= .1000E-05
  last power= .1000E+01
cdelay calc. ended at time= .1000E-05
ratio of fixed source to total source= .3801E+00
ratio of flux shift to total fixed source= .9966E+00
ratio of delayed n. source to prompt source= .2055E-02
Flux.dat file updated by norm, time = .1000E-05
*****
Time,tstop,delt,tout,tk = .1000E-05 .1000E-04 .9000E-07 .1090E-05 .1900E-05
iter = 1  istate = 1
Reactivity = 7.30358E-04
Gen = 3.72856E-07
Beta = 8.10000E-05
Beta = 6.87000E-04
Beta = 6.11999E-04
Beta = 1.13800E-03
Beta = 5.11999E-04
Beta = 1.69999E-04
Betatn = 3.19999E-03
Lamda = 1.29000E-02
Lamda = 3.10999E-02
Lamda = .134
Lamda = .331
Lamda = 1.26
Lamda = 3.21
*****
Time,tstop,delt,tout,tk = .1000E-04 .1000E-04 .9000E-07 .1009E-04 .1000E-04
iter = 10  istate = 2
Reactivity = 7.30358E-04
Gen = 3.72856E-07
Beta = 8.10000E-05
Beta = 6.87000E-04
Beta = 6.11999E-04
Beta = 1.13800E-03
Beta = 5.11999E-04
Beta = 1.69999E-04
Betatn = 3.19999E-03
Lamda = 1.29000E-02
Lamda = 3.10999E-02
Lamda = .134
Lamda = .331
Lamda = 1.26
Lamda = 3.21
*****
ptkin finished at time= .1000E-04
  last power= .1017E+01
cdelay calc. ended at time= .1009E-04
ratio of fixed source to total source= .6446E-01
ratio of flux shift to total fixed source= .9707E+00
ratio of delayed n. source to prompt source= .2017E-02
Flux.dat file updated by norm, time = .1009E-04
*****
TDKENO-M performed an improved quasistatic calculation.
TDKENO-M performed a steady-state adjoint calculation.
TDKENO-M performed a steady-state forward calculation.
TDKENO-M performed 3 transient calculations.
The calculation was completed in 0.4795734E+01 min.
*****

```

5.3 Output file rho.dat

The values of reactivity calculated by subroutine RHO are contained in this output file along with the generation time and effective delayed neutron fractions. This file contains a series of outputs from different reactivity calculations. Each output begins with either a -1 or a -2 which indicates whether the calculation used interpolated or extrapolated fluxes. A -1 flag denotes that the calculation used extrapolated fluxes and a -2 denotes that the calculation used interpolated fluxes.

5.3.1 Sample rho.dat file

```
-1
.0000000E+00 .3744335E-06 .3055803E-04 .3907257E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8100001E-04 .6869999E-03 .6119999E-03 .1138000E-02 .5120000E-03 .1700000E-03
.1000000E-06 .3744335E-06 .3055803E-04 .3907257E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8100001E-04 .6869999E-03 .6119999E-03 .1138000E-02 .5120000E-03 .1700000E-03
.2000000E-06 .3744335E-06 .3055803E-04 .3907257E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8100001E-04 .6869999E-03 .6119999E-03 .1138000E-02 .5120000E-03 .1700000E-03
.3000000E-06 .3744335E-06 .3055803E-04 .3907257E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8100001E-04 .6869999E-03 .6119999E-03 .1138000E-02 .5120000E-03 .1700000E-03
.4000000E-06 .3744335E-06 .3055803E-04 .3907257E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8100001E-04 .6869999E-03 .6119999E-03 .1138000E-02 .5120000E-03 .1700000E-03
.5000000E-06 .3744335E-06 .3055803E-04 .3907257E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8100001E-04 .6869999E-03 .6119999E-03 .1138000E-02 .5120000E-03 .1700000E-03
.6000000E-06 .3744335E-06 .3055803E-04 .3907257E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8100001E-04 .6869999E-03 .6119999E-03 .1138000E-02 .5120000E-03 .1700000E-03
.7000000E-06 .3744335E-06 .3055803E-04 .3907257E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8100001E-04 .6869999E-03 .6119999E-03 .1138000E-02 .5120000E-03 .1700000E-03
.8000000E-06 .3744335E-06 .3055803E-04 .3907257E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8100001E-04 .6869999E-03 .6119999E-03 .1138000E-02 .5120000E-03 .1700000E-03
.9000000E-06 .3744335E-06 .3055803E-04 .3907257E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8100001E-04 .6869999E-03 .6119999E-03 .1138000E-02 .5120000E-03 .1700000E-03
.1000000E-05 .3744335E-06 .3055803E-04 .3907257E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8100001E-04 .6869999E-03 .6119999E-03 .1138000E-02 .5120000E-03 .1700000E-03
-2
.0000000E+00 .3744335E-06 .3055803E-04 .3914710E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8100001E-04 .6869999E-03 .6119999E-03 .1138000E-02 .5120000E-03 .1700000E-03
.1000000E-06 .3742900E-06 .1323545E-03 .3914710E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8100001E-04 .6870000E-03 .6120000E-03 .1138000E-02 .5120000E-03 .1700000E-03
```



```

.2000000E-06 .3741465E-06 .2341905E-03 .3914710E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8099998E-04 .6869999E-03 .6119999E-03 .1138000E-02 .5120000E-03 .1700000E-03
.3000000E-06 .3740031E-06 .3360515E-03 .3914710E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8099999E-04 .6869999E-03 .6120000E-03 .1138000E-02 .5120000E-03 .1700000E-03
.4000000E-06 .3738596E-06 .4379657E-03 .3914710E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8099999E-04 .6869999E-03 .6119999E-03 .1138000E-02 .5119999E-03 .1700000E-03
.5000000E-06 .3737161E-06 .5398598E-03 .3914710E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8099999E-04 .6869999E-03 .6119999E-03 .1138000E-02 .5120000E-03 .1700000E-03
.6000000E-06 .3735724E-06 .6417960E-03 .3914710E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8100001E-04 .6870001E-03 .6120000E-03 .1138000E-02 .5120000E-03 .1700000E-03
.7000000E-06 .3734287E-06 .7437427E-03 .3914710E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8100000E-04 .6870000E-03 .6119999E-03 .1138000E-02 .5120000E-03 .1700000E-03
.8000000E-06 .3732851E-06 .8457223E-03 .3914710E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8100000E-04 .6870001E-03 .6120000E-03 .1138000E-02 .5120000E-03 .1700000E-03
.9000000E-06 .3731414E-06 .9477155E-03 .3914710E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8099999E-04 .6869999E-03 .6119998E-03 .1138000E-02 .5119999E-03 .1700000E-03
.1000000E-05 .3729977E-06 .1049727E-02 .3914710E-13
.1676800E+05 .5899200E+05 .1219700E+05 .9181500E+04 .1085200E+04 .1414300E+03
.8099998E-04 .6870000E-03 .6119999E-03 .1138000E-02 .5120000E-03 .1700000E-03

```

5.4 Output file flux.out

The normalized flux shape distributions are contained in this output file for each of the energy groups as well as each of the spatial regions. Also contained in this file is the time of each of the flux shape calculations.

5.4.1 Sample flux.out file

```

flux at time=.0000E+00 group= 1
1.670472E-01 5.563998E-01 6.784357E-01 8.293718E-01 9.266717E-01 9.418316E-01
8.852198E-01 8.093197E-01 7.454078E-01 8.177118E-01 9.015638E-01 8.112158E-01
7.369277E-01 7.956918E-01 8.664557E-01 9.198877E-01 9.018717E-01 8.018478E-01
6.573238E-01 5.392158E-01 1.623264E-01
flux at time=.0000E+00 group= 2
5.467278E-02 1.092384E-01 1.162852E-01 1.287152E-01 1.382828E-01 1.387520E-01
1.293760E-01 1.191160E-01 1.121264E-01 1.207244E-01 1.323544E-01 1.188724E-01
1.097808E-01 1.180464E-01 1.290672E-01 1.366644E-01 1.360867E-01 1.256812E-01
1.125708E-01 1.070184E-01 5.365318E-02
flux at time=1.0000E-06 group= 1
1.823611E-01 6.087489E-01 7.512240E-01 9.188441E-01 1.025996E+00 1.029687E+00
9.530403E-01 8.589637E-01 7.795646E-01 8.435740E-01 8.968463E-01 7.847601E-01
6.999922E-01 7.462457E-01 8.035786E-01 8.402659E-01 8.200388E-01 7.297654E-01
6.012915E-01 4.978580E-01 1.489566E-01
flux at time=1.0000E-06 group= 2
6.033601E-02 1.198631E-01 1.272698E-01 1.409502E-01 1.526740E-01 1.518204E-01
1.399260E-01 1.252825E-01 1.156989E-01 1.234606E-01 1.317317E-01 1.146232E-01
1.044292E-01 1.103874E-01 1.177961E-01 1.243005E-01 1.241395E-01 1.137117E-01
1.031216E-01 9.855019E-02 4.883561E-02
flux at time=1.0090E-05 group= 1

```

```

1.802600E-01 5.942785E-01 7.350117E-01 9.004663E-01 9.982772E-01 9.987129E-01
9.283276E-01 8.413092E-01 7.661208E-01 8.315411E-01 8.935103E-01 7.793484E-01
6.961046E-01 7.451782E-01 7.994739E-01 8.329597E-01 8.114197E-01 7.226345E-01
5.917856E-01 4.889515E-01 1.484267E-01
flux at time=1.0090E-05 group= 2
6.501836E-02 1.268395E-01 1.340680E-01 1.509453E-01 1.623615E-01 1.612706E-01
1.481227E-01 1.331265E-01 1.223619E-01 1.312151E-01 1.423173E-01 1.233794E-01
1.113750E-01 1.170124E-01 1.265836E-01 1.342684E-01 1.328469E-01 1.229227E-01
1.115646E-01 1.062308E-01 5.415092E-02
flux at time=1.0000E-02 group= 1
2.295858E-01 7.704574E-01 9.482068E-01 1.164879E+00 1.294740E+00 1.297853E+00
1.197407E+00 1.083756E+00 9.867509E-01 1.076199E+00 1.149749E+00 1.002511E+00
8.979581E-01 9.656869E-01 1.035059E+00 1.078718E+00 1.042191E+00 9.218639E-01
7.539604E-01 6.220564E-01 1.864705E-01
flux at time=1.0000E-02 group= 2
7.545748E-02 1.518985E-01 1.601864E-01 1.783776E-01 1.929991E-01 1.931676E-01
1.768196E-01 1.583309E-01 1.469479E-01 1.565476E-01 1.690063E-01 1.468470E-01
1.328318E-01 1.397690E-01 1.515151E-01 1.608142E-01 1.570381E-01 1.448328E-01
1.293624E-01 1.233330E-01 6.152108E-02

```

5.5 Output file cdelay.dat

This output file contains the delayed neutron precursor spatial distribution data as well as the data used for incorporating the flux shape derivative. This output file consists of a header line which contains the time as well as the delayed neutron fraction and the flux shape derivative contribution factor.

Following the header line is a sequence of cumulative distribution functions. The first sequence of data is the cumulative density functions for the energy, angular, and spatial distributions for the delayed neutrons. The second sequence of data is similar to the first sequence with the exception that it is for the flux shape derivative probabilities.

5.5.1 Sample cdelay.dat file

```

21 2
.380143E+00 .996650E+00 .205475E-02 .000000E+00
.629260E-02 .160645E-01 .443955E-01 .692012E-01 .767628E-01 .784710E-01
.561962E-01 .220467E-01 .000000E+00 .371462E-01 .196387E+00 .368017E-01
.000000E+00 .217066E-01 .551935E-01 .763573E-01 .748599E-01 .673828E-01
.430066E-01 .156066E-01 .612166E-02
.100000E+01 .000000E+00 .100000E+01 .000000E+00 .100000E+01 .000000E+00
.100000E+01 .000000E+00 .100000E+01 .000000E+00 .100000E+01 .000000E+00

```

```

.100000E+01 .000000E+00 .100000E+01 .000000E+00 .000000E+00 .000000E+00
.100000E+01 .000000E+00 .100000E+01 .000000E+00 .100000E+01 .000000E+00
.000000E+00 .000000E+00 .100000E+01 .000000E+00 .100000E+01 .000000E+00
.100000E+01 .000000E+00 .100000E+01 .000000E+00 .100000E+01 .000000E+00
.100000E+01 .000000E+00 .100000E+01 .000000E+00 .100000E+01 .000000E+00
.727156E-01 .133826E-01 .354849E-01 .537173E-01 .589178E-01 .600087E-01
.428773E-01 .168551E-01 .470480E-01 .284239E-01 .150032E+00 .281004E-01
.463021E-01 .166327E-01 .423411E-01 .585325E-01 .576406E-01 .524563E-01
.343660E-01 .130450E-01 .711204E-01
.342024E+00 .657976E+00 .464250E+00 .535750E+00 .498136E+00 .501864E+00
.522951E+00 .477049E+00 .532728E+00 .467272E+00 .535923E+00 .464077E+00
.537906E+00 .462094E+00 .536161E+00 .463839E+00 .530738E+00 .469262E+00
.535391E+00 .464609E+00 .536796E+00 .463204E+00 .537252E+00 .462748E+00
.533153E+00 .466847E+00 .534180E+00 .465820E+00 .533171E+00 .466829E+00
.533829E+00 .466171E+00 .529959E+00 .470041E+00 .520481E+00 .479519E+00
.498349E+00 .501651E+00 .461555E+00 .538445E+00 .339812E+00 .660188E+00

```

5.6 Output file keno.out

This output file is simply the standard KENO V.a output files for each of the flux shape calculations. Note that the output has been modified to include the amplitude derivative and shape derivative information as well as the delayed neutron source distribution information.

5.6.1 Sample keno.out file

```

*****
****          program verification information          ****
****          ****
****          code system:  ncsshp  version:  1.0          ****
****          ****
*****

*****
****          ****
****          ****
****          program:  tdkenom          ****
****          ****
****          creation date:  09/11/96          ****
****          ****
****          library:          ****
****          ****
****          this is not a ncsshp  configuration controlled code          ****
****          ****
****          jobname:  ut9          ****
****          ****
****          date of execution:  09/11/96          ****
****          ****
****          time of execution:  08:28:05          ****
****          ****
*****
*****
*****
***          benchmark problem 16-a1  perturbed state  k16a1p1  ***

```

```

***
*****
***
***          numeric parameters          ***
***
***          tme          maximum problem time (min)          430.00          ***
***
***          tba          time per generation (min)           20.00          ***
***
***          gen          number of generations                353          ***
***
***          npg          number per generation                2100         ***
***
***          nsk          number of generations to be skipped  6          ***
***
***          beg          beginning generation number          1          ***
***
***          res          generations between checkpoints        0          ***
***
***          x1d          number of extra 1-d cross sections    0          ***
***
***          nbk          neutron bank size                     125         ***
***
***          xnb          extra positions in neutron bank        0          ***
***
***          nfb          fission bank size                     2100         ***
***
***          xfb          extra positions in fission bank        0          ***
***
***          wta          default value of weight average       .5000         ***
***
***          wth          weight high for splitting              3.0000        ***
***
***          wtl          weight low for russian roulette        .3333         ***
***
***          rnd          starting random number                2BC5 8CFE126D ***
***
***          nb8          number of d.a. blocks on unit 8        200         ***
***
***          nl8          length of d.a. blocks on unit 8        512         ***
***
***          adj          mode of calculation                    forward      ***
***
***          input data written on restart unit                no          ***
***
***          binary data interface                              no          ***
***
*****
***
***          benchmark problem 16-a1      perturbed state      k16a1p1          ***
***
*****
***
***          logical parameters          ***
***
***          run          execute problem after checking data    yes          ***
***
***          plt          plot picture map(s)                    no          ***
***
***          flx          compute flux                            yes          ***
***
***          fdn          compute fission densities              no          ***
***
***          smu          compute avg unit self-multiplication    no          ***
***
***          nub          compute nu-bar & avg fission group      no          ***
***
***          mku          compute matrix k-eff by unit number     no          ***
***
***          mkp          compute matrix k-eff by unit location   no          ***
***

```

```

*** cku compute cofactor k-eff by unit number no ***
*** ckp compute cofactor k-eff by unit location no ***
*** fmu print fiss prod matrix by unit number no ***
*** fmp print fiss prod matrix by unit location no ***
*** mkh compute matrix k-eff by hole number no ***
*** mka compute matrix k-eff by array number no ***
*** ckh compute cofactor k-eff by hole number no ***
*** cka compute cofactor k-eff by array number no ***
*** fmh print fiss prod matrix by hole number no ***
*** fma print fiss prod matrix by array number no ***
*** hhl collect matrix by highest hole level no ***
*** hal collect matrix by highest array level no ***
*** amx print all mixed cross sections yes ***
*** far print fis. and abs. by region no ***
*** xs1 print 1-d mixture x-sections yes ***
*** pax print xsec-albedo correlation tables no ***
*** xs2 print 2-d mixture x-sections yes ***
*** pwt print weight average array no ***
*** xap print mixture angles & probabilities yes ***
*** pgm print input geometry no ***
*** pki print fission spectrum yes ***
*** bug print debug information no ***
*** p1d print extra 1-d cross sections yes ***
*** trk print tracking information no ***
***
*****
*****
***
*** parameter input completed ***
***
*** ..... 0 io's were used reading the parameter data ..... ***
***
*****
*****
This code used method 4 to calculate shape
dpf2t,f2dpf,d2p,time = .380143E+00 .996650E+00 .205475E-02 .000000E+00
dpdt,time,pow,xdelt = .715206E+02 .100000E-05 .100007E+01 .000000E+00
*****
***** data reading completed *****
*****
***
*** benchmark problem 16-a1 perturbed state k16a1p1 ***
***
*****
*****
1 =id material= 1
group sgt nap abp nfp chi mwa1 mwa2 mwa3

```

```

1 2.41100E-01 9.83998E-01 1.60017E-02 3.46085E-03 1.00000E+00 1 2 1
2 4.17200E-01 9.75561E-01 2.44391E-02 7.85618E-04 1.00000E+00 3 3 2

scattering transfer array for material 1
  from grp 1 grp 2
  to grp
+ 0 9.84834E-01 1.00000E+00
+ 1 1.51659E-02

2 =id material= 2

group sgt nap abp nfp chi mwa1 mwa2 mwa3
1 1.84900E-01 9.72396E-01 2.76041E-02 4.03018E-02 1.00000E+00 1 2 1
2 3.66800E-01 9.64343E-01 3.56570E-02 3.01559E-02 1.00000E+00 3 3 2

scattering transfer array for material 2
  from grp 1 grp 2
  to grp
+ 0 9.88403E-01 1.00000E+00
+ 1 1.15965E-02

3 =id material= 3

group sgt nap abp nfp chi mwa1 mwa2 mwa3
1 9.43200E-02 9.26917E-01 7.30831E-02 .00000E+00 .00000E+00 1 2 1
2 1.87620E-01 9.13069E-01 8.69310E-02 .00000E+00 .00000E+00 3 3 2

scattering transfer array for material 3
  from grp 1 grp 2
  to grp
+ 0 9.80363E-01 1.00000E+00
+ 1 1.96370E-02

4 =id material= 4

group sgt nap abp nfp chi mwa1 mwa2 mwa3
1 1.94145E-01 9.72396E-01 2.76041E-02 4.03018E-02 1.00000E+00 1 2 1
2 3.85140E-01 9.64343E-01 3.56570E-02 3.01559E-02 1.00000E+00 3 3 2

scattering transfer array for material 4
  from grp 1 grp 2
  to grp
+ 0 9.88404E-01 1.00000E+00
+ 1 1.15965E-02

5 =id material= 5

group sgt nap abp nfp chi mwa1 mwa2 mwa3
1 1.75655E-01 9.72396E-01 2.76041E-02 4.03018E-02 1.00000E+00 1 2 1
2 3.48460E-01 9.64343E-01 3.56570E-02 3.01559E-02 1.00000E+00 3 3 2

scattering transfer array for material 5
  from grp 1 grp 2
  to grp
+ 0 9.88403E-01 1.00000E+00
+ 1 1.15965E-02
*****
***
*** benchmark problem 16-a1 perturbed state k16a1p1 ***
***
*****
***** additional information *****
***
*** number of energy groups 2 use lattice geometry no ***
*** no. of fission spectrum source group 1 global array number 0 ***
*** no. of scattering angles in xsecs 0 ***
*** number of units in the global x dir. 0 ***
***

```

```

*** entries/neutron in the neutron bank 16 ***
***
*** number of units in the global y dir. 0 ***
***
*** entries/neutron in the fission bank 9 ***
***
*** number of units in the global z dir. 0 ***
***
*** number of mixtures used 5 use a global reflector yes ***
***
*** number of bias id's used 1 use nested holes no ***
***
*** number of differential albedos used 0 number of holes 0 ***
***
*** total input geometry regions 21 maximum hole nesting level 0 ***
***
*** number of geometry regions used 21 use nested arrays no ***
***
*** largest geometry unit number 1 number of arrays used 0 ***
***
*** largest array number 1 maximum array nesting level 0 ***
***
*** +x boundary condition vacuum -x boundary condition vacuum ***
***
*** +y boundary condition specular -y boundary condition specular ***
***
*** +z boundary condition specular -z boundary condition specular ***
***
*****
*** benchmark problem 16-a1 perturbed state k16a1p1 ***
***
*****

```

0 media bias geometry description for those units utilized in this problem

region	num	id	global	unit	1	----
0 1 cuboid	1	1	+x = 40.000	-x = .00000E+00	+y = 1000.0	-y = -1000.0 +z
= 1000.0						
0 2 cuboid	4	1	+x = 43.000	-x = .00000E+00	+y = 1000.0	-y = -1000.0 +z
= 1000.0						
0 3 cuboid	4	1	+x = 50.000	-x = .00000E+00	+y = 1000.0	-y = -1000.0 +z
= 1000.0						
0 4 cuboid	4	1	+x = 59.100	-x = .00000E+00	+y = 1000.0	-y = -1000.0 +z
= 1000.0						
0 5 cuboid	4	1	+x = 68.200	-x = .00000E+00	+y = 1000.0	-y = -1000.0 +z
= 1000.0						
0 6 cuboid	4	1	+x = 77.374	-x = .00000E+00	+y = 1000.0	-y = -1000.0 +z
= 1000.0						
0 7 cuboid	4	1	+x = 84.374	-x = .00000E+00	+y = 1000.0	-y = -1000.0 +z
= 1000.0						
0 8 cuboid	4	1	+x = 87.374	-x = .00000E+00	+y = 1000.0	-y = -1000.0 +z
= 1000.0						
0 9 cuboid	3	1	+x = 96.374	-x = .00000E+00	+y = 1000.0	-y = -1000.0 +z
= 1000.0						
0 10 cuboid	2	1	+x = 101.37	-x = .00000E+00	+y = 1000.0	-y = -1000.0 +z
= 1000.0						
0 11 cuboid	2	1	+x = 125.37	-x = .00000E+00	+y = 1000.0	-y = -1000.0 +z
= 1000.0						
0 12 cuboid	2	1	+x = 130.37	-x = .00000E+00	+y = 1000.0	-y = -1000.0 +z
= 1000.0						
0 13 cuboid	3	1	+x = 139.37	-x = .00000E+00	+y = 1000.0	-y = -1000.0 +z
= 1000.0						
0 14 cuboid	5	1	+x = 142.37	-x = .00000E+00	+y = 1000.0	-y = -1000.0 +z
= 1000.0						
0 15 cuboid	5	1	+x = 149.37	-x = .00000E+00	+y = 1000.0	-y = -1000.0 +z
= 1000.0						
0 16 cuboid	5	1	+x = 158.50	-x = .00000E+00	+y = 1000.0	-y = -1000.0 +z
= 1000.0						

```

0 17 cuboid      5 1   +x = 167.60   -x = .00000E+00 +y = 1000.0   -y = -1000.0   +z
= 1000.0      -z = -1000.0
0 18 cuboid      5 1   +x = 176.75   -x = .00000E+00 +y = 1000.0   -y = -1000.0   +z
= 1000.0      -z = -1000.0
0 19 cuboid      5 1   +x = 183.75   -x = .00000E+00 +y = 1000.0   -y = -1000.0   +z
= 1000.0      -z = -1000.0
0 20 cuboid      5 1   +x = 186.75   -x = .00000E+00 +y = 1000.0   -y = -1000.0   +z
= 1000.0      -z = -1000.0
0 21 cuboid      1 1   +x = 226.75   -x = .00000E+00 +y = 1000.0   -y = -1000.0   +z
= 1000.0      -z = -1000.0

```

benchmark problem 16-a1 perturbed state k16a1p1

volumes for those units utilized in this problem

unit	region	geometry region	volume	cumulative volume
1	1	1	1.60000E+08 cm**3	1.60000E+08 cm**3
	2	2	1.20000E+07 cm**3	1.72000E+08 cm**3
	3	3	2.80000E+07 cm**3	2.00000E+08 cm**3
	4	4	3.64000E+07 cm**3	2.36400E+08 cm**3
	5	5	3.64000E+07 cm**3	2.72800E+08 cm**3
	6	6	3.66960E+07 cm**3	3.09496E+08 cm**3
	7	7	2.80000E+07 cm**3	3.37496E+08 cm**3
	8	8	1.20000E+07 cm**3	3.49496E+08 cm**3
	9	9	3.60000E+07 cm**3	3.85496E+08 cm**3
	10	10	2.00000E+07 cm**3	4.05496E+08 cm**3
	11	11	9.60000E+07 cm**3	5.01496E+08 cm**3
	12	12	2.00000E+07 cm**3	5.21496E+08 cm**3
	13	13	3.60000E+07 cm**3	5.57496E+08 cm**3
	14	14	1.20000E+07 cm**3	5.69496E+08 cm**3
	15	15	2.80000E+07 cm**3	5.97496E+08 cm**3
	16	16	3.65040E+07 cm**3	6.34000E+08 cm**3
	17	17	3.64000E+07 cm**3	6.70400E+08 cm**3
	18	18	3.65920E+07 cm**3	7.06992E+08 cm**3
	19	19	2.80000E+07 cm**3	7.34992E+08 cm**3
	20	20	1.20000E+07 cm**3	7.46992E+08 cm**3
	21	21	1.60000E+08 cm**3	9.06992E+08 cm**3

unit	uses	region	mixture	total volume
1	1	1	1	1.60000E+08 cm**3
		2	4	1.20000E+07 cm**3
		3	4	2.80000E+07 cm**3
		4	4	3.64000E+07 cm**3
		5	4	3.64000E+07 cm**3
		6	4	3.66960E+07 cm**3
		7	4	2.80000E+07 cm**3
		8	4	1.20000E+07 cm**3
		9	3	3.60000E+07 cm**3
		10	2	2.00000E+07 cm**3
		11	2	9.60000E+07 cm**3
		12	2	2.00000E+07 cm**3
		13	3	3.60000E+07 cm**3

14	5	1.20000E+07	cm**3
15	5	2.80000E+07	cm**3
16	5	3.65040E+07	cm**3
17	5	3.64000E+07	cm**3
18	5	3.65920E+07	cm**3
19	5	2.80000E+07	cm**3
20	5	1.20000E+07	cm**3
21	1	1.60000E+08	cm**3

total mixture volumes	
mixture	total volume
1	3.20000E+08 cm**3
2	1.36000E+08 cm**3
3	7.20000E+07 cm**3
4	1.89496E+08 cm**3
5	1.89496E+08 cm**3

keno message number k5-123 execution terminated due to completion of the specified number of generations.

benchmark problem 16-a1 perturbed state k16a1p1
lifetime = 6.92827E-07 + or - 9.16060E-10 generation time = 3.79794E-07 + or - 4.53918E-10

no. of initial generations	skipped	average k-effective	deviation	67 per cent confidence interval	95 per cent confidence interval	99 per cent confidence
6		1.00101 + or - .00044		1.00058 to 1.00145	1.00014 to 1.00188	.99970 to 1.00232
7		1.00098 + or - .00044		1.00055 to 1.00142	1.00011 to 1.00186	.99968 to 1.00229
8		1.00101 + or - .00044		1.00057 to 1.00144	1.00013 to 1.00188	.99969 to 1.00232
9		1.00098 + or - .00044		1.00054 to 1.00142	1.00011 to 1.00186	.99967 to 1.00230
10		1.00098 + or - .00044		1.00054 to 1.00142	1.00010 to 1.00186	.99966 to 1.00230
11		1.00100 + or - .00044		1.00056 to 1.00144	1.00012 to 1.00188	.99968 to 1.00232
12		1.00100 + or - .00044		1.00056 to 1.00144	1.00012 to 1.00189	.99968 to 1.00233
13		1.00105 + or - .00044		1.00061 to 1.00149	1.00017 to 1.00193	.99973 to 1.00237
14		1.00105 + or - .00044		1.00061 to 1.00149	1.00017 to 1.00193	.99973 to 1.00237
15		1.00100 + or - .00044		1.00056 to 1.00144	1.00012 to 1.00188	.99968 to 1.00232
20		1.00096 + or - .00044		1.00051 to 1.00140	1.00007 to 1.00185	.99962 to 1.00229
25		1.00104 + or - .00045		1.00059 to 1.00149	1.00014 to 1.00194	.99969 to 1.00239

benchmark problem 16-a1 perturbed state k16a1p1
fluxes for this problem

region 1	region 2	region 3	region 4	region 5	region 6
group flux	percent flux	percent flux	percent flux	percent flux	percent flux
1	4.531E-08 .46	1.513E-07 .43	1.867E-07 .39	2.283E-07 .35	2.549E-07 .34
2	1.499E-08 .55	2.978E-08 .71	3.162E-08 .62	3.502E-08 .55	3.794E-08 .56

benchmark problem 16-a1 perturbed state k16a1p1
fluxes for this problem

region 7	region 8	region 9	region 10	region 11	region 12
group flux	percent flux	percent flux	percent flux	percent flux	percent flux
1	2.368E-07 .29	2.134E-07 .30	1.937E-07 .28	2.096E-07 .30	2.228E-07 .25
2	3.477E-08 .54	3.113E-08 .57	2.875E-08 .55	3.068E-08 .58	3.273E-08 .44

benchmark problem 16-a1 perturbed state k16a1p1
fluxes for this problem

region 13	region 14	region 15	region 16	region 17	region 18
group flux	percent flux	percent flux	percent flux	percent flux	percent flux
1	1.739E-07 .32	1.854E-07 .35	1.997E-07 .36	2.088E-07 .38	2.038E-07 .40
2	2.595E-08 .59	2.743E-08 .69	2.927E-08 .62	3.089E-08 .55	3.085E-08 .61

benchmark problem 16-a1 perturbed state k16a1p1
fluxes for this problem

region 19	region 20	region 21	
group flux	percent flux	percent flux	
1	1.494E-07 .45	1.237E-07 .47	3.701E-08 .50
2	2.562E-08 .67	2.449E-08 .80	1.213E-08 .65

congratulations! you have successfully traversed the perilous path through keno v in 116.84550 minutes

Appendix C: Description of Benchmark Problems

Problem 16-A1

Identification: 16-A1

By: H.L. Dodds, Jr. (University of Tennessee, Knoxville)

Date Submitted: November, 1977

Descriptive Title: Delayed Supercritical Transient; One-Dimensional, Two-Group Neutron Transport Problem in a Fast Reactor

Suggested Function: Test transient one-dimensional neutron transport methods

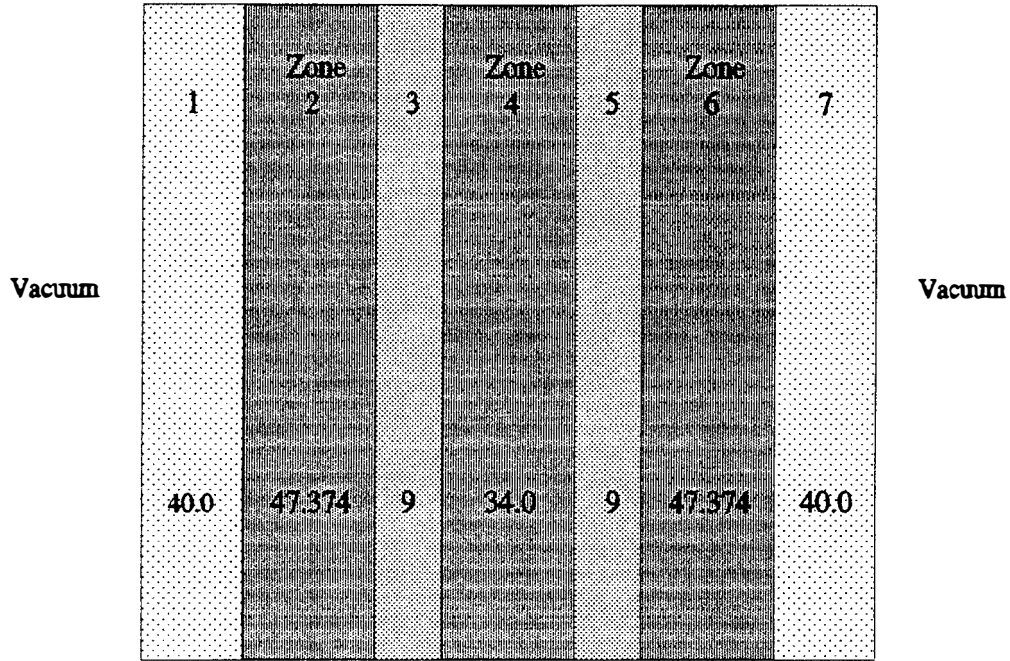
Reactor Configuration: Figure C.1

Data: Initial two-group constants are shown in Table C.1. Delayed neutron parameters, prompt and delayed spectra, and velocities are shown in Table C.2.

Reduction of Source Situation:

1. One-dimensional (slab), two-group neutron transport theory
2. Isotropic scattering
3. Zero return current boundary conditions on external surfaces
4. Steady-state initial conditions
5. Six delayed neutron precursor groups

Initiating Perturbation: At time = 0.0 sec, the density of the material in Zone 2 is increased by 5% and the density in Zone 6 is decreased by 5% resulting in a step insertion of reactivity at $t = 0.0$ sec.



Note: All Dimensions are in Centimeters

Figure C.1: Schematic Diagram of Benchmark Problem 16-A1

Table C.1: Benchmark Problem 16-A1 Initial Two-Group Data

Zone	Group	$\nu\Sigma_f^i$	Σ_t^i	$\Sigma_s^{i\rightarrow i}$	$\Sigma_s^{i\rightarrow j}$
1,7	1	8.3441×10^{-4}	2.411×10^{-1}	2.336×10^{-1}	3.598×10^{-3}
	2	3.2776×10^{-4}	4.172×10^{-1}	4.070×10^{-1}	0.0
2,4,6	1	7.4518×10^{-3}	1.849×10^{-1}	1.777×10^{-1}	2.085×10^{-3}
	2	1.1061×10^{-2}	3.668×10^{-1}	3.537×10^{-1}	0.0
3,5	1	0.0	9.432×10^{-2}	8.571×10^{-2}	1.717×10^{-3}
	2	0.0	1.876×10^{-1}	1.713×10^{-1}	0.0

Table C.2: Benchmark Problem 16-A1 Delayed Neutron Parameters^a

Delayed Neutron Group	Delayed Neutron Fraction, β	Decay Constant, λ
1	8.10×10^{-5}	1.29×10^{-2}
2	6.87×10^{-4}	3.11×10^{-2}
3	6.12×10^{-4}	1.34×10^{-1}
4	1.14×10^{-3}	3.31×10^{-1}
5	5.12×10^{-4}	1.26
6	1.70×10^{-4}	3.21

^aPrompt and delayed neutron spectra are identical with $\chi_1 = 1.0$ and $\chi_2 = 0.0$.
Also, $1/v_1 = 1.851 \times 10^{-9}$ sec/cm and $1/v_2 = 1.088 \times 10^{-8}$ sec/cm.

Expected Primary Results:

1. Initial k-eff and initial scalar flux distribution for each group.
2. Convergence requirements on flux (and eigenvalue) if an iterative solution is used.
3. Total reactor power versus time (normalized so that total power = 1.0 MW at t = 0.0).
4. Time-dependent group flux distributions.
5. Sensitivity of results to time step size.
6. CPU time, I/O time, and core storage requirements.

Possible Additional Results:

7. Zone-averaged power fractions versus time.
8. Sensitivity of results to spatial mesh size.
9. Sensitivity of results to angular quadrature (if discrete ordinates method).

The initial configuration is made critical by dividing the production cross sections by k-eff, and the initial precursor concentrations are in equilibrium with the initial critical flux distribution.

Based on preliminary static k-eff calculations of the initial critical configuration using ANISN³², an S₄ quadrature with 114 spatial intervals (as defined in Tables C.3 and C.4) is a sufficiently accurate representation for the angular and spatial discretization. Specifically, by using a finer spatial mesh (i.e., 228 intervals), k-eff changed by 0.0001 and using an S₈ and S₁₆ quadrature, k-eff changed by 0.0003 and 0.0003, respectively. Therefore, it is suggested that the "Expected Primary Results" given above be obtained initially using the discretization indicated in Tables C.3 and C.4 if the conventional discrete ordinates method is used.

Table C.3: S₄ Angular Quadrature

Cosine (μ)	Weight
-1.0	0.00
-0.788675	0.25
-0.211325	0.25
+0.211325	0.25
+0.788675	0.25

Table C.4: Spatial Mesh

Zone	Number of Intervals
1	20
2	24
3	5
4	16
5	5
6	24
7	20

Problem 16-A2

- Identification: 16-A2
- By: H.L. Dodds, Jr. (University of Tennessee, Knoxville)
- Date Submitted: November, 1977
- Descriptive Title: Prompt Supercritical Transient; One-Dimensional, Two-Group Neutron Transport Problem in a Fast Reactor
- Suggested Function: Test transient one-dimensional neutron transport methods
- Reactor Configuration: Same as Problem 16-A1
- Data: Same as Problem 16-A1
- Reduction of Source Situation:
1. One-dimensional (slab), two-group neutron transport theory
 2. Isotropic scattering
 3. Zero return current boundary conditions on external surfaces
 4. Steady-state initial conditions
 5. Six delayed neutron precursor groups
- Initiating Perturbation: At time = 0.0 sec, the density of the material in Zone 2 is increased by 10% and the density in Zone 6 is decreased by 10% resulting in a step insertion of reactivity at $t = 0.0$ sec.

Problem 16-A3

Identification: 16-A3

By: H.L. Dodds, Jr. (University of Tennessee, Knoxville)

Date Submitted: November, 1977

Descriptive Title: Transient Initially Prompt Supercritical, then Subcritical;
One-Dimensional, Two-Group Neutron Transport Problem
in a Fast Reactor

Suggested Function: Same as Problem 16-A1

Reactor Configuration: Same as Problem 16-A1

Data: Same as Problem 16-A1

Reduction of Source Situation:

1. One-dimensional (slab), two-group neutron transport theory
2. Isotropic scattering
3. Zero return current boundary conditions on external surfaces
4. Steady-state initial conditions
5. Six delayed neutron precursor groups

Initiating Perturbation: At time = 0.0 sec, the material in Zone 5 is changed from a mixture of sodium and control rod materials to 100% sodium (i.e., control rod bank ejection). Then, at $t=0.0001$ sec, the material in Zone 3 is changed from a mixture of sodium and control rod materials to 100% control rod material (i.e., full insertion of the control rod bank). The cross sections for sodium and for the control rod material are shown in Table C.5.

Table C.5: Two-Group Constants for Sodium and Control Rod Materials

Material	Energy Group	Σ_t^i	$\Sigma_s^{i \rightarrow i}$	$\Sigma_s^{i \rightarrow j}$
Sodium	1	6.830×10^{-2}	6.3293×10^{-2}	1.294×10^{-3}
	2	1.257×10^{-1}	1.21099×10^{-1}	0.0
Control Rod	1	1.795×10^{-1}	1.59078×10^{-1}	3.101×10^{-3}
	2	3.903×10^{-1}	3.35661×10^{-1}	0.0

Problem 16-A6

- Identification: 16-A6
- By: H.L. Dodds, Jr. (University of Tennessee, Knoxville)
- Date Submitted: May, 1978
- Descriptive Title: Material Motion Transient Initially Prompt Supercritical (Step Perturbation), then Subcritical (Ramp Perturbation); One-Dimensional, Two-Group Neutron Transport Problem in a Fast Reactor
- Suggested Function: Same as Problem 16-A1
- Reactor Configuration: Same as Problem 16-A1
- Data: Same as Problem 16-A1
- Reduction of Source Situation:
1. One-dimensional (slab), two-group neutron transport theory
 2. Isotropic scattering
 3. Zero return current boundary conditions on external surfaces
 4. Steady-state initial conditions
 5. Six delayed neutron precursor groups
- Initiating Perturbation: At time = 0.0 sec, the mixture of sodium and control rod material in Zone 5 is changed (a decrease in rod material and an increase in sodium) resulting in the cross sections for Zone 5 at $t=0.0$ sec given in Table C.6. In addition, for the time interval between $t = 0.0$ sec and $t = 0.5$ sec, the densities of the materials in Zones 1, 2, 4, 6, and 7 are changed linearly (i.e., materials motion) resulting in final cross sections for each zone at $t = 0.5$ sec as shown in Table C.7.

Table C.6: Two-Group Constants for Step Perturbation in Zone 5

Energy Group	Σ_t^i	$\Sigma_s^{i \rightarrow i}$	$\Sigma_s^{i \rightarrow j}$
1	9.05399×10^{-2}	8.24499×10^{-2}	1.6550×10^{-3}
2	1.7860×10^{-1}	1.640×10^{-1}	0.0

Table C.7: Two-Group Constants for Ramp Perturbations

Zone	Group	$\nu \Sigma_f^i$	Σ_t^i	$\Sigma_s^{i \rightarrow i}$	$\Sigma_s^{i \rightarrow j}$
1	1	1.71696×10^{-3}	2.62999×10^{-1}	2.54691×10^{-1}	3.8449×10^{-3}
	2	1.63779×10^{-3}	4.60642×10^{-1}	4.48897×10^{-1}	0.0
2	1	6.70661×10^{-3}	1.6641×10^{-1}	1.5994×10^{-1}	1.8765×10^{-3}
	2	9.95507×10^{-3}	3.3012×10^{-1}	3.18349×10^{-1}	0.0
4,6	1	2.98072×10^{-3}	7.39599×10^{-2}	7.10843×10^{-2}	8.3399×10^{-3}
	2	4.42448×10^{-3}	1.4672×10^{-1}	1.41488×10^{-1}	0.0
7	1	9.93014×10^{-3}	4.66791×10^{-1}	4.50559×10^{-1}	6.1429×10^{-3}
	2	1.38292×10^{-2}	8.64919×10^{-1}	8.38759×10^{-1}	0.0

Problem 16-A7

Identification: 16-A7

By: H.L. Dodds, Jr. (University of Tennessee, Knoxville)

Date Submitted: May, 1978

Descriptive Title: Material Motion Transient Initially Prompt Supercritical (Step Perturbation), then Subcritical (Step Perturbation); One-Dimensional Two-Group Neutron Transport Problem in a Fast Reactor

Suggested Function: Same as Problem 16-A1

Reactor Configuration: Same as Problem 16-A1

Data: Same as Problem 16-A1

Reduction of Source Situation:

1. One-dimensional (slab), two-group neutron transport theory
2. Isotropic scattering
3. Zero return current boundary conditions on external surfaces
4. Steady-state initial conditions
5. Six delayed neutron precursor groups

Initiating Perturbation: This perturbation is identical to the perturbation for Problem 16-A6 except for the ramp representing material motion. Specifically, the ramp between 0.0 sec and 0.5 sec is replaced by a step which occurs at $t = 0.01$ sec. The magnitude of this step change at $t = 0.01$ sec is determined by the cross sections given in Table C.7.

Problem 14-A2

Identification: 14-A2

By: S. Langenbuch (GRS-Munich)
W. Werner (GRS-Munich)

Date Submitted: June, 1976

Descriptive Title: Super Prompt-critical Transient; Three-dimensional, Two-group Neutron Diffusion Problem, with Adiabatic Heatup and Doppler Feedback in a Thermal Reactor

Suggested Function: Test 3-D Neutron Kinetics Solution, Especially for Coarse Mesh Methods

Reactor Configuration: Figure C.2 and C.3

Data: Initial two-group constants are shown in Table C.8. Delayed neutron parameters, prompt and delayed spectra, and velocities are shown in Table C.9.

Reduction of Source Situation:

1. Three-dimensional (x-y-z), two-group diffusion theory
2. Two delayed neutron precursor groups
3. Adiabatic heatup:

$$\alpha[\Sigma_{f_1}(\bar{x},t)\phi_1(\bar{x},t) + \Sigma_{f_2}(\bar{x},t)\phi_2(\bar{x},t)] = \frac{\partial}{\partial t}T(\bar{x},t)$$

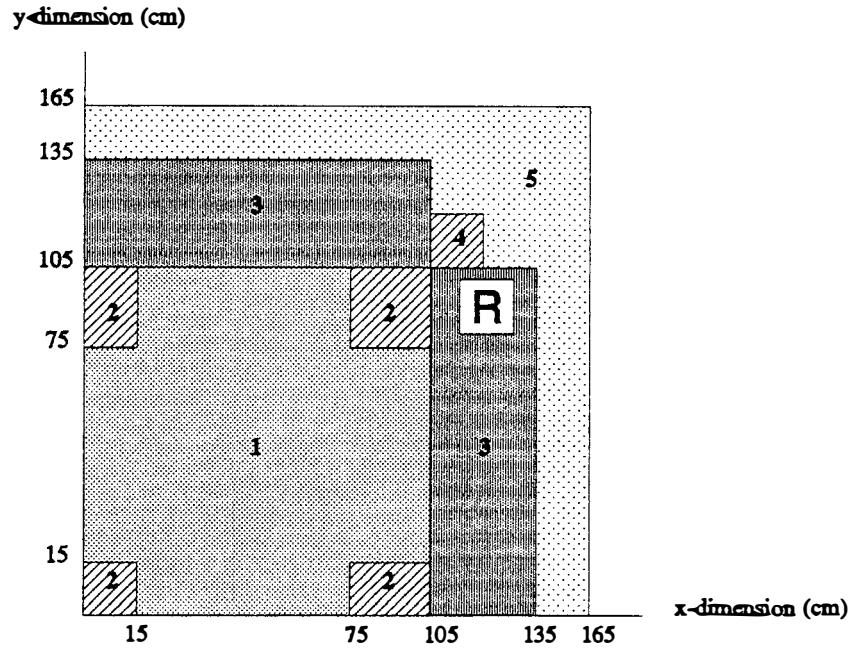


Figure C.2: Quadrant of Reactor Horizontal Cross Section for Benchmark 14-A2

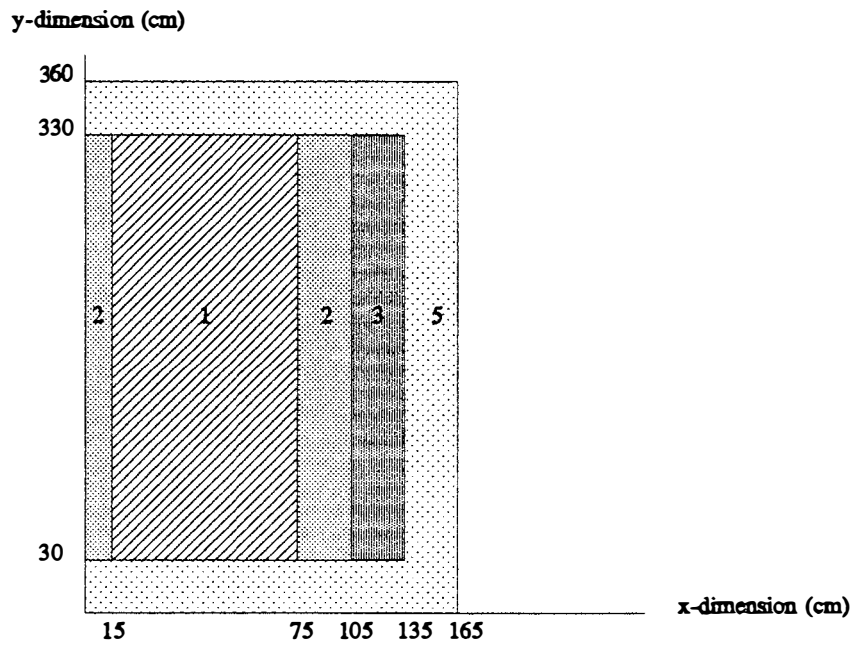


Figure C.3: Reactor Vertical Cross Section for Benchmark 14-A2

Table C.8: Benchmark Problem 14-A2 Delayed Neutron Parameters^a

Delayed Neutron Group	Delayed Neutron Fraction, β	Decay Constant, λ
1	5.40×10^{-3}	6.54×10^{-3}
2	1.087×10^{-3}	1.35

^aPrompt and delayed neutron spectra are identical with $\chi_1 = 1.0$ and $\chi_2 = 0.0$.
 Also, $1/v_1 = 3.333 \times 10^{-6}$ sec/cm and $1/v_2 = 3.333 \times 10^{-4}$ sec/cm.

Table C.9: Benchmark Problem 14-A2 Initial Two-Group Data

Zone	Material	Group	D_i	Σ_s^i	$\nu \Sigma_f^i$	Σ_s^{1-2}
1	Fuel 1 with rod	1	1.255	8.252×10^{-3}	4.602×10^{-3}	2.533×10^{-2}
		2	0.211	1.003×10^{-1}	1.091×10^{-1}	
2	Fuel 2 without rod	1	1.268	7.181×10^{-3}	4.609×10^{-3}	2.767×10^{-2}
		2	0.1902	7.047×10^{-2}	8.675×10^{-2}	
3	Fuel 2 with rod	1	1.259	8.002×10^{-3}	4.663×10^{-3}	2.617×10^{-2}
		2	0.2091	8.344×10^{-2}	1.021×10^{-1}	
4	Fuel 2 without rod	1	1.259	8.002×10^{-3}	4.663×10^{-3}	2.617×10^{-2}
		2	0.2091	7.332×10^{-2}	1.021×10^{-1}	
5	Reflector	1	1.257	6.034×10^{-4}	0.0	4.754×10^{-2}
		2	0.1592	1.911×10^{-2}	0.0	

4. Doppler feedback:

$$\Sigma_{a_1}(\bar{x},t) = \Sigma_{a_1}(\bar{x},t=0) [1 + \gamma(\sqrt{T(\bar{x},t)} - \sqrt{T_0})]$$

5. Power:

$$P(\bar{x},t) = \epsilon[\Sigma_{f_1}(\bar{x},t)\phi_1(\bar{x},t) + \Sigma_{f_2}(\bar{x},t)\phi_2(\bar{x},t)]$$

Data for feedback model:

$\alpha = 3.83 \times 10^{-11} \text{ K cm}^3$	conversion factor
$\gamma = 3.034 \times 10^{-3} \text{ K}^{1/2}$	feedback constant
$\epsilon = 3.204 \times 10^{-11} \text{ W sec / fission}$	energy conversion factor

Initiating Perturbation:

The initial configuration is made critical by dividing the production cross sections by k_{eff} .

The initial flux distribution is normalized such that the average power density is:

$$\bar{P} = \frac{\epsilon}{V_{\text{core}}} \int (\Sigma_{f_1}\phi_1 + \Sigma_{f_2}\phi_2) dV = 1.0 \times 10^{-6} \text{ Wcm}^{-3}$$

Further, the initial precursor concentrations are in equilibrium with the initial critical flux distribution. Finally, the initial temperature is 300K.

Cross Section Perturbation:

$$\frac{\Sigma_{a_2}(t)}{\Sigma_{a_2}(t=0)} = 1 - 0.0606184t \quad t \leq 2$$
$$0.8787631 \quad t \geq 2$$

where, $t =$ time (sec).

Appendix D: Description of Mesh Intervals

The number of mesh intervals for Benchmark Problems 16-A1, 16-A2, and 16-A3 are 21, 32, and 29, respectively. The mesh intervals are defined in detail in Tables D.1, D.2, and D.3 as x-dimensions since these problems are one-dimensional. Note that the x-dimensions are given as ranges so that the top and bottom numbers correspond to starting and ending points for each mesh interval, respectively. Similar information for Benchmark Problems 16-A6 and 16-A7 (36 intervals each) is presented in Table D.4. Note that the y and z dimensions are ± 1000.0 cm for each of the Benchmark 16 problems. Also given in the tables is the reactor zone (refer to Figure 3 on page 25) corresponding to each mesh interval.

The 217 mesh intervals for Benchmark Problem 14-A2 are given in Table D.5 as x-dimensions, y-dimensions, and z-dimensions since the problem is three-dimensional. Note that the dimensions are given as ranges so that the top and bottom numbers correspond to starting and ending points for each mesh interval, respectively. Also given in Table D.5 is the reactor zone (refer to Figures 11 and 12 on pages 39 and 40) corresponding to each mesh interval.

Table D.1: Mesh Intervals for Benchmark Problem 16-A1

Mesh Interval	x-dimension (cm)	Zone
1	0.0 40.0	1
2	40.0 43.0	2
3	43.0 50.0	2
4	50.0 59.1	2
5	59.1 68.2	2
6	68.2 77.374	2
7	77.374 84.374	2
8	84.374 87.374	2
9	87.374 96.374	3
10	96.374 101.374	4
11	101.374 125.374	4
12	125.374 130.374	4
13	130.374 139.374	5
14	139.374 142.374	6
15	142.374 149.374	6

16	149.374 158.5	6
17	158.5 167.6	6
18	167.6 176.748	6
19	176.748 183.748	6
20	183.748 186.748	6
21	186.748 226.748	7

Table D.2: Mesh Intervals for Benchmark Problem 16-A2

Mesh Interval	x-dimension (cm)	Zone
1	0.0 5.0	1
2	5.0 20.0	1
3	20.0 35.0	1
4	35.0 40.0	1
5	40.0 43.0	2
6	43.0 50.0	2
7	50.0 59.1	2
8	59.1 68.2	2

9	68.2 77.374	2
10	77.374 84.374	2
11	84.374 87.374	2
12	87.374 89.374	3
13	89.374 94.374	3
14	94.374 96.374	3
15	96.374 101.374	4
16	101.374 113.374	4
17	113.374 125.374	4
18	125.374 130.374	4
19	130.374 132.374	5
20	132.374 137.374	5
21	137.374 139.374	5
22	139.374 142.374	6
23	142.374 149.374	6
24	149.374 158.5	6
25	158.5 167.6	6

26	167.6 176.748	6
27	176.748 183.748	6
28	183.748 186.748	6
29	186.748 191.748	7
30	191.748 206.748	7
31	206.748 221.748	7
32	221.748 226.748	7

Table D.3: Mesh Intervals for Benchmark Problem 16-A3

Mesh Interval	x-dimension (cm)	Zone
1	0.0 10.0	1
2	10.0 30.0	1
3	30.0 40.0	1
4	40.0 45.0	2
5	45.0 55.0	2
6	55.0 72.374	2
7	72.374 82.374	2

8	82.374 87.374	2
9	87.374 88.374	3
10	88.374 90.374	3
11	90.374 93.374	3
12	93.374 95.374	3
13	95.374 96.374	3
14	96.374 101.374	4
15	101.374 125.374	4
16	125.374 130.374	4
17	130.374 131.374	5
18	131.374 133.374	5
19	133.374 136.374	5
20	136.374 138.374	5
21	138.374 139.374	5
22	139.374 144.374	6
23	144.374 154.374	6
24	154.374 171.748	6

25	171.748 181.748	6
26	181.748 186.748	6
27	186.748 196.748	7
28	196.748 216.748	7
29	216.748 226.748	7

Table D.4: Mesh Intervals for Benchmark Problems 16-A6 and 16-A7

Mesh Interval	x-dimension (cm)	Zone
1	0.0 5.0	1
2	5.0 10.0	1
3	10.0 20.0	1
4	20.0 30.0	1
5	30.0 35.0	1
6	35.0 40.0	1
7	40.0 43.0	2
8	43.0 50.0	2
9	50.0 59.1	2

10	59.1 68.2	2
11	68.2 77.374	2
12	77.374 84.374	2
13	84.374 87.374	2
14	87.374 96.374	3
15	96.374 101.374	4
16	101.374 106.374	4
17	106.374 115.374	4
18	115.374 125.374	4
19	125.374 130.374	4
20	130.374 131.374	5
21	131.374 134.374	5
22	134.374 138.374	5
23	138.374 139.374	5
24	139.374 142.374	6
25	142.374 149.374	6
26	149.374 158.5	6

27	158.5 167.6	6
28	167.6 176.748	6
29	176.748 183.748	6
30	183.748 186.748	6
31	186.748 191.748	7
32	191.748 196.748	7
33	196.748 206.748	7
34	206.748 216.748	7
35	216.748 221.748	7
36	221.748 226.748	7

Table D.5: Mesh Intervals for Benchmark Problem 14-A2

Mesh Interval	x-dimensions (cm)	y-dimensions (cm)	z-dimensions (cm)	Zone
1	0.0 15.0	0.0 15.0	30.0 80.0	2
2	15.0 75.0	0.0 15.0	30.0 80.0	1
3	75.0 105.0	0.0 15.0	30.0 80.0	2
4	105.0 135.0	0.0 15.0	30.0 80.0	3

5	0.0 75.0	15.0 45.0	30.0 80.0	1
6	75.0 105.0	15.0 45.0	30.0 80.0	1
7	105.0 135.0	15.0 45.0	30.0 80.0	3
8	0.0 75.0	45.0 65.0	30.0 80.0	1
9	75.0 105.0	45.0 65.0	30.0 80.0	1
10	105.0 135.0	45.0 65.0	30.0 80.0	3
11	0.0 60.0	60.0 75.0	30.0 80.0	1
12	60.0 90.0	60.0 75.0	30.0 80.0	1
13	90.0 105.0	60.0 75.0	30.0 80.0	1
14	105.0 135.0	60.0 75.0	30.0 80.0	3
15	0.0 15.0	75.0 90.0	30.0 80.0	2
16	15.0 45.0	75.0 90.0	30.0 80.0	1
17	45.0 75.0	75.0 90.0	30.0 80.0	1
18	75.0 90.0	75.0 90.0	30.0 80.0	2
19	90.0 105.0	75.0 90.0	30.0 80.0	2
20	105.0 120.0	75.0 90.0	30.0 80.0	3
21	120.0 135.0	75.0 90.0	30.0 80.0	3

22	0.0 15.0	90.0 105.0	30.0 80.0	2
23	15.0 45.0	90.0 105.0	30.0 80.0	1
24	45.0 75.0	90.0 105.0	30.0 80.0	1
25	75.0 90.0	90.0 105.0	30.0 80.0	2
26	90.0 105.0	90.0 105.0	30.0 80.0	2
27	105.0 120.0	90.0 105.0	30.0 80.0	3
28	120.0 135.0	90.0 105.0	30.0 80.0	3
29	0.0 60.0	105.0 120.0	30.0 80.0	3
30	60.0 90.0	105.0 120.0	30.0 80.0	3
31	90.0 105.0	105.0 120.0	30.0 80.0	3
32	105.0 120.0	105.0 120.0	30.0 80.0	4
33	120.0 135.0	105.0 120.0	30.0 80.0	5
34	0.0 75.0	120.0 135.0	30.0 80.0	3
35	75.0 105.0	120.0 135.0	30.0 80.0	3
36	105.0 135.0	120.0 135.0	30.0 80.0	5
37	0.0 15.0	0.0 15.0	80.0 130.0	2
38	15.0 75.0	0.0 15.0	80.0 130.0	1

39	75.0 105.0	0.0 15.0	80.0 130.0	2
40	105.0 135.0	0.0 15.0	80.0 130.0	3
41	0.0 75.0	15.0 45.0	80.0 130.0	1
42	75.0 105.0	15.0 45.0	80.0 130.0	1
43	105.0 135.0	15.0 45.0	80.0 130.0	3
44	0.0 75.0	45.0 60.0	80.0 130.0	1
45	75.0 105.0	45.0 60.0	80.0 130.0	1
46	105.0 135.0	45.0 60.0	80.0 130.0	3
47	0.0 60.0	60.0 75.0	80.0 130.0	1
48	60.0 90.0	60.0 75.0	80.0 130.0	1
49	90.0 105.0	60.0 75.0	80.0 130.0	1
50	105.0 135.0	60.0 75.0	80.0 130.0	3
51	0.0 15.0	75.0 90.0	80.0 130.0	2
52	15.0 45.0	75.0 90.0	80.0 130.0	1
53	45.0 75.0	75.0 90.0	80.0 130.0	1
54	75.0 90.0	75.0 90.0	80.0 130.0	2
55	90.0 105.0	75.0 90.0	80.0 130.0	2

56	105.0 120.0	75.0 90.0	80.0 130.0	3
57	120.0 135.0	75.0 90.0	80.0 130.0	3
58	0.0 15.0	90.0 105.0	80.0 130.0	2
59	15.0 45.0	90.0 105.0	80.0 130.0	1
60	45.0 75.0	90.0 105.0	80.0 130.0	1
61	75.0 90.0	90.0 105.0	80.0 130.0	2
62	90.0 105.0	90.0 105.0	80.0 130.0	2
63	105.0 120.0	90.0 105.0	80.0 130.0	3
64	120.0 135.0	90.0 105.0	80.0 130.0	3
65	0.0 60.0	105.0 120.0	80.0 130.0	3
66	60.0 90.0	105.0 120.0	80.0 130.0	3
67	90.0 105.0	105.0 120.0	80.0 130.0	3
68	105.0 120.0	105.0 120.0	80.0 130.0	4
69	120.0 135.0	105.0 120.0	80.0 130.0	5
70	0.0 75.0	120.0 135.0	80.0 130.0	3
71	75.0 105.0	120.0 135.0	80.0 130.0	3
72	105.0 135.0	120.0 135.0	80.0 130.0	5

73	0.0 15.0	0.0 15.0	130.0 180.0	2
74	15.0 75.0	0.0 15.0	130.0 180.0	1
75	75.0 105.0	0.0 15.0	130.0 180.0	2
76	105.0 135.0	0.0 15.0	130.0 180.0	3
77	0.0 75.0	15.0 45.0	130.0 180.0	1
78	75.0 105.0	15.0 45.0	130.0 180.0	1
79	105.0 135.0	15.0 45.0	130.0 180.0	3
80	0.0 75.0	45.0 60.0	130.0 180.0	1
81	75.0 105.0	45.0 60.0	130.0 180.0	1
82	105.0 135.0	45.0 60.0	130.0 180.0	3
83	0.0 60.0	60.0 75.0	130.0 180.0	1
84	60.0 90.0	60.0 75.0	130.0 180.0	1
85	90.0 105.0	60.0 75.0	130.0 180.0	1
86	105.0 135.0	60.0 75.0	130.0 180.0	3
87	0.0 15.0	75.0 90.0	130.0 180.0	2
88	15.0 45.0	75.0 90.0	130.0 180.0	1
89	45.0 75.0	75.0 90.0	130.0 180.0	1

90	75.0 90.0	75.0 90.0	130.0 180.0	2
91	90.0 105.0	75.0 90.0	130.0 180.0	2
92	105.0 120.0	75.0 90.0	130.0 180.0	3
93	120.0 135.0	75.0 90.0	130.0 180.0	3
94	0.0 15.0	90.0 105.0	130.0 180.0	2
95	15.0 45.0	90.0 105.0	130.0 180.0	1
96	45.0 75.0	90.0 105.0	130.0 180.0	1
97	75.0 90.0	90.0 105.0	130.0 180.0	2
98	90.0 105.0	90.0 105.0	130.0 180.0	2
99	105.0 120.0	90.0 105.0	130.0 180.0	3
100	120.0 135.0	90.0 105.0	130.0 180.0	3
101	0.0 60.0	105.0 120.0	130.0 180.0	3
102	60.0 90.0	105.0 120.0	130.0 180.0	3
103	90.0 105.0	105.0 120.0	130.0 180.0	3
104	105.0 120.0	105.0 120.0	130.0 180.0	4
105	120.0 135.0	105.0 120.0	130.0 180.0	5
106	0.0 75.0	120.0 135.0	130.0 180.0	3

107	75.0 105.0	120.0 135.0	130.0 180.0	3
108	105.0 135.0	120.0 135.0	130.0 180.0	5
109	0.0 15.0	0.0 15.0	180.0 230.0	2
110	15.0 75.0	0.0 15.0	180.0 230.0	1
111	75.0 105.0	0.0 15.0	180.0 230.0	2
112	105.0 135.0	0.0 15.0	180.0 230.0	3
113	0.0 75.0	15.0 45.0	180.0 230.0	1
114	75.0 105.0	15.0 45.0	180.0 230.0	1
115	105.0 135.0	15.0 45.0	180.0 230.0	3
116	0.0 75.0	45.0 60.0	180.0 230.0	1
117	75.0 105.0	45.0 60.0	180.0 230.0	1
118	105.0 135.0	45.0 60.0	180.0 230.0	3
119	0.0 60.0	60.0 75.0	180.0 230.0	1
120	60.0 90.0	60.0 75.0	180.0 230.0	1
121	90.0 105.0	60.0 75.0	180.0 230.0	1
122	105.0 135.0	60.0 75.0	180.0 230.0	3
123	0.0 15.0	75.0 90.0	180.0 230.0	2

124	15.0 45.0	75.0 90.0	180.0 230.0	1
125	45.0 75.0	75.0 90.0	180.0 230.0	1
126	75.0 90.0	75.0 90.0	180.0 230.0	2
127	90.0 105.0	75.0 90.0	180.0 230.0	2
128	105.0 120.0	75.0 90.0	180.0 230.0	3
129	120.0 135.0	75.0 90.0	180.0 230.0	3
130	0.0 15.0	90.0 105.0	180.0 230.0	2
131	15.0 45.0	90.0 105.0	180.0 230.0	1
132	45.0 75.0	90.0 105.0	180.0 230.0	1
133	75.0 90.0	90.0 105.0	180.0 230.0	2
134	90.0 105.0	90.0 105.0	180.0 230.0	2
135	105.0 120.0	90.0 105.0	180.0 230.0	3
136	120.0 135.0	90.0 105.0	180.0 230.0	3
137	0.0 60.0	105.0 120.0	180.0 230.0	3
138	60.0 90.0	105.0 120.0	180.0 230.0	3
139	90.0 105.0	105.0 120.0	180.0 230.0	3
140	105.0 120.0	105.0 120.0	180.0 230.0	4

141	120.0 135.0	105.0 120.0	180.0 230.0	5
142	0.0 75.0	120.0 135.0	180.0 230.0	3
143	75.0 105.0	120.0 135.0	180.0 230.0	3
144	105.0 135.0	120.0 135.0	180.0 230.0	5
145	0.0 15.0	0.0 15.0	230.0 280.0	2
146	15.0 75.0	0.0 15.0	230.0 280.0	1
147	75.0 105.0	0.0 15.0	230.0 280.0	2
148	105.0 135.0	0.0 15.0	230.0 280.0	3
149	0.0 75.0	15.0 45.0	230.0 280.0	1
150	75.0 105.0	15.0 45.0	230.0 280.0	1
151	105.0 135.0	15.0 45.0	230.0 280.0	3
152	0.0 75.0	45.0 60.0	230.0 280.0	1
153	75.0 105.0	45.0 60.0	230.0 280.0	1
154	105.0 135.0	45.0 60.0	230.0 280.0	3
155	0.0 60.0	60.0 75.0	230.0 280.0	1
156	60.0 90.0	60.0 75.0	230.0 280.0	1
157	90.0 105.0	60.0 75.0	230.0 280.0	1

158	105.0 135.0	60.0 75.0	230.0 280.0	3
159	0.0 15.0	75.0 90.0	230.0 280.0	2
160	15.0 45.0	75.0 90.0	230.0 280.0	1
161	45.0 75.0	75.0 90.0	230.0 280.0	1
162	75.0 90.0	75.0 90.0	230.0 280.0	2
163	90.0 105.0	75.0 90.0	230.0 280.0	2
164	105.0 120.0	75.0 90.0	230.0 280.0	3
165	120.0 135.0	75.0 90.0	230.0 280.0	3
166	0.0 15.0	90.0 105.0	230.0 280.0	2
167	15.0 45.0	90.0 105.0	230.0 280.0	1
168	45.0 75.0	90.0 105.0	230.0 280.0	1
169	75.0 90.0	90.0 105.0	230.0 280.0	2
170	90.0 105.0	90.0 105.0	230.0 280.0	2
171	105.0 120.0	90.0 105.0	230.0 280.0	3
172	120.0 135.0	90.0 105.0	230.0 280.0	3
173	0.0 60.0	105.0 120.0	230.0 280.0	3
174	60.0 90.0	105.0 120.0	230.0 280.0	3

175	90.0 105.0	105.0 120.0	230.0 280.0	3
176	105.0 120.0	105.0 120.0	230.0 280.0	4
177	120.0 135.0	105.0 120.0	230.0 280.0	5
178	0.0 75.0	120.0 135.0	230.0 280.0	3
179	75.0 105.0	120.0 135.0	230.0 280.0	3
180	105.0 135.0	120.0 135.0	230.0 280.0	5
181	0.0 15.0	0.0 15.0	280.0 330.0	2
182	15.0 75.0	0.0 15.0	280.0 330.0	1
183	75.0 105.0	0.0 15.0	280.0 330.0	2
184	105.0 135.0	0.0 15.0	280.0 330.0	3
185	0.0 75.0	15.0 45.0	280.0 330.0	1
186	75.0 105.0	15.0 45.0	280.0 330.0	1
187	105.0 135.0	15.0 45.0	280.0 330.0	3
188	0.0 75.0	45.0 60.0	280.0 330.0	1
189	75.0 105.0	45.0 60.0	280.0 330.0	1
190	105.0 135.0	45.0 60.0	280.0 330.0	3
191	0.0 60.0	60.0 75.0	280.0 330.0	1

192	60.0 90.0	60.0 75.0	280.0 330.0	1
193	90.0 105.0	60.0 75.0	280.0 330.0	1
194	105.0 135.0	60.0 75.0	280.0 330.0	3
195	0.0 15.0	75.0 90.0	280.0 330.0	2
196	15.0 45.0	75.0 90.0	280.0 330.0	1
197	45.0 75.0	75.0 90.0	280.0 330.0	1
198	75.0 90.0	75.0 90.0	280.0 330.0	2
199	90.0 105.0	75.0 90.0	280.0 330.0	2
200	105.0 120.0	75.0 90.0	280.0 330.0	3
201	120.0 135.0	75.0 90.0	280.0 330.0	3
202	0.0 15.0	90.0 105.0	280.0 330.0	2
203	15.0 45.0	90.0 105.0	280.0 330.0	1
204	45.0 75.0	90.0 105.0	280.0 330.0	1
205	75.0 90.0	90.0 105.0	280.0 330.0	2
206	90.0 105.0	90.0 105.0	280.0 330.0	2
207	105.0 120.0	90.0 105.0	280.0 330.0	3
208	120.0 135.0	90.0 105.0	280.0 330.0	3

209	0.0 60.0	105.0 120.0	280.0 330.0	3
210	60.0 90.0	105.0 120.0	280.0 330.0	3
211	90.0 105.0	105.0 120.0	280.0 330.0	3
212	105.0 120.0	105.0 120.0	280.0 330.0	4
213	120.0 135.0	105.0 120.0	280.0 330.0	5
214	0.0 75.0	120.0 135.0	280.0 330.0	3
215	75.0 105.0	120.0 135.0	280.0 330.0	3
216	105.0 135.0	120.0 135.0	280.0 330.0	5
217	135.0 165.0	135.0 165.0	0.0 360.0	5

Vita

Charles Lewis Bentley was born in Elizabethtown, Kentucky on December 22, 1968. He graduated from East Hardin High School in May 1987. The following August he entered Western Kentucky University where he received a Bachelor of Science degree in Physics in May 1990.

In August 1990 he accepted a Pasqua Nuclear Engineering Scholarship at the University of Tennessee, Knoxville. In May 1992 he received the degree of Bachelor of Science in Nuclear Engineering.

In June 1992 he accepted a Research Fellowship from the Nuclear Engineering/Health Physics Fellowship Program sponsored by the U.S. Department of Energy. In August 1992 he began graduate study at the University of Tennessee toward a Master of Science degree in Nuclear Engineering. This degree was awarded in August 1994.

In August 1994 he began pursuing a Doctor of Philosophy degree in Nuclear Engineering which was awarded in December 1996.