THERMOMETRIC MEASUREMENT OF DEPTH

by

PRIVATDOZENT DR. G. WÜST, CURATOR OF THE Institut und Museum für Meereskunde of THE UNIVERSITY OF BERLIN.

From the technical point of view, the problem of deep-sea sounding seems nowadays to have been solved to the last detail, thanks to the development of methods of sounding by wire and the perfection attained in methods of echo-sounding. But with respect to the sources of error in soundings as measured by wire and as observed by echo, i. e. the question of reducing the measured depth to the true depth, we are still only at the point where we started. To anyone with personal experience of the continually changing external conditions of deep-sea sounding (sea, current, angle of wire, drift, etc.) it is obvious that the question of the sources of error cannot be solved by theoretical considerations, and that a conclusive representation of their values can only be obtained by means of observations. In this connection it is of very great value to take strictly simultaneous soundings by wire and by echo at the same position of the ship, as was done, for example, at 322 stations during the Meteor Expedition. But no less important is the checking of the two soundings by a third indirect method of sounding, independent of the first two. It is well known that the practical needs of navigation, viz. to be able to obtain depth data with the ship steaming at full speed, have led to the discovery of a whole collection of appliances for the indirect measurement of depths, mainly based on the principle of measuring the pressure; but either they are capable of use up to 200 m. only, or they give approximate values only at great depths.

The fact that, as a result of experience of the thermometric method of depth measurement gained by the German Atlantic Expedition in the hydrographic and exploring vessel *Meteor*, we possess an indirect method of sounding which enables us to sound with sufficient accuracy at any depth up to 6,000 m., is thus of importance. In the course of this expedition the method was employed regularly for serial oceanographic measurements, and worked extremely well. At the author's instigation the method was employed more often, even with soundings by wire, during the latter stages of the expedition (Profiles X to XIV) in tropical waters. After all these trials there was no longer any doubt that the thermometric method of depth measurement is a valuable auxiliary for finding the true depth when sounding by wire, and at the same time for determining the sources of error in the depth by wire (due to the slope of the wire) and in the depth by echo (due to the reduction).

Reverting to the detailed explanations given by the author in Vol. IV of the *Meteor* reports (1932), the following is a summary of the thermometric method of depth measurement and the results obtained thereby during the *Meteor* expedition. To this have been added the principal results of a study

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of the mean relationship between depth by wire and true depth for different angles of wire, as obtained with regard to both the serial oceanographic measurements and the soundings by wire of the *Meteor* expedition.

1. THERMOMETRIC METHOD OF DEPTH MEASUREMENT.

I. Historical Notes.

The thermometric method of depth measurement did not originate, like most other methods of sounding, from the needs of marine surveying or practical navigation, but is an outcome of the efforts made in scientific exploration of the sea to check the depth of reversal of reversing thermometers and of instruments for taking samples of sea water, in order to obtain the high order of accuracy required in the measurement of temperature and observation of salinity in the ocean deeps $(+0.01^{\circ}C \text{ and } + 0.02^{\circ})_{00}$ respectively). While in exploring the sea we have always attempted, by manœuvring the ship, to keep the angle of departure of the wire as small as possible in serial measurements of temperature and salinity, we have also taken more and more into account the fact that at times, through the drifting of instruments (e.g. in waters with strong currents), appreciable variations in temperature and salinity readings may arise from the fact that too great a depth is attributed to the measurements, namely the depth by wire (= length of wire run out). But owing to the lack of systematic research into the relationship between angle of wire and true depth, we have hitherto had to neglect this source of error completely in the exploration of the sea; and we have as a rule taken the length of wire run out as read from the counter, *i. e.* the *Solltiefe* or depth by wire, as being equal to the measured depth : in other words,

length of wire or Solltiefe (assumed depth) = true depth. D = W.

Isolated trials for checking the measured depth have been undertaken since 1906. They were based on the idea first propounded by RUPPIN (1906), of using simultaneously a reversing thermometer protected against pressure and alongside it a reversing thermometer not protected against pressure; and of obtaining, from the difference in level of the columns of mercury in the two instruments, a measure of the depth at which the reversing frame or the sampling bottle had reversed. Research on a vast scale, extending over the column of water comprised between 10 and 1,500 m. depth, was undertaken by BRENNECKE (1921), using this method, during the outward passage of the Deutschland in 1911/12; without however using the results obtained for correcting the serial measurements. A. SCHUMACHER (1923), on the other hand, developed the fundamental mathematical principles of this method in the form of an exact formula of correction, and of "auxiliary tables for the reversing thermometer with open protecting tube", and dealt also theoretically with the question of the accuracy of the thermometric method of depth measurement.

2. Open unprotected reversing Thermometers of the German Atlantic Expedition.

Armed with the experience acquired, A. MERZ, when the German Atlantic Expedition was in preparation, entrusted the firm of RICHTER & WIESE with

the construction of some unprotected reversing thermometers usable to a depth of 6,000 m. (3,280 fms.) with several new improvements on the models previously used (scale polished to a plane, visible point of

MODEL I,

usable to 6,000 m. (3,280 fms.) depth, graduated in fifths of a degree from -2° to $+60^{\circ}$, volume between 200° and 300°, accuracy of reading $\pm 0^{\circ}$ 02.

rupture, large loop in the stem, improved graduation). After many experiments the firm in question succeeded in making two new models which satisfied the required conditions (Fig. 1).

MODEL II,

usable to 2,000 m. (1,093 fms.) depth, graduated in tenths of a degree from -1° to $+30^{\circ}$, volume between 100° and 200°, accuracy of reading $\pm 0^{\circ}01$.

FIGURE 1.

Unprotected reversing thermometers (German Atlantic Expedition Pattern)

As in model I pressures reaching 600 atmospheres act directly upon the mercury reservoir and the stem, the construction of these instruments represents a remarkable technical performance. The thermometers were submitted to a severe test by the *Physikalisch-Technische Reichsanstalt*, to wit : (I) from the point of view of slight errors of graduation; (2) from that of the coefficient of pressure, *i.e.* of the rise in level of the mercury for each kg/cm² increase of pressure. These trials revealed the important fact that the coefficients of pressure vary but imperceptibly with the increase in pressure, or in other words each instrument has in practice a *pressure constant* valid without alteration over the whole range of the scale up to the limit of rupture. In



the instruments of the German Atlantic Expedition this pressure constant lies between 0.0750 and 0.1050, or a mean of 0.0900; *i. e.* on the average, the rise of the mercury is 0°09 per 10 m. (33 ft.) of water-pressure. The pressure constant of each instrument is determined to within about \pm 0.0005.

The correction of the readings of the unprotected thermometers follows from the formula deduced by A. SCHUMACHER:

$$C = \frac{(T + v_0) (Tw - t)}{6080} \cdot (1 + \frac{Tw - t}{6080})$$

where

- T = the reading of the *main* thermometer of the *unprotected* thermometer,
 - t = the reading of the *auxiliary* thermometer of the *unprotected* thermometer,
- v_0 = the volume of the quantity of mercury broken off up to the graduation 0°0 of the main *unprotected* thermometer.
- Tw = the true temperature (calculated from the readings of the *protected* thermometer).
- 6080 = the coefficient of apparent expansion of mercury in normal Jena glass.

The attached graphic table of corrections, which enables the required corrections C for all the current values of $T + v_0$ and Tw - t to be determined rapidly and with sufficient accuracy, was worked out from this formula (Plate I).

3. Method of taking observations, and calculation of true depth.

Two modern reversing thermometers, one protected against pressure, the other open and unprotected, are placed side by side in a double thermometer case mounted in a reversing frame or in a reversing water-sampling apparatus. By screw release or, better, by messengers, simultaneous release of both thermometers at the same level is obtained when the greatest depth has been reached (in soundings by wire, on reaching the bottom; in serial measurements, on reaching the depth of measurement), after a lapse of 5 to 10 minutes for the mercury to settle down. In the main thermometer of the protected thermometer, the mercury shows the true temperature of the depth examined. In the unprotected thermometer on the other hand, the mercury will reach a level which, in harmony with the pressure constant of the instrument, will be exactly proportional to the pressure, *i.e.* to the depth of water. Suppose the depth is 6,000 m. and the true temperature 2000; the unprotected reversing thermometer (with a pressure constant equal to 0.0900) will indicate in this case a temperature of $2.00 + \frac{0.09 \times 6,000}{10}$, or 56°00. On recovery, it is true, the level of the mercury will alter slightly in the main thermometers, and with the readings effected necessarily with a magnifying glass only rough values will be obtained of the true temperatures, or of the temperature of the unprotected instrument. But thanks to the instrumental temperature reading



PLATE I

taken from the auxiliary thermometer, we are able, by using a formula of correction (for unprotected thermometers we use the formula given below), to calculate the correction C which must be applied to the readings to obtain the true temperature of the depth, or the true height of the mercury in the unprotected thermometer (at the moment of reversal at the depth).

Let :

- Tw be the true temperature of the depth (*i. e.* the corrected reading of the protected reversing thermometer),
- Tu the true height of the unprotected reversing thermometer at the depth of reversal.

Then

$$\Delta t = Tu - Tw,$$

 Δt being the true rise of the mercury level in the unprotected thermometer at the moment of reversal in the depths. Further, let α be the pressure constant (*i. e.* the rise in level in the unprotected thermometer for an increase in pressure of $r \text{ kg/cm}^2$) and ρm the mean density of the column of water to be measured.

The thermometric depth required or the true depth W (independent of the length of wire run out and of the angle of the wire) is then obtained from the equation:

$$W = \frac{10}{\alpha. \rho m} \cdot \Delta t = Q \cdot \Delta t,$$

where $Q = \frac{10}{\alpha. \rho m} \cdot$

The pressure constant α is indicated to the 4th decimal place on the test certificate of each unprotected thermometer; the value of Δt is given us to two decimals by the readings of the two instruments (after applying all corrections). It thus only remains to determine the density ρm of the column of water in question, i. e. the mean density, taking account of temperature, salinity and pressure. If, as in oceanographical calculations, it were required to obtain values of ρm to the 5th decimal place, the determination of these values would be a very laborious affair, for it would be necessary for the calculation to have recourse to BJERKNES' hydrographic tables. But a calculation of the errors shows that it is quite sufficient, for columns of water of over 1,000 m., to calculate ρm to the nearest 5 units of the 4th decimal place, and for the next 1,000 m. we only need the 3rd decimal of pm. Within these limits of error we can take the distribution of the density in the sea as being constant. For the Atlantic Ocean it is thus quite sufficient to extract the values of ρm from the following table of mean distribution of density (Table I).

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HYDROGRAPHIC REVIEW.

TABLE I.

MEAN	DENSITY	\mathbf{OF}	COLUMNS	\mathbf{OF}	WATER	IN	THE	ATLANTIC	OCEAN.	

Column of Water.	Mean Density.	Column of Water.	Mean Density.
m		· m	
0 - 100	1,0262	0 - 2600	1.0336
0 - 200	267	0 - 2700	330
0 – 300	271	0 - 2800	341
0 - 400	275	0 - 2900	344
0 – 500	278	0 - 3000	346
0 - 600	1,0282	0 - 3100	1,0349
0 – 700	285	0 - 3200	351
o — 800	288	0 – 3300	353
o 900	291	0 - 3400	356
0 - 1000	294	0 – 3500	358
0 - 1100	1,0297	0 – 3600	1,0361
0 - 1200	300	0 - 3700	363
0 – 1300	302	o – 3800	366
0 – 1400	305	0 – 3900	368
0 - 1500	. 308	0 - 4000	370
0 - 1600	1,0310	0 - 4100	1,0373
0 – 1700	313	0 - 4200	375
0 – 1800	316	0 – 4300	377
0 - 1900	318	0 – 4400	380
0 - 2000	321	0 – 4500	383
0 - 2100	1,0323	0 - 4600	1,0385
0 - 2200	325	0 - 4700	387
0 – 2300	328	o – 4800	390
0 - 2400	331	o – 4900	392
0 - 2500	334	0 - 5000	395

TABLE 2.

THERMOMETRIC MEASUREMENT OF DEPTHS IN THE METEOR. SOUNDING STATION Nº 249.

Unprotected reversing thermometer N° 1437.	Protected reversing thermometer N° 1095.				
Length of wire to reversing frame = 5025 m. Temperature as read = 42.28° (27.5°) Reading + calibration cor- rection = 42.34° (27.5°) Temperature (at moment of reversal) $Tu = 41.22^{\circ}$	Length of wire to reversing frame = 5025 m. Temperature as read = 1.18° (27.8°) Reading + calibration cor- rection = 1.18° (27.5°) True temperature of depth Tw = 0.66°				
Elevation of level Pressure constant of instrument n° n Mean density of the column of water (o Depth of reversal determined thermo Distance, depth of reversal to driver Depth of the sea determined thermo	$\Delta t = Tu - Tw = 40.56^{\circ}$ $4437 \dots \alpha \dots = 0.0786$ $D - 5025 \text{ m.}) \rho m \dots = 1.0396$ Demetrically W \dots = 4970 m. Tube. = 65 m. metrically \dots = 5035 m.				
Depth of wire 5080 m. (for a 10° an The screw-release reversing frame w	gle of wire); depth by echo 5040 m.				

The screw-release reversing frame was fixed to the sounding wire 55 m. above the driver tube, and reversed on raising after a travel of 10 m. through the water.

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With the help of this table, and using the appropriate pressure coefficient, we can work out for each unprotected thermometer a new table for all columns of water (or, which is practically the same thing, for all lengths of wire), from which the values of the quotient Q can be extracted directly. Nothing else remains but to multiply this value Q by the rise of level Δt , to obtain the true depth W required.

For the Pacific and Indian Oceans, tables of the mean density of columns of water can also be prepared, the values of which do not differ appreciably from those of our table above. For secondary seas with large salinity anomalies, it is preferable to work out special tables of mean density. The method of summary calculation of thermometric depth indicated below seems to us to be the simplest and most easily understood for practical purposes. But it will be noticed that for the thermometric depth calculations of SUDA (1931) and GEISSLER (1931) we have given slightly different methods of calculation.

Let us illustrate the method of thermometric depth measurement by an example (Table 2).

The question now arises, with what degree of accuracy do we get the true depth by this thermometric method. The accuracy of the result depends on the errors of the three variables α , ρm and Δt . Adding the partial errors, the calculation furnishes the maximum and mean errors of thermometric depth measurement contained in Table 3.

TABLE 3.

LIMITS OF ERROR OF THE THERMOMETRIC DEPTH MEASUREMENTS.

Solltiete.	Total max	imum error.	Solltiefe.	Mean error.		
m	m %				%	
100 500 1000 2000 3000 5000	$ \pm 6 \pm 9 \pm 14 \pm 23 \pm 3^2 \pm 49 $	$\begin{array}{c} \pm & 6,0 \\ \pm & 1,8 \\ \pm & 1,4 \\ \pm & 1,1 \\ \pm & 1,1 \\ \pm & 1,0 \end{array}$	100 500 1000 2000 3000 5000	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	3,0 0,8 0,6 0,5 0,4 0,4	

In other words: The mean accuracy of the depths of reversal determined by thermometric depth measurement in the course of the German Atlantic Expedition was from 0.4 to 0.6 % for depths over 1,000 m. while between 100 and 1,000 m. its absolute value remained nearly constant and was \pm 5 m. in round numbers.

II. RESULTS OF THERMOMETRIC DEPTH MEASUREMENT WHEN SOUNDING BY WIRE.

The thermometric depth measurements made on the tropical profiles and

with the object, among other things, of checking soundings by wire, have not the same degree of accuracy as regularly taken serial measurements; firstly because the measurements were taken in a frame released not by messengers but by screws, and also because, to avoid the formation of kinks, the necessary 5 minutes "adapting time" for the thermometers was not observed.

The use of screw frames could not be avoided in sounding by wire, because, owing to the danger of the driver tube being carried away, we could not wait for the impact of the messengers. With release by screw, reversal on raising only took place, as a rule, after a travel through the water of about 10 m. But even after applying this correction, the result of the thermometric depth measurement in sounding by wire admits a further source of error, arising from the shortening of the "adapting time" (2 to 5 minutes). In unfavourable cases the difference of temperature Δt may on this account be much too small; and in summing the two sources of error, large inconsistancies may sometimes be produced in the values of the thermometric depth, as shown by the figures in brackets in Table 4.

TABLE 4.

SYNOPTIC TABLE OF THE THERMOMETRIC DEPTH MEASUREMENTS AT THE SOUNDING STATIONS.

- COLUMN 2. --- Solltiefe, i. e. length of wire from surface to reversing frame at the moment of touching bottom (thus the depth by wire diminished by the length of wire below the reversing frame).
- COLUMN 3. Temperature read off the protected reversing thermometers graduated in tenths of degrees.
- COLUMNS 4 & 5. Maker's number and corrected readings of the open unprotected reversing thermometers.
- COLUMN 6. Rise of level in the reversing thermometer unprotected against pressure, i. e. difference Δt between corrected readings of the protected and open reversing thermometers.
- COLUMN 7. Depth of reversal (measured depth) of the reversing frame calculated from the formula $W = \frac{10}{\alpha. \rho m}$. Δt . The measurements marked with an * are manifestly false, *i. e.* the tripping of the reversing frame did not occur at the nearest point to the bottom but at a lesser depth.
- COLUMN 8. Distance of reversing frame from driver tube, increased by 10 m. for travel through the water (on account of the delay in release by the screw); in other words, the distance of the measured depth from the bottom of the sea.
- COLUMNS 9 to 12. Depth of sea bottom by the three different methods of sounding. The values in brackets are obviously false measurements.

NOTE. — Measurements marked with an asterisk (*) are manifestly false, values in square brackets [] have been incorrectly read. Thermometric depths in brackets () must therefore not be used for determining the true depth of the bottom; the same applies to the depth by wire at Station 256 and the depth by echo at Stations 243, 288a, 290, 292 and 302.

Table	4.
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	1	2 Solltief 2	3 Protected	4 Unprote	5 CTED	6	7	8	9	10 Depth of	H	12
		(Length	THERMO- METER.	THERMO	ME1ER.		Thermo-				Mine	بالم ــــــــــــــــــــــــــــــــــــ
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$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	station.	reversing	Tempera-	Maker's	Tempe-	level.	measure-	-depth	metric	Echo	Angle	
No. m L1 m L5 L5 242 5116 2.21 1437 33.645 41.44 5082 50 5132 5169 0° 5156 243 4287 2.30 1437 37.01 34.71 4265 65 4330 (4105) 0° 4341 2443 1849 3.55* 1437 18.2** 14.66* 1812* 65 (1872) 1954 0° 3378 246 4934 0.70 1437 39.50 38.74 4755 65 4520 4888 0° 4878 250 0.66 1437 13.2 41.35 181 70 5151 5122 3° 5171 251 4683 0.77 1437 13.23 13.9971 65 2970 2794 0° 4202 252 2437 31.23 38.40 65 3905 30.4 3905 30.4 4564 10° <t< td=""><td></td><td>ffame)</td><td>ture.</td><td>IN</td><td>fature.</td><td>A</td><td>ment.</td><td>ment</td><td>aepin.</td><td>ueptu.</td><td>OI WITE</td><td>D.</td></t<>		ffame)	ture.	IN	fature.	A	ment.	ment	aepin.	ueptu.	OI WITE	D.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	No.	т	C° .				m		16	E.b		D8
			1									
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	242	5116	2.21	1437	43.645	41.44	5082	50	5132	5169	00	5156
	243	4287	2.30	1437	37.01	34.7I	4265	65	4330	(4195)	00	4342
	244	3371	2.47	1437	28.98	20.51	3204 1910*	50 65	(1872)	3378	200	3411
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	244a	1949	3.55*	1437	10.21*	14.00*	3008*	05 65	(1072)	7360	300	2004
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	245	4034	2.355	1437	20.59	28.74	4755	05 65	4820	4888	00	4989
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	240	5111	0.70	+457 1437	39.30 42.15	11.13	5081	70	5151	5122	30	5171
	240	5025	0.66	1437	41.22	40.56	4970	65	5035	5040	100	5080
	250	4913	0.87*	1437	37.78*	36.91*	4530*	65	(4595)	4985	0 ⁰	4968
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	251	4663	0.77	1437	[33.32]	[32.55]	[3997]	65	(4062)	4658	00	4718
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	252	2437	3.12	1437	22.00	18.88	2330	67	2397	2402	300	2494
	254	3953	2.34	1437	33.57	31.23	3840	65	3905	3992	00	4008
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	256	2921	2.82	1437	24.74	21.92	2705	65	2770	2794	00	(2976)
	257	4080	1.83	1437	34.38	32.55	4002	65	4067	4080	00	4135
	258	4514	1.08*	I437	35.85*	34.77*	4275*	60	(4335)	4564	100	4564
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	260	3456	2.51	1437	29.95	27.44	3380	65	3445	3513	5°	3511
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	201	2687	2.89	1437	24.16	21.28	2625	05	2690	2748	00 70	2742
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	202	3779	2.495	1437	32.30	29.01	4900	05 67	0700	0772	5°	0004 1507
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	203	4002	2.30	1437	30.10	35.74	4009	05 65	(5010)	5420	° 00	5447
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	204	5195	2.34	143/	42.74	40.42	4084*	65	(5040)	5949	T 5 ⁰	5180
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	205	4702	2.35	143/	42.99	37.84	4647	65	4712	4748	- J 00	4757
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	267	4190	2.36	1437	35.60	37.34	4097	65	4162	4216	7 ⁰	4245
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	268	2861	3.14*	1437	20.58*	17.44*	2155*	65	(2220)	2914	20	2916
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	271	3471	2.84*	1437	25.50*	22.66*	2795*	65	(2860)	3493	5°	3526
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	272	3666	2.98*	1437	24.52*	21.54*	2656*	55	(2711)	3657	00	3711
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	273	3293	2.82*	1437	25.64*	22.82*	2812*	55	(2867)	3268	20 ⁰	3338
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	274	2541	3.25*	1437	20.82*	17.57*	2171*	65	(2236)	2543	15°	2596
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	277a	3188	2.76*	1437	28.44*	24.68*	3042*	70	(3112)	3248	100	3248
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	286	2741	2.90	1437	24.54	21.64	2669	62	2731	2743	3°	2793
$"$ 3271 2.66 1437 29.07 26.41 3294 68 3322 3364 5° 3329 $288a$ 4303 2.08 1437 37.05 34.97 4300 64 4364 (4460) 5° 4357 $288b$ 4338 2.05 1437 37.40 35.35 4345 65 4410 4400 0° 4393 289 4896 1.77 1437 41.54 39.77 4881 68 4949 4843 10° 4954 290 4671 1.90 1437 39.91 38.01 4668 63 4731 (4562) 5° 3017 292 1083 4.71 1437 26.72 24.00 2959 63 3022 3024 5° 3017 292 1083 4.71 1437 34.31 32.03 3938 63 4001 3984 20° 4166 296 2398 3.26 1437 32.64 30.24 3722 65 3787 3710 0° 3814 297 3759 2.40 1437 32.64 30.24 3722 65 3787 3710 0° 3814 298 4126 2.22 1437 35.13 $3^{\circ}.01$ 4046 60 4106 4046 $0^{\circ} - 5^{\circ}$ 4176 299 4632 1.46 1437 38.95 37.49 4046 60 41	287	3361	2.65	I437	29.78	27.12	3340	64	3404	3364	30	3415
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	»	3271	2.66	1437	29.07	26.41	3254	68	3322	3364	50	3329 ADEM
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	288a	4303	2.08	1437	37.05	34.97	4000	67	4004	(4400)	5°	4007
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2800	4000	2.05	1437	37.40	35.35	4040	68	4410	4900	100	4050
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	209	4671	1.//	143/	20.01	38.01	4668	63	4731	(4562)	50	4724
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	201	2964	2.72	1437	26.72	24.00	2959	63	3022	3024	50	3017
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	202	1083	4.71	1437	13.43	8.72	1080	63	1143	(1020)	30	1136
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	294	4113	2.28	1437	34.31	32.03	3938	63	4001	3984	200	4166
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	296	2398	3.26	1437	22.16	18.90	2334	60	2394	2334	00	2448
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	297	3759	2.40	1437	32.64	30.24	3722	65	3787	3710	00	3814
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	»	3496	2.50	1437	30.57	28.07	3457	325	3782	3752	00	3811
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	298	4126	2,22	1437	35.13	32.91	4046	60	4106	4046	0° - 5°	4176
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	299	4632	1.46	1437	38.95	37.49	4605	64	4669	4677	00	4686
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	300	4717	1.52	1437	40.13	38.61	4740	63	4803	4666	00	4770
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	301	3501	2.57	1437	30.52	27.95	3441	55	3496	3444	00	0040
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	302	3574	2.50	1437	31.00	29.10	0000	04	3047	(3403) 9072		2000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	303	3931	2.40	1437	34.09	31.09	0000	05	0900 (4620)	1709	<u>ح</u> ا	4010
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	300	2010	2.305	1457	1 39.90	37.00	3004	25	3031	3028	±0	3034
	310	4125	2.43	1437	35.64	33.21	4083	25	4108	4140	5°	4140

.

In Table 4 we give a synoptic table of the thermometric depth measurements made at the 51 stations of profiles XI to XIV. To exclude the danger of collision with the tailing, the reversing frame was, as a general rule, secured to the latter at a distance of 50 to 55 m. (27 to 30 fms.) from the driver tube. This distance (increased by 10 m. on account of the delay in tripping by screw) must consequently be added to the depths of reversal obtained thermometrically, to obtain the thermometric depth of the bottom. A comparison of the bathymetric figures thus obtained with those furnished by the two other methods of sounding (by wire and by echo) shows that in 14 cases the thermometric depth was far too small, clearly because reversal did not take place at the point nearest the bottom but at a lesser depth. In 6 cases the result of the wire or the echo sounding is clearly in error.

There remain then 31 cases in which the depth of the sea was determined simultaneously and in impeccable fashion by all three methods. By suitable calculation of averages we obtain figures which enable us to form an idea of the sources of error in the three methods of sounding. The working up of the materials in this respect was done by Professor H. MAURER in Vol. II of the Meteor report (1933). While on the subject of this work we would mention the established fact that the depth of the sea as determined thermometrically must be increased by an average of 15 m. to obtain a value agreeing as closely as possible with the true depth of the sea. It even seems plausible that this systematic error may have a practically constant absolute value, *i. e.* that with the increase in depth of the sea it may diminish in percentage, given that the variations discussed above are independent of the length of wire run out. If we bear in mind the fact that in the soundings by wire the foremost question was that of obtaining bottom samples, and that for this reason we could hardly give much attention to the elimination of every source of error in the thermometric depth measurement, the results obtained may be considered to be good. The measurements have proved without fear of contradiction that thermometric depth measurement is an excellent method of checking the results obtained by other methods of sounding, and that by comparing the results with echo soundings it can furnish the means of undertaking systematic research into the true vertical velocity of sound in the sea. For, as we know, tables of reduction for echo soundings are based for the most part on theoretical formulae; direct measurements of the velocity of sound have hitherto been made but rarely, and usually only near the surface.

Such systematic investigations will enable us also to answer more truthfully than has been possible till now, the question of the accuracy of sounding by wire, and in particular of the magnitude of the error introduced by the angle of the wire. Our 31 cases are not sufficient for this purpose, and we are consequently reduced to seeking a rough solution of the question by taking our stand on the wire and echo soundings taken simultaneously at all the *Meteor's* sounding stations. This we shall now do.

III. RELATION BETWEEN DEPTH BY WIRE AND DEPTH BY ECHO FOR DIFFERENT ANGLES OF WIRE AT THE SOUNDING STATIONS.

Our investigations lead us to the important question of the sources of error in sounding by wire and by echo. It had generally been assumed until now in the exploration of the sea that the length of wire run out, read from the counter at the moment of touching bottom, agreed to within a few metres with the true depth. KRÜMMEL (1907) worked out, for example, the total mean error of a modern sounding at + 5 m. VON DRYGALSKI (1926) is much more sceptical, concluding that the "error in rough seas may reach 100 m. and more". The Meteor's simultaneous soundings by wire and echo show even greater differences, although when sounding the ship was always "manœuvred over the wire." The question arises whether these differences are due solely to the sources of error in the acoustic soundings, or whether they are principally caused by the errors of the wire soundings resulting from the deviation of the wire from the vertical. Some light can be shed upon this question by a statistical study of the differences which arose between the wire and echo soundings at 322 sounding stations of the Meteor. After eliminating the 7 false observations, I have grouped the remaining 315 depths obtained synchronously by wire and by echo according to the intervals of the angle of wire, and have calculated for these intervals mean values of the quotients depth by echo / depth by wire. The result is given in Table 5.

TABLE 5.

DEPENDENCE OF THE RATIO DEPTH BY ECHO / DEPTH OF WIRE ON ANGLE OF WIRE.

Angle of wire β	No. of cases.	Mean depth by wire (round figures).	Ratio Depth by echo / depth by wire v = Eb / Db	Difference with respect to v
$0^{0} - 4^{0}$	96	3500	0.993	$\begin{array}{c} \pm & 0.014 \\ \pm & 0.013 \\ \pm & 0.018 \\ \pm & 0.016 \\ \pm & 0.018 \\ \pm & 0.020 \\ \pm & 0.019 \\ \pm & 0.013 \\ \pm & 0.021 \end{array}$
$5^{0} - 9^{0}$	59	3650	0.993	
$10^{0} - 14^{0}$	54	3600	0.989	
$15^{0} - 19^{0}$	47	3050	0.982	
$20^{0} - 24^{0}$	25	2800	0.978	
$25^{0} - 29^{0}$	12	3400	0.972	
$30^{0} - 34^{0}$	9	3750	0.966	
$35^{0} - 39^{0}$	4	3500	(0.968)	
$4^{0} - 44^{0}$	9	3500	0.957	



Mean relation between quotient ∇ (echo sounding | wire sounding) and angle of wire β at the sounding stations of the German Atlantic Expedition.

The Table, as well as Fig. 2, shows that the relation between the quotient v and the angle of wire follows a definite law, viz: the depth by wire represents, more or less, a function of the angle of the wire. But if we calculate the mean departure of the single values from the mean values of the quotients, we find that the difference is fairly large; *i.e.* that there must still be a series of sources of error in the values of the quotient, engendered in part by the poor basis of comparison for the values of the angle of wire (I), and in part also by other errors in the two methods. A remarkable point is that the curve does not pass through zero, which means that even for an angle of wire of 0° the concordance in the results of the two methods is not, on the whole, perfect. This difference must be due to other sources of error in the methods, and a special study will be necessary to determine by what distribution of the errors these residual differences can be eliminated.

The first question which arises is to know by what factor of reduction the soundings by wire, taken with an angle of wire β , must be multiplied to reduce them to a zero angle of wire. To answer this, by obtaining the factor of reduction k required, we must make our curve of relation pass through zero, *i. e.* increase the values of v by 0.005. The values of the factor of reduction thus deduced are given in Table 6 for the different angles of wire.

⁽I) Measured with pendulum quadrant.

TABLE 6.

Angle of wire ß	k	1,000 (I- <i>k</i>)	Angle of wire β	k	1,000 (1-k)	Angle of wire B	k	I,000 (I- <i>k</i>)
0 1	1 000		308	0.085	ΤE	409	0.062	37
10	1.000	0	20	0.905	15	40	0.903	38
10	1.000		21	0.982	10	41	0.901	30
20	0.999	T	220	0.903		4-	0.901	10
3-	0.999		240	0.902	20	43	0.950	41
4° 50	, 0.999		250	0.070	21	44 15 ⁰	0.058	42
5° 69	0.990		260	0.979	22	45 469	0.057	43
79	0.990	2	270	0.970	22	40	0.957	43
/- 80	0.997	3	280	0.977	24	47	0.055	45
08	0.997	3	20	0.970	25	40	0.053	47
95	0.990	4	29	0.975	23	49	0.955	+/
100	0,996	4	300	0.974	26			
110	0.995	5	310	0.973	27			
120	0.994	6	320	0.972	28	ļ		1
130	0.993	7	330	0.971	29			
140	0.992	8	34°	0.970	30		1	
15°	0.000	10	350	0.968	32	1		
160	0.989	11	360	0.967	33	1		
17 ⁰	0.988	12	370	0.966	34			
180	0.987	13	380	0.965	35			
190	0.986	14	39°	0.964	36			

FACTOR OF REDUCTION & FOR SOUNDINGS BY WIRE TAKEN WITH ANGLE OF WIRE β .

With the aid of this factor of correction k we have reduced all the depths observed by wire to an angle of departure of 0°, and by this means have calculated the corrected depths by wire D_{b} . By eliminating the angle of wire we have indeed removed the principal source of error in sounding by wire, but not all the differences between the mean results of the three methods of sounding. For even with an angle of wire of oo, the soundings by wire must, taking the average of numerous cases, furnish a value somewhat in excess of the true depth; observing that the wire, owing to the variable drift, is not necessarily vertical, even when it is tautened while breaking out the driver tube. On the other hand, owing to the influence of the slope of the bottom, the mean values of the echo depth must have a tendency to furnish a slightly deficient value. These two sources of error must be added together, with the result that, even taking the mean of numerous cases, there remains a positive difference $D_k - E_b$. Professor H. MAURER found the figure 0.7 % for this difference, and reached the conclusion that, on an average, soundings by wire D_k corrected to 0° furnish a value about 0.4 % in excess and soundings by echo $E_{\rm b}$ a value deficient by about 0.3 %. In accordance with this distribution of the sources of error, we must then reduce to the true depth the results of the three methods of sounding, as follows:

Corrected	depth by wire	D,	=	0.996 D _k
Corrected	depth by echo	E_{\star}	=	1.003 E _b .
Corrected	thermometric depth	T_{\bullet}	=	$T_{\rm b} + 15.$

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We find the most probable value of the true depth by simply striking the mean, W = 1/3 $(D_v + E_v + T_v)$.

In Table 7 the mean ratios of the depth of bottom (*i. e.* depth observed by wire) and the true depth (*i. e.* depth by wire corrected to true depth), in sounding by wire, have been collected in synoptic form.

It transpires from the table that in 66 % of all the cases the angle of wire was less than 15°, and the error in depth was 1% or less of the length of wire. On the other hand, in 33% of all the cases the angle of wire was greater than 15°, and at the same time the error in depth rose to 1.5% and more, *i. e.* for a length of wire of 4,000 m. the sounding gave a depth of 60 m. or more in excess. In spite of manœuvring the ship continuously, the soundings by wire had to be taken in 7% of cases with an angle of wire of over 30°. In these unfavourable cases the error in depth reached more than 3%, *i. e.* the sounding by wire taken at about 4,000 m. gave depths in excess by 128 to 172 m. with angles of wire of this order. Plate II gives a graphical representation of the position taken up by the submerged wire (piano wire of 1/8 in. circumference (1 mm. diameter) weighted at its lower end by a sinker of about 66 lbs. (30 kgs.), for different angles of departure.

T.	AE	L	Ē	7

MEAN ERRORS OF DEPTH IN SOUNDINGS BY WIRE OF THE GERMAN ATLANTIC EXPEDITION FOR VARIOUS ANGLES OF DEPARTURE OF THE WIRE.

Depth by	L	Difference, Depth by Wire D_b — true depth D_v in metres for an angle of wire of								
wire D _b m	0°-4° (30 %)	5°-9° (19 %)	10 ⁰⁻¹⁴⁰ (17 %)	15°-19° (15 %)	20 ⁰ -24 ⁰ (8 %)	25°-29° (4 %)	30°-34° (3 %)	35°-39° (1 %)	40°-44° (3 % of all cases)	
200	I	I	2	3	4	5	6	8	9	
300	2	2	3	5	6	8	10	11	13	
400	2	3	4	6	8	11	13	15	17	
500	3	4	5	8	II	14	16	19	22	
600	3	4	6	9	13	16	19	23	26	
700	4	5	7	11	15	19	22	27	30	
800	4	6	8	12	17	22	26	30	34	
900	5	6	9	14	19	24	29	34	39	
1000	5	7	10	15	21	27	32	38	43	
1200	6	8	12	18	25	32	38	46	52	
1400	7	10	14	21	29	38	45	53	бо	
1600	8	II	16	24	34	43	51	61	69	
1800	9	13	18	27	38	49	58	68	77	
2000	10	14	20	30	42	54	64	76	86	
2250	11	16	23	34	47	61	72	86	97	
2500	13	18	25	38	53	68	80	95	108	
3000	15	21	30	45	63	81	96	114	129	
3500	18	25	35	53	74	95	112	133	151	
4000	20	28	40	60	84	108	128	152	172	
4500	23	32	45	68	95	122	144	171	194	
5000	25	35	50	75	105	135	160	190	215	
6000	30	42	60	96	126	162	192	228	258	

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It is claimed that the error in the result of the soundings is not nearly as considerable as one might expect from the angle of departure of the wire; in other words the wire, inclined at the surface, follows a much more nearly vertical path as it goes deeper.

While the error in the soundings by wire is appreciably smaller than, for example, in the serial measurements of which we are about to speak, in the present state of observational technique we cannot afford to neglect it. Both from the methodical point of view and for all delicate morphologic research, the reduction of soundings to the true depth seems necessary. The faculty of being always able to carry out thermometric depth measurements simultaneously with sounding by wire, furnishes the means of making this reduction in future with greater precision than has been attainable with the materials available hitherto.



PLATE II.

HYDROGRAPHIC REVIEW.

IV. RELATION BETWEEN DEPTH BY WIRE AND TRUE DEPTH IN SERIAL MEASUREMENTS FOR DIFFERENT ANGLES OF WIRE.

It is interesting to compare the dependence of the depth by wire on the angle of wire, as described above, with the results obtained during serial measurements. In the serial observations of temperature and salinity taken in the course of the German Atlantic Expedition, the true depth of reversal of the water-sampling bottles was determined at three points of each series, i.e. at 9 points at least of a vertical section extending from o to 4,000 m.; for a vertical section of this type was generally carried out in three series : o to 1,000 m.; 1,000 to 2,500 m.; 2,500 to 4,000 m. or bottom. During the actual work, 4 to 8 sample bottles were streamed each time, attached to the wire at intervals of 100 to 500 m. Reversal of the bottles and of the protected and unprotected thermometers in the serial observations was effected by messengers, after a lapse of 10 to 20 minutes for adaptation. The sources of error in the thermometric depth measurement, which appear when sounding by wire owing to the shortening of the lapse of time for adaptation and to the delay in reversal inherent in release by screw, were thus nonexistent. The results of thermometric depth measurement consequently give much more precise results in the serial observations, and on the average can be kept within the limits shown in Table 3 resulting from the partial errors of measurement of the temperature and the pressure coefficient.

The principle of thermometric depth measurement was thus used systematically in the serial observations at every station of the German Atlantic Expedition. Altogether the thermometric depth was observed in 2,400 cases, in round figures, at the 310 stations. These voluminous materials enable us to deduce a mean relationship between the true depth and the depth of the bottom, or depth by wire, for the different angles of departure of the wire, by the same method as was applied above for soundings by wire but with greater accuracy; they also enable us to find a solution for the following special case of the general problem : What curve in space is traced in the water by a sounding wire weighted at various points under the influence of current or drift of ship? A priori we must expect that, for the same angle, the departure of the wire from the vertical will be notably greater in serial measurements than in soundings by wire. For the soundings by wire were taken with a fine piano wire 1/8 in. in circumference (1 mm. diameter), weighted at its lower end only by a driver tube. In the serial measurements, on the other hand, we used a much stronger wire of 1/2 in. circumference (4 mm. diameter), to which from 6 to 10 bulky water bottles were invariably attached, and which offered more resistance to the water than the driver tubes.

Since in the above-mentioned shallow, medium and deep series the wire was weighted in different ways by the water bottles, a separate study was made in the *Meteor* report, Vol. IV, for the three series, as well as for the 3 water bottles in each series fitted with unprotected thermometers; but neglecting the measurements for depths between 0 and 500 m. on account of the limit of error of ± 5 m. in the thermometric depth measurement. If,



with the data of observation thus limited and grouped (1,002 measurements in 549 series), we calculate mean values of the quotients k (true depth / depth by wire), we again find that the ratio between angle of wire β and quotient k follows a definite law. It is shown that the error of depth in the serial measurements is abnormally great, and this on the whole almost invariably at the higher end of the series, while at the lower extremity the wire bends slightly (Plates II and III). Taking it by and large, we see that

HYDROGRAPHIC REVIEW.

the wire weighted with 6 to 10 water bottles assumes more or less the direction of the angle of departure of the wire, so that the error of depth is about proportional to the cosine of the angle of wire β . In absolute quantities, the mean error of depth for the three groups of serial measurements of the German Atlantic Expedition works out as follows:—

TABLE 8.

MEAN ERROR OF DEPTH IN THE SERIAL MEASUREMENTS OF THE GERMAN ATLANTIC EXPEDITION.

SERIES.	Solltiefe	Difference, Solltiefe — true depth in metres for an angle of wire of								
	m	0º - 4º	5° – 9°	100 - 140	15° – 19°	20 ⁰ – 24 ⁰	25° - 29°			
Highest	200	2 m	2 m	4 m	9 m	20 m	32 m			
-	300	3	3	7	13	31	49			
	400	4	4	9	17	41	65			
	500	5	5	11	22	51	81			
	600	5	5	13	26	61	97			
	700	6	6	15	29	71	113			
	800	6	7	17	34	82	130			
	900	6	8	19	38	92	146			
	1000	6	9	21	4 I	102	162			
Middle	1000	5	10	21	42	71	115			
	1200	6	12	25	49	80	137			
	1400	7	14	29	55	90	157			
	1600	8	17	34	59	98	178			
	1800	9	20	38	65	108	189			
	2000	9	22	42	70	120	200			
	2250	10	25	45	77	133	211			
	. 2500	10	28	50	83	148	220			
Lowest	2500	17	23	50	110	265	_			
	3000	18	30	60	117	306				
	3500	21	35	60	130	333				
	4000	24	44	61	140	352				
	4500	27	50	63	158	396				
-	5000	30	55	70	175	440				

It follows from this table that for angles of wire of 10° the mean error of depth already reaches values which cannot be neglected, and that for angles of wire of 20° it grows to enormous values. It is thus, for example, that for a length of wire of 4,000 m. and an angle of wire of 20° to 24°, the depth of the water bottles is found in fact to be reduced by 352 m. If we take the whole group of 1,002 observations, the points of the system of coordinates $K = f(\beta)$ are found to be nearly on the straight line given by the function $K = \cos \beta$ (Fig. 3). Averaging all these series, we obtain as a result the following mean factors of reduction for the depths by wire of

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Mean ratio between quotient k and angle of wire β in the serial observations of the German Atlantic Expedition and the single observations of the Deutschland Expedition.

the serial measurements, to which we have added the percentage of cases affected by the different intervals of angle of wire.

TABLE 9.

MEAN FACTORS OF REDUCTION FOR DEPTHS OF BOTTOM IN THE SERIAL OBSERVATIONS TAKEN WITH ANGLE OF WIRE β .

Angle of wire β .	0 ⁰ – 4 ⁰	5° – 9°	10 ⁰ – 14 ⁰	15° – 19°	20 ⁰ - 24 ⁰	25° – 29°
Percentage no. of cases.	32 %	29 %	23 %	9%	5 %	2 %
Factor of reduction	0.994	0.990	0.980	0.961	0.925	0.895

It is thus a question of applying very significant corrections to the series. If in about 60 % of these cases the correction to the depths is smaller than 1.5 %, it is as much the greater in the remaining 40 %; and in 16 % of all the cases (angle of wire greater than 15°) it becomes more than 4 %, in 7 % of all the cases more than 7.5 %, of the depth by wire. The mean of all the series gives an angle of wire of 8°.

In the foregoing considerations it has been a question of mean values. Taken by itself the error of depth may be less, but it may also be appreciably greater as the *Meteor's* observations show. The resulting errors in the value of temperature and salinity are often, in individual cases, notably larger than the accuracy of the temperature and salinity measurement. In unfavourable cases the values of the temperature may on this account be thrown out by as much as tenths of a degree and, for large vertical gradients, even whole degrees; and the values of salinity by tenths of units or even whole units (of 0.001). We can sum up by saying that the high degree of accuracy in temperature and salinity observations ($\pm 0.01^{\circ}$ and $\pm 0.02 \%$ respectively) required by modern sea exploration, and even claimed by it for years, is in fact attained with certainty only when the error of depth is eliminated from the observations by thermometric depth measurement.

The use of reversing thermometers and water bottles in serial observations is, apart from the serial measurements of the *Challenger* and *Gazelle* Expeditions, a thing of yesterday. Previous expeditions usually only streamed *one* water bottle at a time, suspended by a wire. In this case the error of depth is naturally much less, as we can verify from our scrutiny of the isolated observations taken by BRENNECKE in 1910-11 on the *Deutschland* Expedition (cf. the thin curve of Fig. 3).

V. SUMMARY.

I. Description of the thermometric method of depth measurement with protected and unprotected reversing thermometers, based on the experience acquired in the *Meteor* Expedition.

2. Discussion of the results of the thermometric depth measurements at the *Meteor's* sounding stations.

3. Deduction of a relationship, following a determined law, between the depth by wire and the true depth for different angles of wire. In soundings by wire it is found, taking the relation between the depths by echo and by wire as a basis, that the mean error in depth in two thirds of the cases is less than I % of the length of wire run out; it only assumes higher values, which may reach 4 %, for angles of wire above $I5^{\circ}$.

4. In serial measurements the submerged wire strays fairly considerably from the line of the angle of departure when average conditions are taken as a basis. The error of depth in serial measurements is roughly proportional to the cosine of the angle of the wire, and for angles of wire above 10° it attains values leading to considerable errors in the measurement of temperature and observation of salinity. 5. To sum up we can say that for serial oceanographical observations of temperature and salinity, thermometric depth measurement is an auxiliary which we can ill spare; for it alone is capable of ensuring the desired precision in the determination of temperature and salinity. Besides, it has proved an excellent method of check in dealing with the sources of error of the methods of sounding by wire and by echo. It would be desirable that systematic investigations should be undertaken in nautical surveys on the sources of error of the methods of sounding by wire and by echo, by taking soundings simultaneously by wire, by echo and by thermometric measurement in the circumstances the release of the reversing thermometers by messengers, and the precaution of leaving the thermometers a sufficient time to adapt themselves, are indicated.

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