

FEED-DOWN EFFECT IN DIPOLE ALIGNMENT

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Abstract

The field of strong super conducting magnets contains substantial multipole errors. An upper limit of their value is specified on the reference closed orbit. When the dipole is installed in a real machine, its axis cannot be exactly on the reference orbit, and “feed-down multipoles” are introduced. This paper describes an analytical approach to the alignment specification associated with this effect with an example from the LHC at CERN.

1 THE LHC DIPOLE

The LHC Dipole has unavoidable field shape imperfections. For some components of these field imperfections there is a spool piece corrector mounted at the end of the dipole to compensate the average value of the field error component. Every dipole has a sextupolar corrector and every second dipole has a combined octupolar/decapolar corrector. The usual expansion of the dipole field reads if we assume a two dimensional field along the dipole axis, x being the horizontal and y the vertical co-ordinate:

$$B_y + iB_x = B_{ref} \sum_{n=1}^{\infty} (b_n + ia_n) \left(\frac{x + iy}{R_{ref}} \right)^{n-1} \quad (1)$$

where, in European convention, $n=1$ identifies a dipole field $n=2$ a quadrupole etc. The a and the b indicate the skew and normal components of the field respectively, R_{ref} is the reference radius (17mm) for the LHC. The feed down harmonics due to (a_n, b_n) harmonics, can be calculated by changing x and y in the formula (1) into x_0+x and y_0+y respectively. Then the relevant monomials associated with a given order k are kept. We obtain:

$$b_k + ia_k = (b_n + ia_n) \left[\frac{(n-1)!}{(k-1)!(n-k)!} \right] \left(\frac{x_0 + iy_0}{R_{ref}} \right)^{n-k} \quad (2)$$

where k is the order of the feed-down multipole, with $k < n$.

Figure 1 illustrates the case when there is only one corrector (b_3). The dipole centre is displaced relative to the reference closed orbit by dz where the z -coordinate represents either the horizontal or the vertical displacement. dz_s is the misalignment of the corrector relative to the average dipole axis. dz_s has one contribution from the displacement of the corrector relative to the dipole axis and one contribution that originates from the pitch (yaw) of the dipole. For this configuration dz induces feed-down for components that are not compensated. For the compensated component the corrector misalignment ($dz-dz_s$) contributes with $-b_3$ and the dipole misalignment contributes with b_3 .

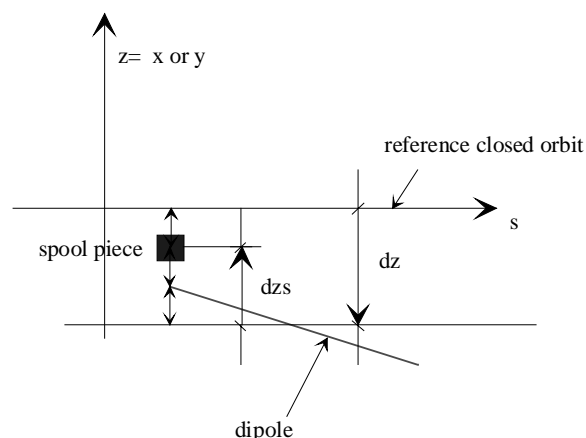


Figure 1: Configuration for a dipole with a field error corrector. dz_s is the displacement of the corrector relative to the average axis of the dipole, dz is the average displacement of the dipole.

For the case where every second dipole has a corrector, the corrector misalignment (dz_1-dz_s) contributes with $-2b_4$ or $-2b_5$ and the dipole misalignment dz_1 or dz_2 contributes with b_4 or b_5 . For the not compensated components the contribution comes from dz_1 and dz_2 for dipole 1 and dipole 2 respectively. The correctors have a random contribution of 2 times their value.

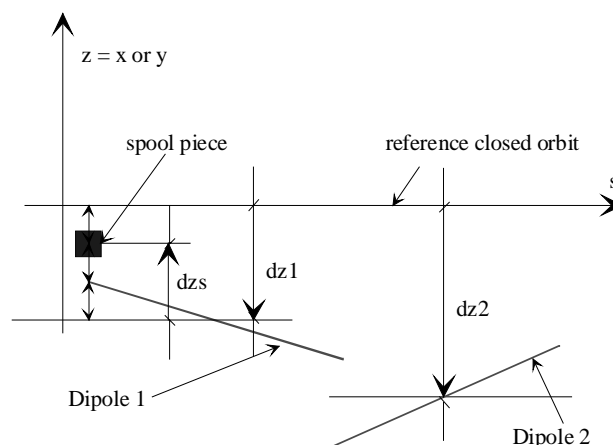


Figure 2: Configuration where one dipole out of two has a corrector.

2 DERIVATION OF EXPRESSIONS FOR ALIGNMENT TOLERANCES

From formula (2) follows with n-k=1, first order feed-down, dipole without corrector

$$-|b_{tol}| \leq (n-1)b_n \frac{dx}{R_{ref}} - (n-1)a_n \frac{dy}{R_{ref}} \leq |b_{tol}|$$

$$-|a_{tol}| \leq (n-1)a_n \frac{dx}{R_{ref}} + (n-1)b_n \frac{dy}{R_{ref}} \leq |a_{tol}|$$

where the suffix tol means tolerance. Solving this system gives

$$|dx| < \frac{|b_n b_{tol}| + |a_n a_{tol}|}{(b_n^2 + a_n^2)} \frac{R_{ref}}{(n-1)}$$

$$|dy| < \frac{|a_n b_{tol}| + |b_n a_{tol}|}{(b_n^2 + a_n^2)} \frac{R_{ref}}{(n-1)}$$

For the dipoles with corrector, the contribution from the misalignment of the dipole is dx_d and the contribution from the corrector is $(dx_s + dx_d)$ relative to the reference orbit (similarly in the direction of the y-co-ordinate)

$$b_{tol,d} + ia_{tol,d} = (b_n + ia_n)(dx_d + idy_d) \frac{(n-1)}{(R_{ref})}$$

$$b_{tol,s} + ia_{tol,s} = (-b_n)((dx_s + dx_d) + i(dy_s + dy_d)) \frac{(n-1)}{(R_{ref})}$$

this gives the following, which can be solved only with an assumption about the relation between dx_d and dx_s , which is set to αdx_d (the corrector tolerance is a fraction of the dipole tolerance), similarly for the y-direction, dy_s is set to βdy_d .

$$-|b_{tol}| \leq -(n-1)b_n \frac{dx_s}{R_{ref}} - (n-1)a_n \frac{dy_d}{R_{ref}} \leq |b_{tol}|$$

$$-|a_{tol}| \leq (n-1)a_n \frac{dx_d}{R_{ref}} - (n-1)b_n \frac{dy_s}{R_{ref}} \leq |a_{tol}|$$

Solving for dx_d and dy_d

$$|dx_d| < \frac{|\beta b_n b_{tol}| + |a_n a_{tol}|}{(\alpha \beta b_n^2 + a_n^2)} \frac{R_{ref}}{(n-1)}$$

$$|dy_d| < \frac{|a_n b_{tol}| + |\alpha b_n a_{tol}|}{(\alpha \beta b_n^2 + a_n^2)} \frac{R_{ref}}{(n-1)}$$

This is valid for systematic components and is the same for dipole with one or two correctors.

For the random effect we have to distinguish the dipole with and without corrector for the components b_4 and b_5 . Starting it over again, now scaling x and y by $R/(n-1)$, for simpler expressions

$$b_{tol} + ia_{tol} = (x + iy)(b_n + ia_n)$$

$$b_{tol} = xb_n - ya_n$$

$$a_{tol} = yb_n + xa_n$$

With x_{d1} and x_{d2} taken as the distance from the dipole 1 and 2 respectively from the closed orbit and $x_{s,p}$ as the distance of the spool piece from the dipole

$$b_{tol} = b_n(x_{d1} + x_{d2}) - a_n(y_{d1} + y_{d2}) - 2b_n(x_{d1} + x_s)$$

$$a_{tol} = b_n(y_{d1} + y_{d2}) + a_n(x_{d1} + x_{d2}) - 2b_n(y_{d1} + y_s)$$

$$b_{tol} = b_n(x_{d2} - x_{d1}) - a_n(y_{d1} + y_{d2}) - 2b_n x_s$$

$$a_{tol} = b_n(y_{d2} - y_{d1}) + a_n(x_{d1} + x_{d2}) - 2b_n y_s$$

If we assume the expectation values, b_n , a_n , x_1 , x_2 , y_1 , y_2 uncorrelated we get

$$b_{tol}^2 = b_n^2(x_{d2}^2 + x_{d1}^2) + a_n^2(y_{d1}^2 + y_{d2}^2) + 4b_n^2 x_s^2$$

$$a_{tol}^2 = b_n^2(y_{d1}^2 + y_{d2}^2) + a_n^2(x_{d1}^2 + x_{d2}^2) + 4b_n^2 y_s^2$$

$$b_{tol}^2 > 2b_n^2 \sigma_{xd}^2 + 2a_n^2 \sigma_{yd}^2 + 4b_n^2 \sigma_{xs}^2$$

$$a_{tol}^2 > 2b_n^2 \sigma_{yd}^2 + 2a_n^2 \sigma_{xd}^2 + 4b_n^2 \sigma_{ys}^2$$

The same relation between the misalignment of the corrector and the misalignment of the dipole as before, $dx_s + \alpha dx_d$ and $dy_s + \beta dy_d$

$$0 < 2b_n^2 \sigma_{xd}^2 (1 + 2\alpha^2) + 2a_n^2 \sigma_{yd}^2 < b_{tol}^2$$

$$0 < 2b_n^2 \sigma_{yd}^2 (1 + 2\beta^2) + 2a_n^2 \sigma_{xd}^2 < a_{tol}^2$$

this gives

$$\sigma_{xd} < \sqrt{\max\left[\frac{b_{tol}^2 b_n^2 (1 + 2\beta^2)}{D}, \frac{a_n^2 a_{tol}^2}{D}\right]}$$

$$\sigma_{yd} < \sqrt{\max\left[\frac{a_{tol}^2 b_n^2 (1 + 2\alpha^2)}{D}, \frac{a_n^2 b_{tol}^2}{D}\right]}$$

$$\text{with } D = 2b_n^4 (1 + 2\beta^2)(1 + 2\alpha^2) - a_n^4$$

For the case all dipoles have a spool piece the factor 2 goes away in front of α and β .

3 ESTABLISHING ALIGNMENT TOLERANCES FROM "BUDGET"

The errors have systematic, systematic per arc (uncertainty) and random error components. Only systematic errors combine to contribute to the systematic alignment budget. For the random budget we use the following value of the components causing feed-down

$$b_n = \sqrt{b_{n,sys}^2 + b_{n,unc}^2 + b_{n,ran}^2}$$

$$a_n = \sqrt{a_{n,sys}^2 + a_{n,unc}^2 + a_{n,ran}^2}$$

Table 1: Summary of feed down budget

n	2	3	4	5
Feed down effect	dipole: closed orbit	quadrupole: β beat	sextupole: resonances, Q'	octupole: anharmonicities Q''
Tolerable systematic a_{n-1}	10% of dipole (0.5u)	$1/\sqrt{8}$ unc. (0.3u)	$1/\sqrt{8}$ unc. (0.3u)	$1/\sqrt{8}$ unc. (0.19u)
Tolerable systematic b_{n-1}	10% of dipole (0.5u)	$1/\sqrt{8}$ unc. (0.3u)	1u	0.07u (Q'')
Tolerable random a_{n-1}	14 % of random in dipole (1.0u)	10% of coupling (0.8u)	10% of increase =46% of total (0.2u)	10% of increase =46% of total (0.3u)
Tolerable random b_{n-1}	14 % of random in dipole (1.0u)	7 % β beat (0.36u)	10% of increase =46% of total (0.7u)	10% of increase =46% of total (0.3u)

For each multipole we set up a budget for the feed-down harmonic $n-1$ for systematic, uncertainty and random errors separately, for both random and skew components. From this budget we calculate systematic, and random parts of the tolerated alignment. It is checked that second-order ($n-2$) contributions can be ignored.

The table of field imperfections used is the "9901" table. It gives values of the field components expressed in units (u) of 10^{-4} relative to the main field.

Table 1 gives the summary of the budget for calculation of the tolerances. For $n=2$ the feed down component is only a dipolar effect. Random b_1 and a_1 allowed is 14 % of random b_1 and a_1 in the field table, which corresponds to 1% of aperture budget, i.e. noise.

For the calculation of the systematic feed-down from a_3/b_3 we do not take the value for the a_3 and b_3 , which are too small, from the error table but the value is divided by $\sqrt{8}$ (random distribution over the 8 arcs) which gives 0.3. For the a_2/b_2 budget (feed down from a_3/b_3) a tune shift or coupling coefficient of 0.03 has to be accommodated. A β -beating of 7% gives us a random b_2 of 0.36. As random a_2 , an increase of the random component of 10% (allowed by the correction system) is taken which gives 46% of the a_2 in the field table.

For the systematic a_4/b_4 feed-down the values in the field table is divided by $\sqrt{8}$ (same argument as for a_3/b_3). The systematic and uncertainty for the feed-down budget are taken as 10% of the a_3/b_3 components in the field table and the random a_3/b_3 are taken as 46% of the random components (increases the random component by 10%).

For the a_5/b_5 feed down we take the values of a_5/b_5 from the table. The Q'' budget requires the systematic b_4 to be less than 0.1. If we assume that the systematic and the uncertainty errors of the field contribute equally

$$\sqrt{b_{4s}^2 + \langle b_{4u} \rangle^2} = 0.1u$$

then the systematic b_4 is $0.1/\sqrt{2} = 0.07u$. The systematic a_4 is set to the rms of the acceptable uncertainty which gives $0.55/\sqrt{8} = 0.19$. The b_4 uncertainty is taken as $0.1/\sqrt{2} \cdot \sqrt{8} = 0.2u$. The a_4 uncertainty is defined by the dynamic aperture and is 0.55u.

The random b_4/a_4 is taken as 46% of the random component of b_4 , i.e. it increases the random component by 10%.

For a_6/b_6 and a_7/b_7 feed down the budget is supposed to be 10% of the allowed component in the error table except for the a_5 and a_6 budget where the value is supposed to be of the same order as in the error table.

4 SUMMING UP RESULTS

Using the formulas above with the established budget, taking the most constraining misalignment for the dipole itself and for the b_3 , b_4 , and b_5 correctors separately, gives the result shown in Table 2. For the dipole itself the misalignment in the x-direction is limited by the contribution from the b_3 multipole feed down and for the y-direction the b_3 and the b_5 are the most constraining. The misalignments of each spool piece corrector are taken relative to the dipole average axis.

	SUMMARY	
	Systematic	Random (rms)
dx, dipole (b_3)	0.14	0.29
dy, dipole (b_3)	0.14	0.93
dy, dipole (b_5)	1.6	0.42
dx, b_3 -corrector	0.09	0.18
dy, b_3 -corrector	0.09	0.61
dx, b_4 -corrector	31.9	1.9
dy, b_4 -corrector	20.1	1.6
dx, b_5 -corrector	0.41	0.35
dy, b_5 -corrector	1.07	0.28

Table 2: Summary of the alignment tolerances in mm for the dipole (w.r.t. reference c.o.) and the correctors (w.r.t. the dipole axis).

The random alignment tolerance of the b_3 spool piece of 0.18 mm is probably not achievable. A complete aperture balance has to be remade (the β beating budget has to be re-evaluated). The random tolerance of 0.29 mm for the dipole is smaller than the r.m.s. closed orbit distribution and this would also imply a revision of the aperture budget. For the b_5 corrector the tolerance is pessimistic as the effect of random a_4/b_4 on dynamic aperture is probably negligible (should be evaluated).

5 REFERENCES

- [1] LHC Alignment Workshop, CERN Dec. 2000, <http://wwwslap.cern.ch/~vrd/aplaw/page.html>